

Reactor Containment Building Integrated Leak Rate Test

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Abstract

This report presents details of the Containment Integrated Leakrate Test successfully performed between June 15 and 20, 1980 at Zion Station, Unit 2. The test was performed in accordance with 10CFR50, Appendix J and the Zion Technical Specifications.

The containment integrated leakrate was found to be 0.007 weight %/day at a test pressure of 28 psig, well within the 0.0465 weight %/day acceptance criteria. The result at the 95% upper confidence limit was 0.019 weight %/day.

A leak of 0.036 weight %/day was imposed on the containment for the supplemental verification test. The instrumentation measured a combined leak of 0.053 weight %/day and 0.064 weight %/day at the 95% upper confidence limit. The difference between the measured combined leak and the imposed plus measured containment leak is 16% of the allowable containment leakrate. The acceptance criteria is that the difference be less than 25%. Thus, the supplemental verification test also meets the acceptance criteria.

Analysis and Interpretation of Type A Test Results

The statistical leakrate was scattered during the first 5 or 6 hours of the test due to the small number of data sets accumulated. The data started falling into place between the 7th and 8th hour of the test. The slope of the leakrate began to flatten out between the 9th and 10th hour of the test. (Event 1 graph 1) Therefore, it was concluded there was a leak out of the containment.

A few hours later the leak in the outer equalizing valve of the personnel air lock was discovered and plugged with a plumbers plug. (Event 2 graph 1) The slope of the leakrate dropped shortly thereafter. Two hours later, the leak in the escape hatch inner equalizing valve was discovered and stopped. (Event 3 graph 1) The leakrate continued to drop. Other points of suspected leakage were checked, but nothing was found leaking.

It was decided to begin a new "24-hour" ILRT when the escape hatch leak was stopped. It was started at data set 122 and graph 1-a was initiated. The leakrate dropped below the limit within 1½ hours and went negative two hours into the test. (Event 1 graph 1a) Then the plumbers plug was removed from the personnel hatch equalizing valve to see what effect it would have on the leakrate. (Event 2 graph 1a) As seen on the graph, the leakrate increased and was above the limit within 45 minutes. Six hours into the new test the plug was reinstalled. (Event 3 graph 1a) The leakrate turned around and was below the limit at 8.5 test hours. The leakrate continued to drop and was negative again at 9.5 test hours.

It was evident that the containment was experiencing some sort of mass addition which resulted in a negative leakrate. The sealing water supply between valve AOV-RV0005 and AOV-RV0006 was thought to be the source of the mass addition. The water supply was isolated to these valves at 14 hours test time. (Event 4 graph 1a) The leakrate turned towards a positive number again. Another new "24 hour" test was begun at this event.

Graph 1b is a plot of the final and successful ILRT. Eleven hours into the new test, constant leakrate results were appearing. The test was continued for one more hour to confirm the results being obtained. The test was terminated at hour 12 test time. Since the test had already been running much longer than 24 hours, the requirement to keep the containment pressurized longer than 24 hours had already been met.

Twelve hours of data were sufficient to determine the leakrate of the containment.

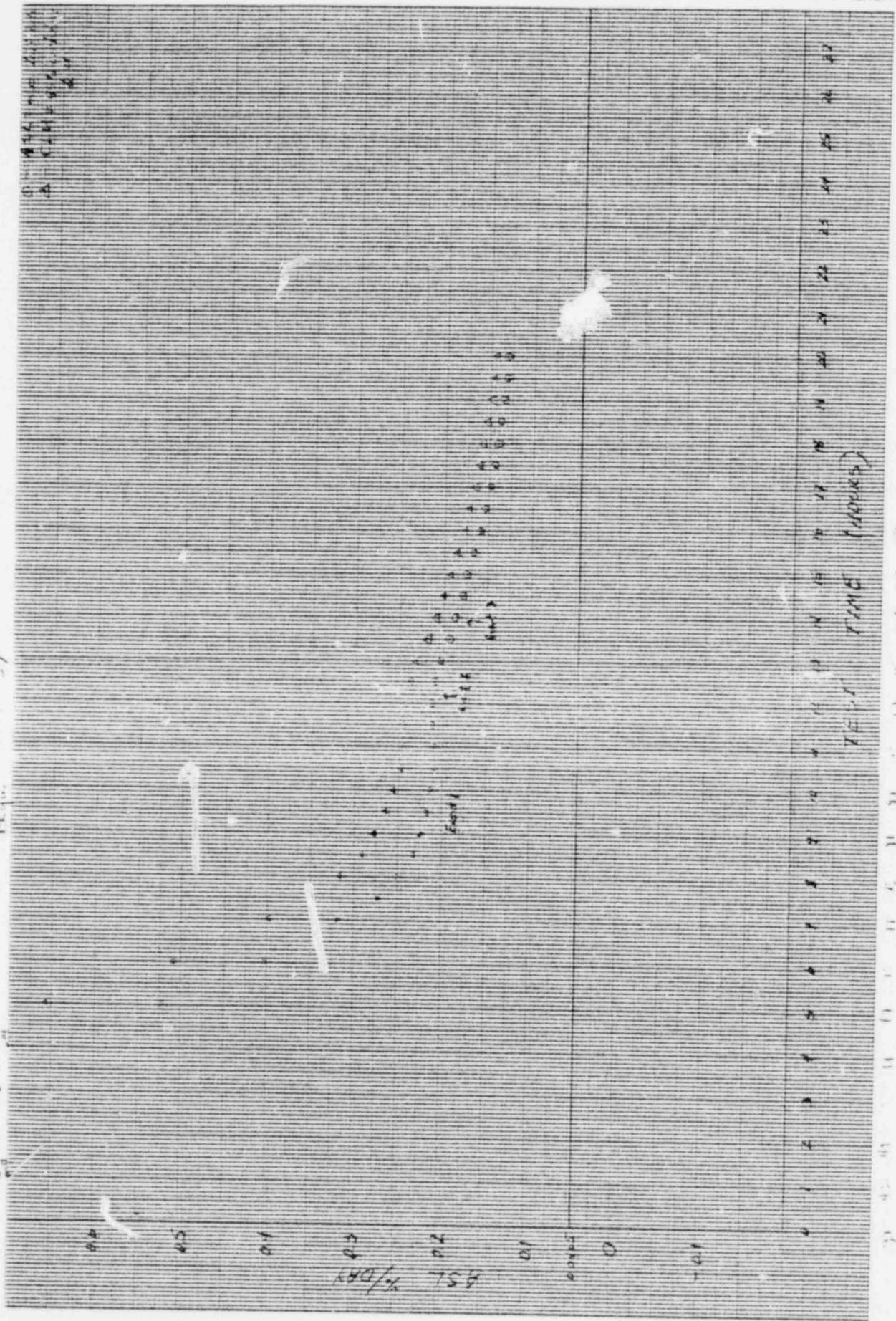
The water leakage past valve AOV-RV0005 was the source of the negative leak during the test. The volume between valves AOV-RV0005 and AOV-RV0006 was pressure tested during TSS 47 (IVSW Leak Test) with water and with air during a special IVSW test before the ILRT. Both tests indicated only a small amount of leakage past these valves. The containment leakrate was so small that the small amount of water leakage past AOV-RV0005 into the containment had a large effect on the test results.

The Zion Unit 2 containment has a very small integrated leakrate. The leakrate measured during this test is nearly seven times less than the allowable leakage of the containment. When compared with the results of the last ILRT performed in February of 1977, the leakrate measured during this test is only .002% greater than the results of the previous test. It can be concluded that the U-2 containment has maintained its leaktight condition over the past 3 years.

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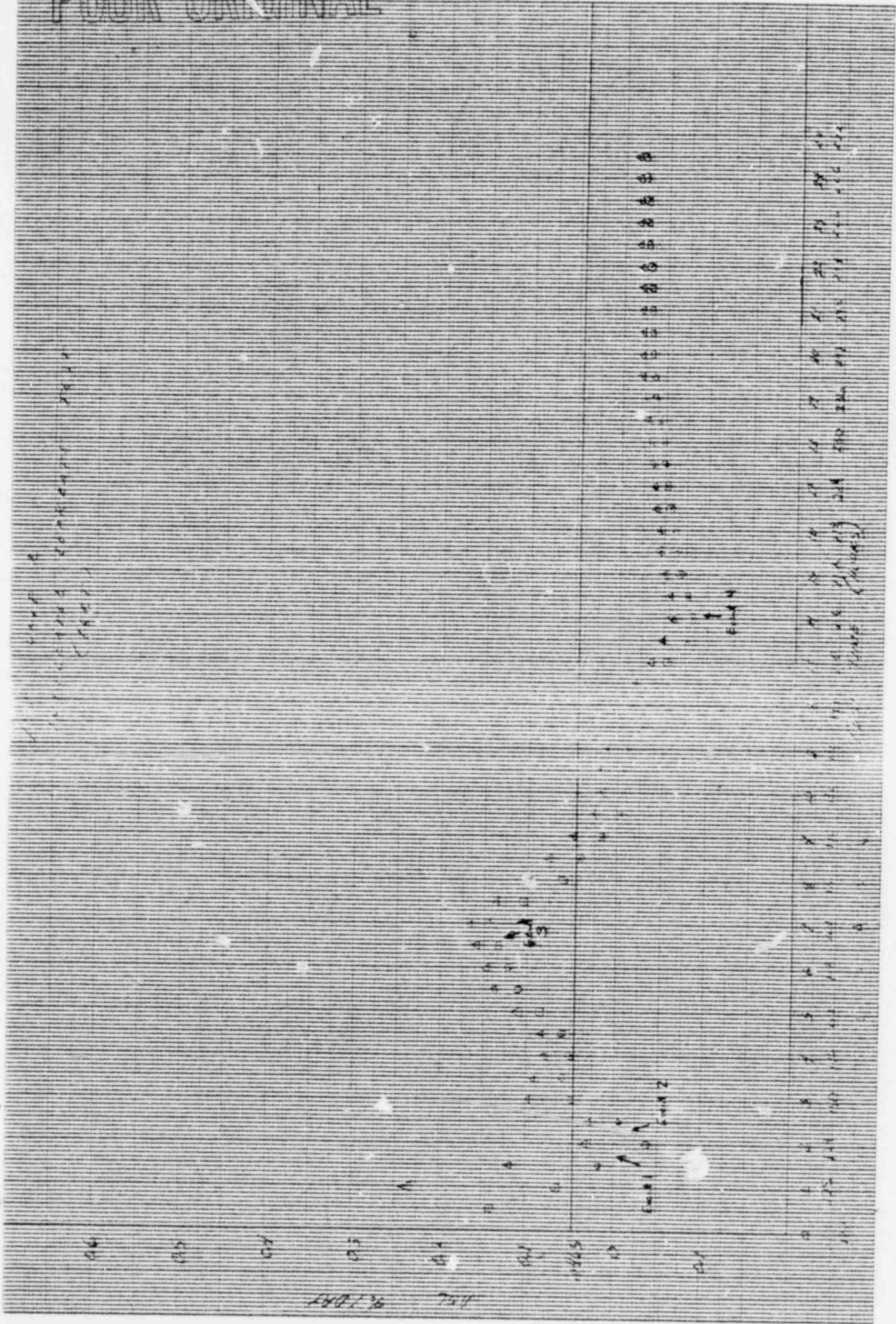
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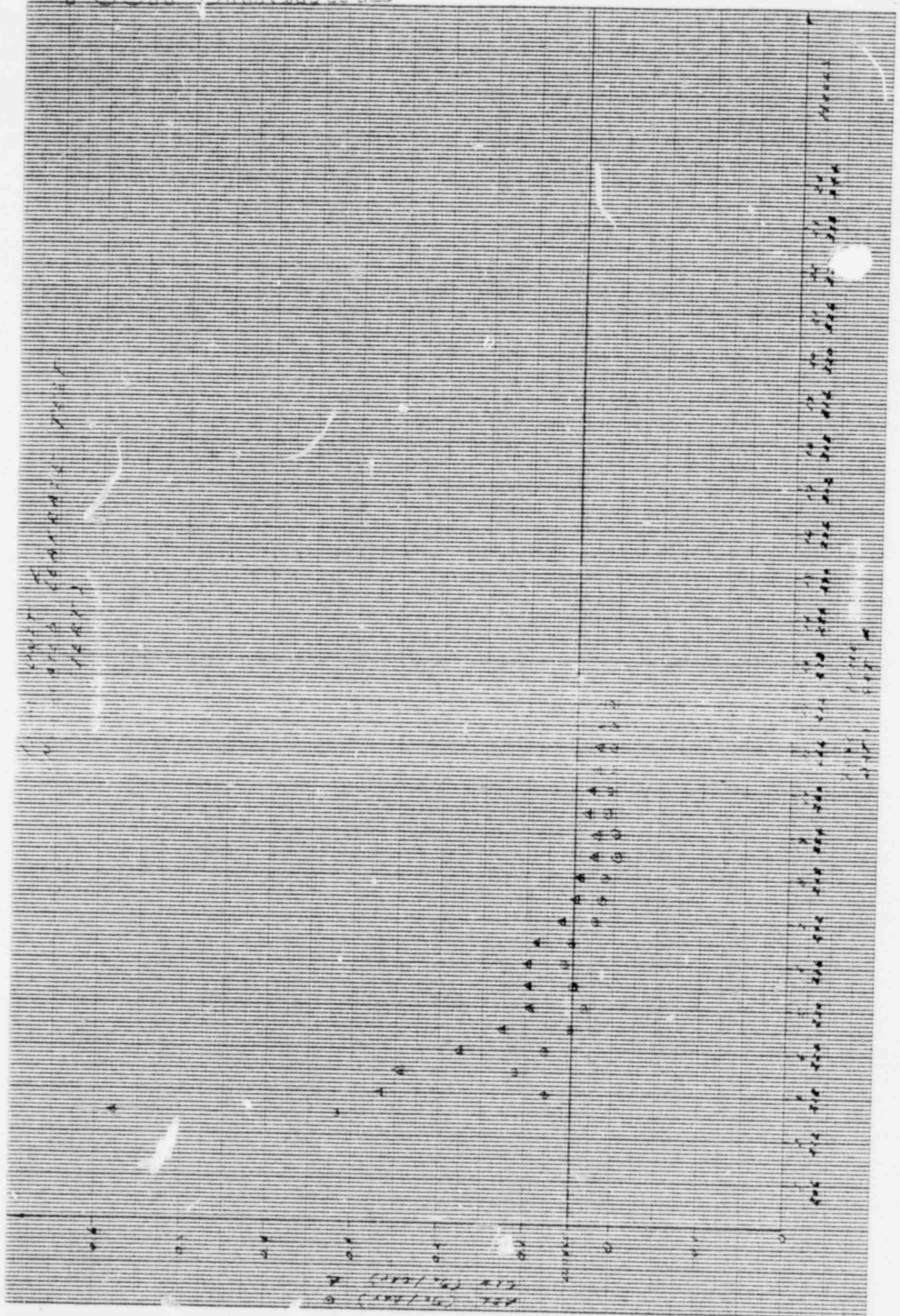


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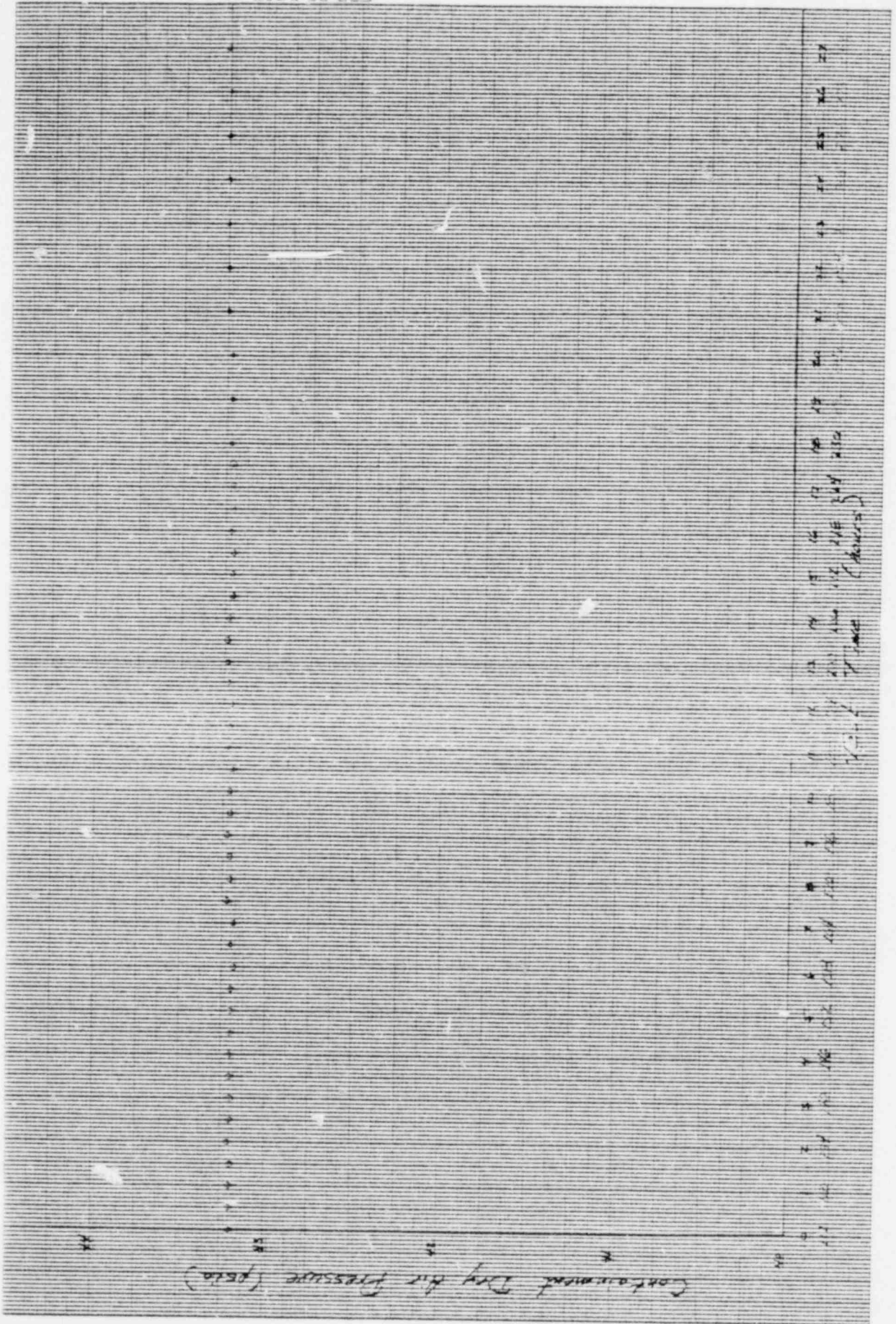
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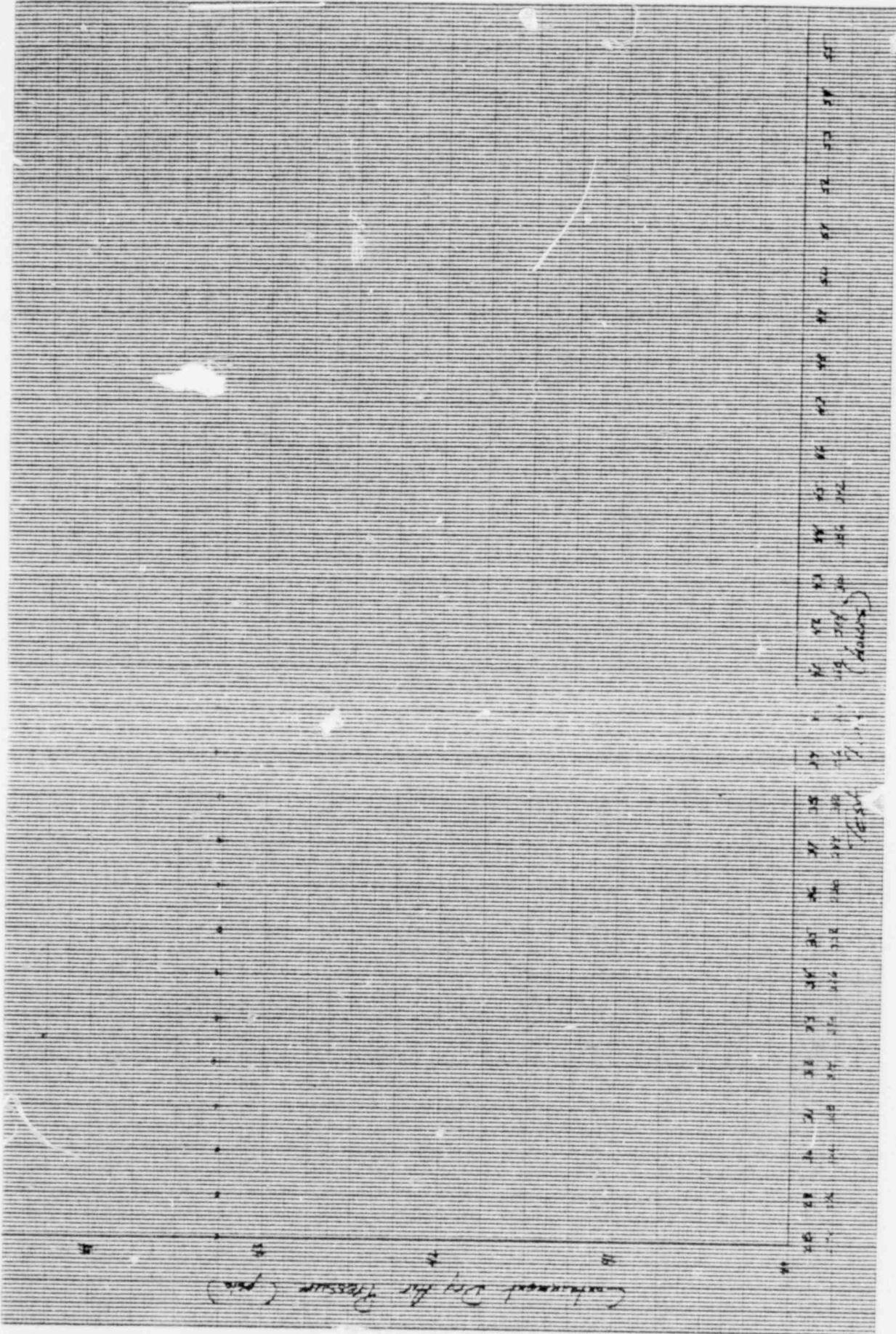
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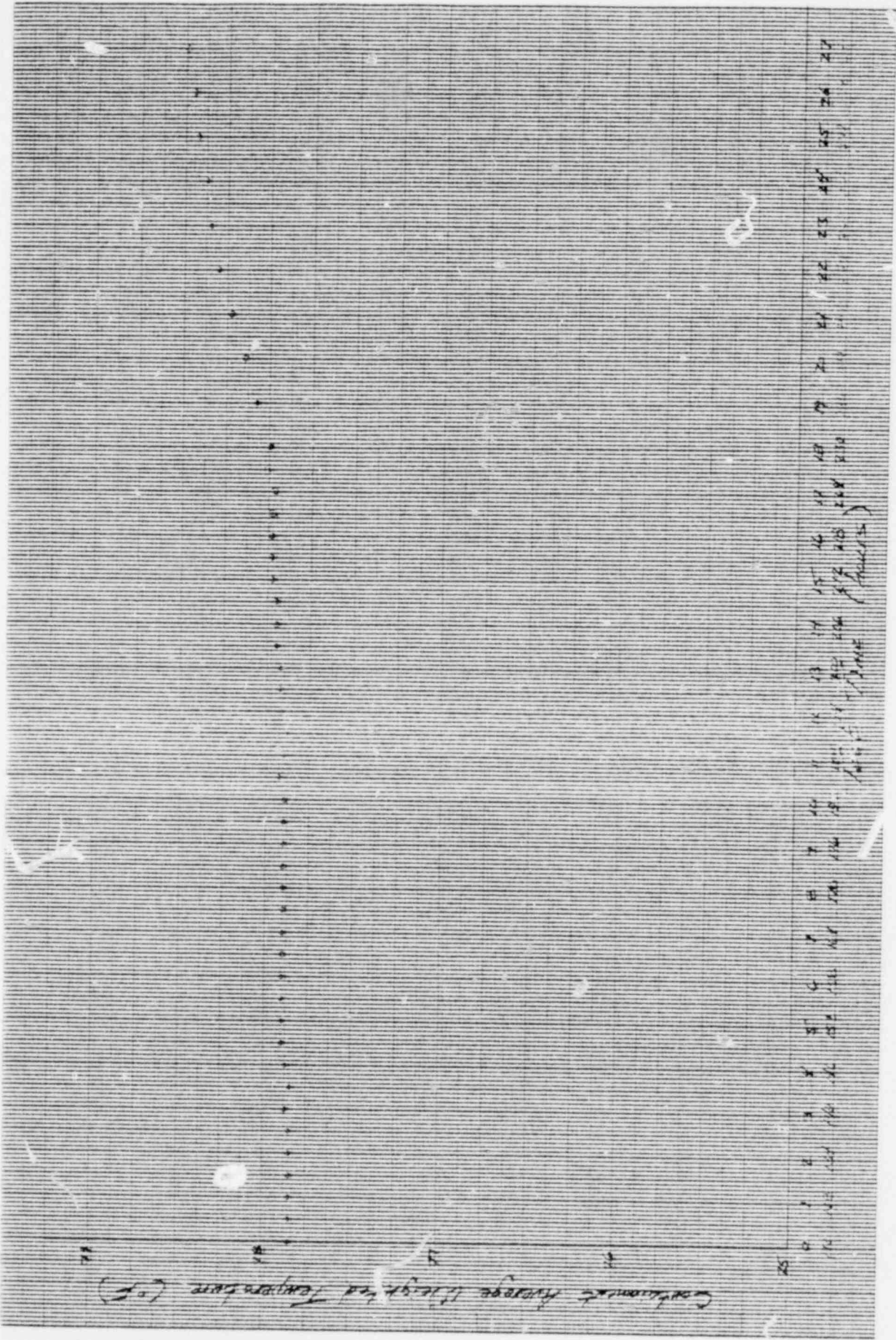
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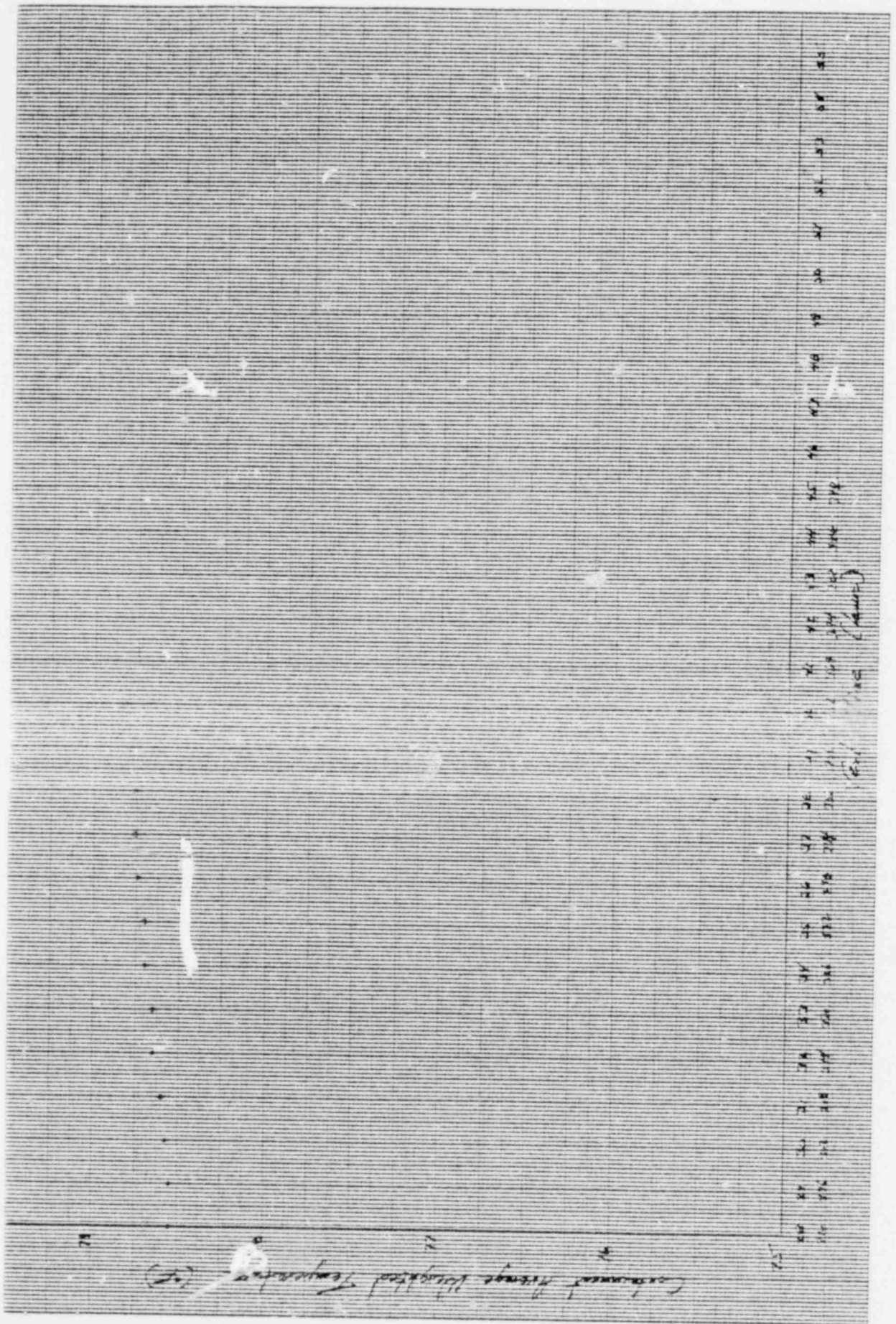
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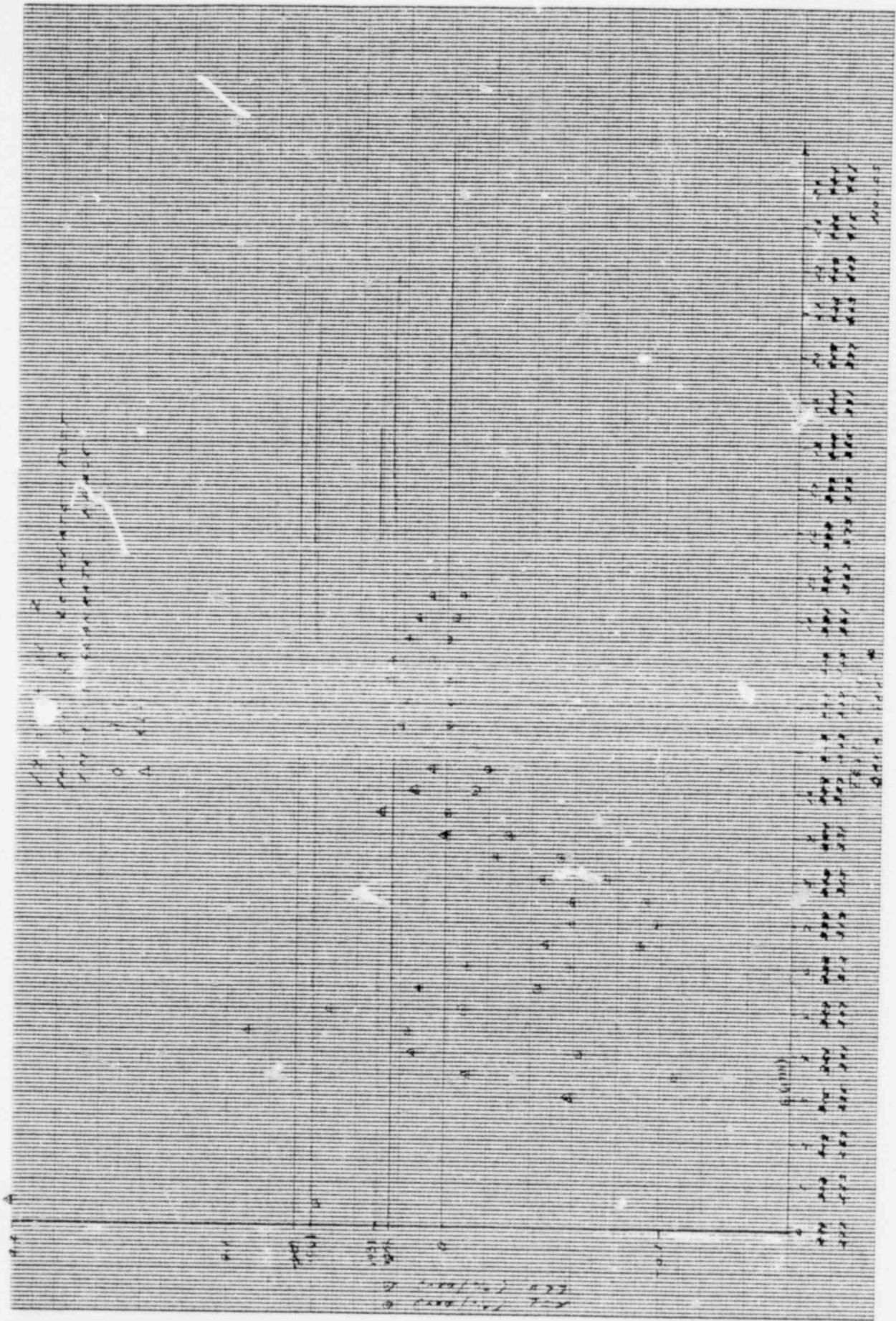
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Analysis and Interpretation of Supplemental
Verification Test Results

A 2.0 scfm leak (.036%/day) as measured by the rotometer was imposed on the containment. The leakrate plot obtained during the first 10.5 hours of this test was scattered in and out of the acceptable tolerance band for no apparent reason. Nothing else was changing during this time. When the raw data was looked at closer, it was evident that positive and negative pressure spikes on the order of 15 to 20 counts were occurring on the precision pressure gauges. These spikes, noticed on the output tapes from the DAS, were occurring at random intervals during this test. This caused the containment dry air mass calculation to change significantly. The oscillation in the leakrate results, as shown on graph 4, were caused by the pressure gauge problem.

The cause for the pressure gauge problems is not known, but water droplets which might have formed in the sensing line may have entered the quartz bourdon tube capsule to cause the problem. As soon as the problem was discovered the pressure standard used to calibrate the precision pressure gauges was connected to a containment pressure sensing line.

A new supplemental verification test was begun at data set 340 (graph 4a) using the pressure standard instead of the 2 gauges. Eight hours later, successful results were obtained and the test was terminated at 8.33 test hours. The successful results of this test demonstrate the validity of the leakage rate test measurements.

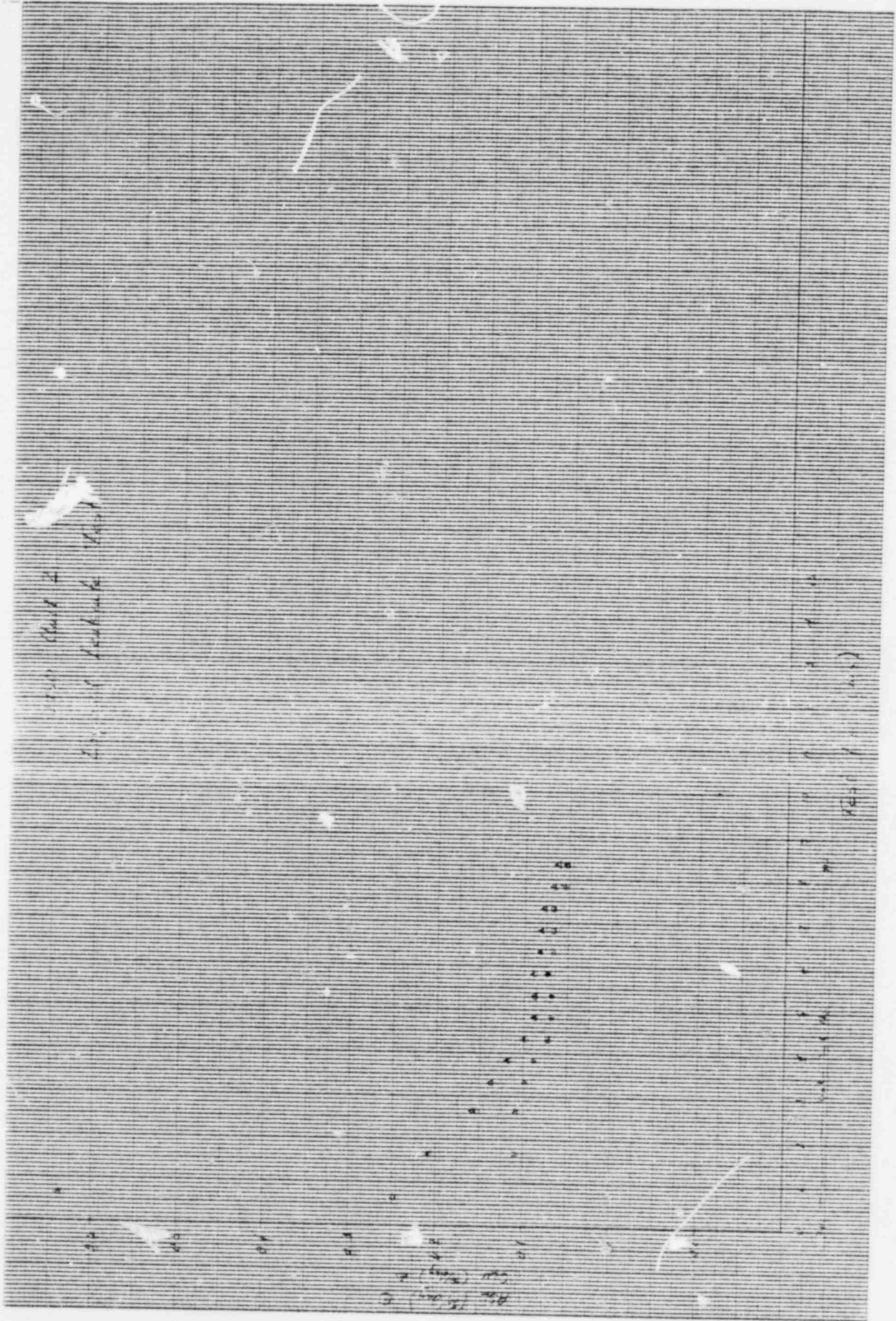


DATE: 10 MAR 1960, 6-18-80

POOR ORIGINAL

NO. 3410-110, DIEZEL ENGINE PARTS
10 X 10 PER HALF INCH

DIEZEL ENGINE PARTS
MADE IN U.S.A.



Handwritten notes in the upper left quadrant of the grid area.

Handwritten notes in the middle right area of the grid.

Vertical handwritten text or markings in the lower middle section of the grid.

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POOR ORIGINAL

Test Log for
U-2 Containment ILRT
6-15-80 - 6-20-80

Sunday, 6-15-80

- 1700 Valve line-ups completed. Procedure signed off.
2030 Attempted to start both compressors. Had oil pump problems.

Monday, 6-16-80

- 0030 Started West compressor. Attempted start on east compressor, 4KV breaker problem, compressor tripped. Contacted OAD, will check problem in AM since 4KV feed is common to both compressors.
0045 Discovered RV0008 leaking thru, spinning purge exhaust fans backwards. Cranked down on valve, but still leaks.
0200 Received fire detection alarms in the containment. Containment pressure \approx 2 psig.
0330 Filled pressurizer from 38% \rightarrow 70%. Partial clear done on seal injection and normal charging to fill it.
0830 Other compressor started.
0930 Both compressors tripped on 2nd stage temperature high.
1130 Discovered AOV-RV0005,6 went closed, dead heading the compressors. The fuses to some containment isolation valves were mistakenly pulled and that affected RV0005 & 6 (fail close valves).
1300 Both compressors started again.
1930 East compressor tripped due to low N₂ pressure.
2000 East compressor back on.
2130 Containment at 41 psia. Filled pressurizer again.
2145 B RCFC tripped. Decided to leave it off.
2215 Stopped compressors. Containment at 43 psia.
2340 Containment sample completed per test procedure.

Tuesday, 6-17-80

0315 Found multiplexer cable penetration leaking.

0630 Outer airlock door closed. Airlock equalized with containment pressure.

1600 Determined from accumulated data that there is a leak out of the containment. Began referencing systematic troubleshooting procedure to check for location of leak.

1630 Checked personnel hatch outer cable penetration and equalizing valve. The penetration was okay. The equalizing valve didn't appear to be leaking any more than when the test was started. Measured leak still greater than allowed.

1715 Checked water pressure between RV0005,6. Pressure okay.

1900 Decided to try to stop leak in personnel hatch outer equalizing valve.

1915 A plumbers plug was placed in the discharge part of the outer equalizing valve to stop the leak. It worked.

1930 Increased water pressure between RV0005,6. It had fallen to 15 psig.

2000 Isolated 2VC8405 (letdown).
Checked main steam line pressure gauges, no leakage. Found very small leak in IW header (IW21).

2015 Snoopd outer personnel airlock, no leakage.

2055 Snoopd escape lock. Found a large leak in the escape lock inner equalizing valve. Closed the outer escape lock door and equalized the airlock with the containment pressure.

2100-2300 Checking other points of suspected leakage. Found nothing leaking.

2300 Containment leakrate below limit.

2330 Plumbers plug was removed from the outer personnel airlock equalizing valve.

Wednesday, 6-18-80

0130 Containment leakrate increasing above limit.
 0330 Re-installed plumbers plug.
 0530 Containment leakrate below limit.
 0630 Containment leakrate negative.
 1130 Shut off water supply between AOV-RV0005,6.
 1145 Containment leakrate turning around towards positive. Started new "24 hour" ILRT.
 2140 ILRT terminated. Acceptance criteria met. Average statistical leakrate (ASL) = 0.007 %/day. Upper confidence limit leakrate (CLU) = .019 %/day.
 2220 Obtained containment air sample per procedure.
 2230 Imposed a 2.00 scfm leak (0.036 %/day) on the containment for the supplemental verification test.

Thursday, 6-19-80

0500 Observed problems with precision pressure gauges.
 0830 Installed pressure standard for precision pressure gauges on third containment pressure sensing line.
 0930 Started new supplemental verification test using pressure standard.
 1750 Terminated supplemental verification test. Acceptance criteria met.
 1800 Performing valve line-up necessary for stroking Recirc. Sump valves MOV-SI8811 A, B.
 1900 Stroked recirc. sump valves successfully. Performed release calculation for blowdown of containment. (1.06×10^8 ft³/min. maximum release rate)
 2000 Performing valve line-up for containment blowdown.
 2145 Began containment blowdown.

Friday, 6-20-80

0600 Blowdown completed .
 0630 Entered containment for post-test inspection. Found the following:

0630 con't Containment sump level \approx 1 in. over the top.
RCDT spilling water out of the vent.
 \approx 3/4 in. water on the floor outside the
missile barrier for \approx 3 ft. from the missile
barrier outward.

0715 Post test inspection complete.

0730 Released containment to operating. Test completed.

Summary Analysis of Type B and Type C Test Results

The following table is a summary list of the periodic Type B and Type C tests that were performed since the last Type A test in February, 1977. The results indicate that the isolation capability of all the components tested has not degraded with time.

	<u>1978</u>	<u>1979</u>	<u>1980</u>
Total Type B Leakage (scfh)	48.5	22.48	6.26
Total Type C Leakage (scfh)	34.4	17.77	0.6
Total airlock seals leakage (10 psig test) (scfh)	1.2	0.15	0.07

The following is a cumulative list of Type B and Type C leakages by individual components:

Type C Components

<u>Valve (s)</u>	<u>Leakage (scfh)</u>	<u>Date Tested</u>
2MOV-CS0003	15.2	3-30-78
	1.32	4-10-79
	0	5-28-80
2MOV-CS0005	0.5	3-30-78
	3.11	4-10-79
	0.15	5-28-80
2MOV-CS0007	9.3	3-30-78
	-.23	4-10-79
	0.08	5-30-80
2PR0029	1.1	3-30-78
	2.84	4-06-79
	0.12	6-05-80
2PR0030	0.9	3-30-78
	2.62	4-06-79
	0	6-04-80
2IA01A,B	1.8	3-30-78
	2.46	4-09-79
	0.04	6-14-80

Type C Components con't

2DT9157	2.0	3-30-78
	0.84	4-04-79
	0.16	6-11-80
2AOV-RV0001 → 4	0.1	3-30-78
	0.23	4-04-79
	0.04	5-15-80
2FCV-PR24A,B	3.5	3-30-78
2PR0007,8,9,11,12,13,	2.12	4-06-79
15,16,17,19,20,21	0.01	5-31-80

Type B Components

<u>Electrical Penetrations</u>	<u>Leakage (scfh)</u>	<u>Date Tested</u>
Zone 1	8.0	3-30-78
	0.05	3-06-79
	0.16	5-13-80
Zone 2	9.2	3-30-78
	0.05	3-06-79
	0.11	5-13-80
Zone 3	8.2	3-30-78
	0.07	3-06-79
	0.09	5-13-80
Zone 4	2.4	3-30-78
	0.41	3-06-79
	0.29	5-13-80
<u>Mechanical Penetrations</u>		
Zone 1J	2.7	3-30-78
	1.07	3-22-79
	0	5-13-80
Zone 1B	2.4	3-30-78
	3.7	4-04-79
	0	6-11-80
Zone 2J	0.7	3-30-78
	3.09	3-14-79
	0	5-13-80
Zone 3D	2.9	3-30-78
	1.05	3-16-79
	0	5-13-80
Zone 3K	2.2	3-30-78
	5.57	3-14-79
	0	5-13-80
Zone 4B	4.7	3-30-78
	2.79	3-16-79
	0.12	5-27-80
Zone 4H	1.6	3-30-78
	3.68	3-19-79
	0	5-14-80

Type B Components con't

	<u>Leakage (scfh)</u>	<u>Date Tested</u>
Volume between doors on Personnel Airlock	0.1	3-30-78
	0.54	4-12-79
	0.01	1-14-80
	4.96	6-14-80
	2.30	7-10-80
Volume between doors on Escape Hatch	3.4	3-30-78
	0.31	4-12-79
	0.02	1-14-80
	0.53	6-14-80
	0.16	6-30-80
Personnel Lock Seals (10 psig test)	0	3-30-78
	0.12	4-12-79
	0.39	1-14-80
	0.01	6-13-80
Escape Hatch Seals (10 psig test)	1.2	3-30-78
	0.03	4-12-79
	0.06	1-14-80
	0.06	6-12-80
Equipment Hatch Seal	0.1	4-12-79
	0.06	1-14-80
	0	6-13-80

Calculation of "As Left" Leakage of the
Personnel Hatch and Escape Hatch

Following the ILRT, the inner equalizing valve of the escape hatch and the outer equalizing valve of the personnel hatch were repaired. A Type C local leakrate test was performed at 25 psig on each hatch to determine their "As Left" leakage. These leakages are to be added to the measured containment integrated leakrate to obtain the total integrated leakrate of the Unit 2 containment.

As Left Leakage

Personnel Hatch: .0475 scfh
Escape Hatch: .0817 scfh

$$(.0475 \text{ scfh} + .0817 \text{ scfh}) \times 24 \text{ hrs.} = 3.101 \text{ scfd}$$

$$\frac{3.101}{7332347 \text{ scf @ 25 psig}} \times 100\% = .00004 \text{ \%/day}$$

The "As Left" leakage of .00004 %/day is an insignificant amount to be added to the measured integrated leakrate of .007 %/day. Therefore, the total containment integrated leakrate remains at .007 %/day.

Calculation of Induced Leak for the
Supplemental Verification Test

Volume of containment = 2715000 ft.³

Volume of air in standard cubic feet at 25 psig:

$$2715000 \left(\frac{25 + 14.7}{14.7} \right) = 7332347 \text{ scf}$$

Allowable containment leakage $L_T = .0621$ %/day

In SCFM:

$$L_T = .000621 (7332347) = 4553.4 \text{ SCFD}$$

$$L_T = \frac{4553.4}{24(60)} = 3.16 \text{ SCFM}$$

Allowable measured leakage L_{tm} is:

$$L_{tm} = .75 L_T = .75(3.16) = \underline{2.37} \text{ SCFM}$$

Induced leak should be between 2 and 3 scfm.

2 scfm was chosen.

Calculation of Supplemental Verification Test
Acceptance Criteria

Measured containment leakrate - .007 %/day

Induced leakrate - .036 %/day

Measured combined leakrate - .053 %/day

Allowable containment leakrate (L_T) .0621 %/day

$$\text{Percent } L_T = \left| \frac{.053 - .036 - .007}{.0621} \right| \times 100\% \approx 16\%$$

$$16\% < 25\%$$

The difference between the supplemental test data and the Type A test data is within .25 L_T .

Figure of Merit Calculation

$$FOM = \frac{24}{h} \times (10^2) \left[2 \left(\frac{e_{pt}}{P} \right)^2 + 2 \left(\frac{e_{pv}}{P} \right)^2 + 2 \left(\frac{e_t}{T} \right)^2 \right]^{\frac{1}{2}}$$

E = sensor repeatability error
 error
 E = readout error

h = 24 hrs. P = 43.2 psia T = 537.8 °R

$$e_{pt} = \frac{[(E_{pt})^2 + (\xi_{pt})^2]^{\frac{1}{2}}}{\sqrt{\# \text{ of sensors}}}$$

e = measurement of change of parameter error
 E_{pt} = .001 = 0
 # of sensors = 2

$$e_{pt} = \frac{[(.001)^2 + (0)^2]^{\frac{1}{2}}}{\sqrt{2}} = \underline{.00071}$$

$$e_{pv} = \frac{[(E_{pv})^2 + (\xi_{pv})^2]^{\frac{1}{2}}}{\sqrt{\# \text{ of sensors}}}$$

E_{pv} = .00232 ξ_{pv} = .000056
 # of sensors = 10

$$e_{pv} = \frac{[(.00232)^2 + (.000056)^2]^{\frac{1}{2}}}{\sqrt{10}} = \underline{.00073}$$

$$e_t = \frac{[(E_t)^2 + (\xi_t)^2]^{\frac{1}{2}}}{\sqrt{\# \text{ of sensors}}}$$

E_t = .1 ξ_t = .006

$$e_t = \frac{[(.1)^2 + (.006)^2]^{\frac{1}{2}}}{\sqrt{28}} = \underline{.01893}$$

$$FOM = \frac{24}{24} \times (10)^2 \left[2 \left(\frac{.00071}{43.2} \right)^2 + 2 \left(\frac{.00073}{43.2} \right)^2 + 2 \left(\frac{.01893}{537.8} \right)^2 \right]^{\frac{1}{2}}$$

$$= 10^2 [5 \times 10^{-10} + 6 \times 10^{-10} + 2.5 \times 10^{-9}]^{\frac{1}{2}}$$

$$FOM = \underline{6 \times 10^{-3}}$$

Since the FOM is less than .25 L_T (.0155), the instrumentation is acceptable.

POOR ORIGINAL

17

TEMPERATURE SURVEY

DATE - 6/15/80 TIME - 10:50 AM

UNIT 2 ILRT

PERFORMED BY - T.K. SCHUSTER

@ 560' LEVEL

4 pts inside M.B.

4 pts outside M.B.

① 75°F @ RCP 2D

① 78°F @ E21

② 76°F @ SG 2C

② 73°F @ E22-23

③ 76°F @ RCP 2B

③ 74°F @ E28

④ 76°F @ E20 inside

④ 73°F @ E29-3

@ 592' LEVEL

4 pts inside M.B.

4 pts outside M.B.

① 77°F @ SG 2B-2C

① 72°F @ E31

② 77°F @ RCP 2C

② 74°F @ E29

③ 77°F @ RCP 2A

③ 75°F @ E26

④ 78°F @ RCP 2B

④ 72°F @ E34

@ 617' LEVEL

4 points

① 77°F @ Cont Wall SG 2A

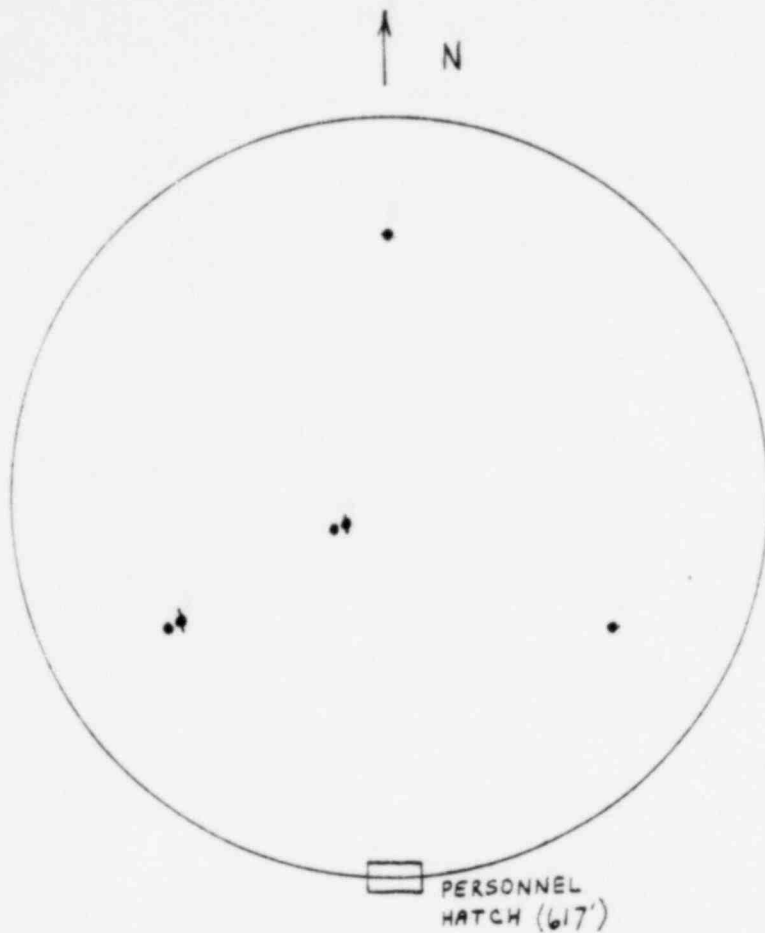
② 77°F @ Cont Wall SG 2B

③ 77°F @ Cont Wall SG 2C

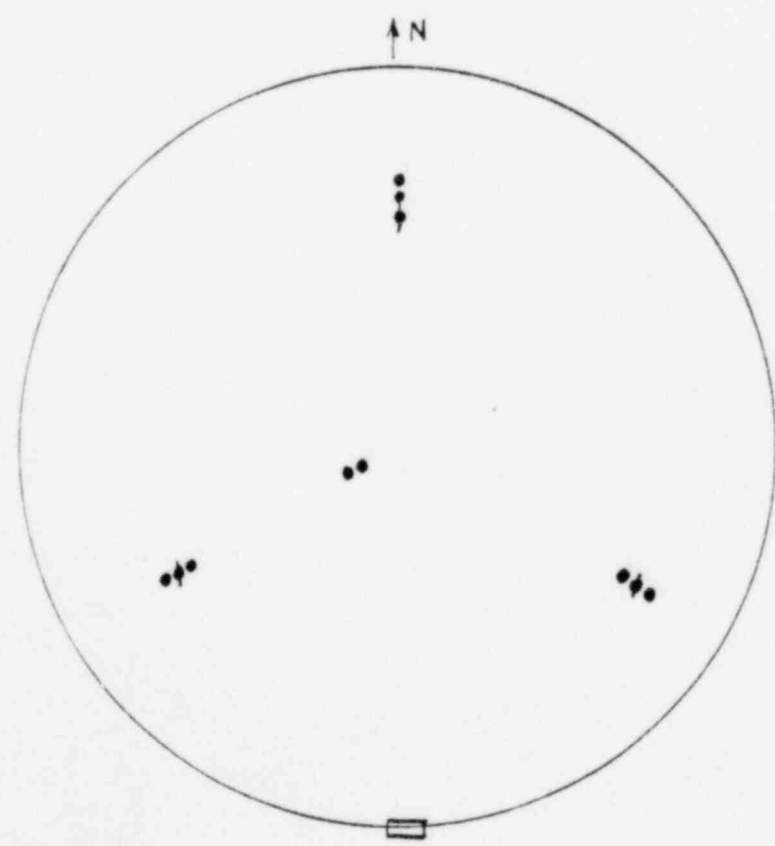
④ 77°F @ Cont Wall SG 2D

On the polar crans - all four points taken were at 77°F

Torenel K Schuster -
6/15/80



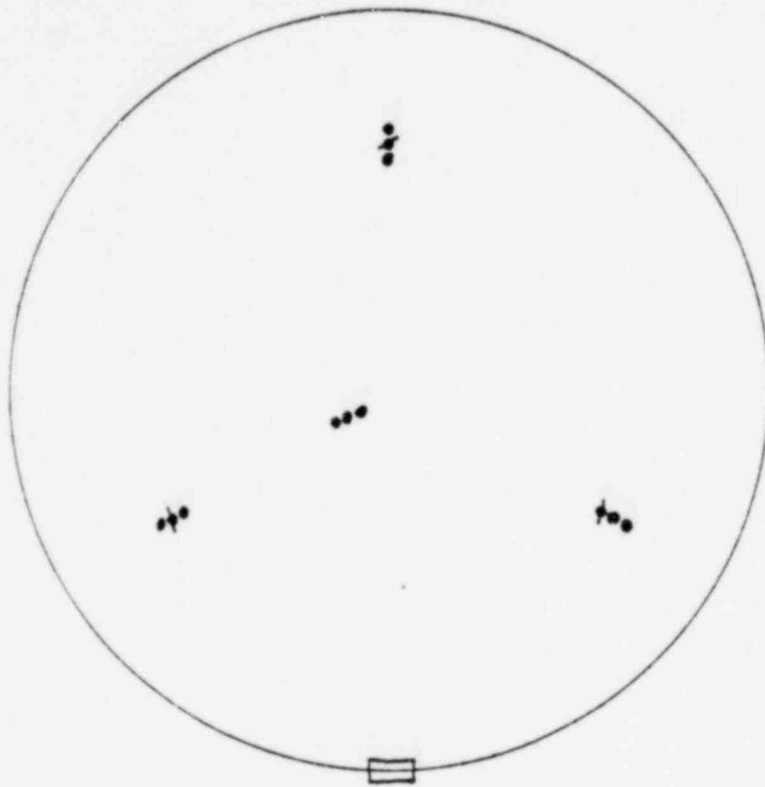
SUBVOLUME 1
 ELEV. 735' - RTD's
 ELEV. 734' - DEWCELLS



SUBVOLUME 2
 RTD's - 710', 690'
 DEWCELLS - 700'

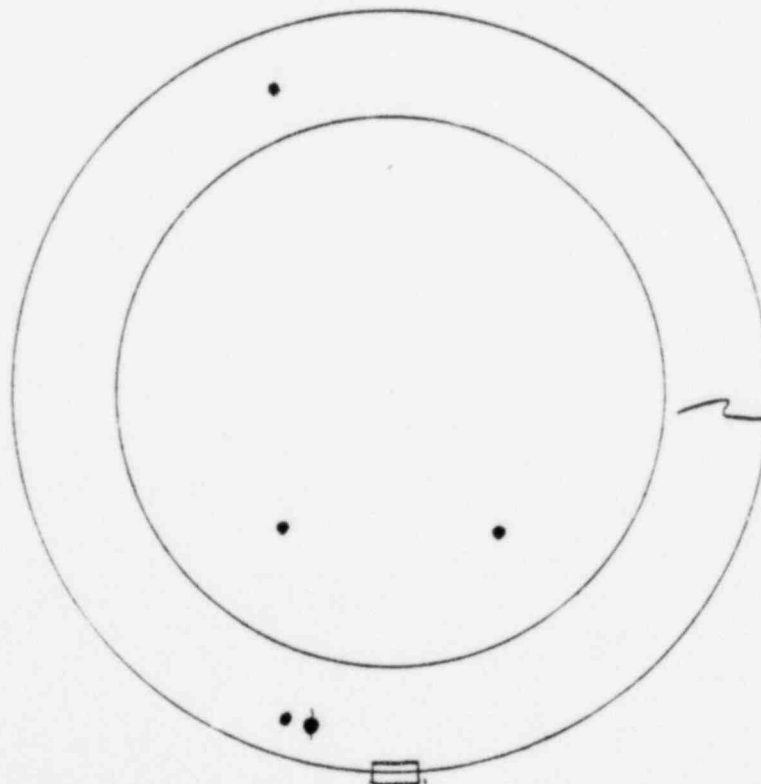
RTD • DEWCELL †

↑ N



SUBVOLUME 3
RTDs - 650', 640', 645'
DEWCELLS - 645'

↑ N

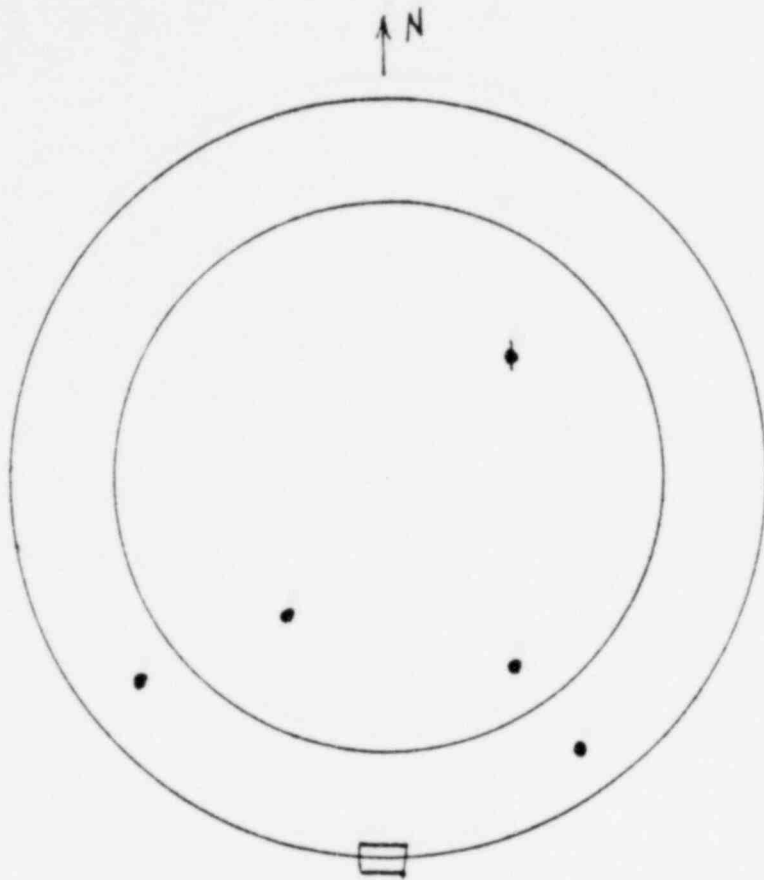


SUBVOLUME 4, 5
RTDs - 592'
DEWCELLS - 592'

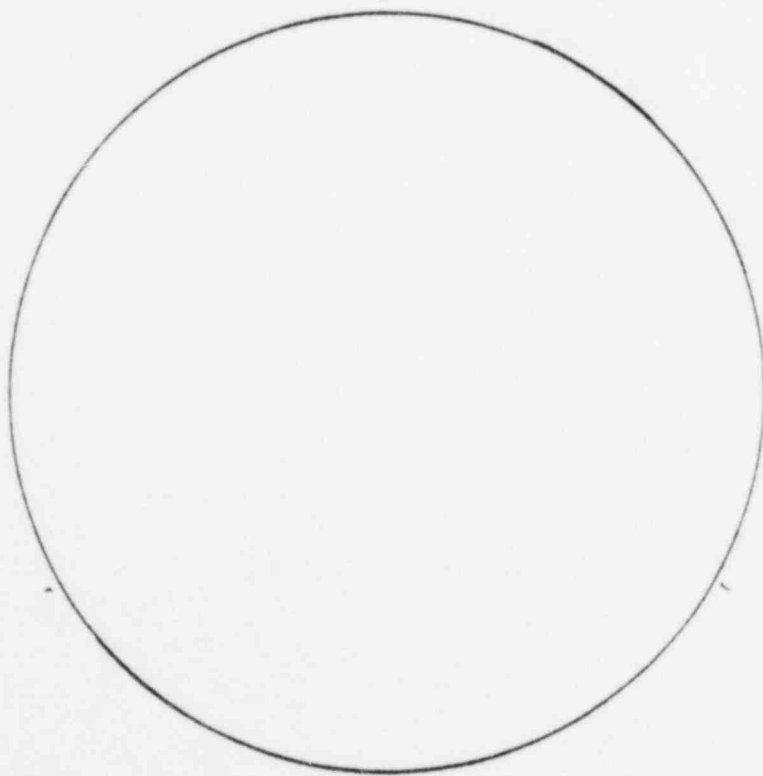
MISSILE BARRIER

RTD •

DEWCELL ♦



SUBVOLUME 4,5
RTD's - 560'
DENCCELLS - 560'





VOLUMETRICS

1025 W. ARBOR VITAE • INGLEWOOD, CALIFORNIA 90301
PHONE (213) 641 3747

PI-1

Gauge s.n. 970		Tube Range: 0-100 psia		s.n. 1140	
Room Temp: 70°F		Tube Temp: 50°C		Reference Pressure: 110 m Torr	
Calibrated by: KAA/ZG		Date: 4-17-80		Calibration Std. No. Model 07726 S.N. 101	
Pressure (true) psia	Gauge Reading counts	Pressure = Gauge Reading x M + C			
		M	C		
1	5	4869			
2	10	9747			
3	15	14651			
4	20	19549			
5	25	24452			
6	30	29345			
7	35	34251			
8	40	39153			
9	45	44043			
10	50	48960	1.020490897	.0500250487	
11	55	53860			
12	60	58757			
13	65	63670			
14	70	68601			
15	75	73526			
16	80	78563			
17					
18					
19					
20					
21					
22					
23					



VOLUMETRICS

1025 W. ARBOR VITAE • INGLEWOOD, CALIFORNIA 90301
 PHONE (213) 641 3747

PI-2

Gauge s.n. 971		Tube Range: 0-100 psia		s.n. 1517	
Room Temp: 70°F		Tube Temp: 50°C		Reference Pressure: 110 m Torr	
Calibrated by: KAA/ZG		Date: 4-17-80		Calibration Std. No. Model 07726 S.N. 101	
Pressure (true) psia	Gauge Reading counts	Pressure = Gauge Reading x M + C			
		M	C		
1	5				
2	10				
3	15				
4	20				
5	25				
6	30				
7	35				
8	40				
9	45				
10	50	1.012206121	-0.2165714448		
11	55				
12	60				
13	65				
14	70				
15	75				
16	80				
17					
18					
19					
20					
21					
22					
23					

RTD Buffer Amp Calibration

<u>Channel</u>	<u>RTD</u>	<u>60°</u>	<u>90°</u>	<u>120°</u>
0	0	58.47	90.18	119.88
1	1	59.29	89.98	120.03
2	2	59.23	90.70	120.06
3	7	58.66	90.10	119.98
4	4	58.97	90.13	120.14
5	5	59.45	90.14	120.11
6	6	59.32	89.93	120.09
7	11	59.25	89.97	120.05
8	8	58.98	89.92	120.00
9	9	59.46	90.18	120.09
10	10	59.53	90.00	119.98
11	15	58.66	89.92	120.06
12	17	59.37	90.14	120.06
13	23	59.01	89.97	120.00
14	15'	59.72	90.01	120.03
15	26	58.68	90.12	120.02
16	16	59.72	90.00	120.01
17	27	59.04	90.03	120.15
18	28	58.76	90.90	120.07
19	19	59.51	90.18	120.04
20	20	58.94	90.73	120.05
21	3	58.91	90.08	120.46
22	12	59.28	90.06	120.79

RTD Buffer Amp Calibration con't

<u>Channel</u>	<u>RTD</u>	<u>60°</u>	<u>90°</u>	<u>120°</u>
23	13	59.46	90.28	119.91
24	22	59.74	91.05	120.14
25	4'	59.05	90.09	119.95
26	14	59.05	90.15	120.06
27	21	59.50	90.23	119.97
28	25	59.74	90.05	120.14

Calibrated by: Kenneth A. Ringer 6-3-80

All channels were within acceptable tolerance bands.

RTD Buffer Amp Calibration

<u>Channel</u>	<u>Dewcell</u>	<u>84.54°</u>	<u>73.64°</u>	<u>67.18°</u>
30	1	83.89	73.11	67.82
31	2	84.12	73.29	67.64
32	3	84.13	73.11	67.65
33	5	84.38	73.21	67.38
34	6	83.54	73.68	68.16
35	10	84.19	72.97	67.40
		<u>85.56</u>	<u>75.83</u>	<u>64.40</u>
36	4	86.13	75.33	64.90
37	7	84.86	75.13	65.14
38	8	85.49	75.00	65.20
39	9	85.52	75.22	64.96

Calibrated by: Kenneth A. Ainger 6-12-80

All channels were within acceptable tolerance bands.

RTD Temperature-Resistance Values

RTD	60°		90°		120°	
	Ω	°F	Ω	°F	Ω	°F
0	106.303	58.59	113.225	90.05	119.778	120.01
1	106.573	59.35	113.212	89.92	119.794	120.09
2	106.645	59.28	113.451	90.64	119.882	120.10
3	106.487	58.93	113.247	90.05	119.923	120.48
4	106.657	58.97	113.435	90.12	120.027	120.15
5	106.620	59.51	113.269	90.07	119.836	120.17
6	106.529	59.38	113.154	89.87	119.749	120.15
7	106.473	58.66	113.269	90.11	119.809	119.97
8	106.488	59.02	113.177	89.88	119.756	120.04
9	106.665	59.44	113.316	90.20	119.878	120.06
10	106.633	59.54	113.242	89.97	119.825	120.00
11	106.620	59.32	113.275	89.91	119.856	120.12
12	106.561	59.33	113.233	90.01	119.972	120.84
13	106.554	59.49	113.231	90.25	119.731	119.94
14	106.519	59.07	113.256	90.14	119.822	120.08
15	106.458	58.68	113.219	89.90	119.822	120.08
16	106.628	59.75	113.202	89.97	119.788	120.03
17	106.567	59.36	113.237	90.15	119.790	120.05
19	106.607	59.54	113.275	90.13	119.828	120.07
20	106.594	58.91	113.485	90.75	119.902	120.03
21	106.633	59.57	113.315	90.14	119.852	120.05
22	107.045	59.77	113.863	91.02	120.272	120.18
23	106.649	59.06	113.357	89.92	119.931	120.06
25	106.699	59.73	113.260	90.05	119.853	120.13

RTD Temperature-Resistance Values con't

RTD	60°		90°		120°	
	Ω	°F	Ω	°F	Ω	°F
26	106.465	58.73	113.287	90.08	119.857	120.06
27	106.466	59.01	113.193	90.07	119.805	120.12
28	106.383	58.74	113.348	90.93	119.748	120.05
15'	106.780	59.78	113.360	89.95	119.965	120.10
4'	106.686	59.15	113.425	89.98	119.975	120.05

Calibrated by: Kenneth A. Ainge 6-4-80

POOR ORIGINAL

25

DC# 84.54°F 73.64°F 67.18°F

1	277.75 Ω 84.55 mV	272.45 Ω 72.93 mV	269.86 Ω 67.20 mV	Board # 9 installed in slot #1, Board #1 unstable
2	276.32 Ω 84.56 mV	271.19 Ω 73.11 mV	268.53 Ω 67.14 mV	
3	276.59 Ω 84.51 mV	271.33 Ω 72.93 mV	268.74 Ω 67.20 mV	
5	275.60 Ω 84.52 mV	270.42 Ω 73.14 mV	267.73 Ω 67.22 mV	
6	277.46 Ω 84.56 mV	272.63 Ω 73.46 mV	269.94 Ω 67.23 mV	Board #10 installed in slot #6, Board #6 zero not attainable
10	275.56 Ω 84.47 mV	270.29 Ω 72.92 mV	267.69 Ω 67.20 mV	Board #6 installed in slot #10 operates ok with DC # 10

85.56°F 75.33°F 64.40°F

4	277.49 Ω 85.56 mV	272.24 Ω 74.80 mV	267.21 Ω 64.44 mV	
7	278.72 Ω 85.47 mV	273.82 Ω 74.95 mV	268.82 Ω 64.37 mV	
8	278.81 Ω 85.60 mV	273.59 Ω 74.61 mV	268.76 Ω 64.39 mV	Check this board before test
9	277.65 Ω 85.62 mV	272.67 Ω 74.39 mV	267.75 Ω 64.30 mV	Board #1 unstable installed in # 9

haststone Bridge # L774337
GR1433-W decade Resistor sta No. 021
Fluke 8600A sta No. 013

Performed
1-31-80 → 2-7-80
J Swalen

FISCHER & PORTER

GROWTH WITH A PURPOSE through worldwide excellence in instrumentation

Commonwealth Edison Co.
Dresdon Nuclear Power Station
C/O Storeroom RR# 1
Morris, IL 60450

Date: 11 April 1979
Subject: CERTIFICATION
Ref: 7903A9328R1 (2R7706A9209R2)

FLOWMETER CALIBRATION ACCURACY CERTIFICATE

A. METER IDENTIFICATION:

- (1) Customer Purchase Order Number 501163 REL DR18
 (2) F&P Serial Number 7903A9328R1 (2R7706A9209R2)
 (3) Model Number 10A3555

B. CALIBRATION SPECIFICATIONS:

- (1) Date: 11 April 1979
 (2) Flow Range 11.1 To .9 Units SCFM
 (3) Metering Fluid Air
 (a) Viscosity 0.0181 CPS
 (b) Specific Gravity 1.0 60/60 F. Density 0.0012 gms/cc.
 (c) Temperature 14.7 PSIA
 (d) Pressure 70° F

C. ACCURACY: ± 1 % of Max. flow.

D. CALIBRATION FACILITIES:

- 1) The equipment and associated procedures used in the calibration of said meter are in accordance with Mil-C-45662A.
 (a) Through establishment of values of physical constants for primary standards using tools of NBS accuracy pedigree.
 (b) Through direct, dynamic comparison of Fischer & Porter and NBS flow facilities using Fischer & Porter Turbine Flowmeters as transfer standards. NBS Test No. 213.31/193098.
 (c) Through inter-laboratory comparison of compatible Fischer & Porter flow facilities.

Very truly yours,

Albert W. Hernandez

Albert W. Hernandez
Manager, Fluids Quality Control

AWH/mdt

VOLUMETRICS

CERTIFICATE OF CALIBRATION

Attention: COMMONWEALTH EDISON CO.

Date: 1/3/80

Test Title:

References:

Purchase Order No. 730266

Volumetrics Job No. 5958

Serial Number 1904

Government Contract No. ---

Gentlemen:

This is to certify that the enclosed Test Data Sheets contain correct and true data obtained in the performance of the test program as set forth in your Purchase Order.

Instrumentation used in obtaining this data has been calibrated using standards which are traceable to the National Bureau of Standards

Calibration Procedure: (MANUFACTURER'S SPECIFICATION)

Reference Standards Used:

<u>EQUIPMENT NO.</u>	<u>CALIBRATION DATE</u>	<u>DUE DATE</u>
<u>REF. STD No.3902/54</u>	<u>12/13/79</u>	<u>6/13/80</u>
<u> </u>	<u> </u>	<u> </u>
<u> </u>	<u> </u>	<u> </u>
<u> </u>	<u> </u>	<u> </u>

Enclosures: Data Sheets (1 Pages)

Quality Control Approval:


R. JOHNSON



VOLUMETRICS

1025 W. ARBOR VITAE • INGLEWOOD, CALIFORNIA 90301
PHONE: (213) 641-3747

Gauge s.n.1061		Tube Range: 0-100PSIA		s.n.1904	
Room Temp: 73°F		Tube Temp: 50.7°C		Reference Pressure: 0.1 MTORR	
Calibrated by: T.F.		Date: 1/3/80		Calibration Std. No. 3902154	
Pressure (true)	Gauge Reading	Pressure = Gauge Reading x M + C			
		M	C		
0.000	0.000				
4.9920	5.035	0.99146	0.000		
9.9840	10.057	0.99403	-0.013		
14.9760	15.085	0.99284	-0.001		
19.9679	20.110	0.99341	-0.010		
24.9596	25.126	0.99516	-0.045		
29.9515	30.142	0.99520	-0.046		
34.9434	35.130	1.00078	-0.214		
39.9353	40.160	0.99243	0.079		
44.9273	45.147	1.00100	-0.265		
49.9192	50.102	1.00745	-0.556		
54.8999	55.067	1.00316	-0.341		
59.8908	60.042	1.00320	-0.343		
64.8816	65.010	1.00459	-0.427		
69.8726	69.985	1.00322	-0.337		
74.8635	74.948	1.00562	-0.506		
79.8545	79.924	1.00301	-0.310		
84.8455	84.898	1.00342	-0.343		
89.8365	89.880	1.00181	-0.206		
94.8275	94.850	1.00423	-0.423		
99.8185	99.828	1.00261	-0.270		

VOLUMETRICS

CERTIFICATE OF CALIBRATION

Attention: COMMONWEALTH EDISON CO. Date: 1/25/80

Test Title: DEWPOINT

References:	Purchase Order No.	<u>919393</u>
	Volumetrics Job No.	<u>5959</u>
	Serial Number	<u>101</u>
	Government Contract No.	<u>---</u>

Gentlemen:

This is to certify that the enclosed Test Data Sheets contain correct and true data obtained in the performance of the test program as set forth in your Purchase Order.

Instrumentation used in obtaining this data has been calibrated using standards which are traceable to the National Bureau of Standards

Calibration Procedure: _____

Reference Standards Used:

<u>EQUIPMENT NO.</u>	<u>CALIBRATION DATE</u>	<u>DUE DATE</u>
<u>VMC 203</u>	<u>10/25/79</u>	<u>4/25/80</u>
<u>VMC 301</u>	<u>3/27/79</u>	<u>3/27/81</u>
_____	_____	_____
_____	_____	_____

Enclosures: Data Sheets (2 Pages)

Quality Control Approval:

C. B. Dreike
C.B. DREIKE



1025 WEST ARBOR VITAE
INGLEWOOD, CALIFORNIA 90301
PHONE: (213) 641-3747

REPORT NUMBER: 5959

REQUESTER: COMMONWEALTH EDISON CO. DATE: 1/25/80

MODEL: 07731

SERIAL NUMBER: 101

REFERENCE: 919393

MEDIA: --

CERTIFIED ACCURACY: .01 OHM

TEMPERATURE: 72°F

OHM METER CALIBRATION

STANDARD	AS FOUND	AS LEFT	
0.00	0.000	0.000	
50.00	49.993	49.993	
100.00	99.995	99.995	
110.00	110.001	110.001	
120.00	120.004	120.004	
130.00	130.005	130.005	
140.00	140.005	140.005	

NOTE: All standards used in this test report are traceable to the United States Bureau of Standards, Washington, D.C.

COMMENTS: STANDARD USED IS VMC-203 PRECISION

DECADE RESISTOR.

TECHNICIAN: T. Ferguson
T. FERGUSON

QUALITY CONTROL: C.B. Dreike
C.B. DREIKE

REPORT NUMBER: 5959

REQUESTER: COMMONWEALTH EDISON CO. DATE: 1/25/80

MODEL: 07731

SERIAL NUMBER: 101

REFERENCE: 919393

MEDIA: AIR

CERTIFIED ACCURACY: .60°F

TEMPERATURE: 72°F

DEWPOINT CALIBRATION

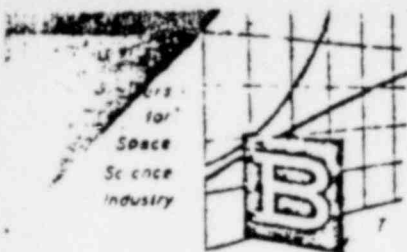
VMC-301	S/N 101 DEWPOINT CALIBRATOR	RESISTANCE VALUES	S/N 101 DEWPOINT CALIBRATOR
52.2°F	51.90°F	100.00	32.00
75.1°F	74.82°F	119.59	122.00
		136.33	199.99
			S/N 101 RTD Calibrator
		106.15	59.96
		112.70	90.09
		119.22	119.97

NOTE: All standards used in this test report are traceable to the United States Bureau of Standards, Washington, D.C.

COMMENTS: CALIBRATION WAS PERFORMED AS DESCRIBED IN
 IN THE RTD AND DEWCELL CALIBRATOR MANUAL. IN ADDITION
 THE ABOVE POINTS WERE VERIFIED AGAINST VMC-301 DEWPOINT
 STANDARD. RESISTANCE STANDARD USED IS VMC-203

 TECHNICIAN: T. Ferguson
 T. FERGUSON

 QUALITY CONTROL: C. B. Dreike
 C. B. DREIKE



BURNS ENGINEERING INC.

10201 Glen Road East 34 Minnetonka, Minnesota 55343
 (Suburban Minneapolis)
 Telephone 935 4400 • Area Code 612

CALIBRATION REPORT

The Resistance Temperature Device (RTD) described below has been calibrated by Burns Engineering, Inc. and the results are tabulated below. In addition, a R vs T table has been generated using the procedure outlined in NBS Monograph IPTS-68. These data are also reproduced below.

CALIBRATION DATA		CALCULATED TABLE	
TEMPF	32.000	RESIS	100.000
RESIS	100.000		100.220
TEMPF	100.000		100.440
RESIS	114.874		100.660
TEMPF	212.000		100.880
RESIS	138.998		101.100
			101.319
			101.539
			101.759
			101.979
			102.198
			102.418
			102.637
			102.857
			103.076
			103.296
			103.515
			103.735
			TEMPF
			032
			033
			034
			035
			036
			037
			038
			039
			040
			041
			042
			043
			044
			045
			046
			047
			048
			049

CALIBRATION DATE February 6, 1980
 CUSTOMER Volumetrics
 PURCHASE ORDER 80975-3000
 MODEL NUMBER WPPOG1-5½-4A
 SERIAL NUMBER 76448

POOR ORIGINAL

954	650	117.047	35	110	130.006
1.173	051	117.264		111	130.120
104.793	052	117.481		112	130.435
104.812	053	117.698		113	130.650
104.831	054	117.915		114	130.865
105.050	055	118.132		115	131.080
105.259	056	118.349		116	131.294
105.489	057	118.566		117	131.509
105.708	058	118.782		118	131.723
105.927	059	118.999		119	131.938
106.146	060	119.216		120	132.153
106.365	061	119.433		121	132.367
106.583	062	119.649		122	132.581
106.802	063	119.866		123	132.796
107.021	064	120.082		124	133.010
107.240	065	120.299		125	133.225
107.459	066	120.515		126	133.439
107.677	067	120.732		127	133.653
107.896	068	120.948		128	133.867
108.115	069	121.165		129	134.082
108.333	070	121.381		130	134.296
108.552	071	121.598		131	134.510
108.770	072	121.814		132	134.724
108.989	073	122.030		133	134.938
109.207	074	122.246		134	135.152
109.426	075	122.462		135	135.366
109.644	076	122.679		136	135.580
109.862	077	122.895		137	135.794
110.081	078	123.111		138	136.008
110.299	079	123.327		139	136.222
110.517	080	123.543		140	136.435
110.735	081	123.759		141	136.649
110.954	082	123.975		142	136.863
111.172	083	124.191		143	137.077
111.390	084	124.406		144	137.290
111.608	085	124.622		145	137.504
111.826	086	124.838		146	137.717
112.044	087	125.054		147	137.931
112.262	088	125.269		148	138.144
112.480	089	125.485		149	138.358
112.698	090	125.701		150	138.571
112.915	091	125.916		151	138.785
113.133	092	126.132		152	138.998
113.351	093	126.347		153	139.211
113.569	094	126.563		154	139.425
113.786	095	126.778		155	139.638
114.004	096	126.994		156	139.851
114.221	097	127.209		157	140.064
114.439	098	127.424		158	
114.657	099	127.640		159	
114.874	100	127.855		160	
115.091	101	128.070		161	
115.309	102	128.285		162	
115.526	103	128.501		163	
115.744	104	128.716		164	
115.961	105	128.931		165	
116.179	106	129.146		166	
116.395	107	129.361		167	
116.613	108	129.576		168	
116.830	109	129.791		169	