Equipment Environmental Qualification Review Responses to

Draft Interim Technical Evaluation Report

for

Zion Station - Units 1 & 2 September 19, 1980

Prepared by: Sargent & Lundy Engineers, Chicago, Illinois

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3.3.1.1 Limit Switch Within Containment NAMCO Controls, Model DX-2400

Plant ID Numbers: MOV-RC8001 A, B, C, D (RC loop isolation)
MCV-RC8002 A, B, C, D (RC loop isolation)
MOV-RC8003 A, B, C, D (RC loop bypass)

MOV-SI8803 A, B, C, D (Accum. tank isolation)

Response:

Limit switches used for indication only do not require environmental qualification. The limit switches for valves Mov-S18808 A, B, C, D are used for indication only.

Mov-RC8001 A, B, C, D and Mov-RC8002 A, B, C, D and Mov-RC8003 A, B, C, D were incorrectly referenced here.

These limit switches, which are used for control, have the qualified NAMCO, Model EAl80 and will be addressed in response to item 3.3.2.3.

3.3.2.1 Valve Motor Actuator Located Within Containment Submittal page references: 1, 2, 4, 5, 7, 8, 9, 13 References 10, 14

Valve ID Numbers: MOV-RC8000A,B (Pressurizer relief block valves)

MOV-RC8001A-D (RC loop isolation) MOV-RC8002A-D (RC loop isolation) MOV-RC8003A-D (RC loop bypass)

MOV-RH8701 (to RHR pump from loop hot leg)
MOV-RH8702 (to RHR pump from loop hot leg)
MOV-RH8703 (to loop hot leg from RHR pump)
MOV-SI8800A-D (from BIT to loop cold leg)
MOV-SI8808A-D (Accum. tank isolation)

Response:

Valves MOV-RC8001 A-D, MOV-RC8002 A-D, MOV-RC8003 A-D, MOV-RH8703, MOV-SI8800 A-D, and MOV-SI8808 A-D are not required to operate in the event of a LOCA or MS/FW line break, as shown in the Zion FSAR. These valves do not change position and since the starter is located outside containment (at motor control center in auxiliary building), an accident in the containment will not cause the valve to fail and change position. No qualification is necessary.

Valves MOV-RH8701 and MOV-RH8702, which are used to establish normal letdown, are required to operate long-term after a LOCA or MS/FW line break inside containment to achieve cold shutdown. Limitorque test report 600198 can be applied to these valve actuators which utilize a Reliance motor with Class H Insulation. As an alternative, it is anticipated by the Licensee that the valves can be operated manually when the containment atmosphere becomes accessible.

3.1.2.1 cont'd

In the event of a small LOCA, it may be beneficial for valves MOV-RC8000 A & B to remain operational long-term. Limitorque test report B0003 can be applied to these valve actuators which utilize a Reliance motor with Class B Insulation. It should be noted that the environmental conditions will be less severe for a small LOCA than for a design basis LOCA. Therefore, long-term qualification should not be required for the worst case LOCA environmental parameters presented in the Zion FSAR.

3.3.2.2 Solenoid Valves Located Within Containment:

Submittal page references: 6, 10 for item 3 & 4; 15 for item 7

Items 3 & 4 ID numbers: PCV-455C, 456 (Pressurizer relief valves)
AOV-VC8149B (Normal letdown isolation)

Response:

Valve AOV-VC8149B is not required to operate after a LOCA or MS/FW line break. This valve is backed up by containment isolation valves VC8152 and VC8153 which are in series.

No qualification is necessary.

. Valves PCV-455 C & 456 may be required to operate long-term depending on the specific types of accident. The Licensee is reviewing the possibility of replacing these solenoids with the qualified NP-1 solenoids.

Item 7 ID numbers: SV-RV091 thru 105 (RCFC damper solenoid
valves)

Response:

The ASCO solenoid valves in question are those for the RCFC dampers. They are model 8300 series valves. The valves have stainless steel, metal-to-metal seats, and all metal internals. The only part which is susceptible to failure under high radiation or temperature environments are the rubber sealing O-rings. Any time this O-ring would fail

3.3.2.2 cont'd

during normal operation the solenoid will vent and shift to the accident mode. In event of a LOCA or MS/FW line break the valves are required short term and will function before an O-ring failure would occur. Once the solenoid has shifted there would not be a reason to want to change the position of the dampers and therefore functional capability of the solenoid long term after the accident does not have to be addressed.

·No qualification is necessary.

Note: Reference 24, which refers to the NP-1 series solenoids,

was not used by the Licensee and therefore the comment
pertaining to this item is not applicable.

3.3.2.3 Limit Switch Located Within Containment

Submittal page references 11, 12

NAMCO EA-180

References: 23

Valv: ID numbers: LCV-RC459 (Regen. Heat Exchanger Isolation

from loop cold leg)

LCV-RC460 (Regen. Heat Exchanger Isolation

from loop cold leg)

MOV-RC8001 A, B, C, D (RC loop isolation)
MOV-RC8002 A, B, C, D (RC loop isolation)
MOV-RC8003 A, B, C, D (Accum. tank isolation)

Response:

The above referenced limit switches are used for control. Commonwealth Edison Company has agreed to seal these limit switches with qualified seals. They are currently in the process of obtaining qualified seals and will seal the switches at the first refueling outage for each unit after the qualified seals arrive on site.

3.3.2.4 Reactor Containment Fan Cooler Motor Located Within Containment

Westinghouse Electric Corporation, 585.5 - CSP 1 Fram 200/200 hp/1200/300 rpm References: 12 and 15

Response:

A letter has been sent to Westinghouse requesting additional information to qualify the RCFC motors for a 40-year life plus accident and to qualify lubricants with respect to the combined effects of steam/chemical spray and radiation exposure. Also, Westinghouse was requested to supply evidence that their test specimen was identical to the installed equipment.

In response to the above reference letter on the RCFC motors, Westinghouse has replied that WCAP-7829 provides the additional information requested. Westinghouse also stated that it was not possible to secure the traceability requested in such a short time, but that this effort has beer initiated.

Franklin Research Center stated that the qualification of the motor-lead-splices and lead-to-cable splices with respect to radiation was not addressed in the submittal qualification reports. Westinghouse Test Report WCAP-7410-L, Volume II of II, page 6-3 (submitted to Franklin Research

3.3.2.4 cont'd

Center) states that the splices were thermally aged followed by a radiation exposure prior to being exposed to the postaccident environment inside the containment. 3.3.2.5 Electronic Flow Transmitter Located at Cl Submittal Page Reference 16 Qual. Reference 9, 20, 21

> FT924 FT926 FT925 FT927

Cold Injection Flow Rate (Model 1032496)

Response:

These transmitters are backed up by FT934 which measures the total flow and is located outside of containment in a non harsh area when FT924, 925, 926, and 927 are in a harsh environment. Therefore, FT924, 925, 926, and 927 are provided with redundancy which will not be subjected to the containment environment.

Electronic Pressure Transmitter Located at Cl Submittal Page Reference 17 Qual. Reference 9, 20, 21

> PT960 PT964 PT961 PT965 PT962 PT966 PT963 PT967

Accumulator Press. (Model 50EP1031)

Response:

These transmitters are not required to work following a LOCA or HELD since they only indicate whether or not the accumulators have injected.

3.3.2.6 Electronic Transmitter Located at Cl Submittal Page Reference 19 Qual. Reference 9, 20, 21

FT512	FT513
FT522	FT523
FT532	FT533
FT542	FT543

Steam Generator Steam Flow (Model 10B2491)

Response:

These transmitters are only required to work immediately following an accident for safeguards actuation. For available qualification refer to the generic reply on Fischer & Porter transmitters attached to these responses.

Electronic Transmitters Located at Cl Submittal Page Reference 20 Qual. Reference 9, 20, 21

LT517	LT518	LT519
LT527	LT528	LT529
LT537	LT538	LT539
LT547	LT548	LT549

Steam Generator Level (Model 13D2495)

Response:

These transmitters are required for long term operation after MS/FW line break. For available qualification see generic reply on Fischer & Porter transmitters attached to these responses.

3.3.2.6 cont'd

Electronic Transmitter Located at Cl Submittal Page Reference 22 Qual. Reference 9, 20, 21

FT414	FT415	FT416
FT424	FT425	FT426
FT434	FT435	FT436
FT444	FT445	FT446

Reactor Coolant Flow (Model 10B2491)

Response:

These transmitters are not required to operate after an accident.

Electronic Transmitters Located at Cl Submittal Page Reference 23 Qual. Reference 9, 20, 21

> PT455 PT457 PT456 PT458

Pressurizer Pressure (Model 50EP1041)

Response:

These transmitters are only required to work immediately following an accident. Post-accident indication is provided by new TMI qualified transmitters (TMI MOD M22-1-80-3) which are the best transmitters available as of April 1980. These transmitters, PT403 and PT405, are the Reactor Coolant Wide Range Pressure transmitters (Barton 763).

Electrical Penetrations Located
Within and Outside of
Containment
D. G. O'Brien, Type 4.1
(Submittal Page References 2 and 17)

Response:

- 1. The attached xerox copies of portions of the D: G. O'Brien Instruction Manual No. 1019 for Type 4.1 and 4.1A Electrical Penetrations identify the materials used, including jacket and insulation materials for cable leads. It should also be noted that the environmental test referenced in Section 4 of Test Report C19QA032 was a saturated steam atmosphere of 46 psig pressure, 273°F temperature, for a 48-hour period.
- 2. The Type 4.1 penetration contains instrumentation type cables, No. 16 AWG twisted pairs and quads and No. 20 AWG thermocouple leads, which will all carry currents of less than 1 amp (generally in the range of 10 to 50 milliamps or 4 to 20 milliamps for the No. 16 AWG and much less for the thermocouple leads) which will not affect the loading conditions imposed on the cables during a LOCA.
- We are still attempting to obtain information from the Vendor, D. G. O'Brien, to determine a qualified life.

Instruction Manual (1019)

For

REACTOR CONTAINMENT STRUCTURE
ELECTRICAL PENETRATION ASSEMBLY
TYPES 4.1 AND 4.1A

(Serial Numbers 4.1Z1 - 4.1Z5 and 4.1AZ1-4.1AZ5)

September, 1971

Prepared For Use On
ZION STATION UNITS I AND II

(Commonwealth Edison, Co., Contract 113967)

Prepared by:
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P. R. Henault, Project Electrical Engineer

P. S. Butters, Project Mechanical Engineer

9/17/7/

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H. P. Hilberg Manager of Nuclear Power Plant Systems

Approved by:

INTRODUCTION

The Electrical Penetration Assembly described herein was designed and manufactured by D G. O'Brien, Inc., Framingham, Mass. for use in the construction of Nuclear Power Plant - Zion Units I and II, Commonwealth Edison Co., Zion, Illinois.

This manual is for use in the installation, test, calibration, and operation of Type 4.1 penetration assemblies. This penetration is designed for low voltage shielded instrumentation cable service. Penetration assemblies of Type 4.1 (instrumentation) are identical for both Zion Units (I and II). Types 4.1 and 4.1A are identical but the 4.1A designation applies to the assembly used with Zion, Unit II.

Information pertaining to other types of penetrations also designed and manufactured by D. G. O'Brien, Inc. for Zion Units I and II can be obtained from other Instruction Manuals. This manual is applicable only to Type 4.1 and 4.1A.

Quality Assurance data is included under a separate cover. This penetration assembly is furnished for use with applicable design data of the following Sargent and Lundy drawings:

- ES_42 Typical Electrical Penetration, Physical Requirements, Dated 10-1-69
- B-213 Reactor Building Containment, Liner Plate Sections and Details, Sheet 2 Rev. T. Dated 10-3-69
- B-214 Reactor Building Containment, Penetration Schedule, Rev. L, Dated 10-3-69
- B-216 Reactor Building Containment, Elevation Electrical Penetrations, Rev. G, Dated 10-3-69

The penetration assembly described herein is furnished by D. G. O'Brien, Inc. as part of an ASME, Class B Nuclear Vessel.

The electrical penetrations for Nuclear Generating Power Plants manufactured by D. G. O'Brien, Inc. are engineered to meet the stringent requirements of the electrical power industry and the Atomic Energy Commission. The careful integration of many scientific and technical disciplines has gone into the development of a state-of-the-art product that is reliable, rugged, dependable, efficient, and economical. Careful control of manufacturing processes and materials plus extensive in-process and final testing ensures that the finest product is delivered to the customer.

This manual is prepared to give the 'customer, in readily available form, the information necessary to efficiently install and maintain the purchased equipment. References throughout this manual to type 4.1 assembly are also applicable to type 4.1A assemblies, unless otherwise specified.

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- 1.0 GENERAL DESCRIPTION
- 1.1 Low Voltage Shielded Instrumentation Cable Penetration
 Assembly (D.G. O'Brien, Inc. Part No. R19D2227P) herein
 referred to as the penetration assembly will be used as
 an interface for passing the Purchaser's low-voltage
 instrumentation cables, from the outside containment
 to the inside containment. As such, it will become a
 critical portion of the cabling system associated with
 the reactor nuclear instrumentation and control system.
- 1.2 The penetration assembly will service electronic instrumentation loads of up to 120 VAC. The assembly will provide the interface between instruments located inside the containment and monitors located outside of the containment that indicate status of operation.
- 1.3 The assemblies are designed and constructed for installation in 12-inch diameter steel pipe containment penetration nozzles that are 3 feet, 6 inches long. Each penetration assembly is identical in basic physical configuration and consists of the assembly having one mechanical seal permanently attached. The second mechanical seal, required for field installation, is furnished separately in the same shipping carton.
- 1.4 The penetration assembly must be inserted into the containment structure nozzle from inside the containment and is permanently installed by means of field welding at the site. Mechanical supports are necessary to position the assembly during the welding operation. The past experience of D. G. O'Brien, Inc. in the Nuclear Power Plant Penetration Assemblies and in underwater and military

applications provides the necessary background experience to assemble and weld penetration assemblies without detrimental heat transfer to the components of internal conductors.

- 1.5 Each assembly is designed to restrain loading due to electrodynamic forces or mechanical stressing. Internally, this is achieved, where required, by groups of cubular cable guides extending the full length of the penetration assembly.
- 1.6 Every penetration assembly is permanently identified by a serial number. Every wire, external to the assembly, is marked at each end with an identification number as specified by the purchaser. Wire numbers in any one multiconductor cable are not repeated.
- 1.7 Sealing and Pressurization. The penetration assemblies provide a dual gas barrier by means of steel header flanges and hermetically glass-sealed electrical contacts. Each of the two gas barriers meet the service environmental conditions individually, providing an overall performance safety factor of two. The double-pressure barrier is formed, at installation, by welding that is in accordance with the ASME Boiler and Vessel Code, Section III, Class B Vessels. Both the internal volume of the penetration assembly and that between it and the penetration nozzle may be pressurized through a pressurization port in the outside containment mechanical seal and holes in the

conister. The conister assemblies are pressurized to 15 psig with dry nitrogen prior to shipment. Gross pressure differential of the penetration assembly in transit and storage can be observed on the pressure gauge that forms part of the assembly.

CAUTION

PRIOR TO INSTALLATION, THE PENETRATION

ASSEMBLY SHOULD BE DEPRESSURIZED AND

THE PRESSURE GAUGE ASSEMBLY AND PURGING

PORT PLUGS REMOVED. REFER TO SECTION 4.0

OF THIS MANUAL.

Safety Factors in Production. Pneumatic testing is 1.8 performed on the prototype and on each production assembly in accordance with the latest revision of Paragraph N-110 in Section III of the ASME Boiler and Pressure Vessel Code and as covered in detail in the Quality Assurance Instruction Data. The allowable leak rate of both penetration gas barriers in series, in prototype testing, is equal to, or better than, 1 x 10⁻⁶ standard cc/sec. of dry helium at 298°F and 54 PSIG. In production, each penetration assembly is subjected to a leak rate test at 54 PSIg and 78°F +5°F and will not exceed 1 x 10-6 standard cc/sec. through both ponetration gas barriers in series. Due to controlled production processes, hermetically glasssealed headers or gas barriers consistently better the leak rate of 1×10^{-6} by two orders of magnitude.

- 1.9 Cable Description
- 1.9.1 Internal Cables. The internal cables and external pigtails are directly terminated to glass-sealed contacts in connectors (pucks) welded into the gas barriers. The electrical characteristics of the internal cables are identical to the purchaser's cables within the tolerances allowed.
- 1.9.2 External Cable Terminations. External cable terminations are made to the pigtail leads on each puck. The pucks are a related part of the penetration assembly gas barrier. All cables are soldered. They are designed and built to function in accordance with the requirements of the circuits they service. All conductors are insulated from each other and from ground:
- 1.9.3 The prototype and all production models are tested to the following:
 - A. Insulation:
 - 1. Test Voltage 500 VDC
 - 2. Minimum Insulation Resistance Conductor-to-conductor 1 x 10⁸ ohms-feet Conductor-to-shield 1 x 10⁸ ohms-feet Conductor and Shield to Ground 1 x 10⁸ ohms-feet
 - B. Dielectric Strength:

Prototype:

Conductor-toconductor 1500 VAC RMS

Conductor-to-shield 1500 VAC RMS

Conductor and Shield to Ground 1500 VAC RMS

Production:

Conductor-to-conductor 600 VAC RMS

Conductor-to-shield 600 VAC RMS

Conductor and shield to ground 600 VAC RMS

Table 1-1 summarizes the technical and design parameters and provides a ready reference of data.

4.1 - CONTROL ELECTRICAL PENETRATOR DESIGN PARAMETER SUMMARY

Number of Conductors

36060 twisted shielded jacketed quads, 16 AWG Boston Insulated Wire P/N 7934-H-004
50 twisted shielded jacketed pairs, 16 AWG Boston Insulated Wire P/N 7933-H-002
10 Twisted shielded jacketed thermocouple pairs, 20 AWG Insulated Wire P/N 7938-H-002

Material and Size of Conductors: Current or signal:

#16 AWG tin plated copper stranded 7/24 #20 AWG Thermocouple wire solid chromel & constantan

Ground or shield:

Copper Mylar tape wrap with #16 AWG bare copper 7/24 strand for pairs & quads #20 AWG solid bare copper for thermocouple pair

 Conductor Insulating Material:

Chlorosulfonated Polyethylene *Hypalon "Bostrad 7"

Temperature Rating:

+90°C

4. Provision for connection of Purchaser's external cable

Pigtoils

5. High Potential Test on production assemblies for 10 seconds: Conductor-to-conductor 600 VACRM Conductor-toshield 600 VAC RMS-Conductor and shield to ground 600 VAC RMS

^{*}Hypalon is a registered trademark of E. I. DuPont DeNamours & Co. "Bostrad 7" is a registered trademark of Boston Insulated Wire & Cable Co.

6. Assembly Body Material 10" I.P.S. Sch. 20 Pipe, ASTM, A-333 GR-1 Carbon Steel End Header Plate 7. ASTM, A-442, GR-60 Corbon Material Steel or ASTM A-516, GR-70 End Header Plate 8. Leaded Carbon Steel Per AISI, C1213 (Tin plated) Conductor Material 9. End Header Plate Conductor Insulating Material 9010 Glass 10. Assembly Dimension Body Outer Diameter 10 3/4" Body Length 4'61" 1.7 x 108 Rad (1.5 MEV 11. Maximum Integrated Gamma Rays) Radiation Exposure 2.24×10^{-5} cc. (Air) Min. 12. Maximum Total Assembly 13. Minimum Insulation 1×10^8 ohms-feet Resistance @ 500 VDC: 14. Total Assembly Calculated Weight 425 pounds 15. 15 PSIG Dry Nitrogen Shipping Pressurization Testing Pressurization 54 PSIG Dry Nitrogen -16. Design Current Rating 1 'AMP

6.0 WIRING

The following drawing (Figure 6-1) depicts the wiring diagram electrical connections of the Zion I and II Electrical Penetrations, Type 4.1 Low Voltage Shielded Instrumentation Cable Service for normal plus postaccident duty.

7.0 TERMINATION INFORMATION

Prior to assembly of any hardware on the penetration assembly, a review of D. G. O'Brien, Inc. Drawing R19D2227G (Sheets 1 and 3) should be made to ascertain layout and sequence for splicing of wires. This drawing also illustrates the location of puck assemblies and electrical connection sequence. The required hardware and material for termination are included in the shipping carton, Kit P/N 115-302.

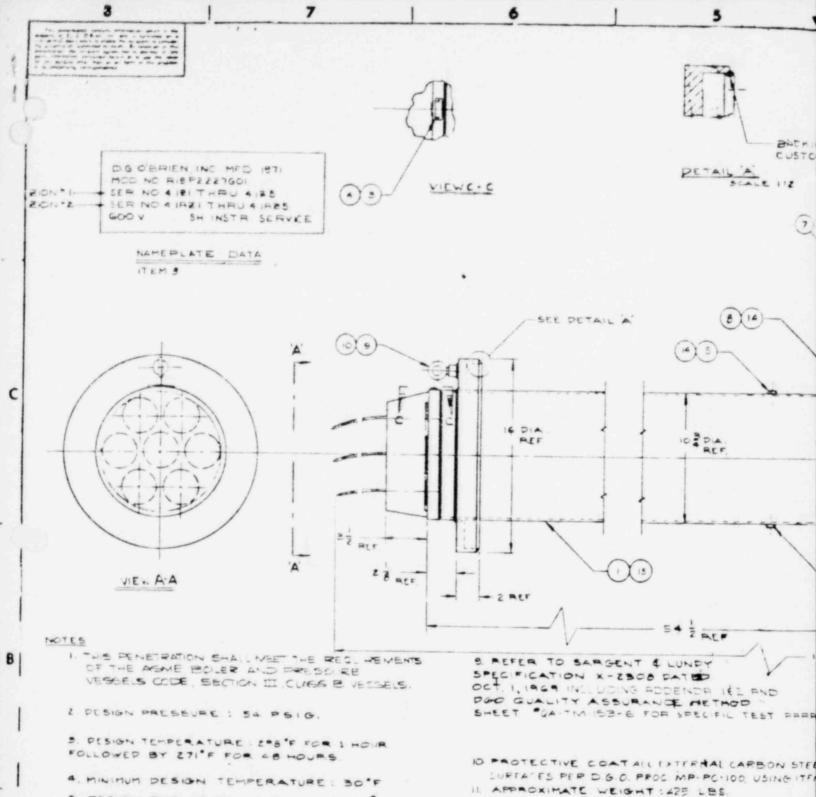
CAUTION

PRIOR TO ASSEMBLY CHECK PIGTAILS AND POTTING WITHIN PUCKS FOR INDICATIONS OF DAMAGE.

All work should be done in as clean an area as possible, well ventilated, and free from moisture and work hazards.

Purchaser's Field Cables shall be prepared as outlined in D. G. O'Brien, Inc. Drawing R19D2227G for termination to the Burndy or AMP wire splices and the Thermo Electric thermocouple connectors.

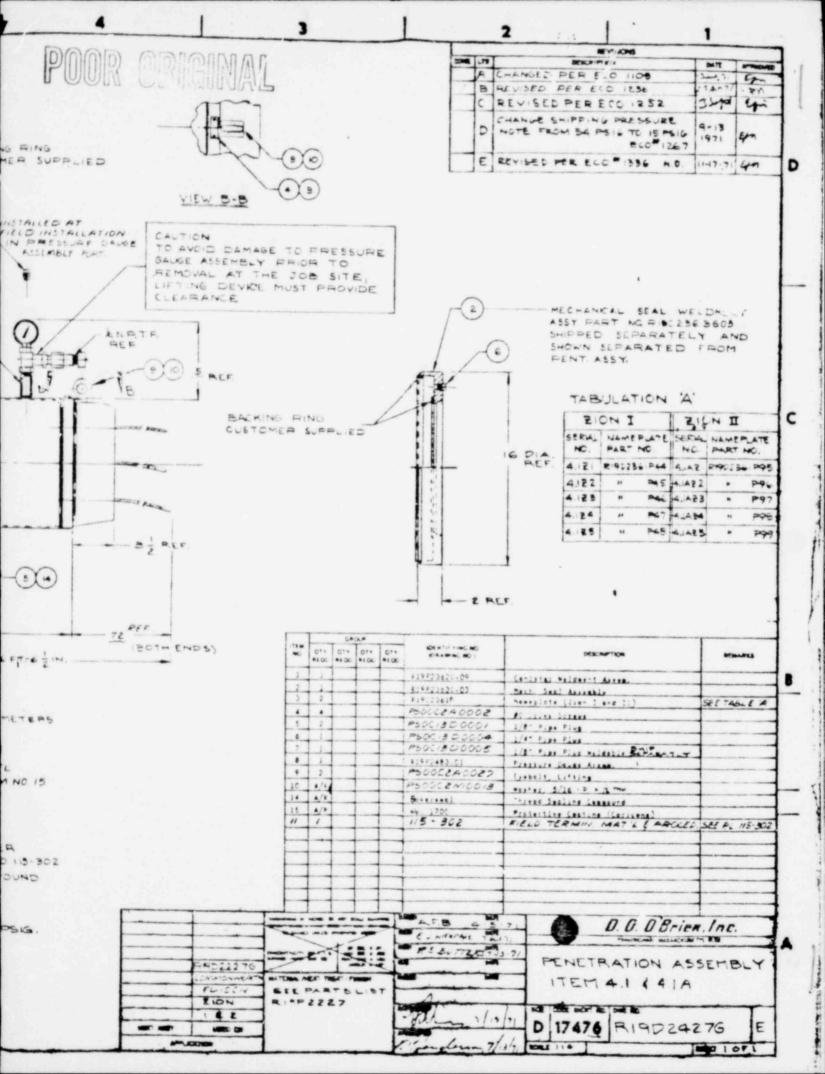
PARTS LIST			Τ	-(D. G. O'Brien, Inc.		REV. DATE	P.L. 115-302	REV. LTR.	
TITLE FIELD TERMINATION KIT ZION 4.1						AUTHENTICATION	CHGE, CONT. NO	17476		SHT OF
	GROUP									
NO.	QTY. REQD	QTY. REQD	QTY. REQD	QTY. REQD.	(DRAWING NO.)		DESCRIPTION			REMARKS
						J.O. 62004 Item	n 4.1 Outside	Cont.		
Hei						J.O. 62004 Item	m 4.1 Inside	Cont.		
							TEST STEEL TO			
01	150	155		-	wew 4		14 416 B	,		
01	450	450		-	31819	Splice, Crimp, 14 AWG, Burndy Splice, Crimp, 14 AWG, AMP		(A1	ternate)	
02	1	-		-				.++!.	INT	ternate,
	12	12	-		#42223 #42123	Jack, No. T3JBS				
03	1. 12	1	-	-	12			, ,		
04	1	1	-	-	Y9M or Y10M	Tool, Crimp, Bu	urnay		(41	ternate)
0.5	1	1	-	-	49900 or 49935	Tool, Crimp	Vannau		AI	ternate)
05	45	1	-	-	2" x 4"	Pad, Air Seal H		0.707/		
06	385	385	-	-	$1/4$ " I.D. $\times 2 - \frac{1}{2}$ "long	Tubing, Heat St			-	
07	385	385	-	-	$3/8$ " I.D. x $3-\frac{1}{2}$ "long	Tubing, Heat St			-	A STATE OF STREET
08	1	2roll	-	-	\$1024	Tape, Heat Seal			-	
09	38	38			1" I.D. x 12" long	Tubing, Heat St				
10	5	5		-	1 1/8" I.D. x 12"long					
11	6	6		-	$1 \frac{1}{2}$ " I.D. x 6" Long	Tubing Heat Shi	rink, Raychem	RT 876	-	
	1									

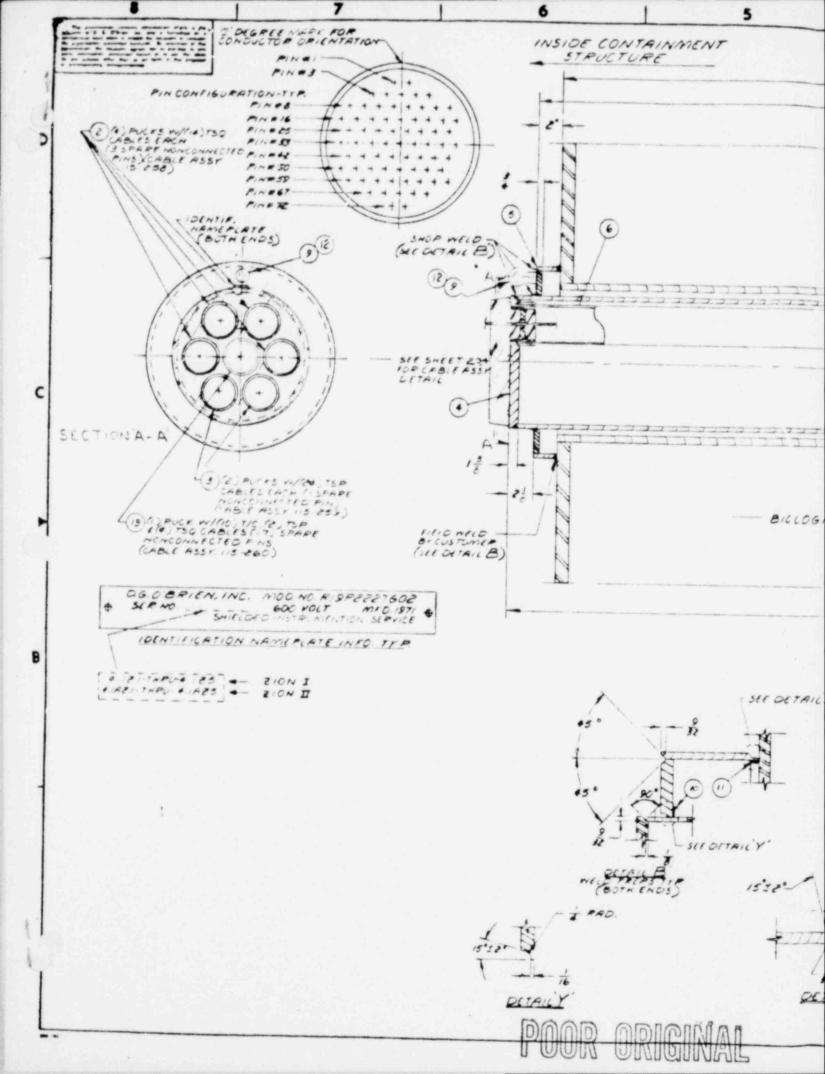


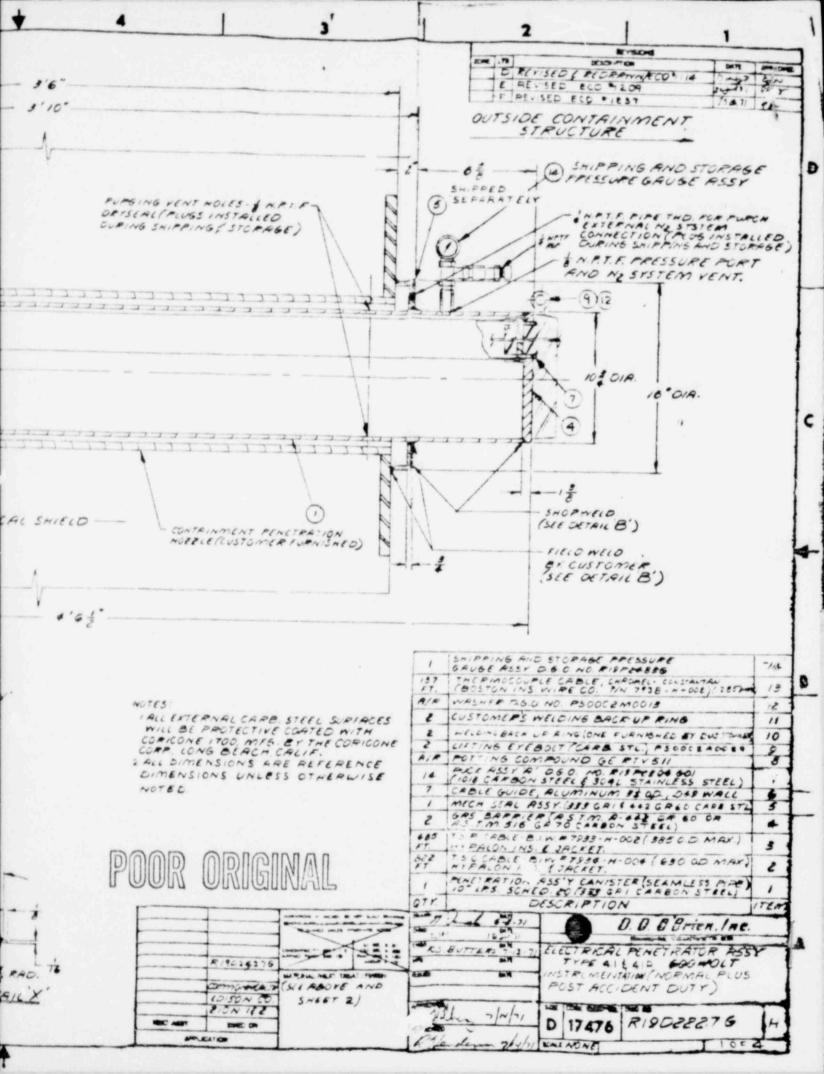
- PADS (1.5 MEV. BAMMA RAYS) TOTAL
- & RELATIVE HUMICHTY MAX LURING THE 40 YEAR LIFE INSIDE AND OUTSIDE CONTAINMENT 50%
- T PENETRATION SEISMIC TEST .25 S AT C TO SSHERTE
- SEE INSTALLATION ASSEMBLY DRAWING PRIEDZ476606
- FIELD CABLE TERMINATION ITEMS, SEE CUSTOMI
- THELD CABLE TERMINATION PROCEDURE DOO NO USE ONLY BREEDER THREED FERENCE COME ON ALL DRYSERL PIPE THREED RESEMBLIES

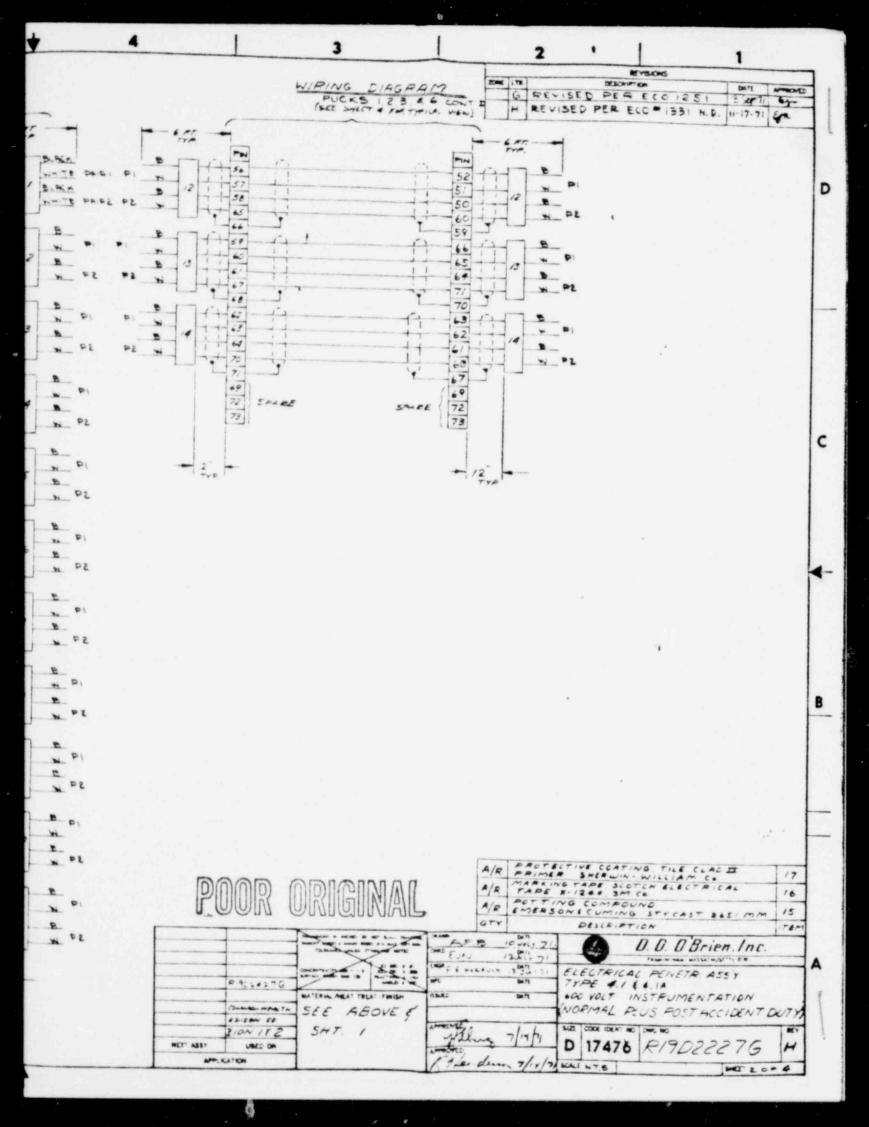
A PENETRATION INTERNAL SHIPPING PRESSEE, 15

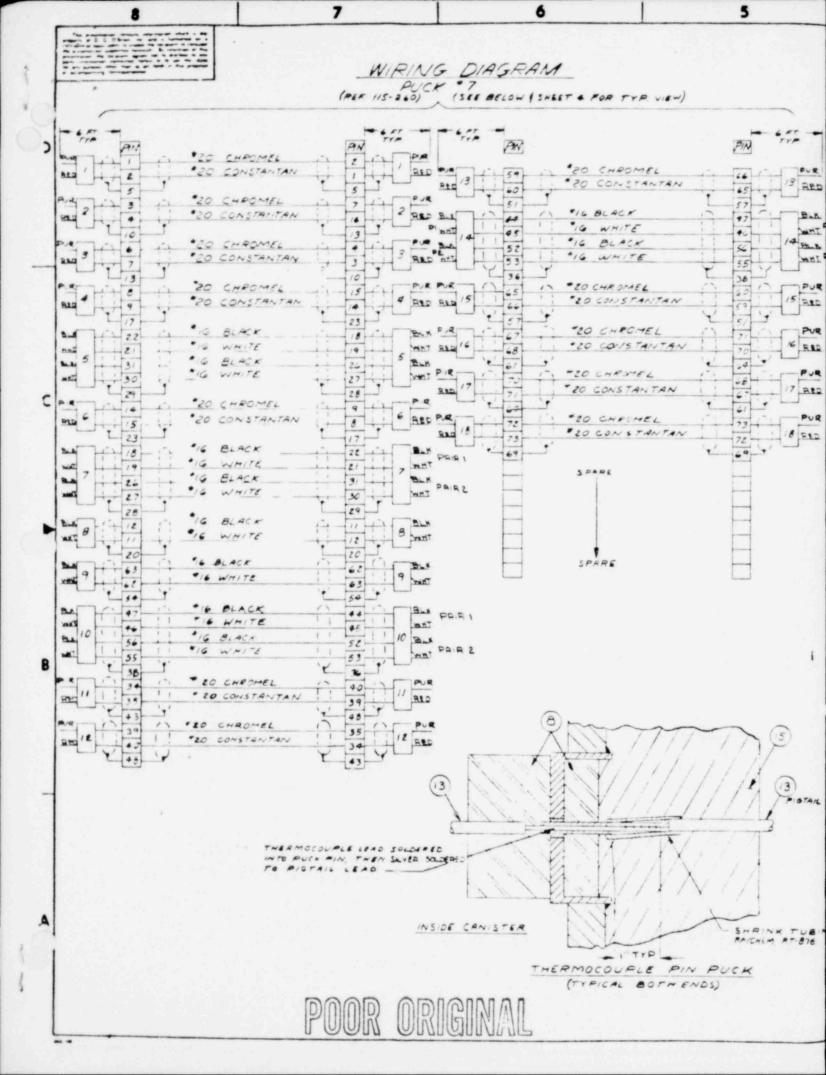
POOR ORIGINAL

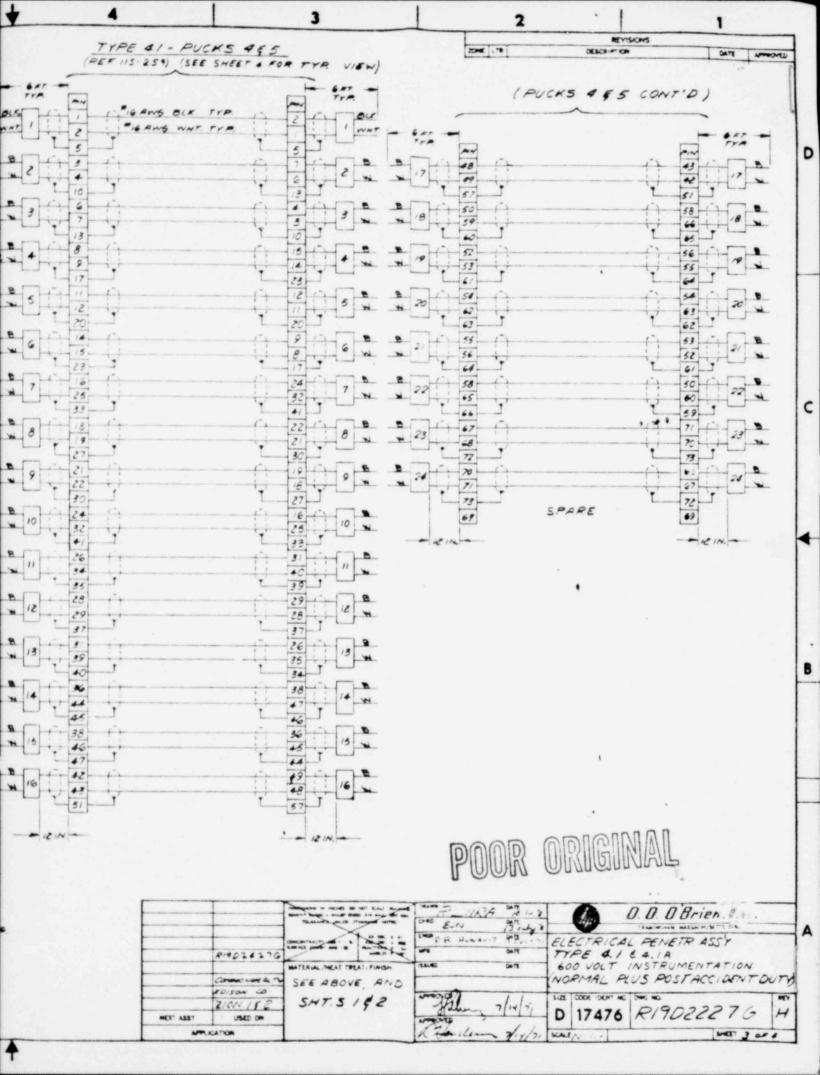


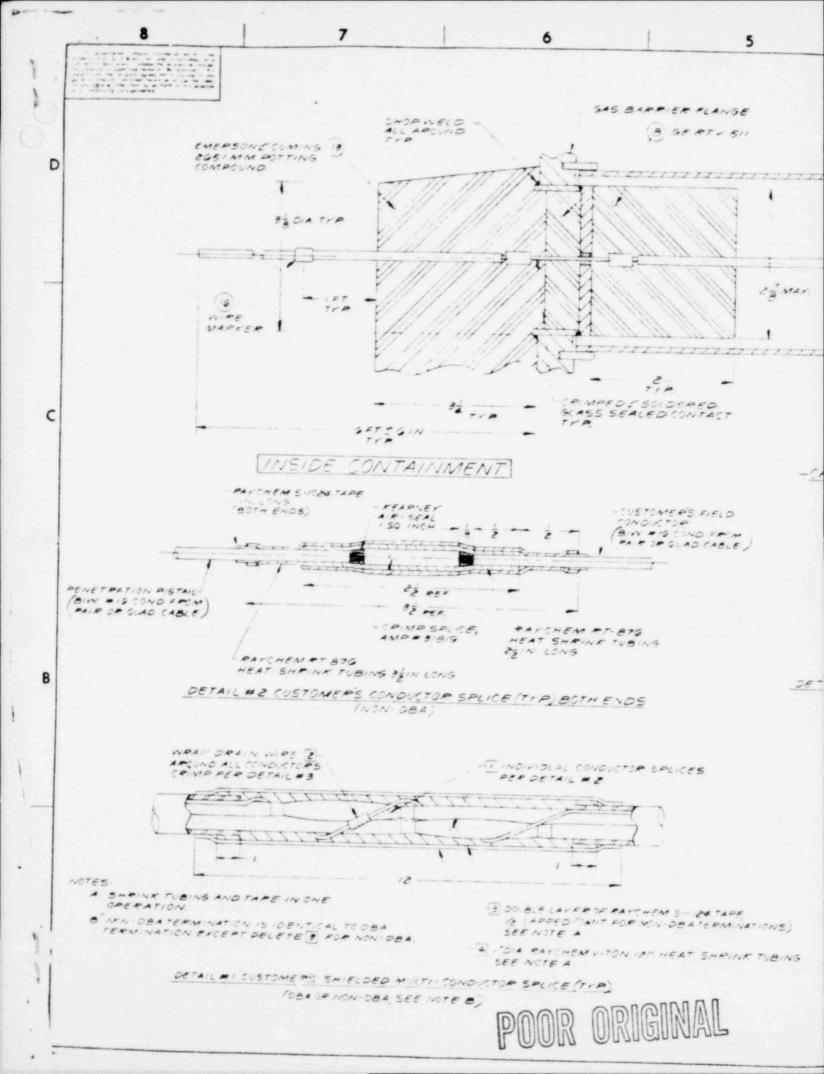


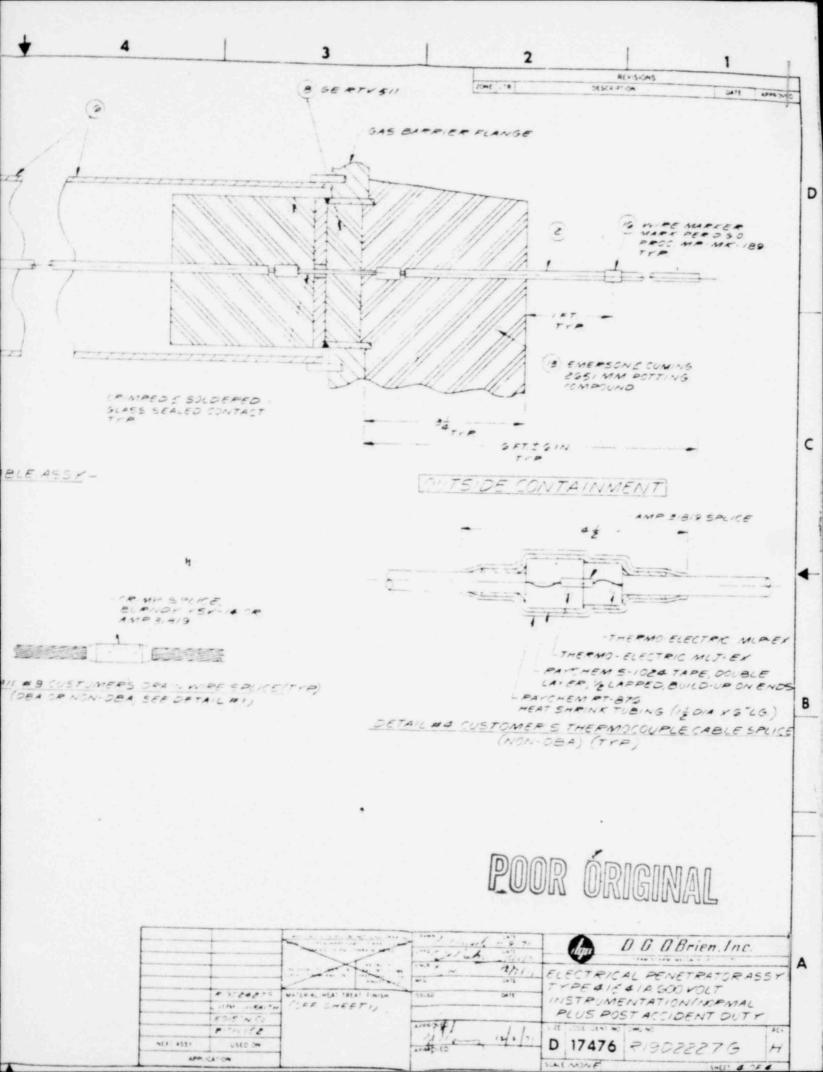












3.3.2.8 Equipment Item No. 17
Electrical Penetrations Located
Within and Outside of
Containment
D. G. O'Brien, Type 3.1
(Submittal Page References 2 and 3)

Response:

1. The attached xerox copies of portions of the D. G. O'Brien Instruction Manual No. 1016 for Type 3.1 and 3.1A Electrical Penetrations identify the materials used, including jacket and insulation materials for cable leads.

The environmental test referenced in Section 4 of the Test Report C19QA051 was a saturated steam atmosphere of 70 psig pressure, 298°F temperature, 100% RH for a 1-hour period, followed by 47 psig pressure, 271°F temperature, 100% RH for a period of 48 hours.

- We are still attempting to obtain information from the Vendor, D. G. O'Brien, to determine the effects of maximum normal and short circuit loads on the conductors simultaneous with and during a postulated LOCA.
- We are still attempting to obtain information from the Vendor, D. G. O'Brien, to determine a qualified life.

Instruction Monual (1016)
For

REACTOR CONTAINMENT STRUCTURE

ELECTRICAL PENETRATION ASSEMBLY

TYPES 3.1 AND 3.1A (Serial

Numbers 3.1Z1 - 3.1Z6 and 3.1AZ1-3.1AZ6)

September, 1971

Prepared For Use On
ZION STATION UNITS I AND II
(Commonwealth Edison Co., Contract 113967)

D. G. O'Brien, Inc. 500 Cochituate Rd., Framingham, Mass.

P.R Venault			Dot	e 9/7/71
R. Henault, Project	ct Electrical	Engineer		9/7/71
Button, Project	ct Mechanical	Engineer		9/7/7/

INTRODUCTION

The Electrical Penetration Assembly described herein was designed and manufactured by D. G. O'Brien, Inc., Framingham, Mass. for use in the construction of Nuclear Power Plant - Zion Units I and II, Commonwealth Edison Co., Zion, Illinois.

This manual is for use in the installation, test, calibration, and operation of Type 3.1 penetration assemblies. This penetration is designed for low voltage control cable service.

Penetration assemblies of Type 3.1 and 3.1A (Zion I and Zion II designations respectively) are identical for both Zion Units.

Information pertaining to other types of penetrations also designed and manufactured by D. G. O'Brien, Inc. for Zion Units I and II can be obtained from other Instruction Manuals. This manual is applicable only to Type 3.1.

Quality Assurance data is included under a separate cover.

This penetration assembly is furnished for use with applicable design data of the following Sargent and Lundy drawings:

- ES-42 Typical Electrical Penetration, Physical Requirements, Dated 10/1/69
- B-213 Reactor Building Containment, Liner Plate Sections and Details, Sheet 2 Rev. T, Dated 10/3/69
- B-214 Reactor Building Containment,
 Penetration Schedule, Rev. L,
 Rev. L, Dated 10/3/69
- B-216 Reactor Building Containment, Elevation Electrical Penetrations, Rev. G, Dated 10/3/69

The penetration assembly described herein is furnished by D. G. O'Brien, Inc., as part of an ASME Class B Nuclear Vessel.

The electrical penetrations for Nuclear Generating Power Plants manufactured by D. G. O'Brien, Inc., are engineered to meet the stringent requirements of the electrical power industry and the Atomic Energy Commission. The careful integration of many scientific and technical disciplines has gone into the development of a product that is reliable and efficient. Careful control of manufacturing processes and materials plus extensive in-process and final testing ensures that the finest product is delivered to the customer.

This manual is prepared to give the customer, in readily available form, the information necessary to efficiently install and maintain the purchased equipment. References throughout this manual to the Type 3.1 assembly also are applicable to type 3.1A assemblies, unless otherwise specified.

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7-1	 Termination Drawing			26

- 1.0 GENERAL DESCRIPTION
- 1.1 Low Voltage Control Cable Penetration Assembly (D.G.
 O'Brien, Inc. Part No. R19D2226G01) herein referred
 to as the penetration assembly will be used as an
 interface for passing the Purchaser's low-voltage control
 cables from outside the containment to inside the containment. As such, it will become a critical portion of
 the cabling system associated with the reactor nuclear
 control system.
- 1.2 The penetration assembly will extend low voltage control power from outside the containment to circuits and elements located inside the containment.
- 1.3 The assemblies are designed and constructed for installation in 12-inch diameter steel pipe containment penetration nozzles that are 3 feet, 6 inches long. Each penetration assembly is identical in basic physical configuration and contains the inside mechanical seal permanently attached. The outside mechanical seal, required for field installation, is furnished separately in the same shipping carton.
- 1.4 The penetration assembly must be inserted into the containment structure nozzle fxm inside the containment and is permanently installed by means of field welding at the site. Mechanical supports are necessary to position the assembly during the welding operation.

- 1.5 Each assembly is designed to restrain loading due to electrodynamic forces or mechanical stressing. Internally, this is achieved, where required, by groups of tubular cable guides extending the full length of the penetration assembly.
- 1.6 Every penetration assembly is permanently identified by a serial number. Every wire, external to the assembly, is marked at each end with an identification number as specified by the purchaser. Wire numbers in any one multiconductor cable are not repeated.
- Sealing and Pressurization. The penetration assemblies provide a dual gas barrier by means of steel header flanges and hermetically glass-sealed electrical contacts. Each of the two gas barriers meet the service environmental conditions individually, providing an overall performance safety factor of two. The double-pressure barrier is continued at installation by welding the mechanical seals as required. Both the internal volume of the penetration assembly and that between it and the penetration nozzle may be pressurized through a pressurization port in the outside containment mechanical seal and vent holes in the canister. The canister assemblies are pressurized to 15 PSIG with dry nitrogen prior to shipment. One day prior to installation, the assembly should be uncrated and any gross pressure differential of the penetration assembly in transit and storage may be observed on the pressure gauge that forms part of the assembly. Prior to assembly, the canister must be

pressurized to 54 PSIG and observed for a period of one day. If there is no indication of leakage at the end of this period of time installation procedures should be initiated.

CAUTION

PRIOR TO INSTALLATION, THE PENETRATION
ASSEMBLY SHOULD BE DEPRESSURIZED AND THE
PRESSURE GAUGE ASSEMBLY AND VENT PORT
PLUGS REMOVED. REFER TO SECTION 4.0 OF
THIS MANUAL.

Safety Factors in Production. Pneumatic testing is 1.8 performed on the prototype and on each production assembly in accordance with the latest revision of Paragraph N-110 in Section III of the ASME Boiler and Pressure Vessel Code and as covered in detail in the Quality Assurance Instruction Data. The allowable leak rate of both penetration gas barriers in series in prototype testing is equal to, or less than, 1×10^{-6} standard cc/sec. of dry helium at 298°F and 54 PSIG. In production, each penetration assembly is subjected to a leak rate test at 54 PSIG and 78°F ±5°F and will not exceed 1 x 10^{-6} standard cc/sec. through both penetration gas barriers in series. Due to controlled production processes, hermetically glass-sealed headers or gas barriers consistently better the leak rate of 1×10^{-6} by two orders of magnitude.

1.9 Cable Description

- 1.9.1 Internal Cables. The internal cables and external pigtails are directly terminated to glass-sealed contacts in connectors (pucks) welded into the gas barriers. The electrical characteristics of the internal cables are identical to the purchaser's cables within the tolerances allowed.
- 1.9.2 External Cable Terminations. External cable terminations are made to the pigtail leads on each puck. The pucks are a related part of the penetration assembly gas barrier. All cables are soldered. They are designed and built to function in accordance with the requirements of the circuits they service. All conductors are insulated from each other and from ground.

- 1.9.3 The prototype and all production models are tested to the following:
 - A. Insulation:
 - 1. Test Voltage 500VDC
 - 2. Minimum Insulation Resistance

 Conductor-to-conductor 1×10^8 ohms-ft.

 Conductor-to-ground 1×10^8 ohms-ft.
 - B. Dielectric Strength:

Ten Seconds, 60 HZ 2200 V AC RMS

Table 1-1 summarizes the technical and design parameters and provides a ready reference of data.

TYPE 3.1 CONTROL ELECTRICAL PENETRATOR DESIGN PARAMTER SUMMARY

402-1KV 14 AWG, (7/.0242) 1. Number of Conductors Kerite 3/64" FR Insulation & 3/64" FR Jacket Material & Size of 2. #14 AWG (7/.0242") Tinned Coppe Conductors: Current or Signal 10 AMP 3. Kerite Type FR Synthetic Rubbe: Conductor Insulating Material Insulation & Jacket 90°C Temperature 4. Provision for Connection Pigtail Leads of Purchaser's External Cable 5. High Potential Test On 2200 vrms Production Assemblies for One Minute 6. Assembly Body Material . 10" I.P.S. Sch. 20 Pipe, ASTM, A-333, GR-1, Carbon Steel End Header Plater 7. ASTM, A-442, GR-60 Carbon Stee. Moterial or ASTM A-516, GR-70 End Header Plute Leaded Carbon Steel Per AISI, C1213 (Tin Plated) Conductor Material 9. End Header Plate 9010 Glass Conductor Insulating Material 10. Assembly Dimension: 10.3/4" Body Outer Diameter 4' 61" Body Length 1.7 x 108 Rad (1.5 MEV 11. Maximum Integrated gamma rays) Radiation Exposure 2.24 x 10-5 cc.

(Air) Min.

Maximum Total Assembly

12.

- 13. Minimum Insulation
 Resistance @ 500 VDC:
- · 1 x 10⁸ ohms-ft
- 14. Total Assembly Calculated Weight
- 600 pounds

- 15. Shipping Pressurization Storage Pressurization
- 15 PŚIG Dry Nitrogen 54 PSIG Dry Nitrogen

16. Design Current Rating

10 amperes, nominal 20 amperes, 1 minute everload

6.0 WIRING

The following drawings (Figures 6-1, 6-2) depict the wiring diagram electrical connections of the Zion I and II Electrical Penetration, Type 3.1 Low Voltage Control Service for Normal Non-Accident Duty plus Post-Accident Operation on no greater than 10 percent of the conductors.



CABLE 1KV 14 AWG Kerite

CONDUCTOR:	14 AWG 7 Strand (7/.0242) Tin plated copper	OD	0.072"
INSULATION:	Rubber Kerite 3/64" Wall "FR" Insulation Black	OD	0.170"
JACKET:	Rubber, Synthetic, Kerite "FR" Block 3/64" Wall	OD	0.274"

Figure 6-2 1KV CABLE (Kerite)

7.0 TERMINATION INFORMATION

Prior to assembly of any hardware on the penetration assembly, a review of D. G. O'Brien, Inc. Drawing R19D2226G (Sheets 1 and 3) should be made to ascertain layout and sequence for splicing of wires. This drawing also illustrates the location of puck assemblies and electrical connection sequence. The required hardware and material for termination are included in the shipping carton, Kit P/N 115-301.

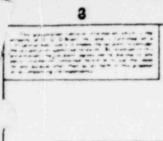
CAUTION

PRIOR TO ASSEMBLY CHECK PIGTAILS AND POTTING WITHIN PUCKS FOR INDICATIONS OF DAMAGE.

All work should be done in as clean an area as possible, well ventilated, and free from moisture and work hazards.

Purchaser's Field cables shall be prepared as outlined in D. G. O'Brien, Inc. Drawing R19D2226G for termination to the Burndy or AMP wire splices.

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)	REV	SHT	0F	BEMARKS					Alternate)				Alternate)										
1.1	n./nc. P.L. DATE 115-301	ALITHENTICATION CHGE, CONT. NO. CODE IDENT. NO.			DESCRIPTION	J.O. 62004 Item 3.1 Outside Cont.	J.O. 62004 Item 3.1 Inside Cont.	Splice, Crimp, 14AWG, Burndy	Splice, Crimp 14AWG, AMP	Splice Kit, Kerite	Splice Kit, Kerite	Tool, Crimp, Burndy	Tool, Crimp, AMP, Inc.	Pad, Air Seal, Kearney	Tubing, Heat Shrink, Raychem	Tubing, Heat Shrink, Raychem R	Tape, Heat Sealable 3/4" wide Raychem						-259-
	D. G. O'Brien. Inc.	FRAMINGHAM, MASS.	FIELD TERMINATION KIT ZION 3.1	CNONIX	(DRAWING NO.)			V5V14	31819	08-1001	05-1133	Y9M or Y10M	49900 or 49935	2" × 4"	3/8" I.D. x 3" long	1/2" I.D. x 4" Long	51024						
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			TERMI	GROUP	OTY. REOD																		
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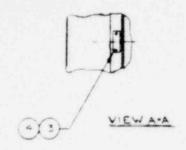
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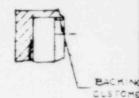
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ZOOV CONTROL SERVICE

ITEM 3

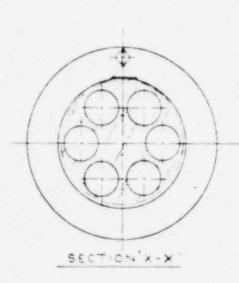


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PEALA

NSTALLED AT
FIELD INSTALLATIO
IN PRESSURE GAUGE
ASSEMBLY PORT



SEE DETAIL A

SIGNA

ACF

PAGE

NOTES

C

- IL THIS PENETRATION SHALL MEET THE REQUIREMENTS OF THE ASME BOILER AND PRESSURE VESSELS CODE, SECTION III, CLASS BYESSELS.
- 2. DESIGN PRESSURE : 54 PSIG.
- 5. PESIGN TEMPERATURE : 248 F FOR 1 HOUR FOLLOWED BY 271 F FOR 48 HOURS
- 4. MINIMUM DESIGN TEMPERATURE : 30 F
- PADS (1.5 MEV. GAMMA RAYS) TOTAL INTEGRATED DOSE
- & PECATIVE HUMIDITY MAX DUPING THE 40 FEAD LIFE NEDE AND OUTSIDE CONTAINMENT 50".
- T PENSTRATION SERVE TEST : 2363 AT G TO 55 HERTE
- B FOR INSTALLATION WELD & ASSEMBLY
 SEE INSTALLATION DRAWING *AIRDZ*TEGOS

- 9. REFER TO SARGENT & LUNDY

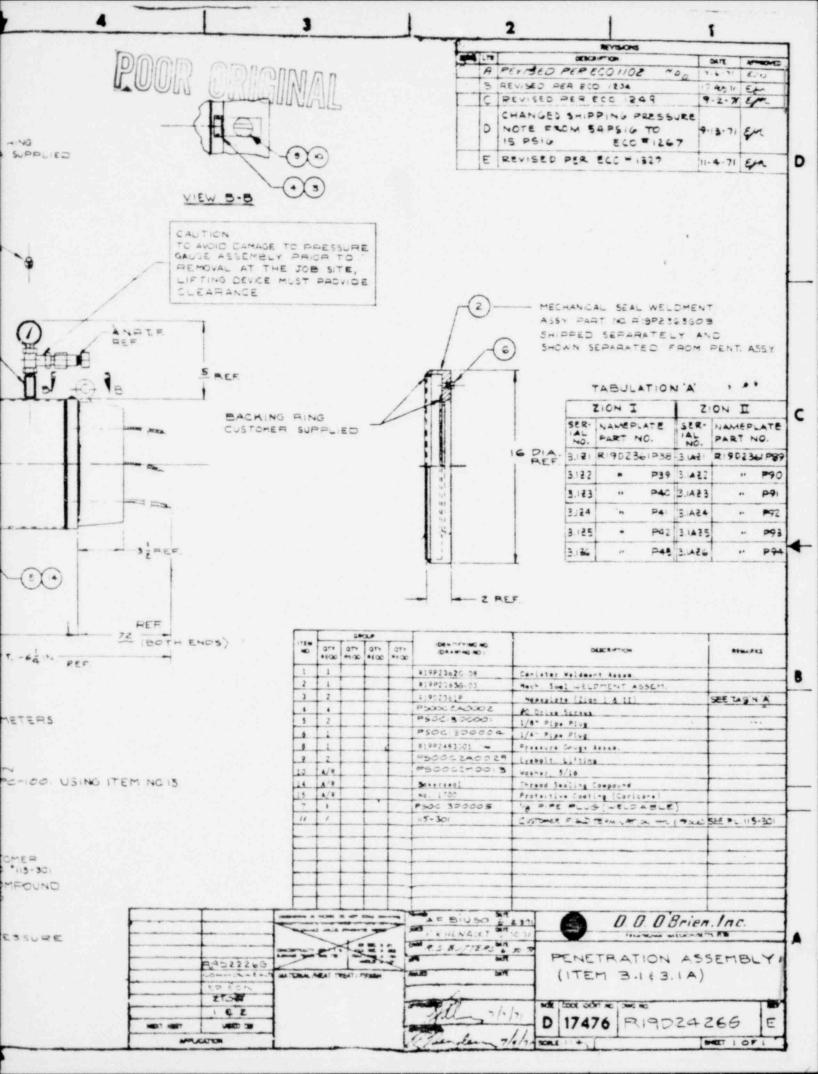
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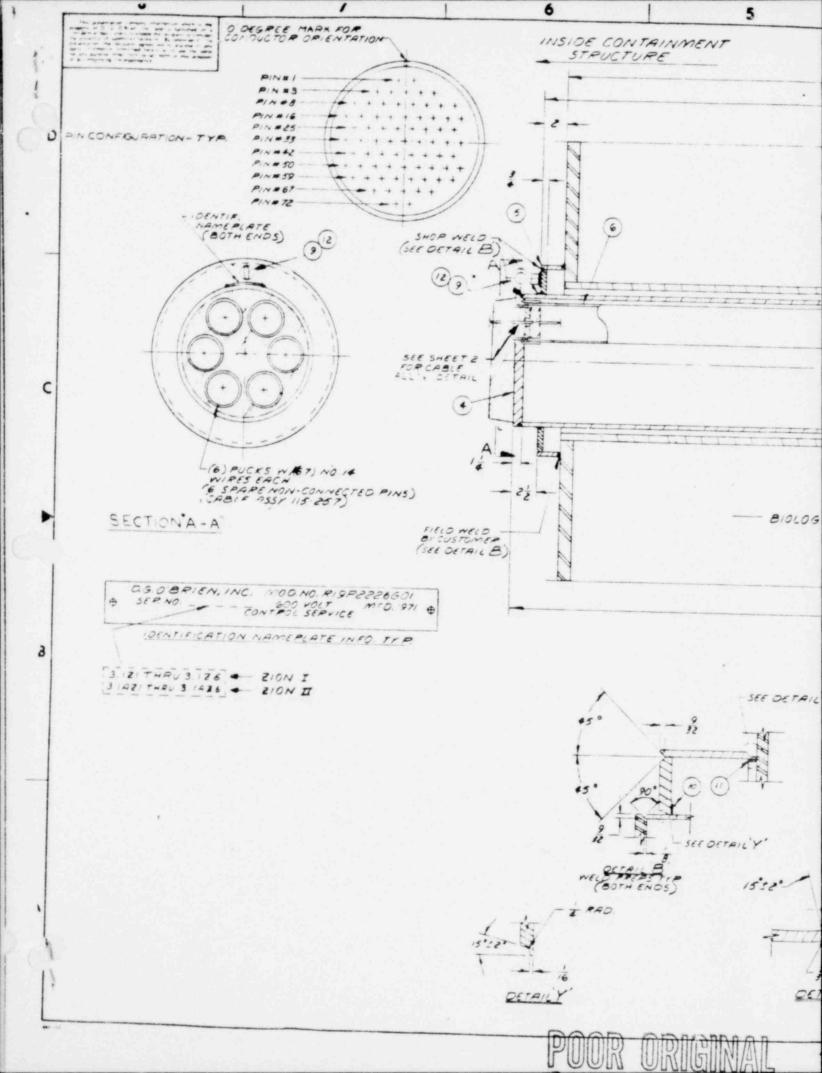
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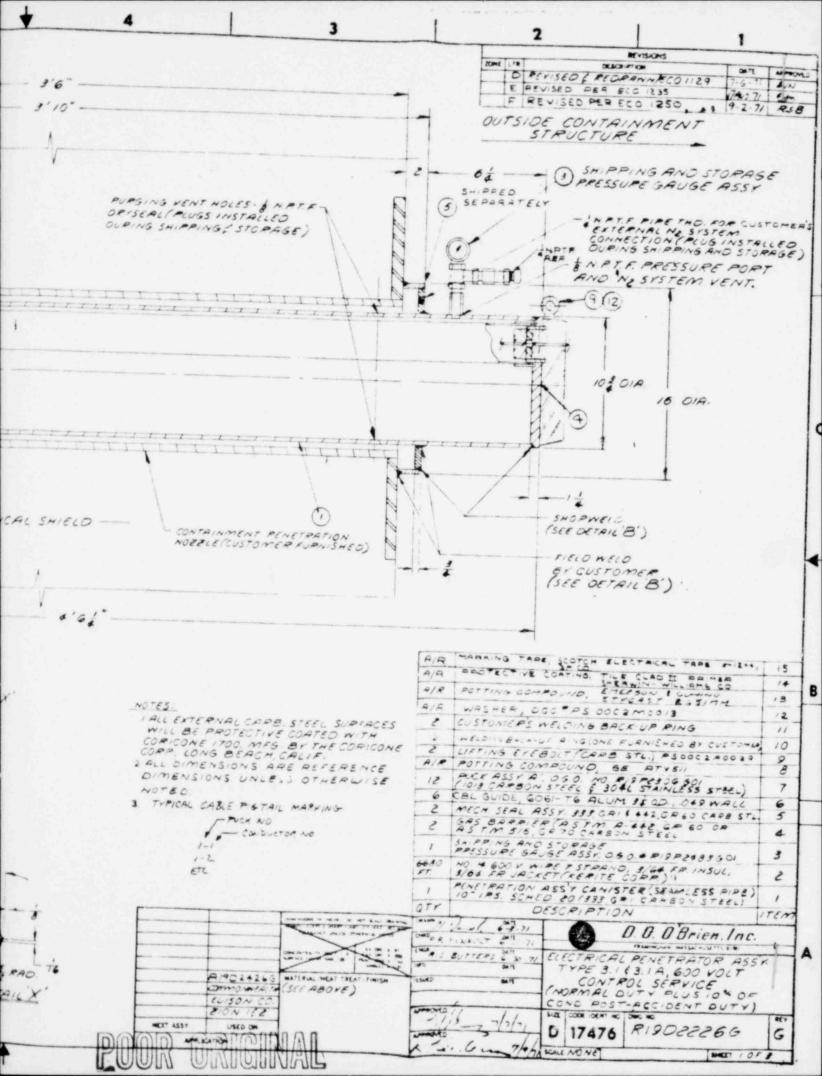
 DOD QUALITY ASSURANCE METHOD

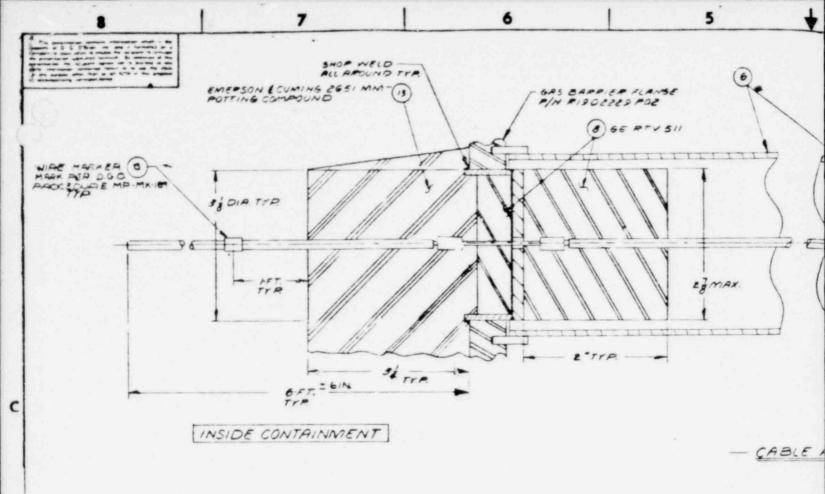
 SHEET \$1-TM-153-5 FOR SPECIFIC TEST PARK
- STEEL SURFACES PER DOO FROM PP
- II APPROXIMATE WEIGHT 600 LSS.
 - 12. FOR CABLE TERMINATION ITEMS, SEE CLS
 - IS USE ONLY BAKERSEAL THREAD SEALING ON ALL DRYSEAL PIPE THREAD ASSEMBLE
 - 14 PENETRATION INTERNAL SHIPPING

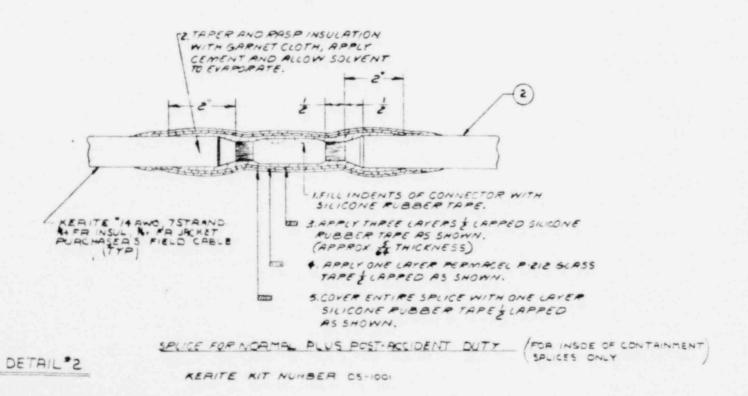
POOR ORIGINAL





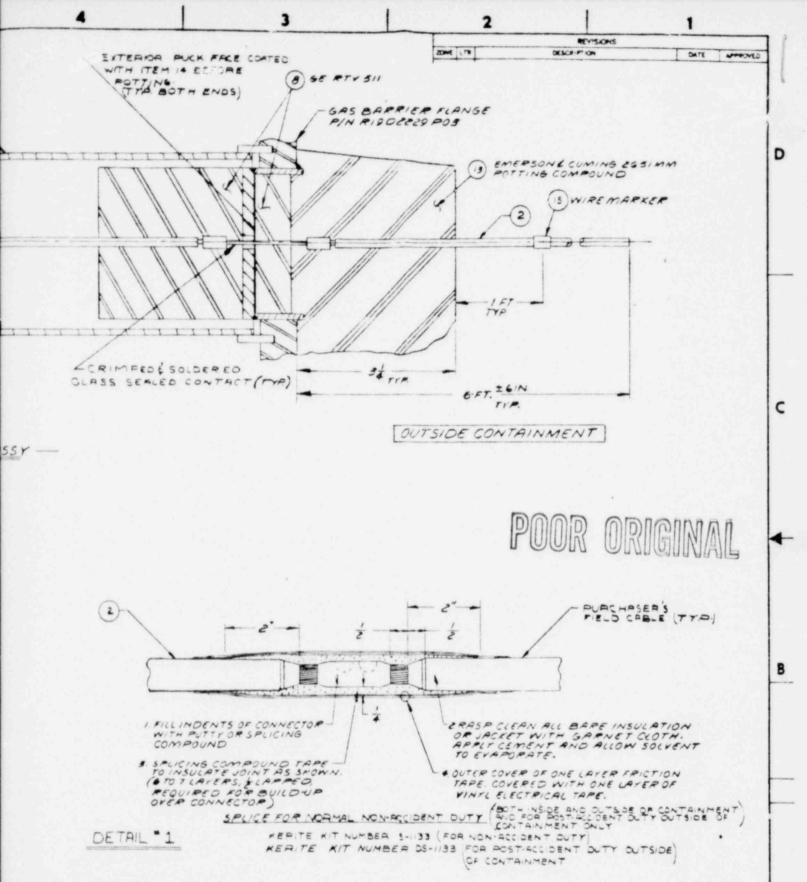


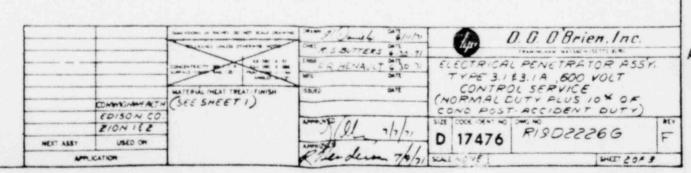




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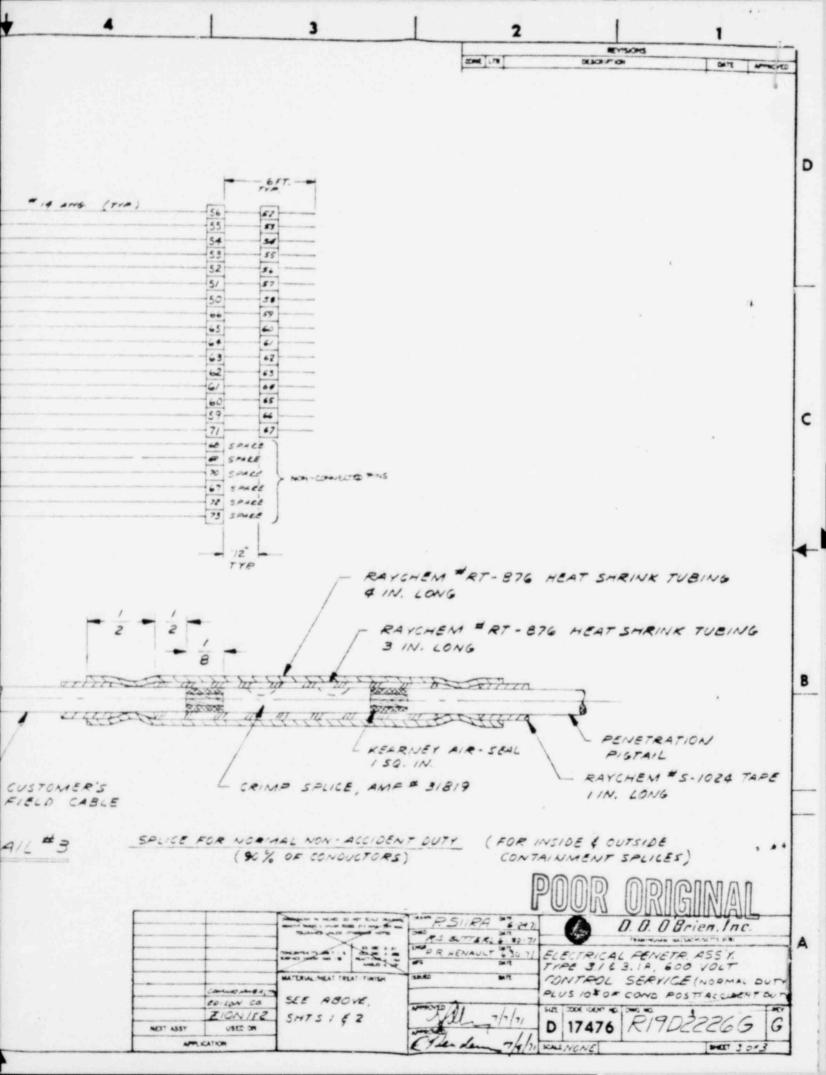
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The programme of contains introduce on which is the rest of the total or the contains on which is the rest of the contains of WIRING DIAGRAM (TYP PUCKS "1 THROUGH "6) -65 TYP 7.6.T AN PIN 14 AWG (TYP) 2 1 7 -. . , ~ 8 24 23 22 21 20 19 65 66 68 .5 -6 , > 18 20 21 22 23 SMES Smet SPACE 7/ 3mc6 25 26 de 3/ 30 29 28 27 26 25 12" 3/ 3/ #0 39 38 37 35 36 37 × 90 40 42 43 44 45 * . 48 47 46 1: DET 57 TEP TTE WIRE MARKER 15 TYP

POOR ORIGINAL



3.3.2.9 Equipment Item No. 18
Electrical Penetrations
Located Within and Outside
of Containment
D. G. O'Brien, Types 2.1, 2.2 and 2.3
Submittal Page References 2 and 13

Response:

 The attached xerox copies of the D. G. O'Brien Instruction Manual No. 1030 for Type 2.2 and 2.2A Electrical Penetrations identify the materials used, including jacket and insulation materials for cable leads.

The environmental test referenced in Section 4.8 of the Test Report C19QA058 was a saturated steam atmosphere of 46 psig pressure, 273°F temperature for a 48-hour period. Following the environmental test, a leak rate test using helium at approximately 275°F was conducted with specified leak rate being met (reference Section 4.09 of Test Report C19QA058).

Thermal aging and radiation exposure of the cable leads are covered by Franklin Institute Test Report FC-2737 and the attached letter to Mr. H. K. Stolt from Mr. R. M. Bowman (Kerite Company) dated August 28, 1980.

We are attempting to obtain copies of the Instruction Manuals for Types 2.1, 2.1A, 2.3 and 2.3A penetrations to be able to indicate the materials used. It should be noted that Types 2.1, 2.1A, 2.3 and 2.3A are not used for safety functions but have been included in the report because they form a part of the containment pressure boundary.

- We are still attempting to obtain information from the Vendor, D. G. O'Brien, to determine the effects of maximum normal and short circuit loads on the conductors simultaneous with and during a postulated LOCA.
- 3. We are still attempting to obtain information from the Vendor, D. G. O'Brien, to determine a qualified life.

Instruction Manual (1030)

For

REACTOR CONTAINMENT STRUCTURE

, ELEC RICAL PENETRATION ASSEMBLY

TYPES 2.2 AND 2.2A

(Serial Numbers 2.2Z1 - 2.2Z5 AND 2.2AZ1 - 2.2AZ5)

JANUARY, 1972

Prepared For Use On ZION STATION UNITS I AND II (Commonwealth Edison Co., Contract 113967)

D. G. O'Brien, Inc. 500 Cochituate Road., Framingham, Mass.

Approved by:

P. Hilberg, Engineering Manager

Nuclear Power Plant Systems

INTRODUCTION

The Electrical Penetration Assembly described herein was designed and manufactured by D. G. O'Brien, Inc., Framingham, Mass. for use in the construction of Nuclear Power Plant - Zion Units I and II, Commonwealth Edison Co., Zion, Illinois.

This manual is for use in the installation, test, calibration, and operation of Type 2.2 penetration assemblies. This penetration is designed for low voltage power cable service.

Penetration assemblies of Type 2.2 and 2.2A (Zion I and Zion II designations respectively) are identical for both Zion Units.

Information pertaining to other types of penetrations also designed and manufactured by D. G. O'Brien, Inc. for Zion Units I and II can be obtained from other Instruction Manuals. This manual is applicable only to Type 2.2.

Quality Assurance data is included under a separate cover.

This penetration assembly is furnished for use with applicable design data of the following Sargent and Lundy drawings:

- ES-42 Typical Electrical Penetration, Physical Requirements, Dated 10/1/69
- B-213 Reactor Building Containment, Liner Plate Sections and Details, Sheet Rev. T, Dated 10/3/69
- B-214 Reactor Building Containment, Penetration Schedule, Rev. L, Dated 10/3/69
- B-216 Reactor Building Containment, Elevation Electrical Penetrations, Rev. G, Dated 10/3/69.

The penetration assembly described herein is furnished by D. G. O'Brien, Inc. as part of an ASME, Class B Nuclear Vessel.

The electrical penetrations for Nuclear Generating Power Plants manufactured by D. G. O'Brien, Inc. are engineered to meet the stringent requirements of the electrical power industry and the Atomic Energy Commission. The careful integration of many scientific and technical disciplines has gone into the development of a state-of-the-art product that is reliable, rugged, dependable, efficient, and economical. Careful control of manufacturing processes and materials plus extensive in-process and final testing ensures that the finest product is delivered to the customer.

This manual is prepared to give the customer, in readily available form, the information necessary to efficiently install and maintain the purchased equipment. References throughout this manual to type 2.1 assembly are also applicable to type 2.1A assemblies, unless otherwise specified.

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5-2	Typical Welding, Zion I & II	21
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7-1	Termination Drawing	25

- 1.1 Low Voltage Power Cable Penetration Assembly (D.G.
 O'Brien, Inc. Part No. R19D2224G01) herein referred
 to as the penetration assembly will be used as an
 interface for passing the Purchaser's low-voltage power
 cables from outside the containment to inside the containment. As such, it will become a critical portion of
 the cabling system associated with the reactor nuclear
 power system.
- 1.2 The penetration assembly will extend low volcage power from outside the containment to circuits and elements located inside the containment.
- 1.3 The assemblies are designed and constructed for installation in 12-inch diameter steel pipe containment penetration nozzles that are 3 feet, 6 inches long. Each penetration assembly is identical in basic physical configuration and contains the inside mechanical seal permanently attached. The outside mechanical seal, required for field installation, is furnished separately in the same shipping carton.
- 1.4 The penetration assembly must be inserted into the containment structure nozzle from inside the containment and is permanently installed by means of field welding at the site. Mechanical supports are necessary to position the assembly during the welding operation.

- 1.5 Each assembly is designed to restrain loading due to electrodynamic forces or mechanical stressing. Internally, this is achieved, where required, by groups of tubular cable guides extending the full length of the penetration assembly.
- 1.6 Every penetration assembly is permanently identified by a serial number. Every wire, external to the assembly, is marked at each end with an identification number as specified by the purchaser. Wire numbers in any one cable are not repeated.
- Sealing and Pressurization. The penetration assemblies 1.7 provide a dual gas barrier by means of steel header flanges and hermetically glass-sealed electrical contacts. Each of the two gas barriers meet the service environmental conditions individually, providing an overall performance safety factor of two. The double-pressure barrier is continued at installation by welding the mechanical seals as required. Both the internal volume of the penetration assembly and that between it and the penetration nozzle may be pressurized through a pressurization port in the outside containment mechanical seal and vent holes in the canister. The canister assemblies are pressurized to 15 PSIG with dry nitrogen prior to shipment. One day prior to installation, the assembly should be uncrated and any gross pressure differential of the penetration assembly in transit and storage may be observed on the pressure gauge that forms part of the assembly. Prior to assembly, the canister must be

pressurized to 54 PSIG and observed for a period of one day. If there is no indication of leakage at the end of this period of time installation procedures should be initiated.

CAUTION

PRIOR TO INSTALLATION, THE PENETRATION

ASSEMBLY SHOULD BE DEPRESSURIZED AND THE

PRESSURE GAUGE ASSEMBLY AND VENT PORT

PLUGS REMOVED. REFER TO SECTION 4.0 OF

THIS MANUAL.

- Safety Factors In Production. Pneumatic testing is 1.8 performed on the prototype and on each production assembly in accordance with the latest revision of Paragraph N-110 in Section III of the ASME Boiler and Pressure Vessel Code and as covered in detail in the Quality Assurance Instruction Data. The allowable leak rate of both penetration gas barriers in series in prototype testing is equal to, or less than, 1×10^{-6} standard cc/sec. of dry helium at 298°F and 54 PSIG. In production, each penetration assembly is subjected to a leak rate test at 54 PSIG and 78°F ±°F and will not exceed 1 x 10⁻⁶ standard cc/sec. through both penetration gas barriers in series. Due to controlled production processes, hermetically glass-sealed headers or gas barriers consistently better the leak rate of 1 \times 10⁻⁶ by two orders of magnitude.
- 1.9 Cable Description
- 1.9.1 Internal Cables. All the internal cables and external pigtails on #6 AWG Conductors only are directly terminated to glass-sealed contacts in center connector (puck) welded into the gas barriers. The electrical characteristics of the internal cables are identical to the purchaser's cables within the tolerances allowed.
- 1.9.2 External Cable Terminations. External cable terminations are made to the pigtail leads on the center puck only.

 The pucks are a related part of the penetration assembly gas barrier. All cables are soldered on the center puck only. All other contacts in the outer periphery are crimped. They are designed and built to function in accordance with the requirements of the circuits they service. All conductors are insulated from each other and from ground.

- 1.9.3 The prototype and all production models are tested to the following:
 - A. Insulation Resistance
 - 1. Test Voltage 500 VDC
 - 22. Minimum Insulation Resistance

 Conductor-to-conductor 1×10^8 ohms-ft.

 Conductor-to-ground 1×10^8 ohms-ft.
 - B. Dielectric Strength:

Prototype:

Conductor-to-conductor 750 MCM 5,000 VAC RMS
Conductor-to-conductor #6 AWG 3,000 VAC RMS

Time: 5 minutes

Production:

Conductor-to-conductor 2,200 VAC RMS

TYPE 2.2 LOW VOLTAGE POWER CABLE PENETRATOR DESIGN PARAMETERS

1. Number of Conductors:

6 #750 MCM, 1000V rated,
61 Strands, plated copper wire,
7/64" wall of Kerite HTK insulation
with a 5/64" wall of Kerite "FR"
synthetic rubber jacket

Plus:

18 #6 AWG, 1000V rated,
7 strands, plated copper wire,
4/64" of Kerite HTK Insulation
with a 4/64" wall of Kerite
"FR" synthetic rubber jacket.

2. Material & Size Of Conductors:

750 MCM - 61/.1109" Tin Plated copper wire 6 AWG - 7/.0612" Tin Plated Copper Wire

Current

750 MCM - 250 AMP 6 AWG - 40 AMP

 Conductor Insulating Material 750 MCM - 7/64" Wall of Kerite
"HTK" synthetic rubber insulation
and 5/64" Wall of Kerite "FR"
synthetic rubber jacket
6 AWG - 4/64" wall of Kerite
"HTK" Synthetic rubber insulation
and 4/64" wall of Kerite "FR"
synthetic rubber jacket.

Temperature Rating:

90°C

4. Provisions for connection of Purchaser's external cable

750 MCM - threaded stud connector #6 AWG - Pigtail leads

5. High Potential Test On Production Assemblies
For One Minute

Conductor-to-conductor 2,200 VAC RMS

6. Assembly Body Material

10" I.P.S. Sch. 20 Pipe, ASTM, A-333, GR-1, Carbon Steel

 End Header Plater Material ASTM, A240, 304L Stainless Steel

8. End Header Plate Conductor Material Copper, Oxygen Free, CDA Type 102 (Hard Temper)

9. End Header Plate
Conductor Insulating
Material

9010 Glass

- 10. Assembly Dimension: Body Outer Diameter Body Length
- 11. Maximum Integrated
 Radiation Exposure
- 12. Maximum Total Assembly
- 13. Minimum Insulation Resistance @ 500 VDC:
- Total Assembly Calculated Weight
- 15. Shipping Pressurization
 Test Pressurization
- 16. Design Current Rating

10 3/4"

1.7 x 10⁸ Rad (1.5 MEV gamma rays)

 2.24×10^{-5} cc. (Air) Min.

Conductor-to-conductor

1 x 10 Ohm-ft.

Conductor-to-ground

1 x 10 Ohm-ft.

450 pounds

15 PSIG Dry Nitrogen
54 PSIG Dry Nitrogen

250 Amperes - 750 MCM 40 Amperes - #6 AWG

6.0 WIRING

The following drawing depicts the wiring diagram electrical connections of the Zion I and II Electrical Penetration, Type 2.2 Low Voltage Power Service for Normal Non-Accident Duty plus Post-Accident Operation on no greater than 10 percent of the conductors.

7.0 TERMINATION INFORMATION

Prior to assembly of any hardware on the penetration assembly, a review of D. G. O'Brien, Inc. Drawing R19D2224G should be made to ascertain layout and sequence for splicing of wires. This drawing also illustrates the location of puck assemblies and electrical connection sequence. The required hardware and material for termination are included in the shipping carton, Kit P/N 115-299.

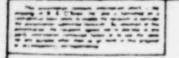
CAUTION

PRIOR TO ASSEMBLY CHECK PIGTAILS AND POTTING WITHIN PUCKS FOR INDICATIONS OF DAMAGE.

All work should be done in as clean on area as possible, well ventilated, and free from moisture and work hazards.

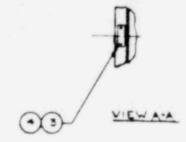
Purchaser's Field Cables shall be prepared as outlined in D. G. O'Brien, Inc. Drawing R19D2224G for termination to Burndy or AMP Wire Splices.

PARTS LIST				-(D. G. D'Brie	n.Inc.	REV. DATE	P.L. 115-299	REV
TITLE FIELD TERMINATION KIT ZION 2,2						AUTHENTICATION	CHGE, CONT. NO.	17476	.NO. SHT_2_ OF
ITEM NO.	QTY. REQD	QTY.	QTY. REQD	QTY. REQD.	IDENTIFYING NO. (DRAWING NO.)	DESCRIPTION		REMARKS	
	\times	\times	><			J.O. 62004 Item J.O. 62004 Item			•
01 02 03	6 -	- 6 15	-	_	QD6534T14 QD6540T14 YS6C-L	Connector, Stud Connector, Stud Splice, #6 AWG	to Cable Burn	dy	
	15	15			328180 YRV6CV10-L	Splice, #6 AWG Splice, #6 AWG	to 6 AWG AMP		Alternate
05	10	2			328182 DS1133 DS1001	Splice, #6 AWG Splice Kit, Ker Splice Kit, Ker	ite	Р	Alternate
07	2	2			DS1219 DS1220	Splice Kit, Ker Splice Kit, Ker	ite ite		
09	1 1 1.	1 1 1			MY29 69120-1 47206	Crimp Tool - Bu Crimp Tool - AM Crimp Head Coup	IP.		Alternate Alternate
	1 1 1	1 1			59220-2 59512- 7 69134-1	Valve, 3 Way, M Handle Control Die Set - AMP		al	Alternate Alternate
	1	1			69133-1	Die Set-AMP			Alternate



DE C'BRIEN, INC. MED 1971 MOD NO RIPPZEZAGOI BON" - SER HO. 2281 THRU 2285 BION 2-SER NO ZZAZI THRUZZAZS GOO Y PHR (& MOMEN, & NO GOOD

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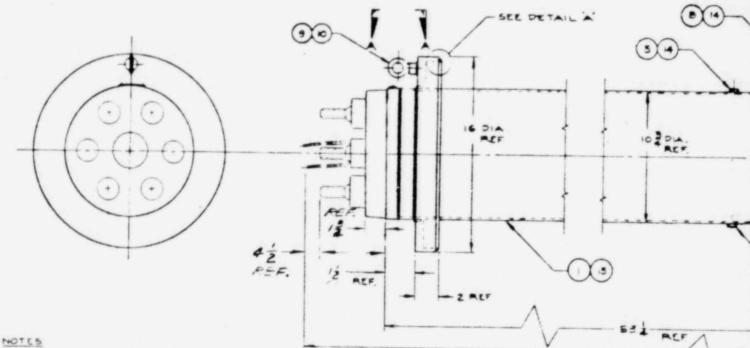


PETAIL'A

7 INSTALLED AT FIELD INSTALLAT IN PRESSURE GA ASSEMBLY PORT

BACK

CUSTO

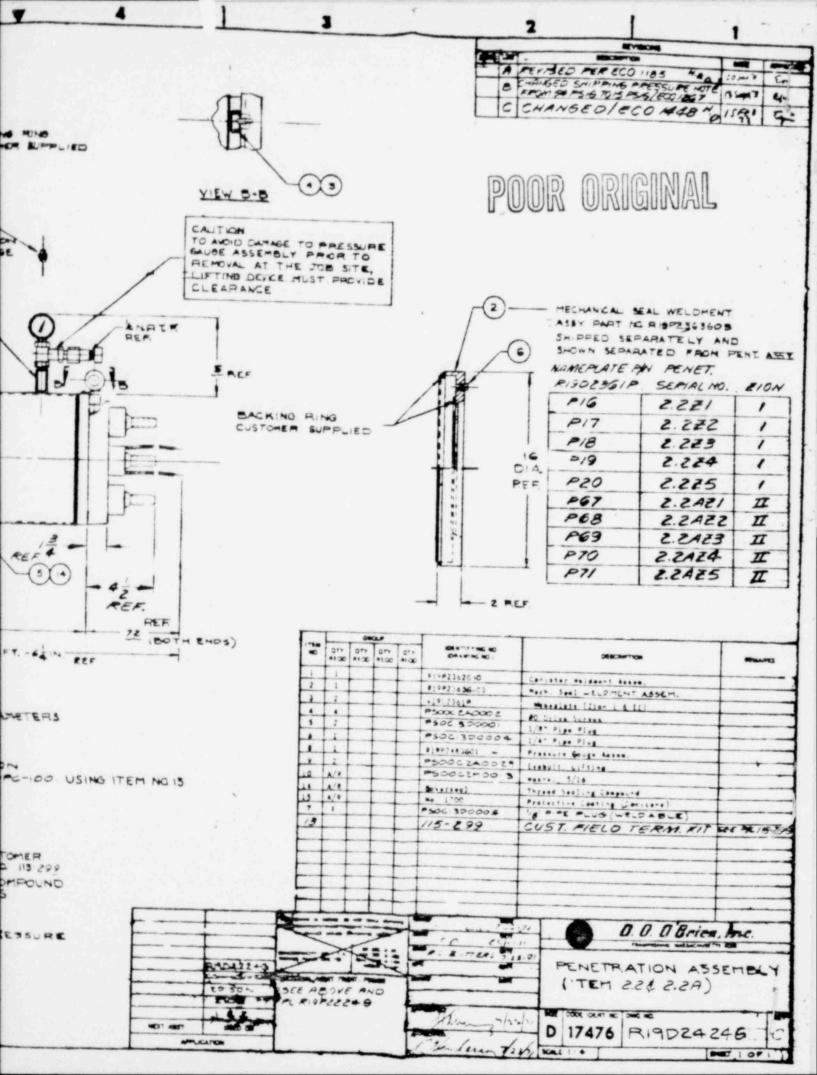


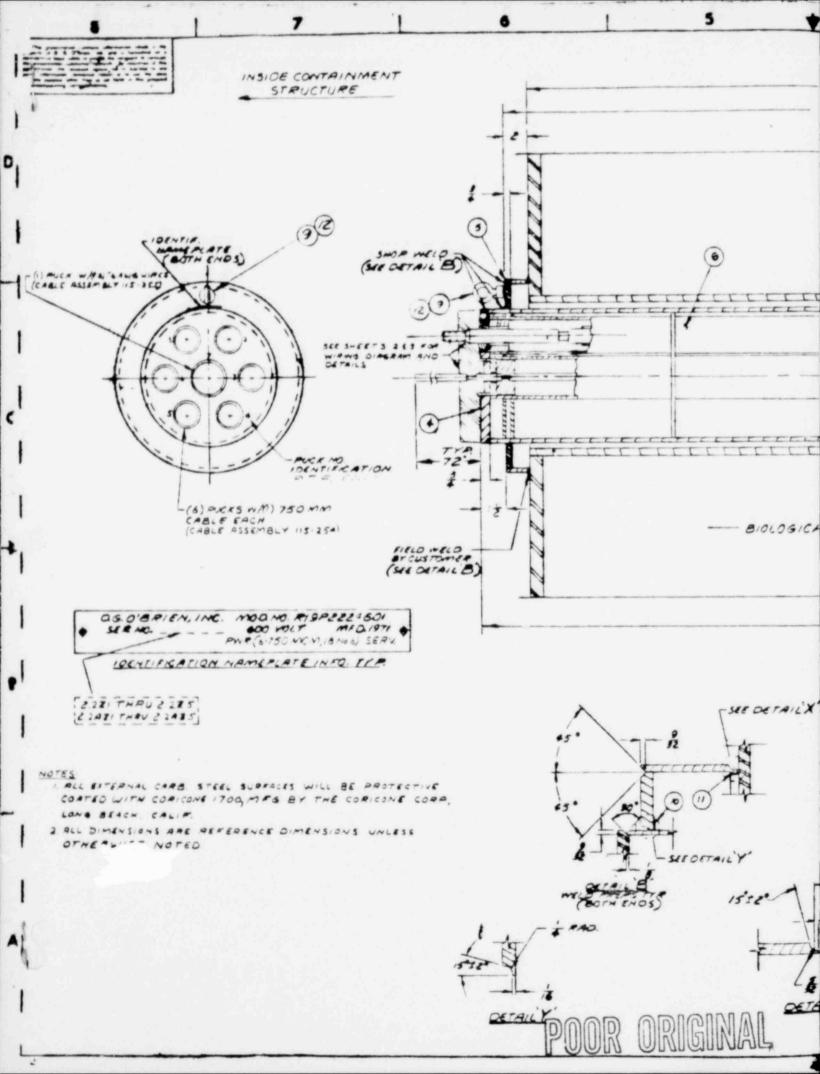
1. THIS PENETRATION SHALL MEET THE REQUIREMENTS OF THE ASME BOILER AND PRESSURE VESSELS CODE, SECTION III, WATER 1969 ADDENDA PARA N-122 FOR AN L DESIGN PRESSURE : 54 PSIG

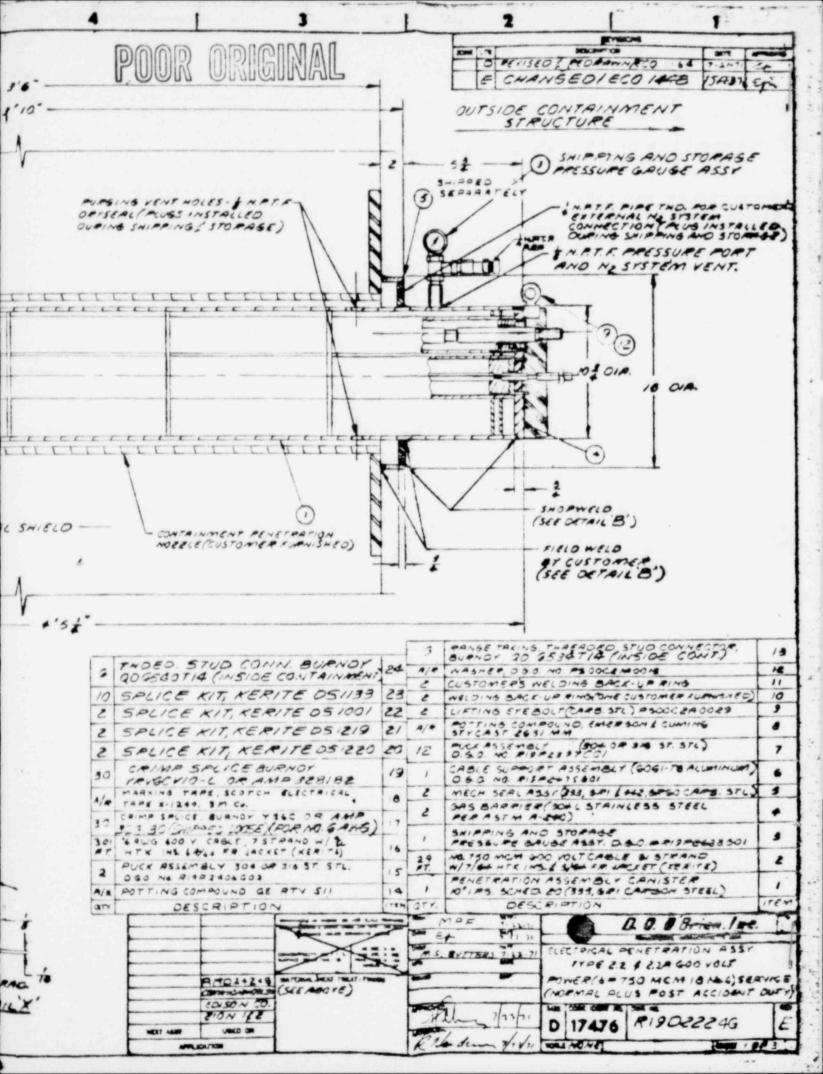
- 5. DESIGN TEMPERATURE : EAS'F FOR ! HOUR FOLLOWED BY 271" F FOR 48 HOURS
- 4. MINIMUM DESIGN TEMPERATURE : 30 F
- 5 DESIGN RADIATION LEVEL: 1.7 x 10 0 RADS (1.5 MEV. GAMMA RAYS) TOTAL INTEGRATED DOSE
- & RELATIVE HUMIDITY MAX DURING THE 40 YEAR LIFE INSIDE AND OUTSIDE CONTAINMENT SOZ
- 7 PENETRATION SEISME TEST : . 256'S AT O TO 55 HERTE
- 8 FOR INSTALLATION WELDING ASSEMBLY SEE INSTALLATION DRAWING "RIADZ476603

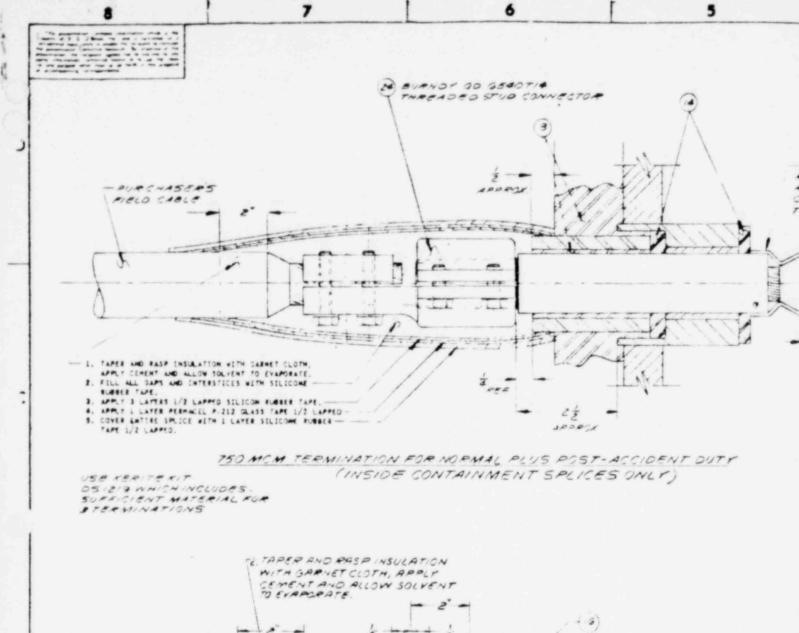
S REFER TO SARGENT & LUNDY SPECIFICATION X-2508 DATED OCT. 1, 1949 INCLUDING ADDENDA IEZ AND DOO QUALITY ASSURANCE METHOD SHEET GA-TH-188 - 5 FOR SPECIFIC TEST PAR

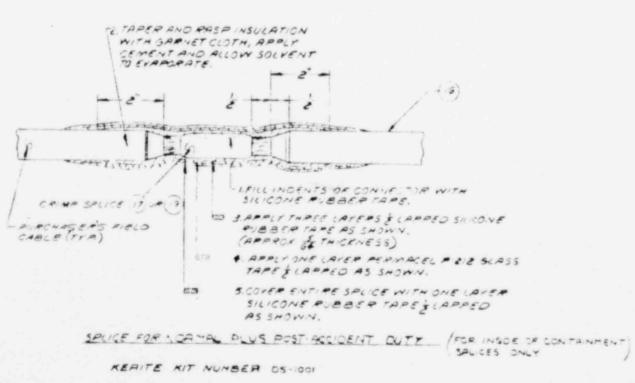
- IC PROTECTIVE COAT ALL EXTERNAL CARE STEEL SURFACES PER DIGO PROS. MP
- III APPROXIMATE WEIGHT 450 LBS.
- IZ. FOR CABLE TERMINATION ITEMS. SEE CUI
- IS. USE ONLY "BAKERSEAL" THREAD SEALING ON ALL DRYSEAL PIPE THREAD ASSEMBLE
- 14 PENETRATION INTERNAL SHIPPING

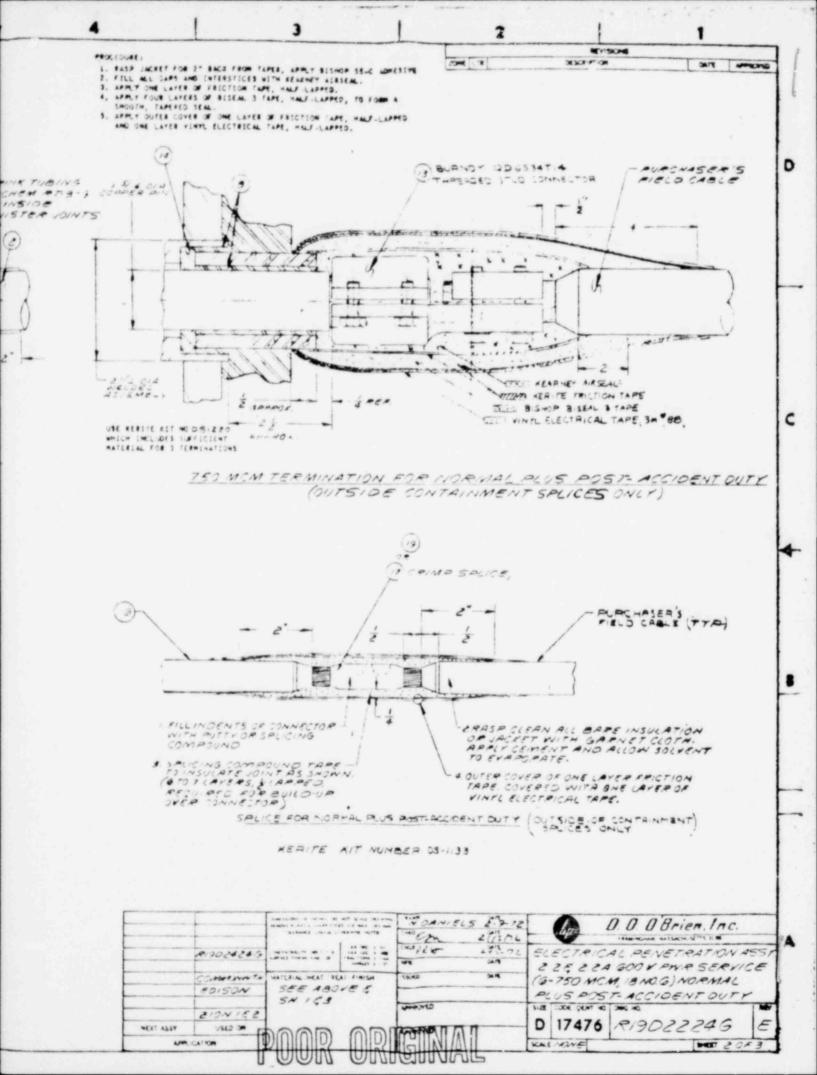


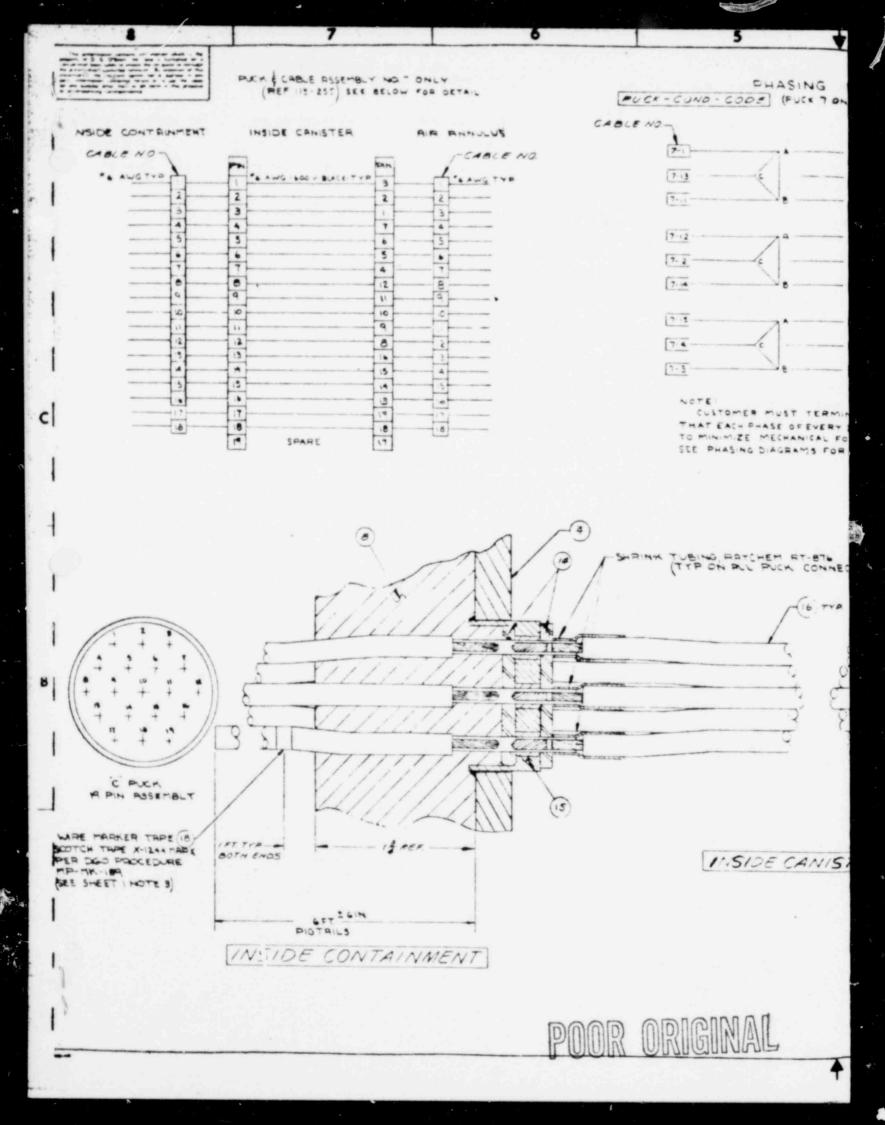


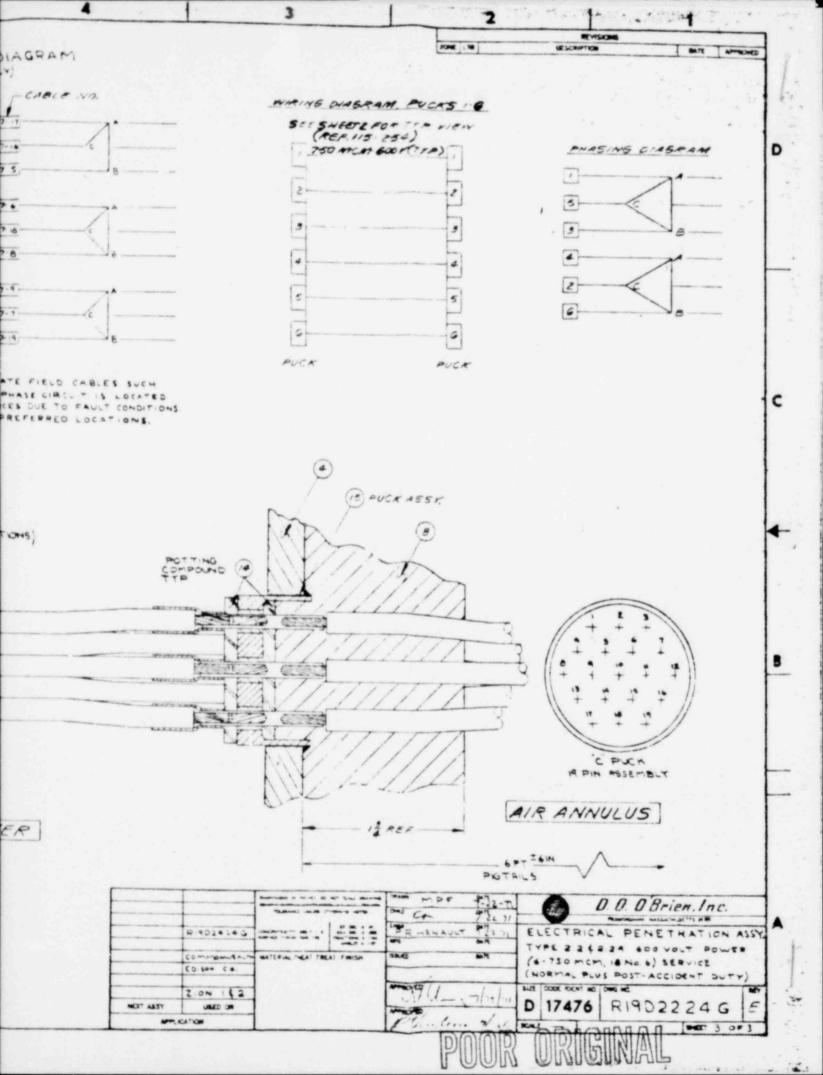












3.3.2.10 Equipment Item No. 24
Instrument and Thermocouple
Cables Located Within
Containment
Boston Insulated Wire and Cable Co.
Submittal Page References 4, 5 and 11

Response:

a) Reference 4, Pages 12 and 13 clearly indicate that the cables tested were single pair #16
AWG Instrument Cable with Bostrad7 and Bostrad75 insulation and jacket. Bostrad7 and Bostrad75 are BIW tradenames for Hypalon insulating material. The Bills of Material, Items A-104 and A-105 clearly indicate the cables purchased from BIW as being insulated with Hypalon and having Hypalon jackets. While the jacket material of each test specimen was not clearly indicated, the statement is made that both Hypalon and PVC jackets are compounded to meet the test requirements of Section VI and VII of Report B901.

Adequate records exist and are available at Zion Station to provide complete traceability for the cable manufactured by BIW and subsequently installed at Zion Station. These records consist of shipment invoices from BIW referencing specific cable reels, BIW Part Numbers, Test Reports for each cable reel referencing cable type (conductor, insulation, jacket material) and cable pull cords referencing individual cables pulled from specific cable reels.

b) Information addressing thermal aging of the specified cable has been requested from BIW. The effects of radiation exposure are addressed in Report B901.

Franklin Research Center indicated in the August 27, 1980 meeting at Bethesda that electrical loading of the instrument cables was not a concern.

Information on the combined effects of preaging and radiation exposure has been requested from BIW.

c) BIW has also been requested to address the subject of how the test specimens would react if subjected to gamma irradiation, simulated-LOCA steam environment and chemical spray (submergence).

- 3.3.2.11 Equipment Items No. 25 and 28
 Cables Located Within Containment
 Kerite Corporation (Various Types)
 (Licensee references 8 and 11)
 - 1. Insufficient evidence has been presented to identify the tested cables as identical in materials or construction to any of those installed. The Guidelines require that the test specimens must be the same as the equipment being qualified. The licensee did not present an analysis comparing the impact of deviations between the test specimen's specific design features, materials, and production procedure to those of the installed equipment. Therefore, an independent conclusion can not be reached regarding the extent to which there is similarity. Hence, the validity of the test as evidence of qualification has not been established.

Response

The attached letter to H.K. Stolt from R.M. Bowman (Kerite Co.) dated August 28, 1980 states that all of the cable supplied to Zion Station was fabricated using the same insulation and the same jacketing materials and further that these were the same compounds which are covered by the Franklin Institute Test Report FC-2737.

The only difference between the Zion cable and those tested is that there are cables at Zion which have different numbers of conductors, the size of the conductors are different for the various size cables and the insulation and jacket thicknesses are different depending on the size of the cable.

Since all the Kerite cable at Zion, medium and low voltage power and control cable, is of the same family and the cable insulation and jacket materials are the same as those tested in Report FC-2737, this test report documents qualification for all the Kerite cable at Zion.

2. The absence of preaging prior to testing together with the identification of the material as subject to thermal degradation requires that a period of qualified life be established. The licensee should provide such analysis.

Response

The attached letter from R.M. Bowman (Kerite Co.) to H.K. Stolt dated August 28, 1980 states that samples B and D as listed in Report FC-2737 were thermally preaged. The report also identifies samples B and D as having been thermally preaged, but it does not state the parameters.

3. The test conditions of steam pressure do not fully envelop the licensee's design test conditions; the design conditions call for 60 psig steam for the first 2.8 hours and 20 psig steam for the next 22.2 hours. However, the test pressure exceeded the predicted conditions, and the test duration with the most severe conditions exceeded the test design by a factor of 4.7. Hence, this deviation is judged acceptable.

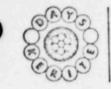
Response

Item 3 has been found acceptable by the FRC review team.

4. The Guidelines require that equipment located within containment and subject to submergence be qualified with actual submergence during testing. The licensee should provide evidence of submergence testing for those installed cables which are subject to it.

Response

We are still attempting to obtain information from the Vendor, Kerite Company, to determine if the cables were tested for submergence.



the kerite company

August 28, 1980

Mr. H. Stolt Station Nuclear Engineering Department Commonwealth Edison Company P O Box 767 Chicago, Illinois 60690

Re: Zion Nuclear Generating Station

Dear Mr. Stolt:

Confirming our several recent telephone conversations, we have looked into the matter of whether or not the samples covered by Franklin Institute Report FC-2737 were preaged.

We have found that the samples identified as Samples B and D were preaged at 150°C in a circulating hot air oven for 168 hours prior to radiation exposure.

These cable samples were described as follows:

- B- 1/C #6 5/64 HTK (N-98) 3/64 FR (HC-711)
- 2/C #12 3/64 FR (HI-70) 4/64 FR (HC-711)

The compounds identified by numbers above are those compounds used in all cables supplied by Kerite to the Zion Station, and are in fact, the identical compounds being used by Kerite today.

We hope the above information will be helpful.

Sincerely,

Robert M. Bowman
Regional Engineer
a subsidiary of HARVEY HUBBELL INCORPORATED

3.3.2.12 Equipment Item No. 26
BIW Cable Splices Located
Within Containment
Raychem Corporation
Submittal Page References 1 and 2

Response:

- Section 1.1, Page 1 of Report ER272 identifies
 the materials of the D. G. O'Brien splice kits
 used for terminating instrumentation cables at
 Zion Station. D. G. O'Brien Drawing R19D2227G,
 Sheet 4 of 4, Revision H identifies these same
 materials as being used for splicing the instrument cables. This drawing plus other reference
 documents are enclosed as an attachment to our
 response to TER Item 3.3.2.7.
- Information has been requested of the Vendor,
 D. G. O'Brien, to address the concern over aging and submergence.

3.3.2.13 Equipment Item No. 27
Kerite Corporation Cable Splices
Located Within Containment
Kerite Corporation
Submittal Page Reference 8

Response:

1. The splice kits (Kerite Splice Kit DS-1001) used for 600 Volt Control Service are shown on D. G. O'Brien Drawing R19D2226G, Sheet 2, Revision F (see attachment to our response to TER Item 3.3.2.8).

The splice kits (Kerite Splice Kits DS-1001) used for 600 Volt Power Service are shown on D. G. O'Brien Drawing R19D2224G, Sheet 2, Revision E (see attachment to our response to TER Item 3.3.2.9).

- 2. Report F-C2737, Page 14 indicates that samples B and D were preaged but did not indicate the parameters. The letter from R. M. Bowman (Kerite Co.) to H. K. Stolt dated August 28, 1980 (see attachment to our response to TER Item 3.3.2.11) indicates that the samples were preaged at 150°C for 168 hours prior to radiation exposure.
- 4. We do not expect the Electrical Penetration, where the installed splices are located, to be subject to submergence due to their location. The postulated flooding of the containment will remain approximately 40+ feet below the penetrations, therefore submergence testing is not applicable.

3.3.2.14 Electric Motor Valve Actuator Located in the Auxiliary Building (A-8)

Submittal page references: 24, 26, 31, 32

References: 10, 14

Valve ID numbers: MOV-FW0050 thru 57 (Aux. FW throttle valves)

MOV-FW0074 thru 76 (Isolation between

condensate FW supply and Essential SW supply to

aux. FW Pumps)

MOV-SW0100

MOV-SW0115

MOV-SW0101 thru 107 (Aux. FW Pump Isolation

from Essential Service

Water)

Response:

Valves MOV-FW0050 through MOV-FW0057 were incorrectly referenced here and will be addressed in response to item 3.3.2.19. The remaining valves are not required to operate after a high energy line break in the auxiliary building. This is the only accident in which the valves would see a harsh environment.

No qualification is necessary.

3.3.2.15 Electronic Transmitter Located at Zone A8 Submittal Page Reference 41 Qual. Reference 9, 20, 21

FT-FW03

Aux. FW Flow (Model 10B2495)

Response:

After a LOCA or MS/FW line break in the containment, this transmitter is located in a non-harsh area.

Therefore, qualification is by experience. After a high energy line break in the auxiliary building (HELB), this transmitter is located in a harsh area. However, there are three other aux. FW flow transmitters which remain in non-harsh environments after the HELB. These transmitters measure auxiliary FW flow to the other three steam generators. Decay heat load can be handled by two steam generators only. Therefore, only two of the remaining three transmitters in non-harsh environments are required to operate to safely shut down the plant after the HELB in the auxiliary building. Qualification is by experience.

3.3.2.16 Equipment Item No. 37
Remote Shutdown Control
Panels Located in the
Auxiliary Building (A-8)
Fischbach-Hatfield Contractor
Submittal Page Reference 16

Response:

- a) The materials used in the construction of the Remote Shutdown Panels (1LP57, 1LP58, 1LP59, 1LP60, 2LP57, 2LP58, 2LP59 and 2LP60) are listed on electrical drawings 22E-1-4626, 22E-1-4629, 22E-2-4628, and 22E-2-4629. We have enclosed copies of these drawings for your reference and have also prepared the attached table which compares the equipment tested with the equipment installed on the panels.
- b) These panels are normally not subjected to a harsh environment when they may be used if the control room becomes inhabitable. If a HELB occurs in the Auxiliary Building, subjecting these panels to a harsh environment, the panels will not be used.

3.3.2.17 Electric Motor Valve Actuator Located in the Auxiliary Building (A-9)

Submittal Page References 1, 18

References: 10, 14

Item 39A Valve ID Numbers: MOV-SI8809A, B (To RC loop cold leg from RHR Heat Exchanger)

Note: Item 39A is in Zone Al2, not A9.

Response:

These valves are only required to function after a LCCA or MS/FW line break in containment. The only potentially harsh environment is radiation. Qualification for radiation has been provided (see generic reply on Limitorque operator attached to these responses). All other parameters remain non-harsh. Qualification is by experience for these parameters.

Item 39B Valve ID Numbers: MOV-VC-LCV112B, C (to charging pumps from volume control tank)

Response:

These valves located in the auxiliary building are required to close upon safety injection initiation after a LOCA or MS/FW line break in containment. These valves are not required to operate (i.e., close) after a high energy line break in the auxiliary building. These valves are located in a non-harsh area during the period that they are required to operate (LOCA and MS/FW line break in containment). Therefore, qualification is by experience.

3.3.2.18 Electronic Transmitter Located at A9
Submittal Page Reference 49
Qual. Reference 9, 20, 21

PT PP15 PT PP17 PT PP18 PT PP19

PP Pressure (Model 5)EP1017)

Response:

These transmitters are located in a non-harsh area during the period that they are required to operate (LOCA and MS/FW line break inside of containment). Therefore, qualification is by experience.

3.3.2.19 Electric Motor Valve Actuator Located in the Auxiliary Building (A-12)

Submittal Page References: 2-5, 7, 12, 13, 19-21, 27, 28

References: 10, 14

Valve ID Numbers:

1. MOV-SI8801A, B MOV-SI8802 MOV-S18803A, B MOV-SI9011A, B MOV-SI8814 MOV-SI8813 MOV-RH9000 MOV-CC9413A, B MOV-CC9438 MOV-CC685 MOV-VC8105 MOV-VC8106 MOV-FW0016 MOV-FW0017 MOV-FW0018 MOV-FW0019 MOV-VC8100 MOV-CC9414 MOV-CC9412A, B

- 2. MOV-VC-LCV112D, E (from RWST to charging pumps)
 - 3. MOV-VC8105 (containment isolation MOV-VC8106 valves) MOV-VC8100
 - 4. MOV-FW0050 (aux. FW throttle valves)
 MOV-FW0051 (aux. FW throttle valves)
 MOV-FW0052 (aux. FW throttle valves)
 MOV-FW0053 (aux. FW throttle valves)
 MOV-FW0054 (aux. FW throttle valves)
 MOV-FW0055 (aux. FW throttle valves)
 MOV-FW0056 (aux. FW throttle valves)
 MOV-FW0057 (aux. FW throttle valves)

Note: Valves MOV-CC9412 A, B are in non-harsh zone A15, not A12.

Response:

Category 1

These valves are required to operate in the event of a LOCA or MS/FW line break in containment. Valves MOV-SI8802, SI9011 A&B, and RH9000 are required long-term after the accident - the remaining valves are only required for short-term operation. For a LOCA the only harsh parameter is radiation. Qualification for radiation is provided (see generic reply on Limitorque operators attached to these responses). All other environmental parameters remain

3.3.2.19 cont'd

nonharsh. Qualification is by experience. Limitorque
Report B0058 provides documentation concerning applicability
of an SMB-0 test to the whole family of actuators.

Category 2

These valves, which are required for medium term operation after LOCA or MS/FW line break, were incorrectly located in Zone Al2. Their actual location is in Zone All. This is a nonharsh zone and therefore qualification is by experience.

Category 3

These ID numbers were duplicated in the VC system and have now been deleted from the system. Refer to Category I for their response.

Category 4

These valves are required only for design basis MS/FW line break. For this accident Zone Al2 is nonharsh. In both the LOCA in containment and the HELB outside of containment, the valves do not have to change position. The valves are normally in the required throttled position to provide adequate auxiliary FW flow to the steam generators and consequently to allow safe shutdown of the plant.

3.3.2.20 Solenoid Operated Valve

Submittal Page References: 6, 8-11, 14

References: 18, 19

ID numbers: Containment Isolation Valves

(Please refer to the report for their listing)

Response:

These valves are all used for containment isolation following a LOCA or MS/FW line break in containment.

After a LOCA the only harsh parameter in Zone Al2 is radiation. These valves are required to operate immediately after the LOCA (short-term) before any degradation due to radiation could occur. The Licensee has replaced or will replace all the internal parts in the solenoid with those which are contained in the qualified NP-1 series. The replaced internal parts will now consist of high temperature/ radiation resistant material. Documentation on the ASCO list will be presented at a later date. This ASCO kit prevents the problem of the stem sticking in the valve and holding the valve open.

Once the valve is closed for containment isolation, it does not have to remain functional since it will not be required to reopen.

3.3.2.21 Motor Valve Actuator Located in the Auxiliary Building (A-14)

Submittal Page Reference: 17

Licensee References: 10, 14

Valve ID Numbers: MOV-VC8110) To seal water heat exchanger

MOV-VC8111) from charging pumps

Response:

These valves are required to function during accidents inside containment. For these accidents the only harsh parameter is radiation. Qualification for radiation has been provided (see generic reply on Limitorque operators attached to these responses).

Limitorque Report B0058 addresses applicability of testing one model for a whole generic family of valves. This we consider sufficient justification for using the test reports referenced.

These valves will not affect the ability to reach cold shutdown after HELB in the auxiliary building.

3.3.2.22 Electric Motor Valve Actuator Located in the Upper Safety
Valve Room (T-2)

Submittal Page Reference: 30

Licensee's References: 10, 14

Plant ID numbers: 1MOV-MS017)

1MOV-MS018) (Atmospheric relief valves,

1MOV-MS019)

1MOV-MS020)

Response:

These valves are not required to mitigate the consequences of an accident. Long-term operation is required to achieve cold shutdown. One hour or more after the accident it may be desirable to open these valves to cool down the primary system. By the time they are needed, the area will be significantly cool to allow an operator to open the valves using the handwheel. Only one of the four valves is needed for cooldown. The steam dumps to the condenser is a non-qualified backup to these valves. Note that these valves can also be operated by instrument air.

Some degree of physical separation exists. The four valves can be divided into two pairs. One pair of valves is about 200 feet from the other pair. While a major steam line break would cause a temperature increase for all four valves, it is likely that one pair would not feel the full effect of the accident. Only one valve is required for the cooldown since each valve can handle 10% of full power. Steam flow and decay heat is less than 2% of full power shortly after the accident.

3.3.2.23 Electronic Transmitter Located at T3

Submittal Page Reference 42

Qual. Reference 9, 20, 21

PT514	PT524	PT534	PT544
PT515	PT525	PT535	PT545
PT516	PT526	PT536	PT546

Steam Generator Pressure (Model 50EP1041)

Reer ise:

Short-term operation is required after an accident.

CECo is studying methods to either relocate these

transmitters or cool them. A more detailed response

on the intended plan of action will be supplied later.

3.3.2.24 Feedwater Flow Transmitter Located in the Steam Tunnel (T-4)
Submittal Page Reference: 39

Qual. Reference: 9, 20

1FT-510	1FT-530
1FT-511	1FT-531
1FT-520	1FT-540
1FT-521	1FT-541

Response:

For a main steam line break (MSLB) outside containment, these transmitters are not used by the automatic circuitry which initiates safety injection and main steam isolation following a MSLB. They are not useful to the operator following MSLB since feedwater is automatically terminated after the trip.

For a feedwater line break (FWLB) upstream of the isolation valve, these transmitters are not required since reactor trip results from low steam generator level.

For a FWLB downstream of the isolation valve, the response is the same as for MSLB.

No qualification is required for these transmitters.

Licensee is investigating radiation level in steam tunnel (see Appendix B of report) and will submit results by September 27, 1980.

RESPONSE TO GENERIC QUESTIONS RAISED BY FRANKLIN INSTITUTE ON VALVE MOTOR OPERATORS

- Part a) We are submitting portions of Limitorque Qualification

 Report B0058 as well as a letter from J. Oliver of

 Limitorque to M. D. Rauckhorst of Sargent & Lundy on the

 item of generic qualification.
- Part b) The motor manufacturer has been listed on the data sheet where available. For those that are blank, we are currently investigating the motor manufacturer with Limitorque and the station. Testing was done with the valve actuator in its worst possible orientation so orientation at the field was not addressed.
- Part c) This test report was referenced before we had received a response from Limitorque regarding which actuator was associated with which test report. We now have the following information:
 - For containment valve actuators, a letter stating which test report is applicable to which actuator.
 - 2. For valves outside containment, a verbal response, to be followed up by a letter stating that Reports B0003 and F-C3271 are applicable to Zion valves. Report F-C3271 is for motors with brakes and B0003 for those without brakes. Although B0003 may not

Part c) cont'd

entirely envelope the temperature, pressure profile, we feel that the test duration at elevated temperature and pressure will provide enough to satisfy the qualification.

Part d) Report B0003 includes radiation to the same actuator prior to the LOCA simulation and will be used in later issues of the report when applicable.

Conclusion:

The Licensee feels that with the presentation of the new reports and the inclusion of operating time, we have given sufficient credence to the continued operation of Limitorque valves.

The following is a generic response to comments submitted by Franklin Research Center (FRC) concerning Fischer & Porter transmitters. Specifically the following paragraph refers to FRC's comments on pages 14 and 15. FRC's comments on subsequent transmitters were almost identical and therefore, the comments should apply to subsequent sections which address transmitters. Specific comments on each section follows the generic reply.

a) Fischer & Porter Report 2205-51-B006 (Reference No. 21) does list model numbers. Additionally we have contacted Fischer & Porter (F&P) to determine the model numbers of the transmitters which were tested in the Franklin Institute Report. They are as follows:

SERIAL NO. IN REPORT	F&P MODEL NO.
6907A117A2	50EP1041
6907A117A1	50EP1041
6907All7A4	50EQ1031
6907A117A6	10B2496
6907A117A3	50EP1031
6907A117A5	10B2496

A letter has also been sent to F&P requesting verification that the Zion transmitters are identical to the test specimen. Fischer & Porter has informed us verbally that if the serial numbers are known, they can make this determination. A list of serial numbers was included in the letter to F&P.

Westinghouse WCAP-9157 dated September 1977 specifically mentioned F&P transmitter model 10B2496 and the serial numbers of the models tested.

b) Commonwealth Edison Company has verified that part no.805B241U01 oscillator-amplifier is used in the electronic circuits of the F&P transmitters. According to Fischer & Porter Report DP#2224-1-004, the oscillator-amplifier can oper satisfactorily up to a total gamma radiation of 1.2x10⁸. Since the noraml radiation dose is much smaller than this amount, the oscillator-amplifier will not have to be replaced every ten years.

- c) Franklin's Institute comment concerning non-sequential testing appears to be correct based upon the documents which were submitted. However, sequential testing of these transmitters is covered in WCAP 9157, dated September 1977.
- Attached is a temperature/pressure profile of the F&P Test

 Report 2204-51-B006 with test conditions superimposed upon

 the anticipated temperature/pressure profile. It appears that

 the temperature profile (up to 24 hours) is acceptable. The

 test pressure profile does not completely envelope the expected

 pressure profile. However, the initial test pressure is considerably higher than the expected pressure and experience has indicated that transmitter failure is generally not related to

 environmental pressure.

Also, WCAP-9157 indicates that the F&P transmitters will perform their mandatory trip and initiation functions based on the report's environmental testing results.

e) F&P Test Report 2204-51-B006 indicated errors of 3.5% WCAP-9157 indicated errors within 2.1%. While these figures appears low compared to test reports that we have seen on other transmitters, the test transmitter 6907All74A5 of the Franklin Institute report, appears to have an abnormally high error considerably above the other F&P transmitters test by Franklin Institute.

Although this is no proof that the transmitters at Zion will not have this large error, it is an indication that most of the transmitters will probably not experience this large error.

- performed their function within a few seconds after an accident. Although no detail studies regarding containment flood level versus time have been performed, it is inconceivable that the RPS transmitters (mounted 2 feet above the containment floor) will be flooded before they send out the RPS signal.

 See Appendix E for those safety related containment instrument that are mounted below the fluid level. If the maximum flood level (3-1/2 feet) is reached, there will still be at least one instrumentation channel (those transmitters mounted above the flood level) available for those variable which requires medium or long term operation.
- g) On November 1979 letter from R. L. Kelly of Westinghouse to N. E. Wandke of CECo. addresses chemical sprays. Westinghouse WCAP-9157 also addresses chemical sprays.

PRESENTE VS TIME FISCHER & PORTER TRANSMITTERS

FROM F. S.F. REPORT 2204-51-8-006 DEC 1906 .

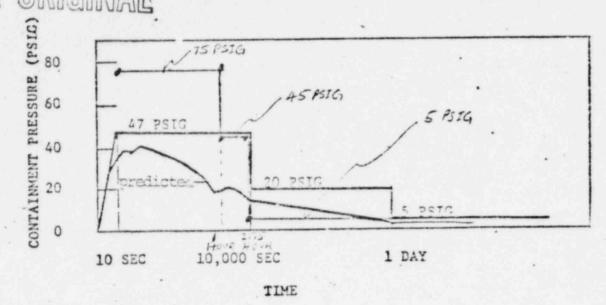


Figure 6.3-1 Post Accident Environmental Conditions for Equipment Design: Pressure versus Time (See Note below)

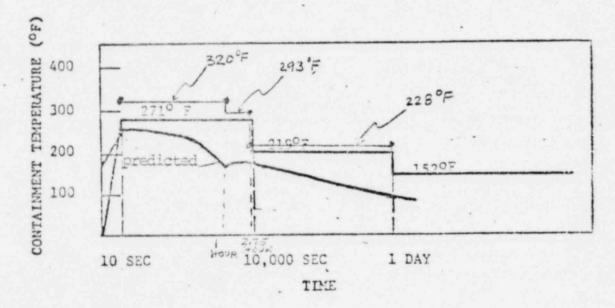


Figure 6.3-2 Post Accident Environmental Conditions for Equipment Design: Temperature versus Time (See Note below)

NOTE: The predicted containment pressure and temperature response curves superimposed in Figures 6.3-1 and 6.3-2 are obtained from Chapter 14 of Zion FSAR for the complete blowdown of the reactor coolant through any rupture of the reactor coolant system up to and including the hypothetical double end severence of a reactor coolant pipe.

The design pressure (47 psig) and temperature (271°F) of the containment are in excess of the peak pressure (42 psig) and temperature (263°F) predicted from the Safety Analysis (Chapter 14 of Zion FSAR).

3.3.3.1 Equipment No. 9
Magnetrol Level Switch: A-153-FEP/VPX-Y-3x-TIM-SIM3H-SIM3H-SIM3H
Containment Recirculation Sump Level
Submittal Page Reference 18

LT-940A LT-941A LT-940B LT-941B

Response:

These switches are required for long term operation after a LOCA. They are used for indication and alarm. Backup is by containment level transmitter-wide range:

(LT-CS46, LT-CS47) (TMI MOD. M22-1-79-37)
(Barton 764) These were the best transmitters
available as of April 1980.

Wyle Test Report 43235-1 dated May 2, 1977 includes

- 1. Nuclear radiation damage Threshold tests.
- 2. Regression Analysis.
- 3. Baseline functional and hydrostatic pressure tests.
- Nuclear radiation aging.
- 5. Elevated temperature/humidity/cycling aging.
- 6. Test set-up.

This Wyle Test Report was not used as a reference in the June 1980 submittal to Franklin Institute for review.

Sargent & Lundy has sent Magnetrol the serial number of the above switches so that magnetrol can verify if the test report covers that switch model. Sargent & Lundy has also requested test reports for chemical spray and submergence. Magnetrol will supply all available information by the end of September 1980. This information will be reviewed for applicability and submitted as appropriate by November 1, 1980.

3.3.3.2 Equipment Item No. 11
ITT Barton Level Transmitter Model 386
Pressurizer Level
Submittal Page Reference 21

LT-459 LT-460 LT-461

Response:

These transmitters are required for long term operation after LOCA, MSLB, and FWLB.

Frank'in Institute Test Report F-C2667 (Westinghouse WCAP-2410-L, Volume I Appendix B) describes a temperature, pressure, and humidity test for Barton 332 transmitter.

A letter from Barton to Mr. John Awal of Commonwealth

Edison dated April 30, 1975 said the Barton 386 has

been qualified to post-accident steam environment; and

that the above F-C2667 test report also apply to Barton 386.

This test report was not used as a reference in the

June 1980 submittal to Franklin Institute for review.

A letter has been sent to Westinghouse requesting available test report documentation and traceability documentation. Therefore, Westinghouse has replied as follows:

"Barton Model 386 transmitters were tested and reported in WCAP-7410L. (Section 4 and App B - at time of the test the 386 was still a 332 mod.).

These tests show good performance during radiation and steam tests to 286°F (maximum errors around -5%)."

Westinghouse also stated that Barton is being contacted

for comparison between units that were tested and units

actually installed at Zion.

3.3.3.3 Equipment Item No. 12
Sostman Resistance Temperature Detectors
Reactor Coolant Hot Leg and Cold Leg Temperature
Submittal Page Reference 24

TE-411A TE-411B .
TE-421A TE-421B
TE-441A TE-441B

Response:

These RTD's are required for short term operation after MSLB and FWLB.

Westinghouse Test Report WCAP-9157 provides adequate qualification of Sostman RTD's for short term accident environment.

With regard to traceability for the RTD's, Westinghouse has replied as follows:

"Both the Sostman Model 118348-1 (bypass line) and the Sostman Model 11901B-2 (wide range) RTD's are reported in WCAP-9157. Although both are not specifically mentioned in the WCAP, the only difference between these models is in the length of the stainless steel housing. These tests demonstrate the performance capability of the Sostman RTD's during and following HELB conditions. While direct traceability of materials is impossible, (due to the fact that Sostman is out of business), the Sostman RTD's were purchased over a short period of time and the materials are identified in WCAP-9157."

3.3.3.4 Equipment Item No. 13
Taylor Humidity Sensor Model 10H5
Containment Relative Humidity
Submittal Page Reference 25

ME-RV42 ME-RV43 ME-RV44

Response:

These humidity sensors are not required to operate after an accident. Therefore, no qualification is required.

3.3.3.5 Equipment Item No. 14
Electric Thermometers, Resistance Temperature
Detectors, 3-wire
Model Containment Temperature
Submittal Page Reference 26

TE-RV42 TE-RV43 TE-RV44

Response:

These Resistance temperature detectors are not required to operate after an accident. Therefore, no qualification is required.

3.3.3.7 Equipment Item No. 19
Electrical Penetrations Located
Within Containment
D. G. O'Brien Type 5.1*

(*Penetration Types 1.1 and 5.2 are addressed at the end of the response for Type 5.1)

Response: (Type 5.1 only)

Documentation relating to the prototype testing for Type 5.1 Electrical Penetrations is contained in D. G. O'Brien Report No. Cl9QA041, dated April 9, 1971 and D. G. O'Brien Report ER192 which have been submitted by letter to Mr. S. J. Crane, dated June 9, 1980.

Enclosed with this transmittal are xerox copies of portions of the D. G. O'Brien Technical Manual No. 1002, dated May, 1971 which indicates materials used and drawings applicable to the Type 5.1 penetration.

Since this type of penetration is not used for LOCA or post LOCA duty, the electrical features do not have to function during or after the accident, only the containment pressure boundary features must remain functional which is documented on Sheet 1 of Report C19QAO41, Paragraph 1.3.

Response: (For Types 1.1 and 5.2)

Documentation relating to the prototype testing for Types 1.1 and 5.2 Electrical Penetrations is contained in D. G. O'Brien Report No's. C19QA055 and C19QA062 (copies of these documents will be furnished as soon as we obtain them from D. G. O'Brien).

D. G. O'Brien Report ER192 is also applicable to Types 1.1 and 5.2.

We are enclosing xerox copies of portions of the D. G. O'Brien Technical Manual 1044, dated January, 1972 which indicates materials used and drawings applicable to Type 5.2 penetrations.

We will send copies of the instructions for Type 1.1 as soon as we obtain it.

Since these types (1.1 and 5.2) of penetration are not used for LOCA or post LOCA duty, the electrical features do not have to function during or after the accident, only the containment pressure boundary features must remain functional which are documented in Reports C19QA055 and C19QA062.

3.3.3.7 (Cont'd)

A printout listing of all types of penetrations and designating those used for Engineered Safety Functions (ESF), Non-Engineered Safety Functions and the spare steel sleeves provided for future used was given to Mr. S. J. Crane at the August 27, 1980 meeting in Bethesda.

Instruction Monual
For
REACTOR CONTAINMENT STRUCTURE
ELECTRICAL PENETRATION ASSEMBLY
TYPE 5.1-TRIAXIAL INSTRUMENTATION
CABLE SERVICE
ZION STATION UNITS I AND II

May 1971

D. G. O'Brien, Inc. Framingham, Massachusetts

Technical Manual No. 1002

For Serial No's. 5.1Z1 thru 5.1Z4 and 5.1AZ1 thru 5.1AZ4

Prepared By:

R. S. Butters, Proj. Engr. Mech. (5/12)

P. R. Henault, Proj. Engr. Elec. (5/12)

Approved By:

R. B. Henderson, Mgr. of Engr. (5/12)

References:

Sargent & Lundy Specification X-2308

D. G. O'Brien, Inc. Contract No. 113967

Zion Stations I & II Commonwealth Edison Co.

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INTRODUCTION

The Electrical Penetration Assembly described herein was designed and manufactured by D. G. O'Brien Inc., Framingham, Mass. for use in the construction of Nuclear Power Plant - Zion Units I and II, Commonwealth Edison Co., Zion, Illinois.

This manual is for use in the installation, test, calibration, and operation of Type 5.1 penetration.

This penetration is designed for triaxial instrumentation cable service. Penetrations of Type 5.1, D. G. O'Brien, Inc., Part No. R19D2228P are identical for both Zion Units I and II.

Information pertaining to other types of penetrations also designed and manufactured by D. G. O'Brien, Inc. for Zion Units I and II can be obtained from other Instruction Manuals. This manual is applicable to Type 5.1 only.

Quality Assurance data is included under a separate cover.

This penetration assembly is furnished for use with applicable design data of the following Sargent & Lundy drawings:

- ES-42 Typical Electrical Penetration,
 Physical Requirements, Dated 10-1-69
- B-213 Reactor Building Containment, Liner Plate Sections and Details, Sheet 2 Rev. T, Dated 13-3-69
- B-214 Reactor Building Containment, Penetration Schedule, Rev. L., Dated 10-3-69
- B-216 Reactor Building Containment, Elevation Electrical Penetrations, Rev. G, Dated 10-3-69

The penetration assembly described herein is furnished by D. G. O'Brien, Inc. as part of Class B Nuclear Vesse

The electrical penetrations for Nuclear Generating
Power Plants manufactured by D. G. O'Brian, Inc.
are engineered to meet the stringent requirements
of the electrical power industry and the Atomic
Energy Commission. The careful integration of
many scientific and technical disciplines has
gone into the development of a state-of-the-art
product that is reliable, rugged, dependable,
efficient, and economical. Careful control of
manufacturing processes and materials plus extensive
in-process and final testing insures the finest

product is delivered to the customer.

This manual is prepared to give the customer in a readily available form the information necessary to efficiently install and maintain the purchased equipment.

SECTION I

GENERAL DESCRIPTION

SECTION I

General Description

Type 5.1 D. G. O'Brien, Inc. Shielded Instrumentation
Triaxial Cable Penetration Assembly Part No. R19D2228P.

General:

The penetration assembly is to be used as an interface for passing the Purchaser's triaxial cables, Type RG 1'/U, Essex P/N 21-529 from the inside containment to the outside containment and as such will become a critical portion of the cabling system associated with the reactor nuclear instrumentation system.

It will extend high voltage, low current instrumentation power to neutron detectors located inside the containment and extend high frequency pulse signals from the detectors to remote monitoring instrumentation location outside of the containment.

The assemblies are designed and constructed for installation in 3 foot 6 inch long, 12 inch steel pipe containment penetration nozzles. Each penetration assembly is identical in basic physical configuration and consists of the assembly with one weld ring permanently attached. The second mechanical seal required for field installation is to be installed by the Customer.

The Assembly must be inserted into the containment structure nozzle from inside the containment.

The Penetration Assemblies are to be permanently installed by means of field welding at the site.

A maximum of three field welds are required for installation. Mechanical supports are necessary to position the Assembly during the welding operation. The past involvement of D. G. O'Brien, Inc. in the Nuclear Power Plant Penetration.

Assemblies and in underwater and military applications has provided a great deal of experience in assembly and welding of Penetration.

Assemblies without detrimental heat transfer to the components of internal conductors.

Each Assembly is designed in a manner that will restrain loading due to electrodynamic forces or mechanical stressing. Internally this is achieved, where required, by groups of tubular cable guides extending the full length of the Penetration Assembly. External supports protect and strain relieve the cable and conductor terminations where required.

Each Penetration Assemnly is permanently identified by a serial number. Each wire beyond the Assembly is marked at each end with an identification number as specified by the Purchaser. Wire numbers in any one multiconductor cable are not repeated.

Sealing and Pressurization:

The Penetration Assemblies provide a dual gas barrier by means of steel header flanges and hermetically glass-sealed electrical contacts. Each of the two gas barriers meet the service environmental conditions individually, providing an overall performance safety factor of two. The double-pressure barrier is formed, at installation, by welding the two weld rings to the containment structure liner plate. Weld preparation and all welding is in accordance with ASME Boiler and Vessel Code, Section III, Class B Vessels.

Both internal volume of the Penetration Assembly and that between it and the penetration nozzle may be pressurized through purging holes in the canister. The canister assemblies are pressurized to 54 psig with dry nitrogen prior to shipment. Gross pressure differential of the penetration assembly in transit and storage can be observed on the pressure gauge that is part of the assembly.

CAUTION: Prior to installation, the Penetration

Assembly should be depressurized and
the pressure gauge assembly and purging
port plugs removed. Refer to Section IV of
this manual.

Pneumatic testing was performed on the prototype and each production assembly in accordance with the latest revision of Paragraph N-110 of Section III in the ASME Boiler and Pressure Vessel Code and as covered in detail in the Quality Assurance Instruction Data. D. G. O'Brien, Inc. has achieved an excellent reputation in man-safety rated equipment and this equipment is a further indication of maintaining this concept.

The allowable leak rate of each penetration gas barrier prototype testing is equal to or less than 1 x 10⁻⁶ standard cc/sec. of dry helium at 298°F. and 70 PSI. In production, each penetration assembly is subjected to a leak rate test of 70 PSIG at 78°F. and will not exceed 1 x 10⁻⁶ standard cc/sec. through each penetration gas barrier or a total assembly. Due to controlled production processes hermetically glass-sealed headers or gas barriers consistently better the leak rate of 1 x 10⁻⁶ by two orders of magnitude or 1 x 10⁻⁸ cc/sec. helium. The usage of dual gas barriers add an additional leak rate factor of safety of two.

Cable Description:

Internal triaxial cables are Type RG 11/U with polyethylene insulation and outer jacket and match the electrical and physical characteristics of the external cable. Each RG 11/U cable is terminated in hermetic, environmental connector plugs which mate with the glass-sealed receptacles in the gas barrier. The internal cables are directly terminated to these receptacles, and the external cables to the positive engagement plugs. The electrical characteristics are identical to the Purchaser's cables within the tolerance allowed.

External cable terminations are to be made to D. G. O'Brien, Inc. triaxial connector plugs. These plugs are designed and built to positively engage with the D. G. O'Brien, Inc. triaxial connector receptacles. The receptacles are a structural part of the Penetration Assembly gas barrier and the internal interconnecting cables are terminated at D. G. O'Brien, Inc. One of the design features of the true triaxial connectors is the ease of cable terminations. All attachments are done by crimp type contacts, thus reducing the the installation time and perplexity of termination.

The cable shielding is continuous and concentric around the center conductor over the entire length of the penetration assembly. In the gas barriers, hermetically glass-sealed conductor contacts and inner and outer shields provide a pressure seal. A positive engagement receptacle plug in a true triax configuration is supplied for the connection of the Purchaser's triax cable. Each cable is terminated in its individual connector. All conductors and shields are insulated from each other and from ground.

Insulation resistance was tested between each conductor, conductor to shield, conductor to ground and shield to ground and meets the 500 VDC with stand test without arc over or breakdown.

The prototype and all production models were tested to the following:

- 1. Test Voltage 500 VDC
- 2. Minimum Insulation Resistance:
 - 1 x 10 12 Chms Center Conductor to Inner Shield
 - 1 x 10¹⁰ Ohms Inner to Outer Shield & Outer Shield to Ground

The penetration assembly was tested to the following:

- 1. Center Wire to Inner Shield 3,000 VDC for 1 Min.
- 2. Inner Shield to Outer Shield 500 VDC for 1 Min.
- 3. Outer Shield to Ground 500 VDC for 1 Min.

The following tabulation of technical and design parameters provides a ready reference of data.

Additional information is provided in each Section of this manual to supplement the above general description.

TYPE 5.1 TRIAX INSTRUMENTATION ELECTRICAL PENETRATOR DESIGN PARAMETER SUMMARY

1. Number of Conductors

20 Triax RG-11/U

2. Material & Size of Conductors:

Current or Signal Ground or Shield

3. Conductor Insulating Material

Temperature

- 4. Provision for Connection of Purchaser's External Cable
- High Potential Test On Production Assemblies for One Minute

#18 AWG Tinned Copper Bore Copper Braid

Polyethylene +75° C.

D. G. O'Brien, Inc. Model No. R19P1010G01

Conductor to First Shield - 3000 VDC Shield to Shield and Shield to Ground - 500 VDC

.10" I.P.S. Sch. Assembly Body Material 20 Pipe, ASTM, A-333 Gr-1, Carbon Steel 7. End Header Plote ASTM, A-442, Gr-60 Carbon Steel or ASTM Material A-516, Gr-70 Leaded Carbon Steel End Header Plate 8. Conductor Material Per AISI, C1213 9010 Glass End Header Plate 9. Conductor Insulating Material Assembly Dimension: 10. 10 3/4 In. Mom. Body Outer Diameter 4 1/2 Ft. Nom. Body Length 11. Maximum Integrated 6 x 108 Rods Radiation Exposure 2.24 x 10⁻⁵ cc. 12. Maximum Total Assembly (Air) Min. Air Leakage Rate When Subjected to the Maximum Post DBA Environment

13. Minimum Insulation
Resistance @ 500 VDC:

Conductor to Shield
Shield to Shield or to
Ground

14. Total Assembly Calculated Weight

15. Shipping & Storage Pressurization 10¹² Ohms Ohms

250 Lbs.

54 "si, Dry Nitrogen 16. Design Current Roting

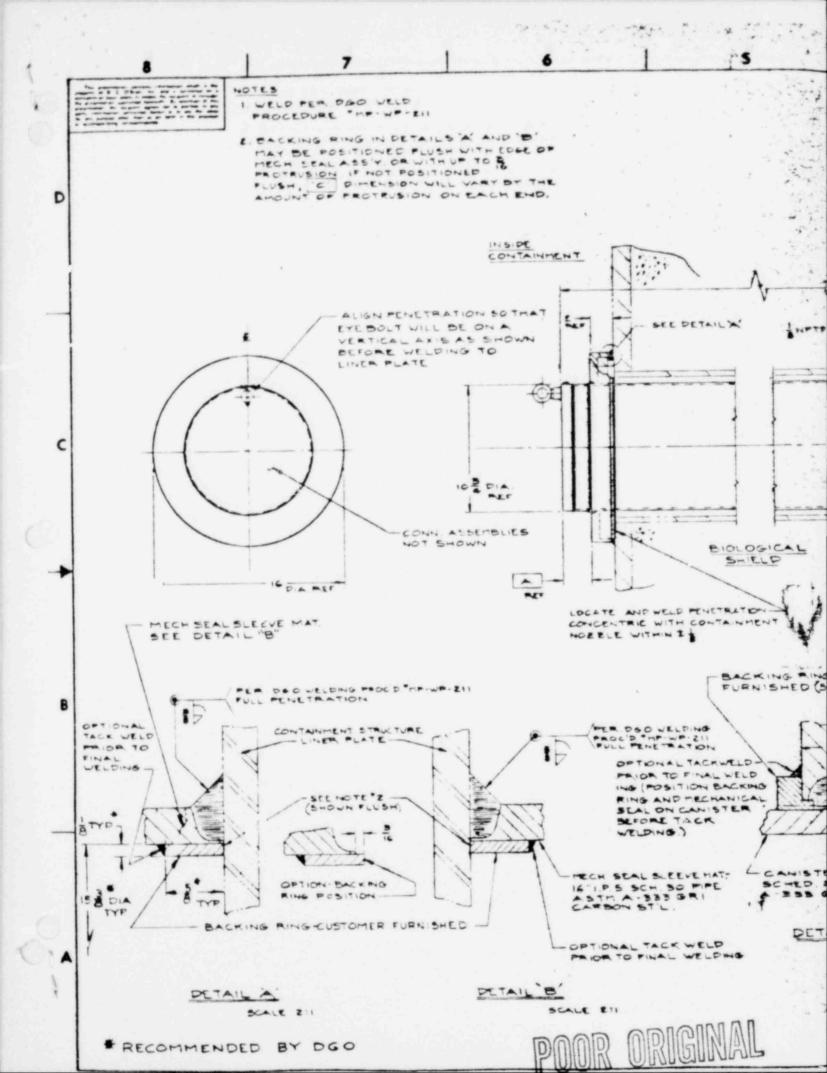
- 1×10^{-11} AMPS to 3×10^{-2} AMPS
- 17. Design Pulse Signal Rating
- Pulses with 10⁻⁸ rise time, 10⁻⁷ sec. width and 10⁻⁷ pulses per second repetition rate

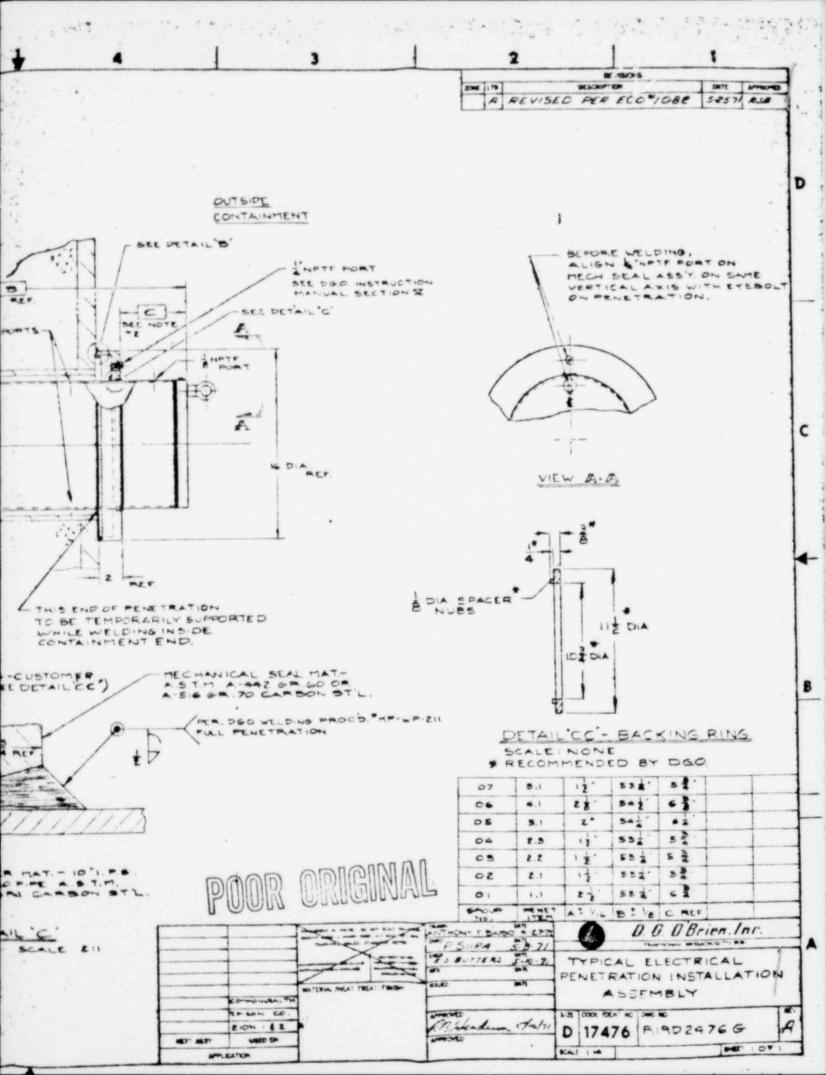
Wiring

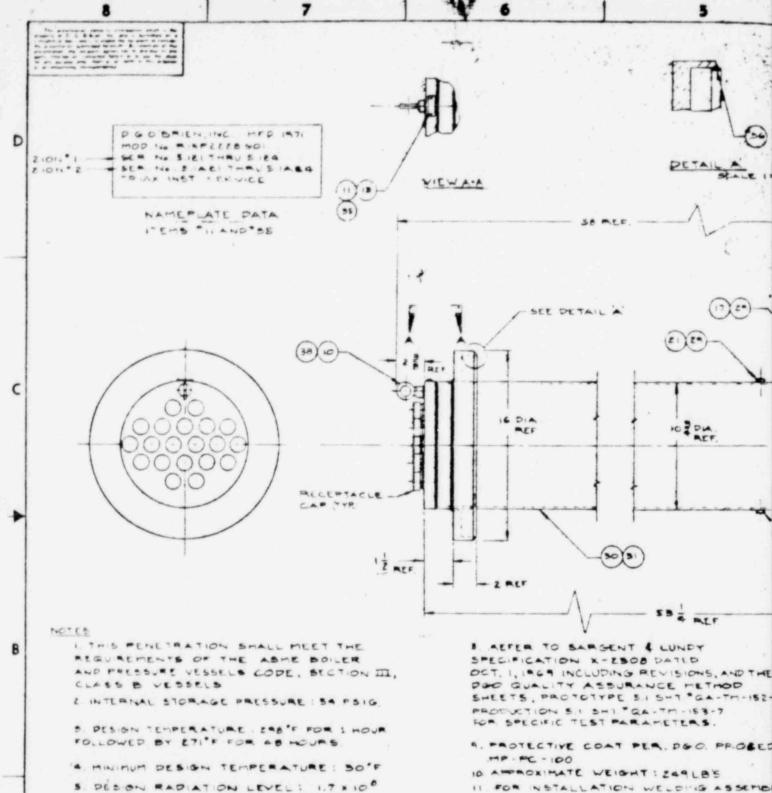
Introduction:

The following drawings depict the wiring diagram electrical connections of the Zion I and II Electrical Penetrations, Type 5.1 "Triaxial Instrumentation Service" for Normal Non-Accident Duty.

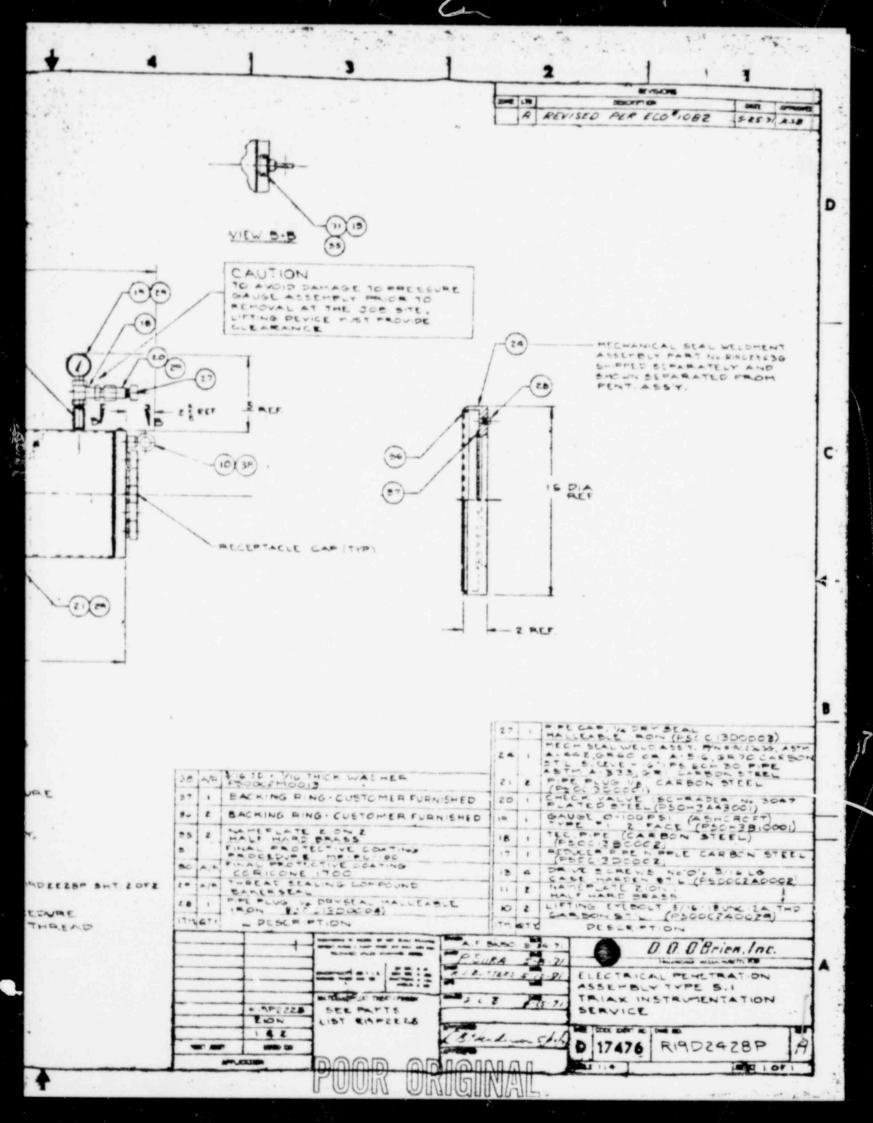
Refer to Section VII for Termination Instructions.

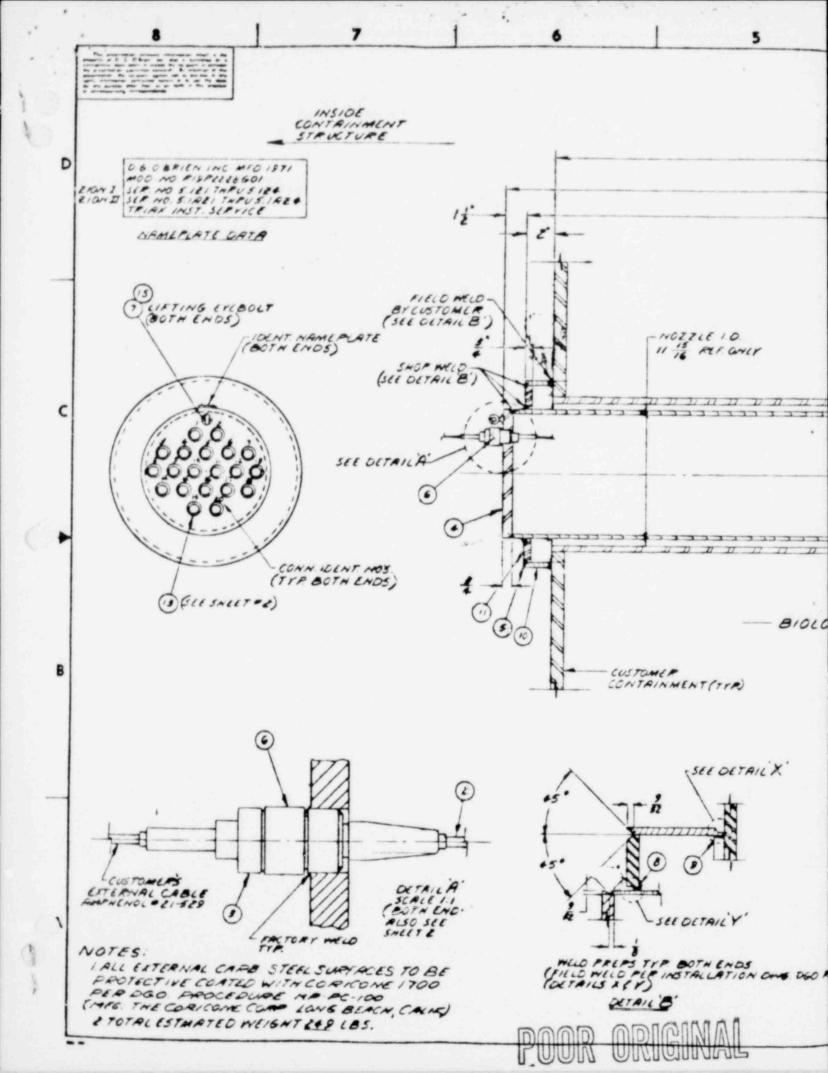


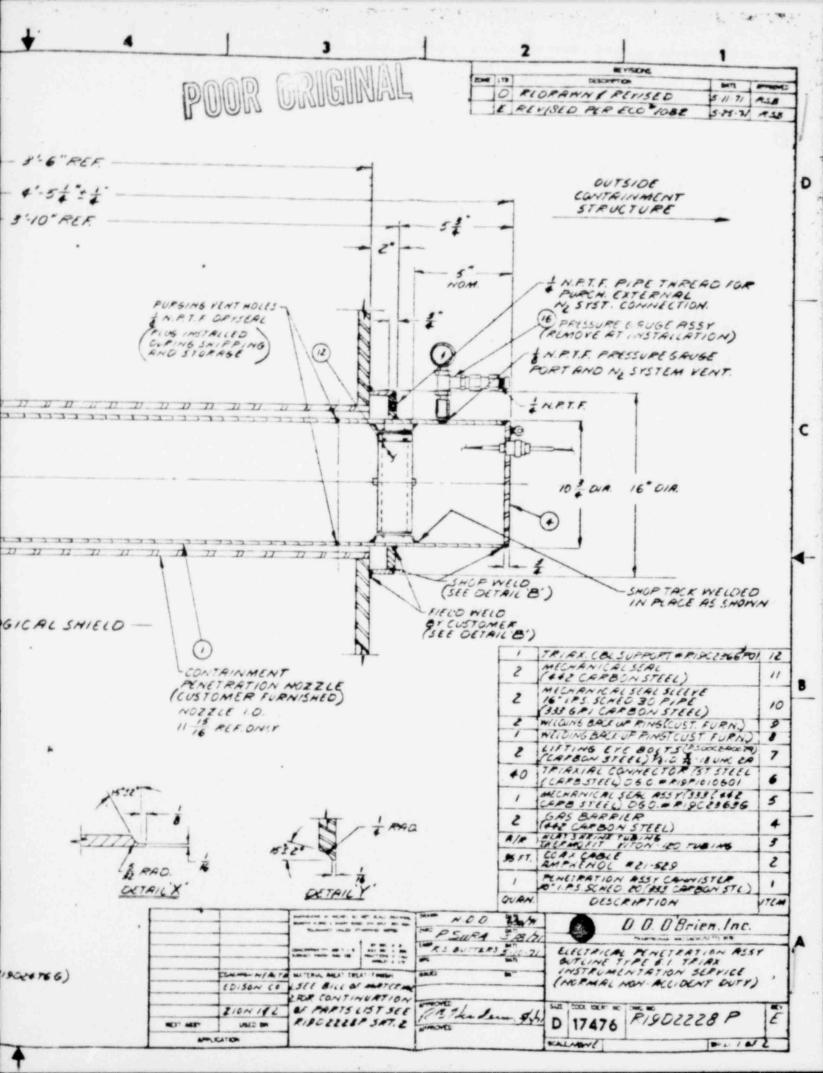




- FADS S MEY GAMMA RAYS).
- & RELATIVE MUMINITY MAX, DURING THE GOYEAR LIFE INSIDE AND OUTSIDE CONTAINMENT 50% ..
- 7 PENETRATION SEISMIC TEST : . 2565 AT SE CPS .
- SEE INSTALLATION ASSEMBLY
- IZ FOR CABLE TERMINATION ITEMS, SEE CABLE TER INATION PEANING "
- IB ALL PRYSEAL PIPE THREADS SHOULD BE TARRED PER DGO PAD MP-HP-ICO.USE O'LY BAKER SEA SEALING COMPOUND "

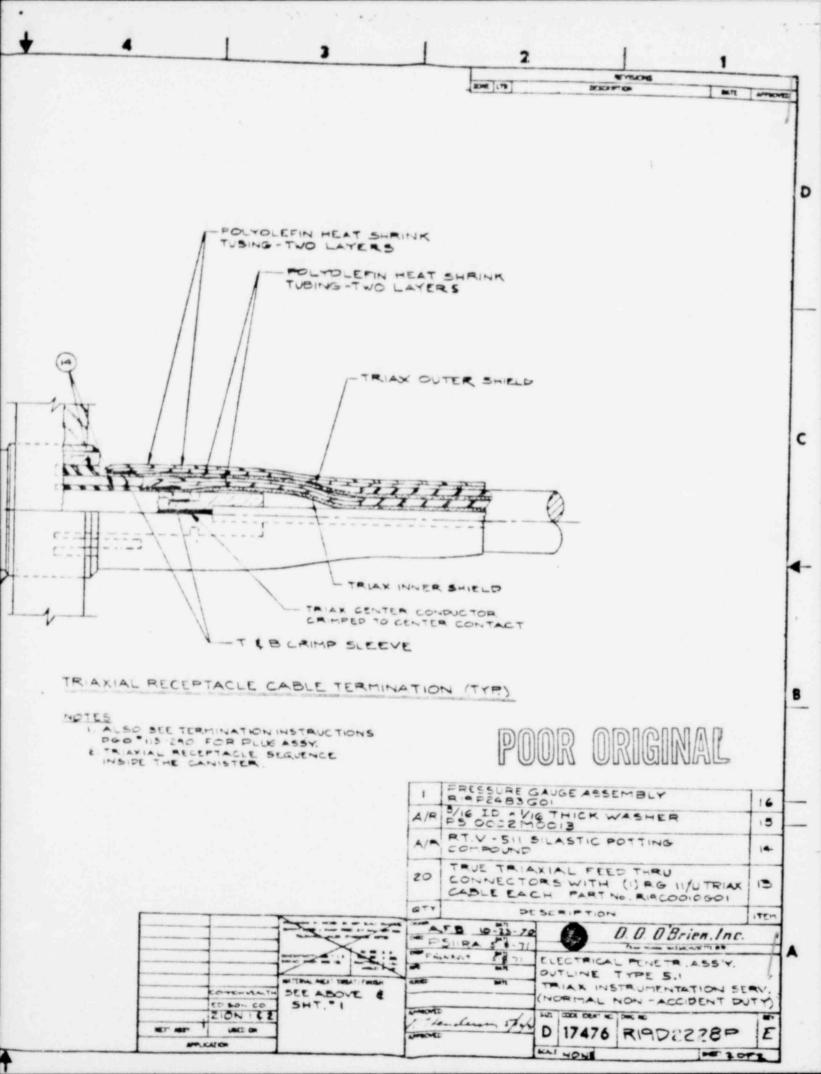






7 5 TYPE SH TRIAXIA LABLES (RECEPT. DENT STAMPED ON OM 5 BARNERS) (SEE SHEET "1) RECEPTACLES RECEPTACLES RECEPTACLES RECEPTACLES D TRAX ZI-ST 100 100 2 101 3 70) -5 (0) 5 20 7 Te) 10 10 10 -11

POOR ORIGINAL



Duplicator O

Instruction Manual (1044)

For

REACTOR CONTAINMENT STRUCTURE

ELECTRICAL PENETRATION ASSEMBLY

TYPES 5.2 AND 5.2A

(Serial Numbers 5.2Z1 AND 5.2AZ1)

JANUARY, 1972

Prepared For Use On
ZION STATION UNITS I AND II

(Commonwealth Edison, Co., Contract 113967)

Prepared by:

D. G. O'Brien, Inc.

500 Cochituate Road

Framingham, Mass.

Approved by

H. P. Hilberg, Engineering Manager

Nuclear Power Plant Systems

1/27/72

INTRODUCTION

The Electrical Penetration Assembly described herein was designed and manufactured by D. G. O'Brien, Inc., Framingham, Mass. for use in the construction of Nuclear Power Plant - Zion Units I and II, Commonwealth Edison Co., Zion, Illinois.

This manual is for use in the installation, test, calibration, and operation of Type 5.2 penetration assemblies. This penetration is designed for Radiation Monitoring instrumentation cable service. Penetration assemblies of Type 5.2 are identical for both Zion Units (I and II). Types 5.2 and 5.2A are identical but the 5.2A designation applies to the assembly used with Zion, Unit II.

Information pertaining to other types of penetrations also designed and manufactured by D. G. O'Brien, Inc. for Zion Units I and II can be obtained from other Instruction Manuals. This manual is applicable only to Type 5.2 and 5.2A.

Quality Assurance data is included under a separate cover. This penetration assembly is furnished for use with applicable design data of the following Sargent and Lundy drawings:

- ES-42 Typical Electrical Penetration, Physical Requirements, Dated 10-1-69
- B-213 Reactor Building Containment, Liner Plate Sections and Details, Sheet 2 Rev. T. Dated 10-3-69
- B-216 Reactor Building Containment, Elevation Electrical Penetrations, Rev. G,
 Dated 10-3-69.

The penetration assembly described herein is furnished by D. G. O'Brien, Inc. as part of an ASME, Class B Nuclear Vessel.

The electrical penetrations for Nuclear Generating Power Plants manufactured by D. G. O'Brien, Inc. are engineered to meet the stringent requirements of the electrical power industry and the Atomic Energy Commission. The careful integration of many scientific and technical disciplines has gone into the development of a state-of-the-art product that is reliable, rugged, dependable, efficient, and economical. Careful control of manufacturing processes and materials plus extensive in-process and final testing ensures that the finest product is delivered to the customer.

This manual is prepared to give the customer, in readily available form, the information necessary to efficiently install and maintain the purchased equipment. References throughout this manual to type 5.2 assembly are also applicable to type 5.2A assemblies, unless otherwise specified.

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- 1.1 Radiation Monitoring Instrumentation Cable Penetration
 Assembly (D. G. O'Brien, Inc. Part No. R19P2438GO1) herein
 referred to as the penetration assembly will be used as
 an interface for passing the Purchaser's Radiation Monitoring
 instrumentation cables, from the outside containment
 to the inside containment. As such, it will become a
 critical portion of the cabling system associated with
 the reactor nuclear instrumentation system.
- 1.2 The penetration assembly will service electronic instrumentation loads of up to 120 VAC. The assembly will provide the interface between instruments located inside the containment and monitors located outside of the containment that indicate status of operation.
- 1.3 The assemblies are designed and constructed for installation in 12-inch diameter steel pipe containment penetration nozzles that are 3 feet, 6 inches long. Each penetration assembly is identical in basic physical configuration and consists of the assembly having one mechanical seal permanently attached. The second mechanical seal, required for field installation, is furnished separately in the same shipping carton.
- 1.4 The penetration assembly must be inserted into the containment structure nozzle from inside the containment and is permanently installed by means of field welding at the site. Mechanical supports are necessary to position the assembly during the welding operation. The past experience of D. G. O'Brien, Inc. in the Nuclear Power Plant Penetration Assemblies and in underwater and military

applications provides the necessary background experience to assemble and weld penetration assemblies without detrimental heat transfer to the components of internal conductors.

- 1.5 Each assembly is designed to restrain loading due to electrodynamic forces or mechanical stressing. Internally, this is achieved, where required, by groups of tubular cable guides extending the full length of the penetration assembly.
- 1.6 Every penetration assembly is permanently identified by a serial number. Every wire, external to the assembly, is marked at each end with an identification number as specified by the purchaser. Wire numbers in any one multiconductor cable are not repeated.
- 1.7 Sealing and Pressurization. The penetration assemblies provide a dual gas barrier by means of steel header flanges and hermetically glass-sealed electrical contacts. Each of the two gas barriers meet the service environmental conditions individually, providing an overall performance safety factor of two. The double-pressure barrier is formed, at installation, by welding that is in accordance with the ASME Boiler and Vessel Code, Section III, Class B Vessels. Both the internal volume of the penetration assembly and that between it and the penetration nozzle may be pressurized through a pressurization port in the outside containment mechanical seal and holes in the

canister. The canister assemblies are pressurized to 15 psig with dry nitrogen prior to shipment. Gross pressure differential of the penetration assembly in transit and storage can be observed on the pressure gauge that forms part of the assembly.

CAUTION

PRIOR TO INSTALLATION, THE PENETRATION

ASSEMBLY SHOULD BE DEPRESSURIZED AND

THE PRESSURE GAUGE ASSEMBLY AND PURGING

PORT PLUGS REMOVED. REFER TO SECTION 4.0

OF THIS MANUAL.

Safety Factors in Production. Pneumatic testing is 1.8 performed on the prototype and on each production assembly in accordance with the latest revision of Paragraph N-110 in Section III of the ASME Boiler and Pressure Vessel Code and as covered in detail in the Quality Assurance Instruction Data. The allowable leak rate of both penetration gas barriers in series, in prototype testing, is equal to, or better than, 1 x 10-6 standard cc/sec. of dry helium at 298°F and 54 PSIG. In production, each penetration assembly is subjected to a leak rate test at 54 PSIg and 78°F +5°F and will not exceed 1 x 10⁻⁶ standard cc/sec. through both penetration gas barriers in series. Due to controlled production processes, hermetically glasssealed headers or gas barriers consistently better the leak rate of 1 x 10-6 by two orders of magnitude.

1.9 Cable Description

- 1.9.1 Internal Cables. The internal cables are directly terminated to glass-sealed contacts in receptacle connectors welded into the gas barriers. The electrical characteristics of the internal cables are identical to the purchaser's cables within the tolerances allowed.
- 1.9.2 External Cable Terminations. External customer cables are terminated to the plug connectors which mate with the appropriate receptacles welded to the gas barrier. All cables are crimped. They are designed and built to function in accordance with the requirements of the circuits they service. All conductors are insulated from each other and from ground.
- 1.9.3 The prototype and all production models are tested to the following:
 - A. Insulation:
 - 1. Test Voltage 500 VDC
 - 2. Minimum Insulation Resistance Conductor-to-conductor 1 x 10⁹ ohms-feet Conductor-to-ground 1 x 10⁹ ohms-feet Coaxial Cable Conductor-to-inner shield 1 x 10⁹ ohms-feet Inner shield-to-ground 1 x 10⁹ ohms-feet
 - B. Dielectric Strength:

Production:

Conductor-to-conductor 1500 VAC RMS
Conductor-to-ground 1500 VAC RMS
Coaxial cable
Conductor-to-inner shield 2000 VDC
Inner shield-to-ground 1500 VAC RMS

Table 1-1 summarizes the technical and design parameters

1. Number of Conductors

10 Times Wire & Cable P/N MI-31285
A) Two twisted shielded jacketed pairs
Conductors:
22 AWG, 7/30 T/C PVC insulated
.010" wall...
Pair Twisted with #36 AWG T/C
Braid and overall tape wrap.
Color Code:
Pair 1 1) White
2) White/Brown
Pair 2 1) White

B) Coaxial Cable
Conductor #26 AWG Tinned Copper
weld insulation foam polyethylene
shield #38 AWG T/C braid
Jacket: Nylon Clear

2) White/Red

- C) High Voltage Wire Conductor #22 AWG 7/30 T/C Insulation: PVC .025" wall
- D) Four single wires
 Conductor #22 AWG 7/30 T/C
 Insulation: PVC .010" wall
 Cable twisted together with tape
 wrap, braid shield #34 T/C and
 overwall PVC jacket. Finished
 0.D. .380"

Coaxial cable: #26 AWG Solid
Tin Plated Copper covered
steel. All other conductors
#22 AWG Stranded Tin Plated Copper
(7/.010")

Coaxial Cable: Foam Polyethylene
All other Conductors: Polyvinylchloride
Coaxial Cable - 80°C
All others - 85°C

- 2. Material and Size of Conductors: Signal
- Conductor Insulating , Material:

Temperature Rating:

- 4. Provisions for Connection of Purchasers external cable
- 5. High Potential Test on Production Assemblies for 10 seconds:

- 6. Assembly Body Material
- End Header Plate Material
- 8. End Header Plate
 Conductor Material
- 9. End Header Plate Conductor Insulating Material
- 10. Assembly Dimension
 Body Outer Diameter
 Body Length
- 11. Maximum Integrated Radiation Exposure
- 12. Maximum Total Assembly
- 13. Minimum Insulation Resistance @ 500 VDC:
- 14. Total Assembly Calculated Weight
- Shipping Pressurization Testing Pressurization

Receptacles

Conductor-to-shield 2000 VDC
Shield-to-ground 1500 VAC RM:
All others:
Conductor-to-conductor
1500 VAC RMS
Conductor-to-ground
1500 VAC RMS

10" I.P.S. Sch. 20 Pipe, ASTM, A-333 GR-1 Carbon Stee.

ASTM, A-442, GR-60 Carbon Steel or ASTM A-516, GR-70

Leaded Carbon Steel Per AISI, C1213 (Tin plated)

9010 Glass

10 3/4" 4' 5 1/4"

1.7 x 10⁸ Rad (1.5 MEV Gamma Rays)

 2.24×10^{-5} cc. (Air) Min.

1 x 10⁸ ohms-feet

275 pounds

15 PSIG Dry Nitagen 54 PSIG Dry Nitaggen

6.0 WIRING

The following drawing (Figure 6-1) depicts the wiring diagram electrical connections of the Zion I and II Electrical Penetrations, Type 5.2 Radiation Monitoring Instrumentation Cable Service for normal non-accident duty.

7.0 TERMINATION INFORMATION

Prior to assembly of any hardware on the canister a review of D. G. O'Brien Drawing No. R19D2438G

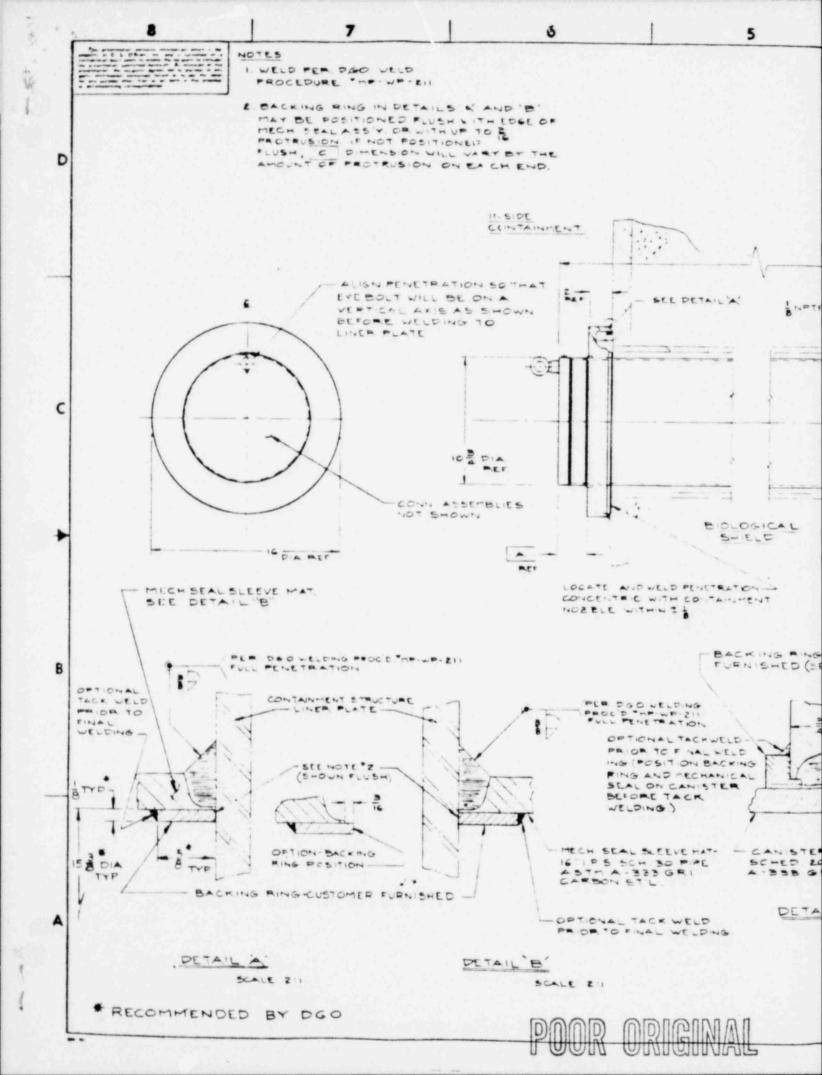
Pages 22 & 24 should be made to ascertain layout of the receptacles and sequence of the assembly on each canister furnished on Zion 1 and Zion 2, Item 5.2 & 5.2A "Containment Area Radiation Monitor Service"

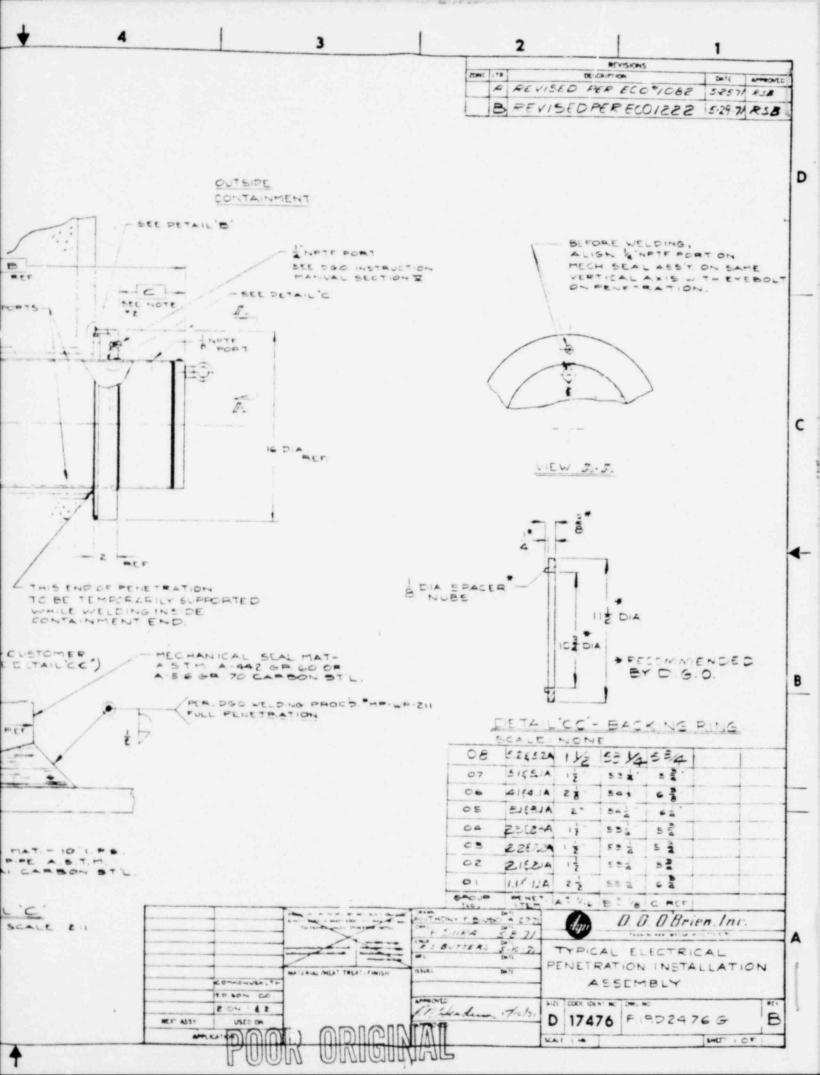
Normal Non-Accident Duty. This drawing illustrates location of receptacles and electrical connection sequence.

The hardware and material required to terminate each plug are included in the carton, Kit P/N 115-317, with each plug. Prior to any assembly work the plug should be inspected to ascertain that all parts are included within the kit and that the plug has not been damaged.

Purchasers Field Cables shall be prepared as outlined in D. G. O'Brien Inc. procedure No. 115-317 (Appendix E) for termination to the D. G.O'Brien Plug, Part No. R19C1002G04.

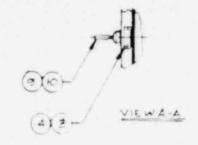
This Procedure should be read thoroughly prior to proceeding with any actual assembly. Tools should be assembled and prepared for installation including dies, heads, and handles. All work should be done in as clean an assembly area as possible. It should be free from any moisture, corrosive vapors and work hazards. The work area should be a well vented area since cleaning solvents will be required.

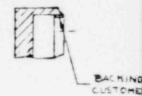




D

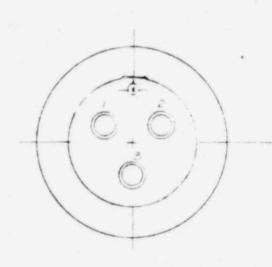
NAMEPLATE DATA





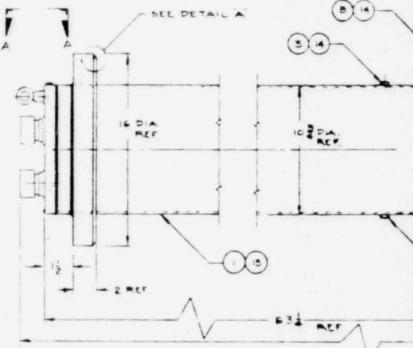
PETAIL A

INSTALLED AT
FIELD INSTALLATION
IN PRESSURE GRUNE
RESEMBLY PORT



NOTES

- HEQUIREMENTS OF THE ASHE BOILER AND FREESURE VESSELS CODE, SECTION DI,
- L DESGN PRESSURE : 54 PSIG
- PESIGN TEMPERATURE FREE FOR I HOUR FOLLOWED BY 271"F FOR 48 HOURS
- 4 MIN MUM DESIGN TEMPERATURE : BO'F
- 5. DESON RADIATION LEVEL : 1.7 x 10 0 RADS (1.5 MEV GAMMA PAYS) TOTAL INTEGRATED DOSE
- & RELATIVE HUMDITY MAX DURING THE 40 YEAR LIFE INSIDE AND DUTSIDE CONTAINMENT 50%
- T PENETRATION SEISME TEST 2565 AT 0 TO 35 HERTE
- 6 FOR INSTALLATION WELDING ASSEMBLY SEE INSTALLATION DRAWING RIBDZ476 608



SPECIFICATION X-2508 DATED

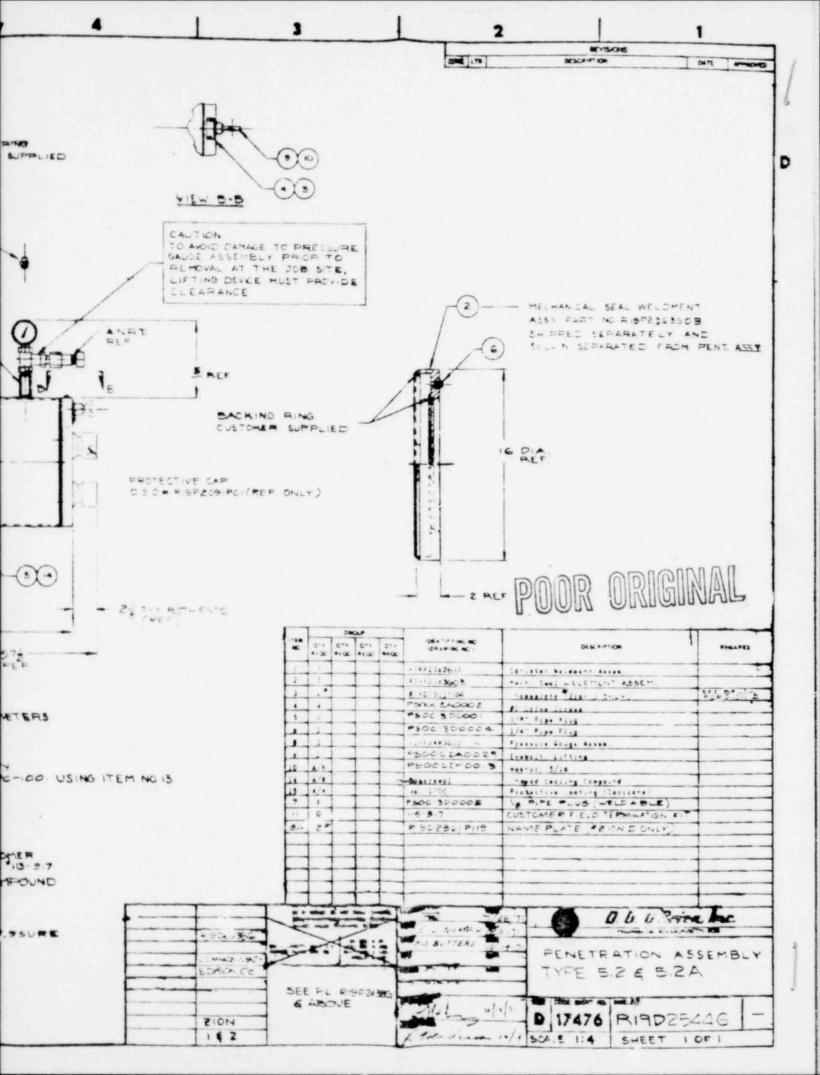
OCT. 1, 1969 INCLUDING ADDENDA 16 2 AND

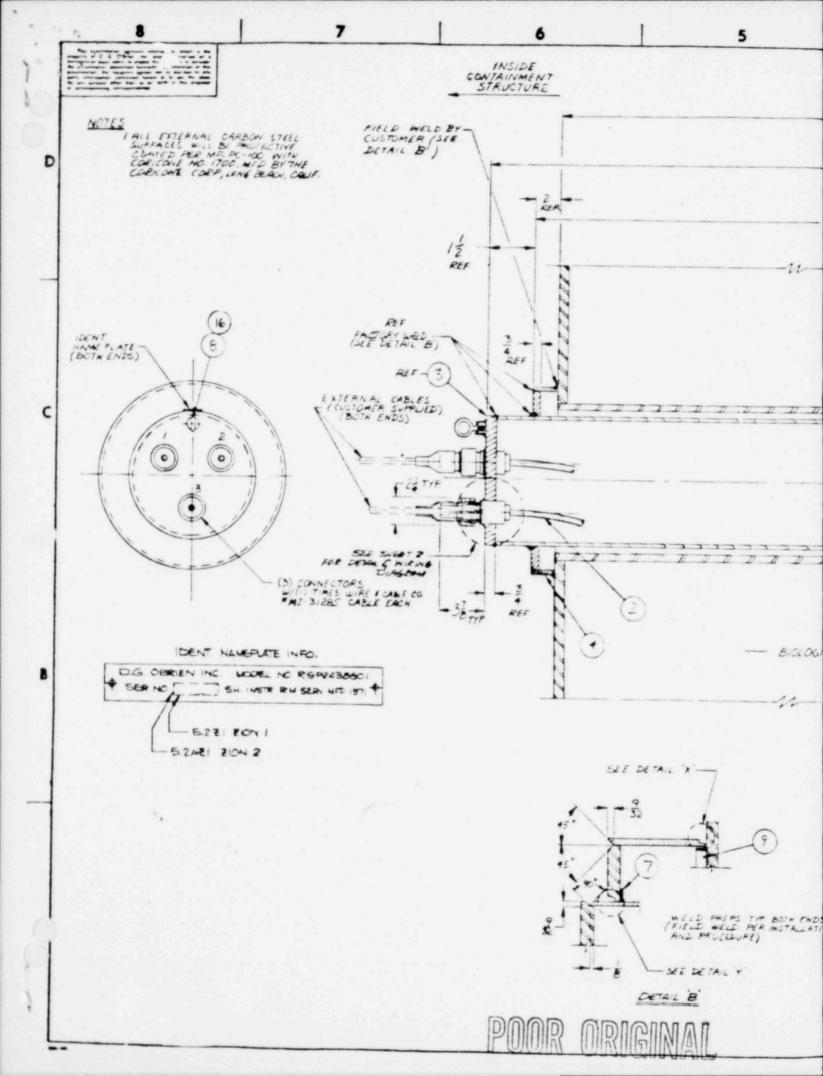
DOD QUALITY ASSURANCE METHOD

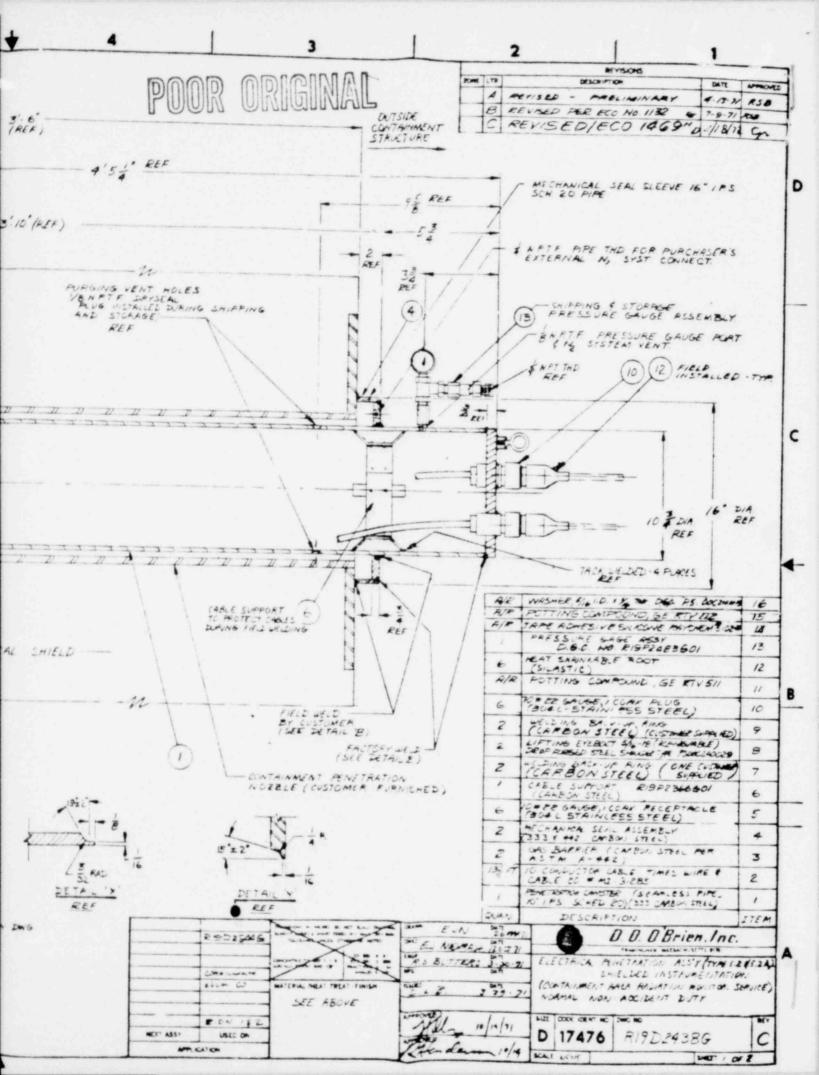
SHEET SA-TH-155-8 FOR SPECIFIC TEST PARA

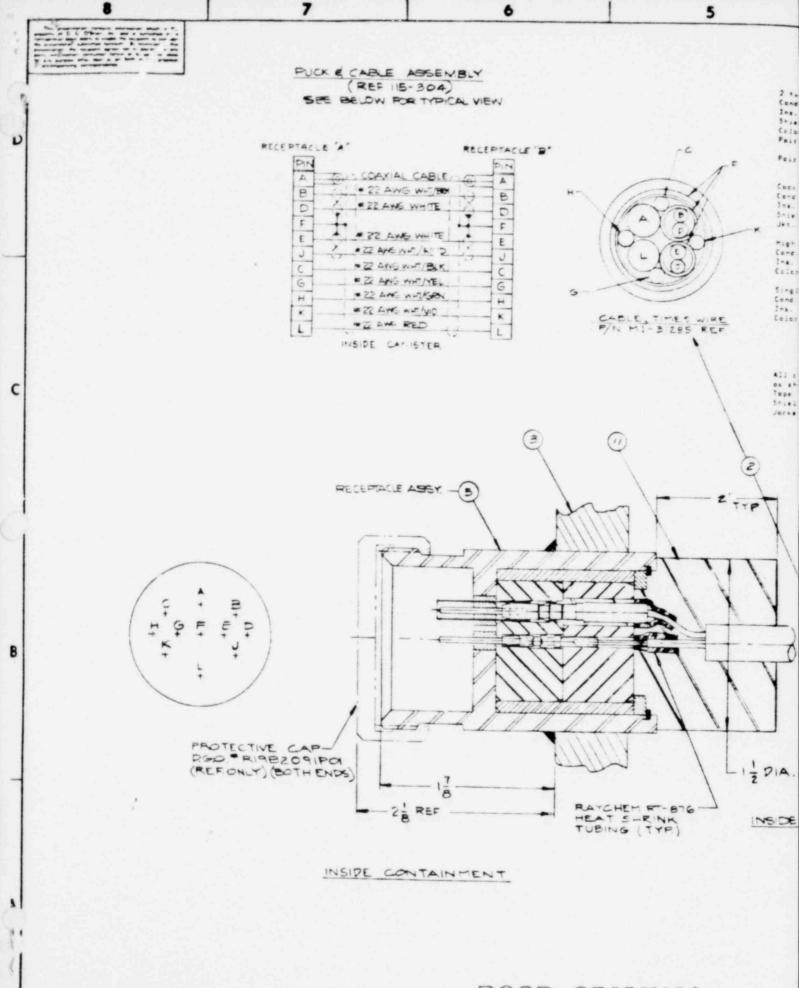
- STEEL SURFACES PER DEO PROC. HP
- IL APPROXIMATE WEIGHT 275 LBS.
 - 12. FOR CABLE TERMINATION ITEMS USE CUST MILO CABLE TERMINATION PROCEDURE, DE
 - IS USE ONLY BAKERSER THREAD SEALING CO
 - 14 PENETRATION INTERNAL SHIPPING

POOR ORIGINAL

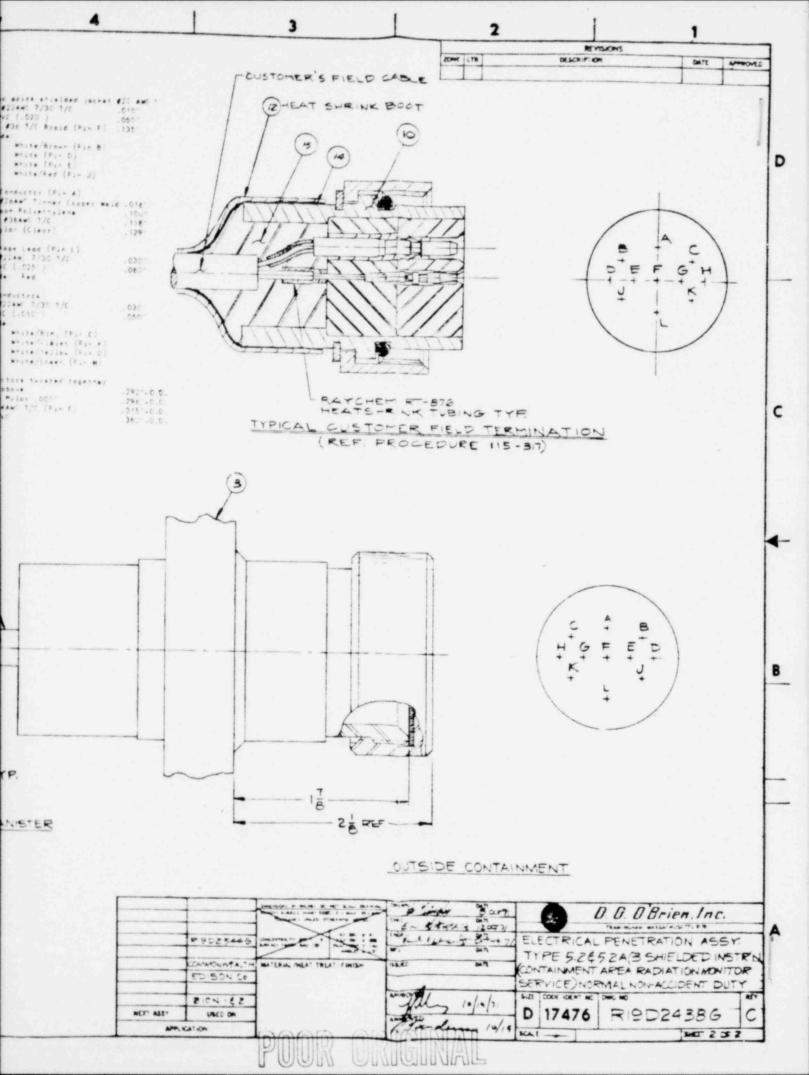








POOR ORIGINAL



3.3.3.8 Equipment No. 20
Reactor Building (Containment)
Junction Box
(Manufacturer not stated)
Model: Type EB-215
(No Licensee reference cited)

Response:

3.3.3.9 Equipment No. 21
Reactor Building (Containment)
Junction Box
(Manufacturer not stated)
Model: Type EB-214
(No Licensee reference cited)

Response:

3.3.3.10 Equipment No. 22

Reactor Building (Containment)

Junction Box

(Manufacturer not stated)

Model: Type EM-47150

(No Licensee reference cited)

Response:

3.3.3.11 Equipment No. 23

Nuclear Instrumentation - Junction Box
(Manufacturer not stated)

Model: Not stated
(No Licensee reference cited)

Response:

3.3.3.12 Equipment Item No. 28
Cables Located Within Containment
Kerite Corporation (Various Types)
Submittal Page References 6 and 11

Response:

The response to TER Item 3.3.2.11 is also applicable to this item. The Bill of Material was incorrectly interpreted as to the type of insulation and jacket materials. Page 3 of Bill of Material A-101, indicates the actual cable purchased, with Kerite "HT" insulation and Kerite "FR" and "NS" jackets. It should be noted that the Bill of Material as originally drafted suggested five specific combinations of insulation and cover while encouraging the bidder to submit qualified alternatives (refer to Item A-101, Paragragh 5, Page 1. The Bill of Material was subsequently revised to reflect the actual purchased insulation-cover combination. Adequate records exist and are available at Zion Station to provide complete traceability for the cable manufactured by Kerite and subsequently installed at Zion Station. These records consist of shipment invoices from Kerite referencing specific cable reels, Test Reports for each cable reel referencing cable type (conductor, insulation, jacket material) and cable pull cords referencing individual cables pulled from specific reels.

Franklin Research Center in our August 27, 1980 meeting at Bethesda, raised a concern about the compounds used in the Zion cables being identical to the compounds used in the cables tested and covered by Franklin Institute Test Report FC-2737.

The attached letter to H. K. Stolt from R. M. Bowman (Kerite Company) dated August 28, 1980 states that the same compounds were used in the Zion cables and test specimer cables.

The concern of preaging the cables prior to LOCA testing is also addressed in the above referenced letter.

3.3.3.13 Motor Located in the Auxiliary Building (A-8)

Submittal Page References: 23, 24

Plant ID Numbers: FW004

FW005

Response:

These are the auxiliary feedwater pump motors. A letter has been sent to Westinghouse requesting available documentation regarding qualification tests for specific environmental parameters and traceability documentation.

FSAR Q10.16 gives the motor nameplate data and justification for operability during adverse environmental conditions.

The turbine-driven auxiliary feedwater pump will be operable without the lube oil pump motor. Therefore, the pump will be available for use after a high energy line break in the auxiliary building.

With regard to motor insulation, Westinghouse has replied as follows:

"The thermal and radiation endurance of the thermalastic epoxy insulation system described in WCAP-8754 is also representative of the thermal and radiation endurance of motors supplied with this system prior to the establishment of IEEE 323-1974.

Westinghouse has verified that the HSDP Motor Driven

Auxiliary Feedwater Pump Motors and HSDP Centri: agal Charging Pump Motors at Zion utilize the thermalastic epoxy insulation system."

3.3.3.14 Equipment Item No. 34
Westinghouse Electric Indicator Model VX-252
Reactor Coolant Pressurizer Pressure and
Pressurizer Level
Submittal Page Reference 45
Qualification Reference 20 does not apply to this indicator.

PI-455B

LI-459B

Response:

These indicators are located in a non-harsh environment for LOCA. Qualification is by experience. These indicators are not required to function after high energy line break. Therefore, no qualification is required.

3.3.3.15 Equipment Item No. 35
United Electric Pressure Switch Model J110-164
Service Water Pumps Start
Submittal Page Reference 49

1PSL-SW13 - Service Water Pump 1A 1PSL-SW14 - Service Water Pump 1B 1PSL-SW15 - Service Water Pump 1C

Response:

These switches do not perform a safety function and are not required to operate after an accident. The service water pumps are started automatically by engineering safety feature actuation.

The control circuit for the service water pump 1A is shown on Drawing 22E-1-4840, Page SW1 (attached). The control circuit for service water pumps 1B and 1C are shown on Drawing 22E-1-4840, Pages SW2 and SW3 respectively. Since the control circuit is identical for pumps 1A, 1B and 1C (likewise for Unit 2) the following analysis is equally applicable to all service water pumps.

The three possible failure modes for the pressure switches are 1) contacts shorting together, 2) contacts failing to close, and 3) contacts shorting to ground.

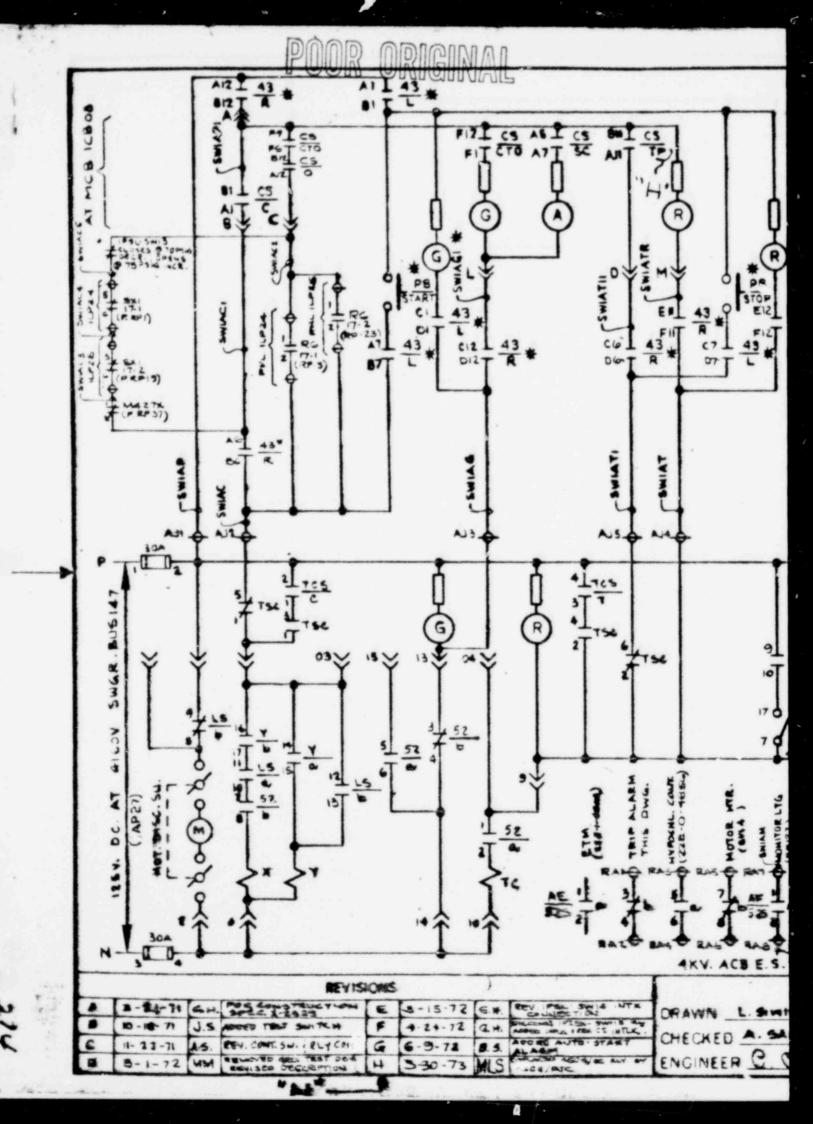
For the failure mode of the contacts shorting together, the service water pump would be started (assuming the remainder of the control functions are aligned for auto-start) thereby giving additional service water pumping capacity.

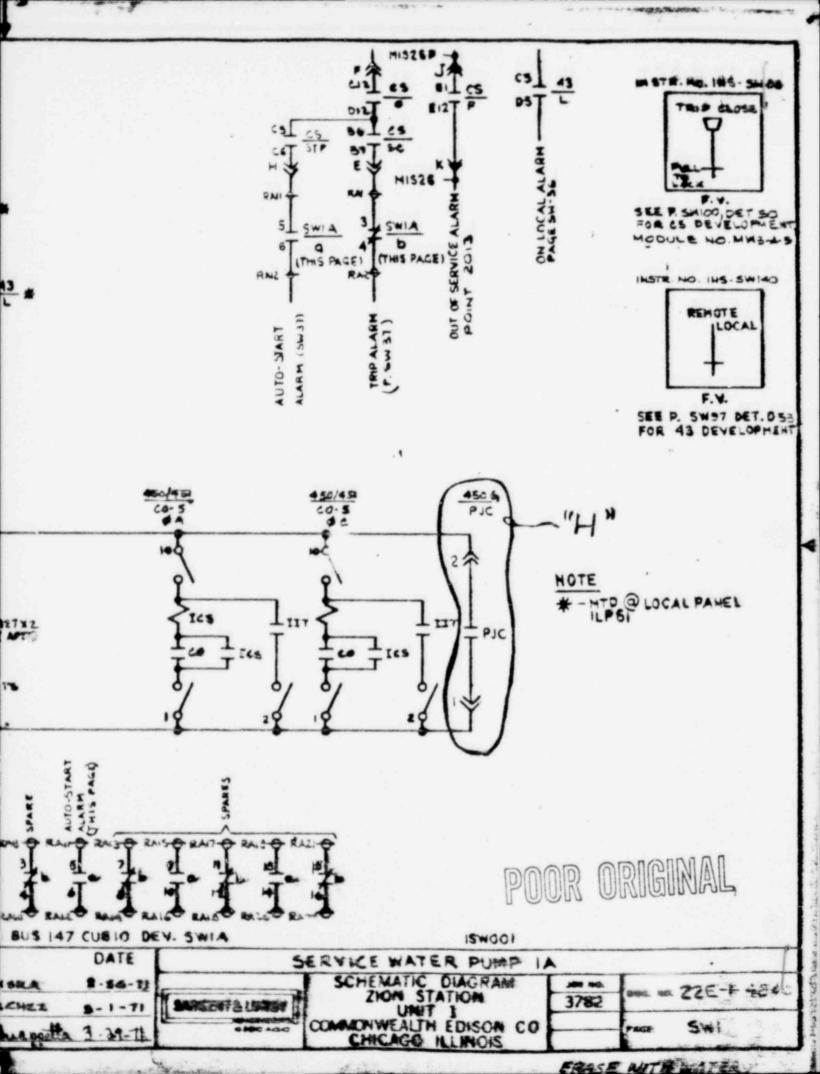
For the failure mode of the contacts failing to close, the service water pump would remain in its standby state of readiness and would be started by the automatic safety actuation circuits.

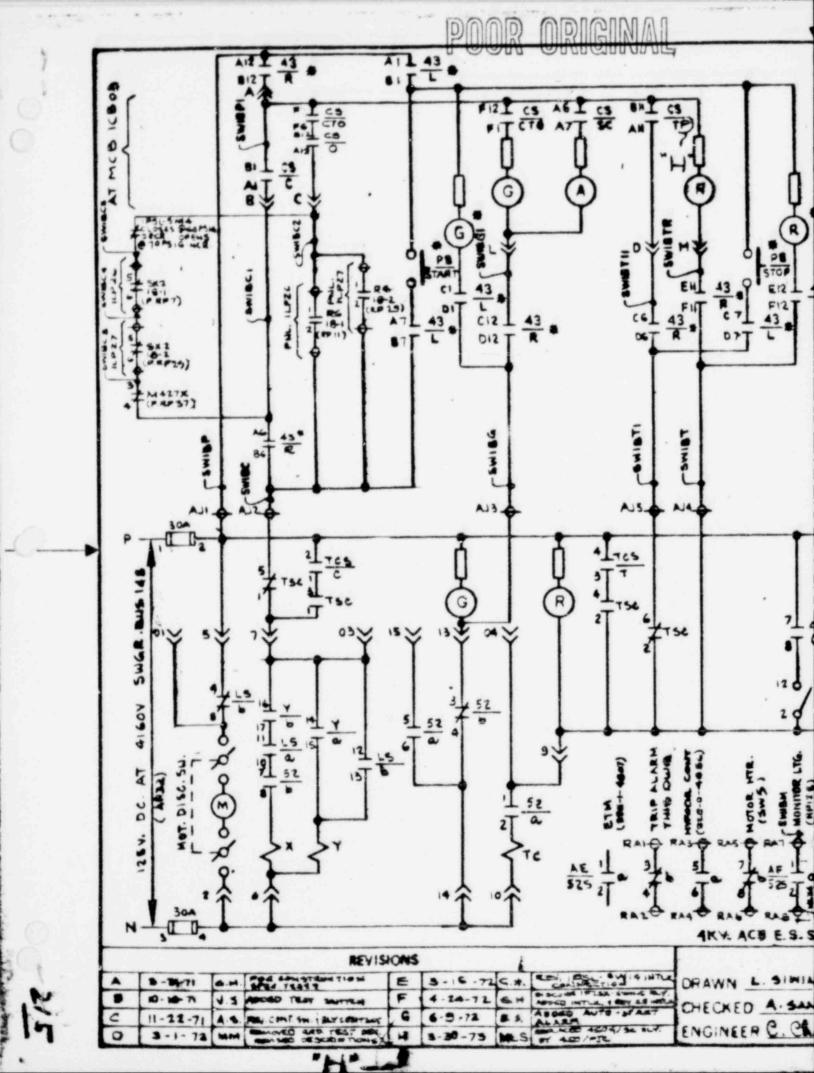
For the failure mode of the pressure switch contacts shorting to ground, an alarm would be sounded (in the control room) indicating a ground on the normally ungrounded 125V DC system. No control action of the service water pump would be affected since both polarities of the 125V dc control circuit are ungrounded, and the fuses will not "blow" until a second ground occurs in the opposite polarity. Zion Procedure ("DC Ground Location Procedure") calls for locating and removing all grounds on the DC systems as soon as detected.

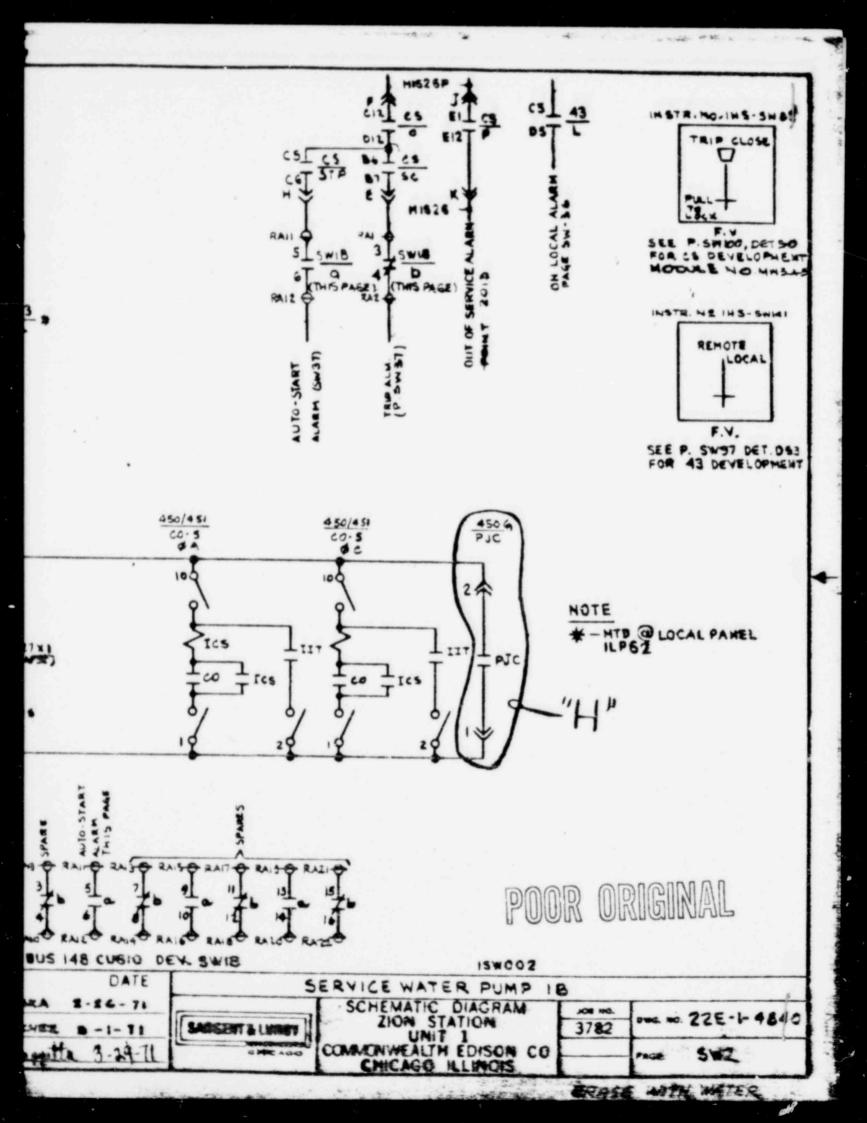
3.3.3.15 (Cont'd)

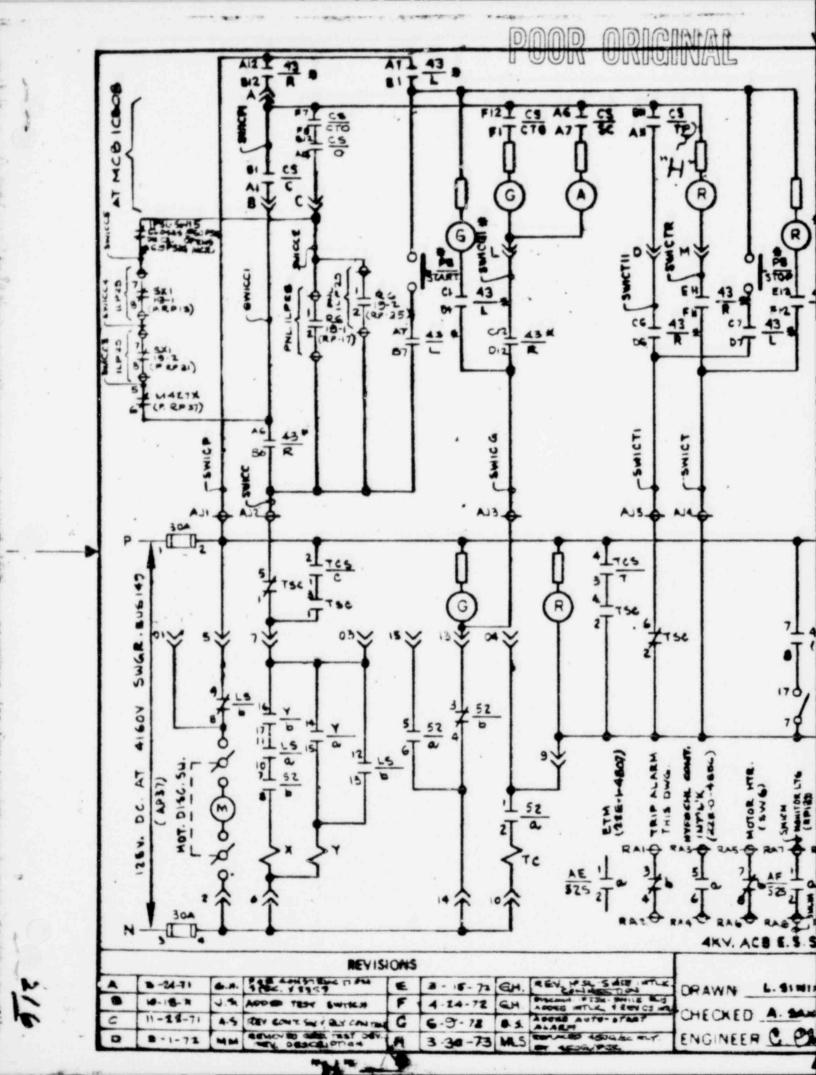
Therefore, no failure mode exists which will degrade the service water pump control circuitry due to the use of an unqualified pressure switch.

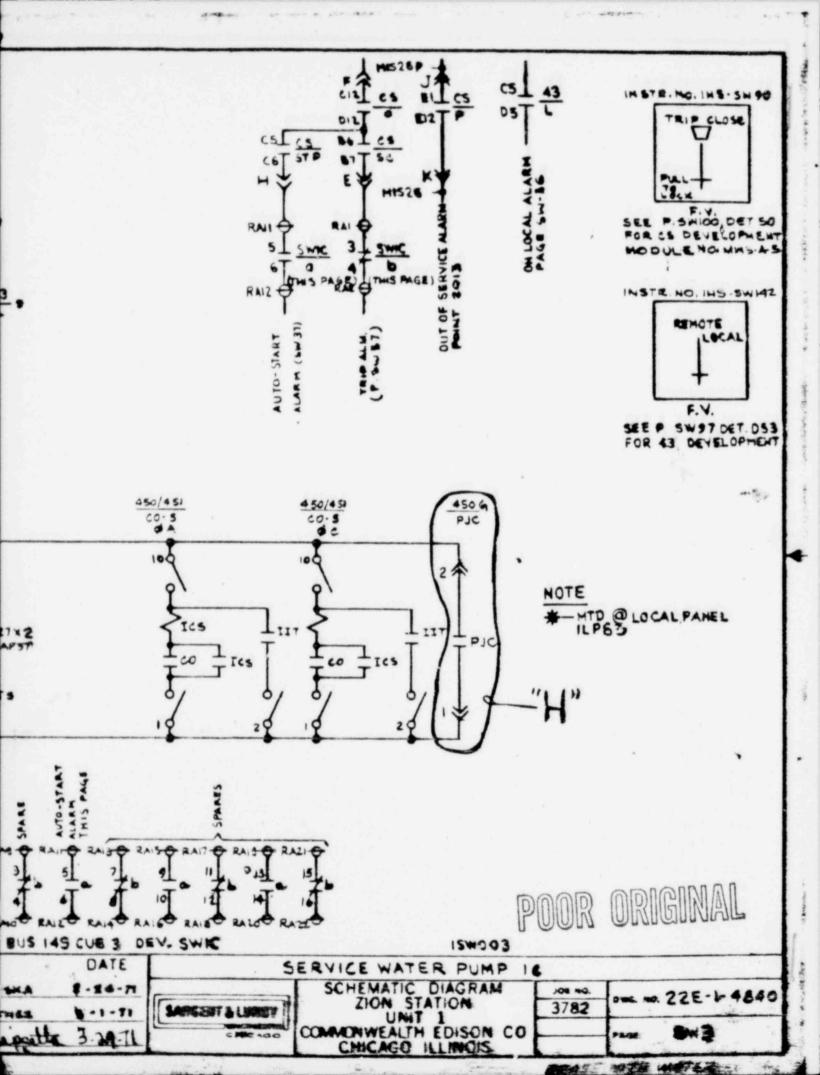












3.3.3.16 Equipment Item No. 36A (Unit 1 only)
Distribution Panel Located in the Auxiliary
Building (A-8)
Fischbach-Hatfield B/M C458
Submittal Page Reference 53 and 54

Response:

This equipment was incorrectly included in the report. The equipment involved are distribution panels for Motor-operated Valve (MOV) heaters. Since the MOV heaters do not perform a safety function the distribution panels are not needed.

3.3.3.17 Equipment Item No. 36B (Unit 2 only)
Motor Control Center (MCC 2383B) Located
in the Auxiliary Building (A-8)
General Electric 7700 Line,
480 Volt
Submittal Reference Page 50

Response:

This motor control center while supplying loads (services) which may be used to mitigate the consequences of a LOCA or HELB inside the containment will not be subjected to a harsh environment at that time. For a HELB (Auxiliary Steam Line Break), outside of containment, the motor control center will be subjected to a harsh environment. The Licensee is currently identifying the electrical components and instrumentation required to operate to mitigate the consequences of the postulated HELB. This list of components will be submitted as part of Appendix F, "Equipment Required To Operate After High Energy Line Break In Auxiliary Building" on September 27, 1980.

The complete list of loads (services) served by motor control center MCC 2383B is shown on Drawing 22E-2-4000AN. A copy of this drawing was given to Mr. S. J. Crane at Bethesda on August 27, 1980, as our response to Appendix D concerns.

3.3.3.18 Equipment Item No. 38 (Unit 1 only)
Junction Boxes Located in the
Auxiliary Building (A-8)
General Electric 7700 Line,
480 Volt
(No Licensee reference cited)

Response:

3.3.3.19 Motor Located in the Auxiliary Building (A-9)

Submittal page references: 22

Plant ID number: 1PP001

Response:

This is the penetration pressurization air compressor motor. The equipment is required only after a LOCA or main steam/feedwater line break inside containment. For these accidents the equipment is located in a non-harsh environment. Qualification by experience.

3.3.3.20 Hydrogen Recombiner Located in the Auxiliary Building (A-9)
Submittal Page Reference: 33

Plant ID Number: RV050

Response:

This equipment is required to function following a LOCA. However, for the LOCA zone A-9 is considered a non-harsh zone and will not see elevated parameters. Qualification is by experience.

Due to its service, the motor in the blower assembly may see high radiation. The Licensee is performing calculations to verify that the radiation exposure to the motor following a LOCA does not exceed 10⁴ rads.

Results will be submitted by September 27, 1980.

A letter has been sent to Rockwell requesting available test report documentation and traceability documentation.

3.3.3.21 Hydrogen Purge Fan Motor Located in the Auxiliary Building (A-9)

Submittal Page Reference: 36

No Licensee reference

Equipment ID numbers: RV020

RV021

Response:

This equipment is required to function following a LOCA.

However, for the LOCA Zone A-9 is considered a non-harsh

zone and will not see elevated parameters. Qualification
therefore is by experience.

Due to its service, the motor may see high radiation. The Licensee is performing calculations to verify that the radiation exposure to the motor following a LOCA does not exceed 10⁴ rads. Results will be submitted by September 27, 1980.

3.3.3.22 United Electric Temperature Switch Model C300
Hydrogen Purge Charcoal Filter Temperature

Equipment Item No. 43A

Plant ID Numbers: PS-RV128 A,B PS-RV129 A,B

Response:

These switches are required to function following a LOCA. However, for the LOCA zone A-9 is considered a non-harsh zone and will not see elevated parameters. Qualification is by experience.

Due to their service, the switches may see high radiation. The Licensee is performing calculations to verify that the radiation exposure to the switches following a LOCA does not exceed 10⁴ rads. Results will be submitted by September 27, 1980.

3.3.3.23 Equipment Item No. 43B (Unit 2 only)
Junction Box Located in the
Auxiliary Building (A-9)
Type EB-214
(No Licensee reference cited)

Response:

3.3.3.24 Equipment Item No. 44

Magnetrol Level Transmitter 82-1212-002

Spray Additive Tank Level

Submittal Page Reference 40

LIS-CS44 LIS-CS45

Response:

These level transmitters are located in a non-harsh environment after LOCA. Therefore, qualification is by experience.

These transmitters are not required to operate after HELB. Therefore, no qualification is required. These Magnetrol switches have replaced the Endress-Houser switches which were used in the June 1980 submittal to Franklin Institute.

3.3.3.25 Equipment Item No. 45
Nuclear Measurement Corporation Radiation
Detectors Models

GM-912, SC-2-15, SC-2B

Auxiliary Building Radiation Submittal Page Reference 46, 47, 48

ORE-AR08 ORE-AR09

Response:

These radiation detectors are not required to operate after LOCA or HELB. Therefore, no qualification is required.

3.3.3.26 Equipment Item No. 47
Control Panel Located in the
Auxiliary Building (A-9)
Powers Regulator Company
Submittal Page Reference 59

Response:

These panels, 1LP22 and 2LP22, serve the Containment Ventilation System. These panels will not be subjected to a harsh environment due to a LOCA or HELB inside containment and also do not contain any components required to mitigate a HELB outside the containment.

3.3.3.27 Equipment Item No. 48
Junction Box Located in the
Auxiliary Building (A-9)
Type EM-47150
(No Licensee reference cited)

Response:

3.3.3.28 Equipment Item No. 49
United Electric Pressure Switch J302-358
Penetration Pressurization
Submittal Page Reference 50

OPSL-PP01A 1PSL-PP23 OPSL-PP10B 2PSL-PP22

Response:

These switches are located in a non-harsh environment after LOCA and HELB inside containment. Therefore, qualification is by experience.

3.3.3.29 Equipment Item Nos. 50, 51
Junction Boxes Located in the
Auxiliary Building (A-9)
Types EM-47159 and EB-214
(No Licensee reference cited)

Response:

3.3.3.30 Equipment Item No. 54A (Unit 1 only)
Control Panel Located in the Auxiliary
Building (A-12)
Westinghouse, Waste Gas and
Recovery Panel
Submittal Page Reference 60

Reference:

This panel is not needed to mitigate the consequences of a LOCA or HELB and should not be included in report.

3.3.3.31 Equipment Item No. 54B
Junction Boxes Located in the
Auxiliary Building (A-12)
Type EB-214
(No Licensee reference cited)

Response:

3.3.3.32 Equipment Item No. 55
Junction Boxes Located in the
Auxiliary Building (A-12)
Type EM-47150
(No Licensee reference cited)

Response:

3.3.3.33 Pump Motor Located in the Auxiliary Building (A-14)
Submittal Page References: 15, 16
No Licensee reference

Pump ID Numbers: VC006 Centrifugal Charging Pump VC007 Centrifugal Charging Pump

VC008 Reciprocal Charging Pump

Response:

Long-term operation is required for LOCA or main steam/
feedwater line break for VC006 and VC007. For the LOCA
the only harsh parameter is radiation. Also, these pumps
are required long-term for a high energy line break in the
auxiliary building. A letter has been sent to Westinghouse
requesting test report documentation and traceability
documentation. Justification for pump operability
is provided in the FSAR, Q10.16.

VC008 is not required to operate after a LOCA or main steam/feedwater line break. Qualification not needed.

With regard to the motor insulation for the centrifugal charging pumps, Westinghouse has replied:

"The thermal and radiation endurance of the thermalastic epoxy insulation system described in WCAP-8754 is also representative of the thermal and radiation endurance of motors supplied with this system prior to the establishment of IEEE 323-1974. Westinghouse has verified that

3.3.3.33 cont'd

the HSDP Motor Driven Auxiliary Feedwater Pump Motors and HSDP Centrifugal Charging Pump Motors at Zion utilize the thermalastic epoxy insulation system."

3.3.3.4 Unit Cooler Fan Motors Located in the Auxiliary
Building (A-14)

Plant ID Numbers: AV010 AV011 AV012

Response:

Long-term operation is required after an accident.

A letter has been sent to Westinghouse to obtain available qualification test reports and traceability documentation.

3.3.3.35 Equipment Item No. 59 (Unit 1 only)
Thermostat Located in the
Auxiliary Building (A-14)
Penn Model A-28-AA37
Submittal Page Reference 38

OTS-AV99 - Residual Heat Removal Pump 1A OTS-AV100 - Residual Heat Removal Pump 1B OTS-AV101 - Residual Heat Removal Pump 2B OTS-AV102 - Residual Heat Removal Pump 2A OTS-AV103A - Containment Spray Pump 1A OTS-AV103B - Containment Spray Pump 1B OTS-AV104 - Safety Injection Pump 2A OTS-AV105 - Safety Injection Pump 2B OTS-AV106A - Containment Spray Pump 2A OTS-AV106B - Containment Spray Pump 2B OTS-AV107 - Safety Injection Pump 1B OTS-AV108 - Safety Injection Pump 1A OTS-AV109 - Charging Pump 2C OTS-AV110 - Charging Pump 2B OTS-AV111 - Charging Pump 2A OTS-AV112 - Charging Pump 1C OTS-AV113 - Charging Pump 1B OTS-AV114 - Charging Pump 1A

Response:

These components are not required to operate after a LOCA or HELB. The cubicle coolers are started automatically, whenever their associated safety system pump is started. The control circuit for the cubicle coolers associated with Centrifugal Charging Pump 1A (shown on Drawing 22E-1-4840, Page AV7) is typical of the control circuit for all the pumps listed above.

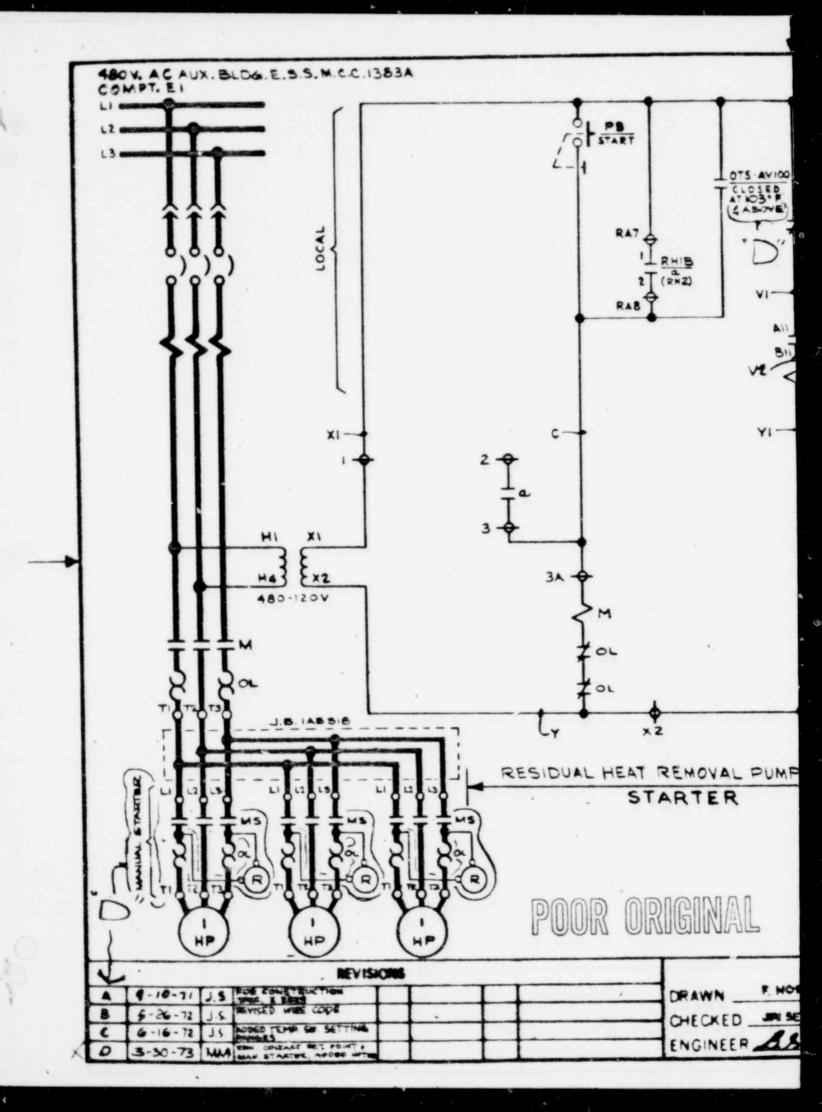
Schematic Diagrams for the Residual Heat Removal Pump 1B unit cooler and the Safety Injection Pump 1A unit cooler are shown on Drawing 22E-1-4840, Pages AV2 and AV3 respectively. Copies of these drawings are enclosed for your use.

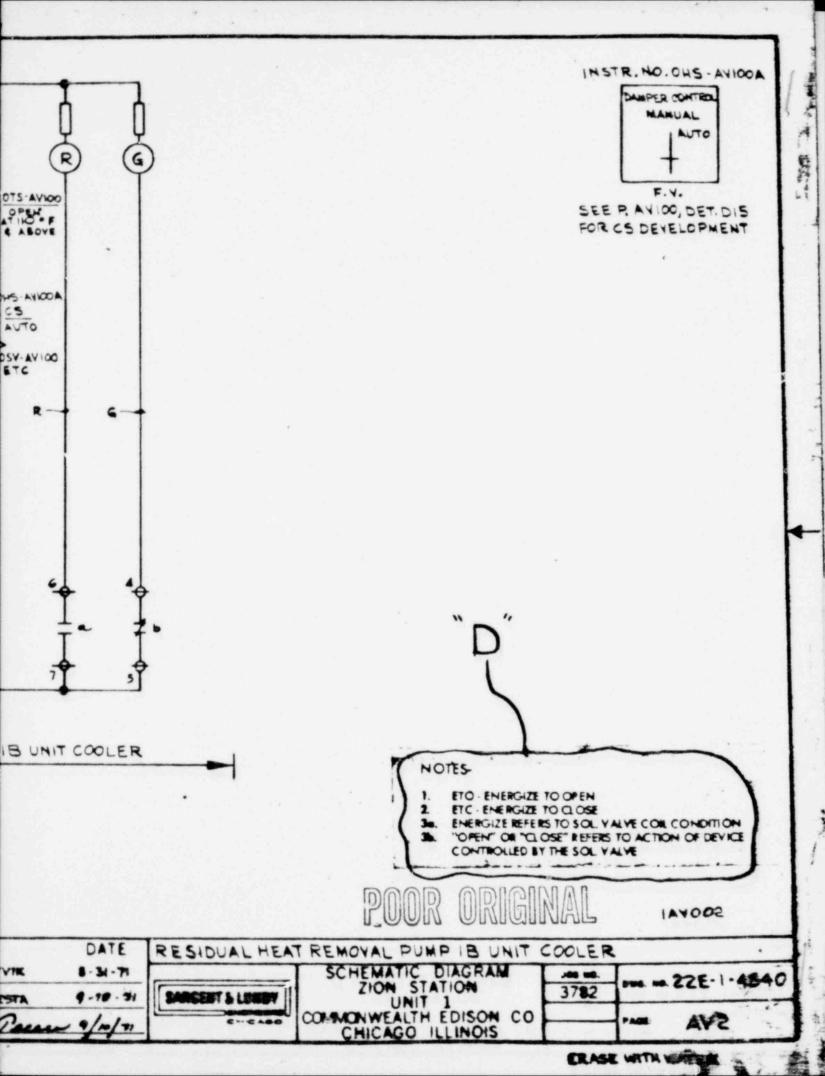
Note: The control circuit for the Centrifugal Charging Pump 1A Unit Cooler will be discussed. All other coolers are similar. The thermostat (OTS-AV114), as well as the pushbutton shown on the schematic (Page AV7), do not perform a safety function and their failure will not impair the operation of the cubicle coolers. The possible failure modes for the thermostat, as well as the pushbutton, are 1) contacts short together, 2) contacts fail to close (remain open), and 3) contacts short to ground.

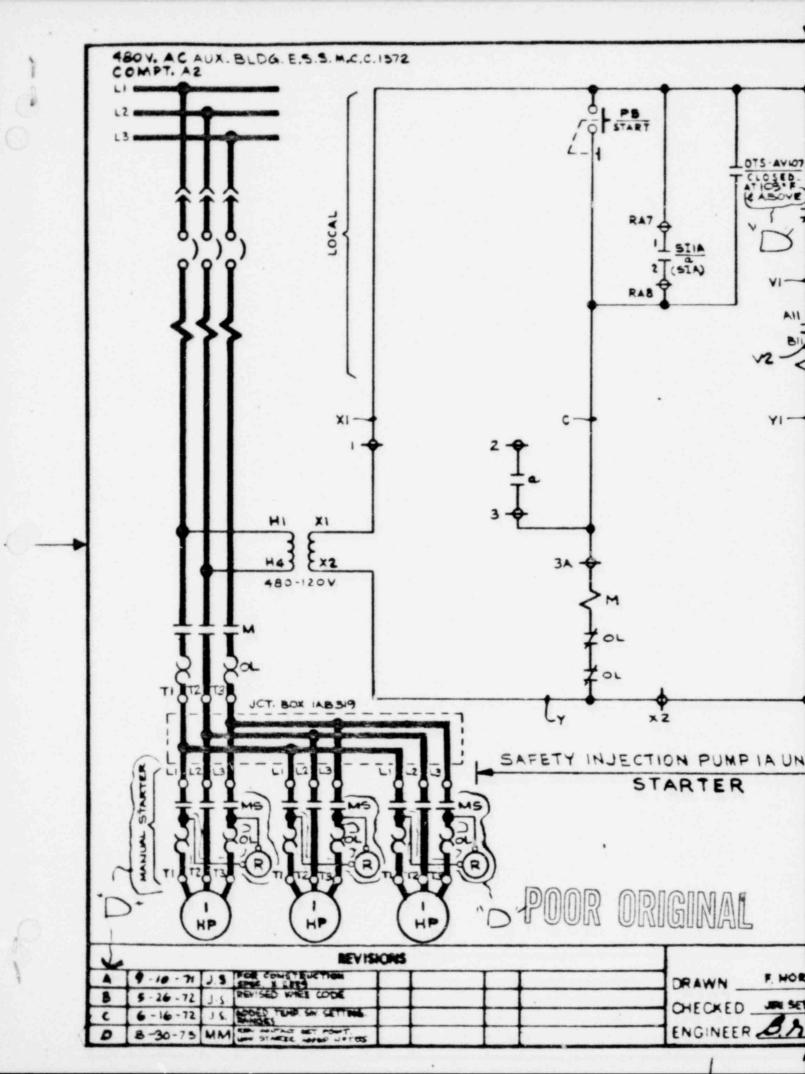
- If the contacts short together, the cubicle cooler will be started and therefore will not impair the function of the cooler to cool the safety pumps.
- If the c stacts remain open, the starting circuit, 'rough the start signal from the safety pump, will still start the cooler and perform its function.
- 3. If the contacts short to ground, the control of the cooler will not be affected due to the control circuit be ungrounded and unfused. The cooler can still be started by the autostart signal in the presence of a short to ground by the thermostat (or pushbutton).

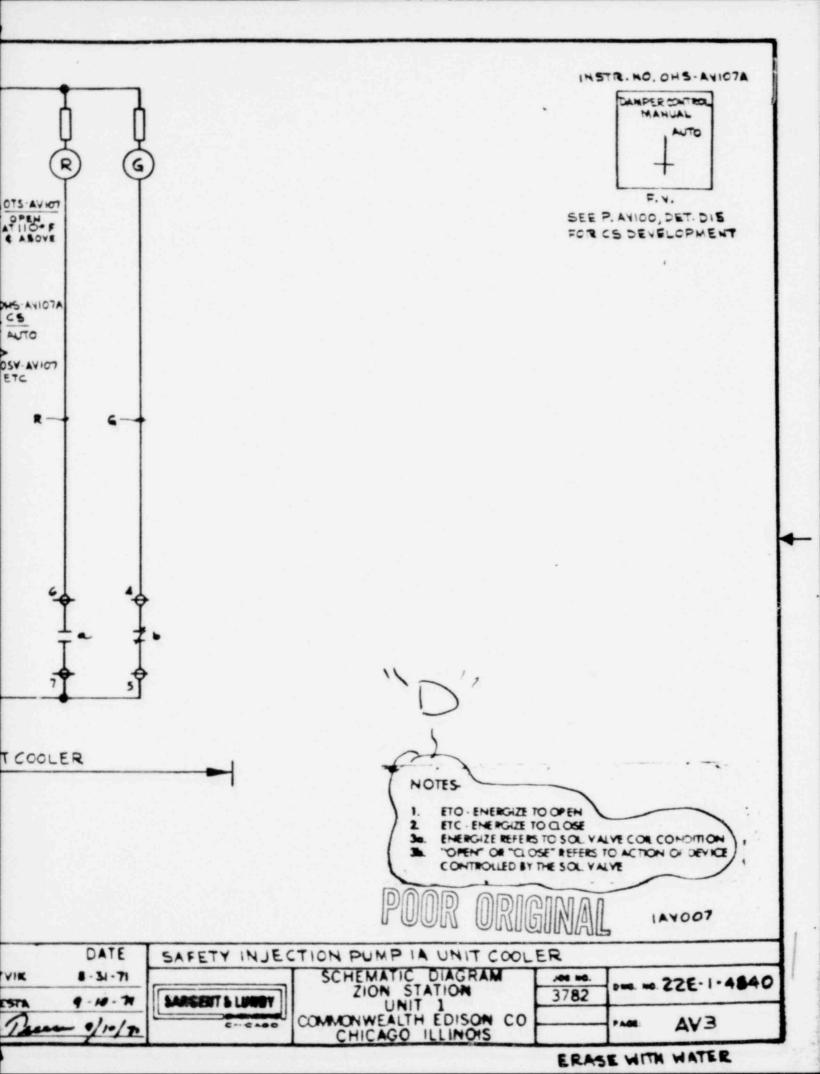
The control of the solenoid valve OSV-AV99 is also not impaired enough to defeat the function of cooling the safety pumps. The solenoid valve controls a damper to normally maintain the pump cubicle at 0.5" H2O negative pressure with respect to the surrounding area. If the thermostat contacts short together, the damper will maintain the 0.5" H2O negative pressure. If the thermostat contacts open, the damper will fail to open, allowing the room to assume the same pressure at the surrounding area. This will not affect the ability of the coolers to cool the pumps.

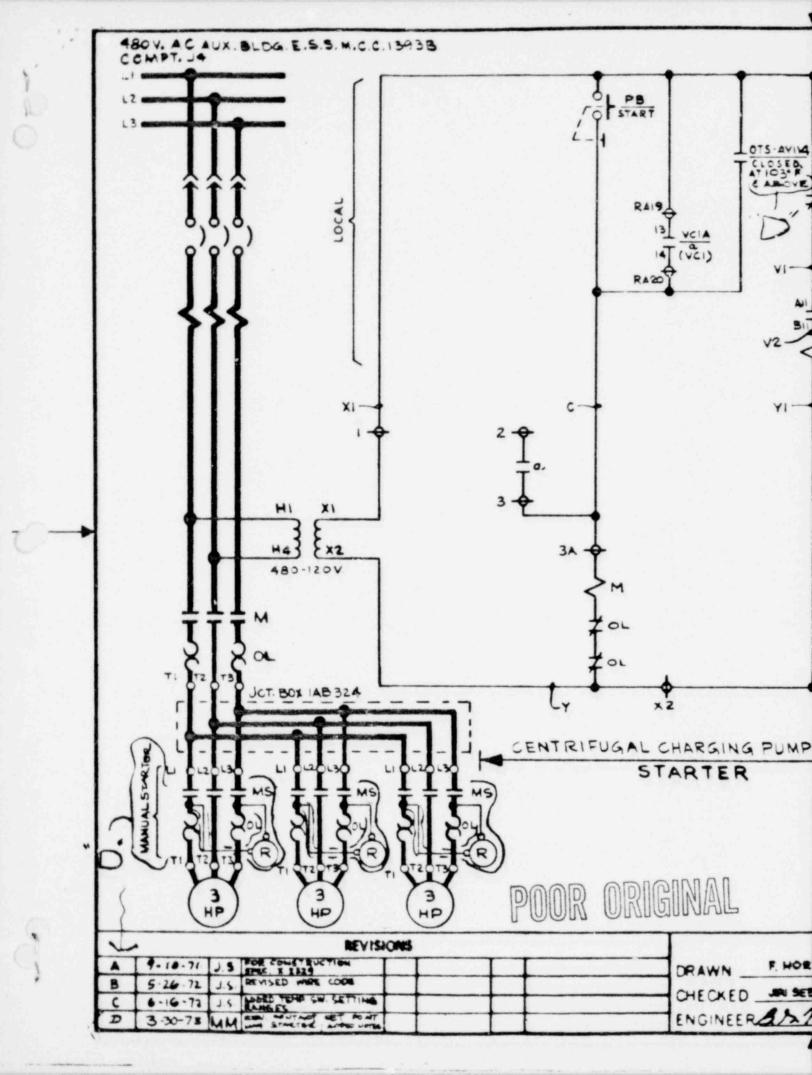
Based on the above analysis, no qualification is necessary.

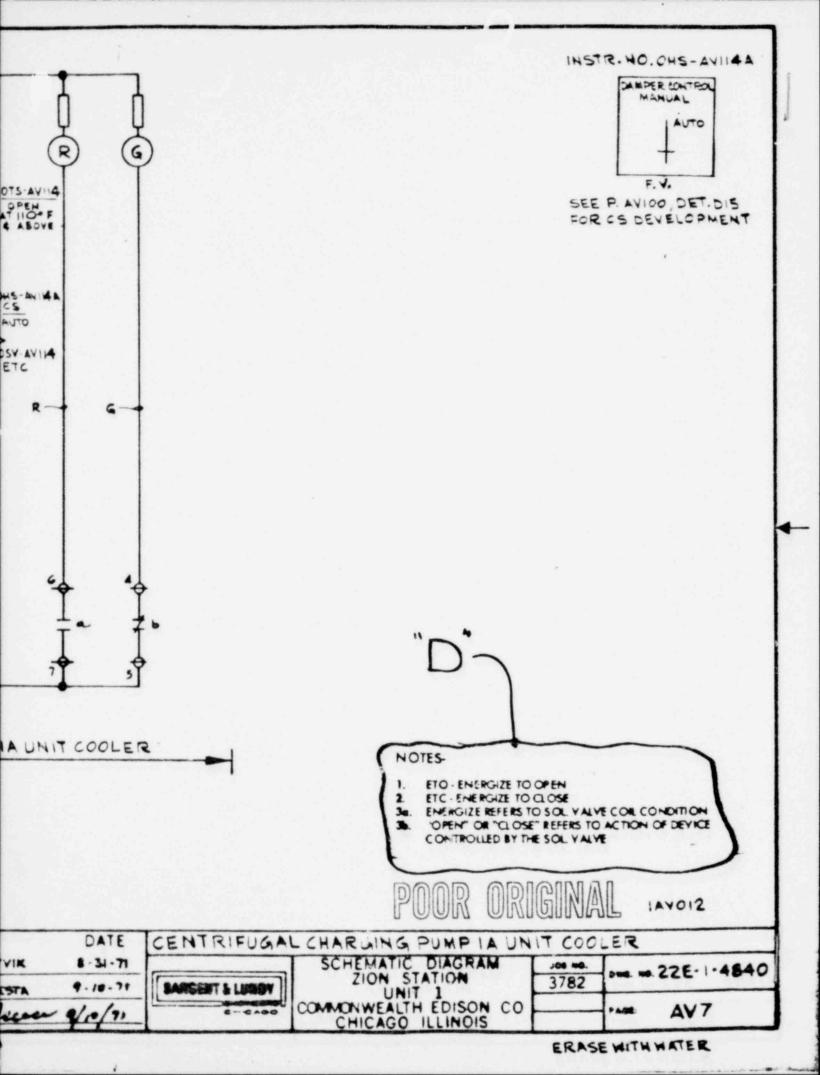












3.3.3.6 Motors Located in the Lower Safety Valve Room (T-3)
Westinghouse Model TBFC

Plant ID Number: MS016

MS017 MS018

MS019

Response:

These are the hydraulic units for the main steam isolation valves. Short-term operation is required. However, the referenced motor is not required if the hydraulic accumulator is charged. Also, once the MSIV valve closes it should remain closed due to steam pressure.

The MSIV's operate following a safeguards actuation in order to isolate steam flow from the steam-generator to the turbine. The MSIV's are equipped with the following:

- Pump: During normal operation this pump maintains both the opening and closing side pressure at close to 800 and 1800 psig respectively. This piece of equipment is not required to operate following safeguards actuation signal.
- 2) Pressure Switch: Sends startup signal to pump should the pressure in either side of line fall below setpoint. Not required to operate following safeguards actuation signal.

3.3.3.36 cont'd

- 3) Accumulator: Both on opening and closing side of valve. The closing side must discharge in order to close MSIV.
- 4) Pilot Operated Check Valve: Two on either side of MSIV.

 These valves must open to allow the accumulator to

 discharge on the closing side of the MSIV and also

 to allow flow from the open side of the valve to

 discharge into the reservoir tank.
- 5) 125 VDC 3-way Solenoid Valve: This is the operator for the check valve. These solenoids (2 per MSIV) must provide the signal to open the check valves. Their operation will ensure that the accumulator closes the MISV.

conclusion: Only the solenoids must operate electrically in the harsh environment in order to shut the MSIV's. They operate a short period of time (5 seconds) after the actuation signal to allow the accumulators to close the valve. Westinghouse has been contacted to provide available qualification for the solenoids.

3.3.3.37 Equipment Item No. 64 (Unit 2 only)
Junction Boxes Located in the
Lower Safety Valve Room (T-3)
Type EB-215
(No Licensee reference cited)

Response:

3.3.3.38 Equipment Item No. 65 (Unit 2 only)
Junction Boxes Located in the
Steam Tunnel (T-4)
Type EB-215
(No Licensee reference cited)

Response: