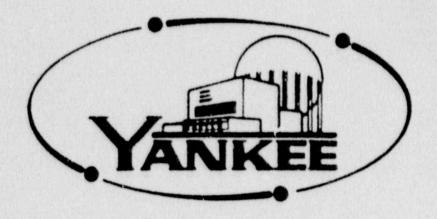
YAEC NO. 1710 NOVEMBER 1989

# YANKEE NUCLEAR POWER STATION PILOT EVALUATION REPORT FOR PLANT LICENSE RENEWAL



YANKEE ATOMIC ELECTRIC COMPANY
in cooperation with
THE ELECTRIC POWER RESEARCH INSTITUTE
THE U.S. DEPARTMENT OF ENERGY
and
SANDIA NATIONAL LABORATORIES

# YANKEE NUCLEAR POWER STATION PILOT EVALUATION REPORT

for

PLANT LICENSE RENEWAL

Prepared by
YANKEE ATOMIC ELECTRIC COMPANY
580 Main Street
Bolton, Massachusetts 01740-1398

Project Director: John Haseltine Assistant Project Manager: William Hinkle

In cooperation with

ELECTRIC POWER RESEARCH INSTITUTE 3412 Hillview Avenue Palo Alto, California 94303

Program Manager: John Carey Project Manager: Richard Burke

and

U.S DEPARTMENT OF ENERGY Office of LWR Safety and Technology 19901 Germantown Road Germantown, Maryland 20874

Program Manager: Dennis Harrison Project Manager: Arthur DuCharme

#### DISCLAIMER OF RESPONSIBILITY

This report was prepared by Yankee Atomic Electric Company (YAEC) as an account of work sponsored by the Electric Power Research Institute, Inc. (EPRI), Department of Energy (DOE), and Sandia National Laboratories (SNL). Neither EPRI, members of EPRI, DOE, SNL, YAEC, nor any person acting on their behalf: (a) makes any warranty, express or implied, with respect to the use of any information, apparatus, method, or process disclosed in this report or that such use may not infringe privately owned rights; or (b) assumes any liabilities with respect to the use of, or for damages resulting from the use of, any information, apparatus, method, or process disclosed in this report.

#### ABSTRACT

The Yankee Pilot Evaluation Report provides the application of a process for evaluating systems, structures, and components for license renewal. The methodology and criteria used are based on the Nuclear Management Resources Council (NUMARC) Nuclear Plant Life Extension (NUPLEX) "Methodology to Evaluate Plant Equipment for License Renewal." The Pilot Report was prepared as part of the Yankee Lead Plant License Renewal Project which is co-sponsored by the U.S. Department of Energy, the Electric Power Research Institute, and Yankee Atomic Electric Company.

The key objectives of the Yankee Pilot Evaluation Report are to demonstrate through a formalized process that:

- o All systems, structures, and components requiring license renewal evaluation are identified.
- Any potentially significant age-related degradation is recognized and properly managed, as necessary.

As presented in the report, these objectives have been met. Of the total 78 systems and 46 structures at Yankee, 43 systems and 27 structures were determined to require evaluation for license renewal. The potential for significant age-related degradation and the methods of managing degradation were assessed for the pilot systems and structures.

The components evaluated in the Pilot Evaluation Report are all related to the Safety Injection (SI) System. Included are SI fluid system and I&C components, Emergency Electrical Power System (EEPS) components, and the structural components of the Primary Auxiliary Building (PAB), Diesel Generator Building (DGB), and Battery Room No. 3 Building (B3B).

The areas of the plant evaluated were generally found to be in good condition with no signs of significant digradation. However, as indicated in the report, several components will require further evaluation and some plant programs will need enhancement to bette address degradation concerns for license renewal.

The methodology, criteria, and technical justification supporting the evaluation process are provided, as well as examples of specific assessments, checklists, and other supporting information to allow the NRC staff to conclude that the process used is both thorough and technically justified. Because the same evaluation process used for the components presented in the Pilot Evaluation Report is being applied to the plant in general, it should simplify future NRC license renewal reviews.

# TABLE OF CONTENTS

				Page					
	DISC	LAIMER O	F RESPONSIBILITY	ii					
	ABST	RACT		iii					
1.0	INTR	ODUCTION		1					
2.0	METH	ODOLOGY.	DDOLOGY						
3.0	EVAL	UATION O	F PLANT SYSTEMS/STRUCTURES/COMPONENTS	6					
	3.1	Identi	fication of Systems and Structures	6					
	3.2	System	and Structural Boundaries	7					
	3.3	System and Structural Boundaries							
				7					
			Systems Relied Upon or Structures Identified in a Licensing Basis Safety Analysis or	8					
		3.3.3	3.3.2.2 Technical Specifications	8 8 9 9 9 9 9 9 10 10 10 10 10					
	3.4	.4 Identification of Systems and Structures for Which Degradation is Potentially Significant to Plant							
				11					
		3.4.1 3.4.2 3.4.3	Uncontrolled Radioactive Release	11 12 12					

### TABLE OF CONTENTS (Continued)

				Page
		3.4.4	Structures Housing Significant Systems	14
		3.4.5	Results - Listing of Systems and Structures	
		3.4.5	For Which Degradation is Potentially Significant	
			to Plant Safety	14
	3.5	Compone	ent Evaluation	15
		3.5.1	Components Important to System or Structure Safety	
			Function	16
		3.5.2	Components Subject to an Established, Effective	
			Replacement, Refurbishment, or Inspection	
			Program	17
		3.5.3	Components Subject to Potentially Significant	
		3.3.3	Age-Related Degradation	19
4.0	PILOT	APPLICA	ATION	24
	4.1	Purpose	e and Scope	24
	4.2	Safety	Injection System Fluid Components	25
		4.2.1	Identification of SI Fluid Components	25
		4.2.2	Safety Function Review	25
		4.2.3	Effective Program Review	26
		4.2.4	Aging-Degradation Review	27
		4.2.5	Summary - SI Fluid Component Review	29
	4.3	Safety	Injection System I&C Components	29
		4.3.1	Identification of I&C Components	29
		4.3.2	Safety Function Review	29
		4.3.3	Effective Program Review	30
		4.3.4	Aging-Degradation Review	32
		4.3.5	Summary - Safety Injection I&C Component Review	32
	4.4	Emerger	ncy Electric Power System (EEPS)	32
		4.4.1	Identification of Components	32
		4.4.2	Safety Function Review	33
		4.4.3	Effective Program Review	34
		4.4.4	Aging-Degradation Review	36
		4.4.5	Summary - EEPS Component Review	37

# TABLE OF CONTENTS (Continued)

				Page					
	4.5		Auxiliary Building/Diesel Generator Building/						
		Battery	Room No. 3 Building Structural Review	. 37					
		4.5.1	Identification of Components	. 38					
		4.5.2	Safety Function Review	. 38					
		4.5.3	Effective Program Review						
		4.5.4	Aging-Degradation Review						
		4.5.5	PAB/DGB/B3B Walkdown Results						
		4.5.6	Summary - PAB/DGB/B3B Structural Review	. 41					
5.0	CONC	LUSIONS		. 50					
ATTA	CHMENT	S							
Α.	Appendix A (Criteria) to NUMARC NUPLEX "Methodology to Evaluate Plant Equipment for License Renewal"								
В.	Plan	t System	and Structures List						
	(Inc	(Including Brief System and Structure Descriptions)							
c.	Step la Review Results - Systems and Structures Which Contribute to Plant Safety								
D.	Step 1b Review Results - Systems and Structures for Which Degradation is Significant to Plant Safety								
E.	Safe	ty Inject	ion System Fluid Component Review Results						
F.	Safety Injection System Applicable Procedures List								
G.	Component Degradation Assessment Tool Description								
н.	Safety Injection System I&C Component Review Results								
ī.	EEPS	Componen	t Review Results						
J.	EEPS	Applicab	le Procedures List						
к.	A Ger	neric Ass	essment of Concrete Structural Components						

Sample Structural Walkdown Data Sheets

L.

# LIST OF TABLES

Number	Title	Page
3.1	Step la Review Results Summary Systems/Structures Which Contribute to Plant Safety	22
3.2	Step 1b Review Results Summary Systems/Structures for Which Degradation is Potentially Significant to Plant Safety	23
4.1	Electrical Component Groupings	43
4.2	Generic Structural Components	44

# LIST OF FIGURES

Number	Title				
2.1	Methodology to Evaluate Plant Equipment for License Renewal	5			
4.1	Safety Injection System	48			
4.2	Emergency Electrical Power System	49			

#### 1.0 INTRODUCTION

The purpose of this document is to provide the results of a pilot application of the Nuclear Management and Resources Council (NUMARC) Nuclear Plant Life Extension (NUPLEX) "Methodology to Evaluate Plant Equipment for License Renewal," (1) to Yankee Nuclear Power Station (YNPS) systems, structures, and selected components as part of the Yankee Lead Plant License Renewal Project. This project is co-sponsored by the U.S. Department of Energy, the Electric Power Research Institute, and Yankee Atomic Electric Company. The general objective of the project is to develop, document, and demonstrate the process of nuclear power plant license renewal and life extension for use by other utilities. Yankee's specific goal in conjunction with this objective is to obtain a 20-year renewal license.

YNPS is an 185 MWe, four-loop, Westinghouse-type pressurized water reactor located in Rowe, Massachusetts. YNPS began operating in 1960 and is the oldest operating commercial nuclear power plant. With almost 30 years of operation, YNPS ranks as one of the best operating nuclear power plants, achieving an average lifetime capacity factor of over 74%. The license to operate YNPS expires on July 9, 2000. This makes YNPS the first commercial nuclear power plant in the U.S. to require a license renewal for operation beyond the year 2000. Because of YNPS's long-standing record for operating safely and reliably, a license renewal evaluation is being made to support plant operation beyond the expiration of the current license. A 20-year license renewal period has been selected.

The first step in a license renewal evaluation is to determine the systems, structures, and components susceptible to significant age-related degradation. These systems, structures, and components are further evaluated to determine if they can be safely operated throughout the license renewal period. A component can be considered suitable for use during the renewal period if its failure would not compromise plant safety; or if it is not subject to significant age-related degradation; or if it is subject to

<sup>(1) &</sup>quot;Methodology to Evaluate Plant Equipment for License Renewal," Nuclear Management and Resources Council, Inc., U.S. Department of Energy/ Sandia National Laboratories, October 6, 1989.

periodic maintenance, refurbishment, or replacement which effectively manages age-related degradation.

The methodology used to determine which systems, structures, and components are susceptible to significant age-related degradation is based on the 'Methodology to Evaluate Plant Equipment for License Renewal," developed under NUMARC NUPLEX sponsorship. A report describing this plant evaluation methodology was forwarded to the NRC in October 1989. The philosophy underlying this methodology initially considers all plant systems, structures, and components as significant and susceptible to age-related degradation. Then, through a series of successive reviews, the number of plant systems, structures, and components requiring further review is reduced. First, on the system/structural level, the initial list of plant systems and structures is reduced to those systems or structures for which degradation is determined potentially significant. Then, on the component level, further review reduces the list of components to those components necessary for the performance of a significant system's or structure's safety function and which have identified aging degradation mechanisms that are not being adequately managed. Such components require further evaluation for operation during the license renewal period.

The remainder of this report is divided into five sections. Section 2 presents a brief overview of the NUMARC NUPLEX methodology. Section 3 discusses the application of the methodology to Yankee plant systems, structures, and components. Each plant system and structure is evaluated for significance and results are presented. This is followed by a discussion of Yankee-specific component evaluation methods. Section 4, "Pilot Application" details the application of the component evaluation methods to components associated with the Safety Injection (SI) System: SI fluid and I&C components, selected Emergency Electrical Power System (EEPS) components, Primary Auxiliary Building (PAB), Diesel Generator Building (DGB), and Battery Room No. 3 Building (B3B) structural components. These components are systematically reviewed for significance, for the ability of existing plant programs to ensure significant component safety functions are properly addressed, and for component susceptibility to age-related degradation. Component evaluation results for each of these components' types are presented. Section 5 presents the overall conclusions.

#### 2.0 METHODOLOGY

The NUMARC NUPLEX "Methodology to Evaluate Plant Equipment for License Renewal" and associated criteria for evaluating systems, structures, and components form the basis for this report. The methodology provides both deterministic and probabilistic approaches to identifying plant systems and structures which contribute to plant safety and, of those, identifying systems and structures for which aging degradation is potentially significant to plant safety. These systems and structures are established as the primary focus of further evaluation. From this list of systems and structures, the methodology describes how to: (1) identify the subset of components that are important to a system's or structure's safety function; (2) identify those components which currently are subject to established effective replacement, refurbishment, or inspection programs; (3) review those remaining components to determine the impacts, if any, I potential age-related degradation. For those components where age-related degradation is a concern, options for resolving such degradation are identified.

The NUMARC NUPLEX methodology consists of two major steps with a series of substeps that progressively focuses the license renewal evaluation. Figure 2.1 summarizes the methodology while Attachment A lists the generic criteria developed by NUMARC NUPLEX as provided in Appendix A to the "Methodology to Evaluate Equipment for License Renewal" report.

Step 1, "Evaluation of All Plant Systems and Structures," reviews all plant systems and structures to determine those that require component-level license renewal evaluation. First, Substep la develops a list of systems and structures potentially requiring further license renewal evaluation based upon the system or structure having a role, whether major or minor, in plant safety. Second, Substep 1b determines if degradation of the systems and structures identified in Substep 1a could potentially affect plant safety. Such systems and structures require component-level evaluation for license renewal. The net result, after Substeps 1a and 1b are completed, is the development of a list of systems and structures requiring further component-level evaluation for license renewal.

Step 2, "Evaluation of Components Within Systems and Structures," addresses plant systems and structures that have been determined by Step 1 to require component-level evaluation for license renewal. Each such system and structure is reviewed: Substep 2a identifies components that are important to performance of the system's or structure's safety function; of these, Substep 2b identifies components that are not routinely replaced, refurbished, or subject to detailed inspection; Substep 2c determines if these remaining components are susceptible to age-related degradation which may significantly affect plant safety; and Substep 2d suggests options which can be used to address potentially significant age-related degradation.

Application of this methodology results in a systematic evaluation of all plant systems, structures, and components. The detail of the review increases while progressing through the successive steps. At each step, some equipment not requiring further detailed evaluation may be identified.

A plant-specific application of the NUMARC NUPLEX methodology and associated criteria is presented in Section 3, which follows.

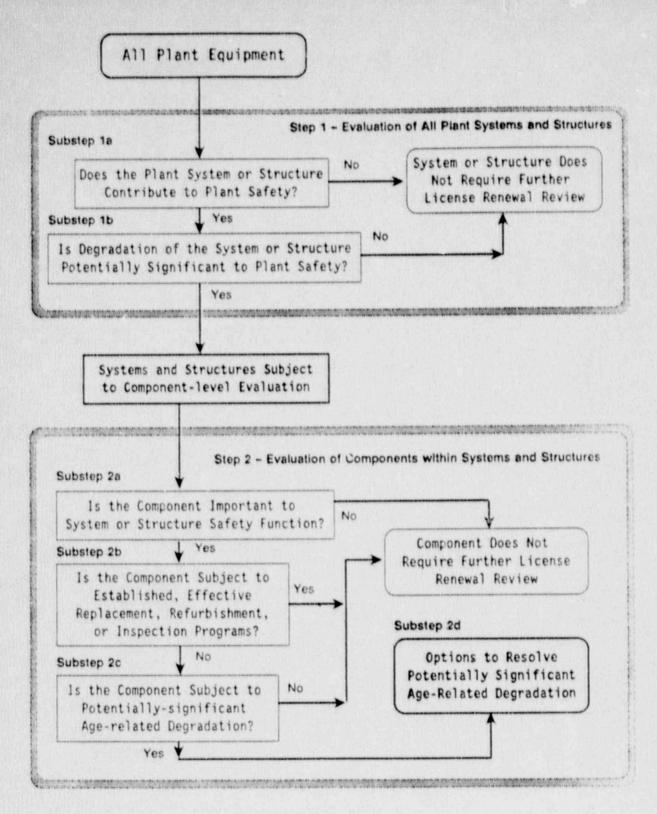


FIGURE 2.1

Methodology to Evaluate Plant Equipment for License Renewal

#### 3.0 EVALUATION OF PLANT SYSTEMS/STRUCTURES/COMPONENTS

All plant systems and structures are first identified. Then, using the NUMARC NUPLEX methodology deterministic criteria, these systems and structures are evaluated to (1) determine if each contributes to plant safety, and (2) of those, determine if their degradation is potentially significant to plant safety and, therefore, require further component-level evaluation.

The systems and structures are initially evaluated using plant-specific criteria to determine if they contribute to plant safety (Figure 2.1, Substep la). These criteria are based upon safety classification, licensing commitments, and role in plant Emergency Operating Procedures (EOPs). The systems and structures, which were determined to contribute to plant safety, are then further evaluated to determine if their degradation is potentially significant to plant safety (Figure 2.1, Substep lb). Again, plant-specific criteria based on radioactive release limits, Main Coolant System or containment leakage limits, and performance or control of plant safety functions are used.

If a system or structure met the requirements of the first set of criteria (Substep 1a), it is passed to the second set for evaluation. If the system or structure meets the second set of criteria (Substep 1b), which is presented in an exclusionary format, it is dispositioned as not requiring further review for license renewal. However, if the system or structure fails the second set of criteria, further component-level evaluation (Step 2) is required.

#### 3.1 Identification of Systems and Structures

A comprehensive list of all plant systems and structures is provided in Attachment B. This list represents the results of a detailed review of plant documentation to ensure that every plant system and structure has been identified an subjected to the plant evaluation process. Plant documents reviewed included the following: FSAR, Systems Training Manual, Appendix R Manual, Fire Hazards Summary Report, flow diagrams and other plant drawings, I&C instrument tag list, and the plant component labeling procedure. A brief description of each system and structure is also provided in Attachment B.

#### 3.2 System and Structural Boundaries

System and structural boundaries are established for evaluation purposes. The boundaries provide a clear demarcation between systems and structures to ensure components are placed into systems or structures in a consistent manner.

Systems are generally defined by plant drawings: electrical one-lines, flow diagrams, etc. Specific boundaries are established, and plant tagging practices are used to establish system components. For license renewal review purposes, system components are categorized into fluid, electrical, and instrument and central systems. Boundary definitions, associated with each category, are used to define the appropriate system for each category.

Structures are defined as any plant building or structure from the soil/structure interface to its external walls and roof, including concrete, structural steel, unit masonry, fire penetration barriers, and cast-in-place equipment anchorages. Lifting equipment, field-fabricated tanks, and supports are also included within the structure review scope. The boundaries are established to ensure that all components are included within either a system or structure.

#### 3.3 Identification of Systems and Structures Which Contribute to Plant Safety

The initial evaluation of systems and structures is to determine if they contribute to plant safety (Figure 2.1, Substep 1a). The evaluation is based on plant-specific criteria developed from Substep 1a of the NUMARC NUPLEX methodology. These criteria are discussed below:

#### 3.3.1 Safety-Related Systems and Structures

The Yankee Safety Classification of Systems Manual was reviewed to identify safety-related systems or structures. If any system or structure contains a component within the Safety Class (SC) boundary designated SC-1, SC-2, SC-3, SC or Requires Quality Assurance (RQA), the system or structure is identified for license remewal review.

# 3.3.2 Systems Relied Upon or Structures Identified in a Licensing Basis Safety Analysis or Evaluation

Those systems relied upon or structures identified in a licensing basis safety analysis or evaluation are determined from a review of current licensing basis-related documentation. This documentation falls into two categories: controlled documents and submittals addressing regulatory issues. The following five controlled documents were reviewed: FSAR, Technical Specifications, Environmental Qualification (EQ) Manual, Appendix R Manual, and the Fire Hazards Summary Report. Submittals addressing the following nine regulatory issues were also reviewed: seismic, heavy loads, internal and external flooding, rain/snow loads, tornado/wind loads, high energy line breaks, permanent radiation shielding, and station blackout. These controlled documents and submittals were chosen as being representative of the plant's current licensing basis and encompassing the results of a wide spectrum of safety analyses and evaluations. It should not be inferred that these documents and submittals alone represent the plant's entire current licensing basis. Rather, they collectively represent a significant portion of the plant's current licensing basis to ensure the identification of any system or structure which may have a role in plant safety. Details of this review of current licensing basis documentation to identify systems relied upon or structures identified in a licensing basis safety analysis or evaluation are given below:

#### 3.3.2.1 Final Safety Analysis Report (FSAR) Transient/Accident Analysis

The FSAR transient/accident analysis sections were reviewed to identify every system which is intended to mitigate or negate a transient/accident or any system whose failure or misoperation produces an undesirable affect.

### 3.3.2.2 Technical Specifications

The Technical Specifications were reviewed to identify any systems or structures governed by one or more Technical Specification. If a single component of a system or structure was identified in the Technical Specifications, the system or structure was included.

#### 3.3.2.3 Environmental Qualification (EQ)

The EQ Manual was reviewed to identify systems where one or more of its components required evaluation. The system was included if it contains components which were evaluated for either harsh or mild environments.

#### 3.3.2.4 Appendix R

The Appendix R Manual was reviewed to identify systems and structures governed by this program. Any system or structure with components relied on to achieve an orderly plant shutdown following a fire as part of the Appendix R evaluation was included.

#### 3.3.2.5 Fire Protection

The Fire Hazards Summary Report was reviewed to identify any system or structure with one or more components governed by a fire protection requirement.

#### 3.3.2.6 Seismic

The seismic NRC Safety Evaluation Report and related correspondence were reviewed to identify any system or structure with one or more seismic components.

### 3.3.2.7 Heavy Loads

The heavy loads correspondence were reviewed to identify plant hoists and lifting equipment evaluated under the topic.

#### 3.3.2.8 Internal Flooding

The internal flooding correspondence were reviewed to identify the plant systems identified as sources of internal flooding or features which mitigate the effects.

#### 3.3.2.9 External Flooding

The external flooding correspondence were reviewed to identify the systems and structures used to mitigate the consequences of external flooding.

#### 3.3.2.10 Rain/Snow

The rain/snow correspondence were reviewed to identify the structures evaluated for rain and snow loads.

#### 3.3.2.11 Tornado/Wind

The tornado/wind correspondence were reviewed to identify systems and structures used to mitigate the effects of tornadoes and high winds.

#### 3.3.2.12 High Energy Line Breaks (HELB)

The HELB correspondence were reviewed to identify systems and structures evaluated as a HELB source or which mitigate the effects.

#### 3.3.2.13 Permanent Radiation Shielding

The FSAR and other documents were reviewed to identify systems and structures used for permanent radiation shielding.

#### 3.3.2.14 Station Blackout

The station blackout submittal were reviewed to identify any system used to cope with a station blackout.

#### 3.3.3 Systems Utilized in Plant EOPs

The plant Emergency Operating Procedures (EOPs) were reviewed to identify systems used by the operator in dealing with plant transients and accidents. The Yankee plant EOPs are based upon the Westinghouse Owners Group Emergency Procedure Guidelines. Systems whose use is explicitly or implicitly called for in the plant EOPs are identified.

# 3.3.4 Results - Listing of Systems and Structures Which Contribute to Plant Safety

The results of the evaluation to identify plant systems and structures which contribute to plant safety are provided in Attachment C. Documented in Attachment C are the individual responses for each system and structure for the criteria discussed in Sections 3.3.1, 3.3.2, and 3.3.3. Table 3.1 summarizes these results. These first level review (i.e., Substep la) results show that 63 out of 78 systems and 33 of 46 structures were identified as being contributors to plant safety. As such, these 63 systems and 33 structures pass on to Substep lb for further evaluation.

# 3.4 Identification of Systems and Structures for Which Degradation is Potentially Significant to Plant Safety

A detailed evaluation of the systems and structures which contribute to plant safety is made to determine the potential significance of age-related degradation to plant safety (Figure 2.1, Substep 1b). Age-related degradation of a system or structure is considered potentially significant to plant safety if the failure of the system or structure contributes to increased radiological health and safety risk to the public.

This second-level evaluation is based on criteria associated with exceeding radioactivity release limits, main coolant system or containment leakage limits, and performing or controlling plant safety functions. These criteria represent a plant-specific application of Substep 1b of the NUMARC NUPLEX methodology. Specific details of these criteria are discussed below.

#### 3.4.1 Uncontrolled Radioactive Release

Criterion 1b.1.a of the NUMARC NUPLEX methodology requires that a system or structure be evaluated further if its failure could directly result in a radioactivity release exceeding FSAR or other off-site dose limits. In order to implement this criterion, the Yankee Technical Specification limit for radiological effluent release to the environment was selected as the threshold with the following ground rules: (1) the system/structure in

question was assumed to be operating at the allowable Technical Specification radioactivity limit, (2) the system or structural related failure causes a release of its radioactive contents, (3) no other accident or transient is in progress. If Technical Specification radioactive release limits could be exceeded upon system or structure failure, then the system or structure requires component-level evaluation (Step 2). Examples of systems and structures which could potentially cause Technical Specification radioactive release limits to be exceeded are the Main Coolant System, Radioactive Waste Disposal System, Primary Auxiliary Building, and Waste Disposal Building.

#### 3.4.2 Main Coolant System or Containment Leakage

Any system or structure which could cause degradation and failure of either the Main Coolant System or Vapor Container (containment) pressure boundary is considered potentially significant to plant safety (NUMARC NUPLEX Criterion 1b.1.b). Main Coolant System and Vapor Container Technical Specification leakage limits are established as thresholds for YNPS. In application, the potential to exceed the 1 gpm Main Coolant System leakage limit and the potential to breech the containment boundary was assessed for each system and structure contributing to plant safety. Of these, those systems and structures which could cause these limits to be exceeded require component-level review. The Main Coolant System and Vapor Container are obvious examples of a system or a structure which meets this criterion. Other examples of systems meeting this criterion are the Charging and Volume Control System, and the Component Cooling Water System which are included on the basis of their Main Coolant System and Vapor Container penetrations. Other structural examples are the Primary and Secondary Vent Stacks, which, upon failure, could potentially impact upon the Vapor Container.

#### 3.4.3 Performance or Control of Plant Safety Functions

The NUMARC NUPLEX methodology, in Criterion 1b.1.c.1, specifies a generic set of plant safety functions. These are:

- 1. Reactor Criticality
- 2. Main Coolant System Integrity
- 3. Main Coolant System Inventory
- 4. Main Coolant System Heat Removal
- 5. Containment Integrity
- 6. Containment Heat Removal

Any system or structure which is required for the performance of or control of these safety functions require component-level evaluation unless its failure is detectable in a time frame which precludes manual or automatic plant trip (Criterion 1b.1.c.2). For application to YNPS, the safety functions used in the plant EOP status trees, which encompass the above safety functions, are substituted:

- 1. Subcriticality (S)
- 2. Core Cooling (C)
- 3. Heat Sink (H)
- 4. Integrity (P)
- 5. Containment (V)
- 6. Inventory (I)

The status of the plant safety functions have been categorized to define the level of challenge to a particular safety function. Any system which fails to operate or maintain its integrity and causes a safety function to deviate from its normal status or degrade to a less desirable state, or any system required to monitor the status of a safety function and whose failure results in the inability to determine the status of that safety function requires component level review. The degradation of such systems is considered potentially significant to plant safety. Examples of systems which can cause one or more safety functions to deviate from normal or degrade to a less desirable state are the Charging and Volume Control System, the Safety Injection System, and the Boiler Feed System. The Charging and Volume Control System and the Safety Injection System can both affect the subcriticality, core cooling, integrity, and inventory safety functions through their ability to add cold, borated water to the Main Coolant System. The Boiler Feed System

directly affects the heat sink safety function (through steam generator feedwater addition) and, to a Jesser extent, the integrity and inventory safety functions (through overcooling due to excess feedwater addition).

If the system's failure could result in a safety function status change but the failure is detectable in a time frame which allows for plant shutdown prior to requiring a manual or automatic plant trip, the system can be excluded from the list of systems for which degradation is considered significant to plant safety. Only two examples of such systems were identified in our review. These are the Heating Steam/Condensate System and the Non-Return Valve (NRV) Enclosure Ventilation System. The first system is used to maintain the 125,000 gallon SI tank temperature between 120°F and 130°F, as required by Technical Specifications. The latter system is required to maintain the NRV enclosure temperature above freezing to ensure proper operation of NRV hydraulics. In either case, sufficient time is available to detect failure in these systems to allow credit for corrective action.

#### 3.4.4 Structures Housing Significant Systems

In lieu of applying the plant safety function related criteria (Criteria 1b.1.c.1 and 1b.1.c.2) directly to structures, a separate criterion was established. Structures which housed significant systems, as identified by Criteria in 1.b.1.a, 1.b.1.b, and 1.b.1.c were designated as potentially significant to plant safety and as requiring component level review. This was done to avoid correlating a structure with a particular safety function or set of safety functions.

# 3.4.5 Results - Listing of Systems and Structures for Which Degradation is Potentially Significant to Plant Safety

The results of the evaluations discussed in Sections 3.4.1 though 3.4.4 are documented in Attachment D for each system and structure identified as a contributor to safety. Degradation of a system or structure is designated potentially significant if any of the above evaluation categories are applicable. Table 3.2 summarizes the results given in Attachment D. Of the 63 systems designated as contributors to plant safety, degradation of 43 are

considered significant. Of the 33 structures designated as contributors to plant safety, degradation of 27 are considered potentially significant to plant safety. These systems and structures are subject to further component-level (Step 2) review for license renewal.

It is recognized that other balance of plant systems warrant further review, beyond the scope of license renewal, based on potential transient initiation, personnel safety, or economic considerations. These areas are being reviewed for potential age-related degradation concerns as part of Yankee's overall plant life extension effort. Industry and plant-specific risk studies are being used to focus the review.

For example, the following system and component reviews have been completed or are in progress:

- o Station Transformers
- o Main Condenser
- o Water Treatment System
- o Turbine Generator
- o Feedwater Heaters

#### 3.5 Component Evaluation

The next step in the methodology is the evaluation of the components within the systems and structures which were designated potentially significant to plant safety in Section 3.4. This component-level evaluation involves several steps. First, all components within the system or structure are identified. For each of these components, subsequent steps address the following questions:

- o Is the component important to system or structure safety function?
- o Is the component subject to established effective replacement, refurbishment, or inspection programs?

o Is the component subject to potentially significant age-related degradation?

Components that are important to the system or structure safety function and are not subject to established effective replacement, refurbishment, or inspection programs, and are subject to potentially significant age-related degradation, require further evaluation for license renewal. These evaluations, which will be component-specific, are beyond the scope of this report.

Plant-specific criteria, based on the NUMARC NUPLEX methodology, address the above questions for each component in each of the systems and structures requiring component level evaluation. These criteria are discussed in subsequent sections below.

## 3.5.1 Components Important to System or Structure Safety Function

Components are designated important to the system or structure safety function unless:

o The component is normally isolated and does not perform an accident mitigating function.

OR

o Component failure would not result in either the failure of any individual train within the system or the failure of the entire system to perform its required safety function,

AND

o Component failure would not reduce the structural support of any other component such that it would not perform its system safety function,

AND

o Component failure would not physically damage any other component such that it would not perform its system safety function.

Components meeting the above criteria are not important to the system's or structure's safety function. Components failing the above criteria are important to the system's or structure's safety function and require further evaluation as described in Section 3.5.2.

# 3.5.2 Components Subject to an Established, Effective, Replacement, Refurbishment, or Inspection Program

Components important to the system or structure safety function that are subject to an established effective replacement, refurbishment, or inspection program are identified using the generic criteria given in Step 2b of the NUMARC NUPLEX methodology. Restating the criteria, a component is subject to an established effective replacement, or inspection program, if:

- o The program is documented, approved, and routinely implemented in accordance with plant administrative procedures.
- o The program procedures ensure that all of the component's significant safety functions are properly addressed.
- o The program establishes specific criteria for determining the need for corrective action and requires such action be taken if these criteria are not met.

A review of plant procedures, based on the above criteria, is used to assess the effectiveness of maintenance/surveillance/inspection activities covering the components being evaluated. Applicable procedures, inspection methods used, inspection frequency, replacement frequency, and refurbishment frequency called for by the procedures for each component are entered into a data base.

Components designated important to the system or structure safety function which are not covered by procedures are subject to further evaluation

in Section 3.5.3. Components which are covered by procedures are further reviewed as described below.

The specific safety-significant functions are established for each component (or groups of similar components) designated important to the system or structure safety function in Section 3.5.1 above. Examples of component significant safety functions are pressure boundary, operability, etc. The safety-significant functions may be component-specific or have generic applicability.

Using the results of the plant procedures review and/or other supporting information, the ability of the component's program(s) to properly address the safety significant functional requirements identified above is determined. If the component's safety significant functional requirements are properly addressed by existing programs, no further review is required. If not, further evaluation, as described in Section 3.5.3, is required.

Generally, components are subject to the actions contained in several procedures, many of which address more than one component. All procedures associated with a component are reviewed to determine overall effectiveness. It is the extent to which a component's applicable procedure set ensures its safety functions are adequately maintained that determines whether or not the component is subject to an "effective" overall program. Procedures may only partially address the component's identified safety functions (i.e., procedures may adequately address some, but not all, safety functions). Additionally, certain "effective" programs, such as the EQ Program or a defined, periodic replacement program, have been designed to ensure component's continued operability. Components under such programs do not require any further evaluation for license renewal because the basis for such effective programs (e.g., EQ) is mandated by the plant's existing license.

Components with all identified significant safety functions (pressure boundary, operability, etc.) covered by an effective program do not require further evaluation. Conversely, components for which any significant safety function is not adequately maintained by an effective program requires further evaluation as described in Section 3.5.3.

Where a determination was made that further license renewal evaluation of a component is not required based on effective programs, the programs credited will be further reviewed as a separate task to assure the validity of the determination. This will involve a detailed review of the program's attributes relative to the cafety functions and specific degradation mechanisms involved.

The effective program conclusion is a judgement of that programs ability of assuring continued functionality of the component during license renewal considering the effects of potential degradation. A negative conclusion does not necessarily infer the inadequacy of current programs, nor does a positive conclusion preclude the necessity for program enhancements.

## 3.5.3 Components Subject to Potentially Significant Age-Related Degradation

Those components that are important to the system's or structure's safety function and are not subject to an effective replacement/refurbishment/inspection (RRI) program are now evaluated to determine if they are subject to potentially significant age-related degradation.

A component is considered subject to age-related degradation unless it is established and documented that potentially significant age-related degradation will not occur during the license renewal period.

The potential for significant age-related degradation occurring is assessed for each component that has been identified as necessary to the system safety function and not subject to an effective RRI Program. Such components are evaluated for age-related degradation mechanisms according to their respective discipline area as follows:

Fluid Systems - Fluid system components are evaluated using a computer based expert system, developed by Yankee, called CoDAT. CoDAT is used to determine the degradation mechanisms which are potentially acting on pressure retraining components based on materials and environmental conditions. Further information on CoDAT is provided in Attachment G. Active fluid components (pumps, motor-operated valves, etc.) are also

evaluated separately for active degradation mechanisms (wear, galling, etc.) in addition to being evaluated for passive degradation mechanisms using CoDAT.

Instrumentation and Control (I&C) Systems - I&C components are reviewed for the following:

- o Deterioration Shown by General Changes in Electrical Characteristics
- o Corresion
- o Mechanical Wear
- o Radiation Damage

Electrical Systems - Electrical components are reviewed for the following:

- o Dielectric Breakdown
- o Mechanical Wear
- o Corrosion
- o Radiation Damage

Structural Components - Structural components are evaluated for potentially significant degradation using generic degradation assessments and a focused plant walkdown. Generic degradation assessments are performed for concrete, steel, building protective systems, and equipment support components. The assessments determine the plausible age-related degradation modes, the stressors, and environment required for the degradation mode to be active and how the degradation is manifested. Plant design and construction features are considered to determine the structural components potentially susceptible to age-related degradation. A focused walkdown is then performed to assess actual material conditions and environments to identify which structural components require further evaluation for license renewal.

Only components with identified potentially significant age-related degradation mechanisms require further evaluation for license renewal. The scope of these component evaluations can range from a simple examination to a detailed analysis, depending upon the component and degradation mechanism involved. Component repair, refurbishment, or replacement will be considered, when applicable. These evaluations are beyond the scope of this report.

The discussion presented in Sections 3.5.1, 3.5.2, and 3.5.3 gave an overview of the plant-specific application of the generic plant evaluation methodology for components. Section 4.0, which follows, focuses this overview on a pilot application which consists of an evaluation of SI related system and structural components. This pilot application is intended to demonstrate the use of the methodology and criteria for components within each plant area. The method of implementation, technical bases, and results are provided.

TABLE 3.1

Step la Review Results Summary
Systems/Structures Which Contribute to Plant Safety

		Results					
	Total	Safety Class (Yes/No)	Licensing Basis (Yes/No)	Used in EOPs (Yes/No)	Contributes to Plant Safety (Yes/No)		
Systems	78	40/38	61/17	45/33	63/15		
Structures	46	4/42	33/13	N/A	33/13		

### TABLE 3.2

# Step 1b Review Results Summary Systems/Structures for Which Degradation is Potentially Significant to Plant Safety

	Total	Rad Release Limits Exceeded (Yes/No)	MCS or Containment Leakage Exceeded (Yes/No)	Req'd for Perf. of or Control of Safety Functions (Yes/No)	Failure Not Detectable (Yes/No)	Structure Houses Significant System (Yes/No)	Degradation of System/Structure Potentially Significant to Plant Safety (Yes/No)
Systems	63	15/48	18/45	36/27	36/2	N/A	43/20
Structures	33	11/22	8/25	N/A	N/A	23/10	27/6

#### 4.0 PILOT APPLICATION

#### 4.1 Purpose and Scope

The purpose of the pilot study is to demonstrate the application of the component-level plant evaluation methodology for a wide spectrum of plant components representing the four major plant discipline areas: fluid systems, electrical, I&C, and structural. The SI System, which was determined to require component-level evaluation in Section 3.4, is the focal point.

The component evaluation includes all SI fluid system and SI I&C components; selected EEPS components; and PAB, DGB, and B3B structural components. The electrical and structural components included herein are related to the SI System and are provided as a demonstration of the evaluation process. However, it was not intended that all SI-related components be addressed in this report.

The EEPS provides the SI System electrical loads with ac power. The PAB, DGB, and B3B house most of the major SI and EEPS components: high and low head SI pumps, accumulator tank, diesel generators, etc.

For each discipline area, the methods by which components are identified and evaluated are presented along with a summary of the results. Although the component-level plant evaluation methodology provides criteria generically applicable to all components, the implementation of the methodology will differ somewhat for each discipline area. This is necessary to take full advantage of particular surveillance and aging aspects associated with each group of components. For example, I&C components are most likely dispositioned on the basis of plant procedures while structural components are better dispositioned on the basis of generic assessments and plant walkdowns. Fluid system and electrical system comments will most likely be dispositioned on the basis of plant procedures and/or aging-degradation assessments.

Finally, a discussion of the use of generic evaluations for groups of similar plant components is presented. In some instances, it may be advantageous to group components for evaluation rather than treat them

individually by system. This grouping may either be by component type or it could be by issue. For example, thermal fatigue is best addressed globally as an issue and then applied to individual components.

#### 4.2 Safety Injection System Fluid Components

#### 4.2.1 Identification of SI Fluid Components

A simplified flow diagram of the SI System is shown in Figure 4.1.

Attached to this report is a detailed SI System flow diagram, (FM-83A - "Flow Diagram - Low Pressure and High Pressure Safety Injection,") which was used in developing the SI System fluid component list and identifying SI Fluid System boundaries. Each individual component on the flow diagram is identified by tag number, description of component, line number, and other specific information depending upon whether it is a pipe, valve, instrument, pump, motor, or other component. Three-hundred ninety-two (392) fluid system components were identified and are listed in Attachment E along with component-level review results.

The above process for identifying fluid system components within the SI system is typical of that used for the remaining fluid systems requiring component level review.

#### 4.2.2 Safety Function Review

Each SI fluid component is reviewed using plant-specific criteria based on the NUMARC NUPLEX methodology to determine if the component is important to the system safety function. For Yankee fluid components, the criteria discussed in Section 3.5.1 are augmented by an additional set of criteria which essentially are an interpretation for fluid system components. If any of the following questions can be answered "yes" (assuming that no credit will be taken for other systems which can perform the same safety function(s)), then the component cannot be dispositioned on a functional basis and further evaluation in Section 4.2.4 is required:

- o Can the component's failure prevent subcriticality from being achieved following a scram?
- o Can the component's failure prevent adequate core cooling?
- o Can the component's failure affect the heat sink capabilities?
- o Can the component's failure cause a loss of integrity of the system pressure boundary?
- o Can the component's failure cause a loss of containment integrity?
- o Can the component's failure affect reactor coolant inventory control?

Of the 392 fluid components identified, only 15 were dispositioned in Step 2a as not being important to the SI System safety function. This rather small number of components being dispositioned reflects the importance of the SI System and the conservatism inherent to the criteria being applied.

### 4.2.3 Effective Program Review

The remaining 377 SI fluid components were then evaluated to determine which are subject to an established, effective replacement, refurbishment, or inspection program. The approach outlined in Section 3.5.2 is used. Fifty-three (53) procedures were identified which deal with SI components to varying degrees. These procedures are listed in Attachment F. The two SI safety system functions that these procedures must address are the pressure boundary function (i.e., integrity of the SI System fluid pressure boundary) and the operability function (i.e., flow path, flow capacity, operability, etc.). Highlights of the effective program review are:

- The high and low pressure safety injection pumps undergo frequent functional testing to demonstrate operability and to detect signs of mechanical wear. Included in the testing are checks/measurements of motor amps, pump vibration, bearing temperatures, proper lubrication, packing and seal leakage, pump performance, and SI System leakage.

- Check valves in the plant were evaluated based on maintenance history and operational requirements. A comprehensive program is currently being implemented to address valves of concern in response to INFO SOER 86-3. This program calls for periodic disassembly and inspection. In addition, SI System check valves are periodically tested for operability during system functional tests.
- Manual valves are routinely checked for external leakage by monitoring for signs of boric acid crystals. This will preclude significant degradation of support steel or adjacent components.
- A commitment to perform motor-operated valve testing using "MOVATS" on critical motor-operated valves will provide additional assurance that the motor-operated valve operability function is maintained.

All pressure boundary function components were conservatively given a degradation review. A review of the 53 procedures for operability function determined that the operability function for 58 of the 70 active components was adequately addressed by these procedures. However, because these 58 components also form part of the SI pressure boundary they require further evaluation. Thus, none of the 377 SI fluid components were dispositioned at this point. As such, all 377 SI fluid components pass on to Section 4.2.4 for further evaluation of potential pressure boundary degradation.

#### 4.2.4 Aging-Degradation Review

The age-related degradation review determines the potential aging degradation mechanisms for a component. To determine the potential degradation mechanisms which may be acting on a specific fluid component, the operating conditions and component materials are compared against the degradation mechanism controlling parameters and their acceptance criteria. A

review of industry documents was performed to identify the specific mechanisms applicable to the Yankee fluid systems. A rule-based computer expert system, CoDAT (Component Degradation Assessment Tool), developed by Yankee, is used to review fluid system pressure boundary components for 20 degradation mechanisms organized into 14 groups. Fatigue is not covered by CoDAT but will be evaluated separately. In some cases, component parts are evaluated; i.e., valve stems and discs. A more detailed discussion of CoDAT and the degradation mechanisms that it addresses is given in Attachment G.

Based on the SI System's materials of construction and infrequent operation, significant degradation would not be expected. The results of the review identified only six components of the remaining 377 components as potentially subject to age-related degradation. The potentially significant degradation mechanisms identified by CoDAT are:

- The SI tank is constructed of aluminum which is susceptible to general corrosion if the fluid pH is less than five or greater than nine.
- Buried piping may experience crevice/pitting and Microbiological Influenced Corrosion (MIC).
- The carbon steel shell material of the SI accumulator may be susceptible to general corrosion if not properly coated.

Potential degradation associated with fluid component operational function are not covered by CoDAT but are evaluated separately. They include general wear and mechanical degradation of pumps and motor-operated valves and degradation specific to pump motors and valve operators.

This separate evaluation identified an additional 12 components as requiring further evaluation (based on operability function), bringing the total to 18 components.

#### 4.2.5 Summary - SI Fluid Component Review

SI System fluid components are subject to three reviews: importance to system safety function, effective programs, and age-related degradation with results provided in Attachment E. Of the 392 components of the SI System, 18 will require further evaluation to assure reliability of function during the license renewal period.

#### 4.3 SI System I&C Components

Instrumentation and Controls (I&C) associated with the SI System fall within generic I&C equipment groupings, which include, but are not limited to, the following component groups:

- o Process controllers, transmitters, sensors, switches, gauges
- o Control switches
- o Indicators and recorders
- o Electronic instrumentation

The SI I&C components for which evaluations have been completed are discussed in this section to demonstrate the general process involved with the evaluation of I&C equipment.

#### 4.3.1 Identification of I&C Components

The I&C components associated with the SI System are listed in Attachment H. One hundred sixty-eight (168) SI I&C components have been identified.

#### 4.3.2 Safety Function Review

Each component is reviewed to determine if it is significant to system safety function using the NUMARC NUPLEX criteria, as applicable.

Instrumentation required for the following plant-specific requirements are considered significant to system safety function:

- o Regulatory Guide 1.97 (post-accident monitoring)
- o Technical Specifications
- o Safety Class Manual
- o EQ Program
- o Appendix R
- o Safe Shutdown System Instrumentation

Of the 168 SI I&C components, 97 components were determined significant to system safety function. These components are further evaluated to determine if they are subject to an effective program.

An example of SI I&C components identified as significant to the system safety function are the SI hot leg and cold leg flow transmitters, SI-FT-5 and SI-FT-6. These instruments are required for post-accident monitoring because they are relied upon in the EOPs to ensure that proper SI flow rates are established during the recirculation phase and the hot leg injection phase of a large break LOCA. An example of SI I&C components determined not to be significant to system operation are SI loop pressure transmitters and indicators, SI-PT-1 through SI-PT-4 and SI-PI-1 through SI-PI-4. These instruments provide ancillary information only and are not required for post-accident monitoring.

#### 4.3.3 Effective Program Review

Each of the significant SI I&C components evaluated is first reviewed to determine if it is included in the Yankee EQ Program. Four (4) SI I&C components are governed by the Yankee EQ Program. These components are considered subject to an effective program and do not require further evaluation.

The remaining significant 93 I&C components evaluated are further reviewed to determine if they are otherwise subject to an effective program. Specific functional requirements for SI I&C components differ according to application. However, the prime function required of instrumentation and control equipment is operability. In general, SI I&C components have verifiable attributes tied to distinct tolerances for operability. These

tolerances are identified in test and calibration procedures. In addition to the criteria given in Section 3.5.2, the attributes of an effective program to assure continued I&C component operability, as applicable, include the following:

- o Cleaning
- o Checking for worn parts
- o Observation
- o Visual inspection
- o Measurement using calibrated test equipment
- o Multipoint calibration

Of the 93 significant SI I&C components not covered by EQ, 50 were determined to be covered by an effective program. Enhancements to existing programs are being considered to increase emphasis on the following:

- Assessment of component general condition and signs of abnormal operation.
- o Data collection for trending.

An example of SI I&C components subject to an effective program are the hot and cold leg flow transmitters, SI-FT-5 and SI-FT-6. These instruments are included in the EQ Program which is a formal program and was established to ensure component operability. Furthermore, the EQ Program identifies all replacements, refurbishments, and inspections required to maintain operability.

Similarly, SI actuation switches, SI-PS-0238 and SI-PS-0239, were also determined to be subject to an effective program because they are maintained in accordance with OP-4634. This procedure functionally checks and, if necessary, adjusts the trip and reset points. It is performed every 31 days.

#### 4.3.4 Aging-Degradation Review

Of the 97 significant SI I&C components evaluated, 43 have not been demonstrated as being subject to an effective program. These 43 SI I&C components may be subject to aging degradation and will be further evaluated.

#### 4.3.5 Summary - Safety Injection I&C Component Review

One-hundred twenty-five (125) of the 168 SI I&C components evaluated were found to not require further review for license renewal. Seventy-one (71) were dispositioned on the basis of unimportance and fifty-four (54) were dispositioned on the basis of being subject to an effective program.

Forty-three (43) SI I&C components will require further evaluation.

#### 4.4 Emergency Electrical Power System

The Emergency Electrical Power System (EEPS) consists of electrical equipment, cabling, busses, breakers, etc., necessary to supply electrical power to essential safeguard loads, including SI equipment, and Safe Shutdown System loads. The EEPS is one of the five electrical subsystems in the plant and is shown in Figure 4.2.

#### 4.4.1 Identification of Components

Identification of the electrical components in the EEPS is required prior to the initiation of component level screening. The objective of this identification process is to gather all electrical components into a data base which can then be used for evaluations. Electrical component identification is based upon a review of plant electrical drawings. Electrical one-lines, selected elementary drawings, and the plant's lighting and power panel manual were used to develop an electrical component data base. This data base includes both the loads (pump motors, valve operators, etc.) and the major electrical components (busses, breakers, etc.) required to deliver power to the loads.

evaluated on either an individual or generic basis. A total of 100 EEPS components are evaluated on an individual basis and are listed in Attachment I. Other EEPS components, such as cables, penetrations, relays, terminations, etc., as listed in Table 4.1, will be evaluated generically, along with other such plant equipment. The electrical equipment types subject to generic evaluation are indicated by an asterisk (\*) on Table 4.1. The corresponding generic evaluations will be documented in future reports.

#### 4.4.2 Safety Function Review

The function of the EEPS is to provide power to loads. Those EEPS components which are necessary to the system safety function are now identified. Such components require further review. Components are designated necessary to the EEPS safety function unless:

The component is normally isolated and does not perform an accident mitigating function.

OR

o Component failure would not result in either the failure of any individual train within the system or the failure of the entire system to perform its required safety function,

AND

O Component failure would not reduce the structural support of any other component such that it would not perform its system safety function.

AND

o Component failure would not physically damage any other component such that it would not perform its system safety function.

The results of this review are shown in Attachment I, Column 2A. Components failing the above criteria are important to the system's safety function and are designated by a "yes" in Column 2A. Components meeting the above criteria are not important to the system's safety function (designated by a "no" in Column 2A) and do not require further review for license renewal.

Components were identified as not necessary to the system safety function for the following reasons:

- o Loads not important to system safety function.
- o Component normally disabled.
- o Component used only for maintenance.
- o Components used only during refueling.

For example, Diesel Generator Building (DGB) Unit Ventilator UV-6 was determined not to require further evaluation because it supplies the normal ventilation to the DGB, but is not relied upon in the event of an accident. However, DGB Exhaust Fans SI-PRV-1 and SI-PRV-2 were determined to require further evaluation because they are relied upon to supply DGB ventilation in the event of an accident.

In total, twelve (12) out of the 100 EEPS components individually evaluated do not require further evaluation on the basis of this safety function review.

#### 4.4.3 Effective Program Review

Components necessary to the system safety function that are subject to an established effective replacement, refurbishment, or inspection program are now identified. For electrical components, this includes components covered either by the EQ Program or an effective plant program.

The EQ Program for electrical equipment is an ongoing NRC-required program which, among other things, considers significant types of degradation which can have an effect on the functional capability of equipment. For those components under the EQ Program, aging is effectively managed and further

review is not required. Those components are identified by a yes under "Step 2B, EQ" of Attachment I. For example, Manual Throwover Switches, SW-TO-1 and SW-TO-2, both provide capability to change the power supply of an emergency motor control center, and both were found to be necessary to the system safety function under Section 4.4.2. However, since SW-TO-2 is located in a potentially harsh environment and is under the EQ Program, it was determined as being covered under an effective program and not to require further evaluation. However, SW-TO-1, which is located in a mild environment, is not under the EQ Program and was determined to require further evaluation. In total, twenty-three (23) EEPS components do not require further evaluation on the basis of EQ.

In addition to the EQ Program, electrical components may also be subject to an effective replacement or inspection program. The plant procedures applicable to each component were identified in Attachment I under "Step 2B, Plant Procedures." The procedures are further identified in Attachment J. These procedures were reviewed to determine if they were effective. A component is subject to an established effective replacement or inspection program if the applicable procedures, either individually or collectively, meet the criteria given in Section 3.5.2.

Forty (40) EEPS components do not require further evaluation on the basis of being subject to an effective program. These components, along with those under the EQ program, are identified by a "no" under "Step 2B, Component Not Subject to an Effective RRI Program."

A number of components were identified as covered adequately by existing plant procedures. For example, important Motor-Operated Valves (MOVs) are covered because they are subject to periodic functional testing per procedures. If an MOV does not meet its functional requirements (e.g., stroke time), then the MOV must be refurbished (in accordance with a specific MOV repair procedure) so that, when retested, it will meet its functional requirements. To further assure MOV reliability, YNPS plans to implement a testing program in accordance with NRC Generic Letter 89-10 starting in 1990. A Diagnostic Testing System will be used to verify the capability of critical

plant MOVs to operate under design conditions. This testing program will include the development of a signature analysis for each MOV. Follow-up testing and trending will be performed as appropriate.

The LPSI and HPSI pump motors are given as another example. These are covered under the EQ Program which analyzes the aging and demonstrates that the motors will be operable for their identified life. In addition, they are functionally tested on a monthly basis.

The review of plant procedures indicated that critical components, in general, are functionally tested on a schedule adequate to demonstrate continued operability. Enhancements to existing programs are being considered to increase emphasis on the following:

- o The use of predictive maintenance.
- o Failure analysis.
- o Trending.

#### 4.4.4 Aging Degradation Review

A component is considered subject to age-related degradation unless it is established and documented that potentially significant age-related degradation will not occur during the license renewal period.

The potential for the occurrence of significant age-related degradation is assessed for each component that has been identified as necessary to the system safety function and not subject to an effective RRI Program. These components are now evaluated for the following age-related degradation mechanisms:

- o Dielectric breakdown.
- o Mechanical wear.
- o Corrosion.
- o Radiation damage.

The results of this review are shown in Attachment I, Step 2C. A yes is indicated under each degradation mechanism for which the component is potentially susceptible. All functionally important components not demonstrated as being subject to program are potentially susceptible to at least one of the aforementioned mechanisms. The rate of degradation due to the particular mechanism is determined by the environmental and service factors, which have yet to be defined. Therefore, no components could be eliminated from further evaluation. These components require further evaluation.

#### 4.4.5 Summary - EEPS Component Review

ELPS component review results are listed in Attachment I. Of the 100 components listed, 75 do not require further evaluation on the basis of either the safety function review (12) or the effective program review (63). The remaining 25 components were all determined susceptible to age-related degradation and require further evaluation. This evaluation is beyond the scope of this report.

## 4.5 Primary Auxiliary Building/Diesel Generator Building/Battery Room No. 3 Building Structural Review

A majority of the SI System-related components are located either within the PAB, the DGB, or Battery Room No. 3 Building (B3B). The low pressure SI pumps, the high head SI pumps, accumulator, numerous manual and motor-operated valves, and SI piping are located in the DGB. SI piping, manual valves, and motor-operated valves are located within the PAB. SI piping traverses the PAB enroute to the vapor container. Most EEPS components are located within the DGB and B3B. The emergency diesel generators, DG-1, DG-2, and DG-3; Emergency Buses 1, 2, and 3; Emergency Motor Control Center (EMCC)-2; Manual Throwover Switch No. 2; conduit; vertical Sections A and B; and cables are all located with the DGB. EMCC-3 and EMCC-4 are located in B3B. EEPS cables supply loads within the PAB or traverses the PAB. The following sections detail the highlights of the evaluations conducted for these structures.

#### 4.5.1 Identification of Components

Except for components with unique plant equipment identification tags (i.e., tanks) and the structures predesignated for detailed evaluations (i.e., vapor container, reactor support structure, neutron shield tank/reactor support ring, and fire-rated seals), structural components are evaluated generically. Table 4.2 lists the generic structural components for the Yankee plant.

#### 4.5.2 Safety Function Review

Four generic categories of structural components which require evaluation were defined: concrete, structural steel, architectural items, and supports for plant equipment. Table 4.2 lists the generic structural components considered in each of these categories. Table 4.2 also indicates those generic components which are important to the structure's or to the equipment's safety function (i.e., if they were to fail, components within the structure, or the integrity of the structure itself, could be in jeopardy). Some generic structural components were evaluated as not necessary to a structure's safety function. These components are also indicated on Table 4.2.

#### 4.5.3 Effective Program Review

The generic structural components which were identified in Table 4.2 as important to safety are further evaluated to determine if each is subject to an effective program as defined in Section 3.5.2 of this report. The following generic structural components: (1) masonry walls, (2) fire doors, and (3) ISI Program support components (snubbers) were determined to be covered by effective programs. The following discussion provides the basis for this dispositioning.

The Masonry Wall Survey Program presently provides for a detailed inspection each refueling of selected masonry walls. This program is implemented in accordance with plant procedures. Enhancements to the Masonry Wall Program (i.e., expanding the number of masonry walls covered) may be necessary upon completion of the structural evaluation.

Fire doors, including jambs and hardware, are inspected each refueling in accordance with plant procedures. The fire doors necessary to the structure's safety function have been identified in the Yankee Fire Hazards Survey and the Appendix R Manual. The associated plant procedures, with minimal enhancements, constitute an effective program for fire doors.

The Yankee Atomic Inservice Inspection (ISI) Program provides for periodic detailed inspection of selected pipe and equipment support components. The ISI Program, supplemented by supporting and implementing plant procedures, provides an effective program for the generic component "snubbers" identified in the ISI Program.

Based on the demonstrated effectiveness of these programs, further evaluation of the components covered by these programs is not required for license renewal. The remaining structural components will be reviewed for potential degradation as indicated in Table 4.2.

Various other plant procedures are in place to assess material condition of structural components, as well as to take remedial actions when required. These programs, however, did not fully meet the conservative criteria for demonstrated effectiveness. For example, concrete components in the Screenwell House and seal pit are inspected periodically in accordance with plant procedures. It is anticipated that these procedures, with some enhancement, will provide for an effective program for these concrete components.

#### 4.5.4 Aging-Degradation Review

The aging degradation review for structures is performed in two steps. First, a generic assessment of the potential for age-related degradation is performed for each of the following structural component groupings: (a) concrete, (b) structural and miscellaneous steel, (c) architectural items, and (d) support components. These generic assessments form the basis for performing the focused plant walkdown of structural components.

The generic assessments are based upon a literature search of available information to identify plausible age-related gradation modes and their effects. Identified degradation mechanisms are investigated to further identify stressors, environment, manifestation, and mitigating design features and construction methods. All these factors are used to focus the plant walkdown by identifying plant areas which may be susceptible to potentially significant age-related degradation. Attachment K provides the "Generic Assessment of Concrete Structural Components" as an example of the assessment process.

The plant walkdown of structural components was performed by a team of four experienced structural engineers, one from Yankee, two from Stone & Webster Engineering Corporation, and one from Bechtel. The Bechtel representative is also a member of the Bechtel team preparing the industry report on Class I structures. All structures requiring component level screening identified in Attachment D were included in the walkdown.

Preparation for the walkdown was performed in accordance with detailed work instructions. The preparation included review of plant drawings and development of walkdown checklists using the information obtained from the generic assessments.

During the walkdown, focused inspections were performed based on preparation guidance, as well as an overall assessment of material condition and environmental conditions. Inaccessible areas were identified for follow-up evaluation. Attachment L provides sample data sheets used in the walkdowns. Components showing signs of degradation or the potential for degradation due to harsh environmental conditions are documented. These components will be subject to further evaluation to determine the cause and significance of the degradation and assess the need for corrective action.

Walkdown findings and follow-up evaluations will determine the need for and schedule for additional inspection. The walkdown was documented on videotape which can be used as the basis for trending material condition as necessary.

#### 4.5.5 PAB/DGB/B3B Walkdown Results

The walkdown was recently completed, and data gathered is now undergoing review. Preliminary findings for the PAB, DGB, and B3B are discussed below.

At the time of the walkdown, the DGB and B3B roofs were being replaced with a membrane-type roofing system. Portions of the PAB roof were also being replaced with a membrane-type roofing system. The remaining portions of the PAB roof, which are tar and gravel roofs, were determined to be in need of replacement.

The DGB is in very good condition. No significant signs of degradation to either DGB structural concrete or steel were observed. Base plates for two columns were observed not to be fully grouted to foundation concrete.

Maintenance requests were initiated to perform the repairs. The initiation of corrosion for some equipment support steel was observed. In particular, support steel and saddles for the SI nitrogen tanks located on the DGB roof are experiencing localized corrosion which will need to be addressed.

The B3B is in excellent condition. No signs of degradation were observed.

The PAB is in very good condition. However, several minor indications of degradation were observed. These include minor cracking, with signs of CaOH leaching, in the wall below the door in south wall due to water intrusion, the initiation of corrosion (minor surface rusting and minor localized pitting) of embedded plates and steel, minor damage to grout for base plate to two columns and one equipment support pedestal, very fine pattern shrinkage cracks on a wall at two locations, and pattern cracking on a portion of the concrete roof exposed to weather.

#### 4.5.6 Summary - DGB/PAB/B3B Structural Review

The focused structural walkdown, supported by the generic component assessments, demonstrated that DGB, PAB, and B3B are not experiencing any

significant aging degradation. The results of the walkdown does show the need to address the minor degradation identified. Specific actions being considered for steel and equipment support are the repair of corrosion spots and the improvement of plant maintenance practices regarding the restoration of protective coatings following equipment installation or maintenance. The need for monitoring the observed cracking is also being assessed. The final results of the structural evaluation will be completed in early 1990.

#### TABLE 4.1

#### Electrical Component Groupings

Category	Group
Communications	*Annunciators
	*Phones
	*Sirens/Horns
Conductors	*Cable
	*Penetrations
	*Bus Duct
Control and Protection	*Breakers
	Capacitors
	Control Board
	*Fuse/Holders
	*Grounding
	Surge Protection
	*Shunts
	Switches
	*Relays
DC Supply Generators	Batteries
	Diesels
	*Heaters
	Motors
	Motor/Generator
	*Solenoids
Power Conversion	Chargers
	Exciters
	Inverters
Switchgear	MCC
	Metal Clad
	OCB
	Panels
Terminations	*Lugs
	*Splices
	*Terminal Blocks
Transformers	*Dry
	Liquid Filled
	Voltage Regulators

<sup>\*</sup>These components will be generically evaluated.

Table 4.2 Generic Structural Components

۸.	Conc	rete (Including Reinforcing Steel)	Important To Safety Function	Not Subject to Effective Program	Requires Further Evaluation
	1.	Foundations (Footings, Beams, and Mats)	Y	Y	Y
	2.	Columns	Y	Y	Y
	3.	Walls	Y	Y	Y
	4.	Ground Floor Slabs and Equipment Pads	Y	Y	Y
	5.	Elevated Floor Slabs	Y	Y	Y
	6.	Roof Slabs	Y	Y	Y
	7.	Cast-In-Place Anchors	Y	Y	Y
	8.	Manholes	Y	Y	Y
	9.	Duct Banks	Y	Y	Y
	10.	Grout	Y	Y	Y
	11.	Concrete Blocks (Shielding)	Y	Y	Y
	12.	Precast Concrete	Y	Y	Y
	13.	Fluid Retaining Walls and Slabs	Y	Y	Y
	14.	Masonry Walls	Y	N	N
	15.	Post-Installed Anchors (Expansion and Grouted Types)	Y	Y	Y
В.		ctural Steel luding Bolts, Rivets, and Welds)			
	1.	Base Plates	Y	Y	Y
	2.	Columns	Y	Y	Y
	3.	Floor Framing	Y	Y	Y
	4.	Roof Trusses	Y	Y	Y

<sup>\*</sup>Y = Yes N = No

## Table 4.2 (Continued)

#### Generic Structural Components

		Important To Safety Function	Not Subject to Effective Program	Requires Further Evaluation
3.	Roof Framing	Y	Y	Y
6.	Vertical Bracing	Y	Y	Y
7.	Horizontal Bracing	Y	Y	Y
8.	Girts	Y	Y	Y
9.	Platform Hangers	Y	Y	Y
10.	Galvanized Steel Frames	Y	Y	Y
11.	Roof Decking	Y	Y	Y
12.	Jet Impingement Barriers	Y	Y	Y
13.	Light Poles	N		N
14.	Stainless Steel Liners	Y	Y	Y
15.	Light-Gage Metal Buildings	Y	Y	Y
16.	Floor Grating	N		N
17.	Checkered Plate Flooring	N		N
18.	Stairs and Ladders	N	-	N
19.	Miscellaneous Frames and Lintels	N		N
Arch	itectural Items			
1.	Building Siding	N	-	N
2.	Roofing (Built-Up or Elastometric, Including Insulation, Ballast, and Flashing)	Y	Y	Y
3.	Fire Doors, Jambs, and Hardware	Y	N	N
4.	Access Doors, Jambs, and Hardware	N		N
5.	Windows	N		N

c.

## Table 4.2 (Continued)

#### Generic Structural Components

			Important To Safety Function		Requires Further Evaluation
	6.	Glass and Glazing	N	-	N
	7.	Caulking and Sealants	Y	Y	Y
	8.	Floor Finishes	N		N
	9.	Coatings (Including Galvanizing)	N		N
	10.	Partitions and Ceilings	N	-	N
	11.	Furnishings	N	-	N
D.	Equi	pment Supports			
	1.	Structural Steel (Including Politing, Welds, and Baseplates)	Y	Y	Y
	2.	Snubbers	Y	N	N
	3.	Spring Supports	Y	Y	Y
	4.	Pre-Engineered Pipe Support Items	Y	Y	Y
	5.	Light-Gage Metal (i.e., Unistruts)	Y	Y	Y
	6.	Post-Installed Anchors (Expansion and Grouted Type)	Y	Y	Y
	7.	Grout	Y	Y	Y
	8.	Solid Lubricants	Y	Y	Y
	9.	Conduits	Y	Y	Y
	10.	Electrical Boxes	Y	Y	Y
	11.	Raceways	Y	Y	Y
	12.	Conduit Clamps	Y	Y	Y
	13.	Instrument Racks	Y	Y	Y
	14.	Instrument Panels	Y	Y	Y

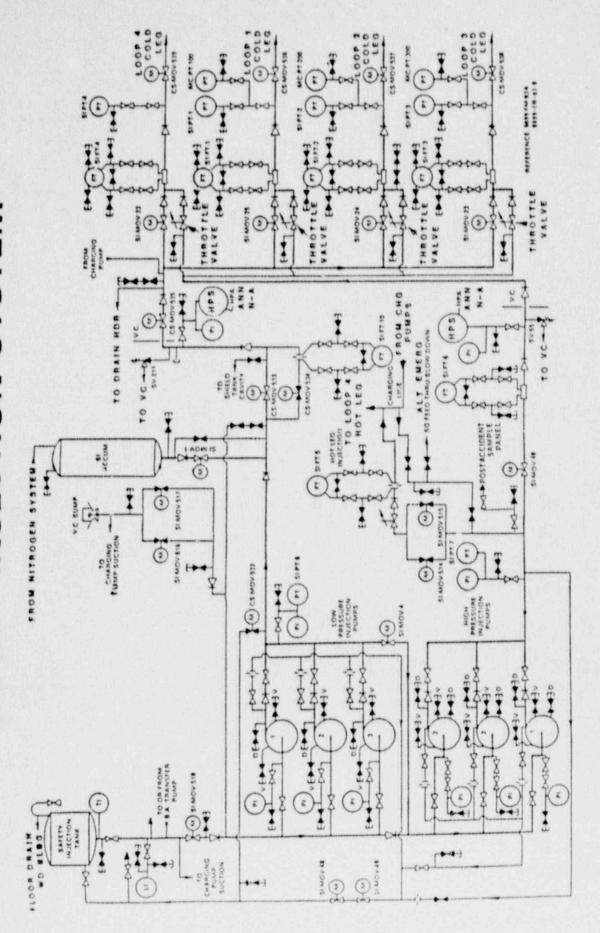
### Table 4.2 (Continued)

#### Generic Structural Components

		Important To Safety Function	Not Subject to Effective Program	Requires Further Evaluation
15.	Power Panel Boxes	Y	Y	Y
16.	Concrete Pedestals	Y	Y	Y
17.	Coatings (Including Galvanizing)	N*	-///	N

<sup>\*</sup> Note: Vapor container coatings are being evaluated separately.

# SAFETY INJECTION SYSTEM



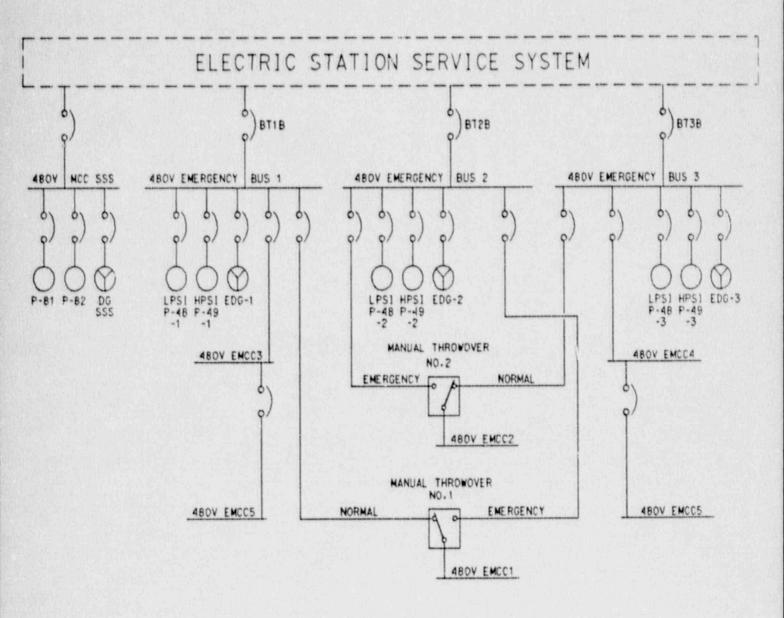


FIGURE 4.2

EMERGENCY ELECTRIC POWER SYSTEM

#### 5.0 CONCLUSIONS

The key objectives of the Yankee Pilot Evaluation Report were to demonstrate through a formalized process that:

- o All systems, structures, and components requiring license renewal evaluation are identified.
- o Assures that any potentially significant age-related degradation is recognized and properly managed, as necessary.

As presented in the report, the objectives have been met. Of the total 78 systems and 46 structures at Yankee, 43 systems and 27 structures were determined to require evaluation for license renewal. The potential for significant age-related degradation and the methods of managing degradation were assessed for the pilot systems and structures. In addition, areas requiring further evaluation or special actions were identified.

The methodology, criteria, and technical justification supporting plant-specific methods of implementing these objectives were provided. A cross section of the plant was evaluated to show the differences in implementation as applied to different discipline areas.

The areas of the plant evaluated were generally found to be in good condition with no signs of significant degradation. However, as indicated in the report, several components will require further evaluation and some plant procedures will need enhancement to better address degradation concerns for license renewal.

Examples of assessments, checklists, and other information supporting the technical bases of the evaluations are provided to allow the NRC staff to conclude that the process used is both thorough and technically justified. Because the same evaluation process used for the components presented in the Pilot Report is being applied to the plant in general, it should simplify future NRC license renewal reviews.

ATTACHMENT A

APPENDIX A

(CRITERIA)

to

NUMARC NUPLEX
"METHODOLOGY TO EVALUATE PLANT EQUIPMENT
FOR LICENSE RENEWAL"

#### Step 1. Evaluation of All Plant Systems and Structures

Substep la. Does the Plant System or Structure Contribute to Plant Safety?

1a.1. Systems or structures that are identified as being safety-related in a licensing basis document.

OR

1a.2. Systems relied upon or structures identified in a licensing basis safety analysis or evaluation.

OR

1a.3.a Systems utilized in plant emergency operating procedures.

or

1a.3.b Systems taken credit for in a risk assessment if a plant unique risk assessment is available and used.

- Substep 1b. Is Degradation of the System or Structure Potentially Significant to Plant Safety?
  - 1b.1.a The system's or structure's failure could not directly result in off-site releases exceeding FSAR or other plant-specific off-site release limits.

and

1b.1.b The system's or structure's failure could not result in reactor coolant pressure boundary or primary containment leakage in excess of technical specification limits.

and

- 1b.1.c.1 The system or structure is not otherwise required
   for the performance or control of:
  - (1) reactor criticality
  - (2) reactor coolant system integrity, inventory, or heat removal
  - (3) containment integrity or heat removal

or

1b.1.c.2 Although the system or structure may be required for these functions, the system's or structure's failure is detectable in a time frame which would allow shutdown prior to requiring a manual or automatic plant trip.

OR

- 1b.2. A plant-unique risk assessment, if available and used, demonstrates that:
- 1b.2.a The system's or structure's failure does not occur in a sequence that has a core damage frequency greater than or equal to 1 x 10<sup>-6</sup> per year or in a sequence that contributes 5% or more to the total estimated core damage frequency.

and

- 1.b.2.b When the system or structure is assumed to fail due to age-related degradation, the total estimated core damage frequency will not increase by more than a factor of 3 or will not exceed 1 x 10<sup>-4</sup> per year.
- Step 2. Evaluation of Components Within Systems and Structures
  - Substep 2a. Is the Component Important to System or Structure Safety Function?

The component is important to system or structure safety function unless:

2a.1. The component is normally isolated and does not perform an accident mitigating function.

OR

2a.2.a Component failure would not result in either the failure of any individual train within the system or the failure of the entire system to perform its required safety function.

and

2a.2.b Component failure would not reduce the structural support of any other component such that it would not perform its system safety function.

and

2a.2.c Component failure would not physically damage any other component such that it would not perform its system safety function.

OR

- 2a.3. For components within the scope of a plant-unique risk assessment, if available and used, the component is not included in the risk assessment models.
- Substep 2b. Is the Component Subject to Established Effective Replacement, Refurbishment, or Inspection Programs?

A component is considered to be subject to an established effective replacement, refurbishment, or inspection program if:

2b.1. The program is documented, approved, and routinely implemented in accordance with plant administrative procedures.

AND

2b.2. The program procedures ensure that all of the component's significant safety functions are properly addressed,

AND

- 2b.3. The program establishes specific criteria for determining the need for corrective action and requires such action be taken if these criteria are not met.
- Substep 2c. Is the Component Subject to Potentially Significant Age-Related Degradation?

The component will be considered subject to potentially significant age-related degradation unless:

2c.1 It is established and documented that potentially significant age-related degradation will not occur during the license renewal period.

OF

- 2c.2 A plant-unique risk assessment, if available and used, demonstrates that:
- 2c.2.a When the component is assumed to fail due to agerelated degradation, the total core estimated damage frequency will not increase by more than a factor of three or will not exceed 1 x 10<sup>-4</sup> per year.

and

- 2c.2.b When an age-related common-cause failure mechanism is postulated that may cause multiple components to fail (among those which have satisfied Criterion 2c.2.a), those components meet Criterion 2c.2.a when their combined failures are considered as a single event.
- Substep 2d. Options to Resolve Potentially Significant Age-Related Degradation.

A variety of options to resolve potentially significant agerelated degradation may be appropriate depending upon the component being addressed. Among the options are:

- Replace the component on a replacement schedule which precludes component age-related degradation from becoming a problem.
- Demonstrate, by detailed investigation, that age-related degradation of the component will not be significant during the license renewal period.

- Demonstrate, by a more rigorous analysis, that the potential age-related degradation of the component is not significant to safety.
- 4. Institute practices which manage component age-related degradation by diagnosing the age-related degradation processes and preventing or mitigating their effect.

## ATTACHMENT B PLANT SYSTEMS AND STRUCTURES LIST

# ATTACHMENT B YANKEB ATOMIC ELECTRIC COMPANY YNPS LICENSE RENEWAL PROJECT SYSTEM AND STRUCTURES LIST

\$200 CERT TO SER	SYSTER	SYSTEM/STRUCTURE TITLE	SYSTEM/STRUCTURE DESCRIPTION
1	AR	AIR REMOVAL SYSTEM	Piping, valves, pumps and other related equipment associated with removing air and non-condensible gases from the main condenser.
2	AS	AUXILIARY STEAM SYSTEM	Piping, valves, and other related equipment associated with the delivery of steam to the following loads: turbine driven emergency boiler feed pump turbine, small hogger, large hogger, steam jet mir ejector, gland steam and building heating steam header and other miscellaneous steam loads.
3	BF	BOILER FEED SYSTEM	Pumps, piping, valves, heat exchangers and other related equipment associated with taking water from the condenser hot well, raising its pressure and temperature, and delivering it to each of the steam generators.
4	BA	BREATHING AIR SYSTEM	A self-contained compressed air system designed to provide breathing air during plant shutdown conditions for work inside the vapor container.
5	CH	CHARGING AND VOLUME CONTROL SYSTEM	Piping, pumps, valves, heat exchangers, tanks and other related equipment associated with controlling main coolant inventory and main coolant chemistry.
6	CF	CHEMICAL PEBD SYSTEM	System provided to help minimize corrosion in secondary piping and equipment through the addition of hydrazine and/or morpholine during plant operation. These chemicals are injected downstream of the boiler feed pumps.
1	CS	CHEMICAL SHUTDOWN SYSTEM	Piping, valves, tanks, and related equipment associated with supplying borated water to the LPST, or charging pumps for chemical reactivity control.
8	CW	CIRCULATING WATER SYSTEM	Piping, pumps, valves, heat exchangers and other related equipment associated with taking water from Sherman Pond, passing it through the condenser, and returning it to Sherman Pond; includes the vacuum priming sub-system.
9	cc	COMPONENT COOLING WATER SYSTEM	Piping, valves, pumps, heat exchangers and other related equipment associated with removing heat from various nuclear plant cooling loads (which may contain radioactive fluids) and transferring that heat to the service water system.
10	CA	COMPRESSED AIR SYSTEM	Piping, valves, compressors, filters, receivers, dryers and other related equipment associated with delivering compressed air to control and service air loads.

						4	11	A	0	H	H	E	N'	1	B							
YA	N	K	EE		1	0	()	C		8	U	B	01	R	1	C	0	0	H	P	A	ķ
7	N	P	8	LI	0	E	18	8		E	E	N	B	Á	1	1	P	10	7	B	C	ľ
	8	Y	51	BH		A	10		S	1	R	U	C	U	R	B		L	1	8	1	
 		*														.,				*		

10.000 miles	SYSTEM !	SYSTEM/STRUCTURE TITLE	SYSTEM/STRUCTURE DESCRIPTION
11	00	CORROSION CONTROL SYSTEM	Functions to minimize main coolant system corrosion rates by reducing dissolved oxygen to a minimum value through the addition of hydrazine when the reactor is subcritical and holding this value during power operation by maintaining a hydrogen cover gas in the low pressure surge tank.
12	DW	DEMINERALIZED WATER SYSTEM	Piping, valves, tanks, demineralizer and other related equipment associated with suppling high quality, demineralized water to the primary and secondary systems.
10	EBP	BMERGENCY BOILER FEED SYSTEM	Piping, pumps, valves, tanks and other related equipment associated with providing emergency feedwater to the steam generators via normal and alternate feed flow paths.
14	ES	EXTRACTION STEAM SYSTEM	Piping, valves, heat exchangers and related equipment associated with taking steam from the high pressure and low pressure turbines (extraction points and exhaust) and delivering it to the feedwater heaters, and subsequently draining and cooling the resulting condensate back to the condenser.
15	FS	FIRE DETECTION AND SUPPRESSION SYSTEM	Equipment related to fire detection and suppression, including firewater, halon, and carbon dioxide suppression sub-systems.
16	PD	PLOOR DRAINAGE SYSTEM	Piping system which provides floor drainage flow paths for numerous equipment drains throughout the plant.
17	FO	FUEL OIL SYSTEM	Piping, valves, pumps, storage tanks and related equipment associated with supplying fuel oil to the emergency diesel generators and the auxiliary boilers.
18	og .	GENERATOR GAS	Piping, valves, blowers, heat exchangers, gas storage bottles and related equipment associated with containing, circulating and cooling hydrogen gas within the main generator.
19	80	GENERATOR SEAL OIL SYSTEM	Piping, valves, pumps, tanks, heat exchangers associated with suppling sealing oil to the main generator labyrinth seals.
20	HC1	HEATING STM/CONDENSATE	Piping, pumps, valves, tanks and related equipment associated with supplying heating steam and returning condensate for various plant loads: safety injection tank heaters, diesel generator building, alternate steam supply to EBF turbine driven pump and space heating loads throughout the plant.
		***************************************	***************************************

# ATTACHMENT B YANEBE ATOMIC BLECTRIC COMPANY YMPS LICENSE RENEWAL PROJECT SYSTEM AND STRUCTURES LIST

CORD :	SYSTEM CODE	SYSTEM/STRUCTURE TITLE	SYSTEM/STRUCTURE DESCRIPTION
21	HV	HYDROGEN VENTING SYSTEM	Piping, valves, analyzers and related equipment necessary to monitor and control the post-accordent hydrogen concentration within the vapor container.
22	10	INERT GAS SYSTEM	Provide nitrogen cover gas to be used primarily during layup to minimize corrosion and for systems using flammable fluids; lubricating cil systems, etc
23	LO	LUBRICATING OIL SYSTEM	Piping, valves, pumps, tanks, purifiers, coolers and related equipment associated with supplying lubricating oil to the turbine, generator and exciter bearings.
24	<b>K</b> C	MAIN COOLANT SYSTEM	Piping, pumps, valves, steam generators and related equipment associated with circulating pressurized water through the reactor core and transferring the sensible heat gained to the secondary system for conversion to steam.
25	MS	MAIN STEAM SYSTEM	Piping, valves and related equipment associated with conveying steam produced in the steam generators up through the high pressure turbine throttle valves.
26	NS	NITROGEN SYSTEM	Piping, valves, nitrogen supply bootles and related equipment associated with the SI accumulator nitrogen charging system.
27	₽₩	POTABLE WATER SYSTEM	A well water system which serves water closets, lavatories, drinking and wash fountains, showers and sinks throughout the plant; this system can also be cross-connected to the turbine lube oil coolers.
28	PR	PRESSURE CONTROL AND RELIEP SYSTEM	Piping, valves, pressurizer, pressurizer heaters, pressurizer sprays, and related equipment associated with controlling main coolant system pressure.
29	PU	PURIFICATION SYSTEM	Piping, valves, pumps, coolers/ion exchangers and related equipment associated with cooling and purifying main coolant in the low pressure surge tank and removing soluble and insoluble impurities.
30	<b>V</b> D	RADIOACTIVE WASTE DISPOSAL SYSTEM	Piping, valves, pumps, tanks, coolers, evaporators and related equipment associated with receiving, containing, treating and disposing of all radioactive waste other than separately handled secondary plant low level radioactive wastes.

# ATTACHMENT B YANEED ATOMIC ELECTRIC COMPANY YMPS LICENSE RENEWAL PROJECT SYSTEM AND STRUCTURES LIST

			SYSTEM AND STRUCTURES LIST
CORD   KBER	SYSTEM (	SYSTEM/STRUCTURE TITLE	SYSTEM/STRUCTURE DESCRIPTION
31	RF	REFUBLING SYSTEM	Piping, valves, pumps and other related equipment associated with refueling operations.
32	SSS	SAFE SHUTDOWN SYSTEM	Piping, valves, pumps, tanks and related equipment associated with providing borated primary make up water to the main coolant system and feedwater to the steam generators in the event other normal and emergency systems are not available.
33	SI SI	SAFETY INJECTION SYSTEM	Piping, valves, pumps, tanks, accumulators and other related equipment associated with restoring main-coolant inventory following a loss of coolant accident.
34	8.4	SAMPLE SYSTEM	Piping, valves, coolers and related equipment associated with primary and secondary system sampling.
35	808	SANITARY DISPOSAL SYSTEM	Plant septic system.
36	SV	SERVICE WATER SYSTEM	Piping, pumps, valves, tanks, heat exchangers and other related equipment associated with providing Sherman Pond water for cooling numerous primary and secondary plant equipment.
37	SP	SHIELD TANK CAVITY PURIFICATION SYSTEM	Equipment, pumps, ion exchange resin beds, filters, valves, piping etc., necessary to remove impurities from the main coolant system during shutdown in order to reduce main coolant radioactivity levels and fouling of heat transfer surfaces.
38	SC	SHUTDOWN COOLING SYSTEM	Piping, valves, pumps, heat exchangers and related equipment used to remove decay heat from the main coolant system during extended shutdown periods.  Used when main coolant system conditions are below 330 F and 300 PSIG.
39	SF	SPENT FUEL SYSTEM	Pumps, piping, valves, coolers, and related equipment associated with spent fuel pit, and transfer of fuel between the fuel vault, spent fuel pit, and the reactor vessel.
40	TO	TURBINE GENERATOR SYSTEM	Turbine/generator assembly and supporting equipment.
41	vo	VENT AND DRAIN SYSTEM	Piping, valves, tanks and related equipment associated with primary and secondary vents and drains, including the steam generator blowdown system.
42	TV	WATER TREATMENT SYSTEM	Equipment, demineralisers, storage tanks, and related equipment necessary to clarify, filter, and demineralise water and to mix and pump water-conditioning chemicals to the primary and secondary plants; thus

		ATT	AC	HAE	NT I			
YANEER	A	TONI	C	BLB	CTRI	C	00	MPAN
YNIS	U	CENS	E	REN	EVAL	P	RO.	JECT
SYST	EH	AND	S	TRU	CTU	ES	L	181

SYSTEM	SYSTEM/STRUCTURE TITLE	SYSTEM/STRUCTURE DESCRIPTION
		providing reactor grade makeup water to the primary plant and condensate grade makeup water to the secondary plant.
HC9	ADMINISTRATION BLDG VENTILATION SYS	Provides air conditioning and ventilation for the administration building.
AD	AIR DISPOSAL (FILTBRED EXHAUST) SYSTEM	Ductwork, fans, filters, dampers and related equipment associated with exhausting potentially contaminated air through the primary vent stack; includes the vapor container ventilation and purge sub-system (used during refueling operations).
HC10	BATTERY ROOM NOS VENTILATION SYSTEM	Fans, ductwork, louvers and related equipment associated with Battery Room No.3 ventilators.
HIDA	BATTERY ROOMS 1+2 VENTILATION SYSTEM	Provides for hydrogen gas removal during battery charging operations; consists of a single exhaust fan taking suction from each battery room and discharging to outside air through a common exhaust duct.
HC5	CONTROL ROOM VENTILATION SYSTEM	Equipment associated with heating or cooling or filtering the control room atmosphere; includes the control room emergency air cleaning system (CREACS).
HC11	EDG BUILDING VENTILATION SYSTEM	Fans, dampers, ductwork and related equipment associated with ventilating the diesel generator building.
BC8	GAS STORAGE ROOM VENTILATION SYSTEM	Natural draft ventilation system consisting of floor vents, windows and roof louvers.
RC1	NRV ENCLOSURE VENTILATION SYSTEM	Exhaust fans, steam unit heaters and related equipment associated with heating/cooling the main steam non-return valve enclosure.
HC14	PAB NON-FILTERED VENTILATION SYSTEM	Provides upper level PAB with summer ventilation; consists of a roof-type exhaust fan with supply air entering through window and door openings.
HC12	SAPETY INJECTION BLDG VENTILATION SYS	Exhaust fans, motor operated louver and related equipment which function to maintain the safety injection building temperature within acceptable limits.
BC13	SCREENWELL PUMPHOUSE VENTILATION SYSTEM	Ventilation system consisting of two centrifugal fans and associated ductwork which can provide outside air, or recirculate pumphouse air, as necessary to maintain acceptable pumphouse temperatures without having to resort to steam heating.
	HC10 HC10 HC11 HC11 HC14	HC10 BATTERY ROOM NOS VENTILATION SYSTEM  HC10 BATTERY ROOM NOS VENTILATION SYSTEM  HC2 CONTROL ROOM VENTILATION SYSTEM  HC11 EDG BUILDING VENTILATION SYSTEM  HC11 EDG BUILDING VENTILATION SYSTEM  HC11 EDG BUILDING VENTILATION SYSTEM  HC11 PAB NON-FILTERED VENTILATION SYSTEM  HC12 SAPETY INJECTION BLDG VENTILATION SYSTEM

# NY

ATTACHMENT B					
	YANKEE	ATONIC	BLECTRIC	COMPA	
	YNPS 1	ICENSE	RENEWAL	PROJEC'	
	SYSTE	IN AND	STRUCTURE	s List	

			**********************************
STATE OF THE PARTY	SYSTEM :	SYSTEM/STRUCTURE TITLE	SYSTEM/STRUCTURE DESCRIPTION
54	HC8	SERVICE BLDG VENTILATION SYSTEM	All equipment, air conditioning units, ventilators etc. necessary to supply ventilation air and heated air to the service building.
55	HC4	TURBING BLDC VENTILATION SYSTEM	Natural draft ventilation system consisting of continous roof ventilators and window openings which provide the necessary air changes to maintain turbine building temperature at acceptable levels.
56	VCHCR	VC HEATING, COOLING, AIR RECIRCULATION	Fans, dampers, coolers, heaters, ductwork and related equipment which operate to maintain vapor container atmosphere below limits during normal operation; includes vapor container post-accident air recirculation sub-system.
5?	DC	DC DISTRIBUTION SYSTEM	Equipment, batteries, battery chargers, cabling, and related equipment necessary to supply do electrical power to plant do electrical loads.
<b>5</b> 8	DG	DIESEL GENERATOR SYSTEM	Emergency diesel generators and related equipment necessary for supplying emergency ac power to the emergency power system in the event of loss of normal ac power.
59	EBPS	BMERGENCY POWER SYCHEM	Equipment, cabling, busses, breakers, etc., necessary to supply electrical power and control to essential safeguard loads.
60	BGTS	GENERATION AND TRANSMISSION SYSTEM	Equipment necessary to generate and deliver station electrical cutput to the 115 kv power grid.
61	ESSS	STATION SERVICE SYSTEM	Electrical equipment, cables, breakers, transformers, busses, relays, etc., necessary to distribute normal ac electrical power and control to station loads, the safe shutdown system and the emergency power system.
62	CI	CONTAINMENT ISOLATION SYSTEM	Equipment necessary to isolate the vapor container (VC) if VC pressure equals or exceeds 5 PSIG; includes isolation actuation circuitry, check valves, automatic trip valves, manual valves, and blank flanges, etc
63	PV	FEEDWATER CONTROL SYSTEM (IAC)	Instrumentation and circuitry associated with main feedwater control.
64	FIDS	FIXED INCORE DETECTION SYSTEM	Equipment, detectors, cabling, etc., necessary to measure and record neutron flux signals at fixed core positions.
65	LN.	LEAK MONITORING SYSTEM	Instrumentation and equipment necessary to perform vapor container integrated leak rate testing.

	TTA	ACHMENT B	
YANKEE	ATOMI	C BLECTRIC	COMPAN
YNPS	LICENS	E RENEWAL F	ROJECT
SYST	BH AND	STRUCTURES	LIST

Break and the second	SYSTEM :	STSTEM/STRUCTURE TITLE	SYSTEM/STRUCTURE DESCRIPTION
66	MIDS	MOVABLE INCORE DETECTION SYSTEM	Equipment, detectors, cabling, drive units, transfer devices etc., necessary to operate the moveable incore detectors which function to accumulate neutron flux data at varying core heights for fixed radial core position.
67	NRV	NONRETURN VALVE SYSTEM	Instrumentation and circuitry associated with Main Steam non-return valves and valve isolation logic.
68	NI	NUCLEAR INSTRUMENTATION SYSTEM	Excore equipment, excore detectors, cabling, counters, analyzers power supplies, etc., necessary to provide indication of reactor power level from cold shutdown to fullpower; provides inputs to the reactor protection system.
69	PZK	PROCESS RADIATION MONITORING SYSTEM	Equipment, detectors, cabling, etc., necessary to monitor radioactivity levels in plant process fluids and effluents.
70	RM	RADIATION MONITORING SYSTEM	Area radiation monitoring system consisting of numerous radiation detectors located throughout the plant.
"1	RCS	REACTOR CONTROL SYSTEM	Control rod drive mechanisms, control circuitry, position indication instrumentation and related equipment necessary to move control rods in order to control reactivity.
72	RPS	REACTOR PROTECTION SYSTEM	Equipment, circuit breakers, instrument channels, bi-stables, control circuitry and related equipment necessary to initiate a reactor scram (and turbine trip) on unsafe conditions which could cause damage to the reactor core or main coolant pressure boundary.
73	SPDS	SAFETY PARAMETER DISPLAY SYSTEM	Equipment, computers, hardware and software, etc., necessary to take digital/analog plant process parameters and display them in varying formats on monitors located in the main control room.
14	\$\$	SECURITY SYSTEM	Plant security system.
15	SG	SG BLDN IAC SYSTEM	Miscellaneous instrumentation and related equipment associated with steam generator blowdown.
76	VC	VAPOR CONTAINER MONITORING SYSTEM	Equipment, instrumentation and related equipment necessary to monitor VC temperature, pressure and humidity.
11	EN	ENVIRONMENTAL SYSTEM	Meteorological instrumentation and related equipment primarily mounted on the meteorological tower.

### ATTACEMENT B YANKEE ATOMIC ELECTRIC COMPANY YNPS LICENSE RENEWAL PROJECT SYSTEM AND STRUCTURES LIST

			SYSTEM AND STRUCTURES LIST
ORD :	SYSTEM   CODE	SYSTEM/STRUCTURE TITLE	SYSTEM/STRUCTURE DBSCRIPTION
78	180	TECHNICAL SUPPORT CENTER SYSTEM	Blectronic equipment servicing the Technical Support Center.
79	AB.	ADMINISTRATION BUILDING	Steel-framed masonry building located inside the owner controlled area which houses offices for plant staff.
80	B3B	BATTERY ROOM NO. 3 BUILDING	Reinforced masonry wall structure which houses Battery No.3 and emergency motor control centers.
81	CLP	CAMERA AND LIGHTING POLES	Yard lighting and security camera utility poles.
82	CB	COMPACTOR BUILDING	Masonry structure which houses the low level radioactive waste compactor.
83	DE_R	DECONTANINATION ROOMS	Radioactive decontamination facility located within service building.
84	DGB	DIESEL GENERATOR BUILDING	Stee) frame and masonry wall structure which houses the Emergency Diesel Generators.
85	EPS	EQUIPMENT AND PIPE SUPPORTS	Generic category consisting of equipment and piping supports.
86	FAG	PENCE AND GATES	Provides physical barrier for the owner controlled area.
87	TANK	FIELD FABRICATED TANKS	Generic category consisting of tanks fabricated on site.
88	PWP	FIRE WATER PUMPHOUSE	Pre-fabricated metal building adjacent to the fire water storage tank which houses the diesel driven fire pump.
89	PDN	FOUNDATIONS FOR OUTDOOR TANKSASTACES	Generic category consisting of foundations for outdoor stacks and tanks.
90	FOTH	FUEL OIL TRANSFER PUMP HOUSE	Structure which houses fuel oil transfer pump.
91	PTCS	FUEL TRANSPER CHUTE STRUCTURE	Reinforced concrete structure which houses the stainless steel fuel transfer chute.
92	GH	GATEHOUSE	Masonry and concrete structure which functions as the security point through which all persons entering the owner controlled area must pass.
93	BBVS	HBATING BOILER VENT STACE	Vents heating boiler exhaust gas to atmosphere.
94	IEP	ION EXCHANGE PIT	Reinforced concrete structure which houses ion exchangers used in the purification system.
95	PHE	LIPTING AND HOISTING EQUIPMENT	Generic category for lifting and hoisting equipment, includes all major lifting devices.

### ATTACHMENT B YANKEE ATOMIC BLECTRIC COMPANY YNPS LICENSE RENEWAL PROJECT

			SYSTEM AND STRUCTURES LIST
CORD   MBBR	SYSTEM !	SYSTEM/STRUCTURE TITLE	SYSTEM/STRUCTURE DESCRIPTION
96	Kī	METBOROLOGICAL TOWER	Steel tower which supports meteorological monitoring equipment.
97	NFV	NEW PUBL VAULT	Reinforced concrete and masonry structure used for storage of new fuel.
98	NEUB	NON ESSENTIAL UPS BUILDING	Masonry structure which houses the non-essential uninterruptable power supply.
99	PCA1	PCA STORAGE BUILDING NO. 1	Steel frame masonry wall structure used primarily to store low-level radioactive materials prior to shipping.
100	PCA2	PCA STORAGE BUILDING NO. 2	Steel frame building used primarily for the storage of contaminated tools and equipment.
101	PCAN	PCA WAREHOUSE	Steel frame building used for the storage of low level radioactive waste.  waste containers, and contaminated equipment.
102	PKOB	PLANT MODULAR OPPICE BUILDING	Modular office building housing plant support personnel; located inside owner controlled area.
103	РВ	POLE BARN	Utility storage building located inside owner controlled area.
104	PAB	PRIMARY AUXILIARY BUILDING	Reinforced concrete and steel frame structure which houses numerous primary related equipment: charging pumps, component cooling pumps and heat exchangers, shutdown cooling pumps and heat exchanger, purification system, etc
105	PVS	PRIMARY VENT STACE	Steel stack (5' diameter, 130' high) used to vent the exhaust of the filtered ventilation system to atmosphere.
106	RSS	REACTOR SUPPORT STRUCTURE	Reinforced concrete structure and steel-encased concrete columns which supports the nuclear steam supply system (reactor vessel, biological shield, steam generators, etc.) and the polar crane.
107	SLBB	S.L.E. DIESEL GENERATOR BUILDING	Masonry structure adjacent the gatehouse which houses the security lighting emergency diesel generator.
108	SSSB	SAFE SHUTDOWN SYSTEM BUILDING	Reinforced concrete structure which houses the safe shutdown pumps and associated equipment.
109	SH	SCREENWELL HOUSE	Reinforced concrete sub-structure and steel frame superstructure which houses circulating water pumps, service water pumps, motor driven fire pump, travelling screens, sluice gates and other related equipment.
10	\$P	SEAL PIT	Reinforced concrete structure that receives circulating water from the

condenser and discharges it to Sherman Pond.

:01:42 /29/89

### ATTACHMENT B YANKEE ATOMIC ELECTRIC COMPANY YMPS LICENSE RENEVAL PROJECT SYSTEM AND STRUCTURES LIST

	SYSTEM :	SYSTEM/STRUCTURE TITLE	SYSTEM/STRUCTURE DESCRIPTION
111	SPVS	SECONDARY PLANT VENT STACE	Vent stack which is used to discharge secondary plant gaseous effluents. i.e., gland steam exhaust, to atmosphere.
112	SB	SERVICE BUILDING	Houses water treatment plant, primary and secondary side machine shops, decontamination rooms, looker rooms and other facilities.
112	SFP	SPENT PUEL PIT	Reinforced concrete structure that provides for underwater storage of spent fuel, spent control rods, and fuel transfer equipment.
114	SPSS	STEAM AND FREDWATER SUPPORT STRUCTURE	Steel frame structure supporting main steam and feedwater piping between the vapor container and the turbine building.
115	ST-W	STORES WAREHOUSE	Houses plant inventory of spare parts, materials, etc
116	SEIE	SUPPORTS FOR ELECT/I+C EQUIPMENT	Generic category for electrical and I&C supports.
117	\$7.5	SWITCH YARD STRUCTURE	Galvanised steel structure which supports oil circuit breakers, disconnects, and provides support for the power lines to Harriman and Cabot Stations.
118	TAB	TRAINING AREA BUILDINGS	One masonry building and one modular-type office building which house the plant training facilities; located outside the owner controlled area.
119	TAS	TRANSFORMER AREA STRUCTURE	Reinforced concrete and steel frame structure which supports the main transformer, the three station service transformers, and associated electrical equipment.
20	ТВ	TURBINE BUILDING	Steel frame structure which houses most secondary plant equipment, including turbine generator, condenser, condensate pumps, boiler feed pumps, heat exchangers, etc The control room and switchgear rooms are located within the turbine building.
21	vc	VAPOR CONTAINER	A nominal 125-foot diameter, vapor tight, steel sphere that houses, but does not support, the reactor support structure and nuclear steam supply system.
22	VEL	VC BLEVATOR ENCLOSURE	Structure which houses elevator to vapor container personnel access hatch.
23	<b>W</b> DB	WASTE DISPOSAL BUILDING	Steel frame building used for processing low level radioactive waste.
24	YACS	YARD AREA CRANE SUPPORT STRUCTURE	Steel frame structure which supports the yard crane.

### ATTACHMENT C

STEP 1a REVIEW RESULTS

SYSTEMS AND STRUCTURES WHICH CONTRIBUTE TO PLANT SAFETY

### ATTACHMENT C VANKEE ATOMIC ELECTRIC COMPANY TAPS LICENSE REMEMAL PROJECT STEP 18 REVIEW RESULTS

12
1
SAFET
Television I
PLAS
10
***
100
CONTRIBU
HICH
SYSTEM/STRUCTURES
1139
518
SAS

									0									**	::	213154
PECORD	SYSTEM	2011-1011		283	1	200.70					***						- 0	0350		STRUCTURE ONTRIBUTE
	and a	ALKON JOHN OF THE MET OF THE	CLASS	490-	SPECS	GUAL	THE .		SEISMIC	THE RESERVE	- 0	M ( )			SHEED SHEED	US (B)		# 66 		SAFETY SAFETY STEP 14
	4	AIR REMOVAL SYSTEM	*		*		•			,				•	•	-		-	ļ	
eu -	NS NS	AUXILIARY SIEAM SYSTEM	-	-	-		-		-									-	ļ	-
er)	16	BOILER FEED SYSTEM	-	-	-		-	*	-							-		-	ļ	*
	ā	BREATHING AIR SYSTEM	*	•	-	*	-			1					•	•		•	ļ	-
	5	CHARGING AND VOLUME CONTROL SYSTEM	-	-	-		*									-	-	*		*
167	8	CHEMICAL FEED SYSTEM	-	*			*		*		*				•	•				
	8	CHEMICAL SHUTDOWN SYSTEM	*		-		-		-				-			*	-	*		-
60	8	CIRCULATING WATER SYSTEM	*				*		*		3-				•	*	*	-		
en.	ម	COMPONENT COOLING MATER SYSTEM	-	*	>-		-		*				-			-	-	*	ļ	-
10	5	COMPRESSED AIR SYSTEM	-		-		-	×								-	*			
=	8	CORROSION CONTROL SYSTEM	*	*		-				1					-	*		•		
22		DEMINERALIZED MATER SYSTEM	-	*	*	-						w				-	*			
12	183	EMERGENCY BOILER FEED SYSTEM	>-		-			*		,			-		•	-	*	<b>3</b> -		-
=	£3	ENTRACTION STEAM SYSTEM	*				•	*			*						*		111	
42	53	FIRE DETECTION AND SUPPRESSION SYSTEM	-	*	-		102	*	-		*				•		*	*		-
40	83	FLOOR DRAIMAGE SYSTEM	-		-						*				•		*	*		-
	0.5	FUEL OIL SYSTEM	-	-		*	-	*								*		*		
60	99	GENERATOR GAS	-	•			•	*							•			*		-
No.	95	GENERATOR SEAL OIL SYSTEM	•	*	•	*	*	>							•			•		
20	128	HEATING STM/CONDENSATE	-	*	-	×		*	*		*				•		-		::::	-
12	ă.	HYDROGEN VENTING SYSTEM	-		-	*	*		*							*	*	-	222	-
23	2	INERT GAS SYSTEM	æ		*					1.	*				•			•		
53	03	LUBRICATING OIL SYSTEM	-	26		*		-									*	•		
7.7	¥	MAIN COOLANT SYSTEM	*		*	*	*	*	*		*						*	-		-
12	*	Section of the section							Sala name	· 日本大田七	1		-							

11			:::					LICENSI	NG BASTS	10							***	::	:::	SYSTEM!
RECORD	\$1578 3000	SYSTEM/STRUCTURE	SAFETY	FS.48 SECTS. 406-	11 15 15 15 15 15 15 15 15 15 15 15 15 1	ENVIR AP		INE SEISMIC	HEAVY TC LOADS	7 INT	Err 1	NING SMON	108- 1180		PERM RAS SHIELS	STA STA STACK		£ ± 56 1 ± 56 1 ± 56		STRUCTURE CONTRIBUTES TO PLANT SAFETY (STEP 18)
92	12	MITROSEM SYSTEM	-	-	11 4				1	-				-		-	-	-		
12	2	POTABLE WATER SYSTEM		-				•		-					-	-	-	•		
28	8	PRESSURE CONTROL AND RELIEF SYSTEM		-		*		*		*		*	-	-		-	-	*	ļ	
23	R	PURIFICATION SYSTEM	*	*		*		*		*				•			-			
330	6	RADIDACTIVE WASTE DISPOSAL SYSTEM	-	-	*			•		*				-			-	*		
E	<b>SE</b>	REFUELING SYSTEM		-	-							•			-		-	•		1
33	SSS	SAFE SHUTBOWN SYSTEM									*	-	-		-		-	*		*
13	SI	SAFETY INJECTION SYSTEM	-	-		-		*		*			-	*		•	-	-		-
*	75	SARPLE SYSTEM	*	*	-	*	*	*	ļ	*		*		-	•	•	-	-		-
33	SOS	SANITARY DISPOSAL SYSTEM	•	*			*	*			*	*			-			•		-
99		SERVICE MATER SYSTEM	-					*		>-				-	-	-	-	-	::::	
F	d.	SHIELD TANK CAVITY PURIFICATION SYTTEM	•		*			780		*	*	*		•		•		•	===	
90) (*)	35	SHUTBOWN COOLING SYSTEM	-	-	-					*	*	•	*	-	-		-	*		
gr.	15	SPENT FUEL SYSTEM	*	-	-		-	*			*		-		•		-	•	====	
40	16	TURBINE GENERATOR SYSTEM	-	-			-	•		*	*	-		-	-	-	-	-		
=	Q,	VENT AND DRAIN SYSTEM	-				-	*		*		*	-	-	-	-	-	*		-
42		MATER TREATMENT SYSTEM			*					*	*	*			*			•		•
£3	HCS	ADMINISTRATION BLDG VENTILATION SYS	*					•		*	*	•		-	-		•	•		
=	07	AIR DISPOSAL (FILTERED EXHAUST) SYSTEM		*	-			•			•					•	-			-
53	HC10	BATTERY ROOM NOS VENTILATION SYSTEM	•					•				*			-	•	-	•		
*	H104	BATTERY ROOMS 1+2 VENTILATION SYSTEM	*			3-					*				-			•		-
	¥CS	CONTROL ROOM VENTILATION SYSTEM	•					•			*		-		-	-	*	-		
89	BCT1	EDG BUTLDING VENTILATION SYSTEM	*	-	· · · ·	2-		*		*		*			*	-	-			
2	HC6	GAS STORAGE ROOM WENTILATION SYSTEM	*		-			*		*	*					•	×	•		
58	HC1	NRV ENCLOSURE VENTILATION SYSTEM		*				*		*	*		*	*				*	:::	*

ATTACHENT C
VANCE ATORIC ELECTRIC COMPANY
THPS LICENSE RENEWAL PROJECT
STEP 14 DEVISE BECALITY

	2015	
	***	
	584	
	Min.	
	3.5	
	KIT	
	630	
	-500	
	-	
	-50	
	20	
	60.	
	-	
*	200	
25	*	
π.		
π.	200	
ĸ	500	
53	-	
а.	200	
•	EN:	
	-	
σ.	-	
ä	8	
-	100	
2112	NC3	
21.63	803 H	
21.434	MCO HO	
21434 2	NCO HOL	
3 12412	HICH CON	
31 12 12	WICH CON	
38 85415	WHICH CON	
2112 18 124 12	S WHICH CON	
127 16 15412	ES WHICH CON	
3163 9 3316	RES WHICH CON	
2163 10 1216	URES WHICH CON	
3163 36 3316	TURES WHICH CON	
3157 16 85915	CTURES WHICH CON	
3157 16 85915	UCTURES WHICH CON	
3157 16 85915	RUCTURES WHICH CON	
3157 16 85915	TRUCTURES WHICH CON	
3157 16 85915	STRUCTURES WHICH CON	
3157 16 15115	/STRUCTURES WHICH CON	
3163 8 3216	M/STRUCTURES WHICH CON	
31634 36 45416	TEM/STRUCTURES WHICH CON	
31634 36 45416	STEM/STRUCTURES WHICH CON	
31634 36 45416	ISTEM/STRUCTURES WHICH COM	
3157 16 15915	SYSTEM/STRUCTURES WHICH COM	
3164 16 16416	SYSTEM/STRUCTURES WHICH COM	
DICK IN MEDICAL MEDICAL	SYSTEM/STRUCTURES WHICH COM	
31634 36 4316	SYSTEM/STRUCTURES WHICH CONTRIBUTE TO PLANT SAFETY	
31634 36 4316	SYSTEM/STRUCTURES WHICH COM	
316.38 36 4316	SYSTEM/STRUCTURES WHICH COM	
316.38 36 4316	SYSTEM/STRUCTURES WHICH COM	
31634 36 4316	SYSTEM/STRUCTURES WHICH COM	
31634 36 4316	SYSTEM/STRUCTURES WHICH COM	
31634 31 3316	SYSTEM/STRUCTURES WHICH COM	
31634 31 2316	SYSTEM/STRUCTURES WHICH COM	
31634 36 4316	SYSTEM/STRUCTURES WHICH CON	
3167 36 7316	SYSTEM/STRUCTURES WHICH CON	
3167 36 1216	SYSTEM/STRUCTURES WHICH CON	
31631 31 3316	SYSTEM/STRUCTURES WHICH CON	
31638 8: 33:6	SYSTEM/STRUCTURES WHICH CON	
31634 36 4316	SYSTEM/STRUCTURES WHICH CON	
31134 31 2316	SYSTEM/STRUCTURES WHICH CON	
31.32 31 2310	SYSTEM/STRUCTURES WHICH CON	
31.31 3: 23:0	SYSTEM/STRUCTURES WHICH CON	
31.34 31 3316	SYSTEM/STRUCTURES WHICH CON	
311.31 31 3316	SYSTEM/STRUCTURES WHICH CON	
311.31 21 1316	SYSTEM/STRUCTURES WHICH CON	
311.31 21 1316	SYSTEM/STRUCTURES WHICH CON	

				*	Section 1	- T T				1			Contract of the last	A STATE OF THE PARTY OF THE PAR			**	ALGERT .
RECORD SYSTEM NUKRER CODE	SYSTEM/STRUCTURE	SAFETY	FS.MB SECTS	150 PE	EWIR	8		07/318/13/ 3#1	HEAVY 141	1 Est	28 SEON 200	90.		# S	1 83	* 0 - 0	986	STRUCTURE CONTRIBUTE TO PLANT SAFETY
11			9	11	11	11				!	!!			SHEE	8	2		(516)
, W	PAR NON-FILLENED VENTILATION STSTEM	-	-	**								*	•		-			•
52   HC12	SAFETY INJECTION BLDG VENTILATION SYS		-		*				*							:::: -	-	
53 HC13	SCREENMELL PUMPHOUSE VENTILATION SYSTEM	*	-									•	•	-				•
54 HC8	SERVICE BLDG VENTILATION SYSTEM		*	•					*		•		-	-				-
10H 55	TURBINE BLOG VENTILATION SYSTEM	*	*	-			-					•						
SB YCHCR	YC HEATING, COOLING, AIR RECIRCULATION	-	-		-				•			•	-	-		-		-
20	DC DISTRIBUTION SYSTEM		-	-	-			x-				-	-		-			
56	DIESEL GENERATOR SYSTEM	-	(m-				*		*		*	-	-	-	-	-	-	-
59 EEPS	EMERGENCY POWER SYSTEM	-		-	*				*					-	-	*		
60 EGTS	GENERATION AND TRANSMISSION SYSTEM		*	-								•	-		-	-		-
£1 : ESSS	STATION SERVICE SYSTEM		>-	*	*	tere.		*	•				-	•	*	-		
13	CONTAINMENT ISOLATION SYSTEM	-	-			*							-		-	-	-	
£	FEEDWATER CONTROL SYSTEM (11C)	*	*					*			•		-		-	-		*
64 FIDS	FIXED INCOME DETECTION SYSTEM	-		*	•			*			•		-		-	-		-
#1 : sp	LEAR MONITORING SYSTEM	•		-							*	-		-	-			
86   11.05	MONABLE INCORE DETECTION SYSTEM			-										-	-	-		
48K 19	NOMFETURE VALVE SYSTEM	*	-	-	>-			*		•		*	-	-	•	-		
	NUCLEAR INSTRUMENTATION SYSTEM	-	-			-			•			*			-		*	*
M84 5 69	PROCESS RADIATION MONITORING SYSTEM			*														+
. O.	RADIATION MONITORING SYSTEM	2-	*	-	*		*				*			*	*			*
71   RCS	REACTOR CONTROL SYSTEM	-	*	-				*		•	•							*
72 RPS	REACTOR PROTECTION SYSTEM	*	-	*	-	-				•					*		*	
13   5905	SAFETY PARAMETER DISPLAY SYSTEM	*	*	-		*				*	•			-		2222		•
53 . 1/	SECURITY SYSTEM	×	*	æ							*	•			*	*		-
16 . 66	"没有有遗憾",有想会在这些有效的,我们是我们也不知识的,我们也不是我们的,我们也没有我们的最后,我有一个,我们们们们们们们们们们们们们们们们们们们们们们们们们们们们们们们们们们们们	-	-	- Demand	-		1						-					

### ATTACHMENT C VARKEE ATONIC ELECTRIC COMPANY TWPS LICENSE REWEWAL PROJECT STEP 14 REVIEW RESULTS

	100
	PLANT
ŀ	53
	THEIR
	CO. TR
	#ICH
	SYSTEM/STRUCTURES

1   1   1   1   1   1   1   1   1   1									LICENSING	THE BASTS	52									5	SYSTEM/
Fig.   Control of State   Fig.   Fi	RECORD			SAFETY	1 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	SPECS.			*****		1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	13.00	# 8 d	8		# 9 M	S12 840	- O - O	8 = 8		PLEASE OF THE PERSON OF T
15   15   15   15   15   15   15   15	903	, L		-		-		11		1		•	•	-		•	•	-	-	ļ	
15   15   15   15   15   15   15   15	11	5.	ENVIRONMENTAL SYSTEM	•	•								•	•	•	-	-	-			
15   100	500	351	TECHNICAL SUPPORT CENTER SYSTEM	•			•						*	•		*			4		
15   Communication and commu	12	88	ADMINISTRATION BUILDING	•							- * *			•	•						
CF   COMPACTION ROUNDS	527	80.00	BATTESY ROOM NO. 3 BUTLOINE	•				*				*	*	-	•	-					
FE   CONTINUENT DE NOME   FE   FE   CONTINUE	-	61.9	CAMERA AND LIGHTING POLES	•	*									-	•	•					
Fig.	82	8	COMPACTOR BUILDING	•				*				*		*		•	•	-			
FINE   FRICE RANDON STORY   FINE	(F) (60)	35	DECONTANTANTION ROOMS								*	*	*	*	•						
Fig.   ENDITIONS ON THE SUPPOSITE   Fig.	*	850	DIESEL GENERATOR BUILDING	*	*						**	*	>	*	•	•	-			::::	
FIRE FREE AND GATES	55	52	EQUIPMENT AND PIPE SUPPORTS	34-	*						*	*	*	*	<b>3</b>	*	•	*	,		
THEN   FIRE MAIR PURPHOUSE	W3	FAG	FENCE AND GATES	•							*	*	*	•	•		•				
FINE FORMANTONS FOR OUTDOOR NAKSSTACKS FORM FUEL DIL TRANSFER DUMP HOUSE FTCS FUEL TRANSFER DUMP	P	788	FIELD FABRICATED TANKS	-		*								*	•	-					-
FOR FUEL TRANSFER PURP HOUSE TAXASSTACES  FILS FUEL TRANSFER PURP HOUSE  F	60	2	FIRE MATER PURPHOUSE	•										*	•	*	•	-		::::	
FOUR FUEL OIL TRANSFER PHUF HOUSE  FIG.  FUEL TRANSFER CRUIT STRUCTURE  FUEL TRANSFER CRUIT STRUCTURE  FUEL TRANSFER CRUIT STRUCT  FUEL TRANSF	22	F08	FOUNDATIONS FOR DUIDOOR TANKSESTACKS	•						•	*	*	•		•	•	-			::::	
FICE   FUEL TRANSFER CAUTE STRUCTURE	200	FOTA	FUEL DIL TRANSFER PUND HOUSE	•									•	•	•	-	•	-			
CHANCES   CATEMOUSE   CHANCE PIT	150	17.05	FUEL TRANSFER CHUTE STRUCTURE	•											•	*	•	*			
HENSE   HEATTHG BOLLER VERT STACK   IEP   TON EXCHANGE PIT	125	8	GATEROUSE	•							*		•	•		-					
IFF   10% ETCHANGE PIT	122	MB4S	HEATING BOILER VENT STACK	•								*	•	•	•	•	•				
LHE   LIFTING AND MOISTING EQUIPMENT	35	431	TON ETCHANGE PIT		*	-									•	*		*	,		
	503 693	害	LIFTING AND HOISTING EQUIPMENT	•	*							*			•	•		*			*
NEUS NOM ESSENTIAL UPS BUILDING NO. 1 N N N N N N N N N N N N N N N N N N	22		METEOROLOGICAL TOWER	*		*-						*		*	•	•	•				
NEUS NOM ESSENTIAL UPS BUILDING NO. 1 N.	# P	858	NEW FUEL WALLT	•						•			*	*		•					
PCAT PCA STORMOR BUILDING NO. 1	98	WEUS	NOW ESSENTIAL UPS BUTIDING	•	*						*	*		*	•	•	•			****	
POLE POLISTONISE BUILDING NO.	60 60	1001		*									*			•	•			1111	
	100		PCA STORAGE BUILDING NO.	*	*	*					*	*	*					*			

### VANAEE ATOMIC ELECTRIC COMPANY TAPS LICENSE REMENAL PROJECT COLO NA DECITA DE COLO.

CASS
187 14 61
4
150
1
ä
CONTR
STIES.
SYSTEM/STRUCTURES BUTCH CONTRIBUTE
SYSTEM

								TICE	CENSING B	BASIS							-	::::	5	SYSTEM!
RECORD	SYSTEM CODE	RECORD SYSTEM SYSTEM/STRUCTURE SYSTEM/STRUCTURE	Safe T	15 45 55 55 55 55 55 55 55 55 55 55 55 55	29ECS	ERVIR QUAL	8 66	18 18	SE15#11C M	HEAVY II	14.000	24.0 24.0 24.0 24.0 24.0 24.0 24.0 24.0	<b>B B</b>		# 68 H	2 1 2 1 2 1 2 1 2 1 2 1 2 1 2 1 2 1 2 1		03 <b>≈</b> 86	B 2 3 5	STRUCTURE CONTRIBUTED TO PLANT SAFETY (STEP 10)
101	PCM	PC# ##REHOUSE	•	*	*		-							*	•		•		::::	
102	80%	PLANT MODULAR OFFICE BUILDING	•	*				-		*	121								::::	
103	82	POLE BARK	•	•			*	*								•	*			
101	88	PRIMARY AUTILIARY BUILDING	•	•	*		-	-	-	*	*	41		*		•				
105	PYS	PRIMARY VENT STACK	•	*	*				-				-				*			
90:	855	REACTOR SUPPORT STRUCTURE	•		-															-
191	SEE	S L.E. DIESEL GENERATOR BUILDING	•		*									-			*			
108	8888	SAFE SHUTDOWN SYSTEM BUILDING	•	*				*									*			-
103	35	SCREENWELL HOUSE			*		-				*					•	*			
116	Ð,	SEAL PIT	•	•												*	•			
E	Shrs	SECONDARY PLANT VENT STACK	•	-					-				*		•		*		111	
112	53	SERVICE BUILDING	*					*												
en T	d 35	SPENT FUEL PIT	•	-	-					*						•	٠			-
=	SFSS	STEAM AND FEEDWATER SUPPORT STRUCTURE					2-		*						•		*			-
W1	ST-8	STORES MAREHOUSE	•	-				-								•				-
, uo	SETE	SUPPORTS FOR ELECT/I+C EQUIPMENT	-	-			•		3-							•	*			
113	SYS	SMITCH YARD STRUCTURE	*	-	*										-	•	-			-
60	148	TRAINING AREA BUILDINGS	•	•													•		::::	
119	TAS	TRANSFORMER AREA STRUCTURE	•					-									*		::::	
128	<b>g</b> 0	TURBINE BUILDING	•				*		*		30-					•	*		-111	-
121	ž	HAPOR CONTAINER		-				-								•	-		::::	
221	WEI.	NC ELEVATOR ENCLOSURE							-							•		,		
123	808	MASTE DISPOSAL BUILDING	•	*			•				*			*		•	*		::::	-
124	THES	MARD AREA CRAME SUPPORT STRUCTURE		*					» · · · ·		*			*					::::	
		医中央性性 医电子 医中央性性 化甲基丁烷基 医髓 医沙丘氏管 医大大性 建设计学 医医生物 医乳球菌素	10	-			-	-	-	-	-	-	-	-	-	-	-	S. S. Services	-	-

### ATTACHMENT D

STEP 16 REVIEW RESULTS

SYSTEMS AND STRUCTURES
FOR WHICH DEGRADATION IS SIGNIFICANT TO PLANT SAFETY

	12 10 49			25 POTENTIALLY STORIFTON	#1 19 PLD#	3#(III	w.	SC2111	*11.4		3	-		97 97 97 97 97 97 97 97 97 97 97 97 97 9
## ### ###############################	F1C589	SYSTEM	ER SYSTEM/STEW.TURE		RAD RELEASE LINITS EXCEDED	MAIN (BB). OR NY ROYDORY LEMENCY		2 S 180			981s199 9 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	 	METARE MESES ICHTFICKET STER	
SE DOUILE FEB 575788  CHARGING SPEINS  CHARGING SPEINS  CONTRESSED ALS STSTEM  CONTRESSED A		2			٠	•	•	•				 		•
15	1	¥	DIVILIBRY STEAM SYSTEM		٠	•		•				 ****		•
CONTRIBUTION STATEM CONTRI	***	*	BOILER FEED SYSTEM	*		٠	•	*	*		•			
CONTRIBUTION SYSTEM  CONTRIBUTION SYSTEM  CONTRIBUTION STATE SYSTEM  CONTRIBUTION STAM SYSTEM  CONTRIBUTION STATEM  CONTRIBUTIO		*	CHARGING AND VOLUME CONTROL SYSTEM			٠	*	*				 		
CG COMPRESSED AIR SYSTEM  CG COMPRESSED AIR SYSTEM  ESS ENTRACTION STEAM SYSTEM  FO FILED CHECKING MAD SUDPRESSIDE SYSTEM  FO FILED CHECKING MAD SUDPRESSIDE SYSTEM  FO FILED CHECKING MAD SUDPRESSIDE SYSTEM  FO FILED CHECKING STEAM SYSTEM  FO FILED CHECKING MAD SUDPRESSIDE SYSTEM  FO FILED CHECKING STEAM SYSTEM  FO FILED CHECKING MAD SUDPRESSIDE SYSTEM  FO FILED CHECKING STEAM SYSTEM  FO FILED CHECKING STEAM SYSTEM  FO FILED CHIRCLE SYSTEM  FOR FILED SYSTEM  FOR FILED CHIRCLE SYSTEM  FOR FILED CHI	100	23	CHEMICAL SHUTDOWN SYSTEM		•	•	*	*	•	٠				•
CA CONFRESED AIR SYSTEM  CA CONFRESED AIR SYSTEM  EST (MEDGEN VOILER FED SYSTEM  FS FIRE DETECTION SYSTEM  FIRE DETECTION SYSTEM  FIRE DETECTION SYSTEM  FS FIRE DETECTION SYSTEM  FIRE DETECTION SY			CIRCULATING MAIER SYSTER		•			٠	*			 		•
CA CONCRESSED AIR STSTEM  ESS (MERCINCY BOLLER TEED STSTEM  ESS (MERCINCY BOLLER TEED STSTEM  FO FIGUR ORGINACE STSTEM  GG GENERALIZED STSTEM  FO FIGUR ORGINACE STSTEM  FO FIGUR ORGINACE STSTEM  FO FIGUR ORGINACE STSTEM  FO FIGUR ORGINACE STSTEM  FO FIGUR STSTE	-	×	COMPONENT CODILING MATER STSTEM		•	٠			*		•	 		
ESS ENTRACTION STEAM SYSTEM  ESS ENTRACTION STEAM SYSTEM  FO FLOED DOMINAGE SYSTEM  FO FUEL DELECTION AND SUPPRESSION SYSTEM  FO FUER DELECTION AND STEAM SYSTEM  FO FUER DELECTION AND STEAM SYSTEM  FO FUER DELECTION AND SELLET SYSTEM  FO FUER SYSTEM  FO FUER SYSTEM  FO FUEL SYSTEM  FO FU		5	COMPRESSED AIR SYSTEM		•		•	•	*	*		 		
ES EXTRACTION STEAM SYSTEM  FO FILOR ORATINGE SYSTEM  FO FILOR ORATINGE SYSTEM  FO FILOR ORATINGE SYSTEM  FO FILOR ORATINGE SYSTEM  FO FILOR ORATING SYSTEM  FO FILOR SYSTEM  FO FILOR SYSTEM  FO FILOR SYSTEM  FO FILOR ORATING SYSTEM  FO FILOR SYSTEM  FOR FILOR SYSTE	e		DEMINERALIZED MATER STSTER		•			•				* * * *		
FS FINE DETECTION STEAM SYSTEM FD FLOOR DARRINGE STSTEM FD FLOOR DARRING S	0	æ	EMERGEMENT BOTLES TEED STSTEM	٠	•	*		•	*					•
	=	£	ENTRACTION STEAM SYSTEM	٠		•		•						٠
	64	22	FIRE DETECTION AND SUPPRESSION SYSTEM		•	•				*		 		٠
	100	62	FLOOR DRAIMAGE STSTEM	*	•			*	٠		•			•
********		0,	FUEL DIL SYSTEM	*	٠	•		*	*			 		
	13	s	CEMERATUR GAS		•				٠	٠				
5 # 2 # # # # # E	*	23	GENERATOR SEAL DIL SYSTEM		•	•			٠	•	•			
# 2 # # # # # # #	2	¥CI	HEALING STR/CONDERSATE	***	*				•	*				
2 2 2 2 2 2 2		£	MYDROGEN VENTING SYSTEM			٠			٠	•		 ****		
F F F F F E	P.	97	LUGRICATING DIL SYSTEM		•	•		•	•		*			
8 8 2 E	22	¥	MAIN COOLANT STSTEN		*	*			٠	٠	*	 		
v z a z	12	¥	MAIN STEAM STSTEM		*			•	*		*	 •		
2 8 2	12		*ITROGER SYSTEM		*	•			*	٠	•			
R E	10	ż	POTABLE BATER SYSTEM	*	٠	•			*	٠	٠			٠
2	*	R	PRESSURE COMINDE AND RELIEF SYSTEM	*	*	*		*	*	٠				*
	10	E	PURST MEANING STORES	*	*				٠	٠		***		

ARKEE ATOMIC ELECTRIC COMPARY THES LICENSE REMEMA PROJECT ATTACHMENT D

SYSTEMS/STRUCTURES FOR WHICH DESPRISATION STAF IS MENTER RESULTS

IS POTENTIALLY SECREFICANT TO PLANE SAFETY

10/31/89

10 38 58

82

10

EUP SAFETY FORCTIONS

DECOMPATION OF EVSTEN OR STRUCTURE POTENTIALLY SIGNIFICANT TO PLANT SAFETY ISTED 16. CONTAINMENT SUBCRITICALITY \* 200 SMC 1000 3MC . 5,5 WE BOOMDARY MAJE COOK 1544451 \* \* \* . 8 (INITS \$1C51868 #E : 5 # 35 . SYSTEM/STRUCTURE CONTRIBUTES 10 PLANT SASETY | #1 4315| \* \* AIR DISPOSAL (FILTERED ERMANST) SYSTEM VC HEATING, COOLING, AIR RECIPCULATION SAFETY INJECTION BLDG WENTLATION STS BATTERY ROOMS 1+2 WENTILATION SYSTEM BATTERY ROOM HOS VENTILATION SYSTEM GENERATION AND TRANSMISSION SYSTEM RADIGACTIVE WASTE DISPOSAL SYSTEM MPY ENCLOSURE VENTILATION SYSTEM EDG BUILDING VENTILATION SYSTEM CONTROL POOM VENTILATION SYSTEM TURBINE BUDG VENTILATION SYSTEM CONTAINMENT ISOLATION SYSTEM STSTEM/STRUCTURE TURBINE GENERATOR SYSTEM DIESEL GEMERALDA SYSTEM SAFETY INJECTION SYSTEM SHUTDOWN COOLING SYSTEM EMERGENCY POWER SPSTEM STATION SEPATOR SYSTEM DC DISTRIBUTION SYSTEM WENT AND DRAIN SYSTEM SERVICE NATER SYSTEM SAFE SHUTDOWN SYSTEM SPERT FUEL SYSTEM REFUELING SYSTEM SAMPLE SYSTEM **WCHCR** 5153 £522 5433 9K19 HC11 HC12 HCS HC5 HC1 × 얆 222 6 2 23 35 10 0 25 35

32

100 \*

32

1 100 gr: 9 = 17 13 25

\* -69

#3 # 10 MARKEE ATOMIC ELECTRIC CONPON MAPS ELECTRICE REMEMBE PROJECT STIRE & BEWIE # 1917

IS POTENTIALLY SIGNIFICANT TO PLANT SAFETY SYSTEMS/STRUCTURES FOR MHICH DEGRADATION

10/11/80

12 \*

EUP SAFETY FUNCTIONS

DECAMBATION OF STREET OF STRUCTURE POTENTIALLY STEWNSTOWNS TO PLANT (4) 4312) HIJES SIGNIFICANT -T35136 THE MINERS THIS CALLY 509CR171CAL177 \* CORE COO: 1863 WE BOSMEDARY EDRAGE! @HELETEDED #F. FASE LINETS SYSTEM/STRUCTURE COMPRESSITES 19 PLANT SAFETY (5717) FOUNDATIONS FOR DUTDOOR TANESASTACES PROCESS BADIATION MONITORING SYSTEM MPSR CONTAINER MONITORING SYSSEN LIFTING AND ADISTING EQUITMENT MOVABLE INCOME DETECTION SYSTEM MUCLEAR INSTRUMENTATION SYSTEM FUEL TRANSFER CAUTE STRUCTURE FEEDMATER CONTROL SYSTEM (18C) FUEL DIL TRANSFER PUND HOUSE FIXED INCOME DETECTION SYSTEM SYSTEM/STRUCTURE STRUCKET OND PIPE SUPPRINTS BATTERY ROOM #9. 3 BUILDING RADIATION NORTTORING SYSTEM DIESEL GENERATOR BUTLDING REACTOR PROTECTION SYSTEM FIELD FABRICATED TANKS REACTOR CONTROL SYSTEM LEAR MONITORING SYSTEM ROMFETURM VALVE SYSTEM METEGROLDGICAL 19869 ENVIRONMENTAL SYSTEM FIRE MATER PURPHBUSE COMPACTOR SUILDING TON ENGHANCE PT SECURITY SYSTEM #101 FTCS 431 1 8 \* 8 . \* -E 2 12 10 49 69 \*\* 29 65 3 RECORD 3 2

TANKER ATOMIC ELECTRIC COMPONY THE LICENSE REMEMBER PROJECT STEP IS MATER RESILTS

IS POTENTIALLY SECREFICANT TO PLANT SAFETY STSTEMS/STRUCTURES FOR MITCH DEGREENING

RECORD

2

20

2 8 æ 60 100

EBF SAFETY FIRETIBAS

DECEMBRATION OF SYSTEM OF STRUCTURE POTENTIALLY THE OF THE PARTY. SMEETY (STES IN) Significant SYSTEM (Dala) and PRINCETTY 20 SUBCRITICALITY COME COOL 1845 1年 - 新新 計画 60 N: 表の第2番の数7 1.00 m. Sei 145 ENCETERED 1 28175 SYSTEM/STRUCTURE CONTRIBUTES TO PLANT SAFETY (\$169 19) \* STEAM AND SEEDMATER SUPPORT STRUCTURE MARD AREA CRAME SUPPORT STRUCTURE SUPPORTS FOR ELECT/TAC EQUIPMENT S. L. E. DIESEL GENERATOR BUTTDING SAFE SAUTONIN SYSTEM BUILDING PLANT MOBULAS OFFICE BUILDING SYSTER/STRUCTURE TRANSFORMER AREA STRUCTURE SEEDMOARY PLANT WENT STACK PRIMARY AUXILIANT BUILDING REACTOR SUPPORT STRUCTURE masti bisposal autubles WE ELEMATOR ENCLOSINE SMITCH YARD STRUCTURE PRIMARY VENT STACE TURBINE BUTIDING SERVICE BUTIDING STORES WARENDUSE VAPOR CONTAINER SCREENMELL MOUSE Spint futt pit HER FUEL WANET YACS +15 \$115 SAGS 57.55 21.50 STS \* 145 455 134 CODE \*\* 955 . 8 788 5 ä 10/10/80

8

ë 16 P

-88

\* 83 2 7 1 8

### ATTACHMENT E SAFETY INJECTION SYSTEM COMPONENT REVIEW RESULTS

## SECTIONS THE PROBLEM CONTRACT STREET STREET

Column   C							22.484.58			-	21.01.0			33.00	-
							SAPERATE STATES	STATE OF THE STATE	*****	0.000000 0.000000000000000000000000000		SAFETY SPECIAL SOUR SOUR SOUR	CRUST TO A STREET	ACTORISE ACTORISE COLUMN INCLUMENTO ACTORISE ACTORISE	FINANCE PROPERTY.
1004, Autoritate restriction   1		CODE	98504197168		381 411	CHARGE	100					2			
1814, 1000 For 19-13 section, series   1.5   1		3	1501. TALVE FOR P-49-3 MICHE.	1608			115	18						•	
1911, NOTE THE PERFECT   1911   1911   1912   1912   1913   1914   1915   1914   1915   1914   1915   1914   1915   191			1505. VALVE FOR P-49-2 MECINC.	1006		-	E	122		¥			E		
Fig. 1   F		7	1501, WALVE FOR P-49-1 MECIAC.	1608	-		18	182					Đ		
First bolidary   First   Fir			RPSI-3 RECIRC			2614	12	22	¥				Ħ		
1915   1917   1915		1	PPSI-2 RECIBE			1014	165	185					1		
1504, NAME FOR FOLIA CENT.   1			MFSI-1 RECIRC			2614	2	185		2			185		
1504, NAME FOR FOLD LEGITIC MOTT   1   155   155   15   15   15   15		1	MPS: PUMP MECINE NOR			FIR	SE SE	9			ä		182		
1504, NATE PARTECLE, 1807   1   155   155   150   17			ISOL. MALVE POR BPSI RECIEC. L.	108			18	34			•		185		
1901, NAME FOR FALL MOTION.   1			1504. VALVE POR P-48-3 MC18C.	1608			183	2					2		
1501, NUMER FOR FACE   1501   1   151		1	1501. VALVE FOR P-48-2 ERCIEC.	100	-		¥	1155	*			8	=		
1592, Nation rate state of the content of the con		150	150L. MAN FOR P-45-1 DECIRE.	1008			183	282	8				=		
1501, NUMBERS SELECTED   1607   1   155   155   150		15	161 12.1	1608			25	2					2		***************************************
CHOS SEPTUT TO LYST WHERE   FINAL SECTION STATES COME WAS I LAND STATES COME WAS INCOME WAS IN		15	150L. WALNE FOR ST-LT-401	1608			E S	all s			•		2	•	
Fight, square particular and the state of	-	\$1	CWCS 5977LF TO LPS! ERR			*	185	35							
PERSON NUMBER POR SET FLAS         PORTION SET FLAS         FERRE SET FLAS		Į,	ISOL. WALVE PROM BORIC ACID TR	1606		•	18	185		£			P		
PRESS ST-607-515         PRESS ST-607-515         PRESS ST-607-515         PRESS COME, REST LANGE 2		15	STPASS VALVE FOR SI-FI-5	1608			18	15					2		
PARES. CORE. PEST LAND 2         PARES. PARES. CORE. PEST LAND 2         PARES. PARES. CORE. PER PARES. CORE. PARES. PARES. PARES. PARES. PARES. PARES. CORE. PARES. PARES. PARES. PARES. PARES. PARES. P		175	917455 SI-#04-515	and the same		8414	12	113					2		
PRESS. CORE. PEST LARGE I.         PRESS. CORE. PEST LARGE II         PRESS. CORE. PEST LARGE II <th< td=""><td></td><td>100</td><td>PRESS. COME. 8751 UNOP 3</td><td>100</td><td></td><td></td><td>112</td><td>185</td><td></td><td></td><td></td><td></td><td>P</td><td></td><td></td></th<>		100	PRESS. COME. 8751 UNOP 3	100			112	185					P		
PMSSS. CORE. #F81 LOOP 1         F007         F         F155		15	PERSS. COMB. #PSI LIGOP 2	1010			E	122	2		*		E	•	
PAREST, CORE, EVEL LOOP 1         PA		N	PRESS. COMM. \$PST LOGP :	100			18	185					£		
PARTICIDATE FOR F-45-1         ROST         T         TGS		15	PRESS. COMM. 8PS1 LOOP 4	\$004			E	22			2		¥		
DESCRIPTION FOR FACE AND TOTAL		\$1	DEALS FALVE FOR P-49-3	\$000			185	185		2			2		
TOTAL SALES FOR FACT AND FOR		25	DEAST WALVE PIR P-49-2	\$697	-		2	185							-
1501, Mills For 1855 Life 2017 9 195		15	DEKIN TALVE POR 7-45-1	Roge			182	18	£				183		
		13	1501, 94036 FOR PaSS LINE	16.00			195	848					<b>H</b>		

68/12/61

# TANGER ATOMIC ELECTRIC COMPART THPS LICENSE REMEMBL PROJECT SAFETT INJECTION SYSTEM PLUID COMPONENT REVIEW RESULTS

	N SOFPLY LES KOOF N SOFFLY LES			MARTINES FORD  9 : PRES FORD  9 : OPERATION  18 : 9 1  1	CORPORATE TO SELECT TO SEL	THE STATE OF THE S		201210	
	5 5 5 5 5 5 5 T								
21.12 20.23 21.12 21.13		E E E . E E							
		E E . E E			2 P P 2 2 2		P P P P P P		
202-2 202-2 202-4 202-3 21-22 21-22 21-22 21-22 21-22 21-22 21-22 21-22 21-23 21-23 21-24			B		P P & & &				
502-14 SI					9 2 2 2		P P P P P		
20 1		. E E . E E	B	B			2 2 2 2		
		EE-EE	<b>F B B B B</b>	8 8 8 8 8 8 8 8			2 2 2		
	21.0	E.EE	E	2 2 2			<b>P P</b>		
	1 1 1	- E E	B B B B	75 75 8 8	日本の日本の日本の日本の日本の日本の日本の日本の日本の日本の日本の日本の日本の日				
		E E	p	13 13	•	4	· · · · · · · · · · · · · · · · · · ·	-	
		E	B B		P	2	¥	•	
		· · · · · · · · · · · · · · · · · · ·	TES.	TRS #0		2	2		
u u u u u u	电聚偶热 医埃德霉属 法医院法院 电分音电影 医溶液管 医皮肤	9118		785 80	¥		2	8	
US US US US US		1414	£	715 m	<b>3</b>	2	#		
u u u u		8414	9	185 B	25		#	•	
15 15 15 15 15 15 15 15 15 15 15 15 15 1		FIPE	18	15 15 15 15 15 15 15 15 15 15 15 15 15 1	2		188		
10 10 10 10 10 10 10 10 10 10 10 10 10 1	150L. VALVE FOR 51-80F-1 87FAS 80FT		¥	. SI					
Ü	1004		2	SH SH		•	¥		
		Edid		#55 <b>8</b> 0					
SI -9-0553 SI CHECE VALVE FOR LPSI LIGHT I	1 1000 1 9050	5	182	785 185	182	21	=		
51 * * * * * * * * * * * * * * * * * * *	1 1,007 4 8087	₽.	185	TRS TRS	183	. TE	12		
SI-V-0035 SI CRECE VALUE FOR SPSI READER	I BEADER RODT	***	12	185 185	182	8. 27.	ā	•	
21 - 4-0645 SE CRECE WALKE FOR LPSI LOOP 3	1 1009 1 8001	<b>#</b> 5	ž	<b>B</b>	2	£ .	2	•	
SI THEOREM SI CHROS WALNE FOR LIFST LAND 2	1 LAOF 2 8057	8	15	75 TE	183	21	Ħ		
01-54-15 NO SET ME A 1980 15	PS 10 810T	٠	16	. SE	*	•	¥	•	
SI V-0735 SI 1500, WASHE FOR SI-PI-31	FI-31 200T		185				12		
51 V 0775.	10.14	g+	\$44.5	192 (6)	*		588	á	

## SAPETT INJECTION STSTEM FLUIS CURPOREST REVIEW RESULTS

18th			STEP 26			82 4MS			
1501   March Polisier   151   March Polisie	6	**********	***********	24 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -	08 182901 08 182901 08 182901 1 18031	CONFORMATION AND AND AND AND AND AND AND AND AND AN	200000 2000000 20000000000000000000000	FOTOTIAL ESS PECADATION PETALETRIS INCETIFIED (STOP EC)	Maria Maria
10   10   10   10   10   10   10   10	108		185	1 S	£		2		
St.   Parks Sales For St. P. 1905   V   First   Firs	<ul><li>・ できる できる できる できる できる できる できる できる できる できる</li></ul>	E.	YRS	9 59	185	2	2	•	
1501, 14,154 FOR 51-7-14   10007   1   155   1	100		2		•	•	2		
10   1904, WALNE FOR SELPT-34   10007   1   1155   1755			185	e 59	•		2		
	1968		183				2		
State   Strike   St			185	785 185	185	22.	2		
SI   VENUE DISCRIPTO   PERI   PROPER			185				E		
	化化甘蔗香油 医原库特 医有骨 化电压管 医医电流管 医腹膜 医医腹膜	841	18S	725	165		2		
SI   LPSI DISCR TO RPSI   PODT   P   PS   PS			185	185 m			P		
SI   VORT VALUE POR P - 48-1   PODT   P   TSS   TSS     SI   SECTION ALTER POR PC SURP DISCORA BODT   P   TSS   TSS     SI   CRECT VALUE LPSI DISCORAGE TO BODT   CHR   TSS   TSS     SI   CRECT VALUE LPSI BIRE   BODT   P   TRS   TSS     SI   VORT COMM. LPSI BIRE   BODT   P   TRS   TSS     SI   VORT VALUE POR SI - TT - 10   BODT   P   TSS   TSS     SI   CSURP DISCORAGE TO BODT   P   TSS   TSS     SI   CSURP DISCORAGE TO BODT   P   TSS   TSS     SI   PORATO POR SI - TT - 10   BODT   P   TSS   TSS     SI   FLOW BLANCA TOR SI - PI - LE ARD S   BODT   TSS   TSS     SI   RADIA VALVE POR SI - PI - LE ARD S   BODT   TSS   TSS     SI   RADIA VALVE POR SI - PI - LE ARD S   TSS     SI   RADIA VALVE POR SI - PI - LE ARD S   TSS     SI   RADIA VALVE POR SI - PI - LE ARD S   TSS     SI   RADIA VALVE POR SI - PI - LE ARD S   TSS     SI   RADIA VALVE POR SI - PI - LE ARD S   TSS     SI   TAON BLANKET POR SI - PI - LE ARD S   TSS     SI   TAON BLANKET POR SI - PI - LE ARD S   TSS     SI   TAON BLANKET POR SI - PI - LE ARD S   TSS     SI   TAON BLANKET POR SI - PI - LE ARD S   TSS     SI   TAON BLANKET POR SI - PI - LE ARD S   TSS     SI   TAON BLANKET POR SI - PI - LE ARD S   TSS     SI   TAON BLANKET POR SI - PI - LE ARD S   TSS     SI   TAON BLANKET POR SI - PI - LE ARD S   TSS     SI   TAON BLANKET POR SI - PI - LE ARD S   TSS     SI   TAON BLANKET POR SI - PI - LE ARD S     SI   TAON BLANKET POR SI - PI - LE ARD S     SI   TAON BLANKET POR SI - PI - LE ARD S     SI   TSS   TSS     SI   TSS   TSS   TSS     SI   TSS   TSS   TSS     SI   TSS   TSS   TSS     SI   TSS   TSS   TSS   TSS     SI   TSS   TSS   TSS   TSS   TSS     SI   TSS   TSS   TSS   TSS   TSS   TSS   TSS   T	· 正是 · · · · · · · · · · · · · · · · · ·	361	185	185 80	2		2	•	
SI   1801. PALVE POR PC STUD DISCLARED BY PORT   F   TES   TES			185	<b>1</b>	•		2	•	
SI   1801. VALUE POI VC SWEP DISCIA BODT   V   TES   TES			185		•	2	2		
SI CHECT VALVE LPSI DISCRARGE TO 400T CHE TES TES  SI VEST COME. LPSI PINE 1000T T CAVITT  SI LPSI (APPE POWES SUPIL 1.3 100PT T TES TES  SI VEST VALVE POR SI-T1-10 100PT T TES TES  SI VEST VALVE POR SI-T1-10 100PT T TES TES  SI PERIN PALVE POR SI-T1-10 100PT TES TES  SI PERIN PARVE POR SI-T1-10 100PT T TES TES  SI PERIN PARVE POR SI-T1-10 100PT T TES TES  SI PERIN PARVE POR SI-T1-10 100PT T TES TES  SI PERIN PARVE POR SI-T1-10 100PT T TES TES  SI PERIN PARVE POR SI-T1-10 100PT T TES TES  SI PERIN PARVE POR SI-T1-10 100PT T TES TES  SI PERIN PARVE POR SI-T1-10 100PT T TES TES  SI PERIN PARVE POR SI-T1-10 100PT T TES TES  SI PERIN PARVE POR SI-T1-10 100PT T TES TES  SI PERIN PARVE POR SI-T1-10 100PT TES TES  SI PERIN PARVE POR SI-T1-10 100PT T TES TES  SI PERIN PARVE POR SI-T1-10 100PT T TES TES  SI PERIN PARVE POR SI-T1-10 100PT T TES TES TES  SI PERIN PARVE POR SI-T1-10 100PT T TES TES TES  SI PERIN PARVE POR SI-T1-10 100PT T TES TES TES TES TES TES T	PISCE BODT		183	185	•	2	2	•	
SI         RECIEC TO SHIRLD TE CANITY         FIPR         FES         TES           SI         VEST CORD. LPSI BINE         BODT         F         TES         TES           SI         LPSI LES BINE         BODT         F         TES         TES           SI         VEST VALVE FOR SI - LI - J         BODT         F         TES         TES           SI         VEST VALVE FOR SI - FI - LD         BODT         F         TES         TES           SI         VEST VALVE FOR SI - FI - LD         BODT         F         TES         TES           SI         VEST VALVE FOR SI - FI - LD         BODT         F         TES         TES           SI         VEST VALVE FOR SI - FI - LD         BODT         F         TES         TES           SI         VEST VALVE FOR SI - FI - LD AND SI - TES         TES         TES         TES           SI         RASI VALVE FOR SI - FI - LD AND SI - TES AND SI - TES         TES         TES         TES           SI         RASI VALVE FOR SI - FI - LD AND SI - TES AND SI - TES         TES         TES         TES           SI         RASI VALVE FOR SI - FI - LD AND SI - TES AND SI - TES         TES         TES         TES			145	5 E	18		2	•	
SI 1/81/44/55 FOURS SUPL.  SI 1/751/44/55 FOURS SUPL.  SUPL.  SUPL.  SUPL.  SUPL.  SUP	化二甲基苯甲二甲甲基苯基苯甲基苯甲甲甲甲甲甲甲甲甲甲甲甲甲甲甲甲甲甲甲甲甲甲甲甲	24	185		•	8	2		
SI LPSI/APSI POWES SUPIL  SI URBI MALVE POR SI-LI-3 RODE 9 755  SI ORAJE PALVE POR SI-FT-10 RODE 9 755  SI PC SUMP DISCLARCE 7 755  SI PRAIN WALVE POR SI-PI-12 AND S RODE 9 7 755  SI RPSI NA POR 1 784 ROR 1 784 ROR 7 785  SI PLOW BLANCHT-LOOP I 184 ROR 7 785	1608		182	185 -	18	8	2		
SST 1474 FOR SI-LI-13 1009 7 9 755 755 755 755 755 755 755 755 75	化克勒氏 医电子工 化次 医医氏皮肤 医皮肤 医皮肤 医虫虫 医甲状腺 医皮肤		155	155 8	E	•	2	•	
SE UNINE FOR SI-FI-10 RODE	1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	173	2	e 51	B	2		•	
SE 14 SE PESSONAGE POR SI-PT-10 BODT P 123 SE-14 SE PESSONAGE POR SI-PT-12 AND S RODT P 185 SE PESSONAGE POR SI-PT-12 AND S RODT P 185 SE PESSONAGE POR SI-PT-12 AND S RODT P 185 SE PESSONAGE POR SI-PT-10 BODT P 185 SE PESSONAGE P 185 SE	100		2	185 85	•	•	2	•	
ST PC SWEP DISCLARGE SI DRAIM WALKE POR SI-PI-12 AND S ROOT T TES SI RPSI INJ BOR SI PLOW BLEMBYT-LOOP I INJ RDR			p	12 E	•	2	2	•	
SI DAAIN WALKER FOR SI-FI-12 AND S ROOT T T TES SI RPSI INJ HOR TO FINJ HOR THE SINCE THE TES SI FLOW BLEMENT-LOOP I NAJ HOR		178	2	£	•		2		
SI RPSI INJ BOK TESS TESS SI PLOW ELEMENT-LOOP I INJ RDR	AND S RODT		12	e E	•		#	•	
SET THE PROPERTY LOND I NOT BEEN BOND IN	の 有 は 日 日 日 日 日 日 日 日 日 日 日 日 日 日 日 日 日 日	176	183	165 N	•	•	22	•	
	理 · 有 · 有 · 有 · 有 · 有 · 有 · 有 · 有 · 有 ·	151	12		•	•	2	•	
ON SAL SAL 15M1 15M1 BUR FMI 15G1-1MBM278 MD14 IS		158	181	785 6	2		<b>14</b> 2	•	

A						STRP 24 :			11 411		HE H	
1						********	CORPORET'S SAFET PRESE BOTH PR. : PRESE BOTH	*******	COMPONENT'S EAST PRESTOR PRESENT PRESTOR PRESENT	*********	MOTABLIAN MOTABL	MATERIA TALLANTINA TAL
	9	SYSTE		0	****	(W 48.			 E	П		
		25	FLOW RURSET-LIGOT 2 (BJ. 838			185	TES #0	•	2	2	•	
1   1   1   1   1   1   1   1   1   1	-	II.	1	<b>E</b>	*5	185	183 m	2				
1   10   10   10   10   10   10   10		N	TACS TLOST - LOT + 101 TO		2.5	12		•		21		
1   1   1   1   1   1   1   1   1   1		15	FLOW BLESSET-FLOW TO CWCS		to.	183	155 #6	•		2		
1   1   1   1   1   1   1   1   1   1		iš	FLOW ELEKTRY - 4PS; 181 499		15	183	185	•		2		
1   10   10   10   10   10   10   10		12	FLOW 180-LPSE 183 808		10	785	. SEL	185	8	2		
1   1   1   1   1   1   1   1   1   1		15	PLOW 188-PLOW TO CWCS		15	185	185	E				
TOTAL TIME STATE   1857   185   18	5 -77-0001	15	PLOW TLASS-LOOP 1 (92 898		ts	2	31 31	22	•			
1		15	PLOT TEASS-LPSI IRJ 808		25	22	185 80	18	•	=	•	
1		15	PLOW TEAMS - LAND 2 (M.) 208		15	£	145 80	185			•	
State   Total Tuste   Total Tuste   Total State   Total		51	FLOW TEASS LADY 3 18J 898		151	153	FES 80	¥	2	2		
State		15	FLOR TRASS-1609 4 184 108		15	2	15 B	¥	•	9		
State   From Teach-Prist late   1857   155   1		25	PLOW TRANS. PLOW TO CWCS	£	10	185	165	F	•	2	•	
1		25	PLOW TRANS-RPSI INU MEN	<b>1</b>	15	12	. 21	TES.	2	2		
State   Late   1867   1867   1867   1869		ii.	BICR LEVEL SWITCH-TE-28	=	15	165	185	185	•	2		
State   Letter, 1987   Letter, 1981   Letter, 198		31			15	185	22.	•		2		
State   Livel Settick-ACCOMMUNITOR   1857   1858   1859	11	SI	LEVEL	1	25		185 80		•	22		
State   Living Staticy - License Later   1857   1858   1859   1	10	15	1	1	151	12	382	•	•	2		
St   LOW LOTEL STITCS -TL-211   ST   TSS	24	175	SAWAL SWITCH ACCORDIATOR	-	150	122	785			2		
ST   LIVEL SHITCH-ACCOUNTATION   1857   1858   1859   18	29	31	4		158	12	185 80	•	•	2		
51 LIVEL SHITCH-ACCHRILATOR  51 LIVEL TRUS-TT-28  51 LIVEL TRUS-TT-28  52 LIVEL TRUS-TT-28  53 LIVEL TRUS-TT-28  54 LIVEL TRUS-TT-28  55 LIVEL TRUS-TT-28  56 LIVEL TRUS-TT-28  57 LIVEL TRUS-TT-28  58 LIVEL TRUS-TT-28  59 LIVEL TRUS-TT-28  50 LIVEL TRUS-TT-28  50 LIVEL TRUS-TT-28  51 LIVEL TRUS-TT-28  52 LIVEL TRUS-TT-28  53 LIVEL TRUS-TT-28  54 LIVEL TRUS-TT-28  55 LIVEL TRUS-TT-28  56 LIVEL TRUS-TT-28  57 LIVEL TRUS-TT-28  58 LIVEL TRUS-TT-28  59 LIVEL TRUS-TT-28  50 LIVEL TRUS-TT-28  50 LIVEL TRUS-TT-28  51 LIVEL TRUS-TT-28  52 LIVEL TRUS-TT-28  53 LIVEL TRUS-TT-28  54 LIVEL TRUS-TT-28  55 LIVEL TRUS-TT-28  56 LIVEL TRUS-TT-28  57 LIVEL TRUS-TT-28  58 LIVEL TRUS-TT-28  59 LIVEL TRUS-TT-28  50 LIVEL TRUS-TT-28  50 LIVEL TRUS-TT-28  50 LIVEL TRUS-TT-28  51 LIVEL TRUS-TT-28  51 LIVEL TRUS-TT-28  52 LIVEL TRUS-TT-28  53 LIVEL TRUS-TT-28  54 LIVEL TRUS-TT-28  55 LIVEL TRUS-TT-28  56 LIVEL TRUS-TT-28  57 LIVEL TRUS-TT-28  57 LIVEL TRUS-TT-28  58 LIVEL TRUS-TT-28  59 LIVEL TRUS-TT-28  50 LIVEL TRUS-TT-28  51 LIVEL TRUS-TT-28  52 LIVEL TRUS-TT-28  53 LIVEL TRUS-TT-28  54 LIVEL TRUS-TT-28  55 LIVEL TRUS-TT-28  56 LIVEL TRUS-TT-28  57 LIVEL TRUS-TT-28  57 LIVEL TRUS-TT-28  58 LIVEL TRUS-TT-28  59 LIVEL TRUS-TT-28  50 LIVEL TRUS-TT-28  50 LIVEL TRUS-TT-28  51 LIVEL TRUS-TT-28  5	101	215			151	183	185	•	•	2		
\$1 \( \text{LOTE} \) SHTOR ACCIVALLATION   1857   185   185   187   18		55	1		158	185	185 10		•	P		
21 LEVEL TLANS. 11-28 18-27 18-35 18-38 18	9	215	1		151	185	155			P	•	
St. Laws: Taxon=1783_actrimilativa (SST 1851 FES No No No		ěř.			158	182			•	2	•	***************************************
		15			*5*	12	* 59			24		

					12 4345				STEP 28			34 ALS	
					CORPORARY INDICATES SAFETY FORCETOR		CONFORMATION : PRESS BORNS : PRESS BORNS : OPERAL : PRESS BORNS : OPERAL : THE PRESS : THE	SHUBET TO REPUBLICATION OR INSPECT	200 E	TION ADDRESS. THOS ADDRESS. THESE BORD	Second of Particular In Process	ACT DESCRIPTION ACT DESCRIPTION BECAMINES (DETTITIES (STEP EC)	
TAS NO./EINE NO.	2000	BESCRIPTION	7487 1187	1653			40						
\$1 57-000¢	īs	LEVEL TRAFS-ACCOUNTATION		1881	2	185					2		
51-175-0225	25	LOW TERP SWITCE-TE-28		1383	E	Ð			8	•	P		
81-91-9019	15	PRESSURE 189-8751 18J 808		1881	¥	2	•	21			2		
\$1-60-14	15	PRESSURE (#0-LPS) (#J KDA		181	E	18	•	12			2	•	
51-91-0012		PRESSURE   FO-LPS  DISCR SEADER		1	<b>3</b> 2	五		=	•	•			
\$1-60-14-15	is	PRESSURE 180-8751 DISCH 808		18	SE SE	E		18		8	2		
SI-PI-093E	15	PRESSURE 180-LPS1-1 015CB		182		E				,		*	
11-01-0031	15	PRESSURE 180-8751-1 01508		1581		18	•						
21-00-14-15	15	PRESSURE 180-LPS1-1 018CF		•		113					,		
51-91-9933	15	PEESSURE   100 - 1751 - 2 515CB		1881		Ħ			1				
1600 ld lS	15	PRESSURE (#0-LPS1-3 019CB		181	•	Ħ							
\$1-11-10135	15	PARSSORR 789-8751-3 015CB		1361		18							
9000-14-15	15	72055045 140-LF51 019CF 064001		1824	2	185	8	185			2		
1940-14-15	15	PRESSURE 189-8751 015CE 878		182	#	2		185	8		E		
\$1.PJ -0008	15	PRESSURE TRO-ACCORDUMN PRESS		188	2	182		2	2		P		
\$100-54-15	15	PRESS SWITCH-8PSI (NJ 894		1881	12	122		¥			¥		
51-85-0011	15	PRESS SWITCH-LPST INJ RDE		1821	183	183	*	185	•		2		
1904-17-12	25	PRESS TRANS-LOOP 1 INJ WRADES		1881	183	2	•	E	2		E		
\$1 PT 4902	15	PRSS TAMS-1,00P 1 (4) 988		282	2	E	8	22	•		P	•	
21 77 1003	13	PRESS TAMES 600P 3 (12) 199		182	115	£		TES	*		Ħ		
\$1.00 FT 100%	15	PRESS TRANS-LOPP 4 (NJ RDE		12	Ħ	E		48		8	2		
SI PT 8866	21	PRESS TRAIS-LPSI BISCH ESR		1581	1	183	•	2			183	*	
21-77-997	55	PRESS TRANS- 4PST DESCH SDR		1821	133	<b>1</b>	*	¥	8	•	¥	2	
1400-11-15	15	1917 10-11-20		182	2	E	•	٠	•	•	E		
21 715 6721	15	TOP 110 SHITCH TE-28		ŧ.	*	ě	à	244	*	•	183	•	

# THE LICENSE PRINT CONTROL OF THE SALES SALES SALES OF THE SALES SA

Colored   Colo						22 484 54				22 4245		*	NE C	
No.						10 57578 10 57578 10 57578 10 57578	CHENCE 1	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	SMACT TO SMACT TO SMACT TO SMACT (183)	73575 73575		SPLET TO SPLET TO SECOND T	ACCUSES INCLUSES INCLUSES INCLUSES	********
1		STSTE		7157 \$155		(8787 24)	E			=				
1		SI	SAPETT INJECTION TARE	3861		185	765		•			2	=	115.78
1		15	SI ACCHRIGATOR TABLE	386.1		24	554			2			2	115-71
State   18th		100	ST ACCOMPLATOR TABLE	CLABBING		22	#FS		•		•	F	2	115-18
1   10   10   10   10   10   10   10	203	15	1506. VALVE FOR T1 -21 BECTRC.	1	108	182	18	165	183		E	2		
1   10   10   10   10   10   10   10	111	15	1501. MAINE POR LPSI EDR	1808	*05	2	183	185	185	•	18	2	•	
1   1   1   1   1   1   1   1   1   1	534	15	1501. WALTE POR CS-809-8513 87	1004	NO.5	2	112	152	TES	*		P		10-21
1801, NAME FOR LOOP 1 STEEL SEE FORT   150   151   1	135	12	1501. 14177 704 1751 878.		101	2	E	185	E	2		2		185-6F
15th	535	is.	1501. VALVE POR 1200 1 51 808	1	101	TES	¥	2	15	*		2	8	18-01
1   1   1   1   1   1   1   1   1   1	537	IS	1501. 94478 704 4007 2 51 878		•	115	1	531	2			<b>P</b>		18.00
State   Stat	255	177	1501" WALTER FOR LOST 2 SE EDE			2	1	2	ž.					18-01
State   Control   1981, 14477   188	11	15	71.21 (50), VALVE	100		12	1	2	•			2	*	
1   1   1   1   1   1   1   1   1   1		10	SAPPLE COM. 1505. VALVE	100		18	2					1		
Statistics statistics   Stati		EX.	74-29 1501. VALVE	1906		2	185		2			2		***************************************
State   Stat	10	15		168		32	112					2		
State   Contract Post   Line   Contract Post		15	DEATH TALTE POR SI-LI-2	100		2	155					£		
State   Contract   C		17	1-11-15 HG4 B4784 1888	1004		122	183				8	22		
1501, National Signature   1501, National Sign		SI	THE TALTE FOR LPS! SIG.	1001	14		#18					4		***************************************
St. 1501, National Services   1501		25		1001		E	185		TES			P		
State   Contract   C		31		1000		2	18		18			2		
St.   Application   Test   T	14	15		1608	ē	1	113	183	ā		£	2	8	
11 SAN ALL MAN PAR ST-77-1 MAN T	22	13		1204	8	1	185	1	E		¥	2		
The state of the s		15	1	101		18	18		£			2	•	
The state of the s		15	1	1608		8	165		785			=	•	
A MAN BEAUTY TO AND PROPERTY IS	65	100	1	*104			2							
		15		BUILD	*	*	24							

						12 4848 :				25	STEP 28		31.41	
						COMPOSED (SPORT)	SAFET FECTION P8 - PRESS BOWN	10 mm	SALECT TO SPORT (SPLACE ON INSPECT	SERER	TOTAL SAFETY TOTAL SERVICE TOTAL SAFETY TOTAL SAFETY TOTA	200000 10 200000 10 200000 10	POTENTIAL ACT RECENTION POTENTION (STR 2C)	110
TAG BO./LINE BO.	STSTE CODS		DESCRIPTION	PAET WAR	CONTRACTOR	(ST87 28)	2	 40			8			
CS-17-05617	is.	1201	150f. VALVE 708 SI -77-3	1691		182	122		185			2		
CS-1-15649	15	1500	1501. VALVE POR 51-PT-2	1001		2	2	*	YRS	•		P	â	
C3-1-1649	15	1500	130L. WALTE POR 51-FT-3	1004		2	165	8	F		8	2		
CS P-0650		ISOL	150L. VALVE PCR 51-FF-2	1908		185	18		18		8			
(3-1-065)	15	1801.	1801. VALVE FOR 51-PT-1	1001		182	E		•			2		
CS-W-0652	15	1201	1301. WALNE POR SI -PT-2	1691		115	E			*		2		
CS-1-0653	15	1500	150L. MALPE POR SI -PT-3	1001	10-	82	165					2		
1596-4-52	E	180	1801. VALVE POR SI -PT-4	100		183	2		2		8	2		
CS-1-1655	21	1980	DESIR VALVE FOR S1-PT-1	2007		182	E		•	•		#		
CS-14-0656	23	DEAT	DEATS TALVE POR 81-77-2	1400		E	185	8				2	•	
CS-11-0657	15	38		100		1	SH.	2	•			2		
CS W 0658	u	1581	PERIO VALVE FOR SI-PT-4	1601		E	182		8		2	2		
0990-4-50	15	1961	1901. VALYE POR 51-71-5	100		182	1465	2		•		12		
CS-1-9881	15	1300	1505. WATE FOR SI-FI-E	1004		£	12		•	8		2		
C3-11-0562	15	1500	1501. WEFE FOR SI-FF-1	1000		¥	15	•	•	2		2	•	
CS-W-DER3	15	1951	[50]. MAT FOR 51 PT-1	9087		2	183					2		
CS-1-2644	15	thu.	VALES POR SI-PT-1 440 CC 800T	FC 800T		E	E		22		2	¥		
CS-V-9865	¥	1800	150L. WAS FOR ST-FF-2	1000		1	Ħ		8	*		2	•	
C3 # 1866	21	TSUF	ISOL. MALTE POR SI-PT-2	100		2	183	2		*		E		
1990-1-52		1083	[50]. VALVE FOR SPT-1 AND NC 9097	1608 38	-	TRS	4		16	•		¥		
CS-9-0668	15	1991	1501. WALVE POR ST-PT-3	1001	-	2	12				8	E		
CS-1-0869	E.	1051	1501. WALVE FUR ST. PT. 3	1001		182	115				•	¥		
CS- V- 6679	18	1051	1505. VALVE POR SI-PT-3 ARD BC 805F	1618 38		185	E	•	4	*	•	185		
(5-1-967)	15	1051	150L. VALVE POR SI-PT-4	ii ii		12	112		8	•		2		
5-1-112	D <sub>0</sub>	150	1501, MANT POR 51 PT-4	No.	*	346	848			•	•	**	•	

## THEY LICENSE REMONE, PROJECT SENTER ASSULTS

51 [50L. Table 75]	91 6. 8. 8.					STREET, SQUARE, SQUARE		11日日日日日日日日日日日日日日日日日日日日日日日日日日日日日日日日日日日日				
	SCRIPTION		*******	COMPARENT PROSTER SAMET	SAFETY PURCTION SAFETY PURCTION OF - DPRINGITITION OF - OPPRINGITITION	PETT FUNCTION:	SERVICE TO EPHRAMICA OR HERET (BILL PRODUC	CORPORES RESTRICTED FR - FR OF - 09	MECHANIS SAFET WICTOR SOMENTY ESSEN IN IN TROCKA 78 - PRESS ROOM OF - OPPRABILITY	STRUCT TO STRUCT	BITALIS DE CONTROL DE	
	· 日本の日本の日本の日本の日本の日本の日本の日本の日本の日本の日本の日本の日本の日	7457 3488	CORPORER	(22.63.5)	£	40			8			
	1901. WALNE POR SI-PT-4	108		2	185		22			2		*
	DEATS VALVE FOR SI -FT-4	1006		185	#							
	DEALS WALVE POR SI PT 4	101	-	183	E					2		
	1501. WALVE POR 51-F1-6	1001		785	2			•		2		
	1501. VALVE POR 51-F1-6	1001		182	1				8			
	BTPASS VALVE POR SI-PI-6	100		Ħ	182		•	•		2	•	
	F 14-15 BOA 21-16-4		•	16	123							
15 34 15 15	PLATE VALVE FOR 51-F1-6	100		2	183			8				
51 TOT 18	TEST NAME TOR SI -FT-1		-	2	1							
21 944 NA	1-11-15 BOR 181-11-1	1000		2	ñ					2		
51 mm ms	VANT VALVE FOR 51-FT-2	1606	-	185	Þ	8	•	•				
SI NUMBERAL	NAIS VALVE FOR 51-77-2	100		#	115			•		2		
711.160 IS	VEST 144/15 FOR 51-FT-3	1498		183	115							
TA MEN IS	04418 WATER TOR SI-FT-3	100	٠	9	SE .					2		
S1 1501. TA	150L. *ALVE POR MC-PT-105	100	•	122	¥					2		
SI DULL TA	DEMIS VALVE FOR SC. PT-155	1001	٠	£	185	•	*	8		P	•	
Si 1501. Fal	1501. YALVE FOR BC - 77-200	100	٠	£	¥		2			2		
ST THAIR TO	DEATE FALST POR BC-PT-205		•	¥	2					2		***************************************
SI 150L. VAL	1501. VALVE POR NC. PT. 308	1004		23	ħ		٤		8	2		
N 6772 15	DEATS WALVE FOR BC-77-380	1908		2	2					P	•	
51 150L. FA	1501. VALVE POR AC-2 PROR LPS!	1 100		2	18	Ħ		8	E	£	•	
NA 1051 IS	[50], Walve For CROSS-TIE BETW 8007	1000	*0*	183	185	185	B	*	Ķ.	183		
607 1547 15	1621 1000 + 1501 MINE	1608	7.	175	#83	122	185			¥		10.51
801 1541 15	LPSI (JOSP 3 1501, WALVE	1000		12	2	183	185	•		<b>S</b>		18.67
51 1851 108	\$957 \$100 \$ 100. MALER	\$1.00	*	185	183	18	524	ě	•	18	•	40-544

						* *				845	5767 28		ST OFF	
						CLANGEST SEPERATION SAPETY PRESTINA	SAPETY FORCTION FR - FEESS BOWN 6P - OPERABILITY	COMPONENTS SAFETY FUNCTION R - PRESS BONNO F - OPERABILITY	COMPONENT SHARET TO REPORT AS OR 1057907 (81) PROGRA	POST POST POST POST POST POST POST POST	CORPORATE SAFETY PRETION AND AND AND AND AND AND AND AND AND AN	2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	POTENTIAL SECRETARISES (STRP 2C)	
TAS NO. /4188 NO.	CODE		DESCRIPTION	PART BARE	CORPORET	18787 241	£	40		2	<b>t</b>	1816 181		
\$2.00 VO# 12	15	1521	1521 (200F 1 150L. WALVE	1001	404	22	165	183	#	8		E	•	185-07
SE #08 - 804 S	15	1501	ISOL. VALVE POR RPS! READER .	1408	102	2	#	185	165		2	2	•	
St #19-0049	15	1506.	ISOL. WALVE FOR SI PURP RECIRC 2007	100	10	18	12		£ .	•	2	2		
51-#18-0045	¥	180F.	ISOL. VALVE POR SI PORP RECIRC. NODT	140	M.	282	185	185	F		2	2		
SI-#0W-0514	15	ISOL.	150L. VALVR 18 BFPASS LIRE PUR BODY	140		Ħ	113	185	2	*	2	2		
\$1.404-0515	II.	1501.	[50]. VALVE FOR CYCS/EPS! 58PP 5007	140		æ	185	185	183		2	=		
\$1 *0*-0\$16	15	ISOT.	ISOL. VALVE POR VC SOMP RECIRE. BODY	140	*0*	8	12	TES	ž.		P			
\$1 #0#-45 7	31	1801.	[50]. WALVE POR SI-ROV-BYPASS BOOT	100	¥(0)	2	145	175	182	8	P	2		化甲烷 医电子 医医囊 医异丙烷 医肾
\$1 <b>*</b> 0 <b>*</b> 0518	15	1501.	[50]. VALVE POR TE-28 SUPPLIT   8057	1661	<b>*</b> 0	18	12	1	2		2	2		
21-# - 1002	II.	1380	CHECK VALVE AC-2 DISCRAEGE LIN WORT	140		12	183	2	183		P	P		
SI-F-0003	15	CHECK	CHECK VALVE POR LPSI READER	100	180	183	165	185	12		2	2		
\$1 - 4 - 0005	15	1201	1501. SALVE FOR P-48-1 SECTION BOST	160		22	115					2		
9000-A-15	25	180F.	[50]. VALVE POR P-48-2 SPCTION 2657	100		22	18	•				2		
SI-W-0007	ží	1801.	150L. VALVE FOR P-48-3 SECTION BODY	140		185	183		•					
\$1-4-010#	15	1561	1561. VALVE POR P-48-1 DISCIAL STOT	1001		B	12		•			2		
51-¥-0909	18	1500	[50]. VALVE POR P-48-2 DISCRAR SOFT	1001		E	18		•			2		
51 W 0010	15	1801	150L. VALVE FOR P-48-3 DESCRAR BODS	1001		B	183		•			2		
SI * - 1611	155	CHRO	CRECE VALVE FOR P-48-1 DISCRAR BODY	1001		2	185	183	183		E			
51 4-0912	M	CHEC	CHICH VALVE FOR P-48-2 DISCRAR BODT	1001	•	B	2	185	18		2	2		
SI-W-0013	IS	1383	CRECE VALVE FOR P-48-3 DISCHAR BODT	1401		185	185	122	185		2			
#190-#-15	21	CHRC	CHECK WALVE FOR APS! BEADER	1508	180	SE .	22	185	3		E	22		
\$1 -4 -0018	55	CHRCE	CHRCE WALFR POR ST LOOP 3	3007		2	182	185	18		8	11	•	
\$1.4-0019	tin	CBBCI	CHRCH WALVE FOR ST LOOP 4	1608	16	185		183	115		2	75		
51-W-0026	155	CHRC	CHRCE WALVE FOR SI LOUP 2	1004	•	2	18	185	182	*	2	111		
21 W-8921	15	CHRO	CHRCE VALVE FOR ST LAMP 1	8004	200	¥	185	£	¥	*	£	145	8	
Control of the last of the las	THE RESERVE AND PERSONS NAMED IN	-	Magness	On the Real Property lies in column 2 is not a least	The second laboratory of	-	-		The second secon		The second secon	The second secon	The second second second	The second name of the last of

### NAMES ATOMIC SECTISE COMPANT THPS LICHES ASSENTE PROJECT SAPETT INJECTION SYSTEM FULLS CHAPMENT REVIEW RESULTS

Column							STEP 24				LS .	ST 23		34 4445	
1   10   10   10   10   10   10   10								S46 - 40	78-713 78-713 55 90/86 881-217	SREART TO SEPREMENTAL CATTORNEY ATTORNEY (ATTO	\$	ECTION ADMOSTLE SCRIPT AND ADMOSTLE SCRIPT AND ADMOSTLE SCRIPT AND ADMOSTLE CONTRACTION SCRIPT AND ADMOSTLE SCRIPT AND ADMOST	SALET TO SECURITY OF SECURITY	POTENTIAL ACT DESABATION PECANISM INCLUDIO (STE 2C)	PARTE
State   Stat	THG MS. /LINE NO.	CODE		PRSCRIPTION	PART TARE	\$602		2	40 :			**			
	81-W-9026	15			1991		22	2			•		2		
	SI W 0027	15	1991	. WALVE POR P-49-1 SECTIO .	1400		18	185			*		2		
18   18   18   18   18   18   18   18	\$1 - ¥ - 102#	15	1361	. WALVE FOR P-49-2 SUCTIO	1001		2	185	2	•			2		
1	6200-A-1S	15	1501	** ** ** ** ** ** ** ** ** ** ** ** **	1400		E	523	2	*	*		11	•	
1	SI-V-0030	15	CREC	E VALVE POR P-49-1 DISCRAR	1400	160	2	151	185	165	*	ħ	12	•	
1864   1864	51-4-6031	SI	0.880	WALVE FOR P-49-2 DISCHAR	1908	165	185	1	183	165	•	E	2		
18th Mark Mark Political and M	SI 4-0032	100		E VALVE FOR F-45-3 DISCRAR	1404	180	185	185	185	12	*	ħ	118		
State   18th	SI-1-0633	15		. WALNE FOR P-49-1 DISCRAR	1608		18	185		£	•	2	22	•	
18   184, 1447 For February 1980 at 18   18   18   18   18   18   18   18	N. 11 - 6034	2	1	VALVE POR P-45-1 DESCRAR	1408	•	185	18			•		2		
1801, NAME THE STILLE-1-4   MOST   1	SI -# -0035	12	1	VALVE POR P-49-3 DISCREE	100		12	382			•	8	2		
State   1984, Fully first   144, 144, 144, 144, 144, 144, 144, 14	51-3-0037	15			1308		185	#ES	2	2	•	•	2	•	
1501 WARR THE STATE LLEST AND THE TEST TO THE TEST TO THE TEST TO THE TEST THE TES	SI-¥-9038	25			1808		18	£	2	2	•		2	•	
State   Contention C.2   Fig. 18	51 w 0039	N			1608	•	185	185			•		2		
1   1504, Water red 51-71-4   1007   7   155   155   150	0#00-#-ES	12			1001	*	2	183	2	*	•		2		
State water for state of sta	51-7-6042	SI			1808		185	2	2	8	•	2	2		
State National Nati	SI * 0964	12			1404	•	12	2	•		•		2		
Si   Rest Note From C-1 (SPPL/16)   Most   Fig.	51 4 9047	22			1004		18	18			•	•	2		
SI         HSS INM OVER PASSIER PROPERTY SOUTH         FIS         HSS         <	3500-#-15	31		18 VALUE FOR AC-1 SUPPLIYEE	1608		E SE	165		•	•	•	2		
SI ISOL, MATERIOL SI-LI-LOT BOOK T TES TES TO	51 ¥ 8055	15		I RDE OVER PRESSURE PROTECT	9097	15	183	185	185	165	•		22		185-09
SI 1501, MAN POR SI-PI-7 ROPE 7 TES 175 TO	1500-1-15	10	1		100	•	185	2		*	•	*	185		
S1 DALIF WATER FOR S1-445-1,-2 ADDT	51 V 0010	15	1		1000		185	#		•	•	2	2		
12	SI -# - 6971	SI			8007		H	185				•	115	•	
94 1504, WALFE FOR STATE 1 AND S MOTH 1 1 THE STATE ST	SI V-9372	35	1 -		BUST	*	22	TES.	*	2			185	•	
THE FORE THAT PER STATE STATE IS NOT THE TAX THAT THE TAX THE TAX THAT THE TAX THE TAX THAT THE TAX THAT THE TAX THE TAX THAT THE TAX THE TAX THAT THE TAX THE TA	ST 4-0073	15		C. WALTE FOR ST-P1-13 AND S	1,004		185	182		•		•	2		
	** 1.5.74	10		C. Make the St. fill St. amb S.	# A A	10	124	544	*	÷			344	4	

## SAFETY INJECTION STETCH PLATE COMPONENT REVIEW ASSILTS

					51 69 24 51 69 24	Spirite Spirite		-	2 415				
					CORPORENT DESTRUCTION SAFETY FUNCTION	SAFETT FORCETOR FR - FESSS BOWN 67 - GERMANILLIT	- PESS BOWD : - PESS BOWD	2081/2011 TO STATE OF THE STATE	100 COMPANY	THE STATE OF THE S	STATE OF THE PARTY	MECHANISM MECHANISM (SETTITION (STEP EC)	
STSTES 0850	DESCRIPTION		2467 8488	1000	182 884 581		8		E	8			
1505. MANT POR ST-PS-18	F08 S1		1001		<b>3</b> 2	185	•	•		2			
130F. WELF	15 FOR 5	130L. VALVE POR SI-PI-11 ASD S 800F	100		8	185		9	•		P		
-	15 104 E	PERIS VALVE POR SI-LLS-3,-4	100		294	185			*				
150L. VALVE POR 51-LT-1	18 POR SI	1-47-1	1001		2	2	2			•	31		
WEST VALVE POR SI-LT-I	E 908 SI	1-17	1000		185	38		•			2		
150c. MLR FOR SI-LT-1	FE FOR S	1-11-1			1	18					¥		
1501. 44	1501. UALVE FOR ST-LS-6	1-12-1	1906		12	1				8	1	•	
150E. **	M FOR AC	[50L. VASVE POR AC-2 (MSTR.	1000		182	185	2		8	•	2		
1801. **	ISOL. WALVE FOR SI-P1-30	05-14-1	1001		TES	#BS					2		
1501.	150L. VALVE POR ST-FT-32	11-11-11	100		32	¥	2		8		2		
176	18. FOR 5	SEATT VALVE POR SI -PI - 13 ARD S	1008	14	183	#		*			2		
BELLE	PLATE WAYN POR P-48-1	-	1004		183	183		9			2		
08419	DEATH VALVE FOR P-48-2	1:0	1000		12	2					2		
	DEATE VALVE FOR P-48-3		1691		185	185			2		2	•	
94.19	S 804 8478	DELIT VALVE POR 51-71-11 APD 5 8097	1608		183	22		185	*		£	•	
1808.	[50]. VALVE POR 51-P1-31	11-11-11	1004		12	382				8	P		
1801	1501. VALVE POR SI-P1-33	1-11-13	1006		18	185	•	8	8	•	B		
1801.	150L. VALVE POR 51-P1-35	1-11-15	1404		2	382	2			•	E		
1547	51 OTE 71	LPSI DDE OFER PRESSURE PROTECT BODY	1001	t	182	183	18	165	•		2		18.00
1501.	. 104 EATE	1501. VALVE FOR PT 508P 515CRA 9087	1006		TES	183			*		=	•	
lsot.	01-14-15 BOR \$1-14-10	61-14-19	1006		18	185			•		2	•	
181	WENT MALYS POR 51-PT-19	11-110	1001		18	165					112	•	
HOLL		TREOTTLE RALFE FOR CVCS/RFST S BODY	9107	-	165	182		¥	•	•	Ħ		
CHECK	NALWE FOR C	CHECK WALVE FOR CYCS/BPS; SUPP. BOD?	100	8	¥	785	183	¥	8	Ħ	£	•	
150%.	130E, TALER POR ST-LE-4	+17-15	2004	*	162	2			•		282	•	
Company of the local division in	Charles of Street, or other Designation of the least of t	The residence of the last of t	And in concession of the last	The second named in column 2 is not the owner, where the owner, which is the owner, where the owner, which is the owner, where the owner, which is the owner, where the owner, which is the owner, which is the owner, which is t	Management consumer or	-	CONTRACTOR STREET	Name and Address of the Owner,	-	The second named of the last of	Contract of the last of	STREET, SQUARE, SQUARE	The Person Name of Street, or other Persons Name of Street, or oth

						STAF 34				15	84 48		H 411	**
						CONTROL OF STREET	SAZETT FUECTION SAZETT FUECTION FR = FAESS ROUND OF = OPERABILITY	*********	SERVICE TO SERVICE TO SERVICE TO OF DESPITE	2 E 8	COMPONENT'S SAFETY PERSON OF A PROPERTY. PER	# 12 mm	POTENTIAL ACT DECEMBRICON POCANICAS (SETTIFICA (SETTIFI	
TAG SO, /LINE SO.	8000		DESCRIPTION	PART EARS				40						
21 w 1655	55	1051	1501, WALVE POR \$1-41-3	1004	*	2	2					2		
5550-A-15	31		1501. VALVE POR SI-LI-4	1001		48	183		8	*		2		
SI-W-0457	22	1051	[50]. VALVE AC-2 (WSTR.	2001		221	165	•			8	2	•	
51-9-0658	55		PERIT VALVE FOR SI-LI-4	1001		E	183		8		*		•	
6550-115	15	36	DEATH VALVE FOR ST-LT-3	1004		E	11		8					
S: #-0550	15		VOT NAME POR SI-45-4	1000		æ	185			8		2	•	
51-1-0661	31		DEATE VALVE FOR ST-LS-5	100		185	2	4				2	8	
51 T 5867	31		CHECK WALVE FOR BYST LOSF 1	1604	16	185	F	* FES	ā	*	2			
81 # DEER	15		CHECE WALKE FOR 8751 1507 2	100		ES.	2	185	F		2	2	*	
SI-9-0569	22		CHECK VALVE FOR 8PS1 4,00P 1	160	<b>18</b> 0	¥	12	183	22	•	2	1	•	
51.4-2670	tis		CRECE WALVE POR 8PS! 1,60P 4	1404		883	2	185	185	*	•	=		
51-7-0671	ts.		TEROTTLE VALVE POR APS: LOOP : BODT	14001		183	2		185	•	2	2		
SI # 0672	21		THEOTILE VALUE FOR 8PS; LOOP 1 BOST	1 1001		185	185		#	•	8	2		
SI-1-0673	15		TREOTTLE VALVE FOR SPS: 1,00P 3 800T	3 8097		165	2		165	•		2	*	
51-9-0674	15		TREOTTLE VALVE POR 8PE: LOUP 4 BODT	1404 -	*	185	185		£		•	2		
51 4 0675	35		TRST COME. LOOP 2	ROM	٠	185	122		182	*		P		
51 4- 04.18	TS.		TEST COME. LOOP 2	1008		•	E	8						
SI-4-1689	š		1501. VALVE POR SI-PI-S	100	*	2	185	•		•	*	B	•	
26.90 A 15	N		150L. WALVE POR 51-F1-5	3001		180	8		2	•	2	18		
1690-11-15	13		TENT VALVE FOR SI-FI-5			182	2		*	•	8	18		
26.90 11.15	35		S-14-15 BOS BATES BIFES	aca.		2	Ē	*		•	8	E		
51 -1 -0423	15		PERIO VALVE POR 51-11-4	1004		185	16	*	2	•	•	28	•	
51-4 0695	15		SEASON VALUE FOR WC SOME RECIEC BODY	1608 31		185	¥		18	•	•	5		
31 1 1646	15		DEALS VALUE FOR TO SUBP SECIEG SITE	EC 8000		163	165		183	•		B		
21.3 0611	25		52 PT 28 CARCY 19, DE 78 29	2004	36	F	1462		*		145	234	•	

# WAYS LICENSE COMMAN PROJECT SAFETY INDECTION SYSTEM FLUTO COMPONENT REVIEW RESILTS

						22 4315	**			SI 63 IS			: Step at	
	100					10 5951ER 585179 10 5951ER 5861708	25 85 85 85 85 85 85 85 85 85 85 85 85 85	COPPORENTS SAFETY FUNCTION  R - PRESS BOUND  P - OPERSHILTTY	CONTONE NT 1 SUBJECT TO 1 REFUREACIENCE : 00 INSTELL : (REJ.) PROGREM :	CORPO FUNCT RECESSES PB - 0F -	CORPOGENT'S SAFETY FUETION RECOILENTY RESIZE BY REL PROGRAD PR. PRESS BOSED OF - OF CHARLITY	01 2000 100 100 100 100 100 100 100 100	ME DESIGNATION OF COMMITTEES (STEP 7C)	 FIRST STATES OF
TAG NO /LINE NO	100E		6ESCR1FT10#	PART NAME	CDDE		82	8	**	2				
\$02.0-A-15	15		ISON WALVE FOR CUCS SIFFLY TO BODY	800v	b	WES	WES				2	5		
SI-4-0765	15	VE 81 90	VE WE WALVE FOR P-48-1	900v		WES	£5				2	5	•	
2016-0-15	IS	UE ME VI	<b>说新 如此 年 Fig P-48-2</b>	w000	>	MES.	£63		*		2	res res	•	
SI 4-0739	25	W. 18. W.	WE ME VALUE FOR P.48-3	800v		WES	#ES	*			2	<b>S</b>		
SI 4-6711	IS		VENT VALUE FOR P.49.1	MODE!		FES.	165				2	£5		
51-6-0712	15	VENT VI	NEWT VALUE FOR P.49.1	BODY		534	sg.		*		2	<b>82</b>	•	
SI V-9713	15		DRATH VALUE FOR P-49-1	A008		RES	965				2	MES		
\$1.0-0-1S	15	WEST W	VENT VALVE FOR P-49-2	V008		55	858				9	32		
91.4-4-15	15		WEST VALUE FOR P.49.2	900v		WES	985				2	£53		
51 W 9717	15		DRAIN VALVE FOR 9-49-2	4408		ÆS	WES	2			•	FES.		
61/8-1/15	22	WEST W	NEWT UNE VE FOR P.49.3	BODY	Þ	346.5	£					rg.		
17.6-4-12	15	WENT W	VENT VALVE FOR P-49-3	900%	25	£5	£3		•		2	re S		
12.4-4-15	25		DRAIN VOLVE FOR P-49-3	9004		98.5	£5				2	£5	•	
77.0-A-15	SI		DRAIN WIVE FOR SI PUMP RECIRC 8989	A-800 A		<b>35</b>	£5	*			•	egg.		
R20-4-15	15		08 A 18 VALUE FOR SI -P 1-32	M000			WES.			,			٠	
SI-4-0732	155		DRAIN VALUE FOR SI-PI-31	4004			FES		*					
SI-W-8733	15		DRAIN VALUE FOR 52-P1-33	BOOM		2	#ES	*						
51-V-6734	25		DRAIN VALUE FOR SI-P1-35	A908	De .		23	*						
SI-4-6738	15	- 1	150L WIVE FOR 51-71-5	AGD8	-	534	465		*			53	•	
SI-v-9739	15		150L VALUE FOR ST-F1-5	A008		<b>FE</b> 5	5				•	5	•	
P-48-1	15		LOW PRESSURE ST PUMP	581583	4	346.5	Ð	88.8	\$		Ð	<b>FES</b>	•	
1-8-1	15		LOW PRESSURE ST PURP	SHEFT		25	88	455	9		£8.	Ð		
1-8-1	SI		LOW PRESSURE ST PUMP	IMELLER		\$ 34	9	¥65	£23		£	£5		
P.49.1	15		LOW PRESSIBLE ST PUMP	0,851,86	0.	25	153	122	52	*	<b>3</b> 4	53	2	
		-	Section 1		*					1				

# SAFETT INJECTION STATES FUEL CONFINENT BATTER RESULTS

					***************************************	-	Standard -	STREET, STREET	***********		Sananas Sananas			
					STREET SATURATE SATUR	24/277 (18/2) 10 24/277 (18/2) 10 79 - 74/25 10(19)	SACAT FREEZING	SHURT TO SERVICE TO SE	CHR780 FRECTO FRESTO FR	10 1 10 10 10 10 10 10 10 10 10 10 10 10	SALET TO SECOND	MANUAL DE LA SELECTION DE LA S	8	THE STATE OF THE S
740 80./1188 80.	STSTE	PRSCRIPTION	21E 148	2000	(82.68.58)	#	8		g	8	18.04		***	
	IS	RICH PRESSURE ST PURP	INTERN		2	182	2	THS		2	2			
	13	4864 IS 88085884 MOT	361690		22	2	18	182	8	P	2			
	15	LOW PRESSURE SI PURP	387		2	#85	E	#		22	¥	•		
	155	LOW PRESSURE SI PURP	INFELIM		185	12	282	185	*	2	2		-	
	15	RICH PRESSURE SI PURP	261582		12	32	5	185		P	2			
And a second second second	15	RICH PRESSURE SI PORP	THE		¥	22	ķ	185		2	B	•		
	15	RICH PRESSURE SI PURP	INTELLE		2	141	8	#		2	2			
	15	LOW PRESSURE SI PTMP	CASING		TES	ě	185	SI I		2	2			
	175	4M64 15 88055584 NOT	3867		TES	165	385	<u> </u>	•	2	2			
	15	4804 IS \$18055\$14 AOT	IFFILE		765	E	Sign	382		2	2			
	155	NICH PRESSURE SI PREP	CASTRG		Ħ	185	葡	<b>S</b>	8		2			
	15	BICH PRESSURE SI PURP	THE SEL		¥	183	Ħ	184		2	2			
	15	BIGS PRESSURE ST PURP	IPEIR	•	183	185	185	116		2	2			
	15	CS-4-786	101		31	2		185			2	•		
CS #0#-8539	15	130f. VALVE POR 100P 4 51 558	104 104	•	185	#	185	20	8		2		185-00	
1/2"-FRSR-902-29	SI	#551-3 #CIEC		FIRE	TRS	£	•	2			2			
1/2"-P858-902-30	15	FFS1-2 BECIEC		1114	122	58.	٠	2	*		12	8		
1/2" - FEST 992-31	Į,	#PSI-1 CECIEC		Hid	¥	183			•		2			
1* - 1851, 101-15	175	MPSI PURP RECIEC NOR		HIM	185		æ				2			
1* - PRSL - 102 - 38	117	LPSI-1 RECIEC		9119	165	183	9		2	8	2			
1" PESL 302 +0	15	UPSI-2 RECIRC		212	22	Ħ	•		2		¥	8		
1* - PESL-392-41	15	UPSI-1 BRCINC		3414	183	185	*	•	•	•	¥	8		
14. 7851-152-1	18	71-28 BISCH TO PURPS		8414	2	183	*	17.5	•		P	*		
10" PESI, 1524-1	II.	TE-28 SISCH TO PHAPS		3/16	346	183	2	185	•	•	21	785	183-78	
49.00.1011			· 日本の日本の日本の日本の日本の日本の日本の日本の日本の日本の日本の日本の日本の日	· · · · · · · · · · · · · · · · · · ·		NA CONTRACTOR								

					11 215			SE 431		32 435 :	
					CORPOGENT INPORTACT SARRT FUNCTION	COCPOSITOR SAFETY CHICAGO PR - PPESS SUCHO OF - OF ERABILITY	SUBJECT TO	COMPONENT'S SAFETY FUNCTION ADMINISTRATION PROPERTY AND ADMINISTRATION OF COMPONENT AND ADMINISTRATION ADMINI	100 PER 100 PE	ACTUALIST DECEMBRIOR RECARDING STATEMENT STATE	THE THE STATE OF T
TAG #0. FLIES #0.	8600	DESCRIPTION	PART BARE	2002							
2"-PRSB-2502 18	15	BPSI SUPL TO CVCS	8	MIN	185	8	•	8	2		
27-PRSH-2501-25	15	E 4007 IN 1548		MIN	185	183 R.	282		2	•	
82 2052-88M-2	55	EPS1 181 LOOP 2		9414	185		2	•	2		
2 PRSS - 2507 - 27	15	1 4007 781 1548		1111	35	125 80	183	£	2		
Z - PRSs -2502-28	15	# 4007 FE 1548		8014	165	8		8	2		
Z*- PRS# 902-13	SI	#PSI-3 \$15C#		PIPR	294	155	•		2		
Z*-PRS8-901-15	S	#PSI-1 915C#		8614	2	2	4		2		
2" PRSR 901 15	ii.	4951-1 B18CB		8414	31	382		•	2		
2 - PRSR 952-17	15	CWCS/MPSI SUPPLITIBLE	有家庭学家还有自然有由人不要或其最高分	2614	185	<b>8</b> S≱	•	•	2	•	
7, 483 102 21	15	CVCS SUPL TO BPST BDR		1138	165	185		2		2	
2PESE -902-23	35	AUI PRES SUPL		MIN	163		•		2		
2 PRSB 902-32	150	3138 184		ын	123	9 52		2	2	8	
7, 485, 767, 78	15	BTPASS CS-801-513		2114	185	. E	Ñ	2	2		
2 1/2" - PMSL 302A 26	25	T1-20 PARTER RETURN	8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	1111	183	2	E		2		
J PEST, 101-45	15	RTPASS SI-MOV-1		HIL	183	15 2	¥	8	2	8	
3* - PRSL-302-5	21	ACCUBILATOR FILL LIFE	5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	HIL	185	785 m		•	2	•	-
1" - 788, 3024-5	S	ACCUMULATOR PTLE LINE		F118	¥	34	R	2	2		115-71
(* CR 155A-3	IS.	THE 28 SUPL TO CYCS PURPS	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	MIM	18	175	•		2	•	
C* -PRSE_2502-16	IS	1 481 10		9114	165	163	2	•	P		
( . PBSB-2502-11	u	181 LOOF 4		W.	22	2	225		2		
15858 2502-10	in	14 71 154		MIN	2	*		•	2		
(* PRSB-2502-8	15	TW 1999 3		3414	282	e 21	E	2	2	•	
C PRSE 2562 9	15	181 LIOP 2		NI I	2	£ £	2	•	1		
1. 7858-902-12	15	#PSI DISCH SPR		1178	<b>S</b>	2 E	£	•	¥		
1 101 701 1	Į,	##51-1 S##L		2074	185	165 80	185		18	•	

# SAFET TATES AND AND CONTRACT TOTAL SAFET. SAFETT TATES STATE, PAIN CONTRACT AND SAFET.

					IN CHES				82 4M2		. 344	
					COPPORES. INVESTOR SAPETTOR	STATE PROTECTION OF THE STATE O	********	STATE OF STA	CHEMINAL STREET PROPERTY STREE	 MUST IN	######################################	
TAS 80.71.188 NO.	3000	8 985CR19710#	PAST 8485	3600	100	2	6					
6 -PESL 302-8	15	Talls T-15ab 15		8414	22	¥	8	TES		2	•	
(* 7451, 391. 9	U.	#PSI-3 SWPL		8414	2	27	•	F	•	2		
F 7151-151-19	15	UPSI -1 SIPLE		8118	¥	¥		ş	8			
C-785L-151-11	15	SI LISI-1 SUPL		FIFE	785	¥		ě		2		
C-1831-183-11		UNI - 1 SM.		1111	185	Ħ	•	Đ		2		
C-185, 151-13	×	TO SUME DISCU TO LPS!		PIN	2	£		•	8	2		
61-102-1031-19	=	LPSI-1 DISCS		11.11	18	*	2	£		2		
6" PES, 311, 12	15	LPSI-1 DISCS		E	12	ħ		135	*	2		
C-181-381-33	N	LPS1-1 915CB		2112	2	72		2	8	E		
6" PESL 302-44	=	PC SUMP DISCR TO LPS!		ш	18	2		2	8	2		
\$-1187-311-\$	IS.	LPSI DISCR 70 BPSI		HI	2	183	*	g,				
8 - 785E 2567-E	15	LPS1 181 BM		2014	2	£	•	292	•	*		
8" - PRSL 302-3	15	USI (8) 868		MIN	2	2	8	£		2		
8 PRSL 1014-3	N	LPSI DISCR BDE		HIH	18	E	•	Ð	•	2		
8" PRS1, 302-29	IS.	LPST BEADER		MIN	8	113		¥		2	•	
2 1/2"-51-1524-8	15	70 SI STST#		8414	¥	185	-			2		

### ATTACHMENT F SI SYSTEM APPLICABLE PROCEDURES LIST

10/24/83

rrocedure so.	202220			678,1711, 4483	**************************************
		**COORT CATEGORY CATEGORY	7 th	RESCHOOL SATISCHAUS, STSTANS	51,85,85,87,00,29,05,09,886,888,848,84,84,84,84,84,84,84,84,84,84,8
IST-PROGRAM					SI,SC,M,TR,M,MS
		**(* CONCART STSTEM LEAR SMSPECTION OR SST PRESSURE TRST	SHIP HANNE BEE	の養命をはる情報を	51, 48, CB, CS, MC, SM, SM, SM, MR, MC, RRPS, RSSS
		MONTBLE VALUE & WC PENSTRATION CHECK	C. This is well to be the second	Signal Si	ST, 85, 84, 85, 88, 87, 69, 60, 69, 69, 69, 69, 89, 89, 89, 89, 89, 89, 89, 89, 89, 8
	10	THE OR CHEMISTER OF THE SATETY PROPERTIES WHO PERFORMED BETTER THE THE PERFORMANCE OF PASSES	S THE RESIDENCE	in management of the contract	\$2 <b>LB</b> 2.10
	254 257	EDEED BEST BEST BEST BEST BEST BEST BEST BEST	SHEELCAST OF 1	<b>○●</b> (1) (1) (1) (1) (1) (1) (1) (1) (1) (1)	5550 (50 EE 15) ET 15
		FLUM TEST OF TWO RPSI PORES	System Cast Land	op5441045	#11 100 100 100 100 100 100 100 100 100
		FLOW TEST OF TWO LEST PORTS	SIRWELL METERS. 1	S#:11#21ps	N. 4475
	97	UNDOR CONTINUED DECEMBER OF	SWILL & S. J. 1	## ## ## ## ## ## ## ## ## ## ## ## ##	C. 15.
		00, 80CS FLOW, M	The same of the same	\$ 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	SI, #S. (M. PR. 6875, 6855
		INSERVICE INSPECTION LEAR TEST OF LOW PRESSURE SAFETT INDECTION SELF ONLY.	A DAY NOTE CHARLE	(A) 电影响	5,12
		NA-SERVICE EMSPECTION FLOW TEST OF THE SAFETY INCECTION STSTEM WALRES	503 T (11.00 T 20), 1	が の の の の の の の の の の の の の	21,889
			STREETLANDS AND 1	(4) (2) (4) (4) (4) (4) (4) (4) (4) (4) (4) (4	S1.85, C5, C8, 68, P8, P8, C8, P8, R9, FFF, RC, SC, C8, P8, P8, S55
		TRAVEL TIME OF WOTOR OPERATED VALUES MASTER LIST	1 304 (081)(188)	9.0	51, 15, 15, 15, 18, 19, 19, 19, 19, 19, 19, 18, 19, 19, 19, 19, 19, 19, 19, 19, 19, 19
	101	RECENTED TRYING OF THE WATOR CONTACHDATION LINE CHEMICAL LINE CHICA IN 4-197	1 To 4 and 12 and 12		01 01 01 01 01 01 01 01 01 01 01 01 01 0
		BATTER MICHEL RECEIPED OF THE SAFETY RESPECTATION OF THE SAFETY BOTTOM O		(A)	
	M.	SAFETT INCECTION ACTUATION SIGNAL, ESTASI, CHARMELS FUNCTO-MAI TEST, SPESSA. CALIMANTON AND TOTAL STAS PEPASS OFMENDELTY TEST	The Line of	京の計画を表現でいる。	SI_00_KI_78_00_SR_R_R_S.S.R.R
		SAFETY INLECTION ACCOMPLATOR LEVELS GWITTH OPERATIONAL CHECK AND CHECK OF	A 100 100 100 100 100 100 100 100 100 10		99 44 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4
	10	ALIBRATION OF THE BEST PURP TIME DELAT RELATS	SECTION 10. 1	ASTRUMENTO.	
		FOR THOMAS, TAST OF THE ACCOMMENTAR BITTERINE PRESIDES. BUSINETING AND STATES.	PASSIBLE IN T	**************************************	

\$8/82/61

TABLE AT MICH. THAT IS CONTROL OF THE TRANSPORT OF THAT THE TRANSPORT TO SECURITY OF THAT THE TRANSPORT OF T

Procedure No.	2 · ·		Gratic Takis	SPECIFIC CLASS	STSTUM CODES
4.43	10 10 10 10 10 10 10 10 10 10 10 10 10 1	ACTIVISIATINE BELAT ACTION WEIGHTON TOW	STREET LANGE AND T	(NCTRONSTATION	15
39-4631	14	S.C. WOT USE UNDERTION FROM CHANNEL (ST.P.5) CALIBRATION	100 FEB. 11.08 F. 10 1	(M.CSUMENTATION	
07-4634	THE STATE OF	SAFETT INJECTION ACTUATION BIOR CONTRIBNENT PRESSURE SENSORS (SI -2: 278 ARD). SI -PS: 233; FUNCTIONAL TEST	1 704 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	#OLIVER SERVICE	IX.
67 4535	46	OFERABLIST TESTING OF THE ACCUMULATOR THIS WAINES SI -TW-504, SI-TW-405 AND SI TY-606	STREET IN THE TANK I	*STRUMBANTON	T.
6-500	1	** NATURABLE OF BOTICE OFFERENCE #0.	100000000000000000000000000000000000000	COMBRAG PLANT	ST MS_CS_CR_NM_NR_NS_SM_PR_NCB_ERW_MC_SS_ SW_CC_CC_ERSS_RSSS
1455-4		PREVENTATIVE MAIN	sa efficable:	TENEST STRILLING STSTERS AND STSTERS AND	25
07.138	11 12 13 14 14 15 15 16 16 16 16 16 16 16 16 16 16 16 16 16	ENVIRONMENTAL QUALIFICATION INSPECTION AND MAINTENANCE OF SAFETY INSECTION SHIPSING ROLF FAM NOTORS - SI-FRV-1 & SI-FRV-2	2.9955198	PRINCES SELLINE SESTONS AND DESCRIPTIONS AND	
44-5151		MAINTENANCE OF APSI PURPS OR MOTORS, PAS OR DISCHARGE CRECK VALVE SI-V-30.31.32	Migripada Y	ELECTUR SAFEGRARDS, STSTEMS AND AGRICUATION	W.
44-552	2	**   **   **   **   **   **   **   **	(E. 1888) (E. 18	SECTION SAFEGUARDS, STSTOMS	UT.
66.573	esa esa	(NOFECTION, TESTING AND MAINTENANCE OF CORLS STARTER, BREAKER AND CHITCHS.	1 may 1 m m	ELECTRICAL STSTEMS AND SQSTPMENT	48F 18, 552, 15, 46, 58, 168
27.54		PISCURRECTIRG OF ECCS MOV'S AND SHUTDOWN COOLING WOV'S	(大) (金) (金) (金) (金) (金) (金) (金) (金) (金) (金		55(5, 26, 52, 52, 53, 52, 53, 52, 53, 53, 53, 53, 53, 53, 53, 53, 53, 53
5817-49	40	RECURRECTION OF ECCS MOTOR OPERATED VALUE NO. OR SHETLINGS COLLING TALLE.		PARTERIOR, STSTERS AND SQUIPMENT	H,K,G,885,885
#15-40		DISCOMMENTING/RECOMMENTING OF BOCS/SI-WOW-22,21,24, AND 25 SEEMER GROW CHOT-2.	No.	FLECTRICAL STSTEMS AND	55. 100 100 100 100 100 100 100 100 100 10
W-E3#	10 M	(ALTERATION OF SAFETY RELATED PRESSURE (MOTORINES)	# 51 (\$ 1 m) (\$ 1 m)		SSS "B" SE "BB 'SB" 15
11374	*	MAINTENANCE OF MISSING THE TRANSPORTER.	N.TREGGE 4	78.8837 70.887	11.78.78.7E
14-431	*	BURIC ACID MIN TANN LEVEL INSTRUMENTATION S. C221 CALIBERTION	16/16/2017 4	PATRICK AND CLARK INC. MARKETS	176
15 F F F S S	10 10 10 10 10 10 10 10 10 10 10 10 10 1	CALIBRATIOS OF TRE SI TARK RICH AND SUP LEVEL ALAUR SWITCHES (SI -815-21)/SI-LLS-220)	(a)tale-statica	THE CALL OF THE COLUMN	TA .
	*	CAPETY INSECTION TAME PTR-28) BICATION TRANSMEDIATION CALIFORNIAN ALACH CALIFORNIA	perpendiction	おきまる からの	TA .
Contraction of the last of the	100000000000000000000000000000000000000		3875, 8385, 753	Excts peoples	

16/24/43

THE STATE OF THE S

	TACT CONTRACTOR  TACTA CORPORE  LACTA SCROWN  TACTA SCROWN	INTERNACIONAL DE LA COMPANSIONAL	OF SAGE 5 LEST ACCOURTANG PRESSURE CHANNEL ST.P.S.CALIBRATION OF SAGE 5 LEST INDECTION TANK PROMATIC LEVEL CHANNEL ST.L. 401 CALIBRATION OF SAGE 6 LEST NAME LACTION CHANNEL CALIBRATION ST.L. 1 OF SAGE 7 SAGE 7 TON CHANNEL (ST.F. 10) CALIBRATION ST.L. 1 OF SAGE 7 SAGE 7 TON CHANNEL (ST.F. 10) CALIBRATION ST.F. 1. 2. 3. 4 OF SAGE 7 SAGE 7 TON CHANNEL (ST.F. 10) CALIBRATION ST.F. 1. 2. 3. 4 OF SAGE 7 SAGE 7 TON CHANNEL CALIBRATION OF SAGE 7 SAG	
15	TANTA LABORER	第11年第1年1日1日第1	SAFETY INJECTION TANK PRESENTE LEVEL CHANNEL SI-L-401 CALIFORTION	
IX.	STATE SANGERS	* (17) (1) (1) (1) (1) (1) (1) (1) (1) (1) (1	LTSS ACCUMULATION PRESSURE CHANNEL ST-P-5 CALIBRATION	40
100 mm m	SPETIT SPETITED	第二十二十二十二十二十二十二十二十二十二十二十二十二十二十二十二十二十二十二十	ST ACCEMULATON LEVEL CHAMMERS CALIBRATION (SI-L-3 & SI-L-4)	
	214-718-59503480	一年の一年の日本の日本の日本の日本の日本の日本の日本の日本の日本の日本の日本の日本の日本の	LPS: PURP PISCHARGE BERGER PRESSURE CRAMMEL (SI-P-6) CALIBBRATION	
	E THE ASSESSED.	単される はま はれの事べ	SP 58451	-
5	BETTE CONTINUE	10578988711110		=
	######################################	# C1		fracedure #0. Brw. #0.

### ATTACHMENT G

BRIEF DESCRIPTION
OF
COMPONENT DEGRADATION ASSESSMENT TOOL (COLAT)

### TABLE OF CONTENTS

		Page
1.0	INTRODUCTION	G-1
2.0	DEGRADATION MECHANISMS	G-1
3.0	INFORMATION SOURCES	G-2
4.0	DEGRADATION MECHANISMS AND CONTROLLING PARAMETERS	G-2
	4.1 General or Uniform Corrosion	G-2
	4.2 Erosion/Corrosion	G-3
	4.3 Two-Phase Erosion	G-3
	4.4 Microbiologically-Influenced Corrosion	G-3
	4.5 Intergranular Stress Corresion Cracking	G-4
	4.6 Transgranular Stress Corrosion Cracking	G-4
	4.7 Irradiation Assisted Eiress Corresion Cracking	G-5
	4.8 Intergranular Attack	G-5
	4.9 Srevice and Fitting Corrosion	0-5
	4.10 Thermal Embrittlement	G-6
	4.11 Irradiation Embrittlement	C-6
	4.12 Eydrogen Embrittlement	G-6
	4.13 Selective Leaching	G-6
	4.14 Galvanic Corrosion	G-7
5.0	DATA BASE REQUIREMENTS	G-7
6.0	CoDAT RESULTS	G-7

### ATTACHMENT G

Brief Description of Component Degradation Assessment Tool (CoDAT)

### 1.0 INTRODUCTION

To automate the degradation mechanism review process, Yankee developed an expert system which is used to review fluid system pressure boundary components. The expert system is called CoDAT (Component Degradation Assessment Tool) and performs a detailed evaluation of Yankee plant fluid system pressure boundary components.

Information from other operating plants experience and industry reports related to age degradation of fluid components were used to form the basis for CoDAT.

### 2.0 DEGRADATION MECHANISMS

Eighteen groups (28 specific) of degradation mechanisms were identified that could cause fluid components to degrade. The 28 degradation mechanisms do not include abnormal stressors from such initiators as improper welding techniques, torquing, cleaning, maintenance, etc.

The degradation mechanisms that could affect fluid systems were selected from an EPRI report titled, <u>Component Life Estimation: LWR</u>

<u>Structural Materials Degradation Mechanisms</u>, NP-5461 and from operating plant experiences. Not all of the mechanisms listed in the EPRI report were applicable to the Yankee operating environment.

Of the 18 degradation mechanism groups applicable to Yankee, the 14 groups evaluated by CoDAT are listed in Table 1.

### 3.0 INFORMATION SOURCES

After determining the degradation mechanisms which could be applicable to the Yankee environment, a search was performed to gain further knowledge related to the controlling parameters of each. The search produced a list of information sources which were found to be helpful in predicting degradation of a fluid component. This information was used to develop the rules employed by CoDAT for assessing the 14 degradation mechanism groups mentioned above.

### 4.0 DEGRADATION MECHANISMS AND CONTROLLING PARAMETERS

EPRI Report NP-5461 describes the possible degradation mechanisms for fluid systems. Most of the degradation mechanisms have controlling parameters which are effective in predicting fluid component degradation. Approximately 50 controlling parameters were determined to be effective in predicting fluid component degradation.

### 4.1 General or Uniform Corrosion

General or uniform corrosion occurs to some extent in all metals. However, recent studies done for EPRI (reference EPRI Report No. NP-5461) indicate that certain material groups are not significantly affected by general corrosion for the extension period. The materials that may be affected are listed below:

Carbon Steel
Ferritic Stainless Steels
Martensitic Stainless Steels
Inconel (Wastage)
Cast Iron
Low Alloy Steels
Aluminum

### (Continued)

General or uniform corrosion is characterized by the uniform thinning of a pressure boundary wall to the point where the component's material allowable stress level is exceeded. However, unlike all other forms of corrosion, its rate of progress can be predicted so that exceeding a component's allowable stress is rarely encountered. General corrosion can lead to other forms of corrosion which are not uniform in nature. One such mechanism is erosion/corrosion.

### 4.2 Erosion/Corrosion

Erosion/corrosion is an increase in metal loss due to the relative movement between the process fluid and the metal surface. It is influenced by the rate of general corrosion of the metal surface and is characterized in appearance by grooves, gullies, rounded holes, and valleys and usually exhibits a directional pattern.

### 4.3 Two-Phase Erosion

Two-phase erosion, like erosion/corrosion, is the result of relative motion between the component material and the process fluid. However, in two-phase erosion, the liquid portion of the process fluid is often accelerated to very high velocities by the vapor portion and therefore causes more severe deterioration of the material.

### 4.4 Microbiologically-Influenced Corrosion

The corrosion rate of a material can be accelerated by microbiological activity due to the severely corrosive environment produced by their waste products. The most common bacteria associated with Microbiologically-Influenced Corrosion (MIC) are sulfate reducers, sulfur, iron, and manganese

### (Continued)

oxidizers. Although stagnant areas are most susceptible (for sulfate reducers), components and piping experiencing bulk fluid velocities exceeding 10 ft/sec have experienced MIC because of localized low flow areas.

Although MIC is usually restricted to systems which contain river, lake, potable, or seawater, MIC has been found in fluid systems which are normally filled with demineralized or distilled water because of contamination during pressure testing of the system or inappropriate alignments with contaminated systems.

### 4.5 Intergranular Stress Corrosion Cracking

Intergranular Stress Corrosion Cracking (IGSCC) occurs in austenitic stainless steels when carbide molecules are formed through the combination of chromium and carbon atoms near the grain boundary. The formation of these molecules depletes the chromium concentration around the grain boundary and reduces the material's resistance to localized corrosive attack. The cracking process, as the name implies, proceeds along the material grain boundaries. Improper welding and/or cooling can produce IGSCC. Corrosive environments, such as process fluids containing halogens, can accelerate IGSCC.

### 4.6 Transgranular Stress Corrosion Cracking

Transgranular Stress Corrosion Cracking (TGSCC) is caused by the aggressive attack of halogens on a sensitized austenitic stainless steel component. TGSCC results in cracking that proceeds across the material grain boundaries through slip planes. Another form of TGSCC occurs when copper alloys are exposed to an environment containing ammonia. This type of TGSCC can produce cracking, pitting, and/or grooving, and is prevalent in feedwater heaters containing admiralty brass tubes.

### 4.7 Irradiation Assisted Stress Corrosion Cracking

Irradiation Assisted Stress Corrosion Cracking (IASCC) is very similar to IGSCC, except that all that is necessary to result in IASCC is a high neutron fluence in an oxygenated water environment. Austenitic stainless steel is the only material which is susceptible to IASCC.

### 4.8 Intergranular Attack

Intergranular attack results in a localized corrosion near or adjacent to the grain boundaries. Knifeline attack, which is one form of intergranular attack, is caused by impurities in the component material or a concentration or depletion of alloying elements near the material grain boundaries. This degradation mechanism usually only attacks stabilized, austenitic stainless steels. Another form of intergranular attack is called weld decay. This mechanism is very similar to knifeline attack except that any cracking experienced is located in the weld.

### 4.9 Crevice and Pitting Corrosion

Crevice or pitting corrosion results in extreme localized corrosion in stagnant or low flow areas. Crevice corrosion, as the name implies, occurs in tight crevices, such as those formed between a flange face and a gasket. Pitting corrosion, on the other hand, is caused by an impurity concentration which sets up small galvanic cells and produces a harsh environment that otherwise may not be severe. The impurity concentration may be caused by alternate wetting and drying on the component's surface or by precipitation of a chemical species.

,

### ATTACHMENT G (Continued)

### 4.10 Thermal Embrittlement

Thermal embrittlement of materials results in a significant reduction of the material's notch toughness. For metals, there are several types of thermal embrittlement: 885°F embrittlement of cast austenitic stainless steels, temper embrittlement, strain aging embrittlement, quench-age embrittlement, and blue brittleness. The type of embrittlement which may be experienced is dependent upon the material, special conditioning of the material, fabrication methods, and the operating temperatures experienced by the component.

### 4.11 Irradiation Embrittlement

Irradiation embrittlement occurs because of long-term exposure to neutron radiation. This embrittlement process also causes a decrease in the material's toughness.

### 4.12 Hydrogen Embrittlement

Hydrogen embrittlement occurs as a result of atomic hydrogen (produced during any corrosion process) becoming trapped within a material's lattice structure. The trapped hydrogen prevents plane slippage and, thereby, decreases the toughness of the material.

### 4.13 Selective Leaching

Selective leaching is the result of one element of an alloy being removed by a corrosion process. The most common forms of selective leaching are graphitization and dezincification.

### ATTACHMENT G (Continued)

Graphitization occurs when the iron matrix from a component fabricated from gray cast iron is removed during a corrosion process. This leaching process removes the iron leaving behind the insoluble graphite which has essentially no strength. This process usually takes several decades. However, under certain conditions (i.e., buried piping under severe soil conditions), it can occur much more rapidly.

Dezincification describes a process whereby zinc is selectively removed from brass components. It occurs most often in copper alloys which contain over 20% zinc.

### 4.14 Galvanic Corrosion

In a general way, all corrosion depends upon galvanic action. However, this review will be limited to the galvanic action that takes place when small differentials exist between the solution potential of adjacent materials. Galvanic corrosion can happen rapidly in process fluids which have a high conductivity, such as seawater. In higher quality water, where the conductivity is much lower, the process may still occur, but it will affect a much smaller area and take longer to occur.

### 5.0 DATA BASE REQUIREMENTS

The identified controlling parameters form the basis for a component data base which CoDAT accesses to identify degradation mechanisms which may be present. Each fluid system evaluated is broken into components (piece parts, if necessary), and appropriate data entered for the parameters identified.

### 6.0 CODAT RESULTS

Once CoDAT accesses and analyzes a fluid component's operating and environmental characteristics, a list of potential aging degradation mechanisms is output for each component or part being evaluated.

### ATTACHMENT G (Continued)

CoDAT is presently undergoing a verification and validation process which is scheduled to be completed early in 1990. The results must, therefore, be considered preliminary. Calculations forming the bases of the degradation review, however, have been completed.

### (Continued)

### TABLE 1

### Fluid Component Degradation Mechanisms Evaluated By CoDAT

General or Uniform Corrosion
Erosion/Corrosion
Two Phase Erosion
Microbiologically-Influenced Corrosion
Intergranular Stress Corrosion Cracking
Transgranular Stress Corrosion Cracking
Irradiation-Assisted Stress Corrosion Cracking
Intergranular Attack
Knifeline Attack
Weld Decay

Crevice/Pitting Corrosion
Thermal Embrittlement
885°F Embrittlement
Strain Age Embrittlement
Blue Brittleness
Temper Brittlement
Quench Age Embrittlement

Irradiation Embrittlement Hydrogen Embrittlement Selective Leaching Dezincification Graphitization

Galvanic Corrosion

### ATTACHMENT H

SAFETY INJECTION SYSTEM TYPICAL 1&C COMPONENT REVIEW RESULTS

# YAMKEE ATONIC ELECTRIC COMPANY WWYS LICENSE RENEUA, PROJECT SAFETY INJECTION SYSTEM ILC CONPONENT REVIEW RESULTS

The state of the s	COMPONENT   COMPONENT   COMPONENT   POTENTIAL   WARRANTS     INFORTANT   SUBJECT TO REFURE   NGT   NGE GGRADATION   FURTHER     TO SYSTEM   REFUGENENT OR   SUBJECT TO   RECHARDSTS   EVALUATION     FUNCTION   PROGRAM   RRT   REFECTIVE   IDENTIFIED     FUNCTION   PROGRAM   RRT   RET   RET   RET   REP   RES   REP   RET   RE	EA VES NO NOME VES VES	EA YES NO NOME YES YES YES	EA YES NO NOME YES YES	FI WES NO DP-6476 NO	FI WES NO OF-6470 NO	FI YES NO 09-6478 NO	FI 9ES NO 07-6470 NO	FI YES NO 00-4631 NO	FI YES NO UP-6469 NO	FI WG 07-54-68	FT WES NO DP-6476 NO -	FT RES NO 09-6478 NO	FT VES NO 08-6476 NO	FT WES NO OP-6478 NO	FT PES PES 0P-463! NO	FT NES 0F-6469 NO	
: COMPT	CONFORCIA	<b>a</b>	83	£3	H	11	H II	FI	14	14		H	F	¥ 14	T.	E E	E	E E
	1000	0801 WELT	1082 99.1	0103 001.1	8031 EM	1002 ER	8083 EM	19 F884 ER	89.95 EM	8086	921.00	101 PTE	0#62 PTE	9083 PTE	0804 PTE	8085 PTE	914 9040	9119
	ER DESCRIPTION CLASS	EB-50-1904-27/19 VOLTAGE 6 MOMITOR	EB-SQ-UGA-27/2a VOLTAGE 6 MONITOR	EB-SQ-UGA-27/39 VIR. TAGE 6 MONITOR	1000 EI SI FLOW ST	1000 12 ST FLOW ST	LOGP #3 S1 FLOW ST	1000 14 SI FLOW ST	SI HOT LEG INJECTION FLOW SPT	HPST HEADER FLOW SPT INDICATOR	LPSI FLOW INDICATOR NE HEADER FLOW	LOOP BY ST FLOW ST TROMSMITTER	LOOP #2 ST FLOW ST TROMSMITTER	LOOP 83 SI FLOW ST TRANSMITTER	LOOP #4 SI FLOW TROWSMITTER	SI NOT LEG INJECTION FLOK SEPT TRANSMITTER	HPST HEADER FLOW SEPT TRANSMITTER	LPSI FLOW IRRASMITTER NO
	SWSTEM TAG NO. CODE	15	SI-En 8802 SI	SI-En-0083	SI-F1-0091 SI	SI-F1-0002 S1	SI-F1-0003 SI	SI +1-000+ SI	SI-FI-6865 SI	SI-F1-8806 SI	SI-FI #010 SI	SI-FT-0001 SI	SI-FT 8082 SI	SI-FT 0803 SI	SI-FT-8014 SI	SI-FT-0805 SI	SI-FT-1006	SI-F1-0818

							: STEP 24	••	STEP 28		H SHEP H	
186 NG	#315 kS	DESCRIPTION	CL #SS	1000	4na 45	CORPORENT	COMPONENT RESPONSENT TO SYSTEM SAFETY FORCTION (STEP 20)	COMPONENT SUBJECT TO R REPLACEMENT INSPELT TO R REPLACEMENT INSPELT TO R R REPLACEMENT INSPELT TO R R R R R R R R R R R R R R R R R R R	COMPONENT SEPLACEMENT OR INSPECT TO REFUGE INSPECT TO REFUGE INSPECT TO REPUGE INSPECT TO REFUGE INSPE	COMPORENT AUT SUBJECT TO AM EFFECTIVE WEI PROSENT (SIEP 28)	POTENTIAL INSE DESPOSATION INCOMMISTRE 106N1 F1ED (STEP 2C)	EVALUATION
SI-N.S-6806	15	ACCUMILATOR REFERENCE LES TEL-TALE, SI LEVEL TRANSPILITER	2	988		S III	•	*	09-5463		,	
SI-# S-0219	SI	SI TOWN MCB PARKLARE HIGH LEVEL SWITCH	ts.	6219	₫.	HLS	SQ.	8	1599-40	9		
S1-8LS-8728	SIS	HI LEVEL SHITCH	98	8228		HES	9	9	18-4351	,		
1989-11-18	IS	LPSI PURP BI AMPETER		1908	#ETER	H	9	9	27.84-90			
SI-11-8802	15	LPST PUMP 02 AMMETER		1082		=	8	8	02-6472			
51-11-6893	ts	LPSI PUNP 83 AMETER	2	\$102		=	6	2	2219-80	,		
SI-11-880¢	15	HPSI PURP BI AMETER		1004	ETER	H	9	9	1299-66		-	
SI-11-000S	15	HPSI PUMP 62 AMETER	*	5808	METER	=	9	8	179-471	,		
9080-11-15	SI	HPSI PURP 83 APPETER	9	9999	RELEG	=	98	9	1799-40			
SI-#S-8#91	ES	TIME DELAY MELAY E8-TBC-62/14-54	3£1	1998	RELAY	SI .	£3	9	8194-46	£	Sg.	eg.
SI-KS-8692	15	TIME DELAY RELAY EB-110C-62/29-58	128	9462	PELAY	29	9ES		8197-40	YES	S <sub>2</sub>	Ş.
SI -KS -6463	15	TIME DELAY RELAY EB-TDC-62/34-SC	1438	1083	RELAY	ñ	SQ.	9	819 35	YES	£5	WES
11-11-1041	15	SI LEVEL INDICATOR	165	1089	55	77	465	*	99-9-46	0.	*	
SI-11-8082	15	SI TARK LEVEL INDICATOR	9	6862		1	•	8	09-6216	,		
51-11-8663	SI	SI ACCUMULATOR LEVEL INDICATOR	145	1013	5.	n	WES	9	08-6463	9		
11-1084	155	SI ACCUMUNATOR LEVEL TROICATOR	15	<b>*</b> 989	<b>5</b> 5	3	MES.	2	09-6463	9		
51-11-0221	51	BART LEVEL INDICATOR	•	\$221		п	2	0	186-4351			
51-11-0461	IS	SI TORK LEVEL INDICATOR	œ.	1441		77	0	9	5999-30	-		1
51.111.8401	15	SI TORK PREDMOTTE LEVEL CHONNEL INDICOTOR/TRONOMITTER	9	1878		ш	2	2	(P-6465	•		

### SAFETY INJECTION SYSTEM INC COMPONENT SENTEN RESOLTS

							: STEP 29		STEP 28		: STEP 2C	
	BISAS						I IMPORTANT TO SYSTEM SAFETY FUNCTION	SUBSECT SUBSECT REPLACE INSPECT	CONFONENT SUBJECT TO REFURB REPLACEMENT OR INSPECTION (RRI) PROGRAM	SUBJECT TO AN EFFECTIVE RRI PROGRAM	POTENTIAL NGE DESPROATION NECHANISMS IDENTIFIED (STEP 2C)	FURTHER FURTHER EVALUATION
TAG NO	3000	DESCRIPTION	CL ASS	4601	40049	3000		. 83	: PLANT PROC :	College Car		
SI-LL(A-691)	St	SI TANK LON-LON LEVEL ALARM (8/S)	146	1966	13	111.6	WES	8	999-40	9		
SI-LLS-8081	IS	ACCUMICATOR LOW MATER LEVEL SWITCH	145		158	STI	YES	9	39-4615	9		
SI-LS-8802	SI	ACCURRE ATOR LOW WATER LEVEL SWITCH	15	6802	#5d	SIT	YES	•	8-4615			
SI-LLS-8083	IS	ACCUMUS ATOR LOW MATER LEVEL SWITCH	145	6003	154	STI FILS	WES	9	09-4615	9		,
\$3-1.5-000*	15	ACCUMULATOR LOW MATER LEVEL SWITCH	15	+989	354	SII	£	*	Ø-4615	9	,	
SI-LLS-8220	ES .	ST TONK MEB PRINCIARM LOW LEVEL	15	1228	MS4	SIII	536		1599-20	2		
51-115-6227	IS	RININGH LEVEL SMITCH		6227		STT TES	9		(9-635)			
SI-LR-3221	15	BIRMT TANK LEVEL RECORDER		9221		87		2	09-6351		,	1
SI-LI-1081	SI	SI TAMK LEVEL TK-28 TRANSMITTER	5	1986	H	11	res res		99-9-40	9		
51-11-6603	IS	ST ACCUMULATOR LEVEL TRANSMITTER	145	£608	PIE	n	SQ.	9	DF-6463	9		,
51-11-8684	ts.	SI ACCUMULATOR LEVEL TRANSMITTER	St	1986	PTE	11	465		OF-6463	G.		
SI-17-023	IS	SART TARK LEVEL TRANSMITTER	9	1221		n	0	9	07-6351			
S1-m34-0803	15	ACCUMINATOR OUTLET TSOLATION VALVE	8	9461	URLUE	MON	76.5	8	09-4615	YES	ÆS	\$2
5410-5/4-15	SI	SI HOT LEG POWER SUPPLY	IS	5908	alls	P./5	AES.		06-4631	9		
SI-P/S-8886	55	HPSI HEADER FLOW TRANSMITTER	145	9006	<b>3</b> 5	81/8	WES	9	38-6469	2		
SI-P/S-040?	15	HPSI NEADER FLOW TRANSMITTER	146	1980	\$150 \$150	5/4	ÆS	8	[9+9-40]	WES .	ÆS	£5
SI-P/S-0160	IS	ST ACCUMULATOR PRESSURE (ONE OF FIVE LOADS ON	15	6160	98	818	985	9	0F-6464	755	YES	WES

### YMPAYEE BIRMINE ELECTRIC CHAPAGA YMPS LICEMSE REMEMAL PROJECT SAFETY INJECTION SYSTEM IEC CHAPOMENT REVIEW RESULTS

Colore   C	-	-						1 STEP 24		82 4315		STEP 22	
State   Page State   Fig.						*		1.0 SYSTEM 5.0 SAFEM 5.0 SAFEM 5.0 SAFEM 6.1 SAFEM 6.1 SAFEM	SUBJECT REPLACEMENT OF THE STREET OF THE STR	04EMT 10 ZEF1088 ENEMT 04 DE 110% (02E1) 05E20	CORFORENT NOT SUBJECT TO AN EFFECTIVE RR1 + #60504F	POTENTIAL RECHOMONTOR RECHONISMS IDENTIFIED (STEP ZC)	FUETHER FUELHTIBE
1		SYSTE		CLASS	<b>4001</b>	91049	COMPONENT	; (STEP 24)	4	PLANT PRIC	(Ster 28)		
1	398	15	POMER SUPPLY SF UNIT	15	9979	ATS.	5/4	YES	9	ROME	YES	fes	5
1   1   1   1   1   1   1   1   1   1	SI-P/5-0388	15	POMER SUPPLY RF UNIT 5 (SIP)	ST	9989	408	8/8	HES	9	3000	465	#S	S S
100   10   10   10   10   10   10   1	1480	IS	POMER SUPPLY UF	12	9409	JARS .	PJS	YES		3404	YES	465	\$
100   1   100   1   100   10	1999-14-15	15	LOOP 41 ST PRESSURE	22	1988		H	£		1999-66			,
LOUP 15 SI PRESSURE   NB   CHR2   P1   ND   ND   CF-647	e-1049-14-15	15	LODP B! MC PRESSURE INDICATOR	2	4		14	9	2	1999-40		,	
100   12   17   15   17   15   18   18   18   18   18   18   18	8-1-8	IS	LOGP BI SI PRESSURE	•	8-1080		Ed.	8	9	1999-40			,
1   100P P. 25   PRESSIBEE   RB   100P P. 2   P. 1   RD   RD   RD	962	St	LOOP BZ SI PRESSURE		6862		ä	8	8	1949-40	,		
100	982-A	IS	LOUP &2 ST PRESSURE INDICATOR		9862-n		E	8	•	139-96			
140 FOR 13 FRESSINE   180	862-B	15	LOUP W2 ST PRESSURE		1012-8		E	9	9	DP-6467	•		
1.00P +3 ST PRESSURE	580	15	LINDE RESSURE INDICATOR	9	8403		E	2		08-6467			.
1401CATOR   1401	863-a	125	LOSP 83 MC PRESSURE INDICATOR	*	€083-#		Е	8	9	2999-40			
1400 P4 51 PRESSURE	963-8	IS	LOOP 83 ST PRESSURE INDICATOR		0803-8		E	•	8	09-6467			.
1   16,50 per NC PRESSURE   NB	•00	IS	LOUP B4 ST PRESSURE INDICATOR	9	1108		н	0	9	99-5-67		4	
Statement   Stat	d	15	LGSP 84 MC PRESSURE INDICATOR	w	9		E	•	•	09-6467			
ST   ST ACCURIL, ATOR PRESSURE   ST   0465   EM   PT   VES   MO   0P-6464	8-+00	IS	LOUP B4 ST PRESSURE INDICATOR	*	8-103		н	98	•	99-6467		,	
S1	540	55	ST ACCUMINATOR PRESSURE INDICATOR	15	5940	85	E	£5	8	1999-30	9		
1949-19 (W 23) 14 7/05/ 92 99-6461	902	15	LPSI PUMP DISCHARGE PRESSURE INDICATOR		9069		И	2	9	DF-6462			
	199	15	HPSI PUMP DISCHARGE	9,	2660			£	¥	19+9-46			

### PAPS LICENSE REGENA PROJECT SOFETY INJECTION SYSTEM ILC CORPONENT REVIEW RESM. IS

\* (E

							: STEP 28		STEP 28		SHF A	
9	SWSTER	DESCRIPTION	CL #SS	500)	808	DOMESMENT CONTROL	1 INFORTINE 81 1 INFORTINE 1 IN SYSTEM 1 SAFETY 1 CHECTION 2 (STEP 2A)	SUBJECT REPLIES PRE-	CONFORCAT SUBJECT TO REFUSE REPLACEMENT OR FROGRAM FRO	COMPOSENT 10 NOT	POTEBITIAL MATERIANISTS INDERTIFIED (STEP ZC)	EVALUATION
6466-19-19-12	15	ACCURIU, ATOR PRESSURE INDICATOR	15	8089	45	Id	MES.	8	07-6216	Qu	-1	
SI-69-14-1S	125	HPSI HEADER CHECK VALVE PRESSURE		8010		E	2	8				
SI-PI-2611	SI	LPSI HEADER CHECK VALVE PRESSURE		11100		14	9	8	30			
SI-P1-0612	IS	LOW PRESSURE ST NEADER	15	\$012	PBP	ä	WES	0	09-6216	98	,	
SI-PI-0613	S	HIGH PRESSURE ST PRESSURE	15	1013	æ	I	YES	<b>a</b>	09-6216	9		
97-PI-0520	22	NZ REGULATED PRESSURE TO ACCUMULATOR BI HEADER	ts	08.20	454	14	MES.	8	07-6216	8	,	
SI-P1-0023	IS	NZ REGULATED PRESSURE TO ACCUMULATOR #2 HEADER	15	1021	ABA .	Id	WES	9	84-62116	02		
SI-PI-2022	IS	NZ REGULATED PRESSURE TO ACCUMULATER A3 HEADER	15	9472	454	id	ves	9	09-6216	9		
87ee-1d-1S	SI	ACCUMULATOR 1859 N2 SUPPLY TO TRIP VALVES		<b>6</b> 028		ı	•	9	M. M.			
SI-PI-0029	SI	ACCUMILATOR SOOD NZ SUPPLY TO PELIEF VALVES		6236		14	9	8	07-6216			
SI-PI-063#	IS ST	RI LPSI SUCTION PUMP PRESSURE INDICATOR	2	9E 94		E .	•	9	¥			
51-PI-0031	SI	RI HPSI SUCTION PURP PRESSURE INDICATOR		0431		E	§	8	300			
SI-PI-8832	SI	#2 LPSI SUCTION PURP PRESSURE INDICATOR	2	<b>8</b> 632		=	R	9	¥			
SI-P1-0033	SI	PRESSURE INDICATOR	9	6433		14		8	¥			
1-P1-0#34	55	#3 LPST SUCTION PUMP PRESSURE INDICATOR	22	#E00		E .	•	8	¥			
SE-84-14-15	15	N3 HPSI SUCTION PUMP PRESSURE INDICATOR	9	0435		E .	9	•	¥		,	,
8590-84-15	S	#2 HEADER PRESSURE	15	8968	30.00	8:	YES		D5-4622	24.5	536	MG.

YMMKEE BIUNIC ELECIPIC CUMPANY
YNDS LICENYE RENEMA. PROJECT
SAFETY INJECTION SYSTEM IEC CONFONENT REVIEW RESULTS

							STEP 24		STEP ZB		R SHP R	
746 ¥0.	3400 #31588	DESCRIPTION	CL #SS	4007	\$100	3000 19366#03	COMPONENT IMPORTANT TO SYSTEM SAFETY FONCTION (STEP 24)	** ** ** ** ** ** **	COMPONENT SUBJECT TO REFURB REPLACENENT OR INSPECTION (RRI) : PROGRAM EQ : PLANT PROC.	COMPONENT NET SUBJECT TO AN EFFECTIVE INCL PROGRAM (STEP 28)	POTENTIAL MAGE DEGRADATION MECHANISMS IDENTIFIED (STEP 2C)	EVALUATION
6588-84-1S	IS	11 HEADER PRESSURE REDUCER TO ACCUMULATOR	15	6508	VALVE	2	WES	9	06-4622	465	FES	WES
S1-PR-8682	IS SI	N3 HEADER PRESSURE REDUCER TO ACCUMINATOR	St	0602	30.360	æ	£	•	09-4622	8	res	ē.
SI -Pg -B613	22	ECCS ACCUMILATING SOU LOS NO SYSTEM BOTTLE PRESSURE REGULATOR	ø	1613	VALVE	25	£	8	¥	MES	WES	SS.
SI_Pg -6614	5	ECCS ACCUMILATION SON LINS NZ SYSTEM BOTTLE PRESSURE REGULATOR	y.	2	VRVE	22	WES		¥	Ş.	4ES	\$2
SI-PS-0007	15	ACCUMULATOR HIGH PRESSURE SMITCH	15	19987	38	82	WES	9	92.99-40	0		
SI-PS-#816	IS ST	HPSI NEADER CHECK VALUE		6110		\$2	9	•	¥0¥			
SI-PS-6811	15	LPSI HEADER CHECK VALVE LEAK ALARM	9	1196		82	•	•	*		,	
SI-PS-8020	15	LEM NZ PRESSURE SMITCH #3 SUPPLY HDR	ST	0828	25	82	YES	8	00-5476	9		
SI-PS-6923	ES .	HIGH W2 PRESSURE SAITCH #3 SUPPLY HOR	15	9021	35.	82	ves.	9	BP-6476	9		
SI-PS-0622	25	LOW NO PRESSURE SMITCH NO SUPPLY HER	ST	0112	2	82	WES.	2	87-5476	9		
\$1-85-8023	IS	HIGH NZ PRESSURE SHITCH NZ HEADER	ts	8623	3.	82	£	9	0P-6476	<b>a</b>		
NZ90-5- 15	15	LOW NO PRESSURE SMITCH BY SUPPLY HEADER	215	6624	25.	25	WES	•	97-6-76	0		
SI-PS-0#25	SI	HIGH NZ PRESSURE SHITCH BI SUPPLY NEADER	15	\$0.05	Z.	٤	YES	9	97.99-40	9	,	,
SI-PS-8026	25	130 LB W2 SUPPLY TO TRIP VALVE HIGH PRESSURE SER	9	6826		٤	•	9	0F-6476			,
SI-PS-8827	Ami L/C	N.2 LOW PRESSURE SWITCH FOR LOB LB NZ SUPPLY TO	2	\$627		82	9	9	00-5476			4

### YANKEE ATOMIC ELECTRIC COMPANY VMPS LICENSE REMEMAL PROJECT SAFETY INJECTION SYSTEM ISC COMPONENT REVIEW RESULTS

		***************************************					: STEP 28		STEP 28		: STEP 2C	1
ar =0	SYSTEM CODE	DESCRIPTION	CL ASS	1000	GROUP	COMPONENT CODE	: TO SYSTEM : SAFETY : FUNCTION	REPLI	HPONENT : CT TO REFURB : ACEMENT OR : CTION (RRI) : PROGRAM : PLANT PROC :	COMPONENT WOT SUBJECT TO AN EFFECTIVE BRI PROGRAM (STEP 28)	POTENTIAL See DEGRADATION MECHANISMS DENTIFIED STEP 2C	: WARRANTS : FURTHER : EVALUATION :
¥6 ₩0.		See LB N2 SUPPLY TO	ST	0028	PSM	PS	YES	₩Đ	0P-6476	₩0	-	
I-PS-0028	SI	SAFETY VALVE HIGH PRESSURE SMITCH										
1-PS-8029	SI	SOO LB M2 SUPPLY TO SAFETY VALUE LOW PRESSURE SMITCH	ST	0029	PSN	PS	YES	MO	0P-6476	*0	-	-
51-PS-0030	SI	M2 LEAK ALARM FOR SI-TV-0608 PRESS SMITCH (2 LB INCREASING PRESSURE)	<b>#</b> 0	0030		PS	₩6	#0	GP-6476		-	
51-PS-0238	S1	HIGH PRESSURE SI ACTUATION	901	8238	PSN	PS	VES	<b>#</b> 0	0P-4634	₩0	-	
S1-PS-0239	SI	SI ACTUATION SWITCH	901	6239	PSW	PS	YES	MO	0P-4634	<b>₩</b> B		-
SI-PT-0001	SI	LOOP #1 SI PRESSURE	<b>W</b> O	0001		PT	₩0	₩0	0P-6467	-	-	-
S1-P1-0002	SI	LOOP #2 ST PRESSURE	<b>M</b> 0	0002		PT	₩0	₩0	OP-6467	-	-	
S1-PT-0003	SI	LOGP 03 PRESSURE TRANSMITTER	₩0	0803		PT	₩0	₩0	3P-6467	-		
SI-P1-0804	S1	LOOP 04 ST PRESSURE TRANSHITTER	*0	8984		PT	₩0	MS	OP-6467			
S1-PT-0005	SI	SI ACCUMULATOR PRESSURE TRANSMITTER	12	0005	PTE	PT	YES	₩0	GP-6464	#0		-
SI-PT-0806	\$1	LPST PUMP PRESSURE TRANSMITTER	MB	0006		PT	<b>M</b> O	<b>N</b> 0	0P-6462			-
S1-P1-8687	SI	HPS1 PRESSURE TRANSMITTER	SP	0007	PTE	PT	YES	₩0	0P-6461	₩0		
S1-S0Y-0845	SI	CLOSES SI-TV-0608 LOW ACCUMULATOR LEVEL	6	0045	VALVE	SOV	YES	₩0	0P-4615	YES	YES	YES
S1-S0V-8046	\$1	TRIPS SI-TV-0684,0605,0606 M2 ACCUMULATOR	6	9046	VALVE	990	VES	NO	9P-4636	VES	VES	VES
S1-S0V-8047	\$1	N2 TO ACCUMULATOR S1-TV-604,605,606	6	9947	VALVE	SON	YES	*(	0P-4636	YES	YES	YES
51-589-085	\$1	ACCUMULATOR SAFETY VALVE	51	6856	SAFAE	204	YES	*	0P-4615	YES	YES	YES

### YANKEE ATOMIC ELECTRIC COMPANY VAPS LICENSE REASKAL PROJECT SAFETY INJECTION SYSTEM INC COMPONENT REVIEW RESALTS

### MANKEE ATORIC ELECIBIE LURPANY MAPS LICENSE REBENAL PROJECT SAFETY INJECTION SYSTEM ILE CORPONENT REVIEW RESULTS

10   10   10   10   10   10   10   10									2000		Creekings	: POTESTIAL	Baggaars
State   Stat								INFORTANT ID SYSTEM SAFETY FUNCTION	SUBJECT SUBJECT REPLACE TASPECTT	7.0 RETURE :	SIGNET TO AN EFFECTIVE SELPROSPICE	RECHAPISTS RECHAPISTS RECHAPISTS RECHAPISTS RECHAPISTS	FUNTAGE EVALUATION
State   Accountainty line digital   State		SYSTE		CL ASS	1006	9998	COMPONENT	: (S)EP 2B)	1	LAST PROC.	Office de		
State   Stat	9503	15		9	6803	RELAY	100	ÆS.	•	06-4638	¥65	S S	res
1   12   12   12   12   12   12   12	1000	15	ACCUMULATOR TIME DELAY RELAY	9	<b>103</b>	RELAY	100	WES	9	06-4636	455	Ş	MS .
State   Stat	1728	25	TEMP INDICATOR BORIC ACID RIX TRAK	8	0220		=	9	9	100E			
State   Stat	1223	Si	SI TABIK TEMP	ST	623	P51	=	YES	8	300	YES	#ES	48
Countries Free Free Free Free Free Free Free Fr	<b>6</b> 223	IS	SI TANK TK-28 HIGH/LOW TENP INDICATING ALARN SWITCH	ts ts	623	350	118	MES.	8	15-94-Si	9		
State   Countries   Preserve Protest	1003	15	CONTROLS PRU-1 POWER ROOF VENTILATOR VIA ENCC 43 - ASSOCIATED DAMPERS	H	100	2	53	£5	£\$	06-6853	9		
State   Courted to the particle particle   Motor   M	1892	ES	COMPROLS PRU-2 POMER ROOF VEHTLATOR - ASSOCIATED DAMPERS VIA ENC. 84	bs	200	#5d	13	SQ.	4ES	gp-4853	9		
Strictory March   1879   187	9863	15	CONTROLS UV-1 UNTI	9	1003		52	9	9	DF-6853			
State   Stat	9084	15	ST BLDG HIGH TEMP ALMPR	2	<b>&gt;</b> 0 <b>8</b> 0		15	8	•	07-6853	,		
State   Stat	1684	25	N2 TRIP VALUE #1 HDR T9 ACCUMULATOR	15	96.84	MUE	R	WES		06-4636	465	ş	9
SI	16.05	55	NZ TRIP VALVE OZ HDR TO ACCURUZATOR	ST	8685	VRVE	2	YES	2	98-4636	455	WES	£
S1	9896	15	NZ TRIP VALVE NS HOR TO ACCUME ATOR	ts	5686	WIVE	1.0	£	8	07-4636	YES	WES .	£
SI 11 LPSI V78PATION CH X NEB 0401-A UN NO	9898	SI	NZ SHUTOFF TO ACCURULATOR ON LOW LEVEL	15	8898	VALUE	2	#ES	9	07-4615	#ES	YES	SE .
SI #1 LPSF VIERATION CH X NG 0001-A UN NO NO SI #1 LPSF VIERATION CH X NG 0001-A UN NO NO NO CH Y PULM PIECEIP	1908	15	#1 LPSI V-BRATION MONITOR	w	1680		5	•	6	308	-		
SI BILPSI VIBRATION MONITOR NE COSI-8 UN UN NO NO NO CH Y PURP PICKUR	n-1990	15	BI LPSI VIBRATION CH X HOTOR PICKUP	9	#-1080		5		•	W.			
	8661-8	- E	#1 LPSI VIBRATION MONITOR CH Y PUMP PICKUP	<b>9</b>	8-1695		5	2	•	*			

### WHY LICENSE RENGHAL PROJECT SAFETY INJECTION SYSTEM HE CONFONENT REVIEW RESULTS

							1 STEP 24	**	8Z 431S		1 STEP II	**
	and					000	COMPONENT HIPPORTANT TO SYSTEM SAFETY FUNCTION		CONTONENT SUBJECT TO REFURB REPLACEMENT OR INSPECTION (PRI) PROGRAM	COMPONENT ROT SUBJECT TO ROT EFFECTIVE ROT PROSEM	POTENTIAL SAFE DECREDATION RECHANISMS IDENTIFIED (STEP 2C)	KARPONTS FURTHER FURTHER FVALUATION
TAG NO	3400	DESCRIPTION	CL #SS	1036	GROUP	3000	1	. E0	: PLANT 790C			
S1-1%-8682	S	12 LPSI VIBRATION MONITOR		6862		5			*			
SI-UN-8082-n	55	62 LPSI VIBRATION MONTION CH X MOTOR PICKUP	•	0\$62-R		5	2	8	¥			
SI-VM-8582-B	15	#2 LPSI VIBRATION MONITOR CH V ZUMP PICKUP	2	1017-8		5	2	•	¥		,	1
SI-1# - 6013	15	#3 LPSI VIBRATION MONITOR		6463		5		*	300			,
SI-UR-803. A	SI	#3 LPSI VIBRATION NOMITOR CH X MOTOR PICKUP		0803-A		5	2	•	¥	1	1	
SI-VM-0603-8	53	#3 LPSI VIBRATION NONITOR CH V PUMP PICKUP	•	9683-B		5	9	9	¥		1	
S1-UN-0004	22	*1 HFST VIBRATION ROWITOR		1010		5	•		×			
SI -18-8084-G	Ti.	#1 HPSI VIBRATION NOMITOR CH X NOTOR PICKUP	•	g-1086		5	•	*	¥		,	
8-1080-15	15	#1 HPS1 VIBRATION MONITOR CH V PUMP PICKUP	9	87		5	9	8	×			
SE-VM-6855	15	#2 HPSI VIBRATION NOMITOR	20	5949		5	•		*			
SI-UM - 8085-A	5	#2 HPSI VIBRATION NOWITOR CH X MOTOR PICKUP		#-5986		5	•		¥		,	
81-18-4865-B	E	62 HPSI VIGRATION NOWITOR CH V PUNE PICKUP	2	8-5808		•	9	•	*			
51-tm-0006	15	83 HPSI VIBRATION MONITOR		9116		5	2	*	¥			
51-4M-8586-A	15	#3 NFSI VERRATION MONITOR CH X MOTOR PICKUP	9	6.6989		5	•		*	1	1	1
SI-18-9696-8	IS	43 HPSI VIBRATION MONITOR CH Y PUMP PICKUP	2	F-592		5	9		¥		-	
THE PERSON NAMED IN COLUMN 2 IS NOT	SAME AND ADDRESS OF	· · · · · · · · · · · · · · · · · · ·	WHITE MAKE	the state of the latest and the late	OR OTHER DESIGNATION OF THE PERSON NAMED IN COLUMN TWO IS NOT THE PERSON NAMED IN COLUMN TWO IS NAMED IN COLUMN TWO IS NOT THE PERSON NAMED IN COLUMN TWO IS NAMED IN COLUMN TWO IS NAME	一年十二十二十二十二十二十二十二十二十二十二十二十二十二十二十二十二十二十二十二		The second lives and the	The same of the same of	The second secon	The second name of the second na	

### ATTACHMENT I

EMERGENCY ELECTRICAL POWER SYSTEM (EEPS)
COMPONENT REVIEW RESULTS
REVIEW RESULTS

**	ACCEPTION HAPPEDIS ACCEPTION HINES ACCEPTION HINES INCHASISES (SIEP ZC)	•		•	•	ars res		WES WES	YES YES	HES HES	WES WES	•	8	8	
STEP X						#ES		£	465	\$	<b>£</b>				
	BETS BETS WES WES WES SEED OF					SA MES		2	8	2	2		,		-
	CORPORATS POTENTIAL AGE PLESSIBLE RECHANISMS RECHANISMS			,		465		483	5	\$	\$5				
	1 2					FE S		\$	2	5	£ .		t		
**	SMETTIVE REL PROCESSES	1		9	2	£	Q#	WES	ð	WES	594			•	
82 dats	CORPORENT SUBJECT TO RETURN DEPLACEMENT OF THE PROCESSION	PLANT PROPERTY.	96-436	96-4751 39-4586	07-4251	*	99-5812	19-5759 117-5756	09-5758 09-5756	99-5268 09-5756	99-5268 89-5756			97-5358 87-4387	
	SUBJECT PROPERTY PROP	90.00	9	9	•	9	£	8	9	YES	<b>8</b>			•	
: STEP 24 :	CORPORENT   10 SYSTEM   50 S		945	46	*6	MES.	WES	#FS	S.	£	YES	9		46.5	
	CONFORCIA	3003	6	88	8.8	2	84.6	ĩ	4	ŭ	8	•	2	ı	
		app. ICaTION	4881 FOKE	4880 POER	4880 POKER	488V TPOMSEEP	1860 TRANSFER	ē	Far	Tā.		FOR	<b>5</b>	# Sales 1	
		1496	BVEAREP	BECORER	BPEARER	SWITCH	SHITCH	#810k	MD 109	#810\$	#010k	20108	10100	20106	
		Cataboay	CTRL & PROT	CIRL : PR01	CTRL & PROT	CTRL & PROT	CTR. 6 PR01	9001	1000	1000	1960	1.046	108	1946	
		DESCRIPTION	486V EBUS-1 TO BUS-6-3 TIE ACB	488V EBUS-2 TO BUS-4-1	488V EBUS-3 TO BUS-5-2	MARGINE THPRINDVER SW NO 1	REGING THROMOUTE SM NO 2	CONTROL ROOM ENERGENCY ATR CLEARING FOR	CONTROL ROOM ENERGEMENT	DGB ROOF EXH FAR	DGB RODE EXH FAS (EMEDGE MCV)	SSS BUILDING UENT FAR	DGB UNIT VENTILATUR	EBG-1 DIESEL LOMSER MOTORS	
		CODE	EE	£	R R	EEPS	EFFS	83	EEPS	EFS	EF8	EFFS	£ 3	EPS .	
		Ta6 #0	aCB - L1-18	ACB-81-78	ACB-81-38	¥-10-1	58. 19-2	FR-5-1	FR 9-2	SI FPW-1	SI-PPU-2	\$55.0F.5	9-20	EDG-E VRE-1	

									SMERT TO BETTOR REPAIRENT OF TREPETTOR (881)	1887 04. FT 10 88. FT FT 10 88. FT FT FT 10 88. FT		COMPRESTS POTENTIAL ACT DESCONTING RECHANISMS	E . E .	ME DEGRAPHIA MECHANISMS INCHAIRED (STEP ZC)		TREES CONTRACTOR
TAS #6	SYSTER	# DESCRIPTION	CATAGORY	¥.	APPLICATION	COMPONENT	: (STEP 24)	2	: PLANT PROC	(SEP 28)	110:		DIE : MEM : COM : 244	72		
EDG-1 WE . 3	E	EDG-3 DIESEL LOUVER HOTORS	1660	<b>*</b> 010*	Letrier	£	SP.		(P-5359 (P-4207	8					•	
7.48.1	£	LOW PRESSURE SAFETY INS	8	<b>9</b> 010 <b>9</b>	<b>8</b>	•	88	€	9-434 9-434 9-434 9-585 9-435	•					2	
P-48-2	8	LOW PRESSURE SAFETY INS	3	8	į.	e	₽.	\$	9-424 9-424 9-424 9-424 9-424	•		,		,	2	
£ .	E	LOW PRESSURE SAFETY INJ	1 (800	4010#	P.		¥	Ð	99-4284 99-4234 99-4234 99-5352 99-5352	2					•	
2.44	£	HIGH PRESSURE SAFETY IND. LOAD PP. 1	9701 0	A010A	b .	2	ş	8	#474 #478 #478 #478 #478 #478	9				1	2	
9.48.2	£.	HIGH PRESSING SAFETY INJ	9807 18	#010# #0	•	8	85	\$2	# + 23 # + 23	:	1				•	
F 49-3	25	PP 3	983	9.	1	8	8	₽	# 55% # 45% # 45% # 45%	•				*		
60 0.	EFFS	SSS SECONDARY MILE-UP PUMP	1001	distri	1	110	534	•	(# 4753	*					•	

SAMEE ATORIC ELECTREC CONTANY
SAWS LICENSE REMEAL PROJECT
PROJECT
PROSENCY ELECTRECAL POWER SYSTEM COMPINEENT REVIEW RESULTS

Column   C								STEP 24		STEP 28		**		STEP X	×	**
State   Stat	Š									POREST 1 10 REFURE CERENT OR 110M (9R1) : POSPAN	COMPONENT  BOT  SUBSTICT TO  EFFECTIVE  BOT  POSSESS  CUTTO NO.		CONTRACTOR	E	POTENTIAL AGE NECESSATION MENANTSHEE INCOMENSE (STEP ZC)	
State   Stat	93		-	Calasory	TYPE	aPPLICATION	1	1000	93	FLORT PROC	( Dic)	310		96: 98		
555 STATEST MACE, IP THE TOO T	433			900	M0.764		ŧ	AES		07-5758 07-4253	•					9
Character ware   Line   miles   1942   miles   1944   miles   19	EE.			DAD	#010#	<b>8</b>	Ĕ	WES	2	¥	¥ES	#ES	1		945	Wes
CHAMPLESS   CHAM				<b>Q</b>	8	78.05	a i	af S	8	07-4703 07-4233 07-4533 07-4537 07-5301	•					9
CHARGI-STATE UNIVER LIMPO INDIGE WRITE 1980 1994 1894 1994 19	<b>B</b>			98		VALVE	•	Ş		99-4733 99-4518 99-4517 99-55181 99-4517	2					2
S   1 P RECENC   LOGAD   MINTON   VARIETY   NEES   MID   NEES   NEES   MID   NEES	Ē			8	90	Part of	:	<u>\$</u>	2	115 b	•					•
1,0040   m5100   M4100   m110   m12   m12   m12   m12   m12   m13   m14   m15   m14   m15   m1	E.			98	8	NA UE	a .	ğ	8	92-4283 92-4283 92-4588 97-4587 97-4587	•		4			9
LOND METOR VALVE ATTR WES (PC-4708 M)  COMPANY ATTR WES (PC-4708 M)  OP-4701  OP-4501  OP-4501  OP-4501	à			980	9	g R	1	ž.	8	AP-5356 0P-4383 0P-4518 8P-4517 0P-5181	•				1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	9
1890 Me109 UNLUF NTS VES (NE-4209 M)	EE			98	M010#	124 VE		•								•
	B	PS LPSI PATH ISO URLUE		(Md	M+109	DBI, 24	ž.	#E	\$5	07-424 07-424 07-4518 07-4517	•					•

## VAPS LITERAS PERSONE PROJECT VAPS LITERAS PERSONE COPOSENT REVIEW RESOLUS

FIGURE :	-									
		8	2	8		•	8		2	•
POTENTIAL AGE DESMONTING MECHANISMS INCOTTERED CSIEP ZO				1			,			
** ** ** ** ** ** **				,	7					
CORPORENTS POTENTIAL ACE DECREDATION RECHARATISMS							1			
CONTRACTOR POTENTIAL MCC. DEGRACATION RECHARISMS		•					,			1
** ** ** ** ** **	-			1						
SUBJECT TO AND STREET TO AND STREET TO STREET TO STREET TO STREET TO STREET TO STREET TO		9	•	•	8	2	9	8	•	6
CORPORENT SUBJECT TO REFURE PEPLACENCY OR PRESECTION (RPI)	P. SALL PROP.	97-428 97-428 97-458 99-4517 97-5101	09-428 09-428 09-4518 07-4517 09-5101	95-478 97-478 97-4518 97-4517 97-5181	92-428 92-4518 97-4517 97-5181	98-5356 98-4517 98-4211	#P-5356 @-4517 @-4211	09-5356 09-4387 09-4517 09-5758 09-4211	97.4233 97.4233 97.4537 97.5538 97.5538	08-4733
	2	8	8	8	8	8		8	•	
10000000000000000000000000000000000000		¥	SP .	ð	ş	£65	MES.	Ð	£	PES
Descond Company	5006	•	61 E		ă.	4	2	•	•	218
	APVLICATION	20.00	VALOE.	展展	VRR 15	92 F	38.05	VA. VE	25 AC	361.06
	TVPE	91.0	#016#	80108 8	91.0	8) 1 (8	8) T(8)	9.16	#37168	301.03
	CATAGORY	0001	961	1080	961	1000	1930	10%	9901	gw() 1
	DESCRIPTION	11.05 1.00P F711 WALVE	EFFS LOOP FILL WALVE	LOOP FILL WALVE	EEPS LOOP FILL WALUE	ENER BOILER FEED WALNE	ERER BOILER FEED WALVE	ENER BOILER FEED UNLUE	ATRS STR DURING WU	OF CAMP CTM DAMP I'U
	CODE	11 5432	1 838	EFS 1	1 5433	1 5433	8 248	E E E	EFFS	26.11
	TAG #0	S-1004-0536	TS-WW-837	SS-MW 4538	PESS (CS-MOR-S2)	EBF .NOV.1555	EBF - MOV-855.6	EBF-#08-#557	MS. MIV 0659	

NAME E ATOMIC ELECIPIE CHRAMM

VARS LICENSE REMEAL PROPET

VARS LICENSE RESEAU PROPET

VARS LICENSE RESEAU PROPET

VAR SELECTORICAL POMER SYSTEM COMPONENT REVIEW RESIRIS

Calaggey
983
9801
85
907
981
1920

## HAPS LIEGASE PERENAL PROJECT PROJECT PROJECT PROJECT PROJECT PROJECT PROJECT COMPONENT PROJECT PROJECT COMPONENT PROJECT PROJECT PROJECT COMPONENT PROJECT PROJECT PROJECT COMPONENT PROJECT P

1	FINE FINE FINE FINE FINE FINE FINE FINE										
			8	8	8	2	9	2	2	•	•
10.14	POTENTIAL RECHARGES TREATFRED CSTEP 2C)							•			
	** ** ** ** ** ** **					,					
-	FR 15			,							
	COMPUSENTS POTENTIAL AGE DECEMBETION RECHARATIONS RECHARATIONS		,	,			1		,	,	
.				,							
	SUBSECT TO STREET PROGRAMM (STEP 20)		8					8	9	8	8
	((PP) DECRIT DECRICATION (PRI) PROGRAM PROGRAM EQ.: PLONE PROC	00-4283 00-4288 00-5881	09-4733 09-4518 09-4517 09-53191 09-4215					07-5356 07-4518 07-4518 07-5181 07-5181	00-4518 00-4518 00-4517 00-5518	# -5356 (# -4283 (# -4518 (# -4517 (# -5181	# 5356 # 473 # 4283 # 4283 # 4518
	COMP. SUBJECT PREVIOUS PREVIOU		8					哥	•	9	MES.
. N.C. CR .	COSPORENT HWORIDAT 14 SWSTER SAFTY FUNCTION (STEP 24)		<b>9</b>	9	8	•	•	£	Ř.	Ş.	\$
	CONCUR. 01		E	£	218	×	2		:	1	
	#PPLECATION		VR.66	WALVE	DRUE	36.786	URI VE	30 00	ar Ar	Well VE	36136
	146		8	#010P	NI N	#910#	90108	9010	85	30108	30 145
	CATAGORY		0001	1000	0001	1690	1000	680	8	9893	(two
								UV BISCHARGE HOR REDCK LOND			
	0.657.0 PF110W		S 1 # -LP TIE	EFFS 1000 4 FILL 810CE	1009 3 FILL BLOCK	1.00P 2 FILL BLECK	EEPS LOOP I FILL BLOCK	S 1 915080	SINTELL INJECTION VALVE	S 1 LP RECIPE	SAFETY INJECTION VOLUE
	SYSIE		EFS	EEFS	EPS	HE SE	EEFS	88	8	E S	603
			*028 AG* -15	12.00 Mg-15	SI-800-0823	SI-#674-8024	SI-MOV-0425	9702-008-15	8#9¢ //D#-15	6448 VOR 12	*:56.40 <b>%</b> :55

### YMPS LICENSE REMEMAL PROJECT EMERGENCY ELECTRICAL POMER SYSTEM COMPONENT REVIEW RESULTS

							: STEP 2A		STEP 26		*			STEP 2	c	
	SVSTEM					COMPOSER	: FUNCTION	SUBJECT REPLAC 1 NSPECT	IN REFURS EMENT OR ION (RRI) POGRAM	COMPONENT NOT SUBJECT TO ON EFFECTIVE REI PROGRAM (STEP 28)	:	POTEN NGE DEGA MECHAN	ABATION ISBS	:::::::::::::::::::::::::::::::::::::::	POTENTIAL  AGE DEGRAPATION  MECHANISMS  TOERT IF IED  (STEP 2C)	EVALUATION
86 NO	C80E	DESCRIPTION	CATAGGRY	TYPE	APPLICATION	EODE			PLONT PROC				: 0000			
									0P-5758							
									gP-5101							
1-M0V-0515	EEPS	SAFETY INSECTION VALVE	E090	M0 10R	VALUE	MTR	VES	VES	AP-5356	*0	-					#6
									09-4233							
									0P-4203							
									DP-4518							
									8P-4517							
									0P-5758							
									0P-5101		-					
1-809-9516	EEPS	SAFETY INJECTION VALVE	L980	<b>M</b> 0169	VALUE	MIR	YES	₩0	6P-4233	*9		-	-	-		₩0
									SP-5356							
									6P-4263							
									OF-4518							
									0F-4517							
									0P-5758							
									OP-5101							
1-MOV-0517	EEPS	SAFETY INJECTION VALUE	LOND	M010R	VALUE .	MIR	YES.	*1	ar-5356	₩0				-		<b>9</b> 0
									5P-4233							
									9P-4293							
									DF-4518							
									9P-4517							
									0P-5758							
									GP-5191							
S1-MOV-0518	EEPS	SAFETY INJECTION VALVE	£040	M) T(M	VAL VE	#1g	YES	**	OP-4233	•0	-					WG
									AP-5356							
									09-4293							
									0P-4518							
									9P-4517							
									10P-5758							
									OP-5101							
VD-MOV-0559	EEPS	REACTOR VENT VALVE	1000	M016F	VAL LE	WIR	YES	WES	0F-4203	₩0						M6
									MP-5356							
									GP-4518							
									89-4517							
									0P-5758							
									DF-5181							
									8P-4262							
VD-MOV-0561	EEPS	PERCTOR VENT BLOCK VALVE	FORD	HI) ((F	<b>४५</b> ए	#19	WES	YES	0F-4262	₩9		4				₩6
									W-3356							
									OP-4263							
									87-4518							
									IP-4517							

		•	•				res	2		•	•	•	*	2		
	# 150 PR			1			\$									
YAIS							2									1.
	E				1.		455									
	COMMENS. MICHIGAN MIC					1	2				1		1.			
	# E						\$	1.								
	# 1916 W   1816	8		8		8	*ES	*	•				•	*	•	*
2 415	. B. S. E	16.4.90	1810	187.6	\$185: 46 \$23: 46	\$ 4750 \$ 5888	*	2185-46	07-5758 07-5812	87.5817 97.5758	95-578	\$ 573	85.528	2185 48	285-20	3.43
	SECTION IN SECTION IN PROCESSION IN PROCESSI		9					150		8				# FS	\$2	W.
2 1215	00 SSTR 00 SST	ð	g.	\$9	\$	\$53	ę	165	\$	#ES	<b>S</b>	M75	9	150	23	320
	ţ×	AUS	ags.	A		k	336	2	¥	33	<b>118</b>	¥	¥	¥.	¥	25
	**************************************	MAK	**	18.15	4.364 36 VIST	(28v at 7967	690 7969	1364 1469	1364 166	490 FIEE	4960 PREE	4364 A889	PINCE DISTR	99£1 01518	2500 000a	STORE DURCE
	Ē.	61 G-60 155	301(40)(5)	33184616	HVENT	1916.9189	¥.		*	W.C.	336	acc.	33	¥tt	*	A THE PLAN
	Catadore	8	85		THE COMMENT	183863	1		1			1	SWITCHES	SWITCHES	SHITING AN	Service Sc
		5	2				1 (B16) 9	5 83483 1	CONTR. S	1 CENTR 5	A CONTRO S	A CENTER S				,
	9650819110	SOLEWID	SOLEWID	SOLEMID	VIIA INCREE !	VITAL LANCETER 62	480V NOTOS CONTROL CENTER SALITORGEA	488V MOTOR CONTRA CENTER SMITCHES	ASSUMPTION CONTROL CENTER SMITCHEORE	488V NOTOR CONTROL CENTER SHITCHEEN	+30V MOTOR CONTROL CENTER SALICONGE OR	498V MOTOR CONTROL CENTER SWITCHEES	SAFE SHUTDOW R.DS	4810 METTON SECTION	480V VERTICAL SECTION	
	# M				E 23	E SA BE	EES .	E 2	E 2	8	E 24	83	8	£ 533	5433	2
	8.8	848	E E E E E E E E E E E E E E E E E E E	E	B	#	H		B	8		8	#	8	15	
		1994-200-903	EB6-569-9982	EDG-50V-#0#3										RT-9591-9	\$ 14.05 TM	

## NAPS LICENSE REMINE PROJECT - NAPS ELECTRON PROJECT - NAPS RESILES - NAPS ELECTRON PROJECT - NAPS RESILES - NAP

**E** 

	1000			8	165	es a	£6	£6	483	165	SS AMES	WES	52	E .	5	£5	
	PRECISE SECONDARY SECONDAR				\$	165	82	£	165	£	52	£	£5	9	465	YES	
-																	
-		9			\$	75	534	5	5	\$	2	25 E	5	£ #5	£	3 465	
-	MYSMIN RYSMIN ROMOISES	2003			£ .	#5	2	# 5	25	3 45	S #ES	S WES	5 465	S WES	2 465	S	
-	MYSTIM MYSTIM E PECSONIN			1	#B	WES	#65	# FB	\$	£	\$	. FS	182	# #5	1 465	, MES	
-		386			5	755	\$	5	25	5	5	₹5 25	5	, M	N.	*	
STATE OF STREET	SENETRAL DESCRIPTION OF STREET OF ST				\$	534	9	82	\$	Ð	19	465	8	£	145	#ES	
Section and a	** ** ** ** **	F. 1881 FREE .	# 45# # 45# # 58#2 # 43#7	92-591 97-5917 97-4787		×				¥	2			¥	¥	*	
the ballanders work	CONTRACT TO RETURN SERVICE OF THE PROPERTY OF	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		5													
named and an address	100 SECTION 1		Ð	Ð	MES	£	eg.	9	52	Si .	MES	£	£	52	Š	Ş	•
		3000	3	8	Œ	ž	E	ť	E	ž	¥	ž	ž	ř	£	Ĕ	ŧ
		@#1109T19#	8384 A999	990 1080	CONTROL PR.	COMPRE, PR.	CONTROL PR.	CONTROL PR	CONTROL PR.	CIRTAIL PR	CONTROL FIR.	((8196)) 78.	(04.20) PR	CONTROL PR.	CONTRINE 78	(08/80), PR	(3815)) PR
		ĬĮ.	# 14 G.	SETM CLRE	FREE	PAREL	1386	FREEL	FREE	Parel	70Æ1	Past.	1 300	Fuel	P.28E	1,594	Fath
		Catadolev	SMITOMSEM	SHITORER	SWITCHGE	SHICKES	SHITCHEE	SWITCHEOR	SWITCHER	SWITCHEE	SWITCHER	SMITCHEEDS	SMITTHERE	SWITCHER	SWITCHEEDS	SWITTER	SWITCHGE
		DESCRIPTION	- 809 ENEX 885 2	*88V EREP 8US 3	RUCLEAR INSTRUMENTATION	MCB FRE IR US-1 LÓNDS	EEPS HCB FR 28 48-7 10805	ACB PR. 38 VB-1 LBMDS	RCB PRE 48 15-11 600 15-2 (1985)	NCB PR. 68 VS-1 10005	MG PR. 71 16.1. 20 16.2	EEPS HEB PM, NO VS-1 EUMDS	RCE POST ACTIBIEST	POST ACTION MONITORING CAS 8	EEPS FEEDWATER COMIDOR CARDINET SWITCHEAD	SI PAREL	Matter Theathfiel Control
		SYSTER	SE SE	E	83	83	8	EFS	£.	EFF	8	5415	88	#	5433	E	SE SE
		105 80	EB05-1	EBIS-3	8 855	#18 18	K8.24	W 53	2	69.63	M.S. 78	80.00	# (#) # du	Post (195-8	70 FCE	15-1	PR AD EST

10 SYSTEM   SEPTICE   COMPANY   CO						: COMPONENT :	COMPONENT CONTROL		160		CHEMINE	2 2	POTENTIAL :	510000 ::
INVINE WILD DISTRIBUTION CARRENT FORES DISTR PRICE TO THE PRICE OF THE							REPUACEN INSPECTION PRINCIPAL		SMITCH TO STATE OF THE PROPERTY OF THE PROPERT	8	RECHARISMS	8 2	(37 4312)	
1707249 WIC DIST PRE SHITCHEER PAREL PORER DISTR PRE 1707249 WIC DIST PRE 1707249 WIC DIST PRE 1707249 WIC DIST PRE 1707249 WIC DIST PRE 1707249 WIC DISTRIBUTION CARRIERTON SHITCHEER PAREL PRINCE DISTR PRE 1707249 WIC DISTRIBUTION CARRIERTON SHITCHEER PAREL PRINCE DISTR PRE 1707249 WIC DISTRIBUTION SHITCHEER PAREL PRINCE PAREL PAR		C#1950#Y	Time	app. 10a110*	CORP	A ANGLE	2			: 916 :		: NE : NEW : COM : NO	46	-
138/248 WAR DIST PART. SMITCHERAR POWEL POWER DISTR PART.  138/248 WAR DIST PART. SMITCHERAR PAWEL POWER DISTR PART.  138/248 WAR DISTRIBUTION CARRIER A SMITCHERAR PAWEL POWER DISTR PART.  138/248 WAR DISTRIBUTION CARRIER A SMITCHERAR PAWEL POWER DISTR PART.  138/248 WAR DISTRIBUTION CARRIER PAWEL POWER PROPER PART.  138/248 WAR DISTRIBUTION CARRIER PAWEL POWER POWER POWER PAWER PAWER POWER PAWER PA	120/249 WAC DIST PR		Plate	SISSO SINIA	Ē									
128/240 WE DIST PRE SMITCHEED PAREL PHREE DISTR PRE 200 PRE 200 PRES DISTR PRE 200 PRE 200 PRES DISTRIBUTION CARRIER SMITCHEED PAREL PHREE DISTR PRE 200 PRES 200 PRE	128/248 VAC BIST PW		PAKI	FORE DISTR	ž	•								
DISTRIBUTION CARDINET A SMITCHARGAN PAREL POMER DISTR PRI 175 NO NOME DISTRIBUTION CARDINET SMITCHARGAN PAREL POMER DISTR PRI 175 NO NOME DISTRIBUTION CARDINET SMITCHARGAN PAREL POMER POSTR PRI 175 NO NOME DISTRIBUTION SMITCHARGAN PAREL POMER DISTR PRI 175 NO NOME DISTRIBUTION SMITCHARGAN PAREL POMER DISTR PRI 175 NO NOME PAREL NI	128/248 1MC 0157 PM		PRREI	PINER DISTR	Ĕ	•								
DISTRIBUTION CARIGET A SMITCHGENE PAREL POWER DISTR PAR WES BY THE DISTRIBUTION CARIGET SMITCHGENE PAREL POWER DISTR PAR WES BY THE DISTRIBUTION CARINET SMITCHGENE PAREL POWER DISTR PAR WES BY THE DISTRIBUTION SMITCHGENE PAREL POWER DISTR PAR WES BY THE DISTRIBUTION SMITCHGENE PAREL POWER DISTR PARE WES BY THE DISTRIBUTION SMITCHGENE PAREL POWER DISTR PARE WES BY THE DISTRIBUTION SMITCHGENE PAREL POWER DISTR PARE WES BY THE DISTRIBUTION SMITCHGENE PAREL PROPERTY WES BY THE PAREL BY THE DISTRIBUTION SMITCHGENE PAREL PROPERTY WES BY THE PAREL BY THE DISTRIBUTION SMITCHGENE DAY POWER DISTRIBUTION WES BY THE PAREL BY THE DISTRIBUTION WES BY THE PAREL BY THE PAREL BY THE DISTRIBUTION WES BY THE PAREL BY	128/248 WE DIST PR		PME	PIER DISTR	ŧ	8								
DISTRIBUTION CACINET  SSS DISTRIBUTION FAMEL SMITCHEAR FAMEL FOMED DISTR FM. VES NO NOTE  UNION BUS DISTRIBUTION SMITCHEAR FAMEL FOMED DISTR FM. VES NO NOTE  UNION BUS DISTRIBUTION SMITCHEAR FAMEL FOMED DISTR FM. VES NO NOTE  FAMEL 01  UNION BUS DISTRIBUTION SMITCHEAR FAMEL FOMED DISTR FM. VES NO NOTE  FAMEL 02	DISTRIBUTION CARIO		1986	POMER DISTR	ŧ	Ð			W.S	\$	£	WES WES	¥	£5
SSS DISTRIBUTION PARKEL SMITCHEAR PARKEL PORKER DISTR PRI VES NO NEED UTINAL BUS DISTRIBUTION SMITCHEAR PARKEL PRINCES PARKEL NO. 1718 BUS DISTRIBUTION SMITCHEAR PARKEL PRINCES PARKEL NO. 1718 BUS DISTRIBUTION SMITCHEAR PARKEL NO. 1718 BUS	DIESEL GEN AUXILIAND DISTRIBUTION CHEINE		15 E	PINCE DISTR	ŧ	ž.			534	\$	£ .	WES WES	8	E S
UTTAL BUS DISTRIBUTION SHITCHERN PAREL PORED DISTR PRE VES NO NEED VITAL BUS DISTRIBUTION SHITCHERN PAREL PORED DISTR PRE VES NO NEED VITAL BUS DISTRIBUTION SHITCHERN DAY POWED DISTRIBUTION VES NO NEED VITAL BUS DISTRIBUTION WES NO NEED VITAL BUS DISTRIBUTION VES NO NEED VITAL BUS DISTRIBUTION VES NO NEED VES NO NEED VITAL BUS DISTRIBUTION VES NO NEED	SSS DISTRIBUTION PR		Hand	POMUP DISTR	ž	res			52	£ .	\$	WS WE	ş	£
VITAL BUS DISTRIBUTION SHITCHER PART, PARE DISTR PR. 165 NO NO.	VITAL BUS DISTRIBUT		PART	POSE DISTR	ž	\$			5	¥	ğ.	WES WES	ħ	\$
TRANSCENDENCE STATE THE PETER STATE TO SEE	VITAL BUS DISTRIBUTE		Ĭ	PORT DISTR	¥	8			465	\$	ě	NES WES	£	ş
1	EPS SSS DIST FOR CAUD 30	A 38 TRANSFIRMER	pay	FORE DISTR	**	MES.		*	945	ě	£ .	WES WES	£	<b>8</b>

### ATTACHMENT J

EMERGENCY ELECTRICAL POWER SYSTEM (EEPS)
APPLICABLE PROCEDURES LIST

10/24/85

TARRES ATTRICE BESCHELC CLARAGE TO SEE STATE STATE TRUES - PLAS - PLAS - PLAS - SEPECTATE STATES - SEPECTATE STATES - SEPECTATE STATES - SEPECTATES - SEPECTATES - SEPECTATES - SEPECTATES - SEPECTATES - SEPECTATES - SEPEC

Procedure to.	Er B		GREAT CASS	STREET, 19833	STOLES WHEN
45 £135	-	■光性の記載 込みでき の事者 ひまのむ 100円	** (** (** (** (** (** (** (** (** (**	ATACTOR SATEOMARRS, STREET	S1, 85, 85, 87, 02, 08, 05, 19, 450, 679, 87, 19, 19, 19, 18, 18, 18, 18, 18, 18, 18, 18, 18, 18
05-4290			SDM 100 大学 100 円	S	\$558"51##6"J#1#6"J\$"35"#5"J#"55"#6"15
o.P. <b>4</b> 203		* THE VALVE & WE PERSTRATION CHECK	1 1000 医黄色性	50 00 10 10 10 10 10 10 10 10 10 10 10 10	51, 85, 88, 85, 88, 89, 08, 07, 05, 08, 01, 05, 08, 88, 88, 88, 88, 88, 88, 88, 88, 88
1627-40		TEST OR OPERATION OF THE SAFETY INCECTION POWPS AND DESTINATION OF EDGS. SUP-195TEM DESIGNATION OF EDGS.	STREET, LANCE STILL I	United States	51,8875
04-4295	12	SYSTEM OPERATION CHECK	1 10 大樓里 11 14 14 15 15 15 15 15 15 15 15 15 15 15 15 15	S#011#####	SSE, 21.8. 12. 12. 12. 12. 12. 12. 12. 12. 12. 12
10-4		SURVEILLANCE OF THE STATICS POSES DC . AC DISTRIBUTION STATES AND THE ENTROPY OF DIFFERENCES.	· · · · · · · · · · · · · · · · · · ·	78-01 Least 10	20,7,7
*SA -40	1		SUMMER COMMENTS.	9 (4) (4) (4) (4) (4) (4) (4) (4) (4) (4)	544 544 544 544 544 544 544 544 544 544
(4.42)	16	SHEROEMET FERDEATER STATEM OPERABILITY TEST	SPECIAL SECTION		50.00 C. S.
1124-451	41	CHRESING STATES OPERABLITY TEST	SHREELLING TOUR.	( ) ( ) ( ) ( ) ( ) ( ) ( ) ( ) ( ) ( )	CH. EEPS, #535
(P-422)	0	#O. SERVICE WATER PIRP OPERABLEITY TEST	STREET LAND. I	5. · · · · · · · · · · · · · · · · · · ·	84.6878
2129-40	503 47-8	WAPOR CONTACTOR (BSSPECTION	STREET LIBERTS TOLL 1	い事のにも可能はな	24 H. H. 15
(4-42)]		65	SHEATSLANDS BOL. 1	()(1)(1)(1)(1)(1)(1)(1)(1)(1)(1)(1)(1)(1	S1,#S,C#,PR,G#PS,RSSS
1404-10			SURVEY LIAMET WAY	S#()41 ##()	24.50,44.50
10 mm / 10 mm	No.	UPSEARCHITY OF THE 120 WOLT A.C. WITH BUS	400	SMOTHER	
41-475		IMPERFANDENT CIRCUIT AND DWESGERGY MCC ACK INTERLOCK UNTRANSILITY	SPREETLANTS LVG. (		\$20 \$40 \$40 \$40 \$40 \$40 \$40 \$40 \$40 \$40 \$4
1014	-	NSS 0456401214 1857	10 10 10 10 10 10 10 10 10 10 10 10 10 1	3#014#830	Sales in the sales
11450	214	(内に乗り) 東上に (のため、 仁東・引・うじ、 東) 米東・北地に しゅう はないない たいしつけん 本体 ははなっこ	SPACE LAND	<b>公</b> ()	\$497,827,78
		の過去に対しては、連合のは他ののは様々には考していった。東・連ないでは、人にのなったの様々には、体性を引き、大・連続のではませ	一 可是 沙鹭园 小块状态	# 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	PR, 6595
	270	A CORPET # ACTUALISC OF CHARACTERS (CARRES), CARLO	STATE STATE OF T		\$4.00°, PC, PERS, SEEPS
***		A CONTRACTOR OF THE STATE OF TH	19 1000 公費日は佐建市	4/14/146	\$444 1.55
10-401	Ξ	・ ・ ・ ・ ・ ・ ・ ・ ・ ・ ・ ・ ・ ・ ・ ・ ・ ・ ・	100 5.98111.05000		Les de la constant de
1.134 10	*	・ 一般の は、	SMEATHURS AND I	· · · · · · · · · · · · · · · · · · ·	N. W. ST. CT. CT. ST. ST. CT. ST. ST. ST. ST. ST.

14/19/89

THREE ATHER SECTION DIRECTORS SECTION DIRECTORS AND PLANT THREE SECTION TO A SECTION OF THE CHARLES SECTION TO A SECTION OF THE CHARLES S

			GARAGE CLASS	Control of the Contro	の 日本の 日本の 日本の 日本の 日本の 日本の 日本の 日本の 日本の 日本
A SECOND		A TAGGEL TIME OF MICHIE OPERATED VALVES -MASTER LIST	SHRILLINE 2-1, 1	Back The state of	100
	80 8 30 30 30 30 40 40 40 41	SAFETY INSECTION ACCOMPLATION LEVEL SWITCH OFFRANTOWAL CHEFT AND CHEST of FUNCTIONS PREPARED BY LEVEL SWITCHES	STREETLINGS ROL. T		\$4## III
64 - 5101	5	MAINTENANCE OF MOTIVATED VALVE NO.	**	Secret. Plant	72, 24, 873, 674, 874, 82, 69, 974, 87, 87, 87, 87, 88, 98, 98, 98, 98, 98, 98, 98, 98, 98
H N N O O O O O O O O O O O O		INCREMENTAL AND THE MAINTENANCY OF THE PRESENT CHARGESTON STRING TO	**(#1884)**	SEACTOR SAFEGUARDS, STSTERS	M, 6875
		-0-1551 10 MAINTENANTS OF UPSI PURPS AND/OR MOTORS, PHR.1.2,1 AND/OR PURP SISTEMATE (NECH	***	ABRICIAE SEPERATOR, STSTEES	
67-575#	60 60 60 60 60 60 60 60 60 60 60 60 60 6	INSPECTION, TESTING AND MAINTENANCE OF GOOD, STARTER, REGARDS AND CONTACTOR		ESCRIPCAL STSTORS 400	RRT_ES, 74, 51, 555, 10, 6875
	ii ii ii ii iii iii	DISCOMMETTION OF ECCS WOW'S AND SHITTION COOLING MOT'S	1 × 0 × 1 × 1 × 1	SECTION STORY SEC	18
04-2749		6 RECOMMENTION OF ECCS WOTHE OFFEATED WANTER WD. OR CHATTERN COLLING PALES	1.000	CLECTRICAL STSTEMS AND	51,50,15,8855,8555
	64 61 61 61 61 61 61 61 61 61 61 61 61 61	PERSONNECTING/ACCONNECTING OF ACCS/S1-MON-22,21,21,24, AND 25 DEGARDS FROM SPCC-2		ELECTRICAL STSTEMS AND	<b>50.14</b> 7.7
	60 61 61 61 61 61 61 61 61 61 61 61 61 61	3 (MSSECTION AND MAINTENANCE OF WITH, 805 (MSERTER   AND 2	2.444.14	FLECTFICAL STATEMS #80	£
2185-4	10 10 10 10 10 10 10 10 10 10 10 10 10 1	S METRICONTRIL CONTRES AND RELATED EQUIPMENT E.S. QUALIFICATION. INSTITUTE AND RELATED EQUIPMENT E.S. QUALIFICATION. INSTITUTE AND		ELECTRICAL SISTEMS #10	<b>S</b>

# ATTACHMENT K

A GENERIC ASSESSMENT OF CONCRETE STRUCTURAL COMPONENTS

# A GENERIC ASSESSMENT OF CONCRETE STRUCTURAL COMPONENTS FOR THE LICENSE EXTENSION PROJECT

November 8, 1989

Major Contributors: N. A. Labrecque

Yankee Atomic Electric Company 580 Main Street Bolton, Massachusetts 01740-1398

#### DISCLAIMER OF RESPONSIBILITY

This report has not been reviewed to determine whether it contains patentable subject matter, nor has the accuracy of its information or conclusions been evaluated. Accordingly, the report is not to be considered a published report and is not available for general distribution; its distribution is limited to employees and advisors of EPRI, SANDIA, DOE, and Yankee Atomic Electric Company for the sole purpose of evaluating the progress and future course of the project described in the report. Until the report has been reviewed and evaluated by EPRI, SANDIA, DOE, and Yankee Atomic Electric Company it should be neither disclosed to others nor reproduced, wholly or partially, without written consent of the parties.

#### ABSTRACT

This study evaluates the plausible modes of degradation of concrete and anchorages to concrete and evaluates the potential significance of the degradation modes for the structures at Yankee Nuclear Power Station (YNPS).

The results of this study are that there are no locations that are susceptible to the following degradation modes for concrete and reinforcing steel:

- 1. Fatigue
- 2. Chemical reactions of aggregates
- 3. Drying and carbonation shrinkage
- 4. Thermal effects
- 5. Microbiological-Induced Corrosion (MIC)

The following modes of degradation may be significant for some, but not all, of the concrete structures:

- 1. Corrosion of embedded metals
- 2. Freeze-thaw damage
- 3. Exposure to aggressive chemicals
- 4. Leaching of calcium hydroxide
- 5. Abrasion
- 6. Degradation of anchorages to concrete due to the following:
  - o Corrosion
  - o Deterioration of adjacent concrete
  - o Vibratory loadings

An inspection program in accordance with the American Concrete Institute guides and practices (ACI 201.1R, 207.3R, and 224.1R) will provide assurance that the above six potentially significant degradation modes are monitored and controlled.

The only locations where radiation exposure may be significant are the Spent Fuel Pit (SFP) and the Reactor Support Structure (RSS) concrete adjacent to the Neutron Shield Tank (NST). The potential and significance of this degradation mode will be evaluated in future reports.

The potential for degradation of concrete at YNPS from exposure to groundwater or river water is insignificant. Chemistry tests of these waters performed during construction and again in 1988 and 1989 show only negligible concentrations of chlorides and sulfates.

# TABLE OF CONTENTS

				Page			
	DISCLA	IMER OF	RESPONSIBILITY	ii			
				iii			
	TABLE	OF CONT	ENTS	iv			
1.0	INTRO	OUCTION.		. 1			
2.0			F COMPONENTS				
3.0	EVALUA	ATION OF	PLAUSIBLE MODES	. 3			
	3.1	Fatious		. 3			
	3.2	Corrosi	on of Embedded Metals	. 4			
	3.3	Extreme	Environments	. 7			
		3.3.1	Exposure to Elevated Temperatures				
		3.3.2	Irradiation Exposure				
	3.4	Appres	sive Environments	. 9			
	3."	ngg. co.					
		3.4.1	Freeze-Thaw Damage				
		3.4.2	Exposure to Aggressive Chemicals				
		3.4.3	Leaching of Calcium Hydroxide				
		3.4.4	Abrasion	. 13			
	3.5	Chemic	al Reactions of Aggregates	14			
	3.6	Drvine	and Carbonation Shrinkage				
	3.7	Therma	1 Effects	11			
	3.8	Anchor	age to Concrete	1/			
	3.9	Microb	iological-Induced Corrosion	19			
4.0	SUSC	EPTIBLE	PLANT AREAS	20			
	4.1	Potent	tially Significant Degradation Modes				
	4.2	Irradi	iation Exposure				
	4.3	Expost	ure to Elevated Temperatures				
	4.4	Abras:	ion				
	4.5	Exposi	ure to Aggressive Chemicals				
	4.6	Freez	e-Thaw Damage				
	4.7	Leach	ing of Calcium Hydroxide				
	4.8	Corro	sion of Embedded Metals				
	4.9	Degra	dation of Anchorages to Concrete				
5.0	INSPECTION						
	5.1	Inene	ection Program	24			
	5.2	Signi	ficance to Structures	2			
	5.2	STRUT	. LUMING TO DITTO TO THE TOTAL THE TOTAL TO THE TOTAL TOT				
STELL ST				2			

#### 1.0 INTRODUCTION

This document provides a generic assessment of the plausible modes of degradation of concrete, including embedded metals, and anchorages to concrete for structures at the Yankee Nuclear Power Station (YNPS).

The plausible modes of degradation were identified from a review of the literature. Each of the plausible modes of degradation is evaluated on a generic basis to identify the stressors and environment required for the degradation to be active, how the degradation is manifested, and the design features and construction methods used at Yankee Nuclear Power Station (YNPS) to mitigate the potential for significant age-related degradation. The areas of the plant potentially susceptible to age-related degradation are then identified. Finally, the requirements of an effective inspection program are identified.

# 2.0 DESCRIPTION OF COMPONENTS

The generic concrete structural components necessary to the function of the structures at YNPS consist of the following. Concrete includes the reinforcing steel, as well as the cement, aggregate, and mixing water.

- o Foundations (Footings, Beams, and Mats)
- o Columns
- o Walls
- o Ground Floor Slabs and Equipment Pads
- o Elevated Floor Slabs
- o Roof Slabs
- o Precast Concrete Beams and Slabs
- o Manholes
- o Duct Banks
- o Fluid Retaining Walls and Slabs
- o Masonry Walls
- o Concrete Blocks (Shielding)
- o Grout
- o Cast-in-Place Anchors
- o Post-Installed Anchors (Expansion and Grouted Types)
- o Embedded Metals (Castings, Weldments, Pipes, and Conduit)

## 3.0 EVALUATION OF PLAUSIBLE MODES

The plausible age-related modes of degradation of concrete components for structures were identified from a review of the literature (see Section 6.0, References) and are as follows:

- o Fatigue
- o Corrosion of Embedded Metals
- o Irradiation Exposure
- o Exposure to Elevated Temperatures
- o Abrasion, Including Erosion
- o leaching of Calcium Hydroxide
- o Exposure to Aggressive Chemicals
- o Freeze-Thaw Damage
- o Chemical Reactions of Aggregates
- o Thermal Effects
- o Drying and Carbonation Shrinkage
- o Microbiological-Induced Corrosion
- o Vibratory Loading on Anchorages to Concrete

#### 3.1 Fatigue

## 3.1.1 Description

Fatigue is a process of progressive permanent internal structural change in a material subjected to repetitive cycles of stress. Fatigue strength of concrete has received considerable attention due to the adoption of ultimate strength design procedures and the use of higher strength material. The effects of fatigue and the considerations for design are discussed in Reference (n).

The fatigue strength of concrete is essentially the same whether the mode of loading is tension, compression, or flexure, and is roughly about 55% of static strength for 10<sup>7</sup> cycles. For design, a conservative modified Goodman diagram is used. Use of this design method is discussed, in detail, in Reference (n).

### 3.1.2 Significance to Structures

Fatigue of reinforcing steel is not a significant degradation mode at the stress levels (24 ksi maximum), stress range (stress fluctuation), and stress cycling to which it is subjected. The lowest stress range known to have caused failure was associated with 1.25 x 10 cycles of loading and a stress range of 21 ksi (from 17.5 ksi to 38.5 ksi), Reference (h).

Reinforced concrete at YNPS was designed in accordance with ACI 318-56 and American Standard Building Code A58.1-1955, Reference (o). The design codes limit the maximum permissible stress levels such that fatigue is insignificant for concrete and embedded metals.

#### 3.2 Corrosion of Embedded Metals

### 3.2.1 Description

Corrosion of embedded metal has been studied in considerable detail and depth. References (j) and (k) provide a summary of the studies.

The majority of the embedded metal is the reinforcing steel. Other embedded metals include carbon and stainless steel piping, structural embedments (plates, anchor bolts, and strap anchors), conduit for electrical cables, and grounding (copper) cables. Corrosion of reinforcing steel due to stray electrical currents has been identified as a degradation mechanism.

Corrosion of carbon steel, reinforcement and embedded items, not only affect the ability of the steel to carry load, but also causes deterioration of the concrete due to severe expansion stresses imposed as a result of volumetric changes.

Concrete's high alkalinity (pH >12.5) provides an environment which serves to protect the steel from corrosion. Corrosion occurs when aggressive ions, most notably chloride, cause a reduction in pH to below 10 and dissolved oxygen is available for the electrochemical reaction. Ions of sulfate and carbonate can also be aggressive. However, these have low solubility in the high calcium environment and, thus, have a low availability to reduce the pH.

Therefore, this degradation mechanism requires the presence of aggressive ions, the presence of oxygen, and the presence of cracks or permeable concrete with intermittent wetting and drying.

#### 3.2.2 Manifestation

The corrosion products produced have a volume approximately eight times that of the original metal. The development of these corrosion products subject the concrete to tensile stress, eventually leading to hairline cracking, followed in time by rust staining, spalling, and more severe cracking. These actions will expose more reinforcing steel and concrete to further deterioration. A loss of bond between the concrete and reinforcing steel will occur along with a reduction in bar cross-section. The degradation associated with reinforcing steel corrosion is most prominently displayed in concrete bridge decks and parking facilities, given the abundant use of deicing salts.

## 3.2.3 Significance to Structures

Corrosion of reinforcing steel due to stray electrical currents has been identified as a potential degradation mechanism, References (c), (j), and (u). However, this mechanism is not significant at YNPS since the reinforcing steel is not used for grounding of plant equipment or for lightning protection. Steel structures and plant equipment are grounded by means of direct connections to the station grounding grid. The potential for corrosion of embedded metal due to induced currents in electrical duct banks is also not significant. This mechanism requires both a direct current and a sodium or calcium chloride electrolyte, Reference (j). As discussed below, it is very unlikely that the necessary electrolyte, significant concentrations of chlorides in solution, exist in the concrete for duct banks.

It is very unlikely that a significant concentration of chlorides is present in the concrete due to mixing water. Chloride concentrations of less than 500 ppm are considered not significant, Reference (z). An analysis of the Sherman Pond water, used as the mixing water, performed in the 1950's,

Reference (h), showed only 2 ppm to 8 ppm chlorides as NaCl. This concentration is insignificant. In addition, the only admixture permitted in the Specification, Reference (f), was Darex AEA.

Corrosion of embedded metals from exposure to groundwater or river water is also insignificant. This is based on the results of water chemistry analyses performed in December 1988 and August 1989, References (s) and (aa). The maximum chloride concentration was only 11 ppm.

Corrosion of carbon steel, reinforcement, and embedded items can occur from spills or leakage of acidic fluids. Corrosion of embedded metals requires permeable concrete or the presence of cracks and the presence of both oxygen and aggressive ions. Aggressive ions may be introduced from spills or leakage of acidic process fluids. Aggressive ions may also be introduced from leakage of acid rainwaters through damaged roofing systems. This mechanism is significant to structural integrity only if left unchecked. Good housekeeping practices to assure that spills and leakages are cleaned up in a timely manner, that joints are tight and properly caulked and sealed, and that cracks in fluid containment areas are sealed will mitigate the potential for this mechanism. Maintenance of the roofing systems, roof drains, and yard drainage will mitigate the potential for damage due to acid rain.

The corrosion potential of embedded copper materials is considered extremely low and of no significance unless they are exposed to ammonia, Reference (j). Only in the water treatment area are sufficient amounts of ammonia handled such that, in the event of a spill, this mechanism could occur.

The corrosion potential of embedded stainless steel materials is considered very low and of no significance unless they are exposed to chlorides, Reference (j). With good housekeeping practices, there are no areas of the plant subject to this degradation mode. The chloride concentrations in plant system fluids are kept very low to minimize corrosion of piping and equipment. Therefore, if spills are cleaned up in a timely manner, this mechanism is not significant.

# 3.3 Extreme Environments

## 3.3.1 Exposure to Elevated Temperatures

#### 3.3.1.1 Description

Exposure of concrete to elevated temperatures can result in reduced compressive strength, modulus of elasticity, and shielding ability. The effects of elevated temperature exposure have been reported in the literature, References (a), (b), (c), and (d).

The results of studies and experiments show the following:

- o At temperature exposures below 150°F, degradation of concrete, mechanical, and shielding properties is not significant.
- o At temperature exposures between 180°F and 212°F, degradation of mechanical properties should not exceed 15%, and degradation of shielding properties will be insignificant unless the time of exposure is many years.

At very high temperatures, surface scaling and cracking may be exhibited. Otherwise, there are no observable characteristics due to exposure to elevated temperatures.

#### 3.3.1.2 Significance to Structures

Generally, the concrete at YNPS is not exposed to temperatures above 150°F. By design, all hot pipes are installed in sleeve penetrations to limit temperature exposure. Therefore, hot pipe penetrations are not significant.

The concrete at the Turbine-Generator (T-G) pedestal-to-turbine interface is not normally subjected to temperatures above 150°F. The machine is insulated and is supported such that an air gap exists to provide the necessary cooling. The T-G pedestal is a massive structure, subject to only very low stress levels. The compressive stress was limited to 400 psi, Reference (o). Therefore, this mechanism is not significant for the pedestal.

The only location that may be of concern is the concrete immediately adjacent to the neutron shield tank due to the potential for gamma heating, which will be evaluated in a separate report.

### 3.3.2 Irradiation Exposure

### 3.3.2.1 Description

Concrete can undergo changes in properties if exposure to neutron and/or gamma radiation exceeds certain levels. The effects of neutron irradiation are documented in the literature, References (a), (b), (c), (d), and (g). The effect of gamma irradiation was reported by Hilsdorf, Kroop, and Koch (Reference (g)).

Existing experimental data related to the effects of radiation on the mechanical properties of concrete allow some general statements. Compressive strength and modulus of elasticity of concrete do not begin to experience reductions until exposure exceeds a neutron fluence of 1019 n/cm2. This reduction is believed to be primarily due to radiation exposure, with some small part due to the temperature rise associated with exposure. Reductions in tensile strength occur at the same exposure level, but are more pronounced than the reductions in compressive strength as exposure increases. Reductions in tensile strength are relevant concerns because of implied reductions in cross-section shear capacity, not because there is a need for tensile capacity directly to resist tensile section forces. Typically, reinforcing steel is provided to resist all tensile cross-section force, with no reliance on concrete tensile strength. Reductions in tensile strength may also affect the pullout strength of anchors. Reduction in compressive and tensile strength of concrete exposed to gamma radiation up to 1010 rads is practically nil, Reference (g).

# 3.3.2.2 Significance to Structures

Radiation damage to concrete is not readily observable. YNPS was designed to minimize exposure of concrete to neutron and gamma irradiation. The reactor pressure vessel is surrounded (radially and at the bottom) by the

neutron shield tank. The only concrete components for which this mechanism may be significant are those exposed to gamma radiation above  $10^{10}$  rads or neutron radiation above  $10^{19}$  n/cm<sup>2</sup>.

### 3.4 Aggressive Environments

#### 3.4.1 Freeze-Thaw Damage

## 3.4.1.1 Description

The repeated action of freeze-thaw cycles can cause damage to hardened concrete. This damage is characterized by scaling, cracking, and spalling. Freeze-thaw damage has been extensively studied and is discussed in References (b), (c), and (j).

Freeze-thaw can affect both the cement paste and the aggregates causing expansion forces. The cement paste can fail when the concrete is critically saturated (when greater than 91% of the water accessible voids are filled with water, Reference (j)) and exposed to ambient temperatures below 28°F. If absorptive aggregates are used, and the concrete is in a continuously wet environment, the concrete may fail if the coarse aggregate becomes saturated.

This mechanism is not significant unless both of the following environmental conditions exist:

- o Exposure to temperatures of 28°F or less.
- Exposure to sufficient water so that the concrete can become nearly saturated.

# 3.4.1.2 Significance to Structures

This mechanism is significant to the structural integrity only if left unchecked. Freeze-thaw damage is significant to structures in that it is progressive and can result in corrosion of reinforcement or undermining of supports for structures or equipment. Concrete that contains air entrainment

is less susceptible to this mechanism, Reference (j). Good housekeeping practices to assure timely removal of ice, snow, and rainwater will mitigate the potential for this mechanism.

Foundations are generally not susceptible to freeze-thaw damage. If water is allowed to pond and freeze at grade beams, damage could occur. However, the potential for this is mitigated by site grading which provides for a positive slope to drain the water away from foundating grade beam.

# 3.4.2 Exposure to Aggressive Chemicals

## 3.4.2.1 Description

Concrete being highly alkaline (pH >12.5) is degraded by acids. Sulfates of potassium, sodium, and magnesium may attack concrete depending on the concentration present in soils and/or groundwater. Spills or leakage from the plant process systems also may be sufficiently acidic as to cause concrete degradation.

Sulfate attack can produce significant expansive stresses within the concrete leading to cracking, spalling, and strength loss. Once established, these conditions allow further exposure to aggressive solutions. Acid rain can be a source for sulfate attack. Areas adjacent to industrial plants which contribute to the sulfur-based acid rain phenomenon are more susceptible to this form of chemical attack.

Acid attack can increase porosity and permeability of concrete, reduce its alkaline nature at the surface of the attack, reduce strength, and render the concrete subject to further deterioration. Acid attack is characterized initially by efflorescence, deposits of salts formed on a surface, and later by scaling.

# 3.4.2.2 Significance to Structures

It is very unlikely that sulfates are present in the concrete due to mixing water. Analyses of Sherman Pond water, used as the mixing water, performed in the 1950's, Reference (h), showed only a trace (i.e., less than 10 ppm) of sulfates (ppm as So<sub>4</sub>). This concentration is considered negligible as it relates to attack on concrete, Reference (e).

Degradation of concrete from exposure to groundwater or river water is insignificant. This is based on the results of water chemistry analyses performed in December 1988 and August 1989, References (s) and (aa). The maximum sulfate concentration was only 18 ppm. Sulfate concentrations below 150 ppm are considered negligible, Reference (e).

Exposure to aggressive chemicals may be a potential degradation mechanism for concrete components which are subject to acidic or alkaline spills or leakage from plant process systems. Exposure to aggressive chemicals is significant to structural integrity only if left unchecked. Good housekeeping practices to assure that spills and leakages are cleaned up in a timely manner, that joints are tight and properly caulked and sealed, and that cracks in fluid containment areas are sealed will mitigate the potential for this mechanism.

Acid rainwaters can cause degradation of concrete. If these waters are allowed to accumulate, the aggressive ions, sulfates, can concentrate in cracks or improperly prepared joints. Acid rain is not significant to walls since the flushing action of the rain will prevent concentration of the aggressive ions. Only a thin surface layer would be affected and this is not significant to the function of the concrete components. The potential for this mechanism is mitigated by good housekeeping practices to assure that roofing is kept in good condition and that cracks, if any, in containment areas are sealed.

Boric acid generally has only negligible effects on concrete,

Reference (r). However, it can make the concrete more susceptible to

erosion. The only area of the plant potentially susceptible to erosion from

boric acid leakage, which cannot be readily observed, is the reactor support structure concrete adjacent to the neutron shield tank. This will be evaluated in a separate report.

## 3.4.3 Leaching of Calcium Hydroxide

### 3.4.3.1 Description

In concrete structures containing cracks, improperly treated construction joints or areas of porous concrete, water may enter and pass through. As water passes through the concrete, it dissolves (leaches) some of the calcium hydroxide (lime).

When most of the calcium hydroxide has been leached away, other cementitious constituents become exposed to chemical decomposition, eventually leaving behind silica and alumina gels with little or no strength. The water's aggressiveness or ability to leach calcium hydroxide depends on its dissolved salt content and its temperature. Water, either from rain or melting snow, can leach lime from concrete. This leaching action of the water must be that of water passing through the concrete, since water that merely passes over it will not cause significant leaching, Reference (d).

Leaching of calcium hydroxide is evidenced on concrete that is alternatively wetted and dried. The white salt deposits that are left on the surface of the concrete are a solution of water, free lime from the concrete, and carbon dioxide that has been absorbed from the air. The leachate from the concrete is nearly colorless until the carbon dioxide is absorbed and the material dries as a white deposit.

Leaching of calcium hydroxide does, however, have a beneficial effect in healing of hairline cracks formed during construction. This process is known as "autogenous healing" and is discussed in detail in Reference (u). In the presence of moisture and absence of tensile stress, it closes dormant cracks.

Healing occurs through the carbonation of calcium hydroxide in the cement paste by carbon dioxide, which is present in the surrounding air and water. Calcium carbonate and calcium hydroxide crystals precipitate, accumulate, and grow within the cracks. The crystals interlace and twine, producing a mechanical bonding effect, which is supplemented by a chemical bonding between adjacent crystals and between the crystals and the surfaces of the paste and the aggregate. As a result, some of the tensile strength of the concrete is restored across the cracked section, and the crack may become sealed.

# 3.4.3.2 Significance to Structures

Leaching of calcium hydroxide is significant only if left unchecked. This mechanism requires both the presence of cracks or porous concrete and an aggressive fluid flowing through the concrete. As discussed in Sections 3.2.3 and 3.4.2.2, the ground and river waters at YNPS are not aggressive.

Therefore, this mechanism is not significant for below grade concrete. For above grade concrete, good housekeeping practices to monitor cracks to assure that they are dormant and sealed or if active are properly caulked and sealed against water intrusion will mitigate the potential for this mechanism.

#### 3.4.4 Abrasion

#### 3.4.4.1 Description

Abrasion is the surface wear of concrete by rubbing and friction.

Abrasion of floors and pavements results from traffic or the movement of equipment directly on the concrete surfaces. Abrasion (erosion) can also occur from the impact from a flowing stream of water.

Abrasion in hydraulic structures is caused by cavitation or the transport of solids along the surface (Reference (m)). Cavitation abrasion is characterized by pitting and is not common at velocities of less than 40 fps. However, for closed conduits, cavitation damage can occur at velocities as low as 25 fps at abrupt changes in slope or curvature.

Abrasion resulting from traffic or the transport of solids (silt, sand, and gravel) is characterized by a worn surface appearance. Erosion from the impact of a flowing stream of water is characterized initially by peeling (the breaking away of the thin flakes of mortar) and in the latter stages by scaling (loss of mortar and exposure of coarse aggregate).

# 3.4.4.2 Significance to Structures

The effects of abrasion are significant only if left unchecked. The effects of this mechanism are readily observable and repairs can be made.

Good work practices mitigate the potential for abrasion to floors and pavements. These include assuring that equipment is not dragged across floors, and that heavy equipment is moved on rollers or pneumatic tires.

The potential for erosion due to the impact of water streams is mitigated by piping equipment drains to floor drainage systems and flashing of scuppers to direct the fluids away from the concrete.

The potential for abrasion in hydraulic structures will be evaluated in a separate report. The significance of this mechanism will be determined considering geometric arrangement, flow velocities, and inspection procedures.

# 3.5 Chemical Reactions of Aggregates

# 3.5.1 Description

A number of deleterious chemical reactions can produce concrete cracking. These are generally related to the concrete aggregates, and include the following:

- o Alkali-silica reaction. Also known as alkali-aggregate reaction.
- o Cement-aggregate reaction.
- o Expansive alkali-carbonate reaction.

The deterioration mechanisms and the locations (sources) of the problem aggregates are discussed in References (b), (c), (d), and (j).

#### 3.5.1.1 Alkali-Silica Reaction

The alkali-silica reaction can cause expansion and cracking of concrete structures. Active silica in the presence of potassium or sodium hydroxide forms an alkali-silica complex which can expand by the imbibition of water. When the alkali concentration is low, calcium hydroxide, derived from the cement, forms a nonexpansive calcium-alkali-silica complex. When the concentration is high, an expansive alkali-silica complex is formed.

In the United States, the problem aggregates generally occur in the Western half (Reference (j)) and the reaction occurs in the early life of the structure.

Alkali-silica reaction is characterized by map cracking. Petrographic examination would usually show a zone depleted in or free of calcium hydroxide surrounding the aggregate, Reference (v).

### 3.5.1.2 Cement-Aggregate Reaction

The cement-aggregate reaction requires a reactive aggregate containing siliceous minerals, a concentration of alkalies in the cement that produce a high pH and abundant hydroxyl, and the presence of an environment that causes severe drying conditions. The aggregates susceptible to this mechanism generally come from the Nebraska, Kansas, and Wyoming areas, Reference (j). This mechanism also requires severe drying condition, such as to cause a net migration of alkali to the surface of the concrete. This environmental condition does not exist at YNPS. This mechanism is, therefore, not significant to YNPS.

# 3.5.1.3 Expansive Alkali-Carbonate Reaction

The expansive alkali-carbonate reaction occurs between some dolomitic limestone aggregate containing clay minerals and the alkalies in the cement. Where the concrete has a constantly renewable supply of moisture, dedolomization can occur, leading to exposure of the clay minerals and their swelling.

Concrete affected by this mechanism is characterized by map cracking and the general absence of silica gel exudations at cracks. Additional signs of the severity of the reaction are closed expansion joints and crushing of the adjacent concrete. Petrographic examination would show rim growth on the aggregate and a highly carbonated paste adjoining the aggregate, Reference (v).

## 3.5.2 Significance to Structures

The alkali-silica reaction and the expansive alkali-carbonate reaction require susceptible aggregates and the presence of water.

An inspection of the Screenwell was performed in 1975, Reference (w). The concrete was found to be in excellent condition both above and below water. No evidence of spalling was found even after 15 years of operation. An inspection of the concrete most for Tanks TK-31 and TK-32 was performed in 1989. This most collects rainwater and normally contains 4 to 12 inches of water. The grade slab was in very good condition with no evidence of cracking or distress at the joints abutting the piers or walls, Reference (x).

After 30 years of service without any indication of degradation due to this mechanism, it is concluded that the structures at YNPS are not subject to significant age-related degradation due to chemical reactions of aggregates.

#### 3.6 Drying and Carbonation Shrinkage

The effects of drying and carbonation shrinkage occur early in the life of the concrete due to loss of moisture. With proper mix design and curing procedures, this mechanism is not significant.

The two factors in mix design which affect shrinkage are the Water-Cement (W/C) ratio and cement content. A low W/C and a lean mix are desirable. A review of Reference (f) shows that mixes having low W/C and being slightly rich were specified for YNPS.

A review of Reference (i) shows that the concrete was to be protected so as to prevent loss of moisture for at least seven days. Thus, the factors affecting shrinkage were considered in the design. The specified mixes have a low W/C ratio, and a long curing time was specified to account for the slightly rich mixture. Therefore, this mechanism is not significant.

#### 3.7 Thermal Effects

The thermal effects as related to cement hydration occur very early in the life of the concrete. Buildup of heat occurs in the first few days while the concrete is relatively plastic. The degradation occurs after the concrete has obtained a certain amount of rigidity and the cooling process tends to set up tensile stressed at the cooler outer surfaces. Thermal effect resulting from cement hydration are primarily of concern with massive concrete structures.

With proper placing and curing procedures, the thermal effects of cement hydration are not significant. At YNPS, this potential was considered in the design. A review of Reference (i) shows that protection from rapid cooldown of the outer surfaces was provided by specifying that concrete surfaces be prevented from going below 50°F, and that concrete be placed only when the concrete temperature was between 50°F and 90°F. Thus, the thermal effect of cement hydration was considered in the construction of the plant and does not need to be re-evaluated for life extension.

#### 3.8 Anchorage to Concrete

## 3.8.1 Description

Steel embedments are used to transmit loads from steel structures and equipment to the reinforced concrete.

The types of embedments or anchors are as follows:

1. Pre-installed anchors such as bolys, studs, and straps.

 Post-installed enchors such as expansion shell, wedge, undercut, and grouted type anchors.

Anchorage to concrete has been studied by ACI Committee 355 and others. Reference (p) discusses this subject in considerable detail. The three factors which affect the performance of the anchorage embedments are improper installation, the presence of vibratory loading, and the anchor type.

Pre-installed anchors have excellent survivability to vibratory loading, Reference (p). The only degradation mechanisms which affect pre-installed anchors are corrosion and deterioration of the concrete within which it is embedded.

Post-installed anchors, except for the undercut type, are subject to age-related degradation from vibratory loading. Expansion shell and grouted-type anchors are particularly susceptible to this mechanism.

Wedge-type anchors generally perform well under vibratory loadings. The initial effect of vibratory loading on post-installed anchors is a loss of prestress. Corrosion and deterioration of the concrete within which the post-installed anchors are embedded are the two other degradation mechanisms.

# 3.8.2 Significance to Structures

#### 3.8.2.1 Corrosion

Corrosion of anchorages to concrete is significant only if left unchecked. The high alkalinity (pH >12.5) of the concrete provides an environment which serves to protect the embedded portions of the anchors. Corrosion of projecting portions of anchors is readily observable and any corrosion can be mitigated by cleaning and painting.

### 3.8.2.2 Deterioration of Adjacent Concrete

Deterioration of concrete adjacent to anchorages is characterized by cracking and spalling. The effects of this mechanism can be evaluated by a visual inspection. Soundings taken from light blows of a hammer can be used to further evaluate the effects of this mechanism.

# 3.8.2.3 Vibratory Loading

The effect of vibratory loading is significant only for expansion shell and grouted-type anchors. The initial effect of this mechanism is loss of prestress and then loosening of the anchor. Loss of prestress can be determined from a bolt torque test. The installation of expansion anchors on pipe supports was the topic of IE Bulletin No. 79-02. In compliance with this bulletin, YNPS in 1979 performed inspections (J.O. No. 79-107) of supports for safety class piping. As a result of these inspections, many expansion shell (Red Head) anchors were replaced with wedge-type (Hilti) anchors.

Grouted-type anchors were found to be acceptable when subjected to bolt torque test.

# 3.9 Microbiological-Induced Corrosion

# 3.9.1 Description

Microbiological-Induced Corrosion (MIC) is caused by corrosive secretions of micro-organisms. The MIC mechanism begins with the fermentation of raw sewage which generates methane and H<sub>2</sub>S gases. These react with water to produce acids which then condense above the water line. This process lowers the pH of the concrete to levels favorable to growth of bacteria. These bacteria, in turn, secrete sulfuric and carbonic acids, which further attack the concrete. This results in deep pitting and spalling of the concrete.

# 3.9.2 Significance to Structures

This mechanism requires water contaminated with sewage and elevated temperatures necessary to promote fermentation. Since this environment is not present for any structure at YNPS, this mechanism is not significant.

#### 4.0 SUSCEPTIBLE PLANT AREAS

# 4.1 Potentially Significants Degradation Modes

The potentially significant age-related degradation modes are as follows:

- o Corrosion of embedded metals
- o Exposure to elevated temperatures
- o Irradiation exposure
- o Freeze-thaw damage
- o Exposure to aggressive chemicals
- o Leaching of calcium hydroxide
- o Abrasion
- o Degradation of anchorages to concrete

#### 4.2 Irradiation Exposure

Degradation due to irradiation requires gamma exposure above  $10^{10}$  rads or neutron exposure above  $10^{19} \, \text{n/cm}^2$ , see Section 2.3.2. The only concrete which may be exposed to gamma irradiation above  $10^{10}$  rads is the interior surface of the SFP and the RSS concrete immediately adjacent to the NST. The only concrete which may be exposed to neutron irradiation above  $10^{19} \, \text{n/cm}^2$  is the RSS concrete immediately adjacent to the NST.

The potential significance of irradiation to the RSS and SFP concrete will be evaluated in separate reports.

# 4.3 Exposure to Elevated Temperatures

Degradation due to elevated temperature requires long-term exposure to temperatures above 150°F. As discussed in Section 2.3.1, the only location that may be of concern is the concrete immediately adjacent to the NST due to the potential for gamma heating. The potential and significance of gamma heating of RSS concrete will be evaluated in a separate report.

#### 4.4 Abrasion

Abrasion is the result of mechanical wear from traffic or the impact of a flowing stream of water or erosion due to cavitation of hydraulic structures. The only structures which may be subject to significant degradation due to erosion are the Screenwell and the seal pit.

Floor slabs in most of the structures may be subject to degradation due to traffic or the impact of a flowing stream of water. However, the effects of abrasion due to mechanical wear are readily observable long before they become significant. Good material handling and housekeeping practices are all that is required to mitigate the potential for this mechanism.

# 4.5 Exposure to Aggressive Chemicals

Exposure to aggressive chemicals is significant to structural integrity only if left unchecked. The areas of the plant susceptible to this mechanism are certain concrete floors and sumps since these may come into contact with acidic or alkaline process fluids from spills or leakage.

Concrete roof slabs may be susceptible to degradation due to acid rain if the roofing system is allowed to degrade, thereby subjecting the roof slabs to these acidic waters. Concrete basins which collect and store rainwater may also be susceptible to degradation if cracks are not properly sealed.

The ion exchange pit may also be susceptible to this mechanism, since it contains water for shielding. The shield tank cavity portion of the RSS and the SFP are lined with stainless steel and, thus, are not susceptible to this mechanism. The potential for degradation of the stainless steel liners is evaluated in a separate report.

The RSS concrete immediately adjacent to the NST may be susceptible to this mechanism due to leakage of shield tank cavity water.

#### 4.6 Freeze-Thaw Damage

Degradation due to freezing and thawing requires exposure temperatures below 28°F and saturated concrete or the presence of cracks exposed to water. The plant areas susceptible to this mechanism are as follows:

- o Piers located outside buildings
- o Horizontal projections from walls where water and ice can accumulate
- o Roof slabs, if roofing has deteriorated, or they are not protected
- o Wall areas near scuppers or where water overflows
- o Duct banks at grade level

#### 4.7 Leaching of Calcium Hydroxide

Degradation due to leaching of calcium hydroxide requires cracks and water passing through the concrete. The water may come from process fluids or rain, snow, and ice. The following areas of the plant are susceptible to this mechanism if the concrete is cracked:

- o All areas susceptible to freeze-thaw damage
- o The ion exchange pit
- o The Screenwell and the seal pit
- o The containment moat for TK-31 and TK-32
- o Sumps and manholes

#### 4.8 Corrosion of Embedded Metals

Degradation due to corrosion of embedded metals requires permeable concrete or the presence of cracks and the presence of both oxygen and aggressive ions. The following areas of the plant are susceptible to this mechanism:

- o All areas susceptible to freeze-thaw damage
- o Floors and sumps that come into conduct with aggressive chemicals
- o The ion exchange pit
- o The Screenwell and the seal pit

- o The containment moat for TK-31 and TK-32
- o Manholes

## 4.9 Degradation of Anchorages to Concrete

#### 4.9.1 Corrosion

All anchorages to concrete are subject to corrosion. However, since concrete has a high pH, corrosion will first occur at the interface of the anchor to the grout or steel attachments. The effects of this mechanism can be evaluated by a visual inspection of the anchor and the surrounding concrete.

### 4.9.2 Deterioration of Adjacent Concrete

Degradation of anchors to concrete due to this mechanism results from overstressing or damage to concrete from corrosion of embedded metals, freeze-thaw damage, exposure to aggressive chemicals, or leaching of calcium hydroxide. Expansion shell and wedge-type anchors are susceptible to this mechanism. Cost-in-place, undercut, and grouted-type anchors are susceptible to this mechanism only when overloaded or when concrete degradation is in an advanced stage.

#### 4.9.3 Vibration Loading

Wedge-type anchors (Red Head and Star Slug-in) are susceptible to this mechanism only when they are used for support of piping, equipment, or platforms that vibrate during plant operations.

#### 5.0 INSPECTION

### 5.1 Inspection Program

The purpose of an inspection program is to identify any changes in the condition of the concrete or concrete properties which may affect the integrity of the structure and its future serviceability. Any changes can then be evaluated, and corrective actions can then be made if required. Guidance for evaluation of concrete in existing structures for service conditions has been developed by the American Concrete Institute (ACI), References (q), (t), and (u). Frequency of inspections is to be based on safety significance and rates of identified likely modes of degradation.

Guidelines for inspection of water-control structures associated with nuclear power plants are contained in Regulatory Guide 1.176, Reference (y).

# 5.2 Significance to Structures

An inspection program which provides for a condition survey in accordance with Reference (t) and evaluations in accordance with References (q) and (u) will provide assurance that the potential for significant degradation due to the following modes is monitored:

- o Corrosion of embedded metals
- o Freeze-thaw damage
- o Exposure to aggressive chemicals
- o Leaching of calcium hydroxide
- o Abrasion
- o Deterioration of anchorages to concrete

## 6.0 REFERENCES

- (a) ACI Special Publication SP-34, "Concrete for Nuclear Reactors."
- (b) NUREG/CR-4652, "Concrete Component Aging and its Significance Relative to Life Extension of Nuclear Power Plants."
- (c) "Concrete Deterioration Inspection System for Extending the Operating Life of Nuclear Power Plants Applied to Surry Unit One," Interim Report, Virginia Polytechnic Institute, July 1987.
- (d) "Pressurized Water Reactor Containment Structures License Renewal Industry Report," Nuclear Management and Resources Council, Inc., August 1989.
- (e) ACI 318-83, "Building Code Requirements for Reinforced Concrete."
- (f) Specification YS-312, "Specification for Ready-Mixed Concrete for Yankee Atomic Electric Plant."
- (g) Hilsdorf, H. R., Kroop, J., and Koch, H. J., "The Effects of Nuclear Radiation on the Mechanical Properties of Concrete,"

  Douglas McHenry International Symposium on Concrete and Concrete Structures, American Concrete Publications SP-55, 1978.
- (h) Specification YS-98, "Specification for Steam Turbine Generator."
- (i) Specification YS-315, "Specification for Concrete Construction and Floor Finish."
- (j) ACI 201.2R-77, "Guide to Durable Concrete," Reaffirmed 1982.
- (k) ACI 222R-85, "Corrosion of Metals in Concrete."
- (1) NRC Letter NYR 87-142, "NUREG-0825, Section 4.11, Seismic Design Considerations," dated July 16, 1987.

- (m) ACI 210R-87, "Erosion of Concrete in Hydraulic Structures."
- (n) ACI 215R-74, "Considerations for Design of Concrete Structures Subjected to Fatigue Loading," Revised 1986.
- (o) Specification YS-200, "Summary of Design Conditions."
- (p) ACI SP-103-87, "Anchorage to Concrete," G. B. Hasselwande, Editor.
- (q) ACI 207.3R-79, "Practice for Evaluation of Concrete in Existing Massive Structures for Service Conditions."
- (r) ACI 515.1R-79, "A Guide to the Use of Waterproofing, Dampproofing, Protective and Decorative Barrier Systems for Concrete," Revised 1985.
- (s) Memo CH 89-01, M. P. Hedges to J. T. McCumber, "Sulfate and Chloride Concentrations for PLEX Evaluations SR No. 88-382," dated January 3, 1989.
- (t) ACI 201.1R-68 (Revised 1984), "Guide for Making a Condition Survey of Concrete in Service."
- (u) ACI 224.1R-84, "Cause, Evaluation, and Repair of Cracks in Concrete Structures."
- (v) ASTM C856-83, "Standard Practice for Petrographic Examination of Hardened Concrete."
- (w) Letter, D. Robinson (Southport Marine, Inc.) to P. Laird (YNPS), "Report of Inspection of Intake Chambers and Intake Pipe," dated November 19, 1975.
- (x) Memo YRP 1072/89, N. A. Labrecque to J. K. Thayer/B. L. Drawbridge, "Repair of Concrete Piers for TK-31 and TK-32," dated July 27, 1989.

- (y) USNRC Regulatory Guide 1.127, "Inspection of Water-Control Structures Associated With Nuclear Power Plants." March 1978.
- (z) Prasad, N. and R. Orr, "Concrete Degradation Monitoring and Evaluation," NUREG CP-0100, March 1989.
- (aa) Memo CH 89-24, M. P. Hedges to T. J. McCumber, "Sulfate and Chloride Concentrations for PLEX Evaluation SR 88-382," dated August 4, 1989.

ATTACHMENT L
SAMPLE STRUCTURAL WALKDOWN DATA SHEETS

Procedure: YR-W1-37 Revision: 2 Page: 1 of 1

# ATTACHMENT A

# Plant Structure Description Form

itle: _						
escripti	ion: Steel frame single story building which houses diesel					
	generato	generators, 480V switchgear, high pressure and low pressure safety injection system. Nitrogen storage tanks				
	pressure					
	supported on steel framing above roof. Accumulator tank					
	encl. is	situated at one corner of the building.				
		Machine Location - 9699-FM-81A				
rrangem	ent Drawings:	Plans & Elevations/Cross Sections - 9699-FA-19A, 20A, 21A				
		Foundation Plans & Dets, Sht. 1, 2 & 3 - 9699-FC-63A, 63B,				
		Plan & Detail, Sht. 1, 2 - 9699-FS-25A, 25B				
		Conduit Drawings - 9699-FE-58A, 58B, 58BA 58BB, 58C				
		Safety Injection Water Piping - 9699-FP-46E, 46F, 46G				
Notes:	New Roof - EDCR-86-308					
	Building is in excellent condition with only minor degradation identified.					
	Some grout is not up tight under 2 column base plates and some rusting					
	was evident on the nitrogen storage support structure on roof and on condu					
	supports at ceiling of accumulator tank enclosure.					
	Preparer: P.	F. McHale Date: 10/18/89				
		N. Labrecque, P. McHale and H. Chander 10/18/89				

Procedure: YR-WI-37 Revision: 2 Page: 1 of 1

# ATTACHMENT B

# Walkdown Data Sheet

•	Structure:	(45) DGB Diesel Generator Building
•	Component Gr	oup: Concrete
١.	Component Ty	pe: Ground floor slabs and equip. foundations
	Potentially	Significant Age-Related Degradation?NOX_YES
5.		of Degradation?NOX_YES  Some minor cracking in various locations.
		Some minor cracking in slabs within diesel gen. cubicles.
6.	Harsh Envir	onment? NO YES
	Describe:	
7.	Remarks:	Equip. pads ok.  Cracks of shrinkage type and of no structural significance.
		Preparer: P. F. McHale Date: 10/23/89