



CONNECTICUT YANKEE ATOMIC POWER COMPANY

BERLIN, CONNECTICUT

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August 8, 1980

Docket No. 50-213  
A00898

Director of Nuclear Reactor Regulation  
Attn: Mr. Dennis M. Crutchfield, Chief  
Operating Reactors Branch #5  
U. S. Nuclear Regulatory Commission  
Washington, D.C. 20555

- References: (1) D. L. Ziemann letter to W. G. Council dated February 15, 1980.  
(2) D. L. Ziemann letter to W. G. Council dated March 6, 1980.  
(3) W. G. Council letter to D. L. Ziemann dated March 11, 1980.  
(4) W. G. Council letter to D. L. Ziemann dated March 12, 1980.  
(5) W. G. Council letter to D. L. Ziemann dated April 29, 1980.  
(6) D. L. Ziemann letter to W. G. Council dated March 28, 1980.  
(7) W. G. Council letter to D. M. Crutchfield dated May 1, 1980.  
(8) W. G. Council letter to D. M. Crutchfield dated June 2, 1980.

Gentlemen:

Haddam Neck Plant  
Environmental Qualification of Electrical Equipment

In References (1) and (2), the Staff identified a need for certain information relevant to evaluating the environmental qualification of Class 1E electrical equipment at the Haddam Neck Plant. Connecticut Yankee Atomic Power Company (CYAPCO) provided this information in References (3), (4), and (5). In Reference (6), the Staff supplemented its information requests by forwarding Enclosures 2 and 3 regarding plant-specific calculations for service condition profiles. References (7) and (8) provided this additional information.

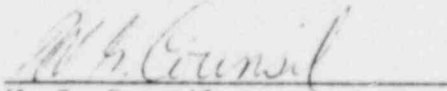
Constraints on available manpower and time resulted in Reference (8) information being submitted to the Staff on a non-QA basis. Completion of CYAPCO's QA review of the Reference (8) information has resulted in the identification of 12 incorrect responses. The attached pages identify these responses, together with the correct results. In 11 of these 12 cases, the incorrect value was conservative or the magnitude of the error was insignificant. The one exception is the response to Item 14b, regarding the mass and temperature of feedwater. In this instance, a significant length of piping was inadvertently omitted from the original calculations.

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CYAPCO trusts these errors have not resulted in any inconvenience to the Staff.

Very truly yours,

CONNECTICUT YANKEE ATOMIC POWER COMPANY

A handwritten signature in cursive script, appearing to read "W. G. Council", is written over a horizontal line.

W. G. Council  
Senior Vice President

Attachment

ATTACHMENT

HADDAM NECK PLANT

ENVIRONMENTAL QUALIFICATION OF ELECTRICAL EQUIPMENT

AUGUST, 1980

Question (1)

Reactor rated power.

Response

1825 MWT

Question (2)

Steam flow rate per steam generator at full speed.

Response

$1.9175 \times 10^6$  lb/hr.

Question (3)

Fluid mass in each steam generator at full power and hot shutdown.

Response

Revised

36058 lb at full power (total)

36014 lb at full power (total)

33117 lb at full power (liquid)

2941 lb at full power (steam)

2897 lb at full power (steam)

70760 lb at hot shutdown (total)

68488 lb at hot shutdown (liquid)

2272 lb at hot shutdown (steam)

Question (4)

Fluid energy in each steam generator at full power and hot shutdown.

Response

Revised

$1.903 \times 10^7$  BTU at full power

$1.898 \times 10^7$  BTU at full power

$3.879 \times 10^7$  BTU at hot shutdown

Question (5)

Steam line flow area.

Response

2.655 ft<sup>2</sup>

Question (6)

Time when steam isolation valves will close following a main steam line break.

Response

Ten (10) seconds -- Note: Non-return valves prevent backflow into the containment.

Question (7)

Mass of unisolated steam between a steam generator and the isolation valve following closure of main steam isolation valves.

Response

312 1B at full power  
409 1B at hot shutdown

Revised

308 1B at full power

Question (8)

Additional mass of unisolated steam if the main steam isolation valve nearest the break fails to close.

Response

Not applicable to CY. Non-return check valves will prevent additional backflow. Non-return valves are upstream of MSIV's.

Mass of steam between MSIV and non-return valves are as follows:

15 1B at full power  
20 1B at hot shutdown

Revised

39.6 1B at full power  
52.6 1B at hot shutdown

Question (9)

Main feedwater line flow area.

Response

0.706 ft<sup>2</sup>

Question (10)

Main feedwater enthalpy.

Response

410.4 BTU/lb

Question (11)

Time when main feedwater isolation valves will close following a main steam line break.

Response

Feedwater isolation manual at CV. Feedwater reg. valves fully closed at 31 seconds following MSLR.

Question (12)

Mass and temperature of feedwater between a steam generator and the feedwater isolation valve.

Response

16203 lb  
432°F

Question (13)

Mass and temperature of feedwater above 240°F between a steam generator and any redundant feedwater isolation valve.

Response

17434 lb  
432°F

Question (14)

Mass and temperature of all feedwater above 240°F.

Response

2.336 x 10<sup>4</sup> LBM @ 242°F  
3.337 x 10<sup>4</sup> LBM @ 289°F  
5.273 x 10<sup>4</sup> LBM @ 366°F  
5.467 x 10<sup>4</sup> LBM @ 432°F  
2.889 x 10<sup>4</sup> LBM @ 436°F

Response

2.302 x 10<sup>4</sup> LBM @ 242°F  
4.496 x 10<sup>4</sup> LBM @ 289°F  
4.806 x 10<sup>4</sup> LBM @ 366°F

Question (15)

Time when auxiliary feedwater injection will begin following a main steam line break.

Response

Six (6) seconds.

Question (16)

Auxiliary feedwater flow rate and enthalpy.

Response

666 gpm  
88.0 BTU/lb

Question (17)

Time when core flooding system will begin injection following a LOCA.

Response

22.2 seconds.

Question (18)

Fluid mass in the reactor system at full power and hot shutdown.

Response

Full power - 366171 lb  
Hot Shutdown - 361773 lb

Question (19)

Fluid energy in the reactor system at full power and hot shutdown.

Response

Hot full power =  $1.9665 \times 10^8$  BTU  
Hot zero power =  $1.9468 \times 10^8$  BTU

Revised

Hot full power =  $2.0510 \times 10^8$  BTU  
Hot zero power =  $1.9659 \times 10^8$  BTU

Question (20)

Hot and cold leg line flow areas.

Response

Hot leg = 4.125 ft<sup>2</sup>  
Cold leg = 4.125 ft<sup>2</sup>  
Cold leg PS = 4.587 ft<sup>2</sup>

Question (21)

Core flooding system flow rate and temperature.

Response

Flow rates - Figures 1 and 2  
Temperature = 100°F

Question (22)

Sensible heat in the core and reactor system metal that is above 240°F at full power operation.

Response

1.002 x 10<sup>8</sup> BTU

Revised

9.916 x 10<sup>7</sup> BTU

Question (23)

Initial hot and cold leg temperatures.

Response

T<sub>hot</sub> = 579°F  
T<sub>cold</sub> = 529°F