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October 8, 1989

U. S. Nuclear Regulatory Commission
Attn: Document Control Desk
Washington, DC 20555

Reference: Beaver Valley Power Station, Unit No. 1
Docket No. 50-334, License No. DPR-66
NRC Generic Letter 88-11

Gentlemen:

In the preparation of our response to NRC Generic Letter 88-11, "NRC Position on Radiation Embrittlement at Reactor Vessel Materials and Its Impact on Plant Operations," a typographical error occurred in Table 1 of Attachment 1.

Please find the corrected Table 1 attached. The correction transposes the surveillance capsule data in parentheses from "Longitudinal Welds (20-714 A & B) Weld Wire Heat 305414" to "Longitudinal Welds (19-714 A & B) Weld Wire Heat 305424." The correction identifies the surveillance weld as the intermediate shell longitudinal weld and brings it into agreement with other documentation.

These corrections have been discussed with the Beaver Valley Project Manager and the reviewers assigned to Generic Letter 88-11. If there are any questions concerning this submittal, please contact my office.

Very truly yours,

J. D. Sieber
Vice President
Nuclear Group

Attachment

cc: Mr. J. Beall, Sr. Resident Inspector
Mr. W. T. Russell, NRC Region I Administrator
Mr. P. Tam, Sr. Project Manager
Mr. R. Saunders (VEPCO)

A008

TABLE 1
BEAVER VALLEY UNIT 1 REACTOR VESSEL
BELTLINE REGION MATERIAL PROPERTIES

	Cu (Wt.%)	Ni (Wt.%)	CF	I[a] (°F)	M (°F)
Intermediate Shell Plate B6607-1	.14	.62	100.5	43	34[b]
Intermediate Shell Plate B6607-2	.14	.62	100.5	73	34[b]
Lower Shell Plate B6903-1	.20	.54	141.8 (167.9)[d]	27	34[b] (17)
Lower Shell Plate B7203-2	.14	.57	98.65	20	34[b]
Longitudinal Welds (19-714 A&B) Weld Wire Heat 305424	.28	.63	191.65 (191.4)	-56	65.5[c] (44.05)
Circumferential Weld (11-714) Weld Wire Heat 90136	.29	.07	132.9	-56	65.5[c]
Longitudinal Welds (20-714 A&B) Weld Wire Heat 305414	.34	.61	210.45	-56	65.5[c]

(a) The initial RT_{NDT} (I) values for the plates are conservatively measured values wheras the weld values are generic mean values for Linde 1092 and 0091 weld flux types [3].

(b) The standard deviation for the initial RT_{NDT} margin term for these materials is assumed to be zero since the initial RT_{NDT} values were obtained from conservative (i.e., "upper bound") test results.

(c) These are maximum "margin" (M) values. The standard deviation for ΔRT_{NDT}, σ_{Δ} , is 28°F for welds except that σ_{Δ} need not exceed 0.50 times the mean value of ΔRT_{NDT}. This exception can occur for these materials at low fluence values.

(d) Numbers in ( ) corresponds to surveillance capsule data.