

OCONEE-1,2,3

THE BABCOCK & WILCOX COMPANY  
POWER GENERATION GROUP

To C. A. Creacy - Service Manager

From D. J. Morris - Plant Equipment Services Section (Ext. 2057)

*D. J. Morris*

BOS 001-9

Cust. Duke Power Company

File No. or Ref. NSS-3,4, & 9

Subj. Trip Report  
PZR Code Safety Valves Meeting

Date May 25, 1976

This letter is cover one customer and one subject only

ATTENDEES

B&W

- C. A. Creacy
- J. C. Simonis
- D. J. Morris

Duke Power Company

- C. D. Hatley
- G. W. Hallman
- Bill Keisler
- Mike Alexander
- S. A. Holland
- W. E. Martin
- Harry Lipe-McGuire
- Ray Rider-McGuire

PURPOSE OF MEETING

To present to Duke the results of B&W's effort toward improving performance of pressurizer code safety valves. The meeting was conducted in accordance with the meeting agenda (Attachment 1).

MEETING MINUTES

Introduction - Presented an outline of the joint effort between B&W, Duke Power, and Dresser (Attachment 2).

Instrumentation on Oconee Unit 2 - Technical presentations by Jack Simonis on the PIPING LOADS/STRAIN GAUGE STUDY and the VIBRATION/ACCELEROMETER STUDY were very well received. These presentations readily demonstrated both the time and effort expended on these studies and the high degree of technical competence of the personnel involved. Due to his direct involvement in this program, he was also able to correlate his findings with other areas of the overall program. Following each technical presentation, a discussion of both specific and general conclusions which could be drawn from these studies as a result of both data analysis AND visual observations/common sense approach to all data presented.

DISCUSSION

Operating Plant Survey - Discussed the extensive nationwide PWR survey on operating plants. These included plants from coast to coast with several on-site visits. Both B&W and non-B&W plants were included in this survey. Specific areas of Maintenance, Handling, Testing, Piping arrangements, and Operating History were covered. A multitude of correlations were made which complemented the theories and results of the presentations by Jack Simonis.

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Several questions were raised by the customer during this discussion in each of the areas covered, indicating a high degree of enthusiasm toward the information presented. At the conclusion of the Survey discussion, handcuts were presented on the information obtained (Attachment 3), and a sample of the Survey questionnaire (Attachment 4).

Present Status at TMI and Crystal River - A brief discussion of recent events at these plants was conducted which primarily emphasized the high degree of correlation between those events and previously discussed theories and information.

Conclusions and recommendations were then presented, along with the schedule for implementing the action plan (Attachments 5 and 6). Duke agreed to the action plan and as a result of the discussions, decided to implement vertical handling of these valves as soon as possible. The agreement was made to have detailed maintenance, handling and testing procedures available for use and an on-site test facility constructed in time for the Unit 3 refueling in September.

The meeting was highly successful and more than adequately accomplished its purpose.

Duke Power was impressed with the work that was required to retrieve the information and well pleased with B&W's interpretation and analysis which provided a logical/common sense set of recommendations.

DJM:Nf

Attachments

cc: K. R. Ellison  
J. A. Middleton  
R. L. Pittman  
H. Honig  
J. M. Neilson (ARC)  
J. C. Simonis

DUKE POWER COMPANY  
PRESSURIZER CODE SAFETY VALVES

MEETING 5/19/76

A G E N D A

INTRODUCTION	DuWayne Morris
PIPING LOADS/STRAIN GADGE STUDY	Jack Simonis
VIBRATION/ACCELEROMETER STUDY	Jack Simonis
DISCUSSION	DuWayne Morris
OPERATING PLANT SURVEY (INCLUDES MAINTENANCE, HANDLING, AND TESTING)	
PRESENT STATUS AT TMI AND CRYSTAL RIVER	
SUMMARY OF CONCLUSIONS	
RECOMMENDATIONS FOR OCONEE NUCLEAR STATION	
ACTION PLAN AND SCHEDULE	

INTRODUCTION

Efforts were initiated by B&W toward improving performance of pressurizer code safety valves as a direct result of B&W and customer concern over recurring problems with excessive valve leakage. This concern was expressed to Dresser which resulted in a joint effort between B&W and Dresser.

The first step taken was to determine, by joint discussion, the probable causes for excessive leakage based upon all information available at the time. The following items were determined to be the most probable causes for excessive leakage:

PROBABLE CAUSES

- A. Ambient temperature and associated thermal profile effects.
- B. External piping loads created by thermal growth during Rx heatup resulting in excessive mechanical strain on valve internals.
- C. Vibration of sufficient magnitude may result in relative seat/disc movement and associated surface degradation.
- D. Maintenance techniques may need to be more stringent to insure proper seating.
- E. Handling and installation should be closely scrutinized to insure that the seating surfaces are not damaged during these processes.
- F. Valve testing, specifically hot vs. cold setting of these valves, needs closer analysis to determine set point drift associated with the thermal growth of valve internals.

Subsequent to determination of the most probable causes listed above, a course of action was established to facilitate assignment of relative magnitudes and/or elimination of each of the aforementioned probable causes as follows:

ACTION TAKEN

- A. An extensive nationwide PWR survey was undertaken on operating plants to provide additional information, both general and specific. This included several on-site visits coast to coast and lengthy survey questionnaires at both B&W and non-B&W plants.
- B. Determine external piping loads at Duke Power Company's Oconee Unit II through both visual observations and installation of strain gauge instrumentation.
- C. Determine effects of vibration at Oconee Unit II by installation of accelerometer instrumentation on the valve body.

- 2 -

- D. Installation of thermocouple instrumentation to provide valve and piping thermal profile information at Coocsee Unit II.
- E. Discuss the results of the above listed actions with Dresser.
- F. Formulate a new plan.

With regard to the action plan, tremendous cooperation, effort, and technical assistance was obtained from all personnel involved in the instrumentation and data retrieval on the Coocsee Unit II valves. The efforts of Olie Bradham, Bill Keisler, Mike Alexander, John Neilson (ARC), Bill Crawford (ARC), and Jack Simons (OFR) were particularly outstanding and greatly appreciated.

PRESSURIZER CODE SAFETY RELIEF VALVES GENERAL INFORMATION

PLANT	REACTOR SUPPLIER	DESIGN ENGINEER	VALVE VENDOR	LOOP SEAL	INLET SIZE	NET MINE	Commercial Date	ICD* INLET CAPACITY DATA PROBLEMS	Overhaul Set Point %	Greening Feature	Open Press. Set Point %	Final Polish GRIT #	Weld Problems Lapping?	Location TESTING	TEST Method	HINDLING
ARKANSAS 1	B+W	BENTEL	DRESSER	No	3"	810	10/74	-0-LCD	2155	2155	86.2	1000	VENDOR	IN PLACE	HYDRO-TEST	
CALVERT CLIFFS	COMBUSTION	BENTEL	DRESSER	No	2 1/2"	800	10/75	YES	2250	2250	90	1000	UTILITY	HOT SHOP	MANUAL SHUT DOWN	
MILSTONE 2	COMBUSTION	BENTEL	DRESSER	No	3"	790	11/72	NO	2235	2235	89.9	8000	UTILITY	WILEY LAB	STEAM-HOT TRUCK	
CONVERT CLIFFS 1	B+W	UTILITY	DRESSER	No	2 1/2"	387	2-23/24 10/75 LCD	NO	2155	2155	86.2	1000	VENDOR	WILEY LAB	STEAM-HOT TRUCK	
PALISADES	COMBUSTION	BENTEL	DRESSER	No	3"	700	12/71	Y. REMAIN	1800	1800	72	1200	UTILITY	HOT SHOP	MANUAL SHUT DOWN	VERTICAL
SANDWICH 1	WESTINGHOUSE	BENTEL	CROSBY	No	3"	430	1/68	YES LCD	2085	2085	83.9	8000	UTILITY	CONTAINMENT	MANUAL SHUT DOWN	VERTICAL
SMUD	L+W	BENTEL	DRESSER	No	3"	913	4/75	-0-LCD	2155	2155	86.2	1000	UTILITY	MMR SHOP	MANUAL SHUT DOWN	VERTICAL
TRINITY 1	B+W	GILBERT	DRESSER	YES	2 1/2"	818	9/74	20 LCD	2155	2155	-83.9 83.5	1000	VENDOR	CONTAINMENT	MANUAL SHUT DOWN	VERTICAL

NOTES: CALVERT CLIFFS 1 - HAS 1/2" INLET EXPANSION LOOP - SET POINT CHANGES NOTED BETWEEN FIRST / SECOND LIFT CHECK SET POINTS - 27% MAIN YANKEE - SUMMER OF '75 UPGRADED PRIMARY PRESS FROM 1800 TO 2235 PSI, NO CHANGES NOTED THIS YEAR - UP UNTIL LAST FUELING CYCLE TESTING WAS CONDUCTED ON SITE WITH ME.

PALISADES - 1973 DE-RATED PRIMARY PRESS. FROM 2100 TO 1800 PSI NORMAL OPERATING

FIELD REPRESENTATIVES - SMUD - WERNER STEEL  
 TRINITY 1 - ROLAND PRUETT - TOM CASHBY  
 CROSBY - TOM CASHBY  
 PALISADES - WERNER STEEL

\*MILSTONE 2 - LOOP SEAL IS ELECTRICALLY HEATED TO 230°F

G. Tom Cashby  
 C. Tom Cashby  
 W. Werner Steel  
 W. Werner Steel

ATTACHMENT 3

PRESSURIZER CODE SAFETY RELIEF VALVES FIRING ARRANGEMENT

PLANT	GIMBAL EXP. JOINTS	BELLOWS	SPRING HANGERS	HYDRAULIC SAFEBITS	INLET EXP. 4-1-P	INLET LOOP SEAL	(CUSTOMER COMMENT)	FIRING ARRANGEMENT
ARKANSAS 1	No	No	Yes	Yes	No	No	YES	SEE TEST RESULTS BY BECHTEL TP 800.29
CAVENDISH			Yes	Yes	Yes	No		
MADEIRA					No	No	Yes	
MILLER 2			Yes	Yes	N/A	Yes		
CONVERSE 1	Yes-18A	No	No	Yes	No	No	Yes	
PARSONS					No	No	No	
SANDRIDGE 1	No	No	Yes	No	No	No	Could be improved	
STUD	Yes-2E	Yes	No	No	No	No	OK	
TMT-1	No	No	Yes	No	N/A	Yes	Yes	

ATTACHMENT 3

PRESSURIZER CODE SHEET, RELIEF VALVES, CRAFTSMANSHIP

PLANT	WHO PERFORMS LAPPING	FINAL PAUSE GRIT #	OPTICAL FLATNESS CHECKS		VISUAL INSPECTION		COMMON ASPECTS	OPTICAL FLATNESS	MISCELLANEOUS AIDS FOR UTILITY	CLEANING FLUID USED	WHO PERFORMS ASSEMBLY	IS OBTAINING PARTS A PROBLEM?
			LAPPING BEFORE USE	AFTER USE	WAVE SENT	WAVE DIS						
APRINESS 1	VENDOR	1000	No	No	No	NO GAPS	EYE BALL	EYE BALL	NOT USED	ACETONE	UTILITY	No
CELESTICUS	UTILITY	1000	No	No	No	EYE BALL	EYE BALL	NOT USED	NOT USED	ACETONE	UTILITY	No
HAINE VALVE	UTILITY	800	No	No	No	EYE BALL	EYE BALL	NOT USED	NOT USED	SOLVENT	UTILITY	No
MILITINE 2												
GENES 1	VENDOR	1000	No	No	No	EYE BALL	EYE BALL	NOT USED	NOT USED	Spot check	UTILITY & VENDOR	NO
BRISADES	UTILITY	1200	No	No	No	EYE BALL	EYE BALL	NOT USED	NOT USED	ACETONE	UTILITY	YES DURING TESTING
SANCOUSE 1	UTILITY	800	Yes	Yes	± Tightend	No	EYE BALL	EYE BALL WITH HIGH SENSITIVITY	GOOD	ACETONE	UTILITY	YES
SMUD	UTILITY	1000	± Tightend	No	± Tightend	No	MIL GAPS	MIL GAPS	GOOD	ACETONE	UTILITY	No
TMI-1	VENDOR	1000	SEE VENDOR									

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ATTACHMENT 3

PRESSURIZER CODE SAFETY RELIEF VALVES TESTING & HANDLING

PLANT	LOCATION OF TESTING	M-LIFT TESTING		LEAKAGE TESTING		IN PLACE TESTING		HANDLING - IN SUPERVISION			
		AMBIENT TEST MEDIUM	TEST MEDIUM	LEAK TEST PRESSURE	LEAK TEST MEDIUM	LEAK TEST TIME	LEAK TEST SPECIFICATIONS	HAVE VALVES BEEN TESTED IN PLACE?	SUCCESS AT PLACE TESTING	ALL VALVES TESTED FROM 0200 - 0200 AT ALL TESTING TIMES?	TESTING HANDLES
BRANDS 2	IN PLACE	STEAM	2500					YES	GOOD	NO	UTILITY
Calver Clipp 1	HOT SHOP	AMBIENT N <sub>2</sub>	2485 ± 1%	2500 PSI	N <sub>2</sub>	5 MIN	410 PSI	NO	N/A	N/A	UTILITY
Calver Clipp 2	HOT SHOP	AMBIENT N <sub>2</sub>	2485 ± 1%	2200 PSI	N <sub>2</sub>	3 HRS	500 PSI	NO	N/A	N/A	UTILITY
Calver Clipp 3	HOT SHOP	AMBIENT N <sub>2</sub>	2485 ± 1%	2100 PSI	N <sub>2</sub>	15 MIN	450 PSI	NO	N/A	N/A	UTILITY
SPUD	HOT SHOP	AMBIENT N <sub>2</sub>	2435	2300 PSI	N <sub>2</sub>	10 MIN	200 PSI	YES	GOOD	YES	UTILITY
THZ-2	HOT SHOP	AMBIENT N <sub>2</sub>	2435	2290 PSI	N <sub>2</sub>	NO BUB	200 PSI	YES	GOOD	YES	UTILITY

NOTES: CALVERT CLIPP 1 - SET POINT DEVIATION IS NOTED ON FIRST LIFT CHECK - IN ONE CASE, MANUAL ACTIVATION REQUIRED, HOWEVER, SUBSEQUENT LIFT CHECKS ARE OK. VALVES ARE NOT COMPLETELY VERTICAL AT ALL TIMES DUE TO PIPING ARRANGEMENT OBSTRUCTIONS DURING INSTALLATION

OCONEE - MAINE YANKEE - LEAK TEST SPECIFICATIONS: ZERO CONDENSATION ON MIRROR HEAD AT DISCHARGE. NEARLY CHANGE IN TRANSDUCER WATER LEVEL AFTER 3 HRS AS A CLOSED SYSTEM DISCHARGE.

## PRESSURIZER CODE SAFETY RELIEF VALVES QUESTIONNAIRE

Page 1 of 8

## OPERATING HISTORY:

1. Do you have machinery history on the valves?  
If yes, may I obtain a copy?
2. Can you discuss the operating history and any items which may not appear in machinery history?  
Include:
  - A.) Description of malfunction:
    1. Downstream temperatures
    2. Quench tank temperature
    3. Time from installation to malfunction
    4. Calculated or known leak rates
    5. Plant conditions or transients which may have contributed to malfunction such as lifting of the electromagnetic relief valve.
  - B.) Any opinion on cause of malfunction?
  - C.) Any unusual conditions noted on disassembly or subsequent testing?  
Including:
    1. Wire drawing, cutting, visual appearance + ability to lap clean.
    2. Foreign matter in seat area?
    3. Internal misalignment?
    4. Scratches and/or cracks in seat or disk?  
Description and size.
    5. Set point OK on re-assembly?
    6. Leak test OK after testing?
    7. Have valves been cause for plant shutdown?
3. What model Number valve do you have?  
Inlet size:            Outlet size:
4. Has there been a difference in performance between one valve installation and the other? If so, what do you attribute this performance to? Briefly describe any difference in downstream piping arrangements.

## PLANT OPERATIONS:

5. Have the code safety valves ever lifted as protective action (overpressurization)?  
If so, describe plant conditions and results.

(2)

Page 2 of 8

6. What is plant operating pressure?  
Electromagnetic relief set press?      Code relief set press?
  
7. Has there ever been a change in the specified normal plant operating pressure?  
If so, state the approximate date of change; state what the change was, and  
any noted change in code valve performance.

## CRAFTSMANSHIP:

8. Who actually performs valve lapping? (Utility - Vendor)
  
9. What type and grit number of lapping compound is used for final polish?
  
10. Are any mechanical aids used to provide uniformity in lapping? If yes,  
please describe.
  
11. Are lapping blocks checked for optical flatness prior to use? If yes,  
what is the required specification for acceptable use?
  
12. Are lapping blocks re-used? Do you change lapping blocks when changing from  
a low to a higher grit number lapping compound?
  
13. Are lapping blocks visually inspected prior to use? If yes, is a magnifying  
glass used?
  
14. Describe your cleanliness procedures and lapping compound removal techniques.
  
15. Are lapping blocks checked for flatness after lapping. If yes, what is acceptable?  
Is a visual inspection of lapping blocks conducted after final polishing?

(3)

16. Is the valve seat and/or disk checked for optical flatness after lapping? If yes, what is the flatness required?
17. Do you conduct a visual inspection of the valve seat and disk after final polish? Describe the technique used.
18. Who supervises lapping assembly? (Utility - Vendor)
19. Who performs the assembly and adjustment of the valves? (Utility - Vendor)
20. Is dirt or other foreign matter a problem?
21. Are any special techniques used for assembly? Is verticality maintained throughout assembly?
22. Are the optical flats used for maintenance of these valves in good conditions and calibrated?

TESTING:

23. Where are the valves tested? (Containment, shop, off-site).
24. How often are valves disassembled and tested?
25. How are the valves tested? (Hydro-assist, N<sub>2</sub> Press, steam, in place etc.)

(4)

26. Lift pressure specification?
27. Are the valves heated during testing?  
State temperature. Any set-point drift noted?
28. Leak testing pressure: Temp:  
Medium (H<sub>2</sub>O, N<sub>2</sub>, steam): Leakage specification:  
Success?
29. Have the valves ever been tested in place?  
Primary press: Temperature: Success?
30. Are there any decontamination problems with these valves?
31. Who supervises the testing?

## HANDLING:

32. Are the valves ever shipped by air or freight?  
Opinion of handling? Re-work required?
33. What method of handling is used on site?  
(Sling, verticality maintained, crate to fork lift used, prevention  
of bumping and jolting).

34. Who supervises handling? (Utility - Vendor - supervisory personnel)

PROCEDURE:

35. Do you have a written maintenance procedure for these valves? If yes, may I obtain a copy?

PIPING ARRANGEMENT:

36. May I obtain a copy of code valve discharge piping drawings including isometrics?

27. Describe your discharge piping arrangement including the following:

- |                              |  |
|------------------------------|--|
| A.) Bellow expansion         | E.) Distance from inlet flange to pressurizer?                     |
| B.) Spring hangers           | F.) Describe any cold spring noted during installation or removal. |
| C.) Hydraulic snubbers       |  |
| D.) Gimbals expansion joints |  |

(6)

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38. Have you ever installed:

- A.) Thermocouples
- B.) Strain measuring equipment
- C.) Vibration monitoring equipment
- D.) Pipe displacement measuring equipment

If yes, what were the results and what is the opinion with regard to data reliability?

39. State your opinion of your code valve piping arrangement including the following:

- A.) Designed well?
- B.) Eliminates excessive stress?
- C.) Has valve Vendor commented on it?
- D.) Opinion of A/E who designed + installed system?

40. Have there been changes in discharge piping and/or support system since initial installation? If so, when? Why? What is your opinion of before and after such modifications?

41. What is your opinion on the H<sub>2</sub> erosion theory?

(7)

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42. What is your opinion of inlet loop seals?

QUESTIONS ABOUT THE VALVE VENDOR:

43. What is your opinion of valve performance?

44. Do you receive good parts support?

45. What Vendor representatives have you been associated with?

46. What is your opinion of their craftsmanship and technical competence?

47. What is your opinion of their availability and co-operation?

48. Has the Vendor made any modifications or material changes? Why? Did this affect performance? Did you agree with the changes made?

49. What is your opinion of the other Vendor? (Crosby-Dresser)  
What experience have you had with Crosby-Dresser?

50. Have you ever requested or acquisitioned new valves as spares or replacements? If so, why? What time-lag resulted from such requests?



(B)

51. Do you notify the Vendor each time you have a problem? If yes, what are the results of such notification?

MISCELLANEOUS

52. Have you discussed code valve problems with other utilities. Who? Problems? Co-operation? Scope of discussion?

53. If you have discussed code valve problems with other utilities, do you believe such discussion and/or visits are useful?

H:re

SCHEDULE OF EVENTS

ACTIVITY	APRIL	MAY	JUNE	JULY	AUG.	SEPT.	OCT.	NOV. & DEC.
1. Inst. & Maint. Man. Draft to B&W Review by B&W	Dresser will be late Plant on Strike							
2. Testing Reconm. Draft to B&W Review to Dresser								
3. Temp Amb & Profile to Dresser ASAP	Complete 3/3/76							
4. CK Power Ramps for Press Trans on B&W Op. Plants ASAP	Complete 3/3/76							
5. Method for Early Leak Detection Pre. Info. to Dresser								

TRANSMITTAL SLIP

PLANT STARTUP SERVICE SITE PROBLEM REPORT

ORIGINAL

\*\*\*CLEARED\*\*\*

TO: \_\_\_\_\_ For Information

Central Engineering Files

C. C. Plunkett - Contract Admin.

C. M. Fletcher - Quality Assurance

R. G. Burney - Task Engineer

W. A. Cobb - Sr. Proj. Manager

FILE: 1247

CONTRACT NO: 620-00 04

SPR 222

TITLE LEAKING PRESSURIZER

RELIEFS & BLOCK VALVES

DATE: 1/29/75

The attached, cleared SPR is submitted for your information.

TO: \_\_\_\_\_ J. L. Hollis - FLORIDA \_\_\_\_\_

\_\_\_\_\_ E. L. Logan - SNUD \_\_\_\_\_

\_\_\_\_\_ B. L. Day - TOLEDO \_\_\_\_\_

\_\_\_\_\_ R. J. Baker - Ocala \_\_\_\_\_

\_\_\_\_\_ L. C. Rogers - MET ED \_\_\_\_\_

\_\_\_\_\_ J. A. Bailey - ARKANSAS \_\_\_\_\_

Attached is one copy of Site Problem Report No. 222 which was processed on Contract 620-00 04. Future contracts have been reviewed for the potential of a similar problem. This problem is not considered applicable to other contracts NSS-3 → 14.

REMARKS: \_\_\_\_\_

\_\_\_\_\_

\_\_\_\_\_

\_\_\_\_\_

cc: R. E. Hosiba

G. K. Wandling  
G. K. WANDLING  
NUCLEAR SERVICE SUPPORT ENGINEER  
NSSSE

CLEARED

SITE PROBLEM REPORT

BARCOCK & WILCOX

CUSTOMER *Duke Power Co.* CONTRACT NO. *620-0004* SPR NO. *222* REV. NO. *0*

VENDOR *Oresser* P.O. NO. TASK NO. *28* GROUP NO. *41* SEQ. NO. *2-5*

SITE ENGINEER *R.S. Baker, Jr.* REQ'D. RESOL. DATE *NA* REQ'D. COMP. DATE *NA*

TITLE *Leaking Pressurizer Reliefs and Block Valves*

DESCRIPTION OF PROBLEM  
*See attached*

STATUS - ACTION TO DATE INCLUDING PERSONS CONTACTED  
*See attached*

FURTHER ACTION RECOMMENDED BY SITE PERSONNEL  
*Duke is handling this problem - No B&W action required at this time.*

ORIGINATOR SIGNATURE *R.S. Baker* DATE *1/20/75*

RESOLUTION

APPROVED BY SIGNATURE DATE

N.S. SUPPORT ENGINEER *[Signature]* *1-27-75*  
TASK ENGINEER *No Eng. Action Required*

PROJECT MANAGER *C.D. Cready* *1-30-75*

COST CATEGORY  NORM  C  D  G  L  VENDOR CLAIM

AUTH. CHARGE NO.  FIELD CHANGE REQ. FC NO.

SITE COMPLETION REPORT  
*See attached*

RECOMMENDED STDS. CHANGE

FINAL DISTRIBUTION

DEVIATIONS  NONE  SEE SPR REV. NO. \_\_\_\_\_

PROJECT MANAGER  
S.O.M./CONSTR. REP.  
QA DOC. FILE  
CENT. ENGR  
FILE 12M.2

DATE COMPLETED SIGNED BY *R.S. Baker* DATE *1/24/75*

S.O.M./CONSTR. REP. APPROVAL *[Signature]* DATE *1/24/75*

INSTRUCTIONS FOR PDS-11091 - SITE PROBLEM REPORT

Initiated by NPG Nuclear Service

- (1) Originator - Fill in: Customer; Contract Number; Vendor; Purchase Order Number; Task Number; Group Number; Sequence Number; Name; Title; Description of Problem; Status; Further Action Recommended by Site Personnel; Originator Signature and Date; Vendor Claim (if applicable).
- (2) Site Operations Manager - Fill in: SPR Number; Revision Number; Req'd. Resol. Date; Req'd. Comp. Date; Approval Signature; Date.
- (3) Nuclear Service Support Engineer - Fill in: Cost Category; Authorized Charge Number.
- (4) Task Engineer - Fill in: Resolution; Recommended Std.'s Change\*; (if applicable, FC Req. and FC Number); Signature and Date.  
  
\*If recommended standard's change, transmit a copy to cognizant Standard Task Engineer to resolve with Standard Plant Manager.
- (5) Field Engineer - Implement resolution; upon completion, fill in: Completion Report; Date Completed and Signature.  
  
NOTE: If necessary to deviate from the approved SPR, note deviation and submit revised SPR to the Site Operations Manager.
- (6) Site Operations Manager - Approve completion; sign.

Initiated by B&W Construction Company

- (1) Originator - (Same as (1) above)
- (2) Construction Co. Site Representative - (Same as (2) above)
- (3) Project Manager - (Same as (3) above)
- (4) Task Engineer - (Same as (4) above)
- (5) Construction Co. Site Representative - (Same as (5) and (6) above)

Description of Problem

With reactor power at about 100% from the first of the year, the plant had to be shutdown and cooled down on 1/18/75 due to the general tank temperature being at  $230^{\circ}\text{F}$ .

On 1/7/75 the temperature was at about  $200^{\circ}\text{F}$  and so Duke shut the electromagnetic relief valve block (2RC-V2). The tank temperature dropped to  $195^{\circ}\text{F}$  by the next day but slowly started increasing again. Between 1/9/75 and 1/18/75, Duke succeeded in keeping the tank temperature below  $215^{\circ}\text{F}$  (DP-1101-01 limit) by using the Unit 1 and 2 A bleed hold up tank as a source of water to bleed and feed well. This cooled the general tank to about  $205^{\circ}\text{F}$  but raised the "A" BAVT temperature to about  $195^{\circ}\text{F}$  on Unit 1 and 2. On 1/18/75 the general tank temperature went to  $230^{\circ}\text{F}$  despite all efforts and the plant had to be shut down.

NSS-4 / SPR-222

Status - Action to Date

Nuclear Service in Lynchburg (R. J. McNeill, J. P. Kennedy) informed on morning phone call each day from 1/7/75 until S/O on 1/18/75.

Duke made a complete check of all pipes leading to the quench tank while the plant was still at hot condition and the following is the results:

1. The thermograph mounted on the discharge pipe of the three pressure relief valves were not reading correctly due to not being installed properly or not installed at all.
2. One or both of the pressure code reliefs was/were leaking through its seat (s).
3. The electromechanical relief (ZRC-RV3) was also leaking through its seat.
4. ZRC-V2 was also leaking through seat because it was not shut completely tight.

NSS-4/SAR-222

Site Completion Report

Since Unit I was shut down and Duke's spare code relief are at the factory, the Ocone I code reliefs (RC-RV4A+B) were removed and installed on Ocone II. The spare reliefs are to be shipped back to the site before Ocone I needs them.

The electronic relief (2RC-RV2) was inspected and found to have two steam cuts on the disc of the valve. Duke replaced the disc with spares.

The electronic relief valve block valve (2RC-V2) would not shut tightly because of the old continuing problem of this valve on all B&W units sticking shut at hot conditions (See NSS-9/SAR-91). In an attempt to prevent this valve from sticking in the shut position, Duke, sometime in the past, reduced the torque switch setting. Because of this the valve did not shut tightly enough to prevent leakage. Duke is



NSS-4/SAR-222

increasing the tongue switch setting on this valve and writing a letter to BSW outlining all the problems they are having with this valve on all units.

The thermocouples have been installed properly on the discharge pipes of the relief and the plant is presently heating up with no leakage past the relief noted yet.