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PRINCIPLE PARAMETERS FOR  
RADIOLOGICAL ASSESSMENT

MAY 1980

THIS DOCUMENT CONTAINS  
POOR QUALITY PAGES

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PRINCIPLE PARAMETERS FOR RADIOLOGICAL ASSESSMENT  
DAWN MINING COMPANY  
MAY 1980

Ore Quality,  $U_3O_8$  : 0.153%

From Newmont Mining Corporation annual report 1979. Grade given is average grade of remaining ore reserves. Does not include protore. The assumption is that additional ore reserves will be discovered and protore will not be milled at Ford. In 1979 the average grade milled was 0.134. During 1980 the expected average grade is 0.105%  $U_3O_8$ .

Ore Activity,  $U_{238}$ ,  $U_{234}$ ,  $Th_{230}$ ,  $Ra_{226}$ ,  $Pb_{210}$  : in pCi/g

$U_{238}$ : 350 $\pm$ 40	$Th_{230}$ : 235 $\pm$ 50
$U_{234}$ : 350 $\pm$ 40	$Ra_{226}$ : 215 $\pm$ 90
$Pb_{210}$ : 500 $\pm$ 15	

Eberline Instrument Corporation Assay

Operating Days Per Year (Plant Factor): 346 days

Bases on 1979 plant availability of 95.4% and two shutdown holidays.

Process Rate: 165,000 tons per year

Based on three year average 1977,78,79.

Mill Water Throughput: 224,000  $m^3$  per year

Based on 40% solids by weight (1979 average).

Total Mine Area

Active Mine Area

Average Mine Depth

} Not applicable  
Mine 22 miles from mill.

Annual Average Morning Mixing Height: 282 meters

From Spokane County Air Pollution Control Authority-Personal Communication 12-4-79.

Annual Average Afternoon Mixing Height: 1521 meters

Same as above.

ORE HANDLING AND STORAGE

Estimated Capacity of Ore Per Delivery: 21.6 metric ton

Based on 1979 average scale readings.

Number of Deliveries: 44 perday or 264 per week

Ore hauled during summer only for 26 weeks, 6 days per week or 156 days. Total ore hauled is 165,000 tons requiring 6,875 trips or 264 trips per week or 44 trips per day.

Estimated Ore Dust Released in Delivery: 0.009 kg per hour

Amount calculated using NUREG-0511 Appendix G-1  
Release rate of 1 metric ton per year for total ore pad  
Emissions corrected to Dawn's smaller mill throughput and assuming two thirds of dust due to loader and one third due to truck delivery.

$$(1000 \text{ kg/MT}) \times (1 \text{ MT/yr}) \times \frac{430 \text{ MT Dawn}}{1800 \text{ MT Geis}} \times (1/3) \div \frac{8760 \text{ hrs}}{\text{yrs}} = 0.009 \text{ kg/hr}$$

Average Grade of Ore and Ranges: 0.153% (.06 to .30)

Based on official ore reserve data.

Capacity of Ore Pad: Present and Final Year of Operation:

115,000 metric tons - present	}	Based on 20 yrs experience
115,000 metric tons - final		

Maximum Area of Ore Pad and Height in Terms of Final Year of Operation: 55,000 sq. meters-area; 6 meters-height

Based on actual measurement of present pad which is not expected to change.

Approximate Amount of Ore Handled Per Day

ie, unloaded, loaded, bulldozed, etc: 1060 metric tons (summer)  
430 metric tons (fall, winter, & spring)

Loader: 430 MT  
Dozer: 200 MT (summer only)  
Trucks: 430 MT (summer only)

Operation Time of Front End Loaders, Hoppers, Feeders, and

Other Ore Pad Equipment: 6 hours per day

Loader utilization 1979 average - 6 hours per day

Estimated Amount of Fugitive Dust Emission : 0.03 kg per hour  
Due to Handling Ore Pad Equipment

Amount calculated using NUREG-0511 Appendix G-1  
 Release rate of 1 metric ton per year for total ore pad.  
 Emissions corrected to Dawn's smaller mill throughput and assuming  
 two thirds of dust due to loader and one third to truck delivery.

$$(1000 \text{ kg/hr}) \times (1 \text{ MT/yr}) \times \frac{430 \text{ MT Dawn}}{1080 \text{ MT Geis}} \times (2/3) \div 8760 \text{ hr/yr} = 0.03 \text{ kg/hr}$$

Dust Emission Control Reduction Factor: 50%  
by Wetting Chemical or Other Controls

Wetting - 50%  
 Water wagon used three times daily or more frequently depending on  
 weather. Mine Safety and Health Administration measurements of re-  
 spirable dust have recorded a maximum of 5% of TLV during their  
 periodic inspections.

Ore Pad Area and Height: 55,000 square meters - area  
 6 meters - height

Ore Storage Time: 180 days

Bases on 6 months ore haul.

CRUSHERS, GRINDERS, RODMILLS,  
FINE ORE BLENDING

CRUSHER

Operation Time: 8 hours per day, 258 days

Crusher on 5 day per week schedule. One shift per day.

Ore Process Rate: 148,500 metric tons per year

165,000 tons x 9 = 148,500 metric tons

Total Ore Quantity Handled: Same as above.

Estimated Dust Lost to Atmosphere: 0.003 metric ton per year

Measured release rate 1.586 grams per hour  
 Hours operated in 1979: 2070 hrs.

$$(2070 \text{ hrs}) \times (1.586) \div (1000 \text{ kg/ton}) \div (1000 \text{ g/kg}) = 0.003 \text{ MT/YR}$$

Efficiency of Emission Control Devices: 99.5 Effective  
 99.9 Design

Data from manufacture of bag house.

BALLMILL

Operation Time: 24 hours per day                      346 days per year

Based on 1979 actual hours operated.

Ore Process Rate: 148,500 metric tons per year

Total Quantity Handled: 148,500 metric tons per year

Estimated Dust Lost to Atmosphere: -0-

Wet process

OTHER

Estimated Dust Lost to Atmosphere through  
Internal Ore Transportation Devices: 0.005 kg per hour

This is only an educated guess

Efficiency of Emission Controls of Internal Ore  
Transportation Devices: 80% effective  
90% design

This is only an educated guess.

Average Daily Capacity of Temporary Bin Storage: 810 metric tons

Efficiency of Controls for Temporary Bin Storage: 80%

This is an estimate only.

YELLOWCAKE DRYING & PACKAGING

Note: The yellowcake drier and packaging are interlocked and one cannot operate if the other is down.

Processing Rate: 0.02 metric tons per hour

Calculated as follows:  $(400,000 \text{ } ^\# \text{ U}_3\text{O}_8) \div (2,200 \text{ } ^\# \text{ /MT}) \div (8712 \text{ hrs}) = 0.02$   
metric ton  
per hour

Operating Time: 298 days per year                      24 hours per day

Based on 1979 data. Yellowcake drying and packaging has excess capacity, hence does not operate the full 346 days the mill operates.

Efficiency of Control of U<sub>3</sub>O<sub>8</sub> Dust Released to Atmosphere: 98% design  
96% effective

Data from manufacturer of wet dust collector (ROTO Clone)

Estimated U<sub>3</sub>O<sub>8</sub> Dust Released to Atmosphere:

Packaging: 0.02 kg/hr }  
 Dryer: 0.02 kg/hr } measured release  
 (total particulate)

Stack Heights: Packaging: 11 meters  
 Drier: 20 meters

Recovery Rate of U<sub>3</sub>O<sub>8</sub>: 90.8% (1979 actual)

Extraction Efficiency: 95.0% (1979 actual)

Yellowcake Yield: 200 tons per year

Calculated as follows:  $(400,000^{\#} \text{ U}_3\text{O}_8) \div (2000) = 200$

Yellowcake Quality, U<sub>3</sub>O<sub>8</sub>: 79%

Actual 1979 data

Yellowcake Drying Stack Effluent, U<sub>3</sub>O<sub>8</sub>: 137 kg per year

Calculation:  $(.02 \text{ kg/hr}) \times (8712 \text{ hr/yr}) \times (79\% \text{ U}_3\text{O}_8) = 137 \text{ kg/hr}$

Yellowcake Drying Stack Filter Efficiency:

98% design  
 96% effective

Data from manufacturer of wet dust collector (ROTO Clone)

TAILINGS

Area, Volume, Capacity of Sand Tailings

Area, Volume, Capacity of Slime Tailings

} Blended in one  
 impoundment

Present Area: 0.43 square kilometers

Present Volume:  $1.8 \times 10^6$  cubic meters

Present Capacity:  $2.2 \times 10^6$  metric tons

} Average grade  
 0.239

Future Additional Area: 0.11 square kilometers

Future Additional Volume:  $1.2 \times 10^6$  cubic meters

Future Additional Capacity:  $1.5 \times 10^6$  metric tons

} Average grade  
 0.153

Operating Time for Each Grade:

Present - 20 years at 0.239  
 Additional - 10 years at 0.153

Fraction of  $U_{238}$ ,  $Ra_{226}$ ,  $Th_{230}$ , and  $Pb_{210}$  to Tailings  
for each Particular Grade:

$U_{238}$ : 7%       $Th_{230}$ : 95%       $Ra_{226}$ : 99.8%       $Pb_{210}$ : 99.8%

From NUREG-0511 Appendix G-1, page G-6

Tailings Density: 1.78 grams per cubic centimeter

From actual measurements taken from test trenches dug in tailings area.

Drying Time Prior to Reclamation: 3 years

This is an estimate based on verbal communications with NRC staff.

Efficiency of Controls for Fugitive Dusting:

Present - 97%  
 Future - 99%

At the present, 97% of the abandoned dry tailings are covered with wood chips to a depth of two feet. Active tails area of 46 acres is kept moist by movement of tailings discharge lines and the solution pond.

In the future the entire active tailings will be under water and all the inactive tailings will be stabilized.

Tailings Activity:  
(slimes)

U: 28 pCi/g  
 $Ra_{226}$ : 200  $\pm$  80 pCi/g  
 $Th_{230}$ : 395  $\pm$  125 "  
 $Pb_{210}$ : 440  $\pm$  10 "

From actual assay determinations - Eberline Instrument Corporation.

Tailings Activity:  
(sand)  
 U: 28 pCi/g  
 $Ra_{226}$ : 110  $\pm$  30 "  
 $Th_{230}$ : 105  $\pm$  30 "  
 $Pb_{210}$ : 166  $\pm$  10 "

From actual assay determinations - Eberline Instrument Corporation.

Tailings Activity:

(solution)	U:	1085		pCi/l
	Ra <sub>226</sub> :	250,000	± 60,000	"
	Th <sub>230</sub> :	285	± 80	"
	Pb <sub>210</sub> :	15,000	± 1000	"

From actual assay determinations - Eberline Instrument Corporation.

Total Tailings Area:

Present: 530 square meters  
 Future: 640 square meters

From survey data.

Tailings Pond (Solution) Area:

Present: 40 square meters  
 Future: 110 square meters

From survey data.

Tailings Impoundment Depth (final year):

Present: 7.7 meters  
 Future: 21.7 meters

Tailings Density: 1.78 g/cubic meter

From actual measurement taken from test trenches dug in tailings area.

Seepage Rate from Tailings Impoundment:

Present: 159 gallons per minute  
 Future: -0-

Seepage calculated from inflow measurements. Tailings entrainment and evaporation estimates.

Future pond will be lined with hypalon.

Fraction U, Th<sub>230</sub>, Ra<sub>226</sub>, and Pb<sub>210</sub> to tailings:

U: 7%  
 Th<sub>230</sub>: 95%  
 Ra<sub>226</sub>: 99.8%  
 Pb<sub>210</sub>: 99.8%

From NUREG-0511 Appendix G-1, page G-6.

Locations of sources & receptors

All locations given in terms of  
 x kilometers east of the yellowcake dryer stack  
 y kilometers north of the yellowcake dryer stack  
 z meters elevation from the base of the yellowcake dryer stack  
 (NOTE: Locations to the south and/or west shall be denoted by  
 a negative value.)

(Data from maps prepared from aerial photography)

<u>Sources</u>	<u>(km) east</u>	<u>(km) north</u>	<u>(m) elevation</u>
1. Yellowcake dryer	0	0	-20
2. Grinder(s)	0	0	-3
3. Crushers	.08	.07	-3
4. Ore Pad	.18	0	-4
5. Fine Ore Blending	.08	.06	-2
6. Tailings pond no. 1 (mid point)	-.55	-.55	-2
7. Tailings pond no. 2 (mid Point)	-.97	-.79	-10
8. Other sources	--	--	--
<u>Extra Receptors</u>			
1. Nearest Resident	.40	-.55	3
2. Nearest Resident in Prevailing wind direction	1.3	.3	1
3. Ranch	1.8	1.5	6
4. Farm	1.8	1.5	6
5. Orchard	1.8	1.5	6
6. Grazing location 1	-2.1	0	6
7. Grazing location 2	0	-2.1	42
8. Garden	.42	-.18	0
9. Town 1	2.3	0	12
10. Town 2	6.7	16.7	145
11. City 1	33.3	-13.3	140
12. Other nearby residents indust- rial (or recreational facilities)	.15	.63	-18
13. Site Boundaries			
N	0	.30	-3
S	0	1.0	7
E	.34	0	0
W	-1.22	0	-6
NE	.34	.24	-3
SW	-1.22	-1.0	-9
SE	.34	-1.0	9
NW	-1.22	0	-6

LAND USE & GRAZING OF CATTLE

Fraction of year spent grazing locally: 67%

Fraction of feed which is pasture graze while grazing: 100%

Fraction of stored feed which is grown locally: 60%

Acreage required to graze one animal unit (450 kg) for one month (AUM): 0.4 ha

All the above are data from local extension agent.

DEMOGRAPHY

The information required to provide the chart was obtained from:

1. State of Washington, Office of Financial Management Population, Enrollment and Economic Studies Division.  
"State of Washington" Population Trends, (1978)
2. Associated Taxpayers of Idaho
3. Spokane Tribe, Planning Department

DAWN MINING COMPANY  
POPULATION DATA

KILOMETERS	N 0.0	NNE 22.5	NE 45.0	ENE 67.5	E 90.0	ESE 112.5	SE 135.0	SSE 157.5	S 180.0	SSW 202.5	SW 225.0	WSW 247.5	W 270.0	WNW 292.5	NW 315.0	NNW 337.5	Total
0.0 0.1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
0.1 0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	7	0	7
0.5 1.0	0	0	0	0	0	0	5	5	5	0	0	0	0	0	0	0	15
1.0 2.0	3	3	10	10	3	6	5	5	10	5	5	0	0	5	10	10	90
2.0 3.0	5	3	15	15	5	10	10	10	10	10	5	5	10	5	10	5	133
3.0 4.0	5	10	15	20	5	25	15	15	20	10	5	5	10	5	5	5	175
4.0 5.0	5	15	15	15	5	30	20	20	20	10	5	5	15	10	10	5	205
5.0 10.0	50	50	30	25	50	50	30	30	20	50	15	15	20	10	10	10	465
10.0 20.0	50	100	50	200	100	50	50	30	50	50	20	50	420	50	20	20	1,310
20.0 30.0	100	265	50	925	925	1,200	200	50	515	50	20	50	50	20	35	10	2,465
30.0 40.0	50	50	50	300	6,104	9,104	14,306	13,224	150	150	50	20	50	30	150	10	43,798
40.0 50.0	2,111	10	10	300	3,106	34,476	176,700	7,580	150	150	1,600	50	25	20	10	10	226,308
50.0 60.0	100	10	10	300	300	87,910	9,799	7,110	150	50	200	360	25	10	10	10	106,354
60.0 70.0	100	10	355	2,140	100	3,000	1,000	247	150	30	520	150	100	10	10	10	7,932
70.0 80.0	1,930	10	10	1,800	2,000	2,705	620	200	550	30	50	1,110	200	10	10	10	14,245
	1,509	536	620	6,050	12,703	138,566	202,760	28,526	1,800	595	2,495	1,820	925	185	297	115	405,502

RM  
3/26/80

ATMOSPHERIC DATA

The only detailed data available was the NOAA, Environmental Data and Information Center information on Spokane, WA (25 miles to S.E.). Also included is U.S. Department of Commerce information on Chewelah, WA (35 miles to N.E.). Unfortunately no data is available by stability classes.

# Local Climatological Data

Annual Summary With Comparative Data

1978



## SPOKANE, WASHINGTON

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### Narrative Climatological Summary

Spokane lies on the eastern edge of the broad Columbia Basin area of Washington which is bounded by the Cascade Range on the west and the Rocky Mountains on the east. The elevations in eastern Washington vary from less than 400 feet above sea level near Pasco where the Columbia River flows out of Washington to over 5,000 feet in the mountain areas of the extreme eastern edge of the State. Spokane is located on the upper plateau area where the long gradual slope from the Columbia River meets the sharp rise of the Rocky Mountain Ranges.

Much of the urban area of Spokane lies along both sides of the Spokane River at an elevation of approximately 2,000 feet, but the residential areas have spread to the crests of the plateaus on either side of the river with elevations up to 2,500 feet above sea level. Spokane International Airport is situated on the plateau area six miles west-southwest and some 400 feet higher than the downtown business district.

Spokane's climate combines some of the characteristics of damp coastal type weather and arid interior conditions. Most of the air masses which reach Spokane are brought in by the prevailing westerly and southwesterly circulations. Frequently much of the moisture in the storms that move eastward and southeastward from the Gulf of Alaska and the eastern Pacific Ocean is precipitated out as the storms are lifted across the Coast and Cascade Ranges. Annual precipitation totals in the Spokane area are generally less than twenty inches and less than 50 percent of the amounts received west of the Cascades. However, the precipitation and total cloudiness in the Spokane vicinity is greater than that of the desert areas of south-central Washington. The lifting action of the air masses as they move up the east slope of the Columbia Basin frequently produces the cooling and condensation necessary for formation of clouds and precipitation.

Infrequently the Spokane area comes under the influence of dry continental air masses from the north or east. On occasions when these air masses penetrate into eastern Washington the result is high temperatures and very low humidity in the summer and sub-zero temperatures in the winter. In the winter most of the severe arctic outbursts of cold air move southward on the east side of the Continental Divide and do not affect Spokane.

In general, Spokane weather has the characteristics of a mild, arid climate during the summer months and a cold, coastal type in the winter. Approximately 70 percent of the total annual precipitation falls between the first of October and the end of March and about half of that falls as snow. The growing season usually extends over nearly six months from mid-April to mid-October. Irrigation is required for all crops except dry-land type grains. The summer weather is ideal for full enjoyment of the many mountain and lake recreational areas in the immediate vicinity. Winter weather includes many cloudy or foggy days and below freezing temperatures with occasional snowfall of several inches in depth. Sub-zero temperatures and traffic-stopping snowfalls are infrequent. The nearby winter sports areas have a season of four to five months with plenty of facilities for skiing and other winter outdoor activities.

noaa

NATIONAL OCEANIC AND  
ATMOSPHERIC ADMINISTRATION

ENVIRONMENTAL DATA AND  
INFORMATION SERVICE

NATIONAL CLIMATIC CENTER  
ASHEVILLE, N.C.

U.S. DEPARTMENT OF COMMERCE, WEATHER BUREAU IN COOPERATION WITH THE WASHINGTON STATE DEPARTMENT OF COMMERCE AND ECONOMIC DEVELOPMENT  
CLIMATOGRAPHY OF THE UNITED STATES 70-43

CLIMATOLOGICAL SUMMARY

STATION: SPOKANE, WASH.  
Spokane International Airport

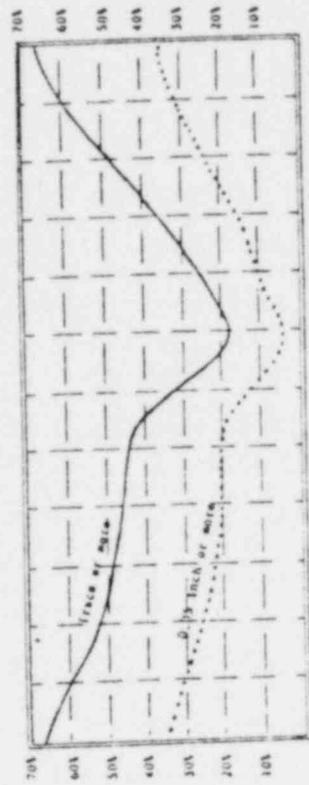
LATITUDE 47° 37' N  
LONGITUDE 117° 31' W  
ELEVATION 2853 Ft.

NORMALS, MEANS, AND EXTREMES

Month	Temperature				Precipitation				Snow, Sleet				Relative humidity			Wind				Mean number of days															
	Normal		Extreme		Year		Year		Year		Year		Year		Year		Year		Year		Year		Year												
	Daily maximum	Daily minimum	Monthly	Record	Record	Lowest	High	Maximum	Minimum	Year	Maximum	Minimum	Year	Maximum	Minimum	Year	Maximum	Minimum	Year	Maximum	Minimum	Year	Maximum	Minimum											
J	37.5	37.2	47.3	102	1940	-24	1950	67.2	1951	109.7	2.43	1951	1.21	1952	1.00	1951	88	84	87	8.4	36	51	58	1954	22	8.6	2	4	25	16	5	0	12	7	1
F	37.5	37.2	47.3	102	1940	-24	1950	67.2	1951	109.7	2.43	1951	1.21	1952	1.00	1951	88	84	87	8.4	36	51	58	1954	22	8.6	2	4	25	16	5	0	12	7	1
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B	37.5	37.2	47.3	102	1940	-24	1950	67.2	1951	109.7	2.43	1951	1.21	1952	1.00	1951	88	84	87	8.4	36	51	58	1954	22	8.6	2	4	25	16	5	0	12	7	1
A	37.5	37.2	47.3	102	1940	-24	1950	67.2	1951	109.7	2.43	1951	1.21	1952	1.00	1951	88	84	87	8.4	36	51	58	1954	22	8.6	2	4	25	16	5	0	12	7	1
S	37.5	37.2	47.3	102	1940	-24	1950	67.2	1951	109.7	2.43	1951	1.21	1952	1.00	1951	88	84	87	8.4	36	51	58	1954	22	8.6	2	4	25	16	5	0	12	7	1
O	37.5	37.2	47.3	102	1940	-24	1950	67.2	1951	109.7	2.43	1951	1.21	1952	1.00	1951	88	84	87	8.4	36	51	58	1954	22	8.6	2	4	25	16	5	0	12	7	1
N	37.5	37.2	47.3	102	1940	-24	1950	67.2	1951	109.7	2.43	1951	1.21	1952	1.00	1951	88	84	87	8.4	36	51	58	1954	22	8.6	2	4	25	16	5	0	12	7	1
D	37.5	37.2	47.3	102	1940	-24	1950	67.2	1951	109.7	2.43	1951	1.21	1952	1.00	1951	88	84	87	8.4	36	51	58	1954	22	8.6	2	4	25	16	5	0	12	7	1
C	37.5	37.2	47.3	102	1940	-24	1950	67.2	1951	109.7	2.43	1951	1.21	1952	1.00	1951	88	84	87	8.4	36	51	58	1954	22	8.6	2	4	25	16	5	0	12	7	1
B	37.5	37.2	47.3	102	1940	-24	1950	67.2	1951	109.7	2.43	1951	1.21	1952	1.00	1951	88	84	87	8.4	36	51	58	1954	22	8.6	2	4	25	16	5	0	12	7	1
A	37.5	37.2	47.3	102	1940	-24	1950	67.2	1951	109.7	2.43	1951	1.21	1952	1.00	1951	88	84	87	8.4	36	51	58	1954	22	8.6	2	4	25	16	5	0	12	7	1
S	37.5	37.2	47.3	102	1940	-24	1950	67.2	1951	109.7	2.43	1951	1.21	1952	1.00	1951	88	84	87	8.4	36	51	58	1954	22	8.6	2	4	25	16	5	0	12	7	1
O	37.5	37.2	47.3	102	1940	-24	1950	67.2	1951	109.7	2.43	1951	1.21	1952	1.00	1951	88	84	87	8.4	36	51	58	1954	22	8.6	2	4	25	16	5	0	12	7	1
N	37.5	37.2	47.3	102	1940	-24	1950	67.2	1951	109.7	2.43	1951	1.21	1952	1.00	1951	88	84	87	8.4	36	51	58	1954	22	8.6	2	4	25	16	5	0	12	7	1
D	37.5	37.2	47.3	102	1940	-24	1950	67.2	1951	109.7	2.43	1951	1.21	1952	1.00	1951	88	84	87	8.4	36	51	58	1954	22	8.6	2	4	25	16	5	0	12	7	1
C	37.5	37.2	47.3	102	1940	-24	1950	67.2	1951	109.7	2.43	1951	1.21	1952	1.00	1951	88	84	87	8.4	36	51	58	1954	22	8.6	2	4	25	16	5	0	12	7	1
B	37.5	37.2	47.3	102	1940	-24	1950	67.2	1951	109.7	2.43	1951	1.21	1952	1.00	1951	88	84	87	8.4	36	51	58	1954	22	8.6	2	4	25	16	5	0	12	7	1
A	37.5	37.2	47.3	102	1940	-24	1950	67.2	1951	109.7	2.43	1951	1.21	1952	1.00	1951	88	84	87	8.4	36	51	58	1954	22	8.6	2	4	25	16	5	0	12	7	1
S	37.5	37.2	47.3																																

Year	Jan	Feb	Mar	Apr	May	June	July	Aug	Sept	Oct	Nov	Dec	Ann'l
1911	1.30	.76	1.52	.53	.26	.87	.71	.01	1.05	.82	2.41	3.88	13.61
1912	1.39	.80	1.60	.71	.28	.78	.21	.27	.06	1.14	2.59	2.13	15.85
1913	1.46	.63	1.19	.29	.59	1.16	.17	.68	1.25	2.77	4.00	4.35	14.91
1914	1.16	.71	1.55	.34	.25	.84	.71	.19	.88	3.45	2.01	1.50	13.83
1915	2.51	.71	1.55	.34	.25	.84	.71	.19	.88	3.45	2.01	1.50	13.83
1916	2.06	.59	.78	.92	.06	.77	.68	.96	.05	.96	.90	1.18	10.51
1917	2.78	1.57	.58	.18	.57	2.33	.07	.23	1.64	.28	.08	2.39	12.70
1918	1.94	1.94	1.90	1.33	.21	3.11	.56	.61	.62	.87	3.05	2.76	18.50
1919	1.44	1.90	2.09	.35	.47	.81	.76	.29	.09	.83	.89	1.63	11.07
1920	1.55	2.37	1.20	.61	.30	.71	.40	.04	.23	.95	.78	2.83	11.47
1921	1.09	5.62	2.91	1.60	.44	.36	1.46	.01	2.12	2.47	2.37	2.59	23.50
1922	1.61	.83	.69	.32	3.18	2.55	.09	1.85	1.36	.85	1.93	2.78	17.74
1923	1.24	1.30	.48	.98	3.19	.91	.34	.08	1.12	2.69	1.70	1.70	14.27
1924	1.25	1.15	1.60	1.33	1.19	1.42	.35	.98	.12	3.13	.60	.54	13.66
1925	1.53	1.08	1.31	1.40	.94	1.11	.21	1.02	.58	.45	1.64	1.14	10.45
1926	1.27	.95	2.48	1.12	2.20	1.37	.55	.24	.79	2.41	2.00	2.00	17.36
1927	1.51	1.43	1.09	.98	1.43	1.08	.63	.07	1.76	1.38	3.16	.90	15.42
1928	1.24	.76	1.17	.31	1.98	1.72	.83	1.57	.61	1.07	1.80	1.80	18.56
1929	2.72	2.75	.45	3.08	3.71	2.17	1.29	.44	.66	2.38	3.13	36.07	36.07
1930	1.50	3.08	2.17	.42	.90	.22	.07	.19	1.06	1.52	2.58	1.50	22.91
1931	4.13	1.93	3.75	.43	.72	2.84	.56	.81	.06	4.05	1.99	2.16	33.00
1932	1.16	1.63	1.72	.38	.66	1.04	.37	.40	.47	2.26	1.88	4.35	19.30
1933	2.41	1.35	1.14	.28	.63	2.44	.68	.18	.52	1.11	.80	3.10	13.00
1934	4.56	1.07	1.27	1.48	1.59	.81	1.36	.50	.19	2.00	1.90	17.73	36.07
1935	4.90	1.07	.43	.53	.78	.75	.85	1.25	.55	.77	1.42	1.44	18.26
1936	1.38	1.32	.79	1.83	.67	.80	1.28	.71	1.13	2.84	3.92	3.82	19.78
1937	2.67	1.44	1.28	.81	.59	1.18	.50	1.41	.09	1.67	.54	1.22	12.88
1938	1.34	1.54	1.28	.81	3.74	2.74	.04	.68	2.33	.82	1.93	18.09	36.07
1939	3.55	3.27	.84	3.22	.71	1.63	1.15	.13	.47	.79	3.72	2.93	20.91
1940	4.90	2.01	1.21	.57	2.26	.39	.05	1.24	2.05	1.32	2.20	1.21	19.57
1941	1.05	1.84	2.26	1.53	2.71	.16	.71	.56	.72	.95	4.64	1.37	17.68
1942	1.63	3.94	1.75	.86	1.77	1.64	.37	.30	.17	1.05	1.83	3.91	19.30
1943	1.39	1.72	2.56	1.02	1.65	.78	.29	.63	.80	1.62	3.02	1.44	17.02

PROBABILITY OF PRECIPITATION OCCURRING ON ANY GIVEN DAY AT SPOKANE  
(Based on 77 years of data ending with 1957)



Note: The probability of a trace or more of precipitation occurring on any day is indicated by the solid line. The probability of 0.05 of an inch is indicated by the dotted line.

Year	Jan	Feb	Mar	Apr	May	June	July	Aug	Sept	Oct	Nov	Dec	Ann'l
1911	34.4	34.8	41.8	49.3	60.2	63.9	72.8	71.2	60.6	49.4	33.3	29.7	50.0
1912	26.1	29.7	31.2	50.0	53.6	63.3	72.4	66.2	62.6	42.0	24.9	24.9	48.1
1913	31.8	31.3	40.2	44.4	52.1	64.0	69.1	69.5	61.2	49.2	38.1	38.1	49.7
1914	37.4	39.4	47.2	56.5	61.2	71.4	71.0	70.3	56.8	51.7	39.1	43.6	49.0
1915	31.3	35.6	38.3	45.2	55.8	65.4	70.2	67.4	63.8	47.0	33.1	31.3	48.4
1916	31.8	37.4	38.7	52.2	62.0	69.3	72.8	71.0	59.1	52.7	32.3	33.0	49.0
1917	9.9	28.6	42.2	46.6	53.6	63.3	72.4	66.2	62.6	40.4	24.2	24.2	48.0
1918	31.5	33.6	41.1	49.8	54.8	66.8	75.0	67.8	67.8	51.2	35.1	34.8	50.8
1919	34.6	28.1	41.2	51.6	54.8	68.9	72.4	72.6	62.1	49.5	39.6	37.0	50.7
1920	30.0	35.9	45.3	50.6	62.5	68.3	72.8	70.6	64.6	53.0	32.2	33.8	51.5
1921	32.0	38.4	45.6	51.8	63.0	71.8	68.5	68.5	55.0	47.5	40.2	33.7	50.5
1922	27.6	31.0	39.6	49.8	53.0	65.6	71.2	70.4	61.8	50.8	34.8	31.2	48.8
1923	31.8	33.2	35.8	50.4	57.4	68.6	69.3	68.6	62.6	50.2	37.6	29.2	47.3
1924	30.2	32.5	37.0	47.9	54.8	62.6	69.7	66.8	61.6	54.2	36.8	28.4	48.7
1925	32.4	35.1	37.8	44.7	58.9	60.5	70.9	69.4	56.6	50.8	36.8	29.8	48.5
1926	30.5	35.7	41.1	48.0	57.0	60.5	69.4	68.6	58.8	44.2	34.0	32.6	48.4
1927	24.5	28.0	36.2	46.2	55.6	63.5	70.1	66.7	59.0	50.8	34.8	31.2	48.8
1928	8.5	26.4	34.0	49.2	58.1	65.4	68.6	68.6	61.6	47.3	34.8	21.5	45.5
1929	9.0	29.8	35.7	43.9	53.2	61.0	69.1	70.7	62.0	46.7	36.2	33.6	45.8
1930	27.1	32.2	34.3	48.3	54.5	61.3	71.0	68.3	60.2	45.7	35.7	22.2	46.8
1931	23.5	30.2	38.7	49.8	56.3	63.0	70.1	68.4	63.8	54.5	32.7	30.3	48.1
1932	37.9	35.3	40.0	45.6	52.4	61.2	69.1	68.0	61.1	51.6	40.3	33.2	49.4
1933	26.9	33.1	36.3	43.5	54.4	57.2	67.5	64.5	57.5	46.2	41.5	30.2	46.6
1934	28.9	27.9	31.2	40.6	49.4	62.7	64.4	64.4	59.4	47.1	28.1	26.8	44.6
1935	28.9	22.6	36.1	49.9	58.1	64.9	71.6	71.6	60.7	46.3	32.7	30.7	47.0
1936	15.0	28.7	37.6	48.0	59.3	67.1	67.5	65.6	62.8	45.0	35.6	35.1	46.9
1937	32.0	39.8	34.9	44.9	42.7	65.6	73.0	73.7	58.1	50.2	35.7	32.4	50.7
1938	29.0	30.3	39.2	47.4	50.6	61.7	70.6	64.4	55.1	46.1	31.5	28.8	46.3
1939	20.3	30.6	34.2	45.9	51.2	62.2	75.1	65.1	60.3	48.6	35.2	26.6	46.4
1940	30.3	37.0	39.9	45.1	53.0	66.8	71.9	74.0	55.9	45.7	30.7	28.6	48.0
1941	22.6	32.4	34.6	48.8	50.8	61.1	68.2	65.4	60.7	47.6	37.9	33.1	47.0

PROBABILITY OF 37°, 28°, 24°, 20° AND 18° OCCURRING AS LATE IN THE SPRING OR AS EARLY IN THE FALL AS THE DATES LISTED IN THE FOLLOWING TABLE:

Year	PROBABILITY - SPRING				PROBABILITY - FALL			
	15X	10X	5X	5X	10X	15X	20X	25X
1911	4/17	4/17	4/17	4/17	9/13	9/13	9/13	9/13
1912	4/17	4/17	4/17	4/17	9/13	9/13	9/13	9/13
1913	4/17	4/17	4/17	4/17	9/13	9/13	9/13	9/13
1914	4/17	4/17	4/17	4/17	9/13	9/13	9/13	9/13
1915	4/17	4/17	4/17	4/17	9/13	9/13	9/13	9/13
1916	4/17	4/17	4/17	4/17	9/13	9/13	9/13	9/13
1917	4/17	4/17	4/17	4/17	9/13	9/13	9/13	9/13
1918	4/17	4/17	4/17	4/17	9/13	9/13	9/13	9/13
1919	4/17	4/17	4/17	4/17	9/13	9/13	9/13	9/13
1920	4/17	4/17	4/17	4/17	9/13	9/13	9/13	9/13
1921	4/17	4/17	4/17	4/17	9/13	9/13	9/13	9/13
1922	4/17	4/17	4/17	4/17	9/13	9/13	9/13	9/13
1923	4/17	4/17	4/17	4/17	9/13	9/13	9/13	9/13
1924	4/17	4/17	4/17	4/17	9/13	9/13	9/13	9/13
1925	4/17	4/17	4/17	4/17	9/13	9/13	9/13	9/13
1926	4/17	4/17	4/17	4/17	9/13	9/13	9/13	9/13
1927	4/17	4/17	4/17	4/17	9/13	9/13	9/13	9/13
1928	4/17	4/17	4/17	4/17	9/13	9/13	9/13	9/13
1929	4/17	4/17	4/17	4/17	9/13	9/13	9/13	9/13
1930	4/17	4/17	4/17	4/17	9/13	9/13	9/13	9/13
1931	4/17	4/17	4/17	4/17	9/13	9/13	9/13	9/13
1932	4/17	4/17	4/17	4/17	9/13	9/13	9/13	9/13
1933	4/17	4/17	4/17	4/17	9/13	9/13	9/13	9/13
1934	4/17	4/17	4/17	4/17	9/13	9/13	9/13	9/13
1935	4/17	4/17	4/17	4/17	9/13	9/13	9/13	9/13
1936	4/17	4/17	4/17	4/17	9/13	9/13	9/13	9/13
1937	4/17	4/17	4/17	4/17	9/13	9/13	9/13	9/13
1938	4/17	4/17	4/17	4/17	9/13	9/13	9/13	9/13
1939	4/17	4/17	4/17	4/17	9/13	9/13	9/13	9/13
1940	4/17	4/17	4/17	4/17	9/13	9/13	9/13	9/13
1941	4/17	4/17	4/17	4/17	9/13	9/13	9/13	9/13
1942	4/17	4/17	4/17	4/17	9/13	9/13	9/13	9/13

In the above table, the 50X point is the same as the average for each freeze category. From a statistical viewpoint based on past data, the probabilities could be considered as follows when converted into the number of occurrences to expect in a 40-year period.

- 15X - 30 years in 40
- 10X - 10 years in 40
- 5X - 4 years in 40

More detailed local monthly and annual climatological data summaries are available from the U.S. Weather Bureau Office, Spokane, Wash.

U.S. DEPARTMENT OF COMMERCE, WEATHER BUREAU IN COOPERATION WITH  
THE WASHINGTON STATE DEPARTMENT OF COMMERCE AND ECONOMIC DEVELOPMENT  
CLIMATOGRAPHY OF THE UNITED STATES 20-45

LATITUDE 48° 15'  
LONGITUDE 117° 45'  
ELEV. 1630 FT.

CLIMATOLOGICAL SUMMARY

STATION CHEWELAI, WASH.

MEANS AND EXTREMES FOR PERIOD 1931-1960

Month	Temperature (°F)								Mean degree days	Precipitation Totals (inches)						Mean number of days								
	Means			Extremes						Mean	Greatest daily	Year	Snow, Sleet				Precip. 10 inch or more	Temperature		Month				
	Daily maximum	Daily minimum	Monthly	Record highest	Year	Record lowest	Year	Mean					Maximum monthly	Year	Greatest daily	Year		90° and above	32° and below		32° and below	0° and below	Max.	Min.
	(a)	(a)	(a)	(a)	(a)	(a)	(a)	(a)					(a)	(a)	(a)	(a)		(a)	(a)		(a)	(a)	(a)	(a)
JAN	31.7	15.0	23.5	55	1953	-38	1950	1293	2.52	1.40	1934	14.7	30.0	1937	9.0	1933	30	30	10	20	30	JAN		
FEB	38.8	18.1	28.5	61	1958	-38	1933	1022	1.83	1.24	1958	9.4	30.5	1937	10.5	1937	6	0	14	20	30	FEB		
MAR	49.4	27.1	38.2	74	1940	-12	1951	831	-1.70	1.44	1945	2.3	14.0	1951	5.0	1956	5	0	5	25	30	MAR		
APR	61.7	32.6	47.2	89	1934	12	1936	534	1.29	1.15	1932	1.1	2.3	1945	2.5	1945	4	0	0	14	0	APR		
MAY	71.3	39.2	55.2	96	1954	16	1954	313	1.67	1.29	1957	1.1	2.3	1945	2.5	1945	4	0	0	5	0	MAY		
JUN	76.0	44.6	60.7	98	1955	26	1952	150	1.58	1.19	1936	1.1	2.3	1945	2.5	1945	5	0	0	5	0	JUN		
JUL	87.3	45.0	66.6	107	1941	32	1960	50	.84	1.70	1955	1.1	2.3	1945	2.5	1945	5	0	0	5	0	JUL		
AUG	86.1	42.4	64.4	103	1958	28	1937	71	.59	1.11	1959	1.1	2.3	1945	2.5	1945	5	0	0	5	0	AUG		
SEP	76.9	37.6	57.3	101	1938	16	1934	252	1.06	1.56	1940	1.1	2.3	1945	2.5	1945	5	0	0	5	0	SEP		
OCT	61.7	31.7	46.7	88	1945	2	1935	567	1.85	1.53	1938	1.1	2.3	1945	2.5	1945	5	0	0	5	0	OCT		
NOV	42.6	26.6	34.6	69	1949	-15	1955	912	2.34	1.38	1941	1.1	2.3	1945	2.5	1945	5	0	0	5	0	NOV		
DEC	34.9	21.0	28.4	58	1956	-27	1961	1135	2.73	1.23	1951	1.1	2.3	1945	2.5	1945	5	0	0	5	0	DEC		
Year	50.9	31.9	45.9	107	1941	-38	1950	7130	19.82	1.56	1940	41.5	39.5	1937	10.5	1937	61	30	31	178	12	Year		

(a) Average length of record, years.

T Trace, an amount too small to measure.

\*\* Base 65°F

+ Also on earlier dates, months, or years.

\* Less than one half

NARRATIVE CLIMATOLOGICAL SUMMARY

Chewelai is located in the northeastern section of the State and near the southern side of Stevens County. The city is in the Colville River valley. Within 5 to 10 miles of the river, north-south ranges of mountains reach elevations of 4,000 to 6,000 feet. The most important agricultural activities are the raising of livestock and the growing of hay and small grain crops. The higher elevations are State and National forest lands. Deposits of copper, silver and other minerals are found in the mountains. The Buckcherry Mountains on the west flank of the valley contain one of the largest magnesite deposits in the United States. A magnesite processing plant is located near the city. Winter ski areas are being developed along some of the mountain slopes.

Summers are warm, dry and sunny and winters are rather cold with considerable cloudiness. Some of the factors influencing the climate are terrain, distance and direction from the ocean and the prevailing westerly winds above the summits of the mountains. The Rocky Mountains protect this area from the more severe winter storms moving southward across Canada, however, the north-south valleys between ranges of mountains descending into British Columbia permit some of the cold air to reach the inland basin of eastern Washington. In a westerly direction, the Cascade Mountains form a barrier to the easterly movement of moist air from over the ocean.

On a typical summer's day, afternoon temperature is in the 80's with nighttime reading in the 40's. In midsummer, maximum temperatures exceed 90° on one day out of three, reaching 100° on a few afternoons. Even on the warmest days, temperatures drop rather quickly after sunset. The growing season is comparatively short and frost has occurred in mid-summer months. The last freezing temperature in the spring usually occurs after the first of June and the first in the fall may occur during the latter half of August.

During the winter season, afternoon temperatures are near freezing and minimum temperatures range from 10° to 20° above zero. Maximum temperatures were below freezing on 60 days in one of the coldest winters and on only 13 days in one of the warmer winters. Minimum temperatures are below freezing on almost every night from the latter half of October through March. Minimum temperatures can be expected

to drop to -14° or lower on at least 4 nights in 2 out of 10 winters. During one of the coldest winters in recent years, 1949-50, minimum temperatures were below zero on 24 nights, -10° on 20 nights, -20° on 12 nights and 30° on 6 nights. The coldest weather generally occurs when cold air from Canada or east of the Rocky Mountains reaches this section of the State. During these cold outbreaks, the sky is frequently clear and the ground is covered with snow, thus a large amount of heat is lost by radiation at night.

Precipitation is light in summer, increasing in the fall, reaching a peak in winter, then decreasing in the spring with a slight increase in May and June followed by a sharp drop in July. Annual precipitation has ranged from 13 to 27 inches. During August, the driest month, the total precipitation is less than .01 inch in 1 summer out of 10; also, the total precipitation is more than 2 inches in 1 summer out of 10. Several thunderstorms and a few hail storms occur each summer.

Most of the precipitation between the latter half of November and the first of March falls as snow. In the higher elevations, snow can be expected after the middle of October and in the lower valleys before the first of December. A snow cover remains on the ground most of the time between the middle of December and the first of March. Snow reaches a depth of 15 to 20 inches almost every winter and 20 to 30 inches in the heavier snowfall seasons. In the higher elevations, snow can be expected to remain on the ground from the last of October until May or June. The few snow survey reports available for elevations above 4,000 or 5,000 feet indicate 6 to 8 feet of snow on the ground the first of April and 4 to 5 feet the first of May.

During the winter season, the loss of heat by radiation at night and moist air crossing the Cascades results in considerable cloudiness and fog. The number of clear or only partly cloudy days each month increases from approximately 6 in winter to 14 in spring and fall and to 25 in midsummer.

In this section of the State, the relative humidity in winter ranges from 75% in the afternoon to 90% at night, and in summer from 30% in the afternoon to 60% at night.

Carl L. Phillips  
St. Climatologist  
U.S. Weather Bureau  
Seattle, Washington

Total Precipitation (Inches)

Year	Jan.	Feb.	Mar.	Apr.	May	June	July	Aug.	Sept.	Oct.	Nov.	Dec.	Ann'l
1931	2.62	1.58	2.22	.48	.37	2.52	.19	T	1.71	1.99	3.19	5.03	21.90
1932	2.27	.73	3.21	2.95	2.61	.71	.31	.18	.32	1.54	3.18	3.35	21.31
1933	2.78	1.60	2.85	.38	1.25	.40	.33	.20	2.42	2.17	.87	6.59	21.64
1934	4.05	.75	1.34	.74	.86	.56	.36	.46	.60	3.52	3.35	2.91	19.10
1935	3.78	1.25	1.18	.24	1.07	.65	1.54	.48	.55	1.58	1.50	2.23	16.95
1936	3.42	1.17	.20	.58	1.15	2.36	.23	T	1.39	.39	.07	1.76	12.72
1937	2.76	3.12	1.79	2.78	.07	4.58	.88	.17	1.06	1.16	5.43	3.38	26.68
1938	2.79	3.60	3.20	.62	.48	.59	.03	.31	.67	2.47	1.22	1.99	17.97
1939	2.91	1.53	1.07	.54	.77	2.49	.22	T	.21	1.09	.63	5.03	16.49
1940	1.30	4.65	2.71	1.97	.63	.44	.24	.10	2.83	4.02	2.02	2.57	23.48
1941	2.76	.80	1.17	.72	4.34	1.40	.66	2.59	2.89	.77	2.62	4.63	24.65
1942	1.10	1.10	.50	1.03	3.35	1.67	1.27	.06	.10	.84	3.16	2.20	16.33
1943	.97	1.21	1.74	1.16	.96	1.18	.24	.80	.08	3.78	.73	1.04	14.04
1944	1.68	1.24	.38	1.90	.98	1.48	.52	.12	.67	.38	2.67	.97	13.09
1945	1.80	1.99	4.35	.75	2.44	1.27	T	.45	1.89	1.17	3.85	2.58	22.53
1946	2.01	2.45	1.38	1.52	.63	1.58	.10	.12	1.44	1.17	3.10	1.15	17.25
1947	1.86	1.67	.58	.97	.89	2.58	.73	.57	2.04	5.08	1.23	1.67	20.00
1948	2.53	2.46	.14	2.52	4.82	3.89	1.50	.79	.94	.73	3.51	2.38	26.10
1949	.89	2.18	2.11	.64	.79	.64	.19	.19	.93	1.48	1.91	1.21	13.26
1950	3.04	2.26	3.20	.59	.53	1.50	1.24	.32	.16	4.15	2.53	3.16	22.59
1951	3.01	1.53	1.89	.52	.65	.79	.31	.71	.55	4.14	2.72	5.02	32.95
1952	2.77	1.19	.90	.33	.71	2.33	.25	.66	.45	.44	.60	3.89	14.95
1953	3.88	1.09	2.17	2.95	1.82	2.09	.70	2.02	.18	.64	2.12	7.07	29.58
1954	3.92	2.06	1.19	1.12	1.96	1.47	1.96	1.97	1.96	.24	2.07	1.67	19.70
1955	1.60	.88	.84	3.82	1.40	2.21	3.72	0	1.50	2.44	2.19	4.48	25.08
1956	3.15	7.08	1.33	.52	1.17	1.16	1.45	1.27	.14	1.64	.49	1.05	15.78
1957	1.55	1.72	2.13	1.09	5.09	1.56	.28	.54	1.33	2.50	1.27	2.60	21.57
1958	3.31	4.17	1.89	3.47	.53	1.63	1.78	.38	.80	.87	3.51	2.68	24.37
1959	4.90	1.74	.80	.62	4.35	.76	.12	1.37	2.35	1.77	2.41	2.33	22.99
1960	1.79	1.43	2.89	2.02	3.29	.38	.01	.92	.75	1.31	5.42	.77	20.96
1961	1.24	3.58	1.19	1.11	3.41	.90	.80	.25	.46	1.92	1.86	3.95	20.67
1962	1.38	1.20	2.01	.93	2.26	.58	.03	.70	1.53	2.56	2.52	2.54	18.24
1963	.51	2.01	2.05	2.15	1.76	1.18	.71	.85	1.02	.73	3.36	1.59	17.72

Average Temperature (°F)

Year	Jan.	Feb.	Mar.	Apr.	May	June	July	Aug.	Sept.	Oct.	Nov.	Dec.	Ann'l
1931	31.2	31.2	41.2	46.6	57.6	61.2	67.2	64.0	56.3	45.6	31.7	25.7	39.7
1932	22.5	25.2	36.2	47.4	53.8	62.6	63.2	64.0	53.8	45.4	38.3	22.4	34.7
1933	26.5	17.8	37.0	45.2	50.5	59.5	64.4	64.6	53.0	46.8	37.2	35.3	33.5
1934	32.6	36.2	43.2	52.8	58.4	60.7	65.6	65.0	53.2	47.0	41.7	29.6	44.7
1935	24.4	29.8	37.2	43.4	52.1	57.6	65.2	62.6	57.6	44.1	31.2	30.1	41.6
1936	28.6	13.3	37.4	48.4	57.8	62.0	66.0	63.9	55.4	48.2	30.0	30.8	45.2
1937	4.6	23.8	39.6	45.8	54.4	59.2	67.4	61.2	57.6	49.0	38.2	30.4	44.3
1938	28.8	31.8	36.6	-	64.3	68.6	62.2	63.6	48.9	-	-	-	-
1939	30.3	23.6	38.4	48.5	54.8	56.4	66.0	65.8	58.2	46.2	35.4	33.0	41.4
1940	26.8	32.6	43.4	49.2	57.6	64.7	70.0	65.3	62.5	50.6	30.8	29.5	48.6
1941	28.6	35.6	44.2	50.6	54.8	61.8	70.6	65.5	54.2	45.5	37.8	31.0	48.1
1942	21.6	31.4	38.7	43.8	52.9	58.4	68.6	67.5	58.3	46.5	32.3	28.4	46.1
1943	18.2	29.3	34.3	49.6	52.0	58.3	66.9	63.2	58.4	46.8	36.6	27.2	45.1
1944	22.8	28.4	36.6	47.8	56.2	62.0	67.2	64.8	59.0	50.4	36.0	26.0	46.4
1945	30.0	33.4	38.3	43.4	56.6	59.8	67.6	65.9	54.8	48.2	33.5	27.6	46.7
1946	25.2	28.1	40.0	48.0	57.1	59.3	66.5	65.4	56.0	42.0	32.6	29.6	45.4
1947	21.4	34.2	42.0	47.0	52.6	60.0	66.1	63.4	57.4	49.1	34.2	30.2	46.9
1948	22.4	27.8	37.2	44.9	55.6	65.8	63.9	64.5	56.9	45.0	34.4	17.2	44.6
1949	-0.4	19.2	38.2	48.9	58.3	60.3	65.8	64.4	58.9	43.0	40.8	26.3	43.7
1950	5.8	26.1	36.0	44.3	52.6	62.1	67.2	65.7	58.0	45.2	34.2	31.7	44.0
1951	24.4	29.4	37.8	47.4	54.7	59.7	66.8	65.0	57.3	46.7	35.3	19.3	44.9
1952	21.3	28.4	37.3	49.4	56.4	60.8	66.5	65.8	59.5	49.2	31.2	29.6	46.3
1953	36.8	35.9	40.6	46.5	53.4	58.2	65.7	65.1	57.8	48.8	38.8	32.9	47.4
1954	25.0	33.7	37.2	44.6	54.6	57.7	63.9	61.0	56.4	43.7	41.6	29.1	45.8
1955	26.7	26.0	31.5	41.9	51.1	61.7	65.4	62.8	56.8	47.1	28.5	23.9	43.5
1956	26.1	20.8	34.5	49.7	57.6	59.1	67.5	64.5	57.2	45.9	32.1	29.3	45.4
1957	10.7	25.4	38.4	47.6	60.2	62.1	68.0	61.5	59.5	46.3	34.5	32.6	45.3
1958	31.8	40.0	40.6	46.6	61.4	65.6	69.4	69.7	56.5	46.4	31.7	29.5	47.1
1959	26.3	27.3	38.7	47.7	50.5	59.9	66.0	62.3	54.8	45.3	30.2	28.7	44.8
1960	18.7	30.2	37.8	46.8	52.0	60.6	69.4	62.4	57.2	47.6	35.1	27.9	45.5
1961	29.3	36.6	39.9	46.1	54.6	65.8	68.3	69.9	53.2	44.3	29.0	23.7	46.7
1962	17.2	30.1	34.3	48.7	51.3	59.1	64.1	63.3	56.9	47.3	36.6	33.5	45.4
1963	20.8	34.8	40.6	45.5	53.5	61.1	63.9	65.5	61.9	48.2	36.2	24.9	46.4

STATION HISTORY

The first climatological station in this area was established at the residence of C.A. LaVigne located 2 1/2 miles northwest of the Post Office in Cheselan. Mr. LaVigne served as cooperative weather observer from 9/1/1925 to 6/1/1936. The elevation at this location was 1668 feet. The station was moved to the residence of Walter J. Goodman who served as cooperative weather observer from 6/1/1936 to 7/25/1940. During this period, the station was located .8 of a mile northwest of the Post Office and at an elevation of 1668 feet. The climatological station was moved to the present site at the Northwest Lignosite Company located 2 miles south of the Post Office on 7/26/1940. The present elevation of the station is 1635 feet.

PROBABILITY OF 32°, 28°, 24°, 20° AND 16° OCCURRING AS LATE IN THE SPRING OR AS EARLY IN THE FALL AS THE DATES LISTED IN THE FOLLOWING TABLE:

	PROBABILITY - SPRING				PROBABILITY - FALL			
	75%	50%	25%	10%	10%	25%	50%	75%
32°	May 21	Jun 4	Jun 18	Jun 30	Aug 2	Aug 12	Aug 25	Sep 6
28°	Apr 23	May 7	May 21	Jun 1	Aug 28	Sep 7	Sep 20	Oct 2
24°	Mar 26	Apr 9	Apr 22	May 5	Sep 7	Sep 18	Oct 1	Oct 12
20°	Mar 10	Mar 24	Apr 7	Apr 18	Oct 4	Oct 15	Oct 27	Nov 8
16°	Feb 18	Mar 3	Mar 17	Mar 28	Oct 19	Oct 30	Nov 11	Nov 23

In the above table, the 50% point is the same as the average for each freeze category.

From a statistical viewpoint based on past data, the probabilities could be considered as follows when converted into the number of occurrences to expect in a 10-year period:





# STATION LOCATION

OFFICE: WASHINGTON

Location	Occupied from	Occupied to	Miles distance and direction from previous location	Latitude North	Longitude West	Elevation above							Remarks			
						Sea level		Ground								
						Ground at temperature site	Wind instruments	Extreme thermometer	Psychrometer	Telepsychrometer	Tipping bucket rain gage	Weighing rain gage		8" rain gage	Hygrometer	
<b>MEMPHIS</b>																
Truitt-Tinker Building Howard Street near Riverside Avenue	8/4/80	1/1/82		47° 40'	117° 25'	1896	-	18	18				2	Observations began 1/1/81.		
Riverside Avenue and Mill (Wall) Street	1/1/82	11/29/84	Near City Center	47° 40'	117° 25'	1895	-	22	22				32	Office destroyed by fire 11/29/84.		
Drumheller, Riverside Avenue & Ford Street	11/10/84	1/1/87	Near City Center	47° 40'	117° 25'	1894	-	24	24				40			
W.D. Flork, Riverside Avenue near Howard St.	1/1/87	8/4/89	Near City Center	47° 40'	117° 25'	1894	-	37	37				48	Fire destroyed building and all records.		
Franklin Block F. Hayes Avenue and Lincoln Street	8/1/89	9/6/89	Near City Center	47° 40'	117° 25'	1896	-	46	46				35			
Riverside Avenue and Division Street	9/6/89	11/15/89	Near City Center	47° 40'	117° 25'	1925	-	36	36				35			
110-112 Riverside Avenue	11/15/89	11/7/90	Near City Center	47° 40'	117° 25'	225	-	41	41				15			
Walters Building Strague Avenue and Stevens Street	11/7/90	6/1/92	Near City Center	47° 40'	117° 25'	1902	109	101	100			492	92	a - Added 7/14/91.		
Jackson Building 700 Riverside Avenue	8/1/92	7/1/02	Near City Center	47° 40'	117° 25'	1894	107	100	99			90	90			
Empire State Building 907 Riverside Avenue	7/1/02	1/1/41	Near City Center	47° 40'	117° 25'	1895	110	101	101			94	94			
<b>MEMPHIS</b>																
Felix Field 4-1/2 Miles NE of City Center	5/1/42	1/1/41		47° 40'	117° 20'	1935	42	28	27			25	26	25		
Felix Field	1/1/41	10/8/47	No Change	47° 40'	117° 20'	1935	453	87	86			43	44	43	City and Airport Offices consol- dated at Felix Field 1/1/41. a - 28 feet to 1/1/42. b - 28 feet to 1/1/42. c - 27 feet to 1/1/42. d - 25 feet to 1/1/42. e - 26 feet to 1/1/42. f - 25 feet to 1/1/42.	
Waller Field, 8 miles SW of City Center	10/8/47	8/1/59	10.5 miles SW	47° 37'	117° 31'	2357	34	7	5			3	5	3	Wind instruments at 20 feet until 7/18/57. Anemometer installed at 20 feet center of runway complex, 11/23/57.	
Waller Field	8/1/59	5/17/65	No Change	47° 37'	117° 31'	2356	20	7	5			3	4	3	4	Hygrometer under construction near center of runway complex.
International Airport (Formerly Waller Field)	5/17/65	Present	0.7 mi. NW	47° 38'	117° 32'	2356	20	8	5			5	5	5	4	Hygrometer and wind instruments not moved 5/17/65.

Requests for information concerning other locations and instrumentation should be made to the Director, National Climatic Center, Federal Building, Asheville, NC 28801.

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I certify that this is an official publication of the National Oceanic and Atmospheric Administration, and is compiled from records on file at the National Climatic Center, Asheville, North Carolina 28801.

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NOAA-NCA-ASHEVILLE - 1050

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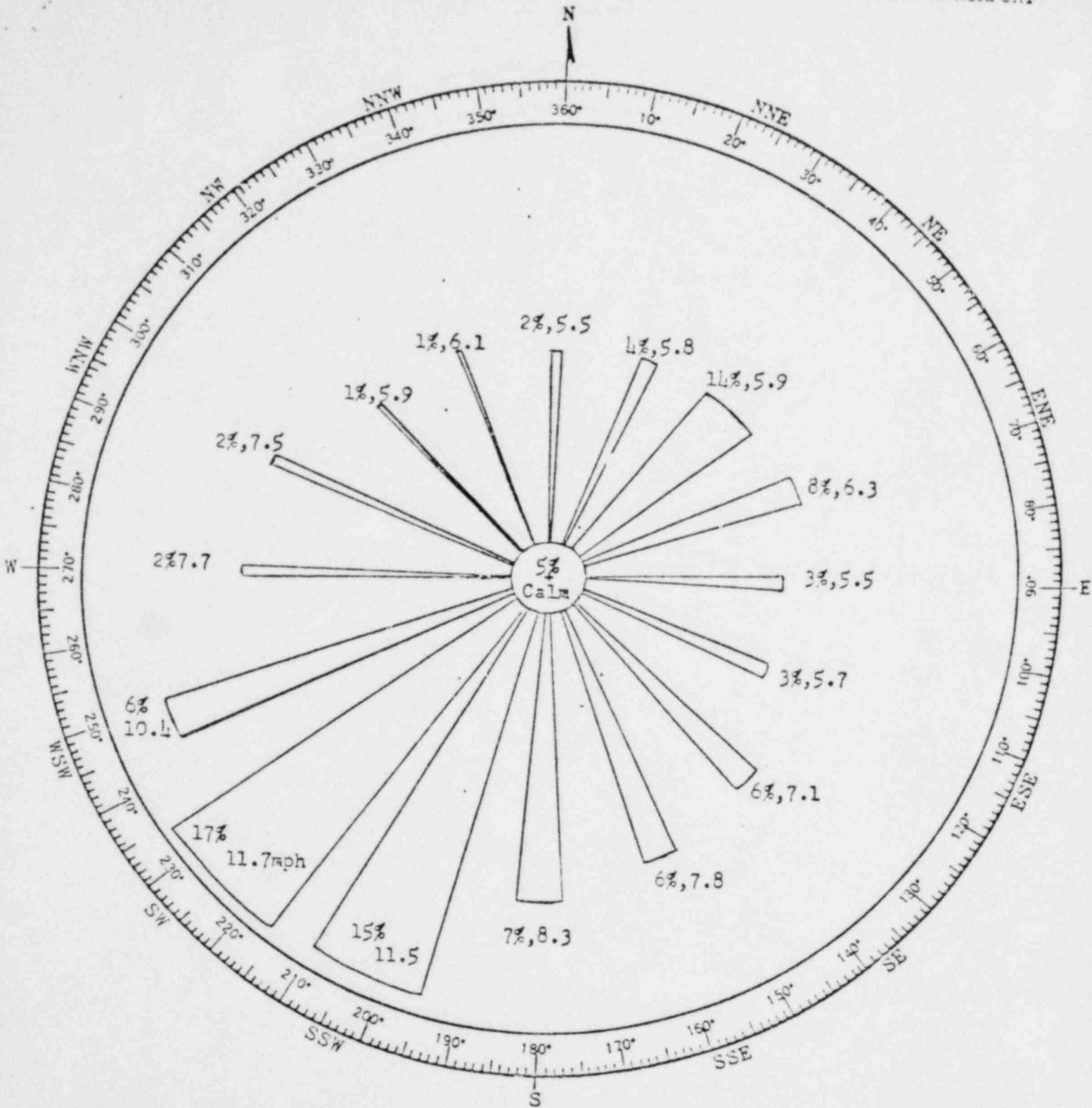
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FIRST CLASS



Percentage frequencies of wind direction (true) and speed (mph) averages. 87,672 hourly observations, 1951-1960. Length of spoke is proportional to speed and width is proportional to frequency.