

Fwd by PWR

JUL 21 1972

Docket No. 50-269

R. C. DeYoung, Assistant Director for Pressurized Water Reactors, L
OCONEE UNIT 1 TECHNICAL SPECIFICATIONS - RADIOACTIVE RELEASES.

Plant name - Oconee

Licensing stage - CL

Docket number - 50-269

Responsible branch - PWR-4

Project leader - I. A. Peltier

Date request received by RA-L - 6/25/72

Requested completion date - timely, prior to 8/30/72

Description of response - Revisions to Oconee Technical Specifications

Review status - Awaiting response from applicant.

The Oconee Technical Specifications are being revised to conform to the versions which incorporate requirements equivalent to proposed Appendix I, 10 CFR Part 50. Specific guidance to Duke Power Company has been supplied in the form of a revised copy of the Maine Yankee Technical Specifications (see attachment #1). A copy of these revised specifications was delivered to Mr. I. A. Peltier on July 11 prior to his meeting with the applicant on July 12.

Subsequent to this meeting Mr. Lionel Lewis of Duke Power called to discuss the following points:

1. Station limit vs. unit limit. They prefer to write limits in terms of the station rather than for a single unit. A single unit limit was written in the guidance because it was not construed to be "as low as practicable" to use a three unit limit when only one unit is operating. This limit will be increased if necessary as the other units come on line.
2. The nearest cow. The nearest cow to Oconee is at the nearest dairy farm which is 4.5 miles west of the site. There had been a closer cow but it was sold last year.³ The applicant calculates a χ/Q at this dairy of 1.22×10^{-7} sec/m³.
3. Iodine release limit. The numerical limit for iodine releases was set equal to the source term for 1 unit (see Radwaste Section for Environmental Statement for Oconee Nuclear Power Station, Units 1, 2, and 3. - Memo dated 3/2/72 from V. Benaroya to J. Kastner). They

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questioned this because they had based their limit on keeping the iodine concentration at the nearest dairy within Appendix I guidelines and, consequently, had arrived at a lower value.

4. Gaseous release limits. They would prefer to write the specification for gaseous release so that low activity gaseous wastes can be released with less than 30 days hold-up time if the hold-up tanks were needed for higher level gaseous wastes. The total release computed on a quarterly basis would be kept within Appendix I guidelines.

Conclusions reached in this discussion were: (1) they will recalculate the iodine release limit, (2) they will rewrite the specification for gaseous waste hold-up time, and (3) they will consider the limit for iodine release based on the single unit source term (no commitment was made).

Follow-up review on these specifications will be provided by RAB through final formulation prior to August 30, 1972.

Original signed by
H. R. Denton

Harold R. Denton, Assistant Director
for Site Safety
Directorate of Licensing

Enclosure:
As stated

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7/19/72 DATE → 7/19/72	7/19/72	7/19/72	

3.16 LIMITS OF LIQUID RELEASES

Applicability: Applies to the controlled release of all liquid waste discharged from the plant which may contain radioactive materials.

Objective: To establish conditions for the release of liquid waste containing radioactive materials and to assure that all such releases are within the concentration limits specified in 10 CFR Part 20.

CPB Control No. 0001
In addition, to ensure that the releases of radioactive material in liquid wastes (above background) to unrestricted areas meet the low as practicable concept, the following liquid release objectives shall apply:

- a. The annual total quantity of radioactive materials in liquid waste, excluding tritium and dissolved gases, shall be less than 5 curies;
- b. The annual average concentration of radioactive materials in liquid waste, prior-to-dilution-in-Bailey-Cove, excluding tritium and dissolved gases, shall not exceed 2×10^{-6} uCi/ml;
- c. The annual average concentration of tritium in liquid waste, prior-to-dilution-in-Bailey-Cove, shall not exceed 5×10^{-6} pCi/ml;
- d. The annual average concentration of dissolved gases in liquid waste, prior-to-dilution-in-Bailey-Cove, shall not exceed 2×10^{-6} pCi/ml.

Specifications: A. Release Quantities and Concentrations of Radioactive Materials in Waste

1. If the unanticipated release of radioactive materials in liquid waste, when averaged over a calendar quarter, is such that these quantities if continued at the same release rates for a year would exceed twice the annual objective, the licensee will:
 - a. make an investigation to identify the cause(s) for such release rates;
 - b. define and initiate a program of action to reduce such release rates to the design levels, and;
 - c. describe these actions in a report to the Commission within 30 days.
2. If the anticipated release of radioactive material in liquid waste, when averaged over a calendar quarter, is such that it exceeds twice the annual objective, the licensee will:
 - a. make an investigation to identify the cause(s) for such release rates;
 - b. define and initiate a program of action to reduce such release rates to the design levels, and;
 - c. describe these actions in a report to the Commission within 30 days.

*Tech Spec 5-7 received
Dec 5, 1980*

val, or any for a year would exceed eight times the annual average, the licensee shall define and implement a program of action to ensure that such release rates are reduced, and shall submit a report to the Commission within 7 days describing the cause for such release rates and the course of action taken to reduce them.

- C. 3. The rate of release of radioactive materials in liquid waste from the plant shall be controlled such that the instantaneous concentration of radioactivity in liquid waste does not exceed the values listed in 10 CFR Part 20, Appendix B, Table II, Column 2.

B. Treatment and Monitoring

1. The equipment installed in the liquid radioactive waste system will be maintained and operated with the intent of keeping releases within the objectives of these Specifications.
2. At least one service water pump shall be in operation when liquid radioactive wastes are being released.
3. Liquid waste discharged from the test tanks shall be continuously monitored during release. The liquid effluent monitor reading shall be compared with the expected reading of each discharge batch. The monitor shall be tested daily and calibrated at refueling intervals. The calibration procedure shall consist of exposing the detector to a referenced calibration source in a controlled, reproducible geometry. The sources and geometry shall be referenced to the original monitor calibration which provides the applicable calibration curves.
4. The effluent control monitor shall be set to alert and automatically close the waste discharge valve such that the requirements of the specification are met. In the event of a limitation in the monitor, the alarm shall sound and automatically close the waste discharge valve.
5. Samples of boric acid shall be continuously monitored, except in refueling periods when the reactor is not operating. Daily grab samples shall be taken.

C. Sampling and Analysis

In addition to the above continuous monitoring, liquid waste shall be sampled on a regular, systematic basis. These samples shall be analyzed by a laboratory acceptable to the Commission. The laboratory shall be required to maintain an association with the Commission's specifications.

basis:

It is expected at the licensee of radioactive materials in liquid waste will kept within the design objective levels and will not exceed the concentration limits specified in 10 CFR Part 20. These levels provide reasonable assurance that the resulting annual exposure to the whole body or any organ of an individual will not exceed 5 millirems per year. At the same time, the licensee is permitted the flexibility of operation, comprising such considerations of health and safety, to assume that the public is provided a dependable source of power under unusual operating conditions which may temporarily result in releases higher than the design objective levels but still within the concentration limits specified in 10 CFR Part 10. It is expected that using this operational flexibility under unusual operating conditions, the licensee shall exert every effort to keep levels of radioactive material in liquid wastes as low as practicable and that annual releases will not exceed a small fraction of the annual average concentration limits specified in 10 CFR Part 20.

The design objectives have been developed taking into account a combination of variables including fuel failures, primary system leakage, primary-to-secondary leakages and the performance of the various waste treatment systems. The actual magnitude of these parameters are as follows:

- a. Maximum expected reactor coolant corrosion product concentrations;
- b. Reactor coolant function product concentration corresponding to 0.1% fuel cladding failures;
- c. Steam generator primary-to-secondary leak rate of 0.01 gpm;
- d. Hydrogenated liquid waste generation rate of 1.75 gpm;
- e. Nonradioactive liquid generation rate of 0.13 gpm;
- f. Secondary-to-primary leak rate of 0.001 gpm due to detector tube leak for monitoring hydrogen activity;
- g. Concentration limits of 10⁻³ for all radioactivities except Cs-137 and Sr-90 which are limited to 10⁻² by iodine evaporators;
- h. Concentration limits of 10⁻³ for Cs, Sr, U, Th and V for calcium hydroxide.

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The application of the above estimates results in the radionuclide discharge concentrations and rates shown in Table 3.16-2. Also given in this table are the radionuclide concentrations in the reactor coolant and the secondary coolant, which are the "source terms" for releases from the primary and secondary systems, respectively. Liquid radioactive-waste is mixed with water in the plenum discharge system prior to release. With four circulating water pumps in operation, the mixed capacity of the system is 400,000 gpm. This is equivalent to a dilution multiple of 2.5×10^{-6} min/gal X the discharge rate in gal/min. Liquid radioactive waste from the waste treatment system is collected and stored in tanks until a quantity sufficient for processing has accumulated. The processed liquid waste is discharged through a recorder controller which provides a measure and control of volume of liquid released. The volume discharged and the analysis of the proportional composite sample provide the basis for reporting the quantity and contamination of activity released.

The operating manual will identify all equipment installed in the liquid waste handling and treatment systems and will specify detailed procedures for operating and maintaining this equipment.

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The low as practicable liquid release objectives expressed in this Specification are based on the guidelines contained in the proposed Appendix I of 10 CFR 50. Since these guidelines have not been adopted as yet, the release objectives of this Specification will be reviewed at the time Appendix I becomes a regulation so as to make this Specification in based upon the guidelines contained therein.

References:

FNAR, Section 9.14, Plume Disposal System

FSIN, Section 11.2.1, Plume Disposal System

Tech Spec Sections 3.6 and 3.7, Exposure and Control of Radionuclides, 10 CFR 50

RADIOACTIVITY MONITORING AND ANALYSISA. Test Tank Releases

Sampling Frequency	Type of Activity Analysis	Sensitivity of Analyte (%)
Each Batch	Cs-137, Sr-87	10 ⁻⁷ uCi/ml
One batch/Month	Ba-133 and Cs-137	10 ⁻⁷ uCi/ml
Weekly Proportional Composite (1)	Am-241, La-140, I-131	10 ⁻⁸ uCi/ml
Monthly Proportional Composite (1)	Cs-137 Emitters	10 ⁻⁹ uCi/ml(2)
	Ba-133	10 ⁻⁹ uCi/ml
	Cs-137	10 ⁻⁷ uCi/ml
Quarterly Proportional Composite (1)	Am-241, Sr-90	10 ⁻⁹ uCi/ml(3)

B. Secondary Pipe Sampling and Analysis (2)

Sampling Frequency	Type of Activity Analysis	Sensitivity of Analyte (%)
Weekly	Cs-137, Sr-87	10 ⁻⁷ uCi/ml
One Sample/Week	Ba-133, Cs-137, I-131	10 ⁻⁷ uCi/ml
Monthly Proportional Composite (4)	Cs-137 Emitters	10 ⁻⁹ uCi/ml(4)
	Ba-133	10 ⁻⁹ uCi/ml
	Cs-137	10 ⁻⁷ uCi/ml
Quarterly Proportional Composite (4)	Am-241, Sr-90	10 ⁻⁹ uCi/ml(5)

NOTES:

- (1) A proportional composite sample is one in which the quantity of each nuclide is proportional to the quantity of all other nuclides in the plant.
- (2) For certain mixtures of gamma emitters, it may not be feasible to measure radiactivities to detect Cs-137. In such a situation, Cs-137 and/or other nuclides are present in the sample at such low concentrations that they do not contribute significantly to the total gamma activity. Under these circumstances, it will be more appropriate to analyze for Cs-137 concentrations of only the Cs-137 fraction of the observed activity, i.e., the fraction which are measurable.

- (3) Secondary plant blowdown and secondary plant leakage are each subject to the sampling and analysis requirements contained in Part A of Table 3.1B-1.
- (4) Since these potential sources of liquid radioactive waste are discharged on a continuous rather than batch basis, the volume of liquid to be used as a basis for obtaining proportional samples from secondary blowdown and leakage is that amount discharged over the period of one week.
- (5) These activity analyses sensitivities are based on the projected capabilities of laboratory instrumentation and techniques to be employed by Maine Yankee. In order to assure that actual Maine Yankee operating experience is utilized, a reevaluation will be performed within 2 years of initial full power operation of the plant to determine whether these sensitivities should be revised.
- (6) One quarterly proportional composite sample will be collected and analyzed for Sr-89 and Sr-90. The proportional inputs to this sample will be from the test tank, secondary blowdown, and secondary leakage facilities.

Table 3.16-2

RADIO-NUCLEIC SUBSTANCES AND DISINTEGRANTS

Reactor Coolant Concentration $6 \text{ M}/\text{ml} \text{ of } \text{H}_2\text{O}_2$	Steam Generator Bleed-off Concentration ($\text{cc}/\text{ml} \text{ at } 70^\circ\text{F}$)	Plant Discharge Concentration (cc/ml)	Fraction of 30 CCP-30 IHM	Experiments Run No.
3-321	2.99-3*	4.22-4	7.20-3	
	3.12-3	6.25-5	1.11-5	
	5.02-3	2.68-4	1.25-2	
	6.25-3	3.57-5	1.32-2	
	8.00-3	5.33-5	1.52-10	
	3.12-4	5.62-7	2.01-32	
	1.62-4	3.77-3	1.62-22	
	3.97-4	4.95-9	2.32-33	
	6.12-5	5.41-9	2.65-15	
	2.50-3	4.70-5	2.27-31	
	1.10-3	1.95-4	1.71-30	
	1.95-4	3.61-7	1.71-32	
	4.02-3	3.00-3	1.81-12	
	6.55-3	7.54-6	1.74-12	
	2.50-2	6.60-5	1.31-10	
	8.37-4	5.92-7	1.75-12	
	6.17-4	2.79-4	1.74-12	
	5.39-3	2.94-5	1.74-10	
	7.17-4	2.10-2	1.73-12	
	2.97-4	2.97-4	1.61-9	
	6.39-6	6.39-6	4.77-11	
	7.00-3	5.00-3	5.76-12	
	5.00-3	5.00-3	5.75-13	
	1.70-3	1.70-3	5.75-31	
	2.00-2	2.00-2	7.00-7	
	1.23-3	1.23-3	8.50-7	
	3.62-2	3.62-2	2.65-10	
			$\sum = 3.62 \times 10^{-9}$	
			$\leq 3.35 \times 10^{-5}$	
				1.07-5
				1.02-7
				2.50-5
				2.50-3

$$1.2, 69-1 = 2.99 \times 10^{-2}$$

$$2, 3, 9$$

$$1.02-7$$

$$1.07-5$$

$$2.50-5$$

3.17 RELEASE OF GASEOUS RADIONUCLIDES

Applicability: Applies to the controlled release of all gaseous waste discharged from the plant which may contain radioactive materials.

Objective: To establish conditions in which gaseous waste containing radioactive materials may be released and to assure that all such releases are within the concentration and dose limits specified in 10 CFR Part 20. In addition, to assure that the releases of gaseous radioactive wastes (above background) to unrestricted areas meet the as low as practicable concept, the following objectives shall apply:

1. Averaged over a yearly interval, the release rate of radioactive isotopes, except I-131 and particulate radionuclides with half lives greater than 8 days, discharged at the plant stack, shall be limited as follows:

$$\sum \frac{Q_i}{(NFC)_i} \leq 800 \text{ m}^3/\text{sec}$$

where Q_i is the annual controlled release rate (Ci/sec) of radioisotope i and $(NFC)_i$ ($\mu\text{ci/cc}$) is defined for radioisotope i in column 1, Table II of Appendix B to 10 CFR 20.

2. Averaged over a yearly interval, the release rate of I-131 and other particulate radionuclides with half lives longer than 8 days, discharged at the plant stack, shall be limited as follows:

$$\sum \frac{Q_i}{(NFC)_i} \leq 5.0 \text{ m}^3/\text{sec}$$

where Q_i and $(NFC)_i$ are as defined above.

Specification: A. RELEASES OF GASEOUS RADIONUCLIDES

1. If the average total rates of release of radioactive materials in gaseous wastes, when averaged over a calendar year, are such that they exceed the applicable release rates for a year would exceed either the annual objectives, the licensee shall:
 - a. take the appropriate action to identify the causes for such rate;
 - b. if necessary, take a prompt self audit to determine if the cause(s) noted in (a) are due to design levies;

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See 720613*

Table 3.17-1

RADIOPACIFIC TESTS & MONITORING AND ANALYSISA. Gas Decay Drum Filtration

Sample Type	Sampling Frequency	Type of Analytical Methods	Sensitivity of Analysis (1)
Gas	Each Drum Balance	Open Circuit	$10^{-5} \mu\text{Ci/cc}$
		Condenser Cell Circuit	$10^{-6} \mu\text{Ci/cc}$ (2)

B. Containment Venting Sampling

Sample Type	Sampling Frequency	Type of Analytical Methods	Sensitivity of Analysis (1)
Gas	Each Vent	Open Circuit	$10^{-5} \mu\text{Ci/cc}$
		Condenser Cell	$10^{-4} \mu\text{Ci/cc}$ (2)

C. Containment Filter Sampling

Sample Type	Sampling Frequency	Type of Analytical Methods	Sensitivity of Analysis (1)
Gas	Weekly	Open Circuit	$10^{-5} \mu\text{Ci/cc}$

The specification describes protection of radioactive gaseous waste holdup and decay during normal operation with several sources involving fuel loading, shutdown and power level. Gaseous de pressurization will affect the radioactive concentration rates considerably. Radon is released from the reactor coolant to the gaseous phase or to air during degassifier treatment of the loadout and drainage water and also during venting of the system. This venting may occasionally be performed to depress the system and to control plant chemistry and/or reduce coolant radioactive radon concentrations to an acceptable value for the protection of plant personnel.

Gaseous waste holdup and decay occurs while it is retained in the reactor coolant system and in the surge drum of the gaseous treatment system. The gaseous waste holdup drums are of sufficient capacity to provide an additional air/water retention period of 60 days during normal operating conditions.

The low level gaseous release objectives expressed in this Specification are based on the guidelines contained in the proposed Appendix I of 10 CFR 50. Since these guidelines have not been adopted yet, the relevant objectives of this Specification will be contained in the final Appendix I because a regulation can not be made until this Specification is based upon the guidelines contained therein.

As written, the low level gaseous release objectives do not apply to the following situations:
1. Normal shutdowns of the reactor system.
2. Normal startups of the reactor system.

As written, the low level gaseous release objectives do not apply to the following situations:
1. Normal shutdowns of the reactor system.
2. Normal startups of the reactor system.

Table 3.17-1

MONITORING CRITICAL VISIT SWEEPING AND ANALYSISA. Gas Decay Drum Releases

Sample Type	Sampling Frequency	Type of Activity Analysis	Sensitivity of Analysis (1)
Gas	Each Drum Release	Cross Gamma	10^{-5} $\mu\text{Ci}/\text{cc}$
		Individual Gamma	
		Tritium	10^{-4} $\mu\text{Ci}/\text{cc}$ (2)

B. Containment Venting Sampling

Sample Type	Sampling Frequency	Type of Activity Analysis	Sensitivity of Analysis (1)
Gas	Each Vent	Cross Gamma	10^{-5} $\mu\text{Ci}/\text{cc}$
		Individual Gamma	
		Tritium	10^{-4} $\mu\text{Ci}/\text{cc}$ (2)
Dehumidified Sample	Each Vent	H-3	10^{-4} $\mu\text{Ci}/\text{cc}$

C. Condenser Air Emission Releases

Sample Type	Sampling Frequency	Type of Activity Analysis	Sensitivity of Analysis (1)
Gas	Monthly	Cross Gamma	10^{-5} $\mu\text{Ci}/\text{cc}$
		Individual Gamma	
		Tritium	10^{-4} $\mu\text{Ci}/\text{cc}$

to the top of 1000 feet above the ground level.

- b. Charcoal filter efficiency of 99% for Iodine on the air exhaust, liquid and gas decay drum systems.

The application of the above estimates result in the radionuclide discharge rates shown in Table 3.17-2.

The noble gas release rate stated in the objectives is based on a Z/Q value from the annual meteorological data. The dispersion factor used, $2.79 \times 10^{10} \text{ m}^3/\text{sec}^2$, is conservative and controls the release rate to a small fraction of 10 CFR Part 20 requirements at the site restricted area boundary (410 microm per year).

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The I-131 and particulate release rate stated in the objectives limits the concentration at the restricted area boundary to less than 1% of the MPC I used in 10 CFR 20. The release rate also controls the average concentrations at nearby commercial dairy farms to much less than 1/100,000 of the 10 CFR 20 requirements.

The minimum one hour release rate limits the dose rate at the site boundary to less than 2 rem/hour even during periods of unfavorable winds (10 m/sec). Adversely stable conditions with $2 \text{ m/sec wind speed}$ occur about 10% of the time.

The maximum capacity in a liquid gas decay drum is specified as 80,400 cubic ft of K-403 equivalent based on a postulated rupture of the drum and all air spaces to escape to the atmosphere. This postulation limits the ambient offsite dose to well below the limit of 10 CFR 100.

The charcoal media section is divided into two sections; carbon dioxide and hydrocarbons. Low volatility, inerted gaseous wastes are first exposed to the charcoal by being fed through a high efficiency filter to the primary vent stack. Hydrocarbon vapors are removed from the stack, then sent through the charcoal media section to the secondary vent stack. The charcoal media section has a total capacity of 1000 cu ft. The charcoal media section is designed to last 10 years. The charcoal media section will be replaced every 10 years due to the degradation of the charcoal media used in the stack. Upon replacement of the charcoal media upon the vent line, the main control valve control valves will close to prevent contamination of the system.

C. Sampling

In addition to the above continuous sampling and monitoring requirements, periodic radioactive waste sampling and activity analysis shall be performed in accordance with Table 3.12-1. Records shall be maintained and reports of the sampling and analysis results shall be submitted in accordance with Sections 5.6 and 5.7 of these Specifications.

Basin:

It is expected that the releases of radioactive materials in gaseous waste will be kept within the design objective levels and will not exceed on an instantaneous basis the dose rate limits specified in 10 CFR Part 20.

These levels provide reasonable assurance that the resulting annual exposure from inhaled gases to the whole body or any organ of an individual will not exceed 5 millirems per year. At the same time, the licensee is permitted the flexibility of operation, compatible with considerations of health and safety, to assure that the public is provided a dependable source of power under unusual operating conditions which may temporarily result in releases higher than the design objective levels but still within the concentration limits specified in 10 CFR Part 20. It is expected that during such a situation flexibility under unusual operating conditions, the licensee will exert every effort to keep levels of radioactive material in gaseous wastes as low as practicable and that annual releases will not exceed a small fraction of the annual average concentration limits specified in 10 CFR Part 20. These efforts shall include consideration of meteorological conditions during releases.

The design objectives have been developed taking into account a combination of system variables including fuel failures, primary system leakage and the performance of radionuclide removal mechanisms. The values selected for these variables include the following:

- a. Primary cooling water accident concentration corresponding to 0.01 rad/s (0.001 rem/s);
- b. Secondary cooling system secondary leak rate of 0.01 gpm;
- c. Steam generator tube burst rate of 5 per cent;
- d. Anticipated ground heat flux to the containment building of 0.15 MW/m² at a rate of 10 minutes per hour;
- e. Infiltration factor of 10.0 for leakage in ruptured defining canals;
- f. Containment pressure of 40 days at 1000°K.

3. In consideration of plant operation, radioactive gaseous waste from the hydrogenated reactor gas system shall be provided a minimum storage time of 60 days except for low radioactivity gaseous waste resulting from purge and fill operations associated with refueling and reactor shutdown.

- CT 5.3.9-3.d. b. Holdup time less than that specified in 3.3.a above shall be covered in the special effluent report required by Section 5.7.E.3 of these specifications.
- CT 5.3.9-3.d. c. The maximum activity to be contained in one gas decay tank shall not exceed 38,400 curies of Ra-106 equivalent.
- 3.4. During the first indication of primary-to-secondary leakage, consistent with sufficient fuel defects, a determination of the iodine partition factor for the blowdown tank shall be made.
- CT 5.3.9.3.7-5. During purging operation, the condenser air ejector discharge shall be continuously monitored for gross radiogas activity. Whenever this monitor is inoperable, grab samples shall be taken from the air ejector discharge and analyzed for gross radiogas activity daily.
- CT 5.3.9.3.7-6. Gross discharged through the stack shall be continuously monitored for gross noble gas and particulate activity. Whenever either of these monitors is inoperable, appropriate gas samples shall be taken and analyzed daily.
- CT 5.3.9.3.7-7. Purging of the reactor building shall be governed by the following criteria:
- a. Reactor building purge shall be filtered through the building's particulate air filters and ductwork unless the concentration of iodine and particulate increases exceed the established MPP inside the reactor building.
 - b. Reactor building purge will be filtered through the building's particulate air filters and ductwork at times whenever irradiated fuel is held in the or any object which is handled near irradiated fuel in the reactor building.

- c. describing the actions in a report to the Commission within 30 days.
2. If the experienced rate of release of radioactive material in gaseous wastes, when averaged over a calendar quarter, is such that these quantities if continued at the same release rate for a year would exceed eight times the annual objectives, the licensee shall define and initiate a program of action to assure that such release rates are reduced, and shall submit a report to the Commission within 7 days describing the causes for such release rates and the course of action taken to reduce them.
3. The rate of release of radioactive materials in gaseous waste from the plant (except I-131 and particulate radioisotopes with half lives greater than 8 days) shall be controlled such that the maximum release rate averaged over any one-hour period shall not exceed:

$$2 \frac{0.1}{(0.01)} = 2.0 \times 10^3 \text{ m}^3/\text{sec}$$

B. Treatment and Monitoring

1. At least one exhaust fan shall be in operation when radioactive gaseous wastes are released to the stack.
2. During release of radioactive gaseous waste from the gaseous waste decay drums to the stack, the following conditions shall be met:
 - a. The gas decay drum effluent monitor and the stack sampling devices for halogens and particulates shall be operable. The normal response of the decay drum effluent monitor shall be verified by comparison with the licensee sample analysis. The monitor shall be tested prior to any release of radioactive gas from a decay drum and shall be calibrated at refueling intervals. The calibration procedure shall consist of exposing the detector to a referenced calibration source in a controlled reproducible geometry. The source and geometry shall be referenced to the original monitor calibration which provides the applicable calibration curves.
 - b. The gaseous waste from the decay drums shall be filtered through the high efficiency particulate air filters and the charcoal adsorber installed.

Table 3.17-1

RADIOACTIVE GAS DRUM RELEASE SAMPLING AND ANALYSISA. Gas Drum Releases

Sample Type	Sampling Frequency	Type of Activity Analysis	Sensitivity of Analysis (1)
Gas	Each Drum Release	Gross Gamma	$10^{-5} \mu\text{Ci/cc}$
		Individual Gamma	
		Uranium	$10^{-4} \mu\text{Ci/cc}$ (2)

B. Containment Venting Releases

Sample Type	Sampling Frequency	Type of Activity Analysis	Sensitivity of Analysis (1)
Gas	Each Vent	Gross Gamma	$10^{-5} \mu\text{Ci/cc}$
		Individual Gamma	
		Uranium	$10^{-4} \mu\text{Ci/cc}$ (2)
Bromidized Sample	Each Vent	U-235	$10^{-6} \mu\text{Ci/cc}$

C. Condenser Air Ejector Releases

Sample Type	Sampling Frequency	Type of Activity Analysis	Sensitivity of Analysis (1)
Gas	Hourly	Gross Gamma Individual Gamma U-235	$10^{-4} \mu\text{Ci/cc}$ $10^{-5} \mu\text{Ci/cc}$ $10^{-5} \mu\text{Ci/cc}$ (2)

Table 3.17-1 (cont'd)

D. Stack Releases

Sample Type	Sampling Frequency	Type of Activity Analysis	Sensitivity of Analysis (1)
Gas	Quarterly	Gross Gamma	$10^{-6} \mu\text{Ci/cc}$
		Individual Gamma Emitters	$10^{-5} \mu\text{Ci/cc}$ (2)
Dehumidified Sample	Each Decay Drum Release	H-3	$10^{-9} \mu\text{Ci/cc}$
Charcoal	Weekly	I-131, I-133, I-135	$3 \times 10^{-12} \mu\text{Ci/cc}$
Particulates	Weekly	Gross α, β	$3 \times 10^{-12} \mu\text{Ci/cc}$
	Weekly	La-140, La-140, I-131	$3 \times 10^{-11} \mu\text{Ci/cc}$
	Monthly Composite of Weekly Samples	Gross β, γ	$3 \times 10^{-12} \mu\text{Ci/cc}$
	Individual Gamma Emitters		$3 \times 10^{-11} \mu\text{Ci/cc}$
	Quarterly Composite of Weekly Samples	Sr-89, Sr-90	$1 \times 10^{-10} \mu\text{Ci/cc}$
	One Weekly Sample/Quarter	Gross α	$3 \times 10^{-12} \mu\text{Ci/cc}$

NOTES:

- (1) The above activity analysis sensitivities are based on the projected capability of laboratory instrumentation and techniques to be employed by Maine Yankee. In order to assure that actual Maine Yankee operating experience is utilized, a reevaluation will be performed within 2 years of initial full power operation of the plant.
- (2) For certain mixtures of gamma emitters, it may not be possible to measure radionuclides at levels near their sensitivity limits when other nuclides are present in the sample at much higher levels. Under such circumstances, it will be more appropriate to calculate the levels of such nuclides using observed ratios with those radionuclides which are measurable.

Table 3.17-2
GASPOUS RADIONUCLIDE RELEASES

Reactor Coolant Concentration ($\text{Ci/M}^3 \text{ O}_2 \text{ H}_2$)	Exposure Time (hr)	Moderated Vents	Mr. Reactor Vent	Containment Vent	Decay Decay Time (hr)
2.99-1K	1.23-4	3.38-1	4.2-4	2.0-6	5.0-1
5.12-1	1.03-5	1.59-6	1.96-6	---	5.0-1
5.02-1	2.16-4	5.31-5	7.9-5	---	5.0-1
7.22-2	3.22-5	1.6-7	1.95-6	---	5.0-1
2.00-1	1.2-4	1.1-5	1.43-6	---	5.0-1
2.00-1	1.00-4	---	6.55-1	1.24-1	5.0-1
2.00-1	1.9-1	---	1.2-1	6.27-3	5.0-1
2.00-1	1.00-2	---	6.6-2	1.05-3	5.0-1
2.26-1	2.26-1	---	2.05-1	6.8-3	5.0-1
2.00-1	2.00-1	---	7.06-2	2.76-1	5.0-1
2.00-1	2.00-1	---	1.59-1	2.44-2	5.0-1
5.60-1	5.60-1	---	3.53-1	4.25-2	5.0-1

$\approx 2.99-1 = 2.99 \times 10^{-1}$