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LTR-NRC-19-66
November 15, 2019

Subject: Comments on Draft Safety Evaluation for WCAP-18240-P, "Westinghouse Thermal Design Procedure (WTDP)" (Proprietary / Non-Proprietary)

- References:**
1. LTR-NRC-18-59 dated August 27, 2018, "Submittal of WCAP-18240-P / WCAP-18240-NP, Revision 0, 'Westinghouse Thermal Design Procedure (WTDP)' (Proprietary / Non-Proprietary)," ADAMS Accession Number ML18242A237 (package)
 2. LTR-NRC-19-36 dated July 12, 2019, "Transmittal of Responses to the NRC Request for Additional Information for WCAP-18240-P, 'Westinghouse Thermal Design Procedure (WTDP),' (Proprietary / Non-Proprietary)," ADAMS Accession Numbers ML19192A275 (Proprietary) and ML19192A268 (Non-Proprietary)
 3. LTR-NRC-19-40 dated July 31, 2019, "Transmittal of CEN-283(S)-P/NP, Part 1, 'Statistical Combination of Uncertainties Part 1; Combination of System Parameter Uncertainties in Thermal Margin Analyses for San Onofre Nuclear Units 2 and 3,' and CEN-283(S)-P/NP, Part 2, 'Statistical Combination of Uncertainties Part 2; Uncertainty Analysis of Limiting Safety System Settings San Onofre Nuclear Generating Station Units 2 and 3,'" ADAMS Accession Numbers ML19214A143 (Cover Letter and Affidavit), ML19214A154 and ML19214A156 (Proprietary enclosures), ML19214A144 and ML19214A145 (Non-Proprietary enclosures)
 4. Draft Safety Evaluation for Westinghouse Electric Company Topical Report WCAP-18240-P / WCAP-18240-NP, Revision 0, "Westinghouse Thermal Design Procedure (WTDP)," EPID L-2018-TOP-0033, Dennis C. Morey (NRC) to Camille Zozula (Westinghouse), dated October 22, 2019

Reference 1 transmitted Proprietary and Non-Proprietary versions of WCAP-18240 to the NRC for review. References 2 and 3 transmitted additional information which was requested to support the NRC review. Reference 4 provided the Draft NRC Safety Evaluation for WCAP-18240-P, "Westinghouse Thermal Design Procedure (WTDP)." Enclosed are Proprietary and Non-Proprietary versions of comments on the proprietary aspects of Reference 4 as well as the correction of factual errors and clarity concerns. A marked-up copy of the draft SE showing proposed changes (including information to be withheld) and a summary table of the proposed changes are provided in the enclosures.

This submittal contains proprietary information of Westinghouse Electric Company LLC (“Westinghouse”). In conformance with the requirements of 10 CFR Section 2.390, as amended, of the Nuclear Regulatory Commission’s (“Commission’s”) regulations, we are enclosing with this submittal an Affidavit. The Affidavit sets forth the basis on which the information identified as proprietary may be withheld from public disclosure by the Commission.

Correspondence with respect to the contents of this submittal, the proprietary aspects of this submittal, or the Westinghouse Affidavit should reference AW-19-4968 and be addressed to Korey L. Hosack, Manager, Licensing, Analysis, & Testing, Westinghouse Electric Company, 1000 Westinghouse Drive, Building 1, Suite 133, Cranberry Township, Pennsylvania 16066.



Korey L. Hosack, Manager
Licensing, Analysis, & Testing

cc: Ekaterina Lenning (NRC)
Dennis Morey (NRC)

Enclosures:

1. Affidavit AW-19-4968
2. Proprietary Information Notice and Copyright Notice
3. LTR-NRC-19-66 P-Attachment, Comments on Draft Safety Evaluation for WCAP-18240-P, “Westinghouse Thermal Design Procedure (WTDP)” (Proprietary)
4. LTR-NRC-19-66 NP-Attachment, Comments on Draft Safety Evaluation for WCAP-18240-P, “Westinghouse Thermal Design Procedure (WTDP)” (Non-Proprietary)

AFFIDAVIT

COMMONWEALTH OF PENNSYLVANIA:

COUNTY OF BUTLER:

- (1) I, Korey L. Hosack, have been specifically delegated and authorized to apply for withholding and execute this Affidavit on behalf of Westinghouse Electric Company LLC (Westinghouse).
- (2) I am requesting the proprietary portions of LTR-NRC-19-66 be withheld from public disclosure under 10 CFR 2.390.
- (3) I have personal knowledge of the criteria and procedures utilized by Westinghouse in designating information as a trade secret, privileged, or as confidential commercial or financial information.
- (4) Pursuant to 10 CFR 2.390, the following is furnished for consideration by the Commission in determining whether the information sought to be withheld from public disclosure should be withheld.
 - (i) The information sought to be withheld from public disclosure is owned and has been held in confidence by Westinghouse and is not customarily disclosed to the public.
 - (ii) Public disclosure of this proprietary information is likely to cause substantial harm to the competitive position of Westinghouse because it would enhance the ability of competitors to provide similar technical evaluation justifications and licensing defense services for commercial power reactors without commensurate expenses. Also, public disclosure of the information would enable others to use the information to meet NRC requirements for licensing documentation without purchasing the right to use the information.
- (5) Westinghouse has policies in place to identify proprietary information. Under that system, information is held in confidence if it falls in one or more of several types, the release of which might result in the loss of an existing or potential competitive advantage, as follows:

AFFIDAVIT

- (a) The information reveals the distinguishing aspects of a process (or component, structure, tool, method, etc.) where prevention of its use by any of Westinghouse's competitors without license from Westinghouse constitutes a competitive economic advantage over other companies.
 - (b) It consists of supporting data, including test data, relative to a process (or component, structure, tool, method, etc.), the application of which data secures a competitive economic advantage (e.g., by optimization or improved marketability).
 - (c) Its use by a competitor would reduce his expenditure of resources or improve his competitive position in the design, manufacture, shipment, installation, assurance of quality, or licensing a similar product.
 - (d) It reveals cost or price information, production capacities, budget levels, or commercial strategies of Westinghouse, its customers or suppliers.
 - (e) It reveals aspects of past, present, or future Westinghouse or customer funded development plans and programs of potential commercial value to Westinghouse.
 - (f) It contains patentable ideas, for which patent protection may be desirable.
- (6) The attached documents are bracketed to indicate proprietary information to be withheld from public disclosure and, in all cases, the bases for withholding are (a, c) from Section 5 of this Affidavit. Westinghouse customarily holds in confidence this type of information as identified in Sections (5)(a) and (5)(c) of this Affidavit.

AFFIDAVIT

I declare that the averments of fact set forth in this Affidavit are true and correct to the best of my knowledge, information, and belief.

I declare under penalty of perjury that the foregoing is true and correct.

Executed on: 2019/1/15



Korey L. Hosack, Manager
Licensing, Analysis, & Testing

PROPRIETARY INFORMATION NOTICE

Transmitted herewith are the proprietary and non-proprietary versions of a document, furnished to the NRC in connection with the review of WCAP-18240-P / NP, "Westinghouse Thermal Design Procedure (WTDP)."

In order to conform to the requirements of 10 CFR 2.390 of the Commission's regulations concerning the protection of proprietary information so submitted to the NRC, the information which is proprietary in the proprietary versions is contained within brackets, and where the proprietary information has been deleted in the non-proprietary versions, only the brackets remain (the information that was contained within the brackets in the proprietary versions having been deleted). The justification for claiming the information so designated as proprietary is discussed in Sections (5)(a) and (5)(c) of the Affidavit accompanying this transmittal pursuant to 10 CFR 2.390(b)(1).

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The reports transmitted herewith each bear a Westinghouse copyright notice. The NRC is permitted to make the number of copies of the information contained in these reports which is necessary for its internal use in connection with generic and plant specific reviews and approvals as well as the issuance, denial, amendment, transfer, renewal, modification, suspension, revocation, or violation of a license, permit, order, or regulation subject to the requirements of 10 CFR 2.390 regarding restrictions on public disclosure to the extent such information has been identified as proprietary by Westinghouse, copyright protection notwithstanding. With respect to the non-proprietary version of this report, the NRC is permitted to make the number of copies beyond those necessary for its internal use which are necessary in order to have one copy available for public viewing in the appropriate docket files in the public document room in Washington, DC and in local public document rooms as may be required by NRC regulations if the number of copies submitted is insufficient for this purpose. Copies made by the NRC must include the copyright notice in all instances and the proprietary notice if the original was identified as proprietary.

**Comments on Draft Safety Evaluation for WCAP-18240-P,
“Westinghouse Thermal Design Procedure (WTDP)”**

(Non-Proprietary)

November 2019

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Comment #	Location	Comment	Proposed Change
1	Page 3, lines 26 and 27	Editorial - Sentence structure is incorrect.	Change "...the NRC staff determined the tiger team approach was <i>determined to be</i> appropriate for this review" to "...the NRC staff determined the tiger team approach was appropriate for this review."
2	Page 4, line 10	Editorial – Improper acronym	Change "SAFDLS" to "SAFDLs" as used on page 4 line 36 and page 6 line 3.
3	Page 4, line 43	Editorial – Improper syntax	Change "...a fraction... <i>are</i> presumed to fail" to "...a fraction...is presumed to fail."
4	Page 5, line 11	The RTDP topical report citation is incorrect.	Change WCAP-13397-P-A to WCAP-11397-P-A.
5	Page 5, lines 14 and 15 Page 6, line 12	Improper reference citation - Reference 13 (Palo Verde UFSAR) was cited in the WTDP topical report (Sections 1.2, 3.0, and 4.3) only with respect to an application of the rods-in DNB calculation method. It was not cited for the DNBR limit calculation method. Reference 13 as cited on page 6 of the draft SE is unrelated to the SCU/MSCU, ITDP, and RTDP methods.	On page 5, delete the reference to the PVNGS UFSAR on lines 14 and 15. On page 6, change "Refs. 9 <i>through 14</i> " to "Refs. 9 through 12 and 14."
6	Page 5, line 31	Editorial – Improper usage	Change "quantifications methods" to "quantification methods."
7	Page 5, line 32	Editorial – improper syntax	Change "...a set of values <i>are</i> independent..." to "...a set of values is independent..."
8	Page 6, line 8	Editorial – improper syntax	Change "...methodologies that <i>has</i> been approved..." to "...methodologies that have been approved..."
9	Page 6, line 11	No reference is provided for the Improved Thermal Design Procedure (ITDP).	The WTDP topical report refers only to the RTDP method (Reference 3 of WCAP-18240-P). While the statement on WTDP as a standalone methodology is correct in the draft SE, the reference to ITDP should cite an independent reference. Draft SE Reference 9 applies to RTDP. The ITDP reference is WCAP-8567-P-A (Chelemer, H., et.al., "Improved Thermal Design Procedure," WCAP-8567-P-A, February 1989).
10	Page 7, lines 33, 35, 38, 40	Editorial – Improper bracketing convention for proprietary information	All of the discussion beginning on line 25 and ending on line 45 is proprietary. With one continuous group of information to be withheld, individual paragraphs need not be individually bracketed. Retain only the open bracket on line 25 and the closed bracket on line 45. All other brackets on lines 33, 35, 38, and 40 should be deleted.

11	Page 8, line 6	Editorial – confusing text	Suggest changing “The DNBR value <i>sampled from based on</i> the correlation statistics is then increased” to “The sampled DNBR value based on the correlation statistics is then increased....”
12	Page 8, Line 10	The specific minimum number of statepoints for the Monte Carlo process should be withheld from public disclosure. The basis for withholding was provided in the original topical report submittal (LTR-NRC-18-59). That number was correctly bracketed on page 12 (line 27) of the draft SE.	Bracket the specific number on page 8, line 10, as was done in Section 4.0, Limitation and Condition #3.
13	Page 8, line 24	Editorial – confusing text	Suggest deleting “only” from the following sentence introduction: “Because Westinghouse demonstrated that <i>only</i> cases that were not used in the statistical analysis were those in which a physically unrealistic combination of state parameters were chosen”
14	Page 9, lines 35, 37, 44, 46, 48 Page 10, lines 1, 2, 3, 5, 7, 11, 13, 17, 19	Editorial – Improper bracketing convention for proprietary information	All of the discussion beginning on line 34 and ending on line 48 of page 9 is proprietary. With one continuous group of information to be withheld, individual paragraphs need not be individually bracketed. Retain only the open bracket on line 34 of page 9 and add a closed bracket at the end of line 48 of page 9. All other brackets on lines 35, 37, 44, and 46 on page 9 should be deleted. When proprietary text carries over from one page to the next, the established convention is to end the leading page with a closed bracket “]” and start the following page with an open bracket “[.” Therefore, add a closed bracket at the end of line 48 on page 9. All text and Figure 1 on page 10 are proprietary, so start off line 1 on page 10 with an open bracket and delete all other brackets except the closed bracket on line 25 of page 10. This is the convention used by Westinghouse in topical report submittals and followed by the NRC in their final Safety Evaluations for recent WCAPs such as PAD5 and FSLOCA.
15	Page 10, line 5	An incorrect value for the standard deviation is listed.	Change the value of the standard deviation to reflect the value shown on Figures 1 and 2 of the draft SE. That

			proprietary standard deviation value was included on page C-2 and Table C-4 of the submitted topical report, and the same value was also provided in the response to RAI-WTDP-01 sub-part b).a in LTR-NRC-19-36 (Enclosure 3, pages 10-11).
16	Page 11, lines 10 through 21	Proprietary information needs to be bracketed.	The rods-in-DNB discussion beginning at line 10 on page 11 and ending at the conclusion of line 21 is proprietary and should be bracketed. The basis for withholding was provided in the original topical report submittal, WCAP-18240-P Section 3.2 (LTR-NRC-18-59, proprietary version of the topical report), and in the response to RAI-WTDP-01 sub-part b).a (LTR-NRC-19-36, Enclosure 3, pages 9-11).
17	Page 13, lines 2, 31, 32, 45	Incorrect references	Reference 1 was signed by Westinghouse employee E. J. Mercier, not E. F. Mercier. Reference 5 has the ADAMS citations interposed. Enclosure 1 of the 5-14-19 NRC RAI letter provided a non-proprietary version of the RAIs under ADAMS ML19108A140, not ML19108A144 (the latter is not publicly available in ADAMS, as would be expected for a proprietary document). Enclosure 2 of the 5-14-19 NRC RAI letter provided a proprietary version of the RAIs under ADAMS ML19108A144, not ML19108A140. Reference 7 should identify the Westinghouse RAI response letter as LTR-NRC-19-36.
18	Page 14, line 6	Suspect ADAMS citation	The ADAMS Accession Number for Reference 9 (ML08065033) could not be verified (document not publicly available); however, the citation appears to be suspect given that there are only 8 digits after the "ML" vs. the typical 9 digits. This ADAMS citation was not provided by Westinghouse in WCAP-18240-P. Please verify.
19	Page 14, lines 22 and 30	Unverifiable ADAMS citations	Please verify the ADAMS citations for Reference 12 and 14. These ADAMS citations were not provided by Westinghouse in WCAP-18240-P and could not be verified.

MARKUPS OF NON-PROPRIETARY VERSION OF THE DRAFT SE

U. S. NUCLEAR REGULATORY COMMISSION

DRAFT SAFETY EVALUATION BY THE OFFICE OF NUCLEAR REACTOR REGULATION

TOPICAL REPORT WCAP-18240-P/WCAP-18240-NP, REVISION 0

“WESTINGHOUSE THERMAL DESIGN PROCEDURE”

WESTINGHOUSE ELECTRIC COMPANY

EPID L-2018-TOP-0033

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20

1 **1.0 INTRODUCTION**

2 By letter dated August 27, 2018 (Ref. 1), Westinghouse Electric Company (Westinghouse)
 3 submitted topical report (TR) WCAP-18240-P/WCAP-18240-NP, Revision 0,
 4 "Westinghouse Thermal Design Procedure (WTDP)" (Ref. 2) to the U.S. Nuclear
 5 Regulatory Commission (NRC) for review and approval. The purpose of this TR was to
 6 describe a new methodology for determining the statistical departure from nucleate boiling ratio
 7 (DNBR) limit for anticipated operational occurrences (AOOs) and calculating the number of rods
 8 that experience departure from nucleate boiling (DNB) for postulated accidents. The
 9 methodology is intended to be applicable to pressurized water reactors (PWRs), including those
 10 with Combustion Engineering (CE)- and Westinghouse-designed nuclear steam supply systems
 11 (NSSSs).

12
 13 The complete list of correspondence between the NRC and Westinghouse is provided in
 14 Table 1 below. This includes Requests for Additional Information (RAIs), responses to RAIs,
 15 audit documentation, and any other correspondence relevant to this review.
 16
 17

Table 1: List of Key Correspondence

Sender	Document	Document Date	Reference
Westinghouse	Submittal Letter	August 27, 2018	1
Westinghouse	Topical Report	August 27, 2018	2
NRC	Acceptance Letter	November 5, 2018	3
NRC	Audit Plan	March 18, 2019	4
NRC	Round 1 RAIs	May 14, 2019	5
NRC	Audit Summary	July 9, 2019	6
Westinghouse	Round 1 RAI Responses	July 12, 2019	7

18
 19 A brief summary of the RAIs is provided in Table 2 below.
 20
 21

Table 2: Listing of RAIs

RAI	Subject
RAI-WTDP-01	Clarification of mathematical method
RAI-WTDP-02	Epistemic Uncertainties
RAI-WTDP-03	Δ DNBR Spatial Sensitivity
RAI-WTDP-04	Criteria for case exclusion

22
 23 This review was performed within the guidelines of LIC-500 (Ref. 8). Additionally, the NRC staff
 24 chose to use a tiger team approach to perform the review. This approach has been previously
 25 suggested by various stakeholders, including industry representatives. Due to the NRC staff
 26 familiarity with the subject matter and the short length of the TR, the NRC staff determined the
 27 tiger team approach was ~~determined to be~~ appropriate for this review.

- 4 -

1 2.0 **REGULATORY EVALUATION**

2 The WTDP TR describes a method for calculating a statistical limit on the DNBR, below which
3 fuel failure may occur. TR also describes a method for using the statistical DNBR limit to
4 determine the number of rods that would be expected to be damaged due to DNB during an
5 accident. These two aspects of the WTDP methodology, though related, are reviewed
6 separately because they relate to different regulatory criteria.

7 2.1 Statistical DNBR Limit

8 General Design Criterion (GDC) 10 from Title 10 of the *Code of Federal Regulations* (10 CFR)
9 Part 50, Appendix A, "General Design Criteria for Nuclear Power Plants," requires licensees to
10 ensure that specified acceptable fuel design limits (SAFDLs) are not exceeded during normal
11 operation, including the effects of AOOs. In pressurized water reactors (PWRs), departing from
12 the nucleate boiling regime could significantly reduce the ability to transfer heat from the fuel
13 rods to the coolant, resulting in an excessive increase in cladding temperature that could cause
14 cladding failure. As such, prevention of departure from nucleate boiling is typically identified as
15 a SAFDL for PWRs. The ratio of the heat flux at which DNB is expected to occur, also known
16 as the critical heat flux (CHF), to the actual heat flux is known as the DNBR. Departure from
17 nucleate boiling is generally prevented by ensuring that the reactor remains above a specified
18 DNBR limit during operation.

19
20 The NRC staff reviews thermal-hydraulic analyses using the guidance contained in
21 NUREG-0800, "Standard Review Plan" (SRP), Section 4.4, "Thermal and Hydraulic Design."
22 SRP 4.4 provides criteria for ensuring the requirements of GDC 10 are met. SRP Acceptance
23 Criterion 1 discusses the use of a limit on the DNBR that provides assurance that there is a
24 95-percent probability at a 95-percent confidence level that the hot rod in the core does not
25 experience DNB during normal operation or AOOs – this is commonly known as a 95/95 DNBR
26 limit.

27
28 The regulation at 10 CFR 50.34, "Contents of Applications; Technical Information," provides
29 requirements for nuclear reactor licensees to provide in a final safety analysis report (FSAR) an
30 evaluation of the design and performance of structures, systems, and components of the facility,
31 including determination of the margins of safety during normal operations and transient
32 conditions anticipated during the life of the facility. In practice, PWRs include analyses of
33 normal operation and transient conditions in their FSARs that evaluate margin to the DNBR
34 limit.

35 2.2 Rods-In-DNB Evaluation

36 As discussed above, GDC 10 requires that SAFDLs not be exceeded for normal operation and
37 AOOs. However, certain postulated accidents have been identified which have the potential to
38 fail fuel. For these accidents, the radiological release must be evaluated and is subject to
39 regulatory limits, either by evaluating margin to the 10 CFR 100 dose limits or by performing an
40 accident source term analysis in accordance with 10 CFR 50.67.

41
42 As part of the radiological consequence analysis for a given transient, a fraction of the fuel rods
43 in the core is ~~is~~ presumed to fail. The rods-in-DNB evaluation proposed as part of WTDP is used
44 to evaluate the number of rods expected to experience DNB during the transient. All rods that
45 experience DNB are assumed to fail. The number of rods that fail in this manner are counted

- 5 -

1 and compared to the number of failed rods in the radiological consequence analysis to ensure
2 acceptability. SRP 15.3.3-15.3.4, "Reactor Coolant Pump Rotor Seizure and Reactor Coolant
3 Pump Shaft Break," and SRP 15.4.8, "Spectrum of Rod Ejection Accidents (PWR)," provide
4 examples of additional, more detailed guidance on the review of the DNBR criterion and the
5 failed rod census.

6 2.3 Regulatory History

7 The NRC staff has reviewed and approved similar methods for performing the statistical DNBR
8 limit analysis discussed in WTDP. The following is a list of the most pertinent methods for
9 DNBR limit analysis:

10

- 11 • WCAP-113397-P-A, "Revised Thermal Design Procedure" (Ref. 9)
- 12 • CEN-283(S)-P, "Statistical Combination of Uncertainties" (Refs. 10 and 11)
- 13 • CEN-356(V)-P-A, "Modified Statistical Combination of Uncertainties" (Ref. 12)
- 14 • ~~Palo Verde Nuclear Generation Station Units 1, 2 and 3 Updated Final Safety Analysis~~
15 ~~Report (FSAR), Revision 19 (Ref. 13)~~
- 16 • WCAP-16500-P-A Supplement 1, Revision 1, "Application of CE Setpoint Methodology
17 for CE 16x16 Next Generation Fuel (NGF) (Ref. 14)

18

19 The following is a list of the most pertinent methods for statistical rods-in-DNB analysis:

20

- 21 • CENPD-183-A, "Loss of Flow" (Ref. 15)
- 22 • Palo Verde Nuclear Generation Station Units 1, 2 and 3 Updated Final Safety Analysis
23 Report (FSAR), Revision 19 (Ref. 13)

24

25 For further details on the history, see Section 1.2 of the WTDP TR.

26 2.4 Criteria for this Review

27 As there are currently no formal frameworks to assess uncertainty quantification methodologies
28 such as WTDP, the NRC staff used portions of the framework described in NUREG/KM-0013
29 (Ref. 16) as well as their own knowledge and experience to ensure that the estimate of the
30 DNBR limit as well as rods-in-DNB was acceptable. This included ensuring that there was
31 evidence to support the common assumptions made by uncertainty quantification methods
32 such as assuming a set of values is from a normal distribution, assuming a set of values is
33 independent of specific parameters, and assuming certain epistemic uncertainties can be
34 treated as aleatory uncertainties.

35 3.0 TECHNICAL EVALUATION

36 The NRC staff considered three separate areas of evaluation for WTDP: the calculation of the
37 DNBR limit, the calculation of the rods-in-DNB, and the replacement of CETOP-D. Each area is
38 discussed below.

39 3.1 DNBR Limit

40 Westinghouse proposed to use a Monte Carlo approach to determine the statistical 95/95
41 DNBR limit. This approach samples operating conditions to determine DNBR sensitivities to
42 fuel parameters and instrument uncertainties. The DNBR sensitivity is then combined with the

- 6 -

1 uncertainty in the prediction of DNBR to calculate the overall DNBR uncertainty distribution.
2 The statistical DNBR limit is the 95/95 upper tolerance limit of this distribution. This limit is
3 considered one of the GDC 10 SAFDLs. This approach is described in Section 2 of the TR with
4 further details provided in response to RAI-WTDP-01.

5
6 The approach proposed by Westinghouse to determine a statistical DNBR limit is based on the
7 existing Statistical Combination of Uncertainties or Modified Statistical Combination of
8 Uncertainties (SCU/MSCU) methodologies that have been approved by the NRC for CE plants.
9 However, WTDP is intended to stand on its own as a replacement for the current statistical
10 DNBR limit methodologies for both CE plants and Westinghouse plants (e.g., SCU/MSCU,
11 Improved Thermal Design Procedure (ITDP), and Revised Thermal Design Procedure (RTDP) –
12 see Refs. 9 through 12 and 14). Therefore, the NRC staff considered the prior approval of the
13 SCU/MSCU methodology as a context for the review of the WTDP DNBR limit method, and
14 reviewed WTDP as a standalone methodology.

15 3.1.1 Input Selection

16 As discussed in Section 2.1 of the TR, the inputs to WTDP include uncertainties in fuel
17 parameters, uncertainties associated with reactor state parameters, and the range of operating
18 space to be covered by the WTDP calculation. The fuel-related parameters (which
19 Westinghouse refers to as the “system” parameters in the TR) include those associated with
20 fuel manufacturing as well as those associated with the DNB correlation and the subchannel
21 code. The operating state of the reactor is defined by the reactor power and its associated
22 power distribution, the coolant temperature, flow rate, bypass fraction, and the reactor pressure.

23
24 Westinghouse provided a list of typical system and state parameters in Section 2.1 of the TR.
25 However, Westinghouse also stated that statistical DNBR limits for a specific plant may or may
26 not include all the uncertainties listed and that the uncertainty inputs will be justified on a plant-
27 specific basis. For parameters whose uncertainty is not included in the DNBR limit calculation,
28 Westinghouse specified that conservative values with respect to DNBR will be used. The NRC
29 staff reviewed the parameters proposed for the uncertainty analysis and found them to be
30 consistent with the existing RTDP and SCU methodologies. The NRC staff also expects that
31 use of conservative values for any of the parameters listed will be more conservative than
32 including the parameter in the uncertainty analysis. Thus, the NRC staff finds the approach for
33 determining the uncertainties to include in the analysis to be acceptable.

34
35 The operating space of the reactor is defined by the set of operating states that occur in the
36 transient and accident analysis. To select input for the Monte Carlo runs, Westinghouse
37 randomly samples over the entire operating space, consistent with the NRC-approved SCU
38 methodology. The state parameters are sampled from a uniform distribution. By using a
39 uniform distribution, Westinghouse assumes that all statepoints are equally likely. In reality, all
40 statepoints are not equally likely, and there is an unknown set of statepoints corresponding to
41 the actual operation of the reactor.

42
43 When actual parameter values are unknown, it is common to assume that all values are equally
44 likely and therefore to sample them from a uniform distribution. This is because, while there are
45 many methods to analyze aleatory uncertainties (e.g., Monte Carlo analysis), there are few
46 methods to analyze epistemic uncertainties, such as the case of unknown probability
47 distributions. However, this assumption may or may not be appropriate. Therefore, the NRC
48 staff asked RAI-WTDP-02.

- 7 -

1 In response, Westinghouse stated that the use of a uniform distribution results in higher DNBR
2 limit than would a normal distribution. The NRC staff agrees that in many cases, the use of a
3 uniform distribution will result in a conservative analysis compared to a normal distribution due
4 to the increased weight given at the extremes of the distribution and the common situation in
5 which the most extreme values of the distribution result in the most conservative cases. The
6 NRC staff does note that this may not always be true, and that the use of a uniform distribution
7 is not inherently conservative. However, the NRC staff does find that Westinghouse is using
8 reasonable distributions for the sampled parameters.

9
10 Because Westinghouse demonstrated that its method adequately samples over the operating
11 space, the NRC staff determined that it was acceptable.

12 3.1.2 Generation of the DNBR Sample

13 The Monte Carlo procedure samples multiple statepoints, with a nominal case and a sensitivity
14 case for each statepoint. The nominal case is based on a random sample of a statepoint, with
15 all parameters at their expected values. The sensitivity case perturbs the statepoint from the
16 nominal case based on the uncertainties in each parameter. The parameter uncertainties
17 accounted for in the sensitivity case include those in state parameters due to measurement,
18 those in fuel-related parameters due to manufacturing, and those in the assembly inlet flow
19 distribution. The specific uncertainties included in the analysis are dependent on the fuel type
20 and plant, as discussed in additional detail in Sections 4.1 and 4.2 of the TR. An approved
21 subchannel code (e.g., VIPRE-W) is then used to calculate the minimum DNBR from both the
22 nominal and sensitivity cases, and the difference between the two at each statepoint is termed
23 the Δ DNBR.

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45] Because the
46 methodology that Westinghouse is using would result in a higher variance for the Δ DNBR than
47 expected and that higher variance will (on average) result in a higher DNBR limit than expected,
48 the NRC considered this approach acceptable.

- 8 -

1 Once the Δ DNBR is calculated, a DNBR value is then randomly sampled based on the CHF
2 correlation statistics to account for the uncertainty in the approved CHF correlation. Prior to the
3 sampling, the mean associated with the CHF correlation is adjusted to account for any biases
4 added to the correlation during the NRC approval process (including the small rounding bias),
5 and the standard deviation is increased to account for the fact that it is based on a sample. The
6 **sampled** DNBR value ~~sampled from~~ based on the correlation statistics is then increased to
7 account for subchannel code uncertainty.
8

9 The resulting DNBR value is then added to the Δ DNBR to obtain a single realization of the
10 Monte Carlo process. This entire process is repeated for a minimum of [] statepoints.
11

12 The NRC staff is aware that in some cases the code may fail or produce an error, resulting in
13 that case not being used. The NRC staff therefore asked Westinghouse in RAI-WTDP-04 what
14 criteria were used to ensure that the code failure or error was reasonable (e.g., the randomly
15 selected statepoint was not physically achievable) and was not the result of a code bug or input
16 error.
17

18 In its response, Westinghouse provided the criteria used to determine if a case could be
19 excluded. The NRC staff reviewed these criteria and found them to be acceptable because (a)
20 they did not allow the case to be excluded simply because it provided unfavorable results,
21 (b) they provided an objective basis for excluding a case, and (c) they would result in a robust
22 (i.e., consistent) calculation of the DNBR limit.
23

24 Because Westinghouse demonstrated that ~~only~~ cases that were not used in the statistical
25 analysis were those in which a physically unrealistic combination of state parameters were
26 chosen, the NRC staff found Westinghouse's approach to be acceptable.
27

28 The NRC staff reviewed the process for generating the DNBR samples to determine the DNBR
29 uncertainty and found that it would result in a representative sample set of the DNBR population
30 over the operating space.

31 3.1.3 Development of the Statistical DNBR Limit

32 Westinghouse proposed different approaches for determining the statistical DNBR limit from the
33 DNBR sample set obtained from the process discussed above. A parametric approach is used
34 if the data can be shown to be from a normal distribution (e.g., Owen's table). A non-parametric
35 approach is used if it can not be shown that the data is from a normal distribution (i.e., Wilks
36 method). The D' test is used to determine if the data is from a normal distribution.
37

38 If the D' test shows that the data can be approximated as normal, Westinghouse will use a
39 parametric approach to determine the 95/95 upper tolerance limit. The 95/95 upper tolerance
40 limit is given by the formula:

$$41 \qquad \qquad \qquad 95/95 \text{ Upper Tolerance Limit} = \mu + k\sigma$$

42
43
44 Westinghouse has two different options for implementing the parametric approach. The first
45 option [

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47
48] The second option uses the formula above, with mean and standard

- 9 -

1 deviation from the DNBR dataset and a k factor from Owen's tables based on the sample size.
2 The NRC staff performing this review were familiar with the second option, but not the first;
3 however, test calculations performed by the staff showed that the first option provided
4 conservative results relative to the second.

5
6 If the DNBR distribution cannot be described as normal based on the results of the D' test, a
7 non-parametric approach based on order statistics is used to determine the 95/95 upper
8 tolerance limit.

9
10 The statistical test and the methods used for determining the DNBR limit applied are among
11 those commonly applied in such instances or were otherwise found by the NRC staff to be
12 conservative relative to these commonly-used methods. Thus, the NRC staff finds the proposed
13 methods for determining the statistical DNBR limit based on the DNBR sample population
14 distribution to be acceptable.

15 3.2 Rods-in-DNB

16 The rods-in-DNB methodology proposed in the WTDP TR is similar to that previously reviewed
17 and approved for CE NSSS analysis (Reference 15). In the WTDP TR, Westinghouse
18 described the method in more detail and asked for its extension to Westinghouse-designed
19 NSSS plants.

20
21 Westinghouse uses an NRC-approved subchannel code (e.g., VIPRE-W) to calculate a table of
22 DNBR versus fuel rod power at the limiting thermal-hydraulic statepoint from the transient
23 analysis. Since the table is generated from the limiting thermal-hydraulic statepoint, it provides
24 the minimum DNBR expected for a given rod power for a given transient.

25
26 Next, Westinghouse generates a table providing the probability of fuel damage as a function of
27 DNBR at a 95% confidence level (termed the DNBR probability distribution in the TR). For
28 example, if a rod were at the 95/95 DNBR limit value, the rod would have a 5% chance of
29 experiencing DNB and therefore a 5% probability of failure. However, after reviewing the WTDP
30 topical report and the previously-approved CE methodology, the NRC staff was unsure as to
31 how this failure probability table was calculated and asked for additional details in
32 RAI-WTDP-01. In its response, Westinghouse provided additional explanation on the process
33 for calculating the probability of failure of a fuel rod. The NRC staff found the explanation
34 provided a logical process, but the staff did question why [

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7 For the next step in the process, Westinghouse then generates a fuel rod census table that
8 contains the fraction of the core greater than or equal to a given fuel rod power. It was not clear
9 to the NRC staff how this table was used and asked for additional clarification in RAI-WTDP-01.

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After a review of the methodology, including the further details provided in response to RAI 1,
the NRC staff agrees with the staff's prior conclusion that this technique is acceptable for
calculating fuel rod failures caused by DNB, and that it is acceptable for use in PWR analysis.

- 12 -

1 3.3 Replacement of CETOP-D

2 In the CE setpoint methodology, Westinghouse uses a simplified thermal-hydraulic code known
3 as CETOP-D to determine correction factors for the online monitoring and protection systems at
4 CE plants. In 1981, the CETOP-D code was chosen for this use instead of a higher-fidelity
5 subchannel code due to the large number of cases needed for the CE setpoints analysis and
6 the relative speed of execution of the code.
7

8 In the WTDP TR, Westinghouse stated that plants may replace CETOP-D with a different
9 NRC-approved subchannel code (e.g., VIPRE-W) to perform the same analysis. The NRC staff
10 reviewed the evaluation model applying CETOP-D and agrees with Westinghouse that other
11 NRC-approved subchannel codes are acceptable to perform the same evaluations, provided
12 that they are able to use approved CHF correlations applicable to the fuel type being modeled
13 and have adequately characterized the code and correlation uncertainties. The NRC staff notes
14 that this change is primarily driven by the greatly increased speed of computation since the
15 evaluation model including CETOP-D was originally implemented in the 1980s.

16 4.0 LIMITATIONS AND CONDITIONS

17 The use of the WTDP methodology is subject to the following limitations and conditions:
18

- 19 1. In application to a given plant, WTDP shall be used with a subchannel code and CHF
20 correlation combination that has been approved for the plant type and the fuel type in
21 use at the plant.
22
- 23 2. Parameter uncertainties used in the 95/95 DNBR limit calculation must be justified on a
24 plant-specific basis.
25
- 26 3. The DNBR distribution used to determine the statistical DNBR limit shall be based on a
27 minimum of [] samples from the operating space.
28
- 29 4. The use of an approved subchannel code (e.g., VIPRE-W) in lieu of CETOP-D must be
30 consistent with the CE-NSSS setpoint methodology as defined in WCAP-16500-P-A,
31 Supplement 1, "Application of CE Setpoint Methodology for CE 16x16 Next Generation
32 Fuel," Revision 1 (Ref. 14).

33 5.0 CONCLUSIONS

34 The NRC staff concluded that the WTDP methodology described in WCAP-18240-P/WCAP-
35 18240-NP, Revision 0, "Westinghouse Thermal Design Procedure (WTDP)," describes an
36 acceptable methodology for determining a DNBR limit that provides assurance at a 95-percent
37 probability and 95-percent confidence level that the hot rod in the core will not experience DNB
38 during normal operation or AOs. The limit derived from the WTDP analysis adequately
39 accounts for the appropriate plant uncertainties and will be applicable across the allowable
40 operating space of the plant. For accidents in which some fuel damage is anticipated, WTDP's
41 rods-in-DNB method provides an acceptable method for evaluating the number of fuel rods that
42 would be expected to experience damage due to DNB.

- 13 -

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