

UNITED STATES NUCLEAR REGULATORY COMMISSION ADVISORY COMMITTEE ON REACTOR SAFEGUARDS WASHINGTON, D. C. 20555

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ACRS Members ACRS Staff

SUMMARY OF REACTOR COOLANT RELIEF SYSTEMS IN OPERATING U.S. LWRs

Based on previous operating history, the probability of a small break LOCA due to activation of a power-operated relief valve (with its block valve open) is 0.1 per reactor year for B&W PWRs (NUREG-0560). Sixty inadvertent blowdowns have occurred in BWRs. The BWR main steam pressure relief systems do not have block valves. This report contains a general description and operating history of these systems.

John G. Stampelos ACRS Fellow

Attachments:

 Summary of PWR Pressurizer Relief Systems

2. Summary of BWR Main Steam Relief Systems

cc: ACRS Fellows

SUMMARY OF PWR PRESSURIZER RELIEF SYSTEMS

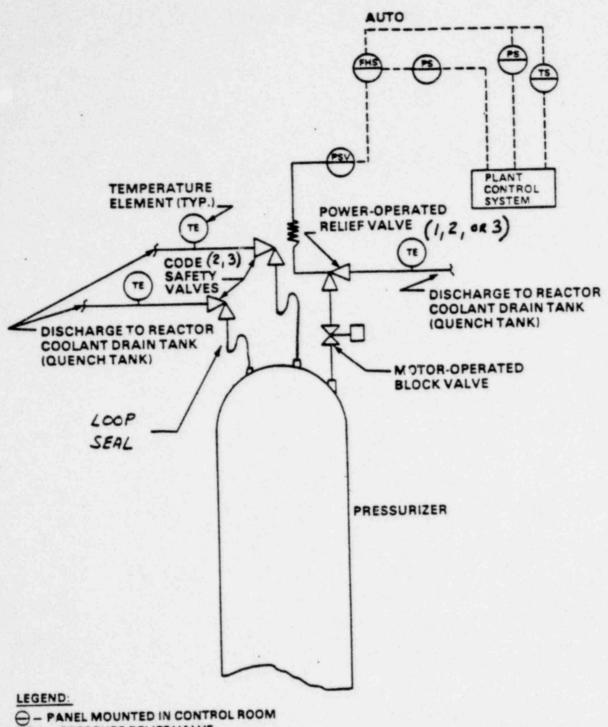
The pressurizer pressure relief system (Figure 1) consists of from two to three spring-loaded backpressure compensated safety valves (Figure 2) and up to three (generally one or two) power-operated relief valves (Figure 3). The safety valves are required for overpressure protection by the ASME Boiler and Pressure Vessel Code. The power-operated relief valve does not contribute to the required relieving capacity of the reactor system but enhances plant availability. The power-operated relief valves limit the lifting frequency of the safety valves and are used to provide overpressure protection during operation at low temperatures. The setpoint of the safety valve is nominally 2500 psig. The setpoint of the power-operated relief valve is nominally 2450 psig.

The safety valves (Figure 2) operate against the force of spring pressure. A water loop seal is provided to minimize valve leakage. The poweroperated relief valve (Figure 3) is a pilot-operated valve. This valve can be operated either manually or automatically by a mode selection switch located in the control room. Reactor coolant system pressure from chamber I (in Figure 3) leaks pass the valve disc guide into chambers II, III, and IV. The valve disc (#2) is held shut by this pressure and the force of the valve spring (#4). When actuated, the solenoid lifts the pilot valve disk (#13) which vents the reactor coolant system pressure in chamber II through chamber IV and into the atmosphere. The main valve disc (#2) moves down and opens. A block valve is provided upstream of the power-operated relief valves in case of failure. Leakage of the power-operated relief valves may be indicated by temperature detection on the valves exhaust pipe, valve position indication detectors, and quench tank level and pressure. The position indicator only indicates whether the solenoid is energized. The safety valves do not have block valves.

The operating history of the spring-loaded safety valves has been unremarkable. The history of the power-operated relief valves is summarized in NUREG-0560 for B&W plants (Table 1). A review (NUREG-0560) of the LERs dealing with feedwater types of transients has indicated that three events have occurred in B&W plants in which these valves have stuck open. There has been about 150 occasions in which pressurizer relief valves have actuated in B&W plants yielding a failure rate of 2 x 10^{-2} per event and a probability of a small break LOCA of about 0.1 per reactor-year if the block valve is not closed. The control circuits for relief valves are currently not single failure proof. A single failure in the control circuits can result in a small break LOCA.

The setpoint pressure of power-operated relief valves has been changed from 2255 psig to 2450 psig because of TMI-2. This should reduce the actuation rate of these valves. The setpoint for the other vendors was around 2450 psig before the TMI-2 experience. The reactor trip setpoint varies from 2300 psig to 2385 psig depending on the vendor.

Attachments: As stated



PSV - PRESSURE RELIEF VALVE

FHS - FLOW HAND-ACTUATED SWITCH

PS - PRESSURE SWITCH

TE - TEMPERATURE ELEMENT

TS - TEMPERATURE SWITCH

ADAPTED FROM NUREG-0560

FIGURE 1: TYPICAL PWR PRESSURIZER PRESSURE RELIEF SYSTEM

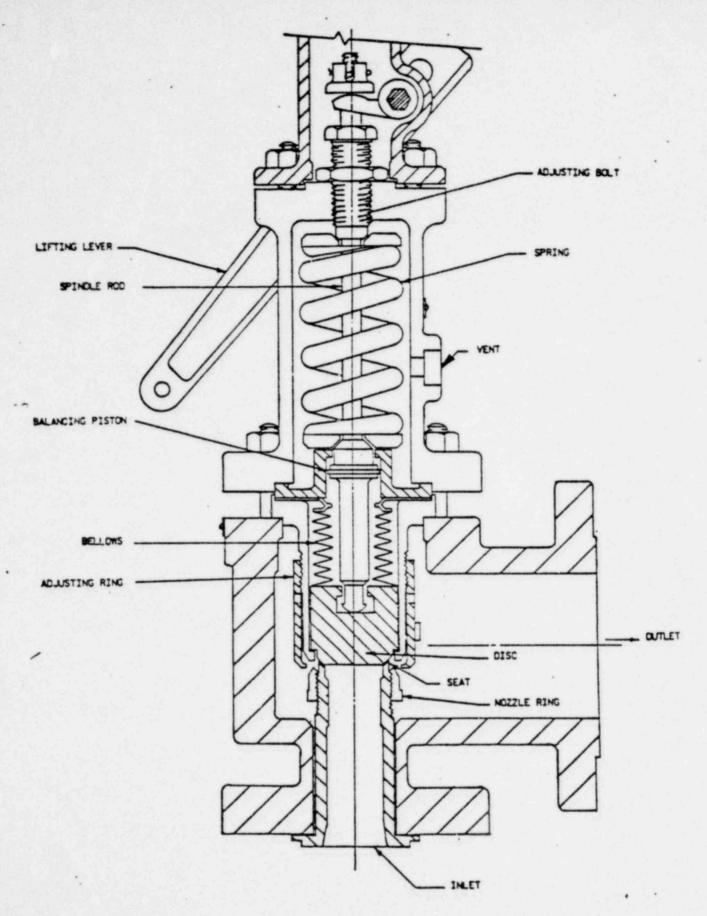
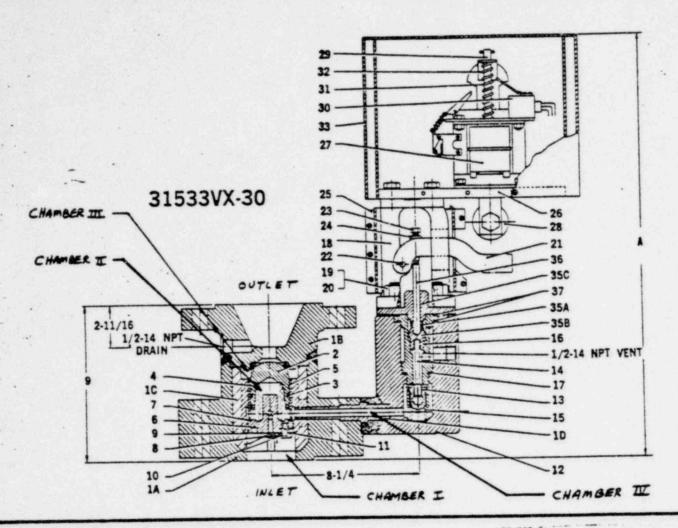


FIGURE 2: TYPICAL PRESSURIZER SPRING- LOADED SAFETY VALVE

ELECTROMATIC Reliety Valves



| PART NO. | ERIALS | PART NO. | MATERIALS |
|---|---|--|---|
| 1 Base Assembly 1A Lower Base 1B Top Flange 1C Cage 1D Tube Insert 2 Disc 3 Piston Ring 4 Disc Spring 5 Guide 6 Guide Retaining Plug 7 Guide Gasket 8 Lock Screw 9 Lockscrew Lockwasher 0 Retaining Lockscrew 1 Retaining Screw Lockwasher 2 Pilot Base 3 Pilot Disc 5 Pilot Disc Spring 6 Pilot Disc Spring 6 Pilot Disc Bushing 7 Seat Bushing Gasket 8 Solendid Bracket 9 Bracket Stud | ASME SA182 F316, Stainless Steel ASME SA182 F316, Stainless Steel ASTM A351 CA15 CF8M ASME SA182 F316, Stainless Steel ASTM A565 Gr. 616, Stainless Steel, Condition T A1S1 420, Hardened Stainless Steel, Condition T A1S1 420, Hardened Stainless Steel AISI 304, Stainless Steel AISI 304, Stainless Steel AISI 410, Stainless Steel AISI 304, Stainless Steel ASTM A565 Gr. 616, Stainless Steel ASTM A565 Gr. 616, Stainless Steel Inconel X-750 ASME S8186 AISI 304, Asbestos ASTM A216 WCB, Csrbon Steel (Cadmium Plated) ASME SA193 Gr. 816 | 20 Bracket Stud Nut 21 Lever 22 Lever Pin 23 Adjusting Screw 24 Locknut 25 Bracket Cover 26 Solenoid Plate 27 Solenoid Plate 28 Solenoid Plunger Head 29 Plunger Assembly Guide Plate Spring Guide 30 Unimax Switch 31 Plunger Spring 32 Soring Bracket 33 Solenoid Cover 34 Spring Cover 34 Spring Cover 35 Bellows Assembly 35A Bellows Piston 35C Bellows Flange 36 Upper Spindle 37 Upper Seat Bushing Gaskets | ASME SA194 Gr. 4 ASTM A216 WCB. Carbon Steel, (Zinc Plated Carbon Steel (Cadmium Plated) AISI 416. Stainless Steel, (Zinc Plated) Carbon Steel, (Zinc Plated) AISI 302. Stainless Steel AISI C1019, (Zinc Plated) Carbon Steel, (Zinc Plated) Carbon Steel, (Zinc Plated) ASTM AA79 TP 430 Brass Tube KBL-7-MB5 24 Ga. Munic Wire. (Cadmium Plated) Carbon Steel, (Zinc Plated) Carbon Steel, (Zinc Plated) AM 350 Stainless Steel ASSME SAA79 Gr. 316L, Stainless Steel ASTM A365, Gr. 316L, Stainless Steel |

FIGURE 3: TYPICAL PWR PRESSURIZER
POWER-OPERATED RELIEF VALVE

ROOR ORIGINAL

RELIEF VALVES ON PRESSURIZER FOR BAW PLANTS

| Valves for B&W Plants | Arkansas 1 | Crystal River 3 | Davis- Besse 1 | Oconee 1 | Oconee 2 | Oconee 3 | Rancho Seco | Three Mile Island 1 | Three Hile Island 2 |
|---|---|--|---|--|----------|---|--|--|--------------------------|
| Code Safety- Relief Valves Mfg Number Type Model no. | Dresser 2 Spring-loaded 3-31759A | Dresser Spring-loaded 24 - 31739A | Crosby 2 Spring-loaded 3XM1X6, | Dresser 2 Spring-loaded 2½ -31739A | Same | Dresser 2 Spring-loaded 24-31739A | Dresser 2 same | Dresser 2 Spring-loaded 24-31739A | Same |
| Size Relief cap. | 3" x 6" 311,733 #/hr 2500 psig | 24" x 6" 311,733 #hr 2500 psig | Type H886 4" x 6" | 24" x 6" 311,973 #/hr 2500 psig | | 25" x 6" 317,973 #/hr 2500 psig | | 24" x 6" 280,000 #/hr 2500 psig | |
| Set press. Reseat press. (approx.) Known malf. (significant) | 2375 None | 2375 None | None | 2375 None | | 2375 None | | 2450 None | 2475 None |
| Power-Operated Relief valves Rfg | Dresser | Dresser | Crosby | Dresser | Same | Dresser 1 | Dresser 1 | Oresser | Same |
| Number Type Model no. Size Relief cap. | 1 Electromatic 31533VX-30 25" x 4" 106,450 #/hr | Electromatic Same | Electromatic HPV-ST 25" x 4" 112,000 #/hr 2235 psig # | Electrometic 31533 VX-30 25" x 4" 100,000 #/hr 2300 psig x | | 51ectromatic 31533VX-30 25" x 4" 100,000 9/hr 2300 psig * | 112,000 #/hr | 31533VX-30 24" x 4" 106,450 #/hr 2300 psig ** | |
| # Set press. Reseat press. Half. date | 2300 psig ** 9/1/74 | None | 9/24/77 | None | None | 2220 ps 1g June 1975 | June 1978 | 2250 psig None | 3/29/78 |
| (significant) cause | Improper venting | | Steam pilot valve system | | | Boric acid crystal buildu bent lever on pilot valve | Valve leakage | | De-energized · vital bus |
| Fail position | Closed (Class 1E) | Closed (1E) | Closed (non- | Closed (non- | | | Closed (non-1E) | | |
| Position Ind. | Yes (Pilot- red/green) | Yes (open- closed) | Yes (on pilot- red/green lights) | Yes (open- closed) | | | No | Pilot-red green | |
| Thermocouple ind. | Yes (computer) | Yes (computer) | | Yes (computer) | | | Yes (computer |) Yes | |
| and alarm Thermocouple type, and location | Strap-on | Well/~50 ft from valve | Strap-on/ ~1 ft | Strap-on/6 7 ft downstrea | | | Strap-on/40 f from valve | • | |
| Block Valve Hfg. Type Fail position Pos. indication | Velan Motor-operated As-is (non-1E) Yes | Dresser Motor-operated As-is (IE) Yes | Valan Hotor-operated As-is (non-1E) Yes | Westinghouse Motor-operated As-is (non-1E) Yes | Same | Same | Velan Motor-operate As-is (non-1E Yes | d Motor-operated) - Yes | I Same |

SOURCE: NUREG 0560

* SETPOINT PRESSURE RAISED FROM 2255 psig To 2450 psig by I'E BULLETIN 79-058

SUMMARY OF BWR MAIN STEAM RELIEF SYSTEMS

The main steam pressure relief system (Table 1) for U.S. BWRs include a total combination of from 6 to 22 safety/relief valves (SRVs), spring-loaded safety valves (SVs), and/or power actuated relief valves (PARVs).

Valve Setpoints

spring-loaded safety valves (SVs)

1225 psig

2. power actuated relief valves (PARVs)

1130 psig

safety/relief valves (SRVs)

1025-1155 psig*

* depends on the plant and the total number of valves employed in the system

A specific number of PARVs or SRVs, in addition to providing overpressure protection, are utilized in the automatic depressurization system (ADS). The ADS is part of the Emergency Core Cooling System. Generally, the ADS is actuated on the simultaneous receipt of a high drywell pressure, reactor vessel low water level, and indication of output pressure from one low pressure core injection or core spray pump signal.

Most SVs discharge directly to the containment drywell whereas the PARVs and the SRVs discharge to the suppression pool. The pressure relief system valves do not have blocking valves. The safety valves (Table 1) are required to provide overpressure protection by the ASME Boiler & Pressure Vessel Code. The relief system valves have leakage indication and alarms via temperature monitoring devices located near the valve exhaust tail pipes. The older design SRVs have a bellows leakage alarm for their pilot stage.

A typical spring-loaded SV (Figure 1) actuates when reactor coolant pressure exceeds the spring pressure. A typical PARV is shown in Figure 2. Main steam in chamber A passes upward around the disk guide into chamber B. In addition, main steam normally pressurizes chamber C via a clearance space between the main valve disc and disc guide. The main valve spring and the steam pressure in chamber C hold the main valve disc shut. PARV actuation is accomplished by energizing the solenoid in the pilot valve which vents the steam in chamber C to the atmosphere. The subsequent differential pressure (between chamber C and chamber B) forces the main valve disc to drop down and open the valve.

The SRVs are typically of two designs. Most BWR plants employ the older 3-stage SRV design (Figure 3). The main valve disk is held in the closed position by the force of the main valve preload spring and main steam pressure acting on the main valve piston (the chamber behind the main valve piston is pressurized through the main valve piston orifice). The main valve disc opens when the second stage piston moves down allowing main steam pressure to bleed from behind the main valve piston. The second stage piston moves down when main behind the main valve piston. The second stage piston disc to the right steam pressure is sufficient to move the pilot stage piston disc to the right and pressurize the chamber immediately above the second stage piston. This and pressurize the chamber immediately above the second stage piston. This are stage SRV has had a significant number of inadvertent blowdown events (Table 2 and Table 5).

The major cause of spurious openings or failures of the 3-stage SRV to reseat has been excessive pilot valve leakage. The principal strategy to assure that pilot leakage is minimized involves increasing the simmer margin, performing more frequent valve maintenance, and replacement with the new 2-stage SRV design. (The simmer margin is the differential pressure between normal system operating pressure and the valve setpoint.) The new 2-stage design (Figure 4) has an improved pilot section design and no second stage piston.

As of April 12, 1979, twenty 3-stage valves have been replaced with the new 2-stage design and ten more are committed to be replaced. Hatch Unit 1, Fitzpatrick, and two of the reactors at Browns Ferry have replaced some of their 3-stage valves with the new design. There have been no inadvertent blowdowns to date with the new 2-stage design. In addition to the mechanical failures associated with the 3-stage valves, several failures of the pneumatic diaphragm operator have occurred. Excessive heating caused by extended service life and improper thermal insulation were the cause. Yearly diaphragm replacement should correct the problem.

The NRC, as part of its continuing program for monitoring safety/relief valve performance, has requested all BWR licensees to provide an operations and maintenance history for each of their safety/relief valves manufactured by Target Rock Corp. The response of the licensees is due September 16, 1979.

Attachments: As stated

TABLE 1

| | | VALVE COMPLEMENT | | | | | | | | | |
|-------------|-----------------|----------------------|-----|---------------------------------|--|--|--|--|--|--|--|
| BWR TYPE | FACILITY | SAFETY/RELIEF VALVES | | POWER-ACTUATED RELIEF VALVES | | | | | | | |
| 2 | Nine Mile Point | | 16 | 6 | | | | | | | |
| 2 | Oyster Creek | | 16 | 5 | | | | | | | |
| 3 | Dresden 2 | 1 | 8 | 4 | | | | | | | |
| 3 | Dresden 3 | 1 | 8 | 4 | | | | | | | |
| 3 | Millstone 1 | 6 | - | • | | | | | | | |
| 3 | Monticello | 7 | - | • | | | | | | | |
| 3 | Pilgrim 1 | 4 | 2 | | | | | | | | |
| 3 | Quad Cities 1 | 1 | 8 | 4 | | | | | | | |
| 3 | Quad Cities 2 | 1 | . 8 | 4 | | | | | | | |
| 4 | Browns Ferry 1 | 11 | 2 | | | | | | | | |
| 4 | Browns Ferry 2 | 11 | 2 | | | | | | | | |
| 4 | Browns Ferry 3 | 11 | 2 | • | | | | | | | |
| 4 | Brunswick 1 | 11 | • | • | | | | | | | |
| 4 | Brunswick 2 | 11 | - | • | | | | | | | |
| 4 | Cooper | 8 | 3 | • | | | | | | | |
| 4 | Duane Arnold | 6 | 2 | • | | | | | | | |
| 4 | Fitzpatrick | 11 | | • | | | | | | | |
| 4 | Hatch 1 | 11 | • | - | | | | | | | |
| 4 | Peach Bottom | 2 11 | . 2 | • | | | | | | | |
| 4 | Peach Bottom | 3 11 | 2 | • | | | | | | | |
| 4 | Vermont Yanke | e 4 | .2 | • | | | | | | | |
| | | | | | | | | | | | |

SOURCE : NUREG - 0462

TABLE 2 Inadvertent Blowdowns Events

| | | Ī | nadver | | | INS EVE | | 1976 | 1977 | 1978 | 1979 | TOTA | 4 |
|-----------------|------|------|--------|------|-----------|---------|------|------|------|------|------|------|----|
| | 1969 | 1970 | 1971 | 1972 | 1973 | 1974 | 19/5 | | 2 | | | 5 | |
| ns Ferry 1 | | | | | _ | - | 1 | - | +- | 2 | | 5 | |
| ns Ferry 2 | | | | | - | 2 | +- | - | + | 3 | 1 | 3 | |
| vns Ferry 3 | | | | - | - | +- | + | + | + | 1 | 1 | 2 | |
| nswick 1 | | | | 1 | - | + | 1 2 | + | 1 | 1 | | 4 | |
| wnswick 2 | | | 1- | - | +- | 1 4 | +- | + | 1 | | | 4 | 1 |
| per | | _ | - | - | + | + | + | + | 1 | | | 1 | |
| esden 2 | | 1 | - | - | + | | + | + | | | | 1 | _ |
| esden 3 | | 1 | - | + | + | - | + | 1 | | | | 1 | |
| ane Arnold | | - | - | + | + | + | 1 | 1 | 3 | | | 13 | |
| itzpatrick | | - | - | - | + | + | 1 | 1 | 1 | 3 | 1 | _ | 5 |
| atch 1 | | - | | + | + | - | 1 | 1 | | 1 | 1 | 1 | 5_ |
| illstone 1 | 1 | - | - | 1 | 1 | - | _ | 1 | | | 2 | _ | 4 |
| Monticello | | | - | 1 | $\dot{+}$ | 1+ | _ | 1 | | | | _ | 1 |
| vine Mile Pt. 1 | | 1 | | - | 1* | -+ | - | | | | | | 1 |
| Oyster Creek | | | - | -+ | -+ | - | 3 | 1 | 2 | 1 | | | 7 |
| Peach Bottom 2 | | _ | | - | - | | 1 | | 2 | | | 1 | 3 |
| Peach Bottom 3 | | | | | 2 | 1 | | 1 | | | 1 | | 5 |
| Pilgrim 1 | | | | - | - | - | | | | | | | 1 |
| Quad Cities 1 | | | | | | - | | | | 2* | | _ | 12 |
| Quad Cities 2 | | 1111 | | | | + | 1 | | 1 | | 1 | 1 | + |
| Vermont Yanke | e | | 0 | 2 | 4 | 2 | 111 | 8 | 10 | 10 | 10 | 3 | 1 |

SOURCE: NUREG-0462 (JULY 1978), UPDATED TO JULY 1979

TABLE 3
Failures to Open Properly on Demand

| | 1969 | 1970 | 1971 | 1972 | 1973 | 1974 | 1975 | 1976 | 1977 | 1978 | 1979 | TOTAL |
|-----------------|------|------|------|------|------|------|------|------|------|------|------|-------|
| Frowns Ferry 1 | | | | | | | | | | | | |
| Browns Ferry 2 | | | | | 118 | | | | | | | |
| Browns Ferry 3 | | | H | 1114 | | | | | | | | |
| Brunswick 1 | | | | | | | | | | | | |
| Brunswick 2 | | | | | | | | | | | - | |
| Cooper | | | | | | | | | | | | |
| Dresden 2 | | 3* | | | | | 2* | | 1* | | | 6 |
| Dresden 3 | 1000 | | | | 1* | 1* | | | | | | 2 |
| Duane Arnold | | | | | | 1 | | | | | | 1 |
| Fitzpatrick | | | | | | | | | | | | |
| Hatch 1 | | | | | | | | | 2 | | | 2 |
| Millstone 1 | | | | | | | | | | | | _ |
| Monticello | | | | 2 | | | | 1 | | | | 3 |
| Nine Mile Point | 1* | | | | | | | | | | | 1 |
| Oyster Creek | | | | | 1* | | | | 1* | | - | 2 |
| Peach Bottom 2 | | | | | | 1 | | | | | | 1 |
| Peach Bottom 3 | | | | | 1 | | | | | | | _ |
| Pilgrim 1 | | | | | | | | | 2 | | | 2 |
| Quad Cities 1 | | | | | | | | 1. | 1* | 2* | | 4 |
| Quad Cities 2 | | | | | | | | 1. | 2* | 1 | | 1 4 |
| Vermont Yankee | | | | | | 1 | | 1 | | | | 2 |
| TOTAL | 1 | 3 | 0 | 2 | 2 | 4 | 2 | 4 | 9 | 3 | | |

^{*}Power Actuated Relief Valve

SOURCE: NUREG-0462 (JULY 1978), UPDATED TO JULY 1979

TABLE 4
Potential Failures to Open Properly

| | 1969 | 1970 | 1971 | 1972 | 1973 | 1974 | 1975 | 1976 | 1977 | 1978 | 1977 | TOTAL |
|-----------------|------|------|------|------|------|------|------|------|----------|------|-------|-------|
| rowns Ferry 1 | | | | | 1 | | | | | | | 1 |
| rowns Ferry 2 | | | | | | | | | | | | |
| Browns Ferry 3 | | | | | | | | | | | | |
| Brunswick 1 | | | | | | | | | | | | |
| Brunswick 2 | 1000 | | | | | | 1 | | | | 1 | 2 |
| Cooper | | | | | | | 1 | 1 | <u>.</u> | _ | | 2 |
| Dresden 2 | | | | | | | | | | | - | |
| Dresden 3 | | | | | | | | | | _ | | |
| Duane Arnold | | | | | | | | 1 | 1 | 1 | _ | 2 |
| Fitzpatrick | | | | | | | | 1 | | 1 | 1 | 11 |
| Hatch 1 | | 1 | | | | | | 1 | 1 | 1_ | 1 | 2 |
| Millstone 1 | | | | | | | 1 | | 1 | - | 1 | 2 |
| Monticello | | | | | | | | | | 1 | | |
| Nine Mile Point | | | | | | | | | 1* | 1 | 1 | 1 |
| Oyster Creek | | | | | | | | | | 1 | | 4 |
| Peach Bottom 2 | | | | | 1 | 2 | | | 1 | | | 4 |
| Peach Bottom 3 | | | | | 1. | | | | | | 1 | 1 |
| Pilgrim 1 | | | | | | | | | | 1 | | + |
| Quad Cities 1 | | | | | | | | | | - | - | + |
| Quad Cities 2 | | | | | | | | 1 | | - | 4. | 1 |
| Vermont Yankee | | | | 2 | | | | 1 | | 1 | | 14 |
| TOTAL . | 0 | 0 | 0 | 2 | 2 | 2 | 3 | 3 | 4 | 1.2 | - 4 | 1 |

^{*}Power Actuated Relief Valve

SOURCE: NUREG - 0462 (JULY 1978), UPDATED TO JULY 1979

TABLE 5

| Event Type | Safety | Relief Vavles | Power Actuated Pressure Relief Valves | Total |
|----------------------------------|--------|---------------|--|-------|
| Inadvertent Blowdowns | | 56 | 4 | 60 |
| Failures to Open | | 12 | 18 | 30 |
| Potential Failures to Open | | 21 | 1 | 22 |

NOTE: SPRING-LOADED SAFETY VALVES (SUS)

ARE NOT INCLUDED IN THIS TABLE

BECAUSE THEIR OPERATING HISTORY

HAS BEEN RELATIVELY GOOD.

· SOURCE: NUREG - 0462 (JULY 1978), UPDATED TO JULY 1979

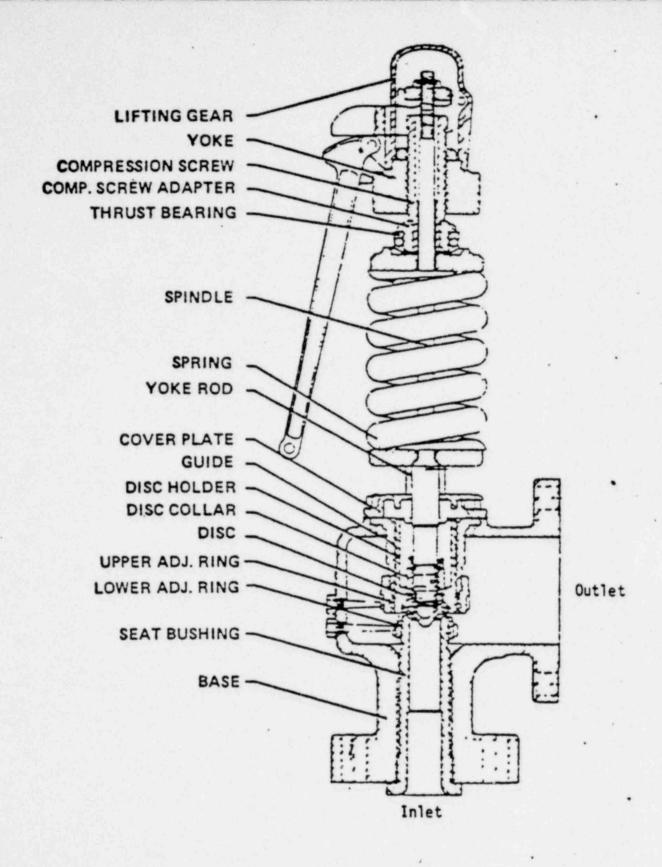
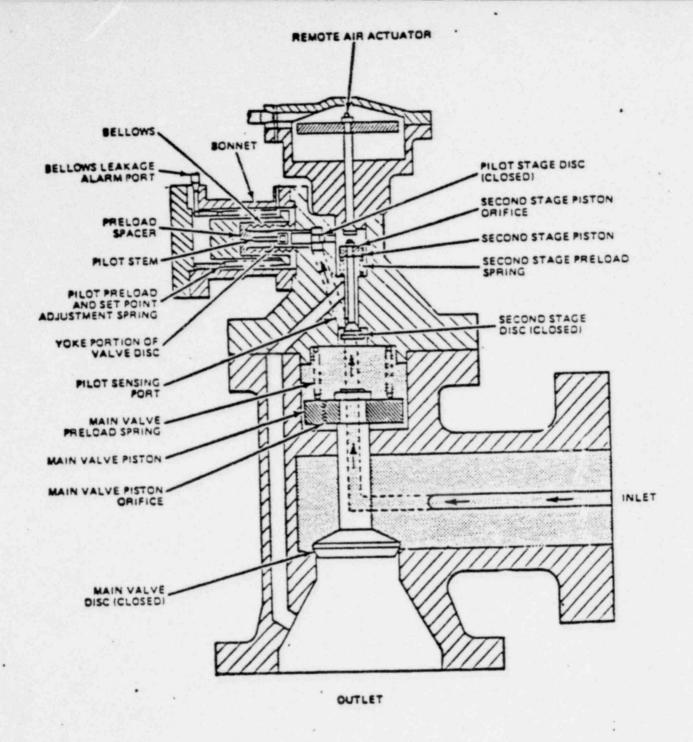


FIGURE 1: TYPICAL BWR SAFETY VALVE

SOURCE : NUREG-0462

VALVE (PARV) RELIEF ACTUATED POWER BWR TYPICAL FIGURE Z:

SOURCE : NUREG-0462



HIGH PRESSURE

FIGURE 3: 3-STAGE SAFETY/RELIEF
VALUE SCHEMATIC (SRV)

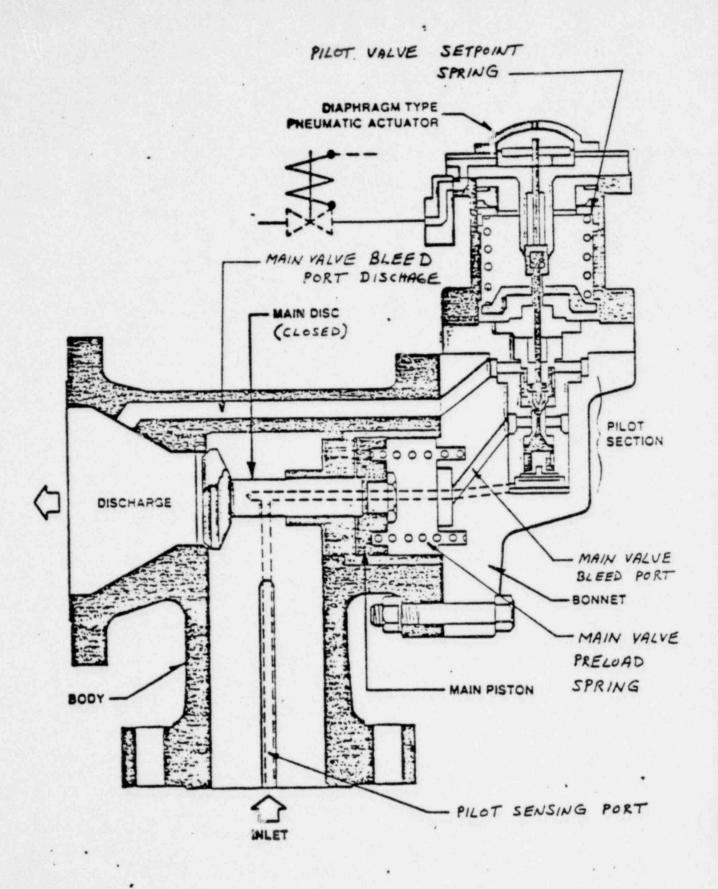


FIGURE 4: 2-STAGE SAFETY/RELIEF