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S. V. TASHJIAN

SAN ONOFRE UNITS 2 AND 3
DOCKETS 50-361 AND 362

SLIDES DEPICTING STRUCTURAL ANALYSIS METHODS TESTING,
PROPERTIES AND ANALYSIS AND TEST RESULTS FOR THE C-E
16X16 FUEL ASSEMBLY FOR SAN ONOFRE UNITS 2 AND 3.

NON-PROPRIETARY VERSION

PRESENTATION TO NRC ON DECEMBER 14, 1978.

COMBUSTION ENGINEERING, INC.
NUCLEAR POWER SYSTEMS
POWER SYSTEMS GROUP
WINDSOR, CONNECTICUT

790202 0269

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I. INTRODUCTION

II. TECHNICAL PRESENTATION

A. DESIGN DESCRIPTION

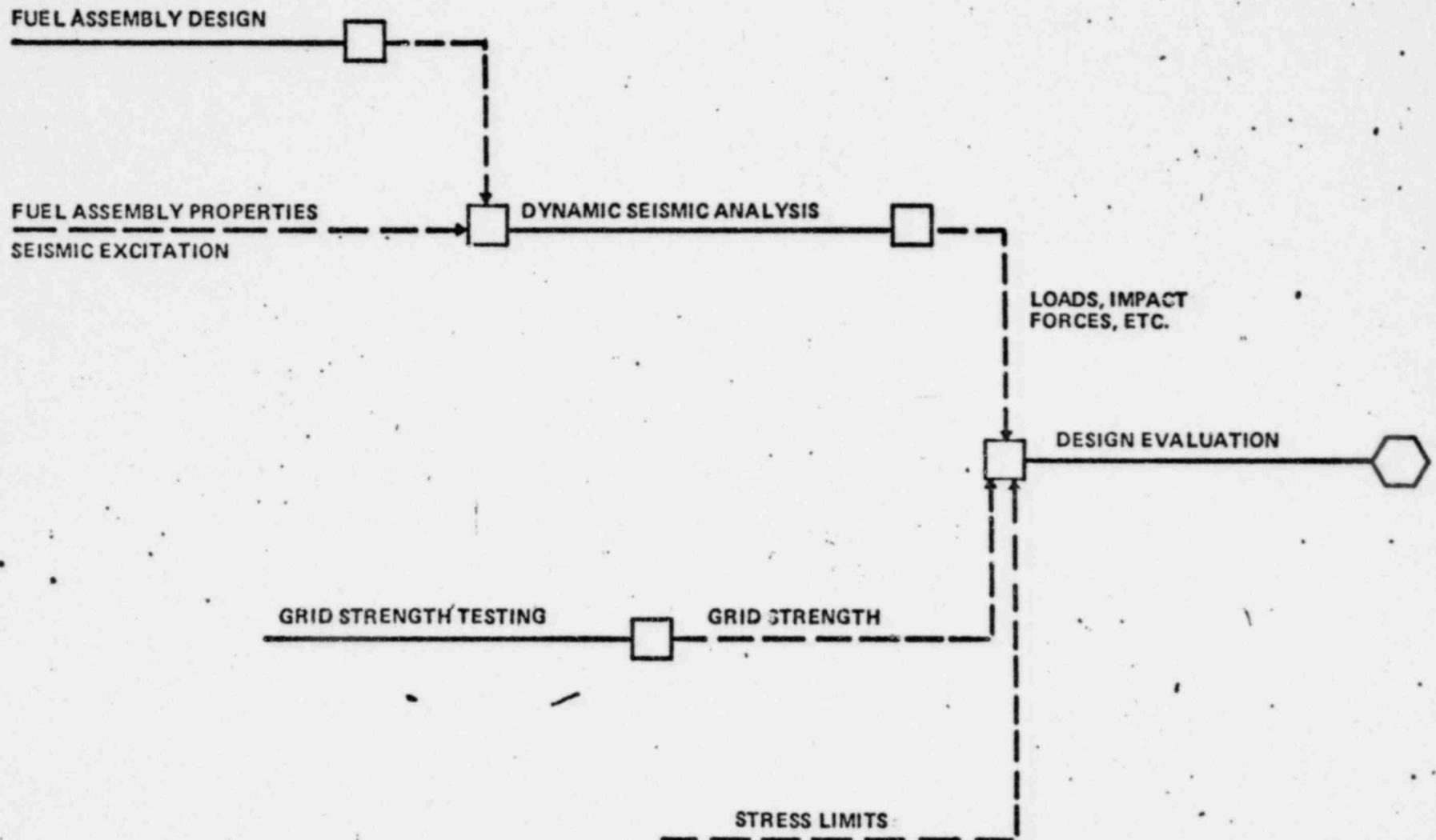
B. ANALYSIS

C. TEST

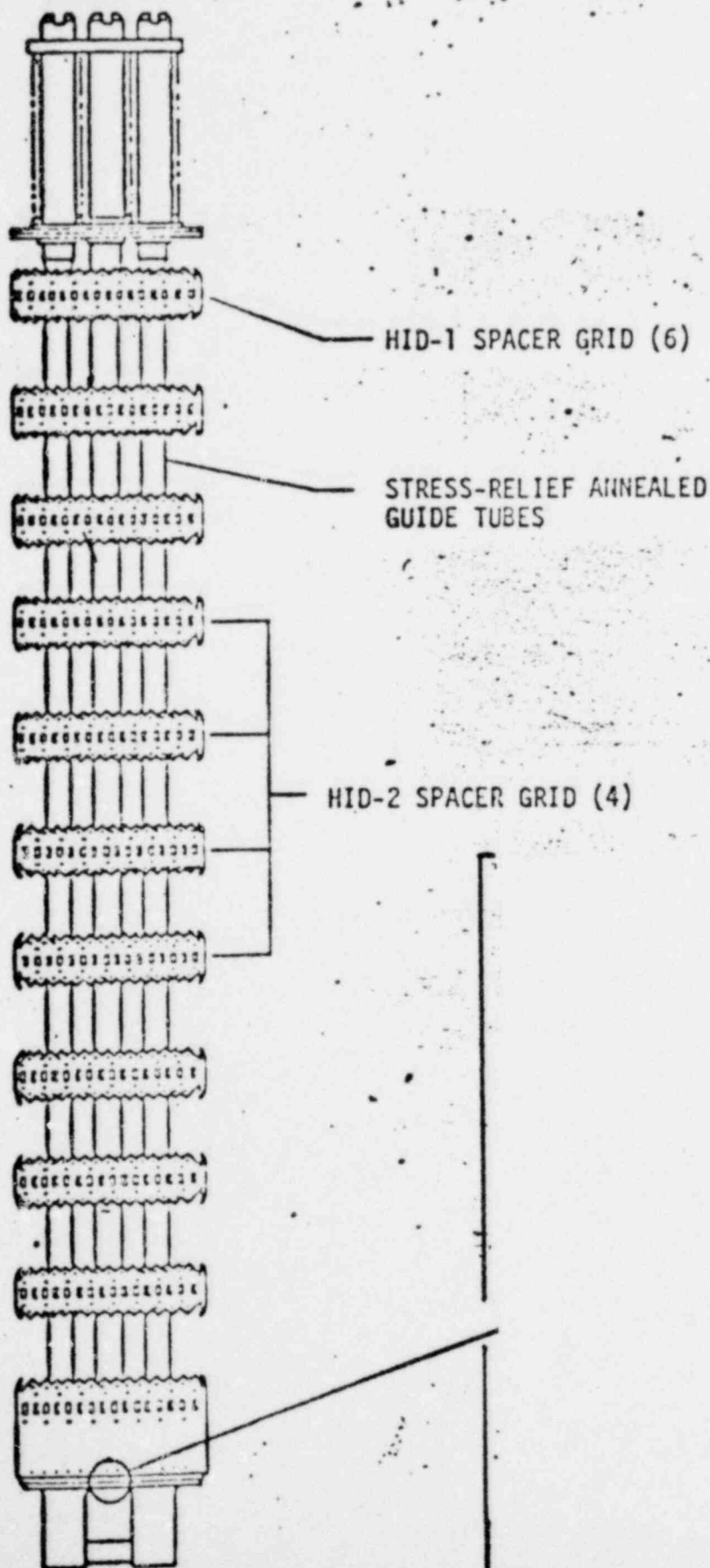
D. DESIGN EVALUATION

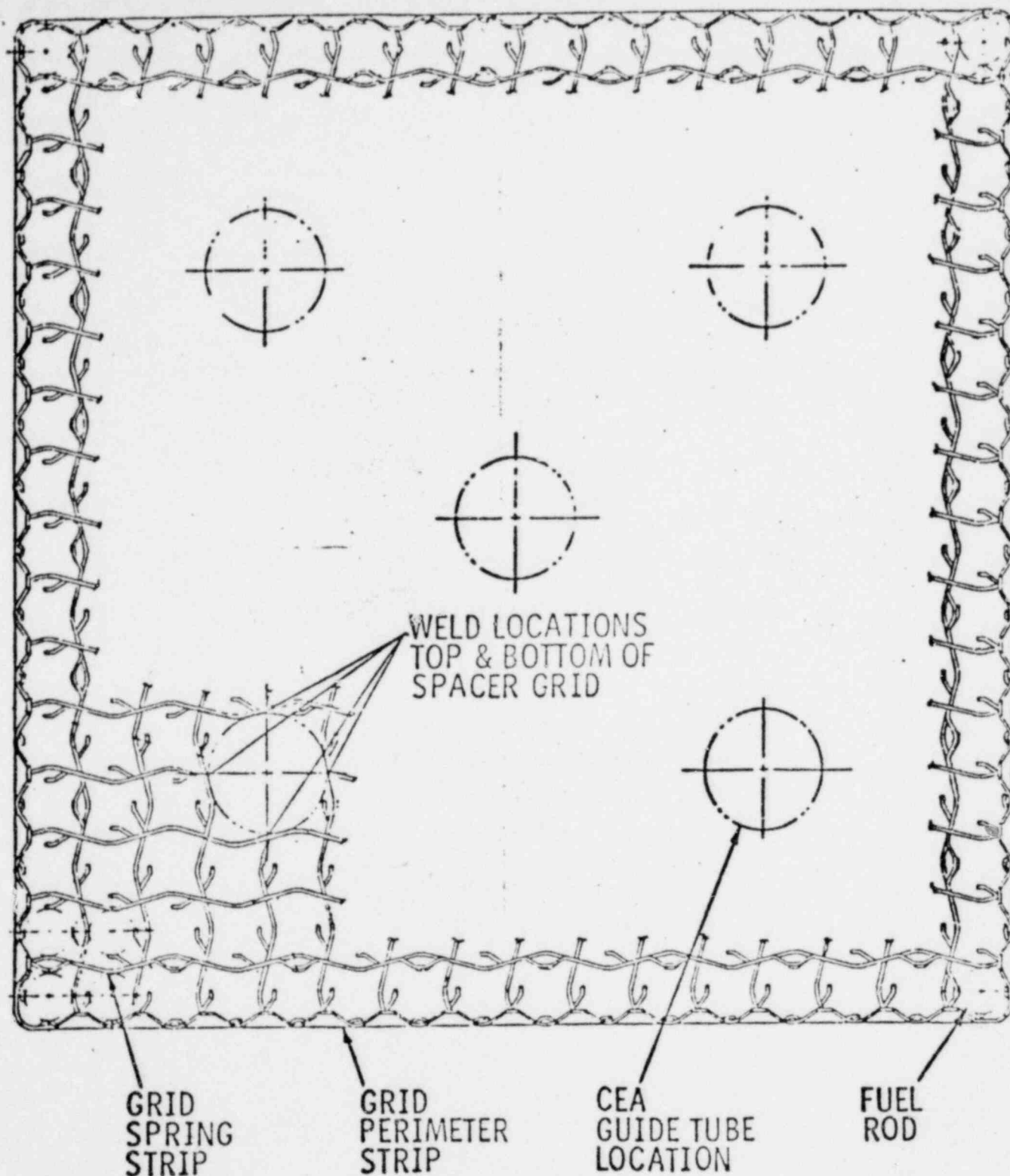
III. DISCUSSION

FUEL SEISMIC DESIGN PROCESS



SONGS-II FUEL ASSEMBLY
SEISMIC DESIGN FEATURES





SAN ONOFRE NUCLEAR GENERATING STATION Units 2 & 3
FUEL SPACER GRID

CESHOCK

- DYNAMIC RESPONSE OF MULTI-SPRING/MASS SYSTEMS
- AXIAL/LATERAL MODEL CAPABILITIES
- PRELOADS, TENSION-AND COMPRESSION-ONLY SPRINGS, AND NONLINEAR SPRINGS
- GAPS, IMPACT, COEFFICIENT OF RESTITUTION
- $\alpha - \beta$ DAMPING
- HYDRODYNAMIC MASS MATRIX
- ARBITRARY TIME DEPENDENT EXTERNAL LOADS
- NUMERICAL INTEGRATION TECHNIQUES: RUNGE-KUTTA-GILL AND NEWMARK
- OUTPUT: DISPLACEMENT, VELOCITY, ACCELERATION, FORCE, SHEAR, IMPACT LOAD AND MOMENT TIME HISTORIES

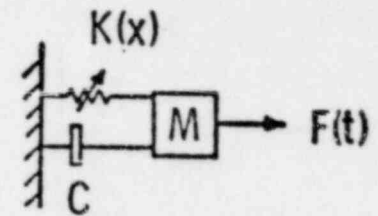
SUMMARY OF THE METHODS EMPLOYED TO VERIFY THE CESHOCK CODE

<u>TYPE OF CESHOCK PROBLEM</u>	<u>METHOD OF VERIFICATION</u>
I. NONLINEAR, DAMPED PULSE EXCITED SYSTEM	PUBLISHED CLASSICAL SOLUTION
A. DEGREE OF NONLINEARITY VARIED (DUFFING OSCILLATOR)	
B. TYPE OF PULSE VARIED	
II. MULTI-DEGREE OF FREEDOM BASE EXCITED LATERAL SYSTEM WITH FRICTION, GAPS, AND DAMPING	INDEPENDENT COMPUTER CODE
A. WITHOUT HYDRODYNAMIC MASS	
B. WITH HYDRODYNAMIC MASS	
III. FRICTION ELEMENT WITH STATIC AND DYNAMIC COEFFICIENTS OF FRICTION	ANALYTICAL SOLUTION
A. COEFFICIENT OF FRICTION VELOCITY NON-DEPENDENT	
B. COEFFICIENT OF FRICTION VELOCITY DEPENDENT	
IV. IMPACT ELEMENT WITH COEFFICIENT OF RESTITUTION	ANALYTICAL SOLUTION
V. HYSTERESIS ELEMENT:	INDEPENDENT COMPUTER CODE
TWO DOF SYSTEM WITH SPRING AND GAP ELEMENTS	

NONLINEAR, DAMPED PULSE EXCITED SYSTEM

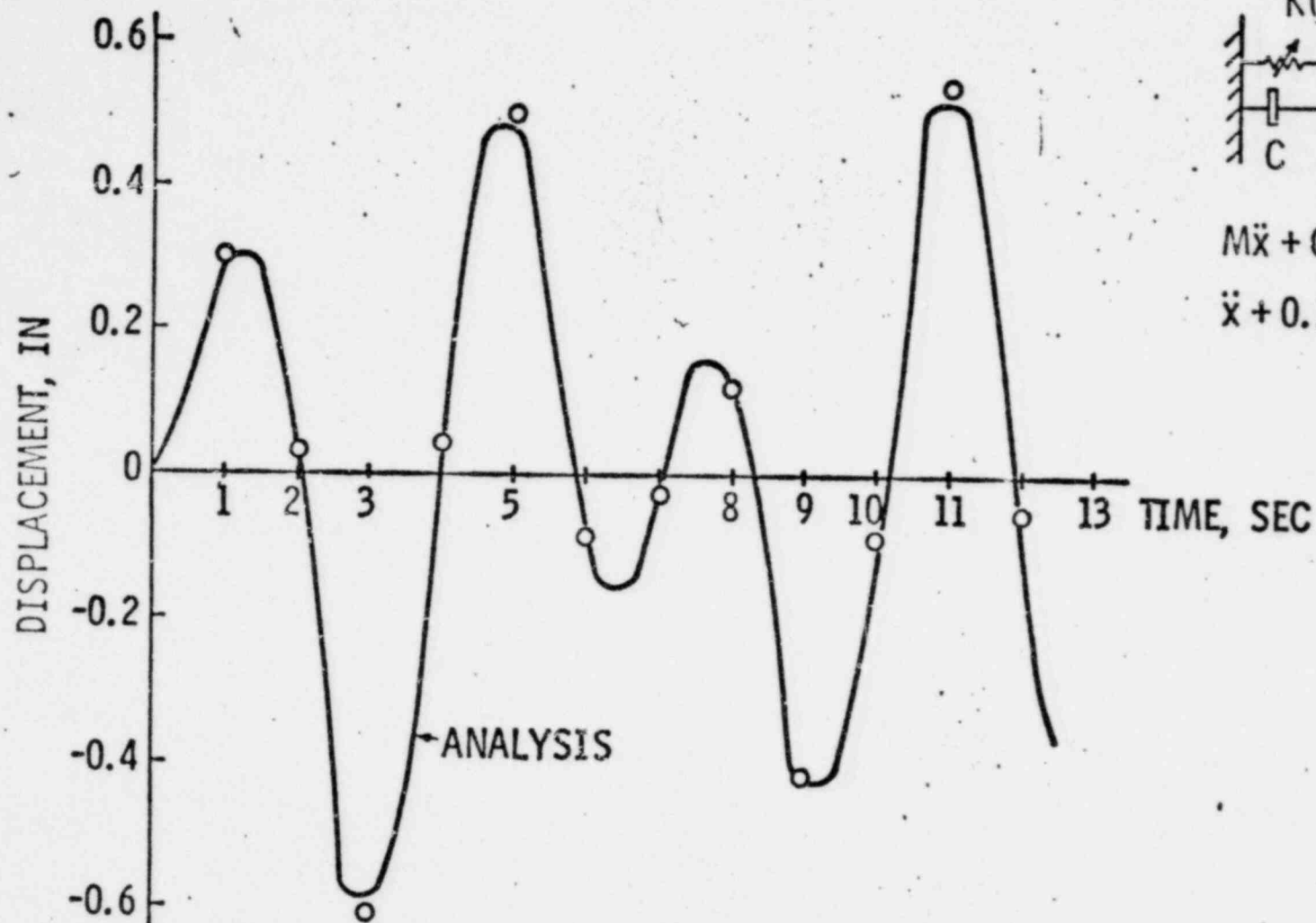
I

DUFFING OSCILLATOR



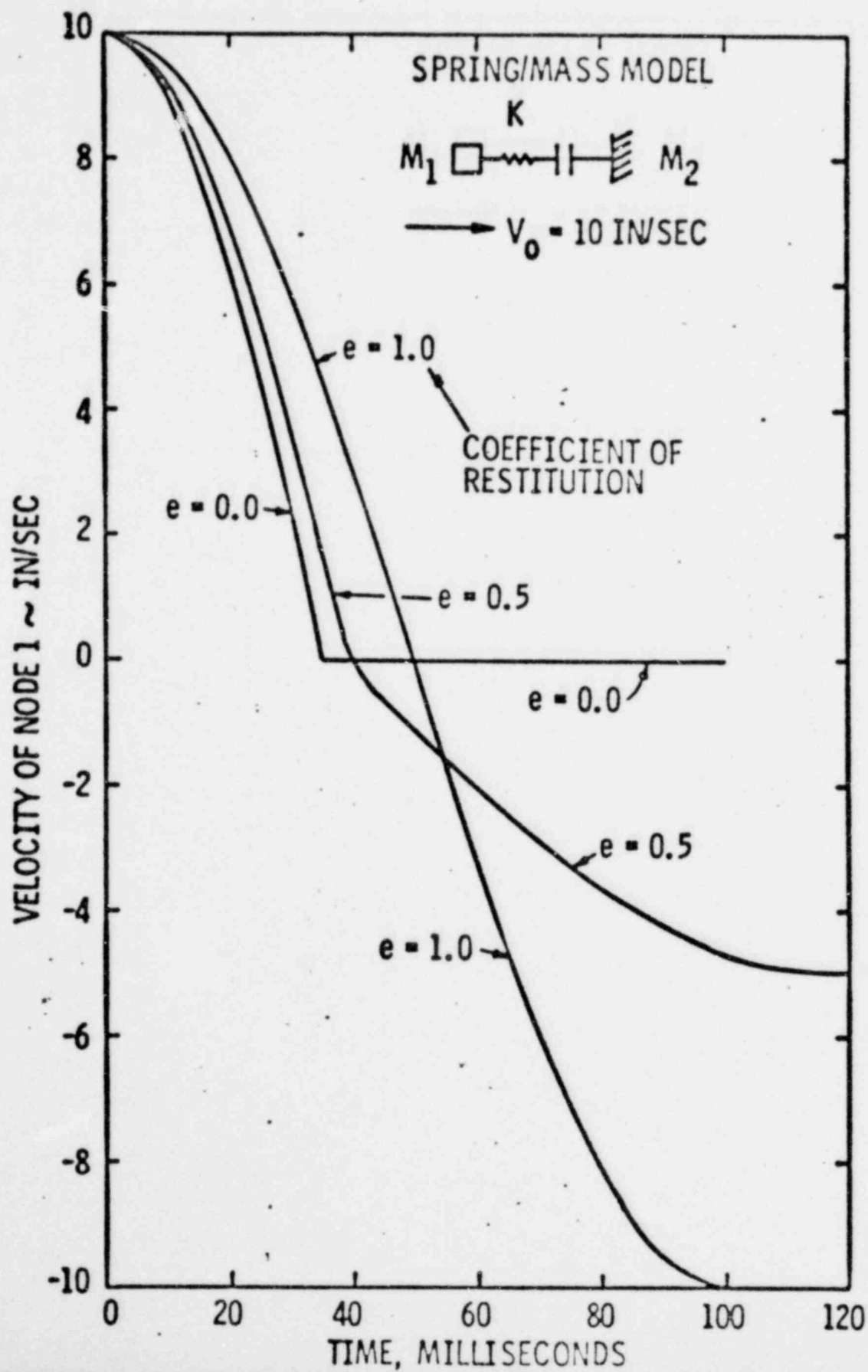
$$M\ddot{x} + C\dot{x} + K(x) = F(t)$$

$$\ddot{x} + 0.1\dot{x} + x(1 + x^2) = \cos 2t$$

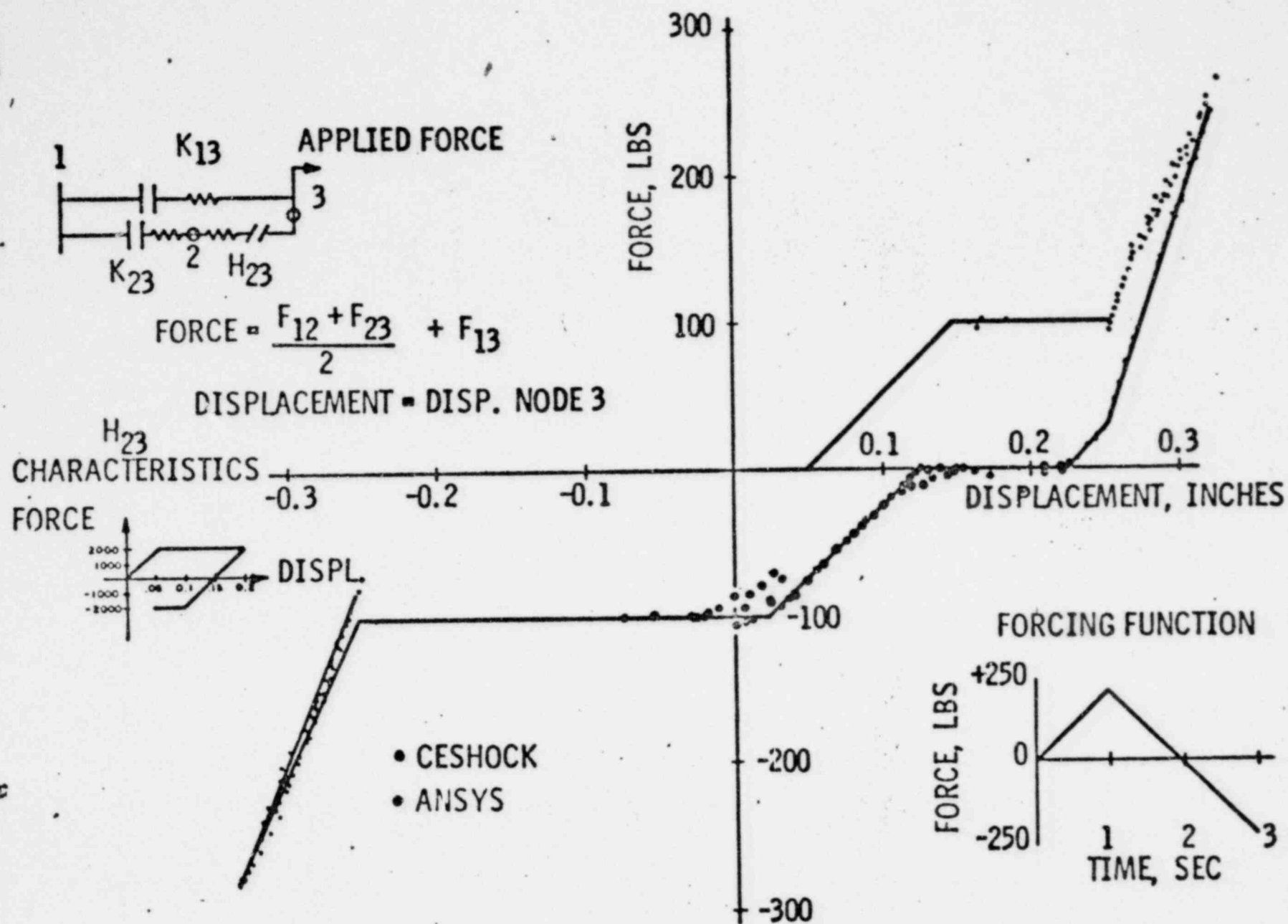


○ CESHOCK

IMPACT ELEMENT WITH COEFFICIENT OF RESTITUTION

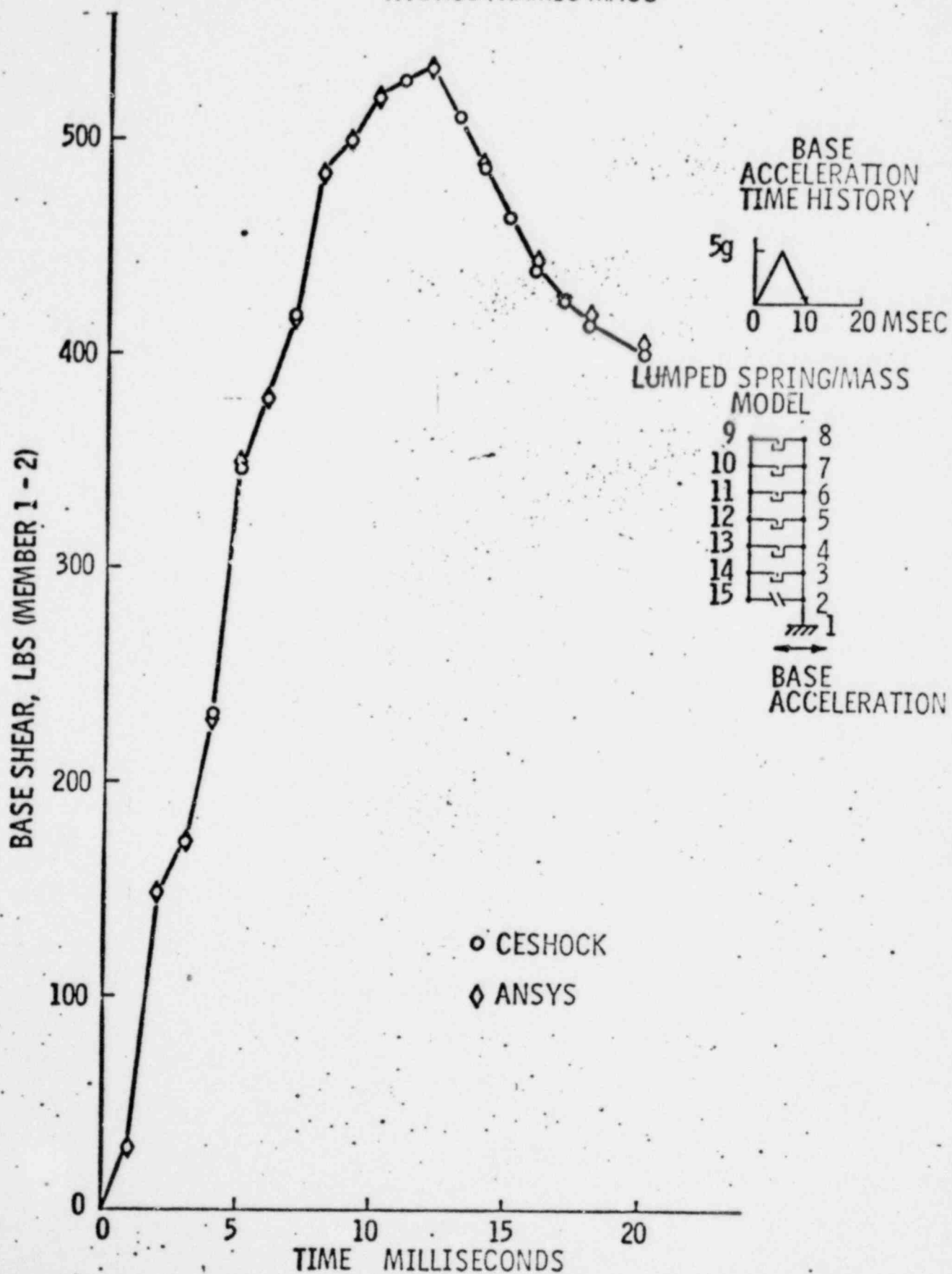


TWO DEGREE OF FREEDOM HYSTERESIS PROBLEM WITH GAPS



II

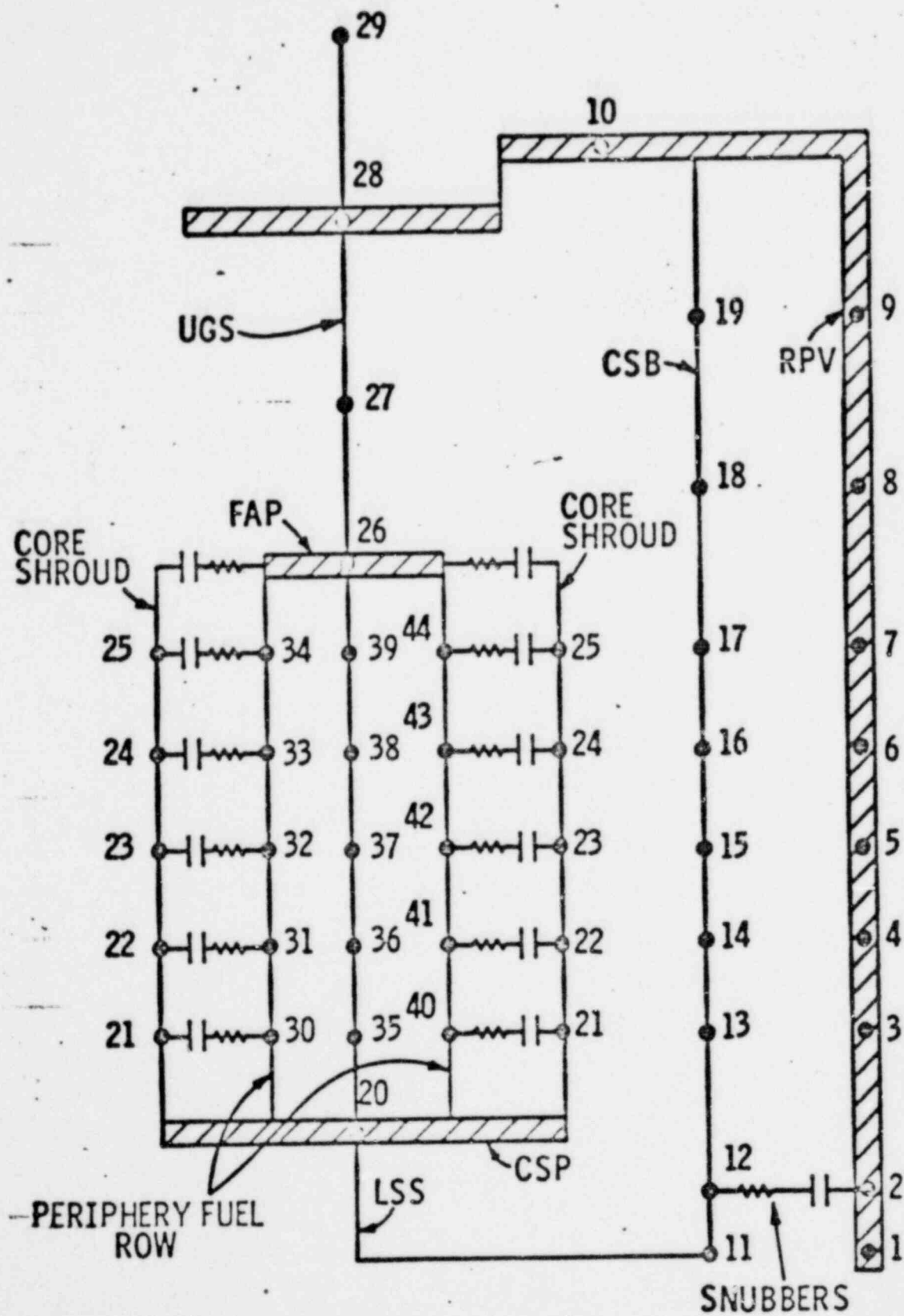
BASE EXCITATION PROBLEM INCLUDES, DAMPING, GAPS HYDRODYNAMIC MASS



FUEL TESTING

- STATIC LOAD - DEFLECTION
- FORCED VIBRATION
- BUNDLE IMPACT
 - HORIZONTAL
 - VERTICAL
- SPACER GRID IMPACT
 - PENDULUM
 - DROP
 - PLUCK

SCE - CORE INTERNALS MODEL



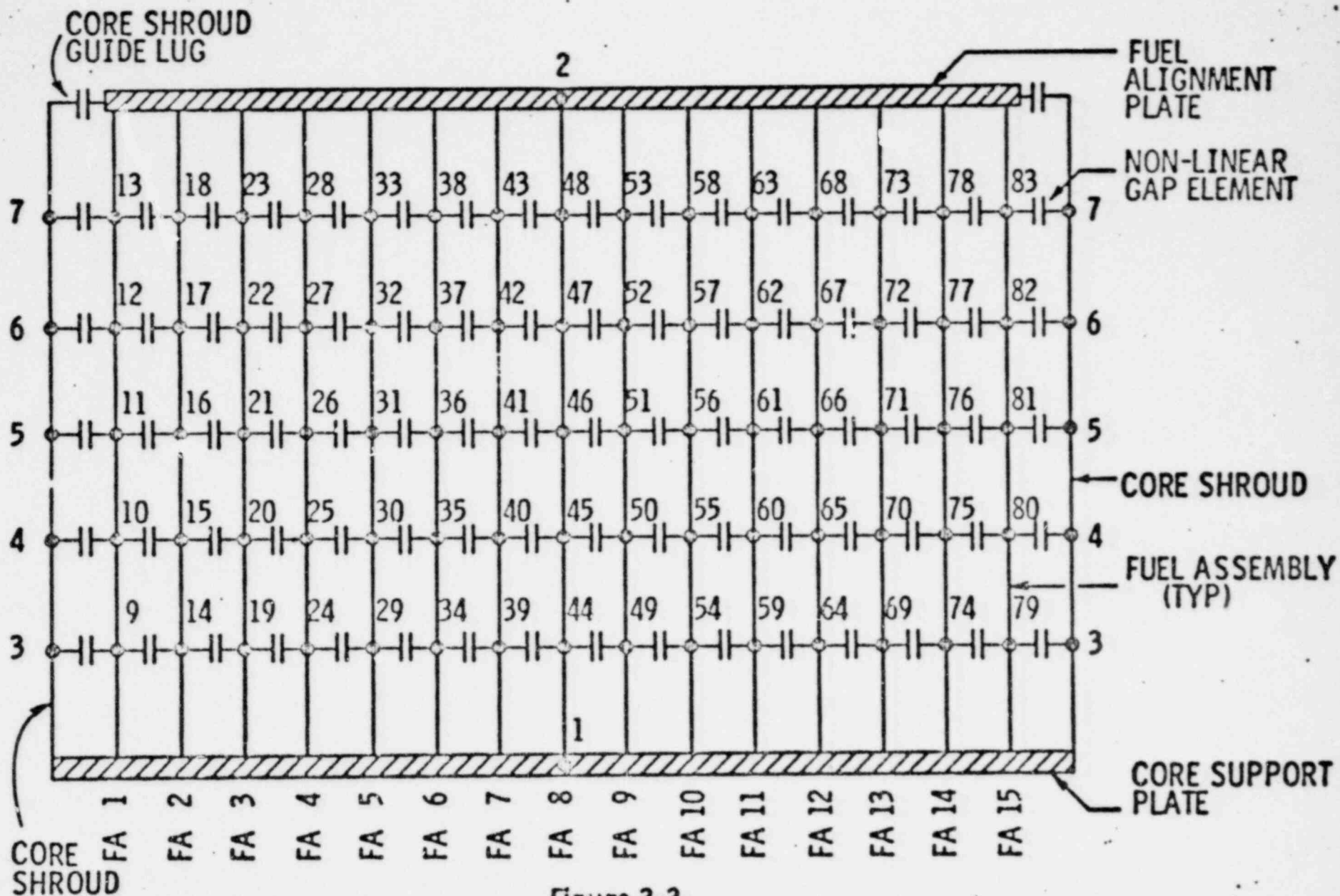
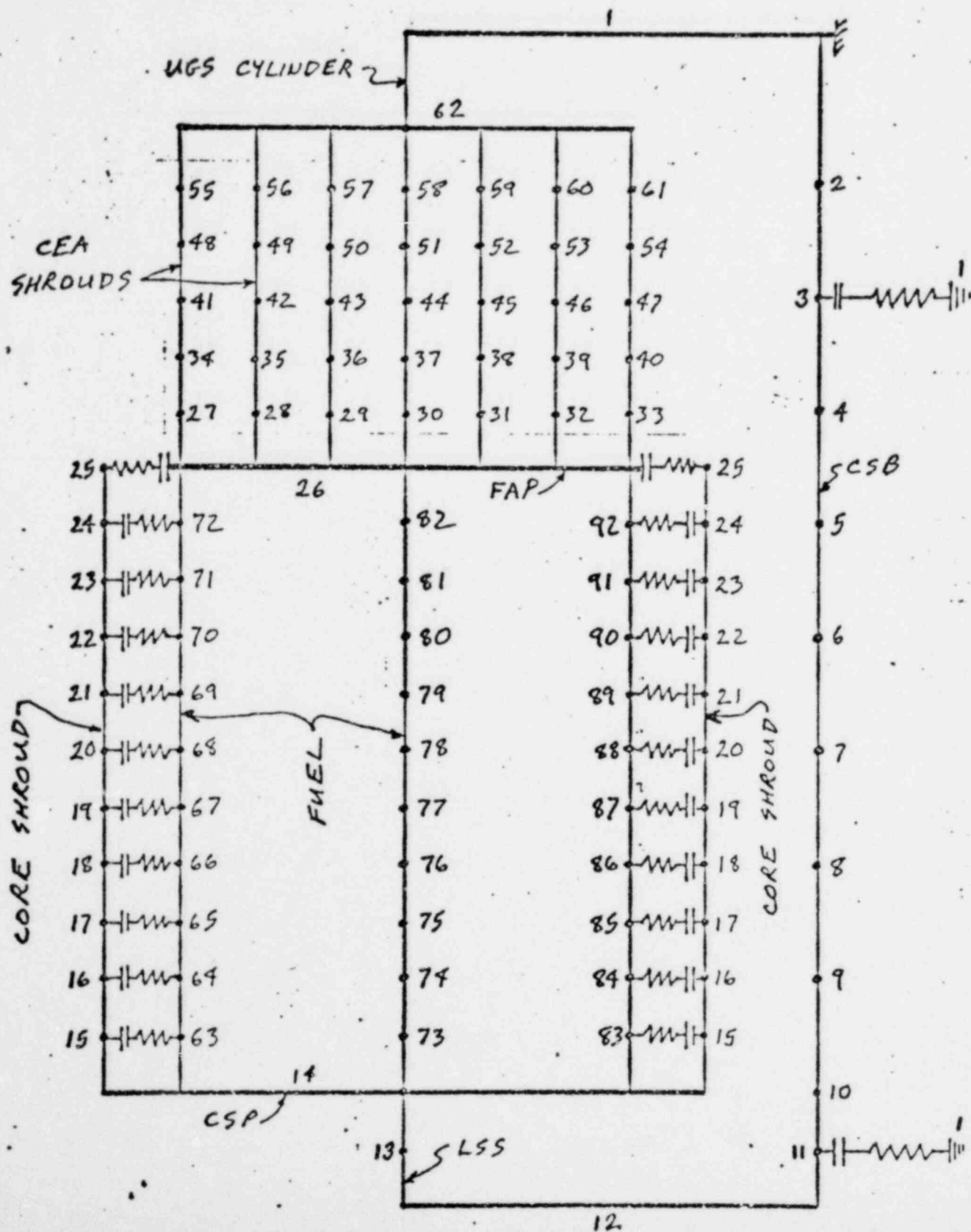


Figure 3-3
DETAILED HORIZONTAL CORE SEISMIC MODEL

SCE HORIZONTAL COUPLED CORE/INTERNALS LOCA MODEL



S.C.E. DETAILED CORE SEISMIC MODEL RESULTS.

ONE ROW OF 17 FUEL ASSEMBLIES

345

S.C.E. DETAILED CORE SEISMIC MODEL RESULTS

ONE ROW OF 17 FUEL ASSEMBLIES

3,45

S.C.E. DETAILED CORE MODEL LOCA RESULTS

ONE ROW OF 17 FUEL ASSEMBLIES

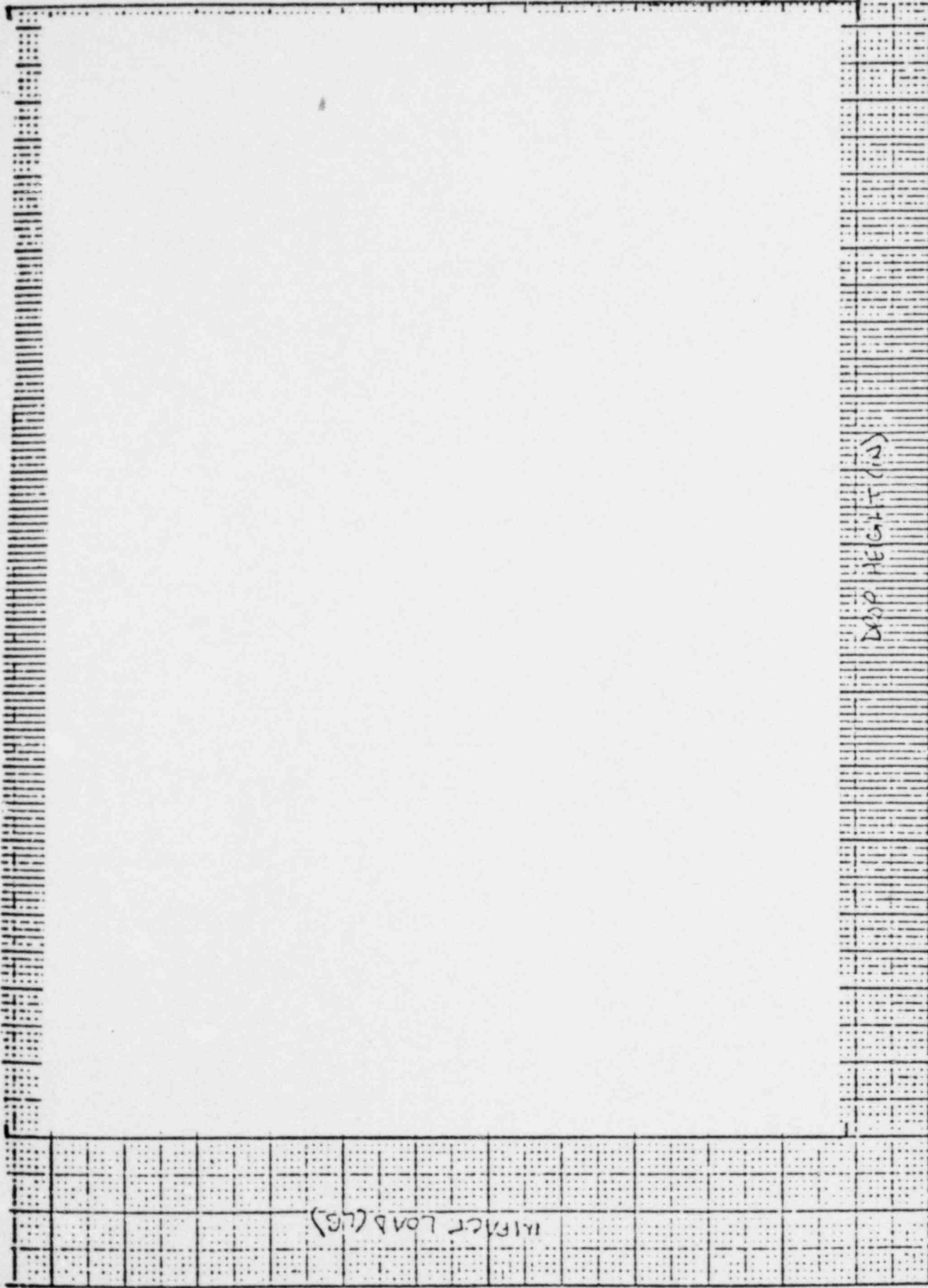
S.C.E. DETAILED CORE MODEL LOCA RESULTS

ONE ROW OF 17 FUEL ASSEMBLIES

345

2,3

COMPARISON OF TYPICAL LOAD DEFLECTION
CHARACTERISTICS



PROPRIETARY INFORMATION

HID-2 ONE SIDED IMPACT

56

DROP 11.647 (IN)

IMPACT LOAD (LG)

HID-1 ONE SIDED IMPACT

PROPRIETARY INFORMATION

SSE

GUIDE TUBE STRESS CALCULATION

STRUCTURAL ANALYSIS

INPUT

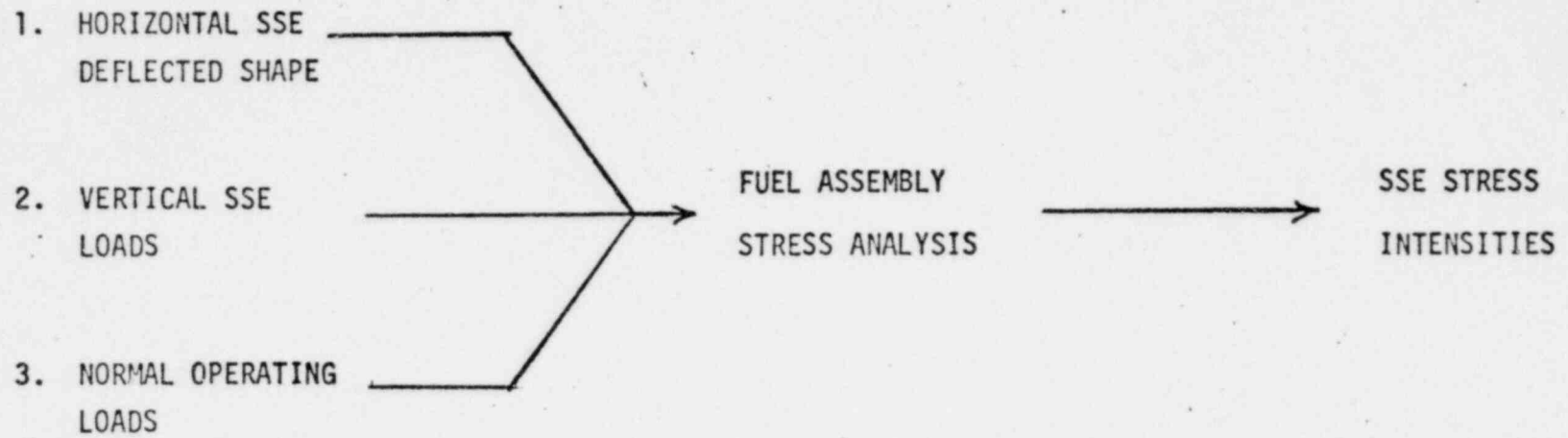
1. HORIZONTAL SSE
DEFLECTED SHAPE

2. VERTICAL SSE
LOADS

3. NORMAL OPERATING
LOADS

FUEL ASSEMBLY
STRESS ANALYSIS

SSE STRESS
INTENSITIES



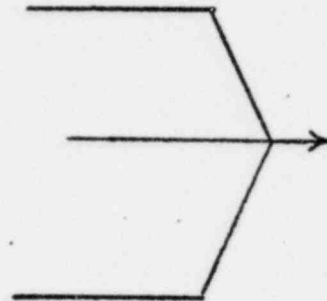
OUTLET BREAK

GUIDE TUBE STRESS CALCULATION

STRUCTURAL ANALYSIS

INPUT

1. LOCA OUTLET BREAK
DEFLECTED SHAPES
2. LOCA OUTLET BREAK
VERTICAL LOADS
3. NORMAL OPERATING
LOADS

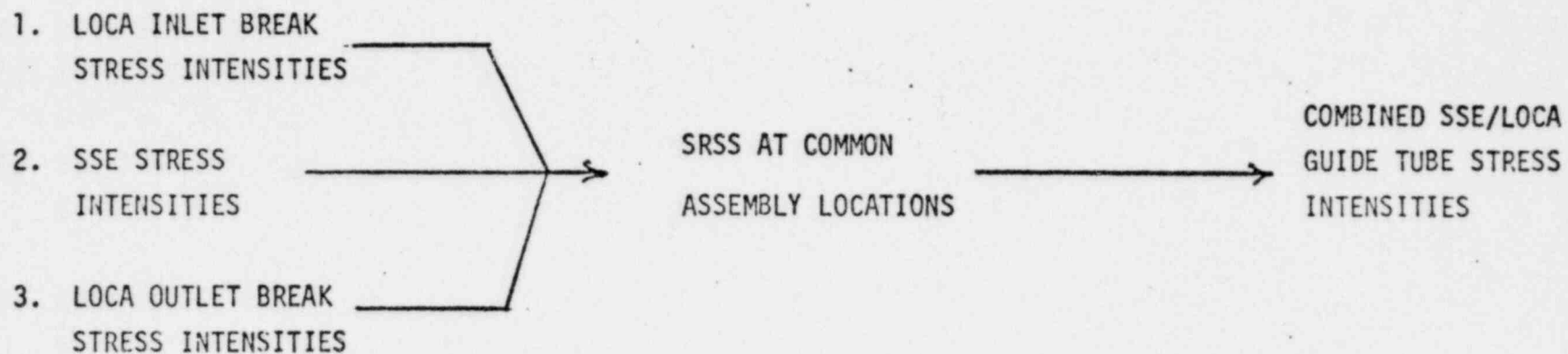


FUEL ASSEMBLY
STRESS ANALYSIS

LOCA OUTLET BREAK
STRESS INTENSITIES

COMBINED SSE/LOCA
GUIDE TUBE STRESS CALCULATION

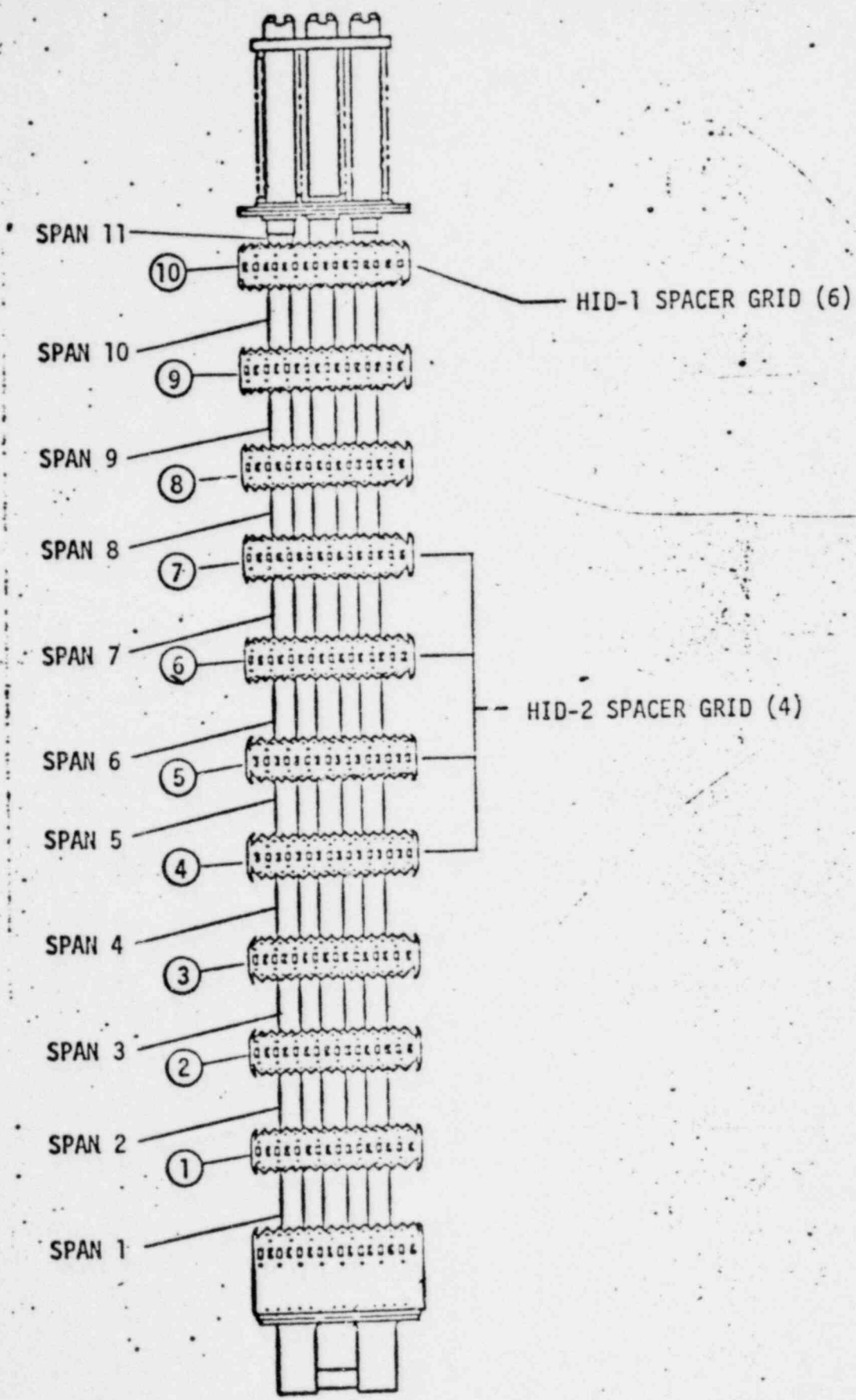
FUEL ASSEMBLY
STRESS ANALYSIS



Faulted Condition Criteria Summary

Component	Statement of Criteria	Numerical Limit
1. End Fitting Castings	$P_m \leq 2.4 S_m$ $P_b + P_m \leq F_s \times 2.4 S_m$	}
2. Upper End Fitting Posts	$P_m \leq 2.4 S_m$ $P_b + P_m \leq F_s \times 2.4 S_m$	
3. Upper End Fitting Springs	Calculated Shear Stress Not to Exceed Minimum Yield Stress in Shear	
4. Guide Tubes	$P_m \leq .7 S_u$ $P_b + P_m \leq F_s \times .7 S_u$ $F_s = 1.39$	
5. Spacer Grids	Impact Load Less Than Tested Grid Strength at Temperature	
6. Fuel Rods	$P_m \leq S_y$ $P_b + P_m \leq F_s \times S_y$ $F_s = 1.36$	

3,4,5



GUIDE TUBE STRESS (PSI)

DBE

CALCULATED

ALLOWABLE @ 650°F

$$\begin{array}{l} P_m \\ P_m + P_b \end{array}$$

3,4,5

LOCA

CALCULATED

ALLOWABLE @ 650°F

$$\begin{array}{l} P_m \\ P_m + P_b \end{array}$$

3,4,5

COMBINED DBE AND LOCA

CALCULATED

ALLOWABLE @ 650°F

$$\begin{array}{l} P_m \\ P_m + P_b \end{array}$$

3,4,5

SPACER GRID IMPACT LOADS (LBS)

D8E

HID-1

HID-2

CALCULATED

ALLOWABLE
@ 600°F

CALCULATED

ALLOWABLE
@ 600°F

3,4,5

LOCA

HID-1

HID-2

CALCULATED

ALLOWABLE
@ 600°F

CALCULATED

ALLOWABLE
@ 600°F

3,4,5

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