

CONTROL BLOCK: | | | | | | | ①

(PLEASE PRINT OR TYPE ALL REQUIRED INFORMATION)

0 1 | N | J | O | C | P | I | ② | 0 | - | 0 | 0 | 0 | 0 | 0 | 0 | - | 0 | 0 | ③ | 4 | 1 | 1 | 1 | 1 | ④ | | | ⑤
8 9 LICENSEE CODE 14 15 LICENSE NUMBER 25 26 LICENSE TYPE 30 57 CAT 58

CONT
0 1 | REPORT SOURCE | L | ⑥ | 0 | 5 | 0 | 0 | 0 | 2 | 1 | 9 | ⑦ | 0 | 9 | 1 | 4 | 7 | 9 | ⑧ | 1 | 0 | 1 | 0 | 7 | 9 | ⑨
7 8 60 61 DOCKET NUMBER 68 69 EVENT DATE 74 75 REPORT DATE 80

EVENT DESCRIPTION AND PROBABLE CONSEQUENCES ⑩

0 2 | During normal operation, a worker discovered a leak in the area of the
0 3 | (1-3) containment spray heat exchanger. Investigation revealed that a 3/4"
0 4 | nipple connected between the water box and the relief valve on the service
0 5 | water side was leaking. Additionally, slight leaks were discovered at
0 6 | the point where the ΔP transmitter instrument lines tap off the ESW
0 7 | outlet pipe on the (1-1) and (1-4) heat exchangers. Safety significance
0 8 | is considered minimal since the exchangers were not inoperable.
7 8 9 80

0 9 | SYSTEM CODE | S | B | ⑪ | CAUSE CODE | E | ⑫ | CAUSE SUBCODE | D | ⑬ | COMPONENT CODE | H | T | E | X | C | H | ⑭ | COMP. SUBCODE | G | ⑮ | VALVE SUBCODE | Z | ⑯ |
7 8 9 10 11 12 13 18 19 20
17 | LER/RO REPORT NUMBER | 1 | 7 | 9 | ⑰ | SEQUENTIAL REPORT NO. | 0 | 3 | 2 | ⑱ | OCCURRENCE CODE | 0 | 3 | ⑲ | REPORT TYPE | L | ⑳ | REVISION NO. | 0 | ㉑ |
21 22 23 24 26 27 28 29 30 31 32
ACTION TAKEN | A | ⑳ | FUTURE ACTION | X | ㉑ | EFFECT ON PLANT | Z | ㉒ | SHUTDOWN METHOD | Z | ㉓ | HOURS ㉔ | 0 | 0 | 0 | 0 | ㉕ | ATTACHMENT SUBMITTED | Y | ㉖ | NPRD-4 FORM SUB. | Y | ㉗ | PRIME COMP. SUPPLIER | Z | ㉘ | COMPONENT MANUFACTURER | Z | 9 | 9 | 9 | ㉙ |
33 34 35 36 37 40 41 42 43 44 47

CAUSE DESCRIPTION AND CORRECTIVE ACTIONS ⑳

1 0 | Analysis of a failed nipple from a similar event revealed that the leaks
1 1 | were caused by corrosion accelerated by galvanic action. The previous
1 2 | analysis also recommended replacement with stainless steel nipples. In
1 3 | addition to repairing the leaks with new nipples, the relief valve
1 4 | nipples on the (1-1), (1-2) and (1-4) exchangers were replaced.
7 8 9 80

1 5 | FACILITY STATUS | E | ㉚ | % POWER | 0 | 9 | 8 | ㉛ | OTHER STATUS | NA | ㉜ | METHOD OF DISCOVERY | A | ㉝ | DISCOVERY DESCRIPTION | Worker's observation. | ㉞ |
7 8 9 10 12 13 44 45 46 80
1 6 | ACTIVITY CONTENT | Z | ㉟ | RELEASED OF RELEASE | Z | ㊱ | AMOUNT OF ACTIVITY | NA | ㊲ | LOCATION OF RELEASE | NA | ㊳ |
7 8 9 10 11 44 45 80
1 7 | PERSONNEL EXPOSURES NUMBER | 0 | 0 | 0 | ㊴ | TYPE | Z | ㊵ | DESCRIPTION | NA | ㊶ |
7 8 9 11 12 13 80
1 8 | PERSONNEL INJURIES NUMBER | 0 | 0 | 0 | ㊷ | DESCRIPTION | NA | ㊸ |
7 8 9 11 12 13 80
1 9 | LOSS OF OR DAMAGE TO FACILITY TYPE | Z | ㊹ | DESCRIPTION | NA | ㊺ |
7 8 9 11 12 80

2 0 | PUBLICITY ISSUED DESCRIPTION | Y | ㊻ | Weekly news release - October 16, 1979. | ㊼ | NRC USE ONLY | 1165-350 |
8 9 10 7 9 1 0 1 8 0 4 1 9 58 69 80
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OYSTER CREEK NUCLEAR GENERATING STATION
Forked River, New Jersey 08731

Licensee Event Report
Reportable Occurrence No. 50-219/79-32/3L-0

Report Date

October 10, 1979

Occurrence Date

September 14, 1979

Identification of Occurrence

During the normal working day it was observed that both containment spray systems had developed small pipe leaks. This event is considered to be a reportable occurrence as defined in the Technical Specifications, paragraph 6.9.2.b.2.

Conditions Prior to Occurrence

The plant was operating at steady state power.

Power: Reactor, 1889.8 MWt
Generator, 638 MWe
Flow: Feedwater, 7.07×10^6 lb/hr
Recirculation, 15.2×10^4 gpm
Stack Gas: 3.85×10^4 μ ci/sec

Description of Occurrence

On Friday, September 14, 1979, at approximately 11:30 a.m., a worker in the area of the (1-3) containment spray heat exchanger noticed water leaking. An investigation revealed that a 3/4" carbon steel threaded nipple connected between the water box and the relief valve on the service water side was leaking. Additionally, a slight leak was noticed at the point where the ΔP transmitter instrument line taps off the (1-1) containment spray heat exchanger emergency service water outlet pipe. At approximately 2:30 p.m., there was a similar leak discovered on the (1-4) containment spray heat exchanger at the point where the ΔP transmitter instrument line taps off the ESW outlet pipe.

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Apparent Cause of Occurrence

All three of the leaks were caused by corrosion accelerated by galvanic action between 90/10 CuNi and SA106 Grade B carbon steel.

Analysis of Occurrence

The containment spray cooling system consists of two independent cooling loops, each capable of removing fission product decay heat from the primary containment. The safety significance of this event is to be considered minimal since the containment spray systems were not inoperable. The leaks discovered would not prevent the equipment from performing its design function.

Corrective Action

Since this was not the first time this type of incident has occurred, analysis from a previous nipple failure resulted with a recommendation to change material selection for replacement nipples to 90/10 CuNi or stainless steel. In addition to repairing the three leaks with stainless steel nipples, the relief valve nipples on (1-1), (1-2), and (1-4) containment spray heat exchangers were changed on September 14, 1979, to stainless steel as a preventive measure. The ΔP transmitter instrument line nipples on (1-2) and (1-3) containment spray heat exchangers have been changed to stainless steel with approval from Generation Engineering. Also, an engineering request has been submitted to examine all lines connected to the containment spray heat exchangers to study material compatibility and make appropriate recommendations for a permanent solution.

Failure Data

Similar Events: RO No. 50-219/79-04/3L-0
RO No. 50-219/79-22/3L-0

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