PHILADELPHIA ELECTRIC COMPANY 2301 MARKET STREET P.O. BOX 8699 PHILADELPHIA, PA. 19101 (215) 841-5001 SHIELDS L. DALTROFF VICE PRESIDENT ELECTRIC PRODUCTION November 16, 1979 Re: Docket Nos .: 50-277 50-278 Mr. William F. Kane Bulletins and Orders Task Force United States Nuclear Regulatory Commission Washington, DC 20555 Dear Mr. Kane: Attached is the remainder of the information requested by the Bulletins and Orders Task Force for preparation of the NRC staff generic report on boiling water reactors. This Peach Bottom plant specific information is provided in a form recommended by the chairman of the BWR Owners Group and supplements the generic information contained in General Electric Company Report NEDO-24708. Should you have any questions, please do not hesitate to contact us. Very truly yours, - the lactor Attachment 1375 180 7911200593

# PLANT Peach Bottom UNIT(S) II & III

BYPASS CAPACITY

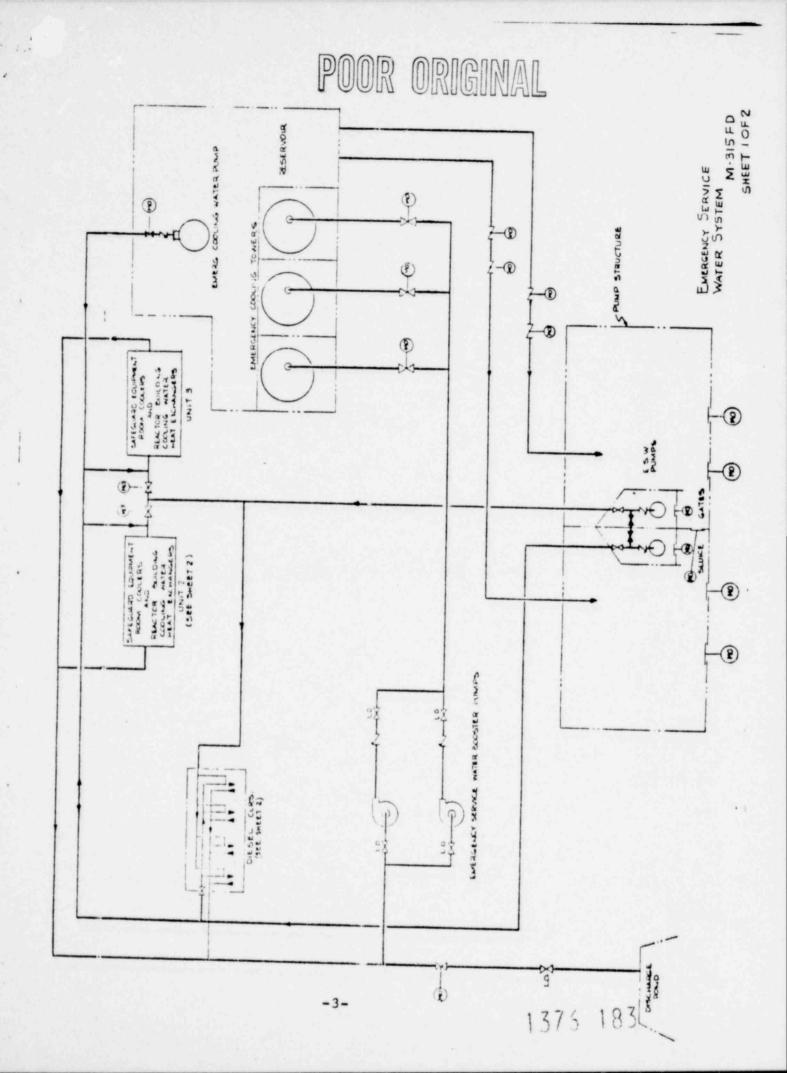
Plant Steam Bypass Capacity, % Rated 26

# PLANT Peach Bottom II & III

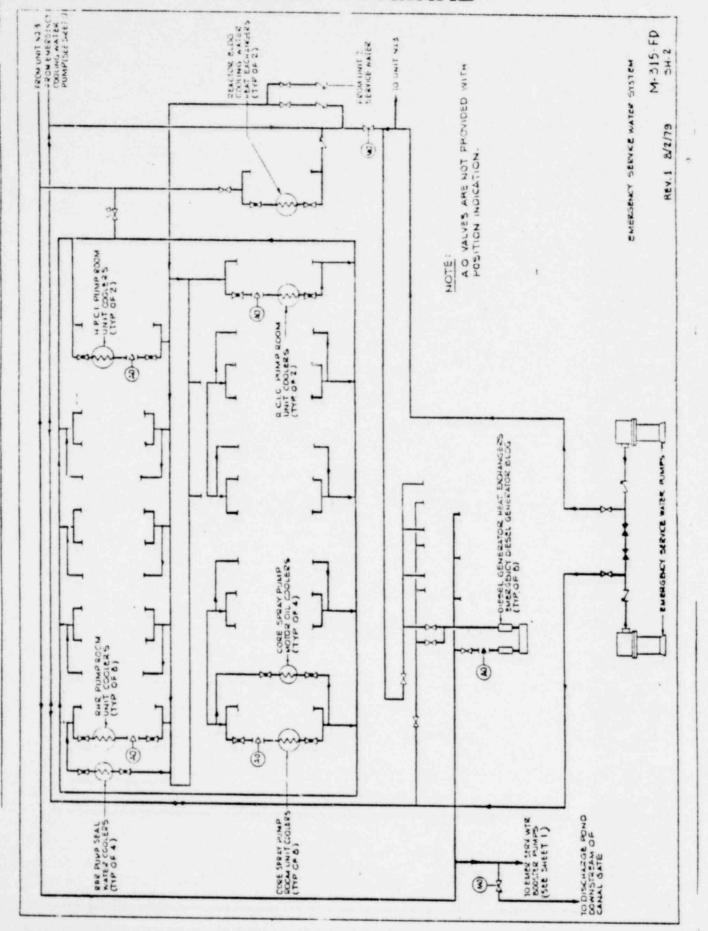
## SYSTEMS AND COMPONENTS SHARED BETWEEN UNITS

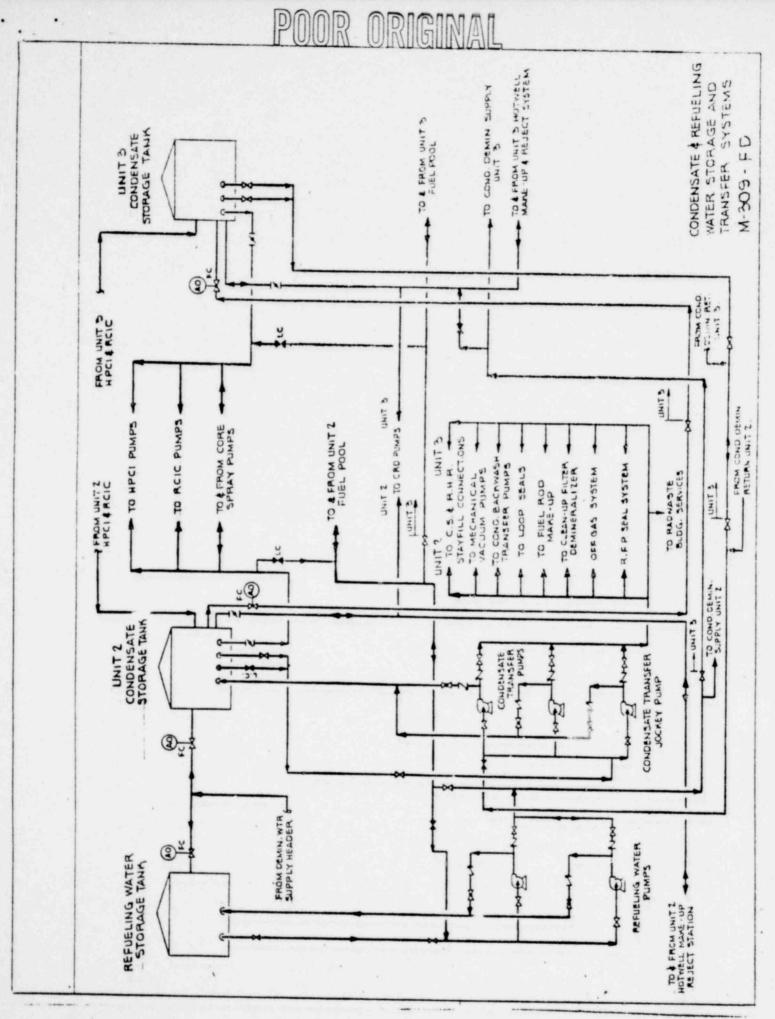
# PAGE 1 CONTINUED PAGE N/A Single-unit plant check here \_\_\_\_ and do not complete

	Between Numbers
11	& III
11	& III
II	& III
II	& III
	Units II II



# POOR ORIGINAL





# PLANT PEACH BOTTOM UNITS II & II PLANT SPECIFIC SYSTEM INFORMATION

	GENEP	AL.	WATER SOURCE	<u>ES</u>	INSTRUMENTATIO	N & CONTROL	FREQUENCY OF SYSTEM  6 COMPONENT TESTS
SYSTEM	Safety Classification	Seismic Category	Safety Classification	Category	Safety Classification <b>D</b>	Seismic Category	
RCIC	Group II	Class T Except as noted on M-309FD	Suppression Pool - GroupI Cond. Stor. Tank-Group III	Suppression Pool-ClassI Cond.Stor. Tank-Non Seismic	Quality Assured Equipment	Class I	See Attached Sheets
solation Condenser	N/A	N/A	N/A	N/A	N/A	NA	N/A
HPCS	N/A	N/A	N/A	N/A	N/A	N/A	N/A
нрст	Group II	Class I Except as noted on M-365 FD	Suppression Pool-Group I Cond.Stor. Tank-Group III	Suppression Pool-Class I Cond.Stor. Tank - Non Seismic	Quality Assured Equipment	Class T	See Attached Sheets
LPCS	Group II	Class I Except as noted on M-362FD	Suppression Pool -Group I Cond.Stor. Tank-GroupIII	Suppression Pool-Class 1 Cond.Stor. Tank - Non Seismic	Quality Assured Equipment	Class I	See Attached Sheets
LPC1	Groups I & II See M-361 FD	Class I	Suppression Pool-Group I	Suprresion Pool-ClassI	Quality Assured Equipment	Class T	See Attached Sheets
ADS	ASME III A	ASME III A	N/A	N/A	Quality Assured Equipment	Class I	See Attached Sheets
SPV	ASME III A	ASME III A	N/A	N/A	Ouality Assured Equipment	Class I	See Attached Sheets
FHF (Including Shutdown Cooling, Steam Condensing, Suppression Pool Cooling, Containment Spray Modes)	Groups I,II III, See M-361 FD	Class I	Supression Pool-Group I High Pressure Service Water Group II	Suppression Pool-ClassI High Pressur Service Water-ClassI		Class I	See Attached Sheets

# 1375 187

# PLANT PEACH BOITOM UNITS II & 11 PLANT SPECIFIC SYSTEM INPORMATION

	GENER	AI.	WATER SOURCE	ES 1	INSTRUMENTATIO	E CONTROL	FREQUENCY OF SYSTEM 6 COMPONENT TESTS
SYSTEM	Safety Classification ①	Seismic Category	Safety Classification	Category	Safety Classification DO	Seismic Category	
SSV (HPSW)	Group II	Class I	Normal source is river Backup source: Emergency Cooling Tower-Group II	Normal source is river Backup source Emergency Cooling Tower-Class	Assured e: Equipment	Class I	See Attached Sheets
FBCCW	Group III	Non-Seismic	N/A closed Loop	N/A closed Loop	Non-Quality Assured Equipment	Non Seismic	System is normally in service No routine testing require!
CRDS	Scram System Group I Remainder- Group III See M-356FD	Scram System Class I Pemainder- Non Seismic See M-356FD	Condensate Sys: Group III Cond. Stor. Tank-Group III	Condensate Sys: Non- Seismic Cond. Stor. Tank - Non Seismic	Quality Assured Equipment	Class I	See Attached Sheets
cst	Group III	Non-Seismic	Group III	Non-Seismic	Non-Quality Assured Equipment	Non Seismic	No Routine Testing Performed
Feedwater	Group I-From outboard chk. vlv. to reactor Remainder- Group III	Class I-From outhoard chk. vlv. to to reactor Femainler- Non-Seismic	Group III	Non-Seismic	Non-Quality Assured Equipment	Non Seismic	See Attached Sheets
Recirc. Pump/Motor Cooling	Group III	Non-Seismic	N/A closed	N/A closed	Non-Quality Assured Equipment	Non-Seismic	System is normally in service No routine Testing is required.

#### NOTES FOR SEISMIC/SAFETY CLASSIFICATION TABLE

 General classification of piping and equipment pressure parts in defined as follows:

Group I - Piping and equipment pressure parts within the reactor primary pressure boundary through the outer isolation valve, inclusive.

Group II - Piping and equipment pressure parts downstream of the outer isolation valve and extensions of containment and the Core Standby Cooling Systems.

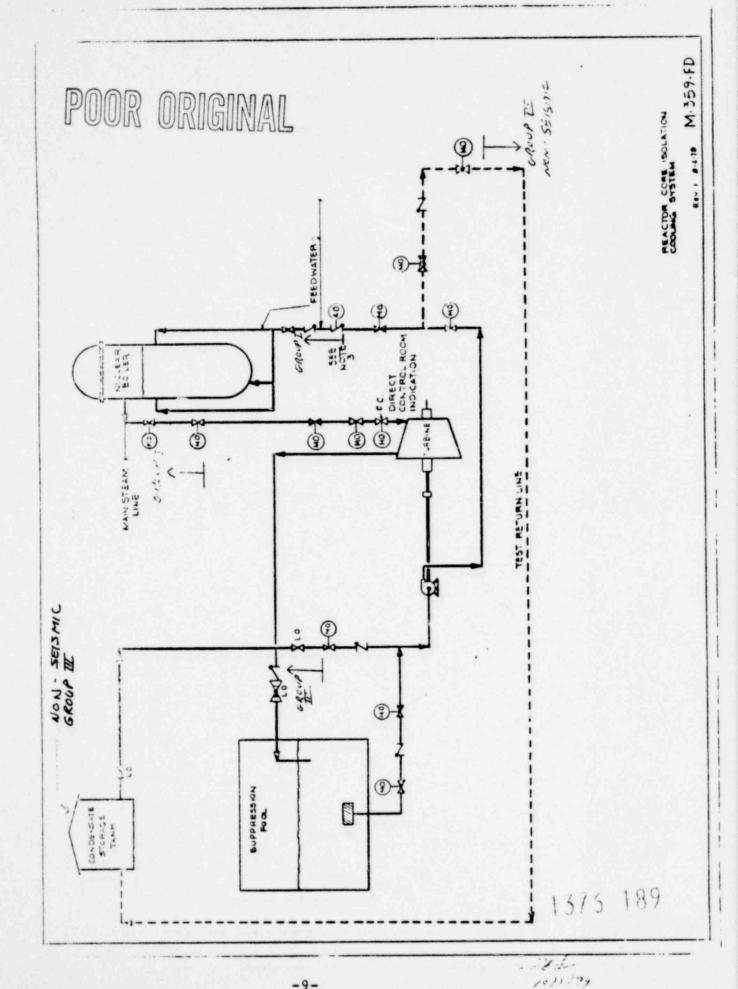
Group III - Balance of plant piping and equipment pressure parts, including power generation systems.

Requirements for these different groups appear in the Peach Bottom Final Safety Analysis Report Appendix A. A copy of Appendix A is included with our submittal for your convenience.

- 2. The RBCCW heat exchangers, Emergency Service Water interface, piping from containment penetrations through isolation valves and the isolation valves are being analyzed and/or modified to meet seismic class I requirements.
- Safety classification and seismic category refer to essential instrumentation only.
- 4. The Peach Bottom Quality Assurance list is the single controlling document which completely identifies the structures, systems, and components important to safety and required to assure:
  - a) integrity of the reactor coolant pressure boundary

b) capability to achieve and maintain safe shutdown
c) capability to prevent or mitigate the consequences of an
accident which could result in potential offsite
expecte comparable to the guidelines of 10 CFR 100.

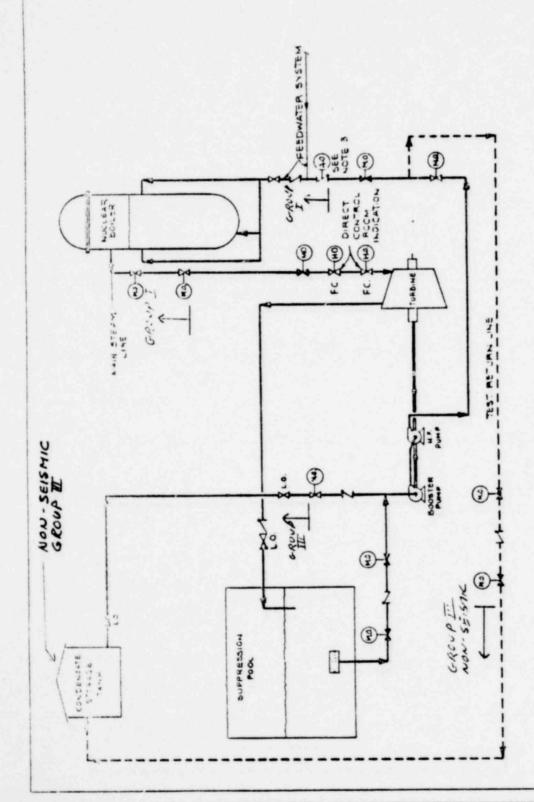
Specific performance criteria must be met for all such equipment and its acceptability must be documented. Non-quality assured equipment may meet or exceed the performance criteria of quality assured equipment but its performance is not documented.

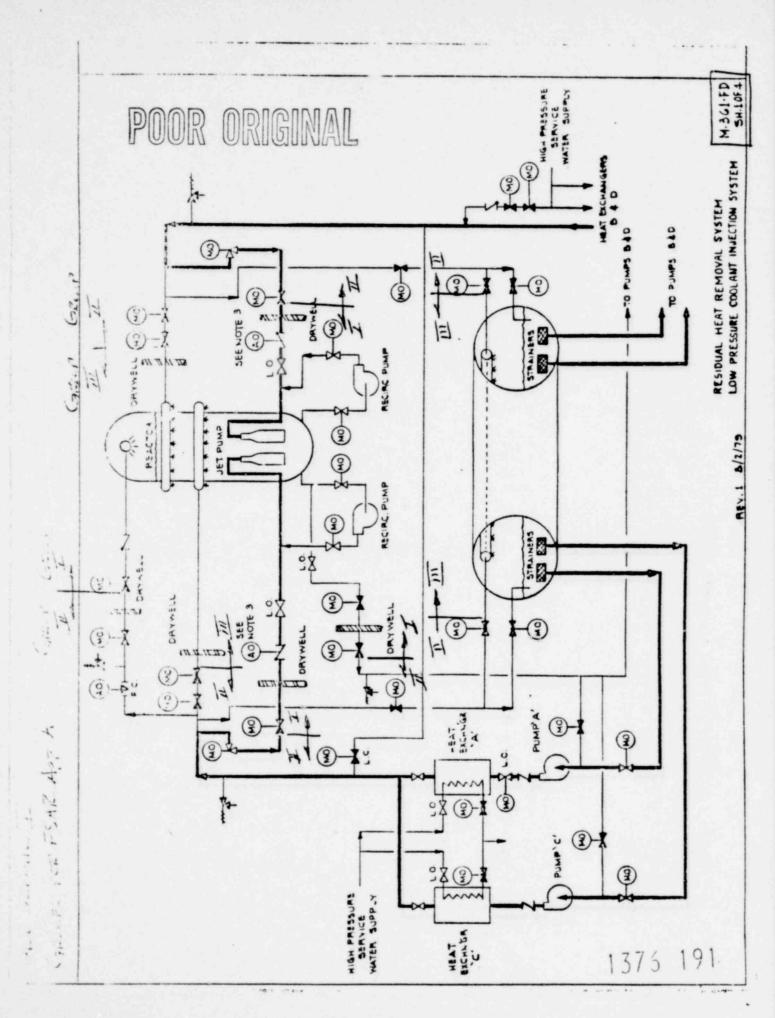


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POOR ORIGINAL

HIGH PRESSURE COCLANT
INJECTION SYSTEM
(HPC!) M-365-FD



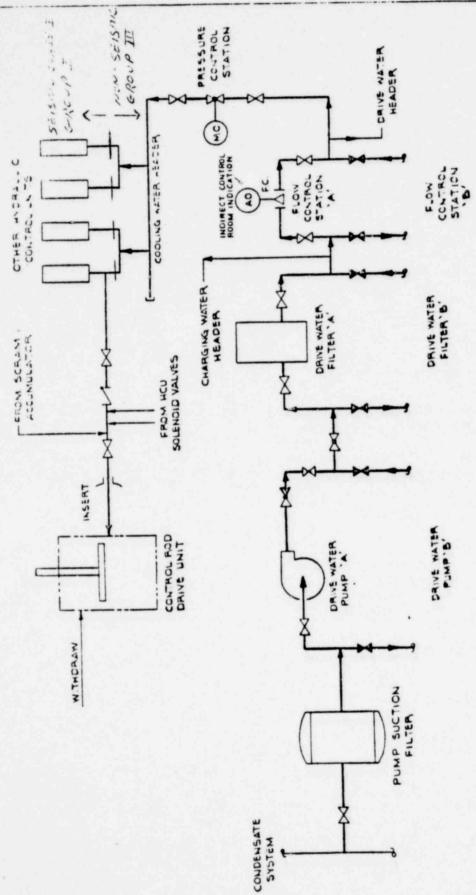


M-362-FD CORE SPEAN COOLING SYSTEM POOR ORIGINAL FROM CST GROUP E CORE 59244 (3)-TO SOME (3)-AC SEE PASSEL VESSEL

> 1375 192 10/1/29

CONTROL ROD DRIVE

HYDRAULIC SYSTEM



1375 193

14/1/29

Frequency of System and Component Tests

#### FREQUENCY

FREQUENCY

SYSTEM - RCIC

#### TEST TITLE

1. RCIC Logic System Functional Test

2. Venting of RCIC Pump Discharge Lines

3. RCIC Pump, Valve, Flow and Cooler

Test 4. RCIC Pump Test

5. RCIC Torus Suction Check

Valve Operability

6. RCIC Flow Rate at 150 psig

Steam Pressure

7. RCIC Simulated Auto Actuation

8. RCIC Vacuum Relief Valve

Functional Test

9. RCIC Turbine Governor

Calibration

10. RCIC Steam Line High Flow

Differential Pressure Switch

Calibration Check

11. RCIC Steam Line High Flow

Differential Pressure Switch Functional Test

12. RCIC Steam Line Pressure Switch Quarterly

Calibration Check

13. RCIC Steam Line Pressure Switch

Functional Test

14. RCIC Steam Leak Detection

Temperature Switch Functional

Test

15. Calibration Check of RCIC

Steam Leak Detection

Temperature Switch

16. Calibration Check of RCIC

low level initiation transmitters/switches

17. Functional Test of RCIC low

level initiation switches

18. Calibration Check of:

A. RCIC Pump Discharge Header

Pressure Transmitter

B. RCIC Pump Suction Header Pressure Transmitter

Once per 6 months Once per month if RCIC Pumps are lined up for torus suction Once per month

Once per operating

cycle

Once per operating

cycle

Once per operating

cycle

Once per operating

cycle

Quarterly

Each Refueling

Outage

Quarterly

Once per month

Once per month

Once per month

Quarterly (accessible switches) - Once

per operating cycle -

(inaccessible switches) Once per operating

cycle.

Once per month

Once per 2 years

C. RCIC Turbine Steam Pressure Transmitter

- D. RCIC Turbine Exhaust Pressure Transmitter
- RCIC Turbine Speed Sensor Calibration Check
- 20. Calibration Check of:
  - A. RCIC Pump Suction Header Pressure Switch
  - B. RCIC Pump Turbine Exhaust Pressure Switch
  - C. RCIC Vacuum Tank Level Switch

Once per operating

Once per operating

TEST TITLE

 HPCI Logic System Functional Test

 Venting of HPCI Pump Discharge Lines

 HPCI Pump, Valve, Flow, and Cooler Test

4. HPCI Torus Suction Check Valve Operability

5. HPCI Auxiliary Oil Pump Surveillance

6. HPCI Flow Rate at 150 psig Steam Pressure

7. HPCI Simulated Automatic
Actuation Test

8. HPC1 Vacuum Relief Valve Functional Test

9. HPCI Turbine Governor Calibration

10. Functional test of HPCI High
Drywell Pressure Initiation Switches

11. Calibration Check of HPCI High Drywell Pressure Initiation Switches

12. Functional Test of HPCI steam Supply Low Pressure Switches

 Calibration Check of HPCI Steam Supply Low Pressure Switches

14. Functional Test of HPCI Steam Supply Line High Flow Differential Pressure Switches

15. Calibration Check of HPCI Steam Supply Line High Flow Differential Pressure Switches

16. Functional Test of HPCI Area High Temperature Switches

17. Calibration Check of HPCI Area High Temperature Switches

18. Calibration Check of HPCI Reactor Low Level Initiation Switches/Transmitters

19. Functional Test of HPCI Reactor Low Level Initiation Switches

20. Functional Test for Condensate Storage Tank Low Level Switches FREQUENCY

Once per 6 months

Once per month if HPCI pumps are lined up for torus suction Once per month

Once per operating cycle Weekly

Once per operating cycle
Once per operating cycle
Quarterly

Once per operating cycle
Once per month

Once per 3 months

Once per 3 months

Once per 3 months

Once per month

Once per 3 months

Once per month

Once per 3 months (accessible) Once per operating cycle (inaccessible switches) Once per operating cycle

Once per month

Once per month

TEST TITLE

FREQUENCY

(transfer HPCI Pump Suction to Torus)

21. Calibration Check of Condensate Storage Tank Low Level Switches

22. Calibration Check of:

- HPCI Pump Discharge Pressure Once per 2 years
- Transmitter HPCI Turbine Steam Pressure Transmitter
- HPCI Turbine Exhaust C. Pressure Transmitter
- HPCI Pump Suction Pressure D. Transmitter
- 23. Calibration Check of HPCI Flow Transmitter
- 24 Calibration Check of HPCI Speed Element
- 25. Calibration Check of:
  - HPCI Pump Turbine Exhaust High Pressure Switches
  - HPCI Pump Suction Low Pressure Switch

Once per 3 months

Once per operating cycle Once per operating cycle

Once per operating cycle Once per operating cycle

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#### TEST TITLE

- Core Spray 'A' Logic System Functional Test
- Core Spray 'B' Logic System Functional Test
- Core Spray 'A' Pump, Valve, Flow, and Cooler Test
- 4. Core Spray 'B' Pump, Valve, Flow and Cooler Test
- 5. Core Spray 'A' Pump Test
- 6. Core Spray 'B' Pump Test
- 7. Daily Core Spray System Test
- 8. Core Spray Simulated Automatic Actuation Test
- Functional Test of Drywell High Pressure Core Spray Initiation Switches
- 10. Calibration Check of Drywell High Pressure Core Spray Initiation Switches
- 11. Functional Test of Reactor Low Pressure Switches (Core Spray Permissive)
- 12. Calibration Check of Reactor Low Level Pressure Switches
- 13. Calibration Check of Reactor Low Level Core Spray Initiation Switches/transitters
- 14. Functional Test of Reactor Low Level Core Spray Initiation Switches
- 15. Functional Test of Core Spray Stayfull Level Switches
- 16. Cali .ation Check of:
  - A. Core Spray suction pressure indicators
  - B. Core Spray pump differential switches for pump minimum flow protection
  - C. Core Spray pump discharge pressure indicators
  - D. Core Spray Discharge Pressure Switches
  - E. Core Spray Discharge Pressure Transmitters
  - F. Core spray Loop Flow

#### FREQUENCY

Once per 6 months

Once per 6 months

Once per month

Once per month

Once per operating cycle
Once per operating cycle
Daily if one diesel, one core spray pump, or LPCI is inoperable
Once per operating cycle
Once per month

Once per 3 months

Once per month

Once per 3 months

Once per operating cycle

Once per month

Once per operating cycle

Once per operating cycle

SYSTEM - LPCS

TEST TITLE

FREQUENCY

#### Transmitters

17. Functional Test of Core spray Sparger to Reactor Differential Pressure Switches

18. Calibration Check of Core Spray Sparger to Reactor differential Pressure Switches Once per month

Once per 6 months

SYSTEM: LPCI

TEST TITLE

RHR 'A' Logic Syssem Functional

 RHR 'B' Logic System Functional Test

3. RHR 'A' Pump, Valve, Flow and Cooler Test

4. RHR 'B' Pump, Valve, Flow and Cooler Test

5. RHR Pump Functional Test

6. Daily RHR System Operability Test

7. RHR Simulated Automatic
Actuation Test

8. LPCI system Valve Swing Bus Test

9. LPCI Cross Connect Valve Position

10. Functional Test for Drywell High Pressure LPCI Initiation Switches

11. Calibration Check for Drywell High Pressure LPCI Initiation Switches

12. Functional test for Reactor Low Level LPCI Initiation Switches

13. Calibration Check of Reactor Low Level LPCI Initiation Switches/Transmitters

14. Functional Test for Reactor Low Pressure Switches (LPCI Permissive)

15. Calibration Check for Reactor Low Pressure Switches

6. Functional Test of LPCI stayfull System Switches

17. Calibration of RHR pressure, flow, transmitters & indicators and pump differential pressure switches

FREQUENCY

Once per 6 months

Once per 6 months

Once per month

Once per month

Once per operating cycle
Daily if one diesel or one RHR pump is inoperable
Once per Operating
Cycle
Bi-monthly

Each refueling outage

Once per month

Once per 3 months

Once per month

Once per operating cycle

Once per month

Once per 3 months

Once per operating cycle
Once per operating cycle

SYSTEM: ADS

TEST TITLE

1. ADS 'A' Logic System Functional

 ADS 'B' Logic System Functional Test

3. ADS Simulated Automatic Actuation Test

4. ADS Relief Valve Accumulator Leak Test

 Functional Test of High Drywell Pressure ADS Initiation Switches

6. Calibration check of High Drywell Pressure ADS Initiation Switches

7. Functional Test for Core Spray
Pump Discharge Pressure Switches
(ADS Permissive)

 Calibration Check of Core Spray Discharge Pressure Switches (ADS Permissive)

9. Functional Test for LPCI Pump Discharge Pressure Switches (ADS Permissive)

10. Calibration Check of LPCI Pump Discharge Pressure Switches (ADS Permissive)

ll. Calibration Check of Reactor
Low Level ADS intiation
Switches/transmitters

12. Functional Test of Reactor Low Level ADS Initiation Switches

13. Calibration Check of Reactor Low Level ADS Permissive Switches/Transmitters.

14. Functional Test of Reactor Low Level ADS Permissive Low Level ADS Permissive Switches FREQUENCY

Once per 6 months

Once per 6 months

Prior to Startup from each refueling outage Once per operating cycle Once per month

....

Once per 3 months

Once per month

Once per 3 months

Once per month

Once per 3 months

Once per operating cycle

Once per month

Once per operating

Once per month

SYSTEM: SRV

TEST TITLE

1. Relief Valve Manual Actuation

 Relief Valve Bellows Leak Detection Pressure Switch Functional Test FREQUENCY

Once per operating cycle
Once per operating cycle

SYSTEM: RHR

TEST TITLE

1. RHR 'A' Logic System Functional Test

2. RHR 'B' Logic System Functional

3. RHR 'A' Pump, Valve, Flow, and Cooler Test

4. RHR 'B' Pump, Valve, Flow, and Cooler Test

5. RHR Pump Functional Test

6. Daily RHR system Operability Test

7. RHR to Fuel Pool Vacuum Relief Valve Functional Test

8. Head Spray Check Valve Functional

9. Calibration Check of Shutdown Cooling Permissive Switches (Reactor Pressure)

10. Functional Test of Shutdown Cooling Permissive Switches (Reactor Pressure)

11. Calibration Check of Containment Spray Reactor Level Permissive Switches/ Transmitters

12. Functional Test of Containment Spray Reactor Level Permissive Switches

13. Functional Test of RHR Stayfull System Level Switches

14. Calibration of RHR pressure & flow transmitters/ indicators and pump differential pressure switches

FREQUENCY

Once per 6 months

Once per 6 months

Once per month

Once per month

Once per operating cycle Daily if one diesel or one RHR Pump is inoperable

Once per Operating

Each time lead spray is used

Once per operating

Once per month

Once per operating cycle

Once per operating

cycle

SYSTEM: SSV (HPSW)

TEST TITLE

 HPSW Pump and Valve Operability and Flow Rate Test

2. HPSW Pump Operability

 Daily HPSW System Operability and Flow Rate Test

4. HPSW Pump Bay MUD Accumulation Measurement

5. HPSW Pressure and Flow Loop Calibration Check

 HPSW Bay level indication calibration FREQUENCY

Once per month

Once per operating cycle
Daily while two or more
HPSW pumps, 1 diesel, or 3 containment cooling subsystem are inoperable
Once per month

Once per operating cycle
Once per operating cycle

SYSTEM: CRD

TEST TITLE

FREQUENCY

1. CRD Withdraw Stall Flow Test

2. CRD Check Valve ISI Functional Test

Once per month
Each time CRD is used
for reactor makeup.
At least once per
operating cycle
Once per 2 years

3. CRD Hydraulic Control Calibration

NOTE: Additional testing on the Reactor Protection System and the Reactor Manual Control System may also

involve the CRD system

SYSTEM: FEEDWATER

TEST TITLE

1. Calibration of Feedwater Control Instruments (Reactor Pressure and Level)

 Calibration of Feedwater Flow Loops FREQUENCY

Once per 6 months

Once per operating cycle

## PLANT Peach Bottom UNIT(S) 11 6 111

#### PRIMARY CONTAINMENT ISOLATION SYSTEM DATA

Page 1

						0	3		0	Mode o		<b>(9)</b>	3	0		Valve	Posi	tion
Penetration Number	Line Size	Line Description	ESF (Yes/No)	Pig. No.	Fluid	Valve Number	Isolation Group (Signal)	Valve	Valve Type	Primary Actuation	Secondary	Closure Time (Sec.)	Power	Position Indication	Normal	Shutdown	Post-	Power Pailure
N-7A to D	26"	Main Steam	No	1	Steam	A to D	I(A,B,C,D & E)	1.1.1.1	GB	Inst.Gas	Spring	3 to 10		D	0	С	С	С
						A0-2-86 A to D	I(A,B,C,D & E)	Outside	GB	Inst.Air		3 to 10	B or F	D	0	C	С	С
N-8	3"	Main Steam	No	1	Steam Water	Mo-2-74	I(A,B,C,D & E)	Inside	GT	AC Motor	Manual	15	Α	D	С	0	С	as is
						MO-2-77	I(A,B,C,D & E)	Outside	GT	AC Motor	Manual	15	F	D	С	0	С	as is
N-9A	24"	Feedwater - - feedwater	Yes	2	Water	2-28A		Inside	ск	flow					0	c	0	
	1	- feedwater	No	-		2-96A	-	Outside	CK	flow		-	-	-	0	c	C	
			No			MO-2-38A	II(A,B,F)	"	GT	AC Motor	Manual	50	D	D	C	C	С	as is
		- HPCI	Yes			MO-23-19	RM		GT	DC Motor	0	20	P	D	С	С		as is
N-9B	24"	Feedwater - feedwater	No	2	Water	2-28B		Inside	СК	flow				-	0	c	0	
		- feedwater	No			2-96B		Outside	CK	flow	-	-	-	-	0	C	C	
	1	- RCIC	No			MD-13-21	RM		GT	DC Motor	Manual	15	E	D	C	0		as is
		- RHCU	No			MO-12-68	11(A,C,D, & G)		GB	AC Motor		5	В	D	0	0		as is
		- startup rec.	No			MO-2-38B	11(A.,B,F)		GT	AC Motor		50	В	D	С	6	С	as is
N-10	3"	Steam to RCIC															^	
		Turbine	No	3	Steam	MO-13-15 MO-13-16	IV(A,B,C, IV(A,B,C)		GT GT	AC Motor DC Motor		15 15	B	D D	0	C C		as is
N-11	10"	Steam to HPCI Turbine	Yes	1	Steam	MO-23-15	V(A,B,C)	Inside	GT	AC Motor		15		D	0	c	0	as io
		Turbine			Sceam	MQ-23-16	V(A,B,C)	Outside	GT	DC Motor	"	15	F	D	0	С		as is
N-12	20"	RHR Shutdown Cooling Sucton	No	4	Water	MO-10-17	II.A, B,E)	Inside	GT	AC Motor		32	P	D	С	0	С	as is
		Doctor Garage				MO-10-18	I(A,B,E)	Outside	GT	DC Motor	"	32	A .	D	c	0		as is
N-13,A,E	. 24"	RHR Shutdown Cooling Return		5	Water	MO-10-25A,	BII(A,B	Outside	GT	AC Hotor		34	1	D	с	0	С	88 18
		The injection				A,B	-	Inside	СК	Flow	-	-	2	D	C	0	С	-
			No .			AO-10-163 A,B	RMP	"	DCV	Inst.Gas	String	5	3	D	С	С	С	C

PLANT Peach Bottom UNIT(S) II & III

PRIMARY CONTAINMENT ISOLATION SYSTEM DATA

Page 2

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alve	Shutdown	00	o	o	o	00	υυ	ပပ	ပပ	٥٥	0	0	0	0000
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)	Position	20	۵	a	a	99	90	90		. 0	a	۵	۵	0000
)	Power Source	< a.	d,5	2	9	< №	< #	<b>₹</b> m		. <	4	4	so.	m < m m
	Closure Tim	2 5	12		2	2 2	2.4	2.5		. 50	12	12	~	~ ~ ~ ~
uo	Secondary	Manua 1			Spring	Manuel "	Spring.		٠.,	Spring	Manuel		Spring	
Mode of Actuation	Primery	AC Motor DC Notor	AC Motor	Plow	Inst.Gas	AC Motor De Motor	Inst.Air Inst.Air	Inst.Afr Inst.Afr		Flow Inst.Air	AC Motor	AC Motor	Inst. Af	
9	Velve Type	55	15	CK	DCV	15	DCV DCV	DCV	85	CK DCV	15	CT	m	<b>80 80 80</b>
	Valve	Inside	Out #1de	Inside		" Outside	Out side		Inside	Out side Out side	Outside	Outside		
9	Teolation Group (Signal)	II(A,C,D,S) II(A,C,D,S)	¥	,	RMP	II(A, B, E)	II(A,B) II(A,B)	11(A,B) 11(A,B)	22	11(A,B)	¥	¥	H	BBB
Θ	Valve TadmuN	Mo-12-15 Mo-12-18	Water Mo-16-12	A,5 Mo-14-13	Ap-14-15	A,B Mo-10-32 Mo-10-33	A0-20-82	Water 10-20-94 A0-20-95		A0-2969A	MO-2373	MD-2374	A0-2505	A0-2519 A0-2520 A0-2521A
	Pluid	Water	Water			Water	Vater	Water	Air	Afr	Water	Water	Afr	
	Fig. No.	۰	8			7	œ	00	0	10	::	=	12	
	(ON/ OOA) ASZ	9	Yes	Yes	ON	° N	° ×	No	No	o <sub>X</sub>	9	No.	o Z	
	Line	RUCU Pump Suction	Core Spray Pump Discharge			RIR Head Spray	Dryvell Pl.Dr. Pump Disch.	Drywell Equip. Dr. Pump Disch.	Service Air Supply	Inst Gas Supply No	RBCW to Recira	RBCW from Recirc	Drywell and Torus Purge Supply	
	Line Size		12"			9	3"	3.	L	L	7		18"	
	Penetration Number	N-14	N-16 A,B			N-17	N-18	N-19	N-21	N-22	N-23	N-24	N-25 6205B	

PLANT Peach Bottom UNIT(S) 11 & 111

PRIMARY CONTAINMENT ISOLATION SYSTEM DATA

Page 3

1.									
9	Power	0.0	a hazu ali de d						
£10			000000000						
Valve Position	Post-	00000	000000000						
alve	Shutdown	20000	000000000						
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	Power	<b>4</b> 1011	< m < m m < m a a a a						
90	Closure Tim (Sec.)		~~~~						
lon	Secondary	Spring	Spring						
Actuation	Primery Actuacion	Inst.Ain Flow Inst.Air Flow Manual	Inst.Afr  " " AC Coll BC Coll AC Coll AC Coll AC Coll AC coll						
9	Valve	CK(2) CK(2) B VB	DCV DCV B B B B B B CV SV SV SV SV SV SV SV SV SV SV SV SV SV	RD XF-CV	RD XFCV	XP C	RO XFO4	ROX	RO XFO
	Valve	Outside :::	Out st de	Inside	Inside Outside	Inside Outside	Inside out side	Inside Out side	Inside Out side
9	Isolation Group (Isngl2)	II. E							
Э	Valve Number	A0-2523 A0-2502A 9-26A	A0-2509 A0-2510 A0-2506 A0-2507 A0-4235 SV-2671G SV-2978G SV-4960B SV-4960B	25,77	174,194. 11 134,154	23	178,198, 138,158	73A, C, E, G	64 C,D
	Fluid		Adr	Water	Water /steam	Steam	Water	Steam	Water
	Pig. No.		2	16	91	16	16	16	16
	(ON/ 00 A) 452		Yes No No No Yes					, -	
	Lit.e Description		Drywell Purge Exhaust -CAD -CAD -purge -inst. gas -CACS sample -CACS sample -CAD sample	Inst.Lines-Core	Inst. Lines RPV Level & Pressure	Inst.Line - RFV Head Pressure	Inst. Lines - RPV Level & Pressure	Inst.Lines- Maj Stm. P.c.sure	Inst. Lines - Recire Loop
	Line Size		18:	L	i.	-	Ŀ	-	ī.
-	Penetration Number		Z-26	N-27E, F	N-28A,B	N-28D	N-29A D, E, F	11-30A, B,C,D,	N-30E, P

	Pailing														
lon	Tower			,							ပ		o	1.1	ပပ
Valve Posttion	Post-			S							o 0	o	o	ပပ	ပ္ပ
lve	Shutdown			0					il e		00	o	o	၁၀	00
2	LamioN			Ų							00	0	o	ပပ	00
9	Posttion										Q I		н		
9	Power										~ ~	,	2		, z
9 **	Closure Time (Sec.)														
lon	Secondary										Spring				-/ Spring
Mode of Actuation	Primery			ŀ							AC Coll DC Squfb	Flow	AC Co11	Flow	Flow AC Colls, Int.Afr
9	Valve	XPC V	RO XPC V	GB(2)	RO	RO	68	RO	XPC V	RO XFC V	BL XV	S,	8 0	¥ ¥	HC.
	Valve	Out side Out side	Inside Out side	Out s1 de	Inside Out side	Inside	Out side	Inside	Out side	Inside	Out side	Outside	Outside	Inside Out side	Inside Outside
9	nolisiosi quoto (isngic)								_		II(A,B) RM		II(A.B.)		
0	Velve	7A, B 8A, B	634,8	,	30 A,B	- 62A,B,C,D			73,8,0,F,	37A, B		,	7-113	3-110 3-110	
	Pluíd	Water 7A,B	Water	Air	Water	Jater	Afr	Steam		Steam	Air	Air		Jater	Water
	Pig. No.	17	91	18	91	16	61	16		16	20	7		21	22
	ESP (Yes/No)		,		1			,			No.	No		o <sub>N</sub>	Yes
	Line Description	Inst. Lines - Recire Pump Seal Pressure	Inst     faes -     Recfre   loop A	ILRT Connections No.	Inst Lines - C.S.Inj. Press.	Inst.Lines - Recire Pump AP	Inst.Line - Drywell Press.	Inst. Lines	Main 9tm. Pre88.	Inst Lines - HPCI Stm Press.	Tif Drives	Tip Purge		CRD Return (	CRD Insert
	Line Size	Ŀ	L	3/4.	L	L	L	1.		L	3/8"	1.		:,7	<u>L</u>
	Penetration Number	N-31 A to 0	N-32A,	N-32C,L	N-32E, F	N-33A, B,C,D,	N-33F	N-34A	to D	N-34E, F	N-35 A	N-35F		N-36	N-37 A to D

SYSTEM DATA 111 & 111 PRIMARY CONTAINMENT ISOLATION Peach Bottom UNIT(S)

2

Page

Pailure 18 O 0/0 Power O C 1 1 Position CC C Accident C 00 0/0 0 00 0 0 0 U -3804 Valve Shutdown 0 0 U 00 U C U C 00 O Normal 0 0 O C 00 C U C U 00 Indication 0 Posttton - -0 a . . 0 OZ Z 0 Source V. V B,B C,D C,D C,D Power . . < 200 z 3 (.sec.) 4 Closure Time = . Spring Manua 1 Spring Manual Actuation Spring Mode of Actuation Secondary . . AC Coils/ Inst.Air Cot1 Motor Coll Gas Afr Motor Coll Coll Inst Plow Plow Actuation Inst Flow AC 8 Primary NC. AC AC AC 0 RO NE XFCV HC U Like DCV 200 SV GB GB GB GB CKC GT GT SV CK Valve Out side Inside Outside Inside Outside Outside Outside Out side Outside Outside Out side Out side Outside Out si de Outside Outside Out stde Out side Outside Outside Inside Inside Inside Location ASTAG (A, B, C, D, E) (A, B, C, D, 0 (Signal) VII VI I 111 dnoag === E E) Isolation 8 2 54 A,3 125A.8 66F,8 SV-2671E, SV-2978E, MO-10-264 SV-4948A 10-538,D 10-53A,C MO-10-31 SV-4949A 0-60A,C 10-53A, C Fates 11-16 Solution 11-17 0 A0-2-40 A0-2-39 0 Number 305A Valve Water Water Steam Water Witer Water Water Air afr Air Fluid A1 16 0 9 59 61 19 PIE. No. 19 1.3 25 14 24 22 Yes Yes No Yes Yes (SE (Yes/No) Yes Yes Yes nst Lines -Rectre Steam Press RWCU Fump Suct. CACS Sample Lines No nst Lines -RCIG Inst Lines-Unit 3, Drywell Press. Containment Spray-KHR nst Lines-Unit Inst Lines-Unit 2 Drywell Press 3, Drywell Press Standby Liquid Control CRD Withdrawal Suction Press. -CAD -KHR -CAD Recirc Loop Sample Jet Pumps Description Instl.ines Line RHR 14. Line Size 14. -= = = = = N-50 0,E N-50B,C N-49B,C N-49E, F N-39A, B N-46A,B Number 4 < 9 N-50A N-38 07-N N-42 Penetration 15-N to

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#### PLANT Peach Bottom UNIT(S) II & III

#### PRIMARY CONTAINMENT ISOLATION SYSTEM DATA

Page \_6\_\_

						0	3		0	Mode o		. 6	3	0	v	alve	Posit	ion
Penetration Number	Line Size	Line Description	ESF (Yes/No)	Pig. No.	Fluid	Valve Number	leolation Group (Signal)	Valve	Valve Type	Primary Actuation	Secondary	Closure Time (Sec.)	Power	Position	Norma1	Shutdown	Post-	Power Failure
N-51C	1"	CACS Sample Line -CACS -CACS -CAD -CAD -RAD Gas	NO " Yes Yes	27	Air	SV-2671C SV-2978C SV-4960C SV-4961C SV-4966C	III III RM RM RM	Outside Outside Outside Outside Outside	sv sv sv sv sv	AC Coil DC Coil AC Coil AC Coil AC Coil			A B C C 3	I I N N	0 0 0 0 0 0 0	0 0 0 0 0 0 0 0	C C O C C	c c c c c
N-51D	1"	CACS Sample Return	No	28	Air	- sv-2980		Out si de	ck sv	Plow DC Co11			В .	- I	0	0	c	c
N-51E	1"	Inst Line - Recire Suction pressure		16	Water			Inside Outside	RO XFCV									
N-52E	1"	Inst :Line - Core Plate Pressure		16	Water	33		Inside Outside	RO XFCV									
N-52F	1"	Inst Gas Surrly	No	10	Air	- AO-2969B	II(A,B)	Outside Outside	CK DCV	Flow Inst Air	Spring	5	В	D	0	0	c c	c
N-53	8"	Chilled Wtr. fr Drywell cooler loop A	om NO	29	Water	MO-2201B	RM	Outside	GT	AC Motor	Manual	42	3	D	0	0	С	as is
N-54	8"	Chilled water from drywell coelers,LoopB	NO	29	Water	Мо-2200В	RM	Outside	GT	AC Motor	Manua I	42	3	D	0	0	С	as 1s
N-55	8"	Chilled wtr. fro drywell coolers Loop B	m No	29	Water	Mo-2200	RM RM	Outside	GT	AC Motor	Manual	42	3	D	0	0	С	as is
N-56	8"	Chilled wtr to Drywell cooler Loop A	No	29	Water	Mo-2201A	RM	Outside	GT	AC Motor	Manual	42	3	D	0	0	С	as 1s
N-57	-3/4"	Main stm.line "D" sample	No	24	Steam	A0-2316 A0-2-317	I(A,B,C,D	,E)Inside E) Outside	DCV DCV	Inst Gas InstAir	Spring Spring	5 5	A B	D D	cc	c	c	c

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#### PLANT Peach Bottom UNIT(S) II & III

#### PRIMARY CONTAINMENT ISOLATION SYSTEM DATA

Page 7

		BAR.				0	3		0	Mode Actua		<b>(9)</b>	3	0		Valve	Posi	tion
Penetration Number	Line Size	Line Description	ESF (Yes/No)	Pig. No.	Fluid	Valve Number	Isolation Group (Signal)	Valve Location	Valve Type	Primary Actuation	Secondary	Closure Iime (Sec.)	Power	Position	Normal	Shutdown	Post-	Power Failure
N-1023	1"	Inst.Line -Unit 2 Drywell Press		19	Air	53B,D 60B,D		Outside Outside	GB GB									
N-203	1"	CACS &CAD Sampl Line - CACS -CACS - CAD - Rad Gas	No No Yes	27	Air	SV-2671B SV-2978B SV-4960D SV-4966D	III III RM RM	Outside Outside Outside Outside	sv sv sv	AC Co11 AC Co11 AC Co11	Spring		A B D	I I N	0 0 0 0 0	0 0 0 0 0 0	C C C C	c c c
N-205A	20"	- Inst - CAD Torus Vacuum	Yes Yes Yes	30	Air	SV- 4961D AO-2502B	RM RM	Outside Outside Outside	GB SV B	-	Spring Spring	5	0 3	N D	C	C	0	C
H-200A		Brenker				9-26B	-	Outside Outside	VB GB	Flow	-	-		-	С	c	С	•
N-206A, E	2"	Inst Lines - Torus Level	Yes	15	Air/ water			Out side	GB									
N-210A, B	18"	RHR Test & Pool cooling return	Yes	31	Water	MD-10-34 A,B 10-19A,B,	VII	Out side	GB CK	AC Motor	Manual -	24	C,D	D -	c c	с о	0	as 12
N-211A,	6"	RHR Torus Spray				D												
В		-RHR	Yes	31	Water	MO-10-38 A,B	VII	Outside	GB	AC Motor	Manual	30	C,D	D	С	С	С	as 1s
		-RHR				MO-10-39 A,B	VII	Outside	GT	AC Motor	Manual	112	C,D	D	С	С	С	as is
		-RHR -CAD				MO-10-34 A,B	VII	Outside	GB	AC Motor	Manual	24	C,D	D	c	C	C	as is
		-CAD				SV-4950 A,B SV-4951	RM RM	Outside Outside	sv sv	AC Co11			C,D	N N	c	c	0	c
		-CAD				A,B		Out side	ck	Flow			-		С	c	0	-
N-212, 214,	12"	HPCI & RCIC Turbine Exhaust																
217B	1	-RCIC	No	33	Steam			Outside	SCK	Flow		-			0	0	0	-
		-RCIC	No			13-50	-	Outside	CK	Flow		-	:	:	0	0	0	-
		-RCIC	NO			RO-4240	TT	Outside	DCV	Inst Air	Spring	5	6	D	0	0	0	C
	24**	-RCIC -HPCI	No Yes		Steam	A0-4241 23-12	TT	Outside Outside	DCV SCK	Inst Air	Spring	5	6	D	0	0	0	C
	24.	-HPCI	Yes		Ceam	23-65		Outside	CK	Flow	-	- 1		- 1	8	8	8	-
		-HPC1	Yes			A0-4247	TT	Outside	DCV	Inst air	Spring	5	6	D	0	101	0	С

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## PRIMARY CONTAINMENT ISOLATION SYSTEM DATA

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-			_			0	3		3	Mode Actua			3	C		Valve	Posi	tion
Penetration Number	Line Size	Line Description	ESF (Yes/No)	Pie. No.		Valve Number	Isolation Group (Signal)	Valve	Valve Type	Primary Actuation	Secondary	Closure Time (Sec.)	Power	Position	Norma1	Shutdown	Post-	Power Failure
	2"	-HPCI -Vac relie -Vac relie			Air	AO-4248 MO-4244 MO-4244A	TT IV(C,D,E) IV(C,D,E)	Outside Outside Outside	DCV GT GT	Inst Aid DC Motor DC Motor	Spring Manual Manual	5 15 15	6 E F	D D D	0 0	0 0	0 C	C as is
N-213A	1"	Torus Drain (with level inst	-	15	Water			Out <b>s1</b> de	GB	垫								
N-215	1"	Inst Line -Unit 2 Torus level	-	15	Air			Outside	GB									
N-216	4"	HPCI Min. Flow	Yes	32	Water	23-62		Outside	СК	Flow	-	-	-	-	С	С	С	-
N-218A	1"	Inst. Gas Suppl	y No	10	Air	A0-2468	17.A,B)	Out si de Out si de	CK DCV	Flow Inst Air	Spring	5	В -	D	0	0	c c	č
N-218B	1"	CACS Sample	No	26	Air	SV-2671A SV-2978A	III	Outside Outside	sv sv	AC Coil	:	:	A B	I	0	0	c	C
N-218C	3/4"	ILRT Connection	No	18	Air	-	LC	Outside	GBC	Manual		-			С	c	С	
N-219	18"	Torus Purge						47.14		1 to the								
	1.0	Exhaust -CACS	No	34	Air	AO-2511	III	Outside	В	Int Air	Spring	5	A	D	C	0	C	C
		-CACS	No			AO-2512	111	Out si de	В	Int Air	Spring	5	В	D	C	0	С	C
		-CAD	Yes			AO-2513	III	Outs1de	DCV	Int Air	Spring	5	A	D	C	C	0	C
		-CAD -CACS	Yes			A0-2514	111	Outside	DCV	Int Air	Spring	5	В	D I	0	c o	C	c
		-CACS ANAL	No		110	SV-2671F SV-2978F	111	Outside	sv sv	AC Co11			A B	1	0	0	С	c
		-CAD	No Yes			SV-4960A	RM	Outside	sv	AC Co11			c	N	c	c	0	c
		-CAD	Yes			SV-4961A	RM	Outside	sv	AC Co11		.	c	N	С	c	0	С
		-Rad Gas	No			SV-4966A	RM	Outside	sv	AC Coil	.	-	3	N	с	С	С	С
N-221	2"	RCIC Vacuum	No	35	Air	13-10		Outside	SCK	Flow		.		-	0	0	0	
11-221		Pump Disch				13-38	-	Outside	CK	Flow	-	-		-	С	С	0	-
N-273	2"	HPCI Turbine Drain	Yes	35	Water	23-13 23-56	:	Outside Outside	SCK CK	Flow Flow		:	:	:	0 C	o c	0	:
N-224	10"	Core Spray test	Yes	36	Warer	MO 74-26	vi	Out si de	GE	AC Motor	Manual	1	с	c	С	С	с	as is

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#### PRIMARY CONTAINMENT ISOLATION SYSTEM DATA

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g.	Line Size	Line	ESF (Yes/No)	Pig. No.	Pluid	Valve Number	10 m		Valve Type	Mode of Actuation		<b>9</b>	3	0	Valve Position			
Penetration Number								Valve		Primary Actuation	Secondary	(Sec.)	Pove r Source	Position Indication	Normal	Shutdown	Post-	Power Failure
			No Yes		water	- 14-66A,C	:	Outside Outside	CKC CKC	Flow Flow	:	:	:	:	c	cc	c c	:
N-225	6"	RCIC & Torus Water Clearup Suct.	No No No	37	Water	MD-13-41 MD-14-70 Mo-14-71	RM II(/,B) II(A,B)	Outside Outside Outside	GT GT GT	DC Motor AC Motor D C Motor	Manual Manual Manual	33 20 20	E E	D D D	c c c	c c c	0 C C	as is
N-226A to D	24"	RHR Pump Suction	n Yes	38	Water	A to D RV-10-72	RM -	Outside Outside	GT RV	AC Motor	Manual -	30	A.B.C.D	D -	o c	0 C	o c	as 1s
N-227	16"	HPCI Pump Sucti	on Yes	39	Water	A to D MO-23-58	IV(A,B,C	Outside	GT	DC Motor	Manua 1	5	Y	D	С		0	as is
N-228 A to D	16"	Core Spray Pump suction	Yes	40	water	Mo-14-7 A to D	RM	Outside	GT	AC Motor	Manual	80	A,B,C,D,	D	6	0	0	as 1s
N-229	4"	Core spray pump Min Flow - Unit 2	Yes	41	Water	14-66B,D	:	Outside Outside	CK CK	Flow Flow	=	=	:	=	0 C	o c	0 C	3
N-230	2"	RCIC Pump Min	No	42	Water	13-29	-	Outside	СК	Flow				-	С	С	С	-
N-233	4"	HPCI Test Line- Unit 2	Yes	43	Water	MO- 23-31	V(D,F)	Outside	GT	DC Motor	Manua	15	P	D	С	С	С	as 1s
N-234	10"	Core scray rest	Yes	44	Water	MO-14-268	VI	Outside Outside	GB CK	AC Motor	Manual	14	D	D	c c	c c	c	as 1s
N-234A N-234B	10"	Core Spray test Line - Unit 3 Core Spray Test Line - Unit 3		44	Water Water	MO-14-268 Mo-14-264	VI VI	Outside Outside Outside Outside	GB GB <sup>CK</sup> CK(2)	AC Motor	Manual Manual Flow	14	C -	D D	CCCC	6	- 1	as is
N-235	4"	HPCI Test Line Unit 3	Yes	43	Water	мо-23-31	V(DF)	Out si de	GT	DC Motor	Manual	15	P	D	С	С	С	as is
I-236A	4"	Core Spray Pump Min. Flow - Unit 3	Yes	45	Water	14-66B,D		Out side	СК	Plow				-	0	0	0	-
N-236B	4"	Core Spray Pump Min Flow - Unit 3	Yes No	41	Water	14-66-A,C		Out side	CK CK	Flow	:	:	-	-	0	0	0	-

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PLANT Peach Bottom UNIT(S) 11 6 111

PRIMARY CONTAINMENT ISOLATION SYSTEM DATA

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	Pailist	
ton	Tower	
Valve Position	Post-	
ve P	Shutdown	
Val	[amrow]	
3	Indication	
	Position	
9	Power	
9 ,,	Closure Tim	
f	Secondary	
Mode of Actuation	Primary	
9	Valve	8
	Velve	Out s I de
0	Isolation Group (Signal)	
0	Valve Number	
	Pluid	At the state of th
	Pig. No.	<u>`</u>
(	(0N/**X) 4SZ	2
	Line	Inst.Line - Unit 3, Torus Level
	Line Stre	
	Penetration Number	м-250

#### PEACH BOTTOM ATOMIC POWER STATION Containment Isolation Valves

#### NOTES:

 Valve Numbering: All valve numbers apply to both units, except 4 digit numbers. For those valves, the first digit designates the unit: 2 or 4 - Unit 2; 3 or 5 - Unit 3.

2.	Valve	Types:	GB	- Globe	DCV	- Diaphram Control Valve
-		-,,	GT	- Gate	VB	- Vacuum Breaker
			CK	- Check	XV	- Explosive Valve
			BL	- Ball	RO	- Restricting Orifice
			В	- Butterfly	BCK	- Ball Check
			sv	- Solenoid	HCU	- Hydraulic Control Unit
			RV	- Relief	XFCV	- Excess Flow Check Valve
			SCK	- Stop Check		

#### 3. Isolation Signals:

	A. Reactor Low Water Level (-48")
Froup I	
	C. High Steam Tunnel Temp. (200AF)
	D. Low Steam Line Pressure (850 psi in kan mode)
	E. High Steam Line Radiation (3 x normal)
roup II	A. Reactor Low Water Level (o")
	B. High Drywell Pressure (2 psig)
	C. RWCU High Flow (300%)
	D. RWCU non-regen. heat exch. high temp. (200AF)*
	E. High Reactor Pressure (shutdown cooling - 75 psig)
	F. High Reactor Pressure (600 psig)
	G. Standby Liquid Control System
	Operation*
Froup III	A. Reactor Low water Level (0")
	B. High Drywell Pressure (2 psig)
	C. Reactor Bldg. High Radiation
	(16 mr/hr)
	D. Refueling Floor High Rad. (16 mr/hr)
Group IV	A. RCIC Steam Line High Flow (300%)
	B. RCIC Steam Tunnel High Temp.
	200AF)
	C. RCIC Steam Line Low Pressure (50 psig)*
	D. High Drywell Pressure (2 psig)
	E. RCIC Steam Line Isolated
Group V	A. HPCI Stm. Line High Flow (300%)

- B. HPCI Stm. Tunnel High Temp. 200AF)
- C. HPCI Stm. Line Low Pressure (100 psig)\*
- D. High Drywell Pressure (2 psig)
- E. HPCI Stm. Line Isolated
- F. Reactor Low Water Level (-48")
- Group VI Reactor Low Water Level (-144")
   High Drywell Pressure (2 psig)

Group VII LPCI Initiation:

- Reactor Low Water Level (-144")
   High Drywell Pressure (2 psig)
   & Reactor Low Pressure (450 psig)
- RM Remote Manual
- M Manual (local only)
- LC Locked Closed
  TT Turbine Trip\*
- RMP Push Bottom, momentary contact opens valve for test
- \* Process Signals
  - 2. Valve control cables are not presently assigned to a safeguard channel. Modification in progress to supply valve with correct designation, diverse isolation signal, and proper reset logic.
- 4. "S" indicates standard closing time. The standard minimum closing rate for automatic isolation valves is based on a nominal line size of 12 inches. Using the standard closing rate, a 12-inch line is isolated in 60 seconds. Conversion to closing time can be made on this basis using the actual size of the line in which the valve is installed.
- 5. The power supplies for the valves are identified as one of the following:
  - A safeguard AC channel A (onsite emergency diesel buses)
  - B safeguard AC channel B (onsite emergency diesel
  - buses)

    c = safeguard AC channel C (onsite emergency diesel buses)
  - D safeguard AC channel D (onsite emergency diesel
  - E safeguard DC channel A (onsite emergency diesel buses)
  - F safeguard DC channel B (onsite emergency diesel buses)
  - N non-safeguard

For cable routing purposes, channels A&C - AC and A-DC are assigned to Division I and channels B&D - AC and B-DC are assigned to Division II.

#### The following special notes apply:

- 1. The power for valve 10-25A automatically transfers between A and C depending upon availability. The controls are assigned to safeguard channel A. The power for valve 10-25B automatically transfers between B and D depending upon availability. The controls are assigned to safeguard channel C.
- Tescable check valve, power and controls do not affect isolation function.
- 3. Valve control cables are not presently assigned to a safeguard channel. Modification in progress to supply valves with correct designations.
- 4. Valves are not powered from onsite supplies and control cables are not assigned to safeguard raceways. Modification in progress to correct concern.
- 5. Controls for the TIP ball, shear and purge valves are not separated and are not assigned to safeguard channels.
- 6. Valve control cables are not presently assigned to a safeguard channel. Modification in progress to supply valve with correct designation, diverse isolation signal, and proper reset logic.
- 6. Position indication for the valves is identified as follows:
  - D. direct indication from position switches at the valve.
  - I. indirect indication usually light is electrically parallel to solenoid.
  - N. no indication as to valve position.

Position is indicated in the control room.

- 7. Isolate only if in shutdown cooling mode.
- 8. Modification in progress to cap this line.

### PBAPS

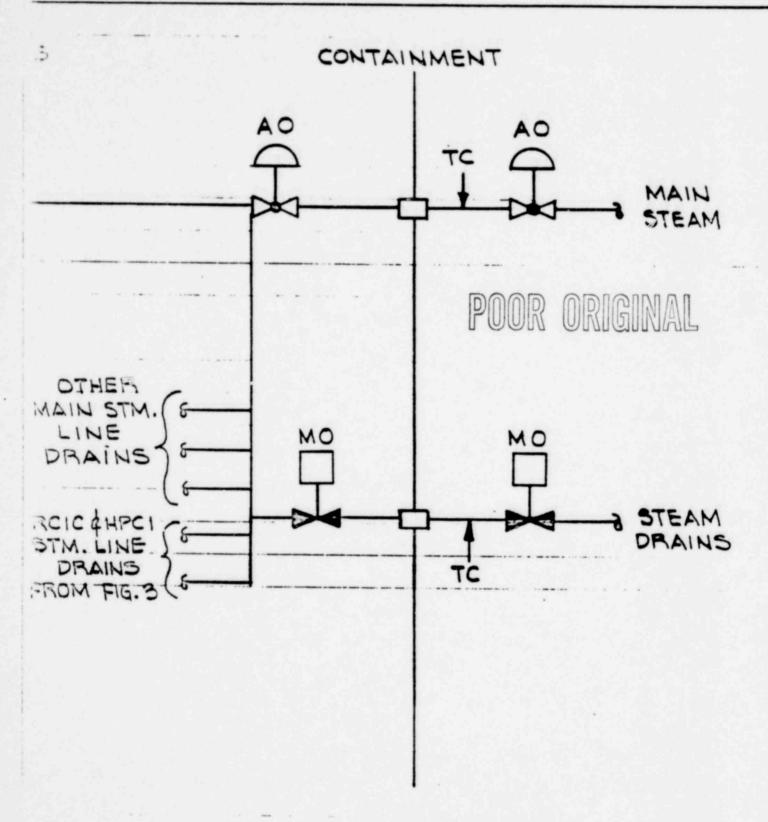
### CONTAINMENT ISOLATION VALVE ARRG'T.

	_	_	-		
1	_	( -	Marie .	NI	D
_	_	<b>~</b>	-	1	-

LETTERS	DESCRIPTION
AO	AIR OPERATED VALVE
MO	MOTOR OPERATED VALVE
TC	TEST CONNECTION
1,05	REACTOR COOLANT SYSTEM
TCK	TESTABLE CHECK YALVE
SV	SOLENOID OPERATED VALVE
RO FL	OW RESTRICTING ORIFICE
LC Y	ALVE LOCKED CLOSED
CV	CONTROL VALVE
XV POOR ORIGINAL	EXPLOSIVE VALVE
MBOLS	
-10 - BALL VALVE	
- FLOW LIMITING (OR EX	CESS FLOW CHECK VLV.)
- CHECK VALVE	L MOTOR
GLOBE VALVE	ACTUATED VALVE
-DO- GATE VALVE	SOLEHOID
P DIAPHRAM	ACTUATED VALVE
ACTUATED VALVE	I. FLOW
- STOP CHECK VALVE	THE RESTRICTING ORIFICE
BUTTERFLY VALVE	EXPLOSIVE VALVE
OIAPHRAM ACTUATED	
- CONTROL VALVE	OPEN NORMALLY
TES:	STRAINER
	CORRESPONDING TO NORMAL POWER
PERATION.	

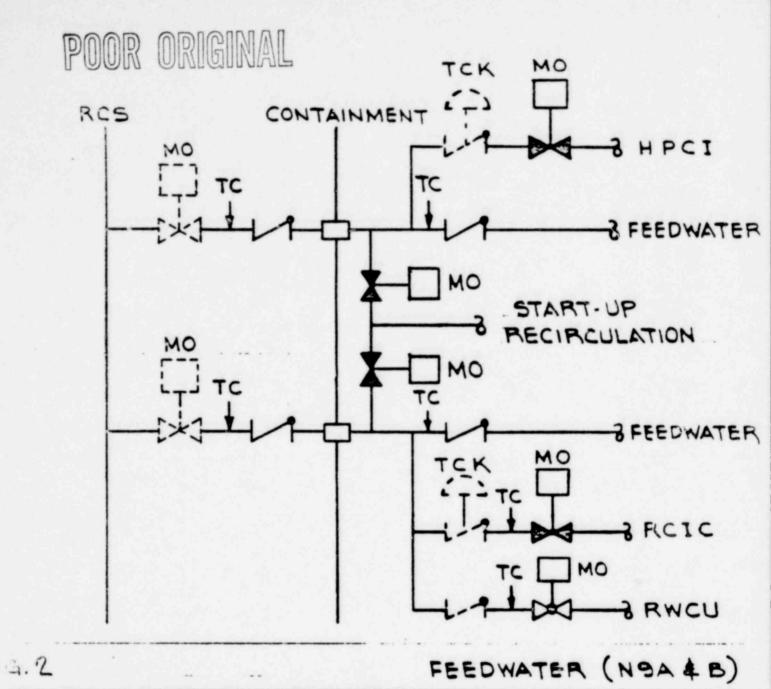
POTTED VLY'S DO NOT NORMALLY PERFORM A CONTAINMENT ISOL. FUNCTION

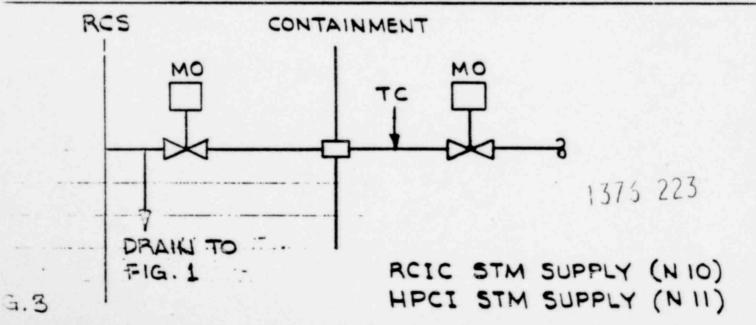
# CONTAINMENT ISOLATION VALVE ARRG'T.



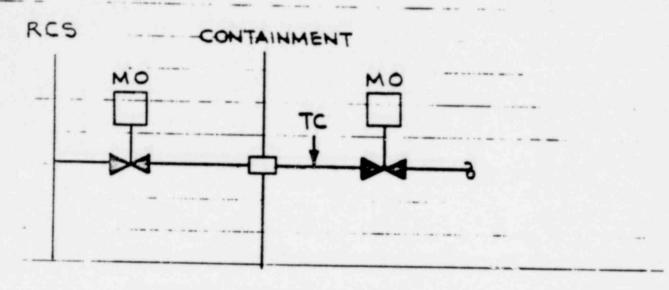
MAIN STEAM LINE (N-7A TO D)

STEAM DRAINS (N-8)

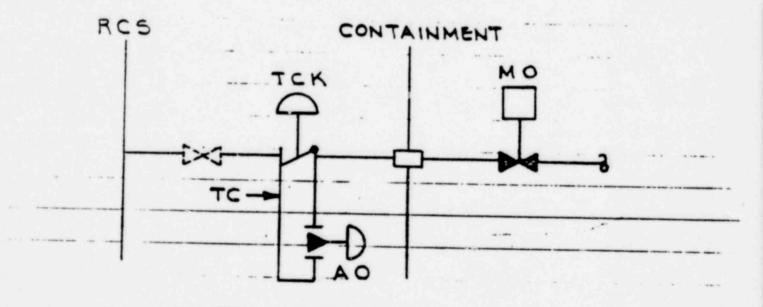




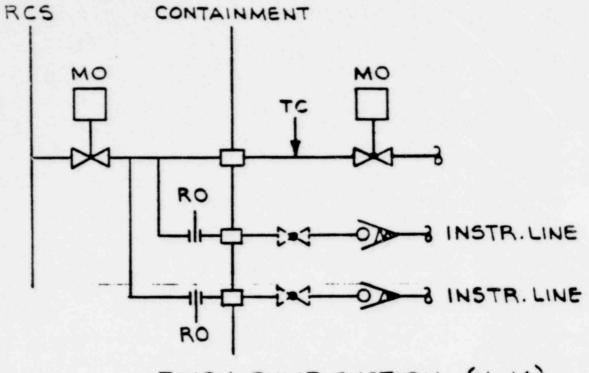
51.5



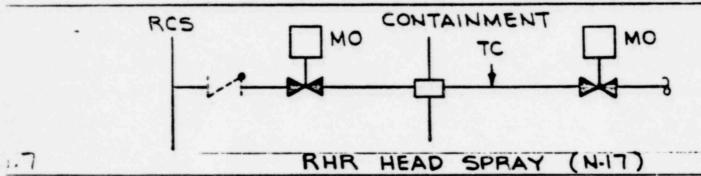
RHR SHUTDOWN COOLING SUCTION (NIZ



RHR SHUTDOWN COOLING RETURN (N-13A &B)



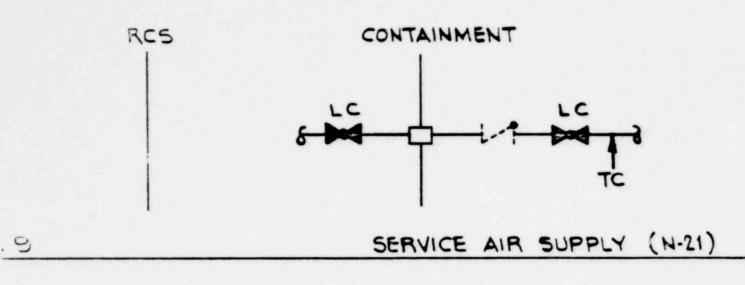
RWCU PUMP SUCTION (N-14)
INSTRUMENT LINE (N-50D,E)

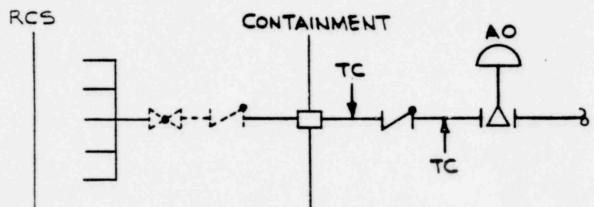


DRYWELL EQUIP DRN. SUMP DISCH. (N-18)
DRYWELL FLOOR DRN. SUMP DISCH. (N-19)

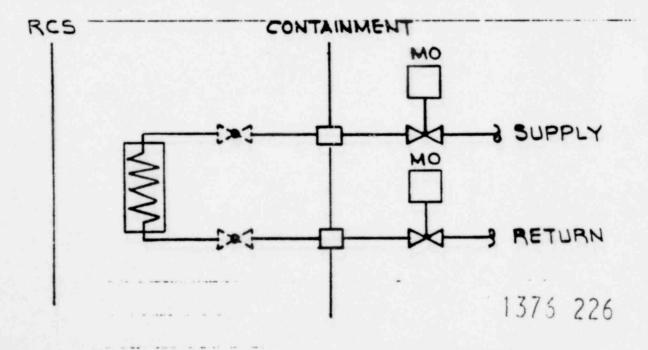
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1. 6





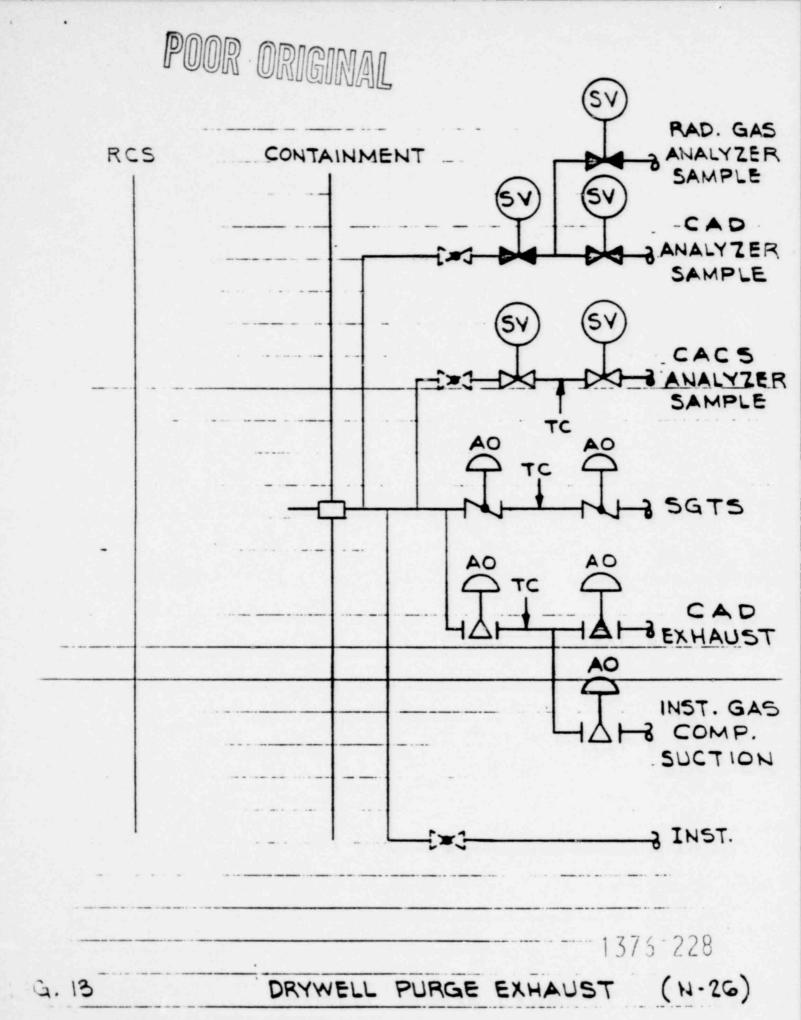
.10 INST. GAS SUPPLY (N-22, N-52F, N-218A)



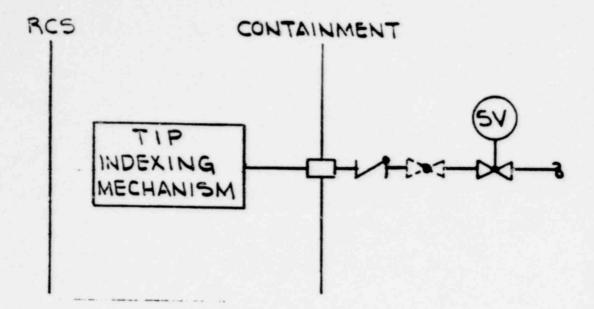
RBCW (N-23 4 N-24)

POOR ORIGINAL RPV CONTAINMENT N2 PURGE N 25 PURGE SUPPLY DRYWELL TORUS N205B & INSTRUMENT N2 MAKE UP SUPPLY TC 1375 227 DRYWELL & TORUS PURGE SUPPLIES ( N-25 & N-205B) 4.12

-47-



-48-



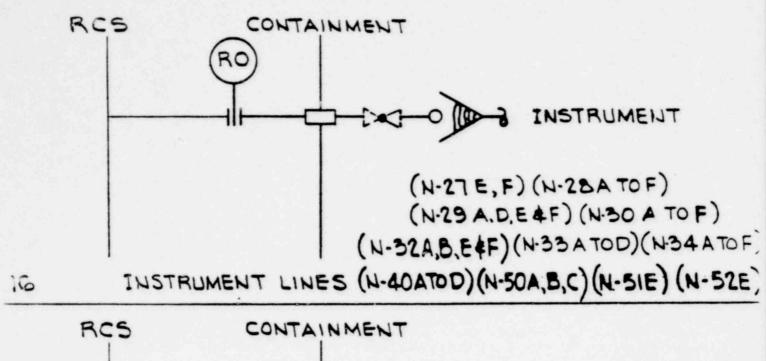
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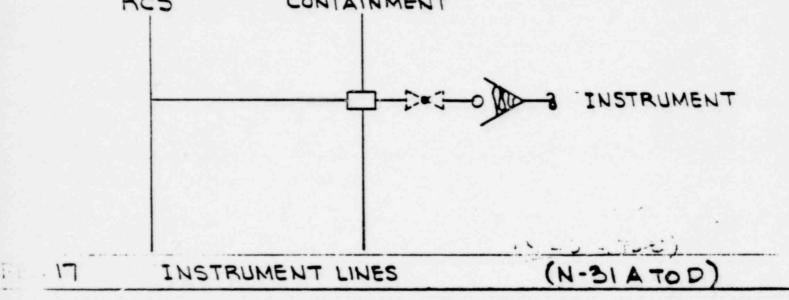
SUPP.
POOL

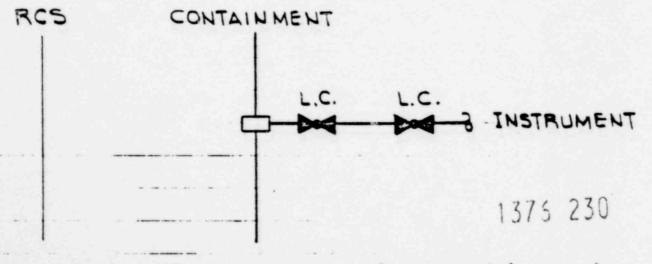
POOL

SUPP.
P

(N-206A,B) (N-215)
INSTRUMENT LINES (N-213A) (N-250)

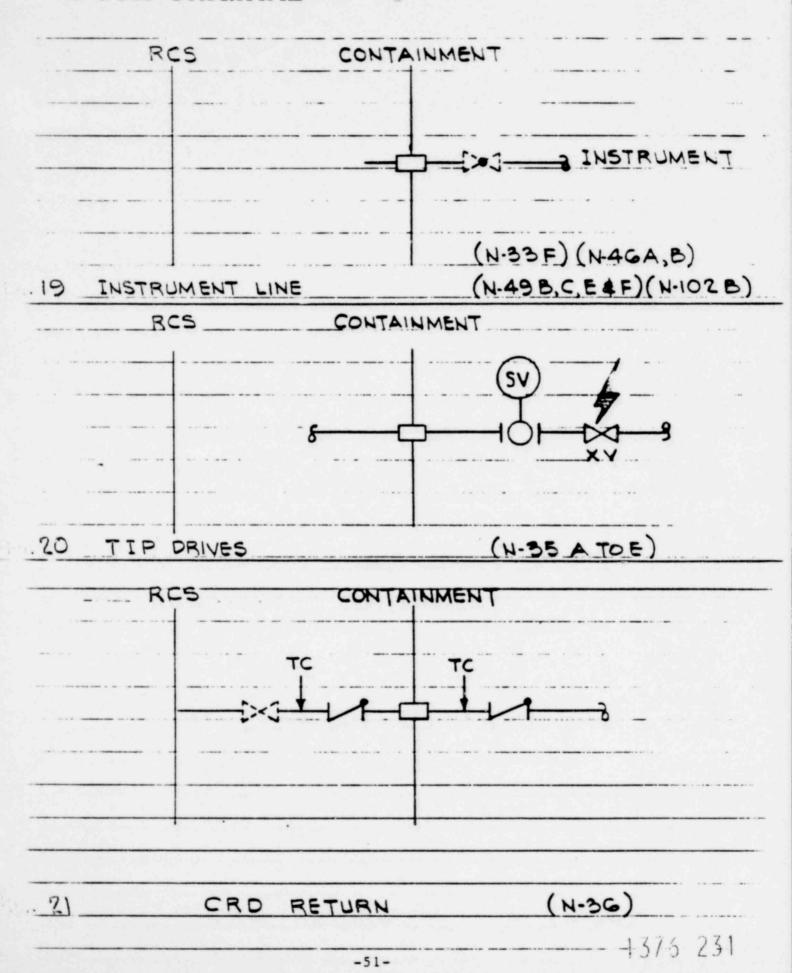


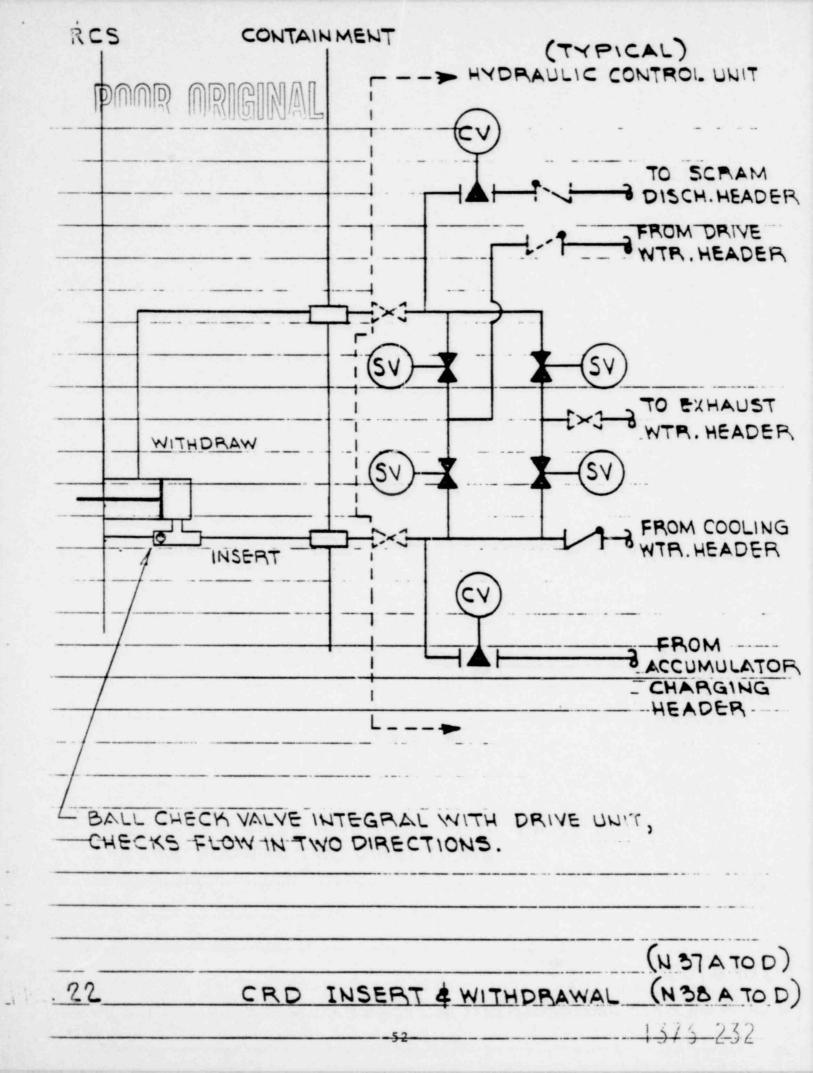


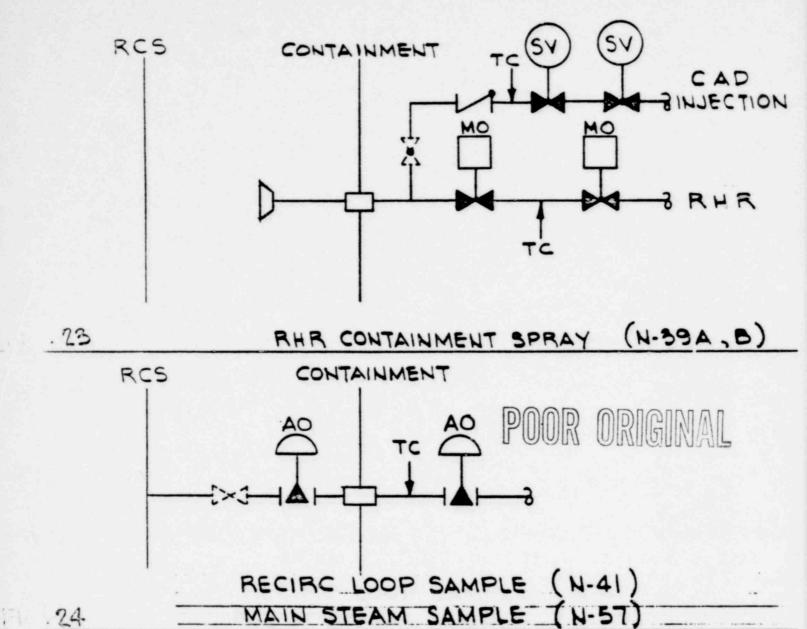


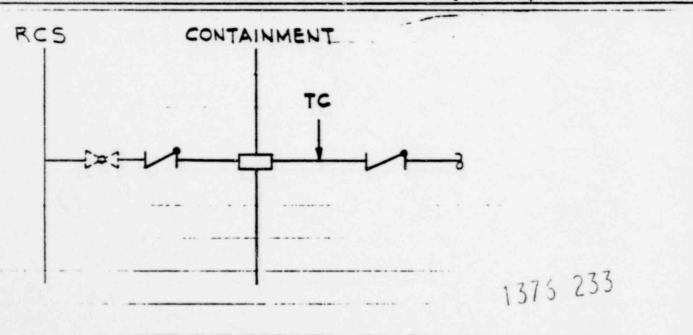
ILRT CONNECTIONS

(N-32 C,D) (N-218 C)



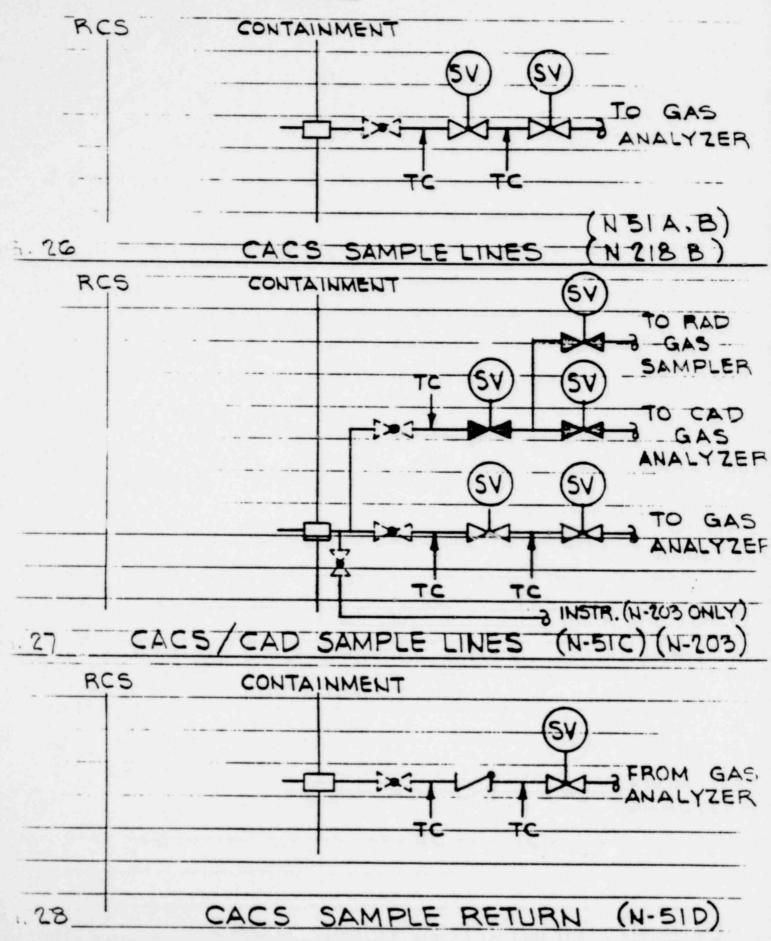




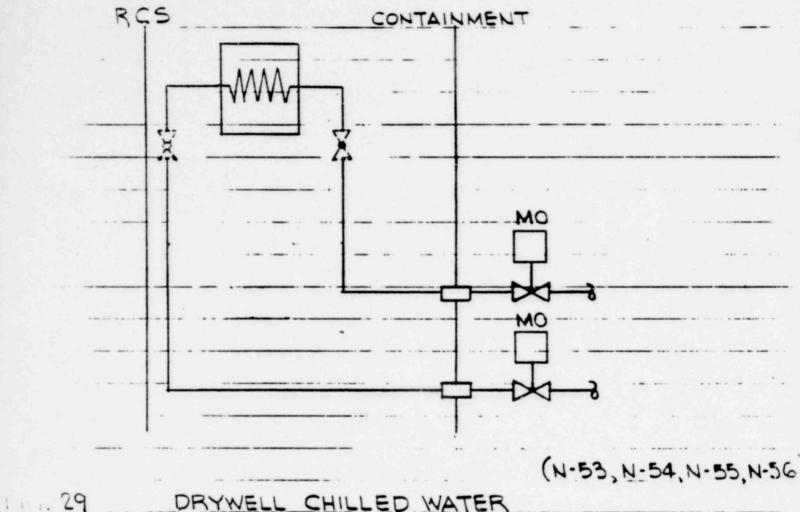


STAND-BY LIQUID CONTROL

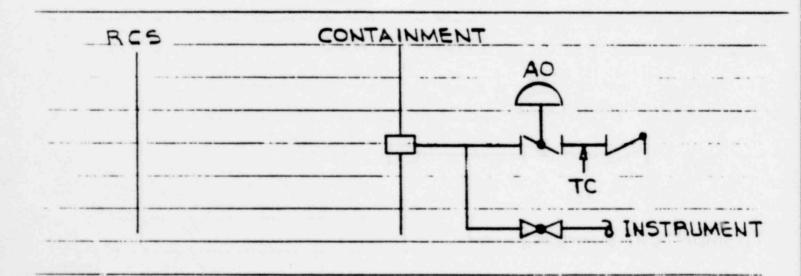
(N-42)



...30

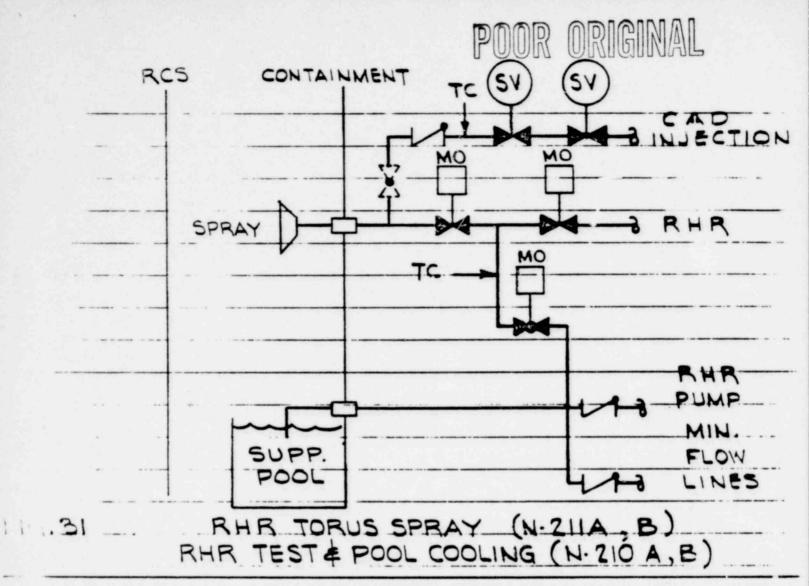


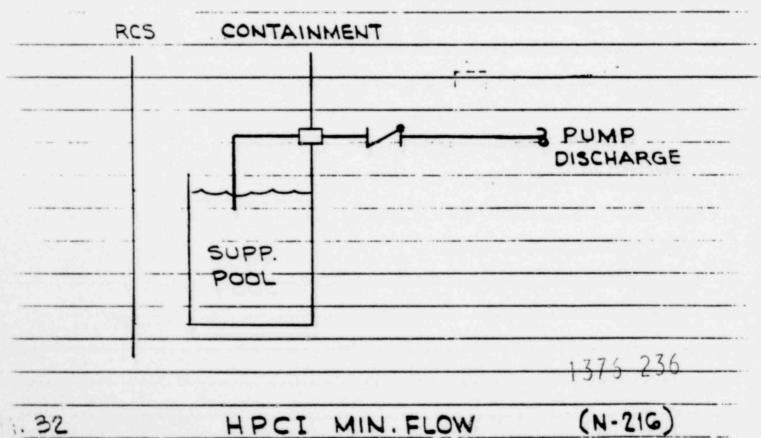
DRYWELL CHILLED WATER

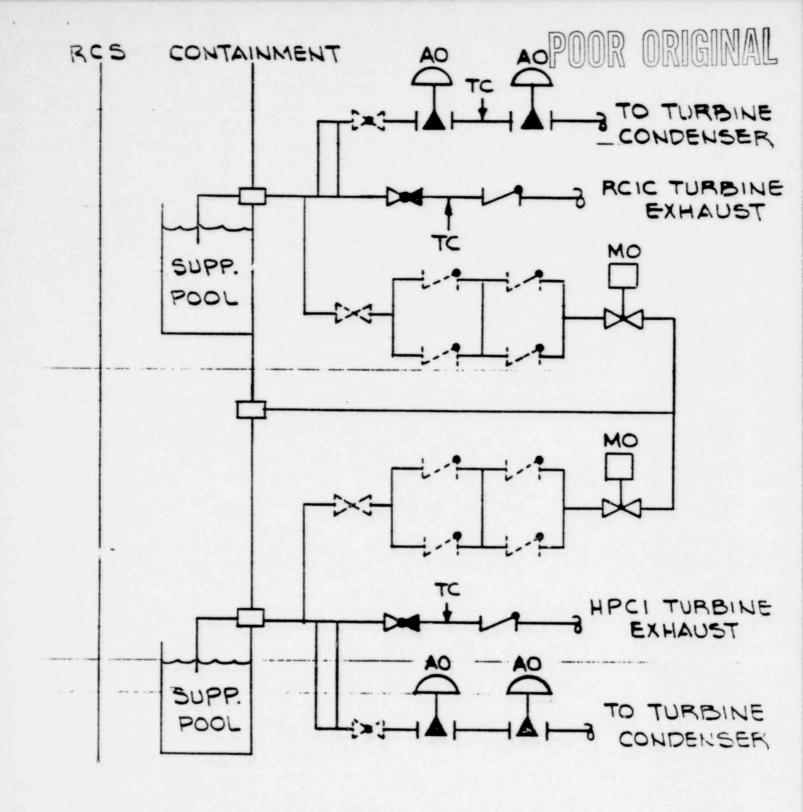


-55-

(N.205A) VACUUM BREAKER TORUS



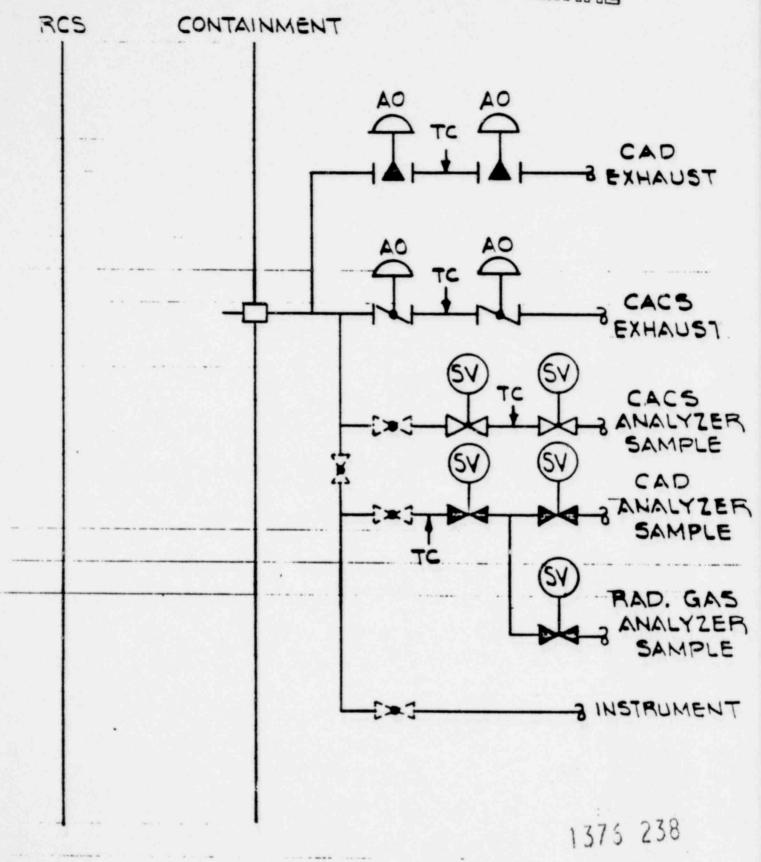




RCIC TURBINE EXHAUST (N-212)

HPCI TURBINE EXHAUST (N-214)

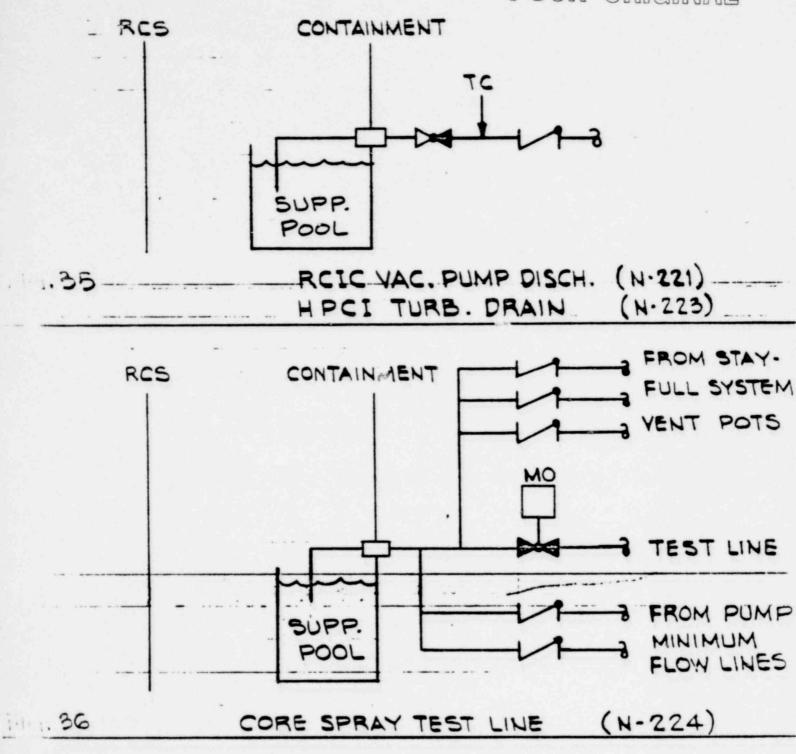
HPCI & RCIC VACUUM RELIEF (N-217B)

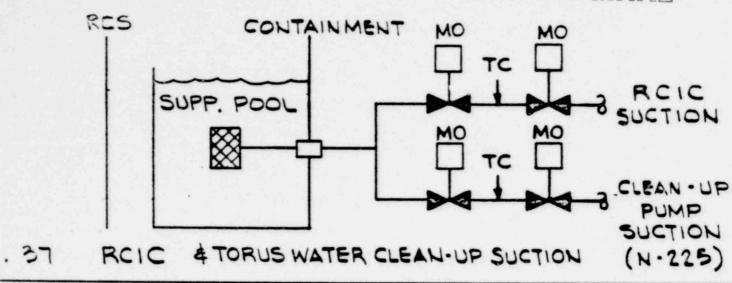


G.34

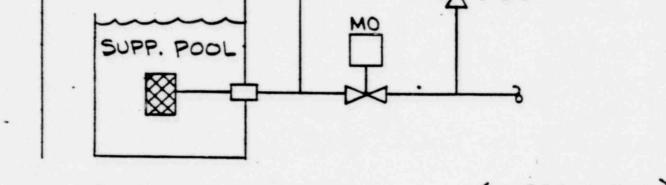
TORUS PURGE EXHAUST

(N-219)





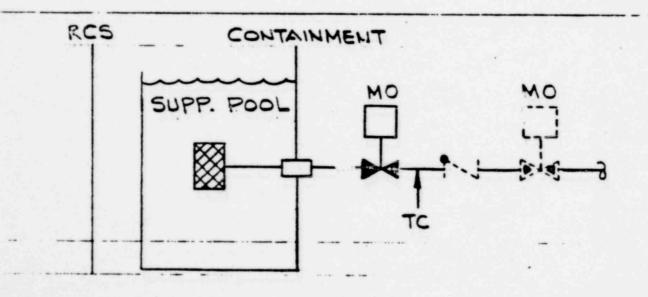
CONTAINMENT



38 RHR PUMP SUCTION

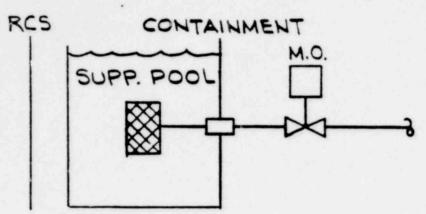
RCS

(N-226 A TOD)

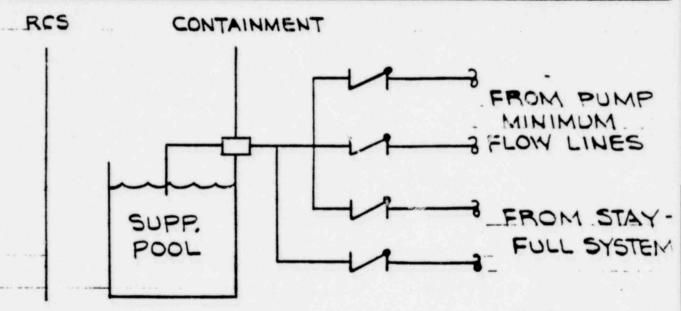


HPCI\_SUCTION

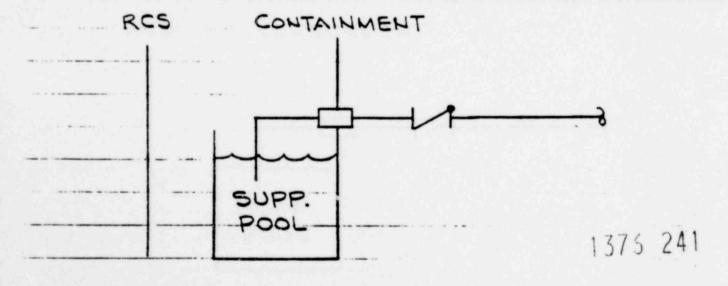
(N-227)



#### CORE SPRAY PUMP SUCTION (N-228 A TOD) . 40

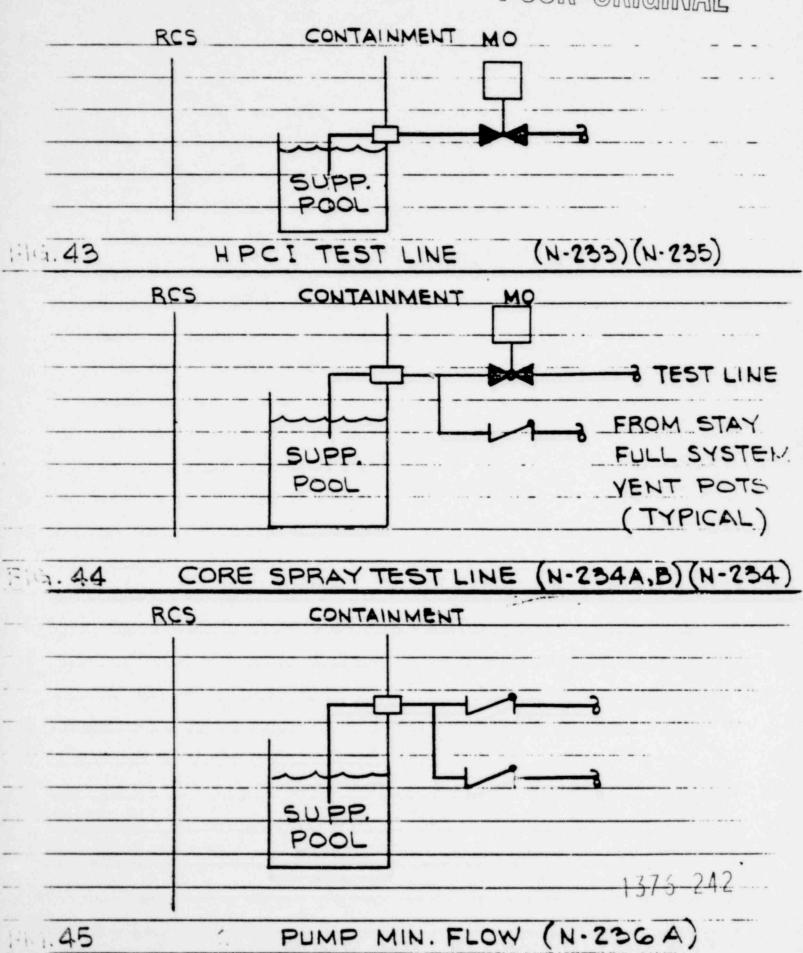


#### CORE SPRAY PUMP MIN FLOW (N-229) (N-236 B) . 41



RCIC PUMP MIN. FLOW (N-230)

1.42



#### PLANT Peach Bottom UNIT(S) II & III

DESIGN REQUIREMENTS FOR CONTAINMENT ISOLATION BARRIERS

#### Question:

Discuss the extent to which the quality standards and seismic design classification of the containment isolation provisions follow the recommendations of Regulatory Guides 1.26, "Quality Group Classifications and Standards for Water-, Steam-, and Radioactive-Water-Containing Components of Nuclear Power Plants", and 1.29, "Seismic Design Classification".

#### Response:

NRC regulatory Guides 1.26 and 1.29 had not been issued at the time Peach Bottom Atomic Power Station was being designed and constructed. The approach to Quality Group and Seismic Class of the piping and valves associated with each line penetrating primary containment is described in the FSAR, Appendix A.

Appropriate Quality Groups are listed on the attached table. All lines penetrating primary containment are Seismic Class I, out to and including the outer isolation valve, with the following exceptions:

 Piping at the following penetrations is presently being upgraded to Seismic class I:

N-21, Service Air Supply N-23, 24 RBCW to and from Recirc. Pumps N-53 to 56 Chilled Water to and from Drywell Coolers

2) Evidence of seismic analysis of the following small lines can not be located at the present time:

# Penetration N-36 A to E N-35F Line Description TIP Drives TIP Purge

Our Engineering Department is continuing to investigate these lines. Reanalyses and/or modifications will be made as necessary to meet seismic standards.

3) Seismic analyses for certain valves can not be located at the present time. All appropriate manufacturers have been contacted and are in the process of supplying analyses for these valves.

#### PLANT \_ Peach Bottom UNIT(S) II & III

#### PROVISIONS FOR TESTING

#### Question:

Discuss the design provisions for testing the operability of the isolation valves.

#### Response:

Isolation valves are designated for operability testing as follows:

- a. power operated, automatically initiated isolation valves are tested once per operating cycle for simulated automatic initiation and closure times.
- b. normally open, power operated isolation valves (except MSIV's) are fully closed and reopened once per quarter.
- c. MSIV's are tripped individually to verify closure time at less than 75% reactor power, once per quarter.
- d. Instrument line excess flow check valves are tested once per operating cycle.

Local leak rate tests are performed once per operating cycle, as indicated on the attached table.

#### PLANT Peach Bottom UNIT(S) II & III

#### CODES, STANDARDS, AND GUIDES

#### Question:

Identify the codes, standards, and guides applied in the design of the containment isolation system and system components.

#### Response:

The following codes, standards, and guides were applied in the design of the containment isolation system and system components:

10 CFR 50, Appendix A, General Design Criteria 54, 55, 56, and 57

IEEE 279 (August 1968)

ANSI B31.1.0 (1967)

Other codes and standards used for design, fabrication, installation, and inspection of piping systems are discussed in detail in FSAR, Appendix A.

By NRC request, isolation valve testing provisions have been reviewed against 10 CFR 50, Appendix J. A Technical Specification change request resulting from this review was submitted in November, 1976.

#### PLANT Peach Bottom UNIT(S) II & III

#### NORMAL OPERATING MOLES AND ISOLATION MODES

#### Question:

Discuss the normal operating modes and containment isolation provision and procedures for lines that transfer potentially radioactive fluids out of the containment.

#### Response:

The following are the systems that have the ability to transfer potentially radioactive gases or liquids outside the primary containment:

#### Gas Systems

Containment Ventilation and Purging System
Drywell Oxygen Analyzer System
Standby Gas Treatment System
Containment Atmospheric Dilution System
CAD Oxygen and Hydrogen Analyzer Systems
Main Steam Lines and Drains
Reactor Core Isolation Cooling Steam Line
High Pressure Coolant Injection Steam Line

#### Liquid Systems

Residual Heat Removal System
Core Spray System
High Pressure Coolant Injection System
Reactor Core Isolation Cooling System
Reactor Water Cleanup System
Drywell Sump Systems
Torus Water Cleanup System
Primary Coolant Sampling Systems

- a. No interlocks currently exist to prevent transfer of potentially radioactive gases or liquids when high radiation levels exist in the primary containment. However, the applicable procedures do require measurement of activity levels within containment prior to venting of containment or resetting of isolation signals.
- b. All such systems are isolated by the applicable containment isolation signals with the exception of the following:
  - The containment Atmospheric Dilution System Oxygen and Hydrogen Analyzer System which is required for post LOCA gas analysis.

- 2. The Residual Heat Removal System sample valves. An Engineering review request has been initiated to review the design to determine if automatic isolation of these lines is necessary
- c. The functional capability of the Primary
  Containment Isolation System is verified by
  surveillance testing every 6 months in accordance
  with the Technical Specifications.

#### P3APS

#### APPENDIX A

#### PRESSURE INTEGRITY OF PIPING AND EQUIPMENT PRESSURE PARTS

#### CONTENTS

#### A.1 SUMMARY DESCRIPTION

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- A.2 CLASSIFICATION OF PIPING AND EQUIPMENT PRESSURE PARTS

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- A.3.1.1 Allowable Stresses
- A.3.1.2 Wall Thickness
- A.3.1.3 Reactor Vessel Nozzle Load
- A.3.1.4 Seismic Design
- A.3.1.5 Analysis of Piping
- A.3.2 Valve Design
- A.3.3 Pump Design

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- A.4.2 Furnace Sensitized Stainless Steel Materials

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#### 2BAPS

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- A.7.1.1 Welds
- A.7.1.2 Castings
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- A.7.2.1 Forgings
- A.7.2.2 Piping and Fittings
- A.7.3 Liquid Penetrant Testing A.7.4 Magnetic Particle Testing
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Schedule II

Schedule III

#### PBAPS

#### APPENDIX A

#### PRESSURE INTEGRITY OF

#### PIPING AND EQUIPMENT PRESSURE PARTS

#### FIGURES

Figure No.

Title

A.2.1 Piping Code Classification (NSSS)

#### PB7.PS

#### APPENDIX A

#### PRESSURE INTEGRITY OF

#### PIPING AND EQUIPMENT PRESSURE PARTS

#### TABLES

Table No.		Title							
A.9.1	Summary	Classification of Piping Systems							
A.9.2	Summary	of Equipment Design Guides							

#### APPENDIX A

# PRESSURE INTEGRITY OF PIPING AND EQUIPMENT PRESSURE PARTS

#### A.1 SUMMARY DESCRIPTION

This appendix provides additional information pertinent to the preceding sections concerning the pressure integrity of piping and equipment pressure parts.

Piping and equipment pressure parts are specified according to service and location. The design, fabrication, examination, and testing requirements are defined for the equipment of each category to assure the proper pressure integrity.

For the purpose of this appendix, the pressure boundary of the process fluid includes but is not necessarily limited to: branch outlet nozzles or nipples, instrument wells, reservoirs, pump casings and closures, blind flanges, studs, nuts, and fasteners in flanged joints between pressure parts, bodies and pressure parts of inline components, such as traps and strainers, and instrument lines up to and including the first shutoff valve.

Specifically excluded from the scope of this appendix are vessels and heat exchangers or any components which are within the scope of the ASME Boiler and Pressure Vessel Code, Sections III and VIII; and non-pressure parts such as pump motors, shafts, seals, impellers, wear rings, valve stems, gland followers, set rings, guides, yokes, and operators; and non-metallic material such as packing and gaskets; fasteners not in pressure part joints such as yoke studs and gland follower studs; and washers of any kind.

This appendix defines the design limitations for piping and valves associated with the reactor coolant primary pressure boundary (nuclear steam supply), primary containment pressure boundary (drywell) and related auxiliary systems within the power generation (operational) systems.

Table A.9.1 specifies systems falling within the applicable codes and the scope of this appendix.

# A.1.1 Code and Specifications

The piping and equipment pressure parts in this nuclear power plant are designed, fabricated, inspected, and

tested in accordance with recognized codes, as far as these codes can be applied, and in accordance with project specifications. Where conflicts occur between the industrial codes and project specifications, the project specifications take precedence.

All piping systems within the scope of this Appendix including pipe, flanges, bolting, valves and fittings are in accordance with ANSI B31.1.0, "Power Piping," including requirements for design, erection, supports, tests, inspections, and additional requirements specified herein.

The weld reinforcement height limitations recommended for pipe butt welds in paragraph 127.4.2 (d) and 127.4.3 of ANSI B31.1.0 (1967) for those piping systems not within the scope of ANSI B31.1.0 Case 74, are modified as follows:

- a. Under cutting shall not exceed 1/32 inches deep, provided it does not encroach on the minimum wall thickness.
- b. The maximum thickness of reinforcement of butt welds shall not exceed the values tabulated below, when the thickness of the thinner component being joined is considered:

Thickness of Base Metal (inches)	Thickness of Reinforcement* (inches)			
	Column I	Column II		
Up to 3/16 inclusive Over 3/16 to 1/2 inclusive Over 1/2 to 1 inclusive	1/16 1/8 5/32	1/16 1/16 3/32		
Over 1 to 2 inclusive Over 2	3/16	1/8 5/32		

\* The weld reinforcement thickness shall be determined from the higher of the abutting surfaces involved.

For double welded butt joints, the limitation on reinforcement given in Column I shall apply separately to both inside and outside surfaces of the joint.

For single welded butt joints, the reinforcement limits given in Column I shall apply to the outside only and the reinforcement given in Column II shall apply to the inside.

The plant piping is classified in three groups, depending on the design requirements for the service.

The design requirements for piping systems designated in Groups I and II are in accordance with the requirements of ANSI B31.1.0 (1967) and supplementary requirements in the project specifications. Namely, these systems require full radiography and supplementary surface inspections of the weld joints and supplementary non-destructive test requirements of the pressure components. Additionally, some of these piping systems are analyzed for seismic Class I design criteria as indicated in Table A.9.1.

The design requirements for some piping in Group III, such as main steam lines downstream of the outer isolation valve to the main turbine stop valve, but excluding the stop valves, are in accordance with the requirements of ANSI B31.1.0 (1967) and supplementary requirements in the project design specifications, namely, full radiography of pressure weld joints.

The above mentioned systems in Groups I and II and a portion of Group III are designated as "critical piping" for design, stress analysis, fabrication, inspection, erection, testing and quality control purposes.

The remaining portion of piping systems in Group III is in accordance with ANSI B31.1.0 and these systems are designated as non-critical systems.

Table A.9.1 summarizes the classification of piping systems and Table A.9.2 lists design guides for plant equipment.

## A.2 CLASSIFICATION OF PIPING AND EQUIPMENT PRESSURE PARTS

Piping and equipment pressure parts may be classified as follows and as shown on Figure A.2.1:

Group I - Piping and equipment pressure parts within the reactor primary pressure boundary through the outer isolation valve, inclusive.

Group II - Piping and equipment pressure parts downstream of the outer isolation valve and extensions of containment and the Core Standby Cooling Systems.

Group III - Balance of plant piping and equipment pressure parts, including power generation systems.

## A.3 DESIGN REQUIREMENTS

## A.3.1 Piping Design

Pressure and temperature conditions to which the piping pressure components are subjected are described in the appropriate system design section of the FSAR.

## A.3.1.1 Allowable Stresses

The allowable stresses for piping design are as follows:

- a. For carbon steel, the allowable stress values of ANSI B 31.1.0 are used.
- b. For austenitic stainless steel, the allowable stress values of ANSI B31.1.0 are used. For material not covered by ANSI B31.1.0, the higher stress values of the ASME Boiler and Pressure Vessel Code, Section I, Appendix A-24 are used.

## A.3.1.2 Wall Thickness

Pipe wall thickness, fittings, and flange ratings are in accordance with ANSI B31.1.0, including adequate allowances for corrosion and erosion according to individual system requirements for a design life of 40 years.

## A.3.1.3 Reactor Vessel Nozzle Load

All piping including instrument piping connecting to the reactor pressure vessel nozzles is designed so that the nozzle to pipe interface load will not result in stresses in excess of the allowable material stresses. Thermal sleeves are used where nozzles are subjected to high thermal stresses.

# A.3.1.4 Seismic Design

Seismic Class I piping is defined as that portion of a piping system whose failure might cause, or increase the severity of, the design basis accident, or which is essential for safe shutdown of the reactor.

The piping is designed and supported to satisfy seismic criteria specified in the loading criteria (Appendix C).

The piping systems indicated as seismic Class I in Table A.9.1 are analyzed for the maximum credible seismic condition.

## A.3.1.4.1 Supplementary Analysis of Seismic Class I Piping

Seismic Class I piping is classified as either rigid or flexible. Rigid piping is that which has a fundamental frequency in the rigid range of the spectrum curves for the building locations. This corresponds to frequencies greater than 20 Hz. These piping systems are analyzed with static loads corresponding to the acceleration in the rigid range of the spectrum curves.

The dynamic analysis of flexible seismic Class I piping systems for seismic loads is performed using the spectrum response method, as applied to a lumped mass mathematical model of the piping systems. The maximum responses of each mode are calculated and combined by the root-mean-square method to give the maximum response quantities resulting from all odes. The response thus obtained was combined with the results produced by other loading conditions to compute the resultant stresses. All modes are used which have frequencies less than 20 Hz. The percentage of critical damping for all modes is 0.5 for the design earthquake and the maximum credible earthquake.

In lieu of the above procedure, some seismic Class I piping is analyzed for a static load equivalent to the peak of the spectrum curve for the applicable floor elevation.

The horizontal acceleration spectrum curves applied to the piping systems are developed as part of the seismic analysis for the building in which the piping is located.

# A.3.1.5 Analysis of Piping

# a. Primary Stresses (Sp)

Primary stresses are as follows:

- Circumferential primary stress (S<sub>R</sub>): circumferential primary stresses are below the allowable stress (Sh) at the design pressure and temperature.
- 2. Longitudinal primary stresses (S<sub>L</sub>): the following loads are considered as producing longitudinal primary stresses: internal or external pressures; weight loads including valves, insulation, fluids, and equipment; hanger loads; static external loads and reactions; and the inertia load portion of seismic loads.

When the seismic load is due to the Design Earthquake (0.05g horizontal), the vectorial combination of

all longitudinal primary stresses  $(S_L)$  does not exceed 1.2 times the allowable stress  $(S_h)$ .

When the seismic load is due to the Maximum Credible Earthquake (0.12g horizontal), the vectorial combination of all longitudinal primary stresses does not exceed material yield stress at temperature unless higher allowable limits are calculated and substantiated by the methods outlined in Appendix C.

## b. Secondary Stresses (SE)

Secondary stresses are determined by use of the Maximum Shear Stress theory:

$$T_{\text{max}} = \frac{1}{2} \sqrt{s^2 + 4s_t^2} = \frac{1}{2} s_E$$

therefore,

$$S_E = \sqrt{s^2 + 4S_t^2}$$
 (see ANSI B31.1.0).

The following loads are considered in determining longitudinal secondary stresses:

- 1. Thermal expansion of piping
- 2. Movement of attachments due to thermal expansion
- Forces applied by other piping systems as a result of their expansion
- Any variations in pipe hanger loads resulting from expansion of the system, and
- 5. Anchor point movement portion of seismic loads.

The vectorial combination of longitudinal secondary stresses ( $S_E$ ) does not exceed the allowable stress range  $S_A$ , i.e.,  $S_E \leq S_A$ , where

$$S_A = f[1.25(S_c + S_h) - S_L]$$

(This is Equation 1 from paragraph 102.3.2 of ANSI B31.1.0 modified to include the additional stress allowance permitted when S<sub>I</sub> is less than S<sub>h</sub>.)

## A.3.2 Valve Design

Valves are designed and rated by the manufacturer to meet the design pressure and temperature. They are in compliance with ANSI B31.1.0, "Power Piping", ANSI B16.5, "Steel Pipe Flanges and Flanged Fittings", or Manufacturers Standarization Society, Standard Practice MSS SP-66, "Pressure-Temperature Ratings for Steel Butt-Welded End Valves."

## A.3.3 Pump Design

The pressure retaining parts of pumps are designed to meet the design pressure and temperature in the piping to which they are attached.

- a. For pumps used in piping systems classified as Group I, the requirements of Section III of the ASME Boiler and Pressure Vessel Code for Class C were used as a guide in calculating the thickness of pressure retaining parts and in sizing the cover bolting.
- b. For pumps used in piping systems classified as Group II, the requirements of Section VIII, Division I of the ASME Boiler and Pressure Vessel Code are used as a guide in calculating the thickness of pressure retaining parts and in sizing the cover bolting.
- c. When a pump is used in piping systems classified as Group III, the standard commercial design is accepted for the specific service.

## A. 4 MATERIALS

The material for piping and equipment pressure parts is in accordance with the applicable design code and the supplementary requirements of the project design specifications.

## A.4.1 Brittle Fracture Control for Ferritic Steels

The fracture or notch toughness properties and the operating temperature of ferritic materials in systems which form the reactor coolant boundary (Group I) are controlled to ensure adequate toughness when the system is pressurized to more than 20 percent of the design pressure. Such assurance is provided by maintaining the material service temperature at least 60 F above the nil ductility transition temperature (NDTT). Further requirements are:

- a. Ferritic steel piping that forms the reactor coolant boundary (Group I) is tested by the Charpy V-notch impact test (ASTM A-370) or drop weight test (ASTM E-208). Such tests are not required for: bolting, with a nominal size 1" and smaller, including nuts; materials whose section thickness is 1/2 inch and less; piping, valves, and fittings whose nominal inlet pipe size is only six inches in diameter and less, regardless of thickness; consumable insert material.
- b. Impact testing is not required on components or piping within the reactor coolant boundary having a minimum service temperature of 250 F or more when pressurized at more than 20 percent of design pressure. For example, the main steam line is excluded from the brittle fracture test requirement since the steam temperature will exceed 250 F when the steam line pressure is at 20 percent of the design pressure.
- c. Impact testing is used to determine that the material and weld metal will meet brittle fracture requirements at test temperature. The acceptance standards are in accordance with Table N-421 of the ASME Boiler and Pressure Vessel Code, Section III, for the minimum service temperature.

# A. 4.2 Furnace Sensitized Stainless Steel Materials

An effort has been made to minimize furnace sensitized austenitic stainless steel materials in the reactor pressure vessel, piping, and pressure retaining components in the critical systems. Austenitic stainless steel is

considered to be furnace sensitized if it has been heated by other than welding within the range of 800 to 1800 F, regardless of the subsequent cooling rate.

# A.5 WELDING PROCEDURES AND PROCESSES

#### A.5.1 General

All welding procedures, welders, and welding machine operators are qualified in accordance with the requirements of Section IX of the ASME Boiler and Pressure Vessel Code for the materials to be welded. Qualification records, including the results of procedure and performance qualification tests and identification symbols assigned to each welder, are maintained.

## A.5.2 Procedures and Processes

Welding procedures and processes are employed which produce welds of complete penetration, of complete fusion, and free of unacceptable defects. The finished surfaces of the weld (both root and crown) merge smoothly into the adjacent component surfaces. Weld layers are built up uniformly around the circumference and across the width of the joint. Weld starts and stops are staggered. Pressure countaining and attachment welds are made by any of the following processes within the limitations described in this appendix:

- a. Gas tungsten-arc welding with filler metal added
- Shielded metal arc welding with low hydrogen coated electrodes
- c. Submerged arc welding with multipass technique
- d. Gas metal arc welding within the limitations in the project specifications.
- e. Gas metal arc welding using shorting arc mode on carbon steel only.

# A.5.3 Dissimilar Metal Welds

Transition pieces are used wherever possible when carbon steel valves are welded to stainless steel piping. For piping systems with nominal wall thicknesses 3/4 inches and greater, the carbon steel transition piece mating to stainless steel is clad, a minimum of 3/16 inches after machining, with stainless steel weld metal (type 309) and stress relieved.

## A.6 FABRICATION AND ERECTION

#### A.6.1 Welded Construction

Piping and equipment pressure parts are assembled and erected by welding, except that flanged or screwed joints are used where necessary for maintenance.

Piping 2 1/2 inches and larger is V groove butt welded. Piping 2 inches and smaller is generally socket welded.

## A.6.2 Branch Connections

For critical piping, branch connections are made by using commercially available standard welding fittings. Integrally reinforced fittings are used for branch connections where standard fittings are not available; however, these fittings are not used for branch connections with nominal sizes larger than one half the nominal size in the main run. For piping where the branch is 2 inches or smaller, welded on forged fittings suitable for full penetration attachment welding are used. Branch connections are attached by full penetration welds.

For non-critical piping, standard fittings are used for the same size branches or one size reductions. Integrally reinforced fittings are used for two or more size reductions; however, stub-ins are permitted in certain special cases.

## A.6.3 Bending

A section of pipe may be bent by either cold or hot methods within the following limitations:

- a. Sections of pipe shall be selected so that thinning will not reduce the wall thickness below the minimum specified.
- b. Hot bending of austenitic stainless steel is not permitted unless followed by solution annealing heat treatment.
- c. The bend radius is limited to five times the nominal pipe diameter, unless otherwise specified.

## A.6.4 Heat Treatment

## A.6.4.1 Heat Treatment of Welds

Pre-heat and post-heat treatment of welds are in accordance with qualified welding procedures per the ASME Boiler and Pressure Vessel Code, Section IX.

## A.6.4.2 Carbon and Low Alloy Steel

The heat treatment of carbon steel and low alloy steel piping components and equipment pressure parts is in accordance with requirements of the ASTM material specifications.

## A.6.4.3 Austenitic Stainless Steel

Austenitic stainless steel piping components and equipment pressure parts are solution annealed at least once. Materials are annealed by heating to a temperature between 1900 and 2050 F and held at this temperature for one hour per inch of thickness, but not less than 1/2 hour, followed by rapid cooling to below 800 F.

## A.6.5 Defect Repair

## A.6.5.1 General

Repair of base metal or weld metal defects is in accordance with the following requirements:

- a. Surface defects such as laps, scabs, slivers, seams, or tears, which do not encroach on minimum wall thickness, are removed by machining or grinding and are blended into the adjacent metal surfaces.
- b. When defects or defect removal encroaches on minimum wall thickness, repairs are made by welding.

# A.6.5.2 Repair Welding

Repair welding is performed employing welding procedures and welders qualified in accordance with Section IX of the ASME Boiler and Pressure Vessel Code.

# A.6.5.3 Inspection of Repair Welds

Repair welds of a depth greater than 10 percent of the wall thickness must meet the inspection requirements for welds specified for the applicable classification of piping. Other inspection methods are not employed without approval.

## A.6.5.4 Heat Treatment After Repair by Welding

Base material repair welds are heat treated as required by the applicable materials specifications. Weld repairs are heat treated as required, in accordance with the project specifications.

## A.7 TESTING AND INSPECTION REQUIREMENTS

## A. 7.1 Radiography

#### A.7.1.1 Welds

Radiographic procedures and standards of acceptance for welds are in accordance with the ASME Boiler and Pressure Vessel Code Section VIII, Division I, Paragraph UW-51, Section III, Paragraph N-624, or Section I, Paragraph PW-51.

## A.7.1.2 Castings

Radiographic procedures for inspection of castings and casting repair welds are in accordance with ASTM E-94 and E-142, plus the following:

- a. Radiographic film shall be of the high contrast, high definition, fine grain type "Kodak AA", "Ansco Superay A", "Dupont 506", or approved equal.
- All radiography is done with lead screens.
- c. Film density in the area to be interpreted is within the range 1.7 to 3.5 as determined by either a film density strip or by a densitometer.
- d. Film location and identification markers are permanently marked on weldments and castings in accordance with the manufacturer's standard shop practice.

Acceptance standards for casting and casting repair welds less than 2 inches thick are in accordance with ASTM E71 as follows:

Category	Severity Level (acceptable)
A	A2
В	B2
c	C2
D	None acceptable
E	None acceptable
F	None acceptable
G	None acceptable

Acceptance standards for casting and casting repair welds 2 inches to less than 4-1/2 inches thick shall be in accordance with ASTM E186 as follows:

Category	Severity Level (acceptable)
A	A2
В	В2
С	Type 1 - CA2
	Type 2 - CB2
	Type 3 - CC2
D	None acceptable
E	None acceptable

Acceptable standards for casting and casting repair welds 4-1/2 inches to 12 inches thick shall be in accordance with ASTM E 280 as follows:

Category	Severity Level (acceptable)
A	A2
В	В2
С	Type 1 - CA2
	Type 2 - CB2
	Type 3 - CC2
D	None acceptable
E	None acceptable

## A.7.2 Ultrasonic Examination

## A.7.2.1 Forgings

Ultrasonic methods and acceptance standards for forgings are in accordance with ASTM A-388, "Ultrasonic Testing and Inspection of Heavy Steel Forgings", or the standard of acceptance is in accordance with Paragraph N-322.1 of the ASME Boiler and Pressure Vessel Code, Section III, as modified in the following paragraphs.

# A.7.2.1.1 Normal Beam Testing - Acceptance Standards

The materials are considered unacceptable, unless repaired, based on the following test indications:

- Indications of discontinuities in the material that produce a complete loss of back reflection not associated with the geometric configuration of the piece. (A complete loss of back reflection is assumed when the back reflection falls below 5 percent of full screen height.)
- 2. Traveling indications of discontinuities with 10 percent or more of the back reflection losts. (A traveling indication is defined as an indication which displays sweep movement of the oscilloscope pattern at a relatively constant amplitude as the search unit is moved along the part being examined.)

# A.7.2.1.2 Angle Beam Testing - Acceptance Standards

Materials are unacceptable where oscilloscope indications exceed those produced by the reference standard. The reference standard notch is the smaller of a depth equal to 5 percent of the material thickness of 3/8 inch.

## A.7.2.2 Piping and Fittings

Ultrasonic methods and acceptance standards for seamless pipe are in accordance with Paragraph N-324.3 of the ASME Boiler and Pressure Vessel Code, Section III. Plate for seam welded piping and fittings is examined prior to fabrication in accordance with Paragraph N-321.1 of the ASME Boiler and Pressure Vessel Code, Section III, or ASTM A-35 or E-273 or A-388.

Seamless fittings made from pipe are ultrasonically examined in accordance with Paragraph N-324.3 of the ASME code, Section III, or ASTM E-213 prior to forming of the firting. After final forming and any required heat treatment specified in the material specification, seamless fittings will be magnetic particle or liquid penetrant examined on all accessible surfaces.

# A.7.3 Liquid Penetrant Testing

Methods, techniques and acceptance standards for liquid penetrant testing are in accordance with Section VIII, Appendix VIII of the ASME code or Section III, Paragraph N-627.

## A.7.4 Magnetic Particle Testing

Methods, techniques and acceptance standards for magnetic particle testing are in accordance with Section VIII, Appendix VI of the ASME code or Section III, Paragraph N-626.

## A.7.5 Ferrite Testing

Austenitic stainless steel welds are subject to ferrite tests in order to determine the presence of a controlled amount of ferrite. The minimum amount of ferrite shall be 3-8 percent as determined by Schaeffler Diagram or by magnetic ferrite indicator.

## A.7.6 Hydrostatic Testing

Hydrostatic testing of pip and components is in accordance with ANSI B31.1.0 or the ASME code, as appropriate.

## A.8 CLEANING

To minimize the requirement for cleaning after erection and to prevent damage during shipment, storage or handling, piping and equipment pressure parts are cleaned and capped by the pipe fabricator prior to shipment.

## A.8.1 Stainless Steel Piping

Austenitic stainless steel interior surfaces are mechanically cleaned, blast cleaned, or in a pickled condition and are free of scale. Blast cleaned surfaces are free of residual quantities of the cleaning medium. The final cleaning operation consists of cleaning with process controlled water with chemical additive. Immediately after cleaning and inspection, all openings in the pipe assemblies are covered with suitable protective covers or caps.

# A.8.2 Carbon Steel and Low Alloy Piping

Carbon steel and low alloy piping steel surfaces are mechanically cleaned per PFI Standard ES-5, shot blast cleaned per Steel Structural Painting Council Standard SP-5, or pickled. After cleaning, piping assemblies are blown out with clean, oil free air. After cleaning and inspection, all openings of the pipe assemblies are covered with suitable protective covers or caps.

## A.9 PIPING DESIGN REQUIREMENTS

## A.9.1 General

Piping design requirements for the plant piping systems may be classified into the following schedules:

Schedule I summarizes the pipe material specifications and design requirements for piping systems in Group I and Group II. Note that Group I piping has additional design requirements above Group II.

Schedule II summarizes the pipe material specifications and design requirements for certain piping systems in Group III. These systems are:

Main steam lines downstream of outer isolation valves to the first remotely operated stop valves, excluding the turbine stop valves.

Feedwater lines upstream of outer isolation check valves to the first remotely operated stop valve in the feedwater pump discharge lines.

Schedule III summarizes the balance of plant piping.

The piping design requirements for the major components of the piping are described in general. No attempt has been made to completely describe each and every detailed component requirement in these piping systems. Various minor deviations from the basic design requirements, e.g., materials substitution, have been reviewed to ensure that such deviations meet the applicable codes and standards to assure the structural integrity of piping systems. However, no deviations are made for non-destructive testing required by codes (radiographic, magnetic particle and liquid penetrant examinations).

#### SCHEDULE I

#### PIPING DESIGN REQUIREMENTS FOR GROUPS I AND II

#### 1. MATERIAL SPECIFICATIONS

#### a. Carbon Steel Piping

Seam welded pipe, 26" and larger, is ASTM A-155-65 Gr. KC-70 (Firebox quality), Class I.

Seamless pipe, 24" and smaller, is ASTM A-106, Gr. B.

Seam welded fittings, 26" butt welding, are ASTM A-234, Gr. WPB-W or WPC-W and MSS SP-48.

Butt weld fittings, 24" through 2-1/2", are ASTM A-234, Gr. WPB, WPB-W or WPC-W. Welded seams are 100 percent radiographed after forming operation and either magnetic particle or liquid penetrant inspection is made on the final weld layer. Surfaces of fittings in the finished condition are examined by either magnetic particle or liquid penetrant method.

Seamless fittings, 2" and smaller, are forged carbon steel, ASTM A-105, Gr. II.

## b. Stainless Steel Piping

Seamwelded pipe, 12" and larger, is ASTM A-358, TP-304, Class I.

Seamless pipe, 12" through 2-1/2", is ASTM A-376 TP 304 or A-312 TP 304. Seamless pipe, 2" and smaller, is ASTM A-376 TP 304 or A-312 TP 304.

Butt weld fittings are ASTM A-403, Gr. WP304 or WP304-W. Welded seams are 100 percent radiographed after forming operations and liquid penetrant test is made on the final layer. Surfaces of fittings, 2-1/2" and larger, are examined by liquid penetrant method.

Seamless fittings, 2" and smaller, socket weld forged stainless steel, are ASTM A-182, Gr. F-304.

#### c. Flanges

Carbon steel flanges are ANSI Standard forged to ASTM A-105 Gr. II.

Stainless steel flanges are ANSI Standard, forged to ASTM A-182, Gr. F-304 or F-316. Surfaces of stainless steel flanges, 2-1/2" and larger, are examined by either magnetic particle or liquid penetrant method.

#### 2. INSPECTION

- a. Butt welds for 2 1/2" and larger pipe joints in the shop and field are 100 percent radiographed.
- b. The final layer of pressure welds in the shop and field are examined by either magnetic particle or liquid penetrant method. This requirement covers all pipe sizes for butt welds.
- c. Pressure retaining forgings over 4" in thickness are examined by ultrasonic method plus either liquid penetrant or magnetic particle methods.
- d. Pressure retaining parts of valves 2 1/2" and larger in nominal pipe sizes are radiographed.
- Valves are shop hydrostatic tested in accordance with the ANSI B 16.5 or MSS SP-66 requirements.

## 3. FABRICATION REQUIREMENTS

Fabrication requirements are in accordance with the project design requirements for critical systems.

## 4. SPECIAL REQUIREMENTS FOR GROUP I SYSTEMS

a. Brittle fracture control for ferritic steel is required for the following portions of Group I systems:

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Feedwater System - from RPV to the outer isolation check valve (valve 6-96) and startup recirculation line isolation valves 38 A and 38 B.

High Pressure Coolant Injection Line - from feedwater line to testable check valve (valve 23-18).

Core Spray - isolation valves 14-14A and 14-14B.

Reactor Core Isolation Cooling System - from feedwater line to testable check valve (valve 13-22).

RHR System shutdown cooling isolation valves (10-17, 10-18 and 10-88), LPCI valves (10-81A and 10-81B)

Cleanup System Return - from feedwater line to check valve (valve 12-62).

Control Rod Hydraulic System Return Line - from valve 3-110 to valve 3-114.

- b. Pressure retaining bolting greater than 1" is examined by either magnetic particle or liquid penetrant method.
- c. Pipe and fittings, 2-1/2" and larger pipe sizes, in Group I systems are 100 percent volumetrically examined per Section III of the ASME code. This requirement applies to Unit 3 only.

#### SCHEDULE II

#### PIPING DESIGN REQUIREMENTS

#### 1. MATERIAL SPECIFICATIONS

## a. Carbon Steel Piping

Seamwelded pipe, 26", is ASTM A-155-65, Gr. KC-70 (Firebox quality), Class I.

Seamless pipe, 24" and smaller, is ASTM A-106, Gr. B.

Seamwelded butt weld fittings, 26", are ASTM A-234, Gr. WPC-W and MSS-SP-48. Welded seams are 100 percent radiographed after forming operations and magnetic particle inspection is made on the final weld layer.

Seamless butt weld fittings, 24" through 2-1/2", are ASTM A-234, Gr. WPB.

Seamless socket weld fittings, 2" and smaller, are forged carbon steel to A-105, Gr. II.

## b. Stainless Steel Piping

Not applicable.

## c. Flanges

Flanges are ANSI Standard, forged carbon steel to ASTM A-105, Gr. II.

### 2. INSPECTION

- a. Butt welds for 2-1/2" and larger pipe joints in the shop and field are 100 percent radiographed.
- b. The final layer of pressure welds are examined by either magnetic particle or liquid penetrant method.
- c. Pressure retaining parts of valves, 2-1/2" and larger, are radiographed.

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- d. Valve butt weld end preparations for field welding are examined by either magnetic particle or liquid penetrant method.
- Valves are shop hydrostatic tested in accordance with ANSI B16.5 or MSS SP-66 requirements.

## 3. FABRICATION REQUIREMENTS

Fabrication requirements are in accordance with the project design specifications for critical systems.

#### **PBAPS**

#### SCHEDULE III

## 1. MATERIAL SPECIFICATIONS (Partial List)

#### a. Carbon Steel Piping

Seamwelded pipe is ASTM A-155-65, Gr. KC-70 Cl.2 or ASTM A-155, Gr. C-55 Cl.2.

Seamless pipe is ASTM A-106, Gr. B or A-53, Gr. A or B.

Fittings are ASTM A-234 WPB, WPB-W or WPC-W, or ASTM A-105, Gr. II.

## b. Stainless Steel Piping

Seamwelded pipe is ASTM A-312 TP-304, 304L plus eddy current test, or ASTM A-358, TP-304 or 304L, Class I.

Seamless pipe is ASTM A-376 TP 304 or ASTM A-312 TP 304 or 304L.

Fittings are ASTM A-403, WP 304WL or ASTM A-182, Gr. F-304.

## c. Low Alloy Piping

Seamless pipe is ASTM A-335, Gr. P-11 or P-5.

Seamwelded pipe is ASTM A-155, Class II, Gr. 1-1/4 CR.

Fittings are ASTM A-234 WP-11, WP-11W, WP-5, or WP-5W, or ASTM A-182, F11 on F5.

## 2. INSPECTION REQUIREMENTS

Inspections are in accordance with material specifications or the requirements of ANSI B31.1.0.

Inspection of valves conforms to ANSI B31.1.0 requirements.

# 3. FABRICATION REQUIREMENTS

Fabrication requirements shall conform to the project design specifications. Those systems requiring thermal stress analysis and special fabrication techniques are identified as Schedule IIIc, the "c" denoting a critical system.

PBAPS

# TABLE A.9.1

# SUMMARY CLASSIFICATION OF PIPING SYSTEMS

Group I (Primary Pressure Boundary)	Design Schedule	Seismic Class
Recirculation System	I	I
Systems from RPV to Outer Iso. Valve:		
Feedwater Lines	I	I
Main Steam Lines	I	I
Main Steam Drain Lines	I	I
Steam to HPCI	I	I
Steam to RCIC	I	I
Core Spray	I	I
Residual Heat Removal:		
Shutdown Supply	I	I
Head Spray	I	I
LPCI	I	I
Reactor Water Cleanup Supply & Return	I	I
CRD Return	I	I
Standby Liquid Control	I	I
Reactor Vessel Instrumentation	I	ı
Sample Lines	·I	I
Small Lines, 2" and under		
To and including first shutoff valve	e I	I
Beyond shutoff valve	III	
CRD System		
Insert and Withdraw Lines	I	I
Scram Discharge Volume	I	I

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PBAPS

# TABLE A.9.1 (Continued)

Group II (Core Cooling and Containment Extension)	Design Schedule	Seismic Class
Residual Heat Removal:		
LPCI	I	1
Containment Cooling and Spray (excluding		
spargers)	I	I
Shutdown Cooling	I	r
Reactor Head Spray	I	ı
Core Spray	I	ı
HPCI:		
Steam Supply and Exhaust	I	I
Suction	I	I
Discharge	I	I
RCIC:		
Steam Supply and Exhaust	I	I
Suction	I	I
Discharge	I	I
Reactor Water Cleanup System		
High Pressure System Only	I	
Standby Liquid Control System:		
Excluding system test components	I	1
Essential instrument lines for Standby		
Core Cooling Systems	I	· I
Inerting System:		
From Containment to the Second		
Isolation Valve	I	ı

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# TABLE A.9.1 (Continued)

Group II (Continued)	Design Schedule	Seismic Class
Containment Ventilation System:		
From Containment to the Second		
Isolation Valve	ı	I
Special Auxiliary Systems:		
High Pressure Service Water	I	I
Emergency Service Water	ı	I
Emergency Cooling Water	I	1
Post - LOCA Containment		
Atmosphere Dilution System	I	I

#### PBAPS

# TABLE A.9.1 (Continued)

Group III (Balance of Plant Systems)	Design Schedule	Seismic Class
Main Steam:		
Downstream of Outer Isolation Valves		
to Main Stop Valve or First Remotel	У	
Operated Valve	II	
Turbine Steam Bypass	II	
Feedwater:		
Upstream of Outer Isolation Check Valv	es	
to First Remotely Operated Valves	II	
Feed Pump Recirc.	IIIc*	
Control Rod Hydraulic System:		
Suction line to Pump	III	
Condensate Supply to CSCS Pumps	III	I
Offgas System:		
Air Ejector to Holdup Pipe	IIIc*	
Holdup Pipe	IIIc*	
Holdup Pipe to Offgas Filters	IIIc*	-
Downstream of Offgas Filter to Stack	III	
Inerting System:		
From the Second Isolation Valves to		
Storage Tank	III	
Standby Liquid Control System:		
System Test Components	IIIc	

\*All welds 100% radiographed

## PBAPS

# TABLE A.9.1 (Continued)

Group III (Continued)	Design Schedule	Seismic Class
Reactor Water Cleanup System:		
Blowdown to Condenser and Radwaste	IIIc	
Low Pressure System	IIIc	
RCIC:		
Suction from Cond. Storage Tank	IIIc	I
Radwaste:		
Liquid Process	III	
Fuel Pool Cooling and Cleanup	III	
Extraction Steam	IIIc	-
Condensate:		
Pump Suction	IIIc	
Pump Discharge	IIIc	
Condensate Service	III	
Auxiliary Steam	IIIc	
Plant Heating	III	
Service Water	III	
Reactor Building Cooling Water	III	
Turbine Building Cooling Water	III	
Instrument Air	III	
Service Air	III	
Fire Protection System	III	
Domestic Water	III	-

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PBAPS

# TABLE A.9.1 (Continued)

Group III (Continued)	<u>Design</u> Schedule	Seismic Class
Lube Oil	III	
Fuel Oil	III	
Chemicals	III	
Chilled Water System	III	
Makeup Water System	III	

#### FLAPS

## TABLE A.9.2

#### SUMMARY OF EQUIPMENT

#### DESIGN GUIDES

## Group I

Reactor Pressure Vessel ASME III, Cl. A Recirc. Pumps See Par. A.3.3 Recirculation Valves MSS-SP-66 Safety Valves, RV ASME III Relief Valves, RV ASME III Main Steam Valves B16.5 Recirc. Flow Nozzle B31.1.0 Steam Flow Nozzle B31.1.0 Feedwater Isolation Check Valves MSS-SP-66 Isolation Valves: Except Listed Below B16.5 MO-10-25, AO-46 MSS-SP-66 AO-13-22, AO-23-18 MSS-SP-66 MO-14-12, AO-14-13 MSS-SP-66

#### PBALS

## TABLE A.9.2 (Continued)

Group II

Containment Vessel

ASME III, Cl. B

Cleanup System

Non-Regenerative Heat Exchanger

Shell: ASME VIII Tube: ASME III, Cl. C

Regenerative Heat Exchanger

ASME III, Cl. C

Filter Demineralizer

ASME III, C1. C

HPCI

Turbine

Per design specification

Pump

See Par. A.3.3

RCIC

Turbine

Per design specification

Pump

See Par. A.3.3

Core Spray

Pumps

See Par. A.3.3

Residual Heat Removal

Pump

Heat Exchanger

See Par. A.3.3

Shell: ASME III, Cl. C

Tube: ASME VIII

Standby Liquid Control

Pump

See Par. A.3.3

Containment Vacuum Relief Valves and

Drywell Vacuum Breakers

B31.1.0 & ASME Sec. III, Cl. B

Post - LOCA Containment

Asme Section III (1971)

Atmosphere Dilution System

Liquid No Tank

Class 2

# TABLE A.9.2 (Continued)

# Group III (Partial List)

## Radwaste:

Waste Filter	ASME	III,	c1. c	
Floor Drain Filter	ASME	III,	c1. c	
Waste Demineralizer	ASME	III,	c1. c	
Fuel Pool Heat Exchangers	ASME	VIII,	Div.	I
Reactor Building Cooling Water Heat				
Exchangers	ASME	VIII,	Div.	I
Turbine Building Cooling Water Heat				
Exchangers	ASME	VIII,	Div.	J
Offgas Filter Vessels	ASME	VIII,	Div.	I
Air Compressor After Coolers	ASME	VIII,	Div.	Ľ
Condensate Demineralizer Vessels	AS ME	VIII,	Div.	I
Make-up Demineralizer Vessels	ASME	VIII,	Div.	I
Auxiliary Boilers	ASME	I		
Auxiliary Boiler Blowoff Tank	ASME	VIII,	Div.	I
Auxiliary Boiler Deaerator	ASME	VIII,	Div.	•
Compressed Air Receivers	ASME	VIII,	Div.	I
Moisture Separator Tanks	ASME	VIII,	Div.	I
Moisture Separator Drain Tanks	ASME	VIII,	Div.	I

#### SYSTEM LEGENDS

- 1. REACTOR RECIRCULATION
- 2. MAIN STEAM
- 3. FEEDWATER
- 4. REACTOR WATER CLEAN-UP
- 5. REACTOR CORE ISOLATION COOLING (RCIC)
- 6. CORE SPRAY
- 7. RESIDUAL HEAT REMOVAL
- 8. CONTAINMENT SPRAY
- 9. REACTOR HEAD SPRAY
- 10. STANDBY LIQUID CONTROL
- 11. HIGH PRESSURE COOLANT INJECTION (HPCI)
- 12. LOW PRESSURE COOLANT INJECTION (LPCI)

#### PIPING CODE

ANSI B31.1.0 - PIPING

GROUP I

GROUP II

GROUP III

#### EQUIPMENT CODE

ASME SECTION III A

ASME SECTION III C

ASME SECTION VIII, API

#### GROUP I:

PIPING AND EQUIPMENT PRESSURE PARTS
WITHIN THE REACTOR PRIMARY PRESSURE
BOUNDARY THROUGH THE OUTER ISOLATION
VALVE, INCLUSIVE.

#### GROUP II:

PIPING AND EQUIPMENT PRESSURE PARTS

DOWNSTREAM OF THE OUTER ISOLATION

VALVE AND EXTENSIONS OF CONTAINMENT

AND THE CORE STANDBY COOLING SYSTEMS.

#### GROUP III:

BALANCE OF PLANT PIPING AND EQUIP-MENT PRESSURE PARTS INCLUDING POWER GENERATION SYSTEMS.

#### -- CONTAINMENT BOUNDARY

PHILADELPHIA ELECTRIC COMPANY
PEACH BOTTOM ATOMIC POWER STATION
UNITS 2 AND 3
FINAL SAFETY ANALYSIS REPORT

PIPING CODE CLASSIFICATION
(NSSS)

FIGURE

A.2.1

----0 CONTAINMENT PRIMARY CONTAINMENT ..... MEACTOR DRYWELL & RECIRC PUMP COOLERS CONDENSER MAIN STEAM CONTAINMENT COOLING SYSTEM REACTOR BLDG COOLING WATER NON REGEN, EXC CONDENSATE STORAGE PILTER SERVICE