### WRAP-PWR-EM SYSTEM DEVELOPMENT AND APPLICATIONS

by

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#### SUMMARY

The WRAP-EM system is a complete computational system for analysis of loss-of-coolant accidents (LOCAs) in light-water power reactors. The system has been developed for use by the Nuclear Regulatory Commission in evaluating and interpreting reactor vendor model methods and results.

WRAP-EM has the capability of predicting fuel parameters during the normal operation of a reactor, performing thermalhydraulic initialization of the reactor system, analysing the behavior of the reactor core during an accident (encompassing the blowdown, refill, and reflood stages), and executing a detailed transient thermal analysis of the hottest pin in the core during the accident. A minimum amount of user intervention is required throughout the analysis.

WRAP-PWR-EM is the integrated system of codes used for the analysis of pressurized water reactors (PWRs). GAPCON-THERMAL-2 is used to initialize fuel parameters as a function of reactor operating time. Both the blowdown and reflood phases of an accident are analyzed by RELAP4/MOD5. The refill calculation is based on a simple accumulator flow model (FLOW4) developed at NRC, and the hot-pin analysis is performed by FRAP-T4-LACE. The auto ated transfer of relevant data from one code to another is accomplished through interface routines developed at SRL (except RELAP4/MOD5-FLOOD to FRAP).

<sup>\*</sup> The information contained in this article was developed during the course of work under Contract No. AT(07-2)-1 with the U. S. Department of Energy.

Because different fuel models are used in the various codes, it is important to ascertain that the conditions predicted at a given time by two different codes are similar. In particular, at the time of accident initiation, the fuel parameters determined by RELAP and FRAP must be similar to, and more conservative than, the parameters predicted by GAPCON. The conservatism requirement is set for licensing concerns. Results achieved using Zion fuel indicate that fuel temperatures predicted by RELAP and FRAP are more conservative than the GAPCON predictions.

The refill portion of the transient is that time during which the lower plenum is being filled with water until the liquid level reaches the bottom of the core. Analysis of this period by RELAP requires very small calculational time-steps. An alternative technique has been developed based on a simple accumulator flow model. Within the refill period, the core is assumed to heat up adiabatically. The core thermal response is calculated by continuing the RELAP4 calculation with the hydraulics calculation bypassed. The lower plenum subcooling, which is required as input to the flood calculations, is calculated by a mixed-average, bulkfluid, temperature calculation. Several assumptions relating to heat transfer during this period have been made to decrease the computational time. Results of sensitivity studies to determine conservative estimates of these parameters will be presented.

The system is presently being evaluated by analyzing various LOFT experiments and the Zion reactor. Results of these analyses will be discussed. Future plans include performing pre-test analyses on the LOFT L2 series experiments as well as reference and sensitivity studies regarding the Zion facility.

#### REFERENCES

- M. M. Anderson. WRAP A Water Reactor Analysis Package. Report DPST-NUREG-77-2, Savannah River Laboratory, E. I. du Pont de Nemours and Company, Aiken, SC (1977).
- M. V. Gregory. User's Guide to Input for WRAP A Water Reactor Analysis Package. Report DPST-NUREG-77-2, Savannah River Laboratory, E. I. du Pont de Nemours and Company, Aiken, SC (1977).
- 3. D. A. Sharp. The BWR Steady-State Capability of the WRAP-EM System. Report DPST-NUREG-78-1, Savannah River Laboratory, E. I. du Pont de Nemours and Company, Aiken, SC (1979).
- M. R. Buckner, et al. The BWR Loss-of-Coolant-Accident Analysis Capability of the WRAP-EM System. Report DPST-NUREG-78-2, Savannah River Laboratory, E. I. du Pont de Nemours and Company, Aiken, SC (1979).
- R. R. Beckmeyer, et al. User's Guide for the BWR LOCA Analysis Capability of the WRAP-EM System. Report DPST-NUREG-78-3, Savannah River Laboratory, E. I. du Pont de Nemours and Company, Aiken, SC (1979).
- D. A. Sharp. The PWR Steady-State Capability of WRAP A Water Reactor Analysis Package. Report DPST-NUREG-77-3, Savannah River Laboratory, E. I. du Pont de Nemours and Company, Aiken, SC (1977).
- H. C. Honeck. The JOSHUA System. ERDA Report DP-1380, Savannah River Laboratory, E. I. du Pont de Nemours and Company, Aiken, SC (1975).

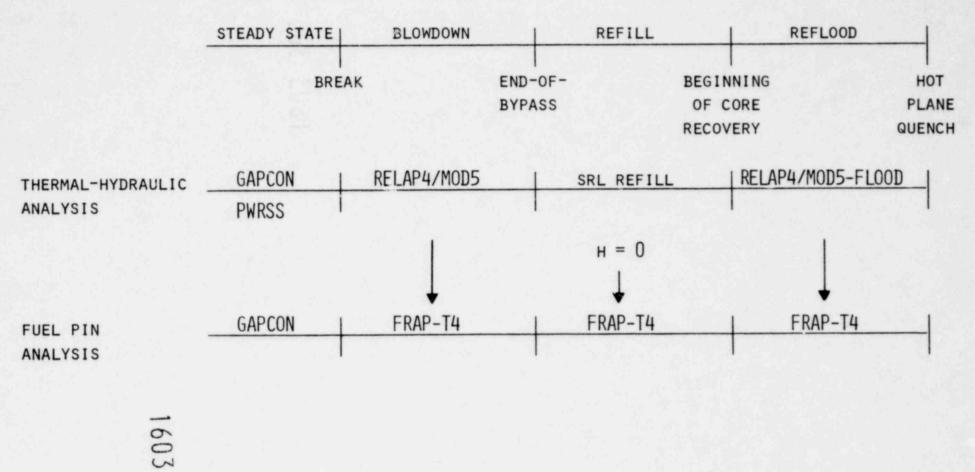
# WRAP-PWR-EM DEVELOPMENT AND APPLICATIONS

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## OUTLINE

- I. System Description
- II. Fuel Model Consistency
- III. Refill
  - IV. Analyses
    - LOFT
    - . ZION
    - FLOOD Sensitivity
  - V. Program

# PWR ANALYSIS SCHEME



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## GAPCON-FRAP CONSISTENCY AT HOTTEST AXIAL NODE

Burnup = 13000 MWD/MT

	GT21	F4L <sup>2</sup>
Centerline Temperature (°F)	3159	3285
Fuel Surface Temperature (°F)	1540	1588
Gap Conductance (BTU/hr-ft <sup>2</sup> -°F)	374	356
Gap Pressure (psi)	1204	1238
Stored Energy (BTU/1b)	163	170

<sup>1</sup> GT2  $\equiv$  GAPCON-THERMAL-2

<sup>2</sup> F4L  $\equiv$  FRAP-T4-LACE

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### GAP CONDUCTANCE

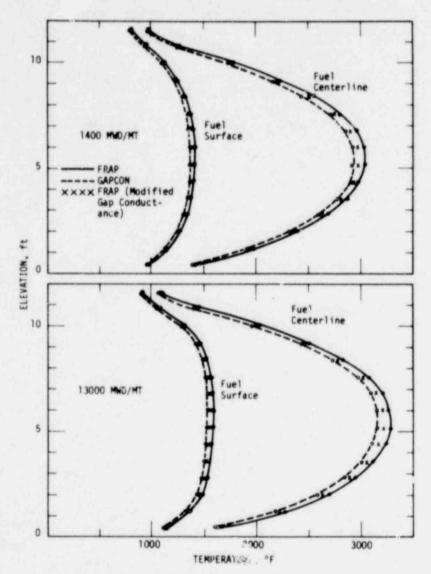
FRAP (Open gap)

$$h = \frac{k}{\Delta X + g + 1.98R} + h_r$$

GAPCON (Open gap)

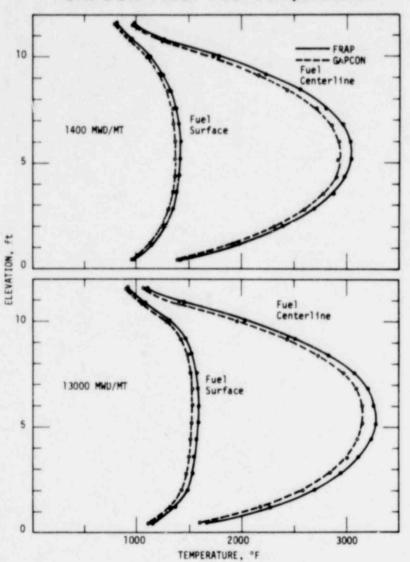
 $h = \frac{k}{\Delta X + g} + h_r$ 

k	H	thermal conductivity of gas	
g and g'	Ξ	temperature jump distances	
$\Delta \mathbf{X}$	111	gap width	
R	Ξ	average roughness	
hr	Ш	radiation term	
h	Ξ	gap conductance	



GAPCON-FRAP Fuel Temperatures

1603 309



GAPCON-FRAP Fuel Temperatures

1603 310

### REFILL

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- RELAP calculation prohibitive
- FLOW4 Simple accumulator flow model
- Core thermal model Adiabatic heatup
- Mixed average bulk fluid model

### GAPCON-FRAP CONSISTENCY AT HOTTEST AXIAL NODE WITH MODIFIED GAP CONDUCTANCE CORRELATION

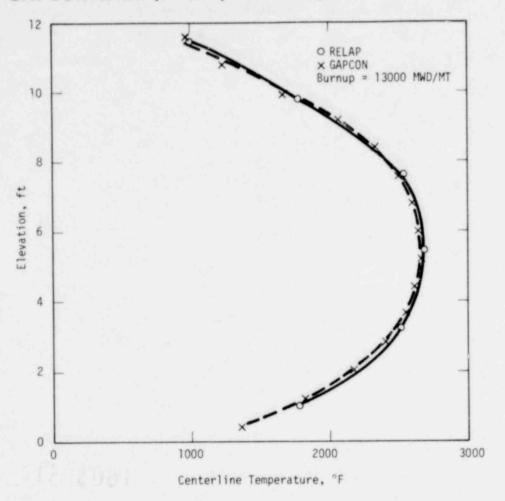
Burnup = 13000 MWD/MT

	GT2 <sup>1</sup>	F4L <sup>2</sup>	F4LM <sup>3</sup>
Centerline Temperature (°F)	3159	3285	3234
Fuel Surface Temperature (°F)	1540	1588	1550
Gap Conductance (BTU/hr-ft <sup>2</sup> -°F)	374	355	372
Gap Pressure (psi)	1204	1238	1222
Stored Energy (BTU/1b)	163	170	166

<sup>1</sup> GT2 = GAPCON-THERMAL-2

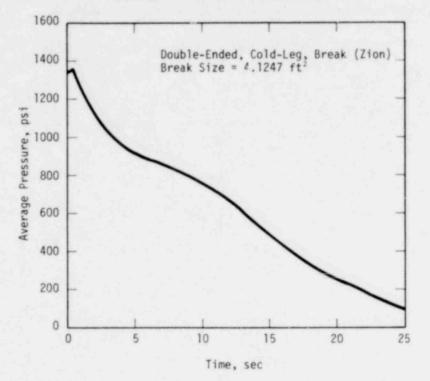
<sup>2</sup> F4L  $\equiv$  FRAP-T4-LACE

<sup>3</sup> F4LM ≡ FRAP-T4-LACE MODIFIED



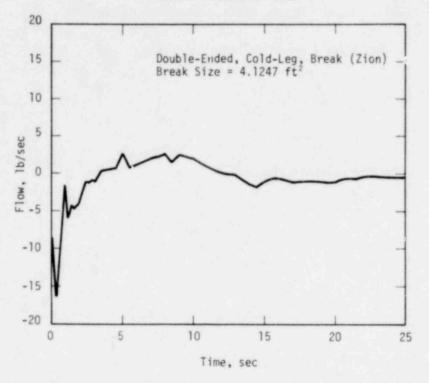
GAPCON-WRAP(RELAP) Fuel Temperature Comparison

1603 313



# Lower Plenum Pressure

1603 314

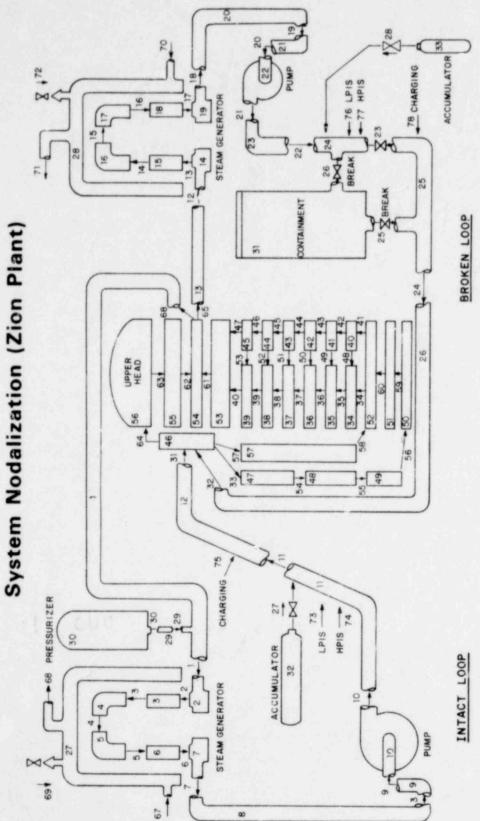


Zion Core Flow

1603 315

1603-3162

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### PROGRAM

- PWR System Checkout and Evaluation
- Verification Studies
  - 1. LOFT (L1-5 and L2-3)
  - 2. Semi-scale (S-06-03 and MOD3)
  - 3. Zion
- WRAP Analysis for NRC
  - 1. LOFT Pre-test Calculations
  - 2. Reference and Sensitivity Studies
  - 3. NRC Licensing Concerns