



October 19, 2018  
L-2018-195  
10 CFR 50.36

U.S. Nuclear Regulatory Commission  
Attn: Document Control Desk  
Washington, D. C. 20555-0001

Re: Turkey Point Unit 3  
Docket No. 50-250  
Core Operating Limits Report

In accordance with Technical Specification 6.9.1.7, the attached Core Operating Limits Report (COLR) is provided for Turkey Point Unit 3. The COLR is applicable for Unit 3 Cycle 30.

Should there be any questions, please contact Mr. Robert Hess, Licensing Manager, at 305-246-4112.

Sincerely,

A handwritten signature in black ink, appearing to read 'Robert Hess', is written over a horizontal line.

Robert Hess  
Licensing Manager  
Turkey Point Nuclear Plant

Attachments

cc: Regional Administrator, Region II, USNRC  
Senior Resident Inspector, USNRC, Turkey Point Plant

## **Turkey Point Unit 3 Cycle 30 Core Operating Limits Report (COLR)**

## 1.0 INTRODUCTION

This Core Operating Limits Report for Turkey Point Unit 3 Cycle 30 has been prepared in accordance with the requirements of Technical Specification 6.9.1.7.

The Technical Specifications (TS) affected by this report are listed below with the section and page for each one of the TS addressed in this COLR document.

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## 2.0 OPERATING LIMITS

The cycle-specific parameter limits for the specifications listed in the Introduction are presented below and listed sequentially by Technical Specification (TS). These limits have been developed using the NRC-approved methodologies specified in TS 6.9.1.7.

### 2.1 Reactor Core Safety Limits – Three Loops in Operation (TS 2.1.1)

- Figure A1 (page 14A-A7) In Modes 1 and 2, the combination of Thermal Power, reactor coolant system highest loop average temperature and pressurizer pressure shall not exceed the limits in Figure A1.

### 2.2 Reactor Trip System Instrumentation Setpoints (TS 2.2.1)

#### NOTE 1 on TS Table 2.2-1 Overtemperature $\Delta T$

- $\tau_1 = 0s, \tau_2 = 0s$  Lead/Lag compensator on measured  $\Delta T$
- $\tau_3 = 2s$  Lag compensator on measured  $\Delta T$
- $K_1 = 1.31$
- $K_2 = 0.023/^\circ F$
- $\tau_4 = 25s, \tau_5 = 3s$  Time constants utilized in the lead-lag compensator for  $T_{avg}$
- $\tau_6 = 2s$  Lag compensator on measured  $T_{avg}$
- $T' \leq 583.0^\circ F$  Indicated Loop  $T_{avg}$  at RATED THERMAL POWER
- $K_3 = 0.00116/psi$
- $P' \geq 2235 \text{ psig}$  Nominal RCS operating pressure
- $f_1(\Delta I) = 0$  for  $q_t - q_b$  between  $-18\%$  and  $+7\%$

For each percent that the magnitude of  $q_t - q_b$  exceeds  $-18\%$ , the  $\Delta T$  Trip Setpoint shall be automatically reduced by  $3.51\%$  of its value at RATED THERMAL POWER; and

For each percent that the magnitude of  $q_t - q_b$  exceeds  $+7\%$ , the  $\Delta T$  Trip Setpoint shall be automatically reduced by  $2.37\%$  of its value at RATED THERMAL POWER.

Where  $q_t$  and  $q_b$  are percent RATED THERMAL POWER in the top and bottom halves of the core respectively, and  $q_t + q_b$  is total THERMAL POWER in percent of RATED THERMAL POWER.

NOTE 2 on TS Table 2.2-1 Overtemperature  $\Delta T$  (Not affected by COLR, included for completeness)

The Overtemperature  $\Delta T$  function Allowable Value shall not exceed the nominal trip setpoint by more than 0.5%  $\Delta T$  span for the  $\Delta T$  channel, 0.2%  $\Delta T$  span for the Pressurizer Pressure channel, and 0.4%  $\Delta T$  span for the  $f(\Delta I)$  channel. No separate Allowable Value is provided for  $T_{avg}$  because this function is part of the  $\Delta T$  value.

NOTE 3 on TS Table 2.2-1 Overpower  $\Delta T$

- $K_4 = 1.10$
- $K_5 \geq 0.0/^\circ\text{F}$  For increasing average temperature
- $K_5 = 0.0$  For decreasing average temperature
- $\tau_7 \geq 0 \text{ s}$  Time constants utilized in the lead-lag compensator for  $T_{avg}$
- $K_6 = 0.0016/^\circ\text{F}$  For  $T > T''$
- $K_6 = 0.0$  For  $T \leq T''$
- $T'' \leq 583.0 \text{ }^\circ\text{F}$  Indicated Loop  $T_{avg}$  at RATED THERMAL POWER
- $f_2(\Delta I) = 0$  For all  $\Delta I$

NOTE 4 on TS Table 2.2-1 Overpower  $\Delta T$  (Not affected by COLR, included for completeness)

The Overpower  $\Delta T$  function Allowable Value shall not exceed the nominal trip setpoint by more than 0.5%  $\Delta T$  span for the  $\Delta T$  channel. No separate Allowable Value is provided for  $T_{avg}$  because this function is part of the  $\Delta T$  value.

**2.3 Shutdown Margin Limit for MODES 1, 2, 3 and 4 (TS 3.1.1.1)**

- Figure A2 (page 14A-A8)

**2.4 Shutdown Margin Limit for MODE 5 (TS 3.1.1.2)**

- $\geq 1.77\% \Delta k/k$

## 2.5 Moderator Temperature Coefficient (MTC) (TS 3.1.1.3)

- $\leq + 5.0 \times 10^{-5} \Delta k/k/^{\circ}F$  BOL, HZP, ARO, and from HZP to 70% Rated Thermal Power (RTP)
- From 70% RTP to 100% RTP the MTC decreasing linearly from  $\leq + 5.0 \times 10^{-5} \Delta k/k/^{\circ}F$  to  $\leq 0.0 \times 10^{-5} \Delta k/k/^{\circ}F$
- Less negative than  $- 41.0 \times 10^{-5} \Delta k/k/^{\circ}F$  EOL, RTP, ARO

## 2.6 MTC Surveillance at 300 ppm (TS 4.1.1.3)

- Less negative than  $- 35.0 \times 10^{-5} \Delta k/k/^{\circ}F$  (-35 pcm/ $^{\circ}F$ ) Within 7 EFPD of reaching equilibrium boron concentration of 300 ppm.
- The Revised Predicted near – EOL 300 ppm MTC shall be calculated using the algorithm contained in WCAP-13749-P-A:

$$\text{Revised Predicted MTC} = \text{Predicted MTC} + \text{AFD Correction} - 3 \text{ pcm}/^{\circ}F$$

If the Revised Predicted MTC is less negative than the SR 4.1.1.3.b 300 ppm surveillance limit and all the benchmark criteria contained in the surveillance procedure are met, then an MTC measurement in accordance with SR 4.1.1.3.b is not required to be performed.

The neutronics methods used with WCAP-13749-P-A are those described in WCAP-11596-P-A, "Qualification of the Phoenix-P/ANC Nuclear Design System for Pressurized Water Reactor Cores," June 1988.

## 2.7 Analog Rod Position Indication System (TS 3.1.3.2)

- Figure A3 (page 14A-A9) The All Rods Out (ARO) position for all shutdown Banks and Control Banks is defined to be 228 steps withdrawn.

## 2.8 Control Rod Insertion Limits (TS 3.1.3.6)

- Figure A3 (page 14A-A9) The control rod banks shall be limited in physical insertion as specified in Figure A3 for ARO = 228 steps withdrawn.

## 2.9 Axial Flux Difference (TS 3.2.1)

- Figure A4 (page 14A-A10)

**2.10 Heat Flux Hot Channel Factor  $F_Q(Z)$  (TS 3.2.2)**

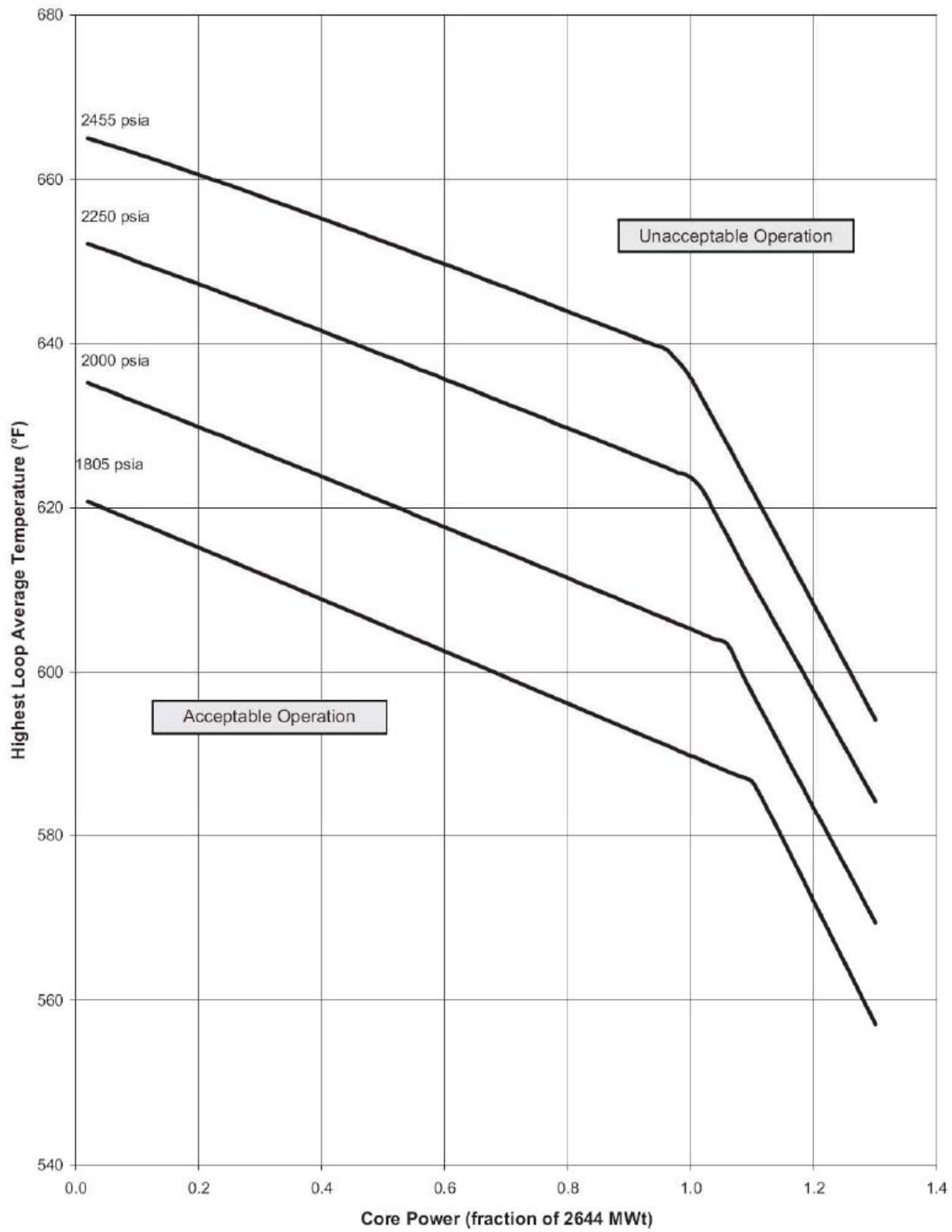
- $[F_Q]^L = 2.30$
- $K(z) = 1.0$  For  $0' \leq z \leq 12'$  where  $z$  is core height in ft

**2.11 Nuclear Enthalpy Rise Hot Channel Factor (TS 3.2.3)**

- $F_{\Delta H}^{RTP} = 1.600$   $PF_{\Delta H} = 0.3$

**2.12 DNB Parameters (TS 3.2.5)**

- $RCS T_{avg} \leq 585.0^\circ F$
- Pressurizer Pressure  $\geq 2204$  psig

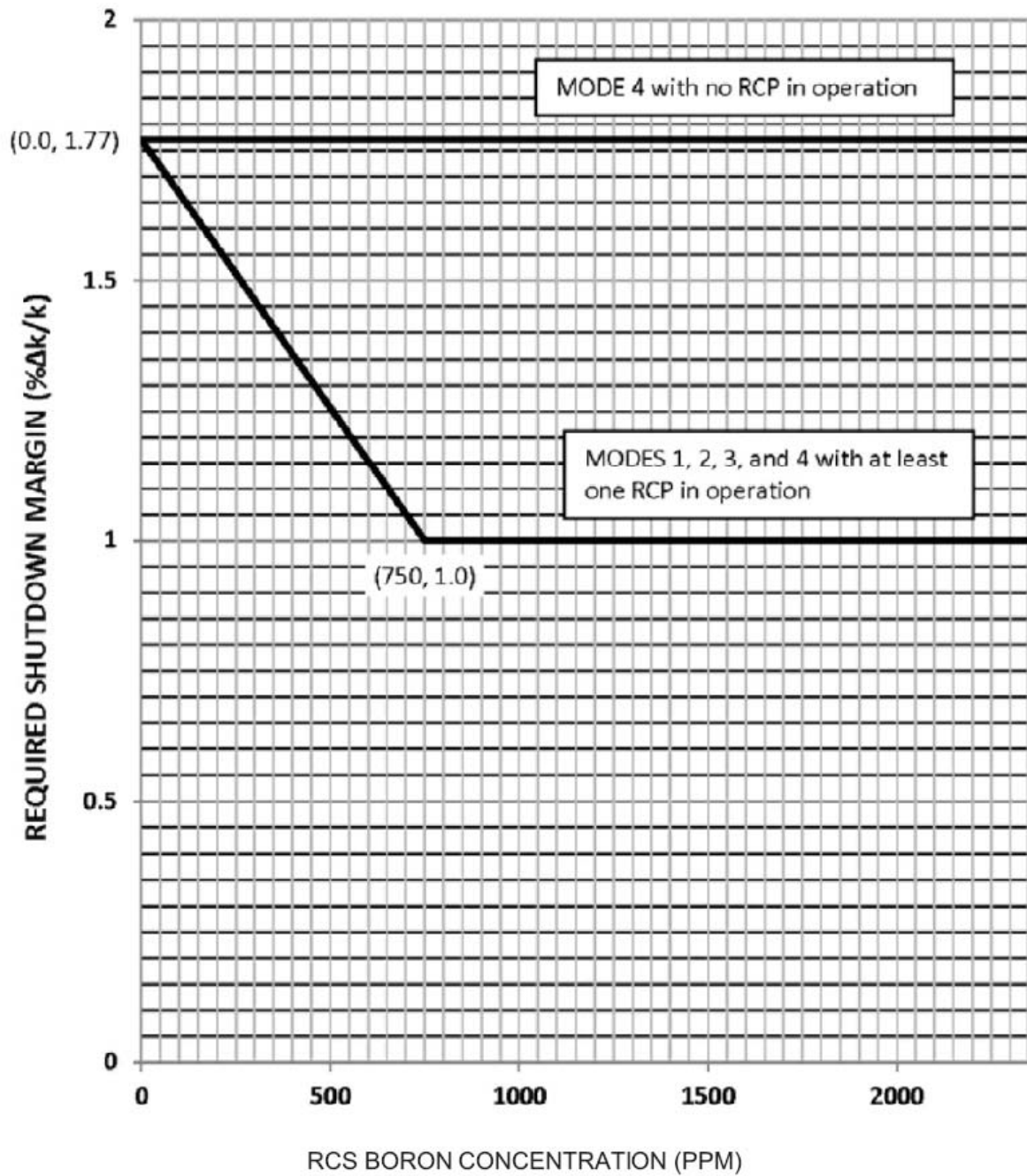


**FIGURE A1 Reactor Core Safety Limit – Three Loops in Operation**



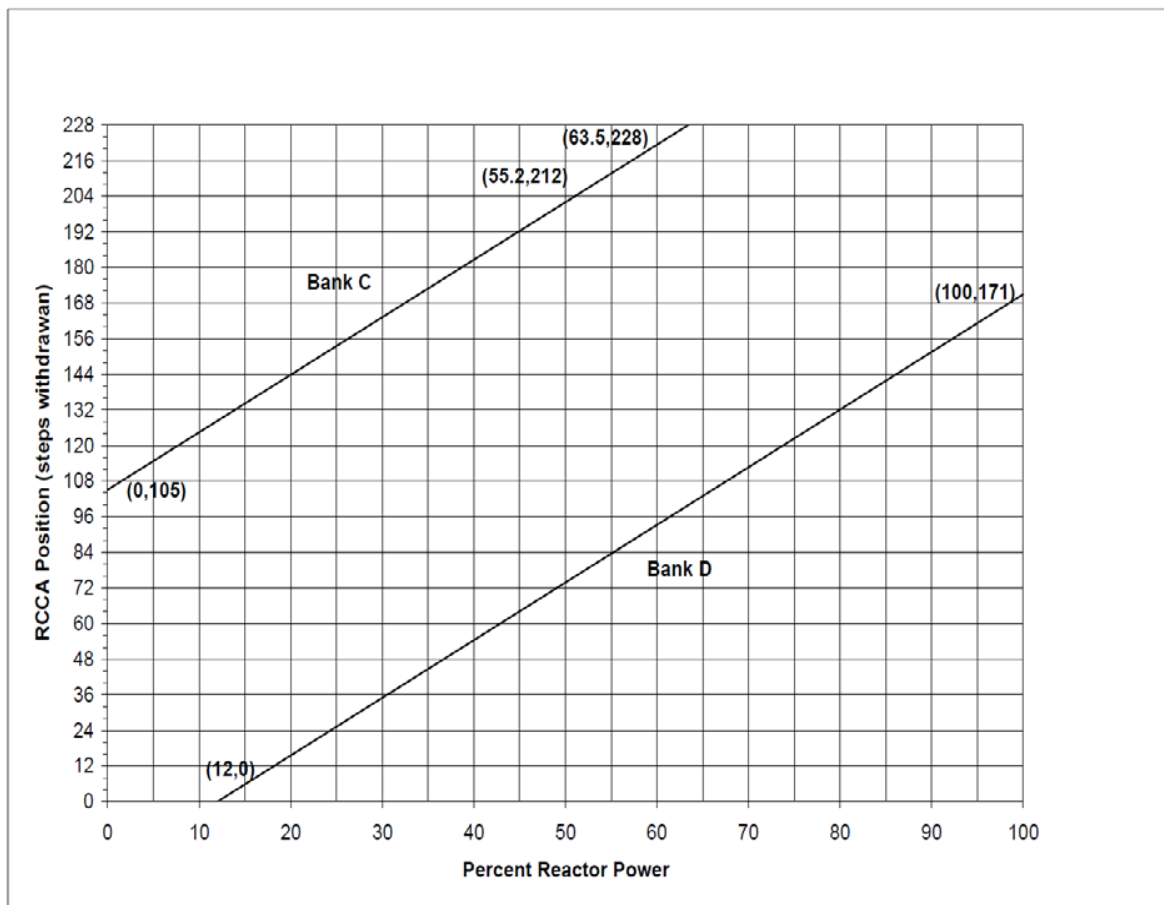
**FIGURE A2**

**Required Shutdown Margin vs Reactor Coolant  
Boron Concentration**



**FIGURE A3**

**Turkey Point Unit 3 Cycle 30 Rod Insertion Limits vs Thermal Power**  
**ARO = 228 Steps Withdrawn, Overlap = 100 Steps**



**FIGURE A4**

**Axial Flux Difference as a Function of Rated Thermal Power  
Turkey Point Unit 3 Cycle 30**

