



South Texas Project Electric Generating Station P.O. Box 289 Wadsworth, Texas 77483

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NOC-AE-18003600
10 CFR 50.36

Attention: Document Control Desk
U.S. Nuclear Regulatory Commission
Washington, DC 20555-0001


South Texas Project
Units 1 and 2
Docket No. STN 50-498 and STN 50-499
Revisions to the Unit 1 Cycle 21 and Unit 2 Cycle 20 Core Operating Limits Reports

Reference: Letter from L.M. Regner, NRC, to G.T. Powell, STPNOC, "South Texas Project, Units 1 and 2 – Issuance of Amendments to Revise Technical Specifications for Administrative Changes and to Relocate F_{xy} Exclusion Zones to the Core Operating Limits Report", June 7, 2018 (AE-NOC-18003111)

In accordance with Technical Specification 6.9.1.6.d, STP Nuclear Operating Company submits the attached revised Core Operating Limits Reports for Unit 1 Cycle 21 (Revision 2) and Unit 2 Cycle 20 (Revision 1). These revisions incorporate changes made in accordance with License Amendment Nos. 213 and 199 related to relocating the F_{xy} exclusion zones to the Core Operating Limits Reports.

There are no commitments in this letter.

If there are any questions regarding this matter, please contact Wendy Brost at (361) 972-8516 or me at (361) 972-4414.


Michael C. Page
General Manager, Engineering

web

Enclosures: 1. South Texas Project Unit 1 Cycle 21 Core Operating Limits Report, Revision 2
2. South Texas Project Unit 2 Cycle 20 Core Operating Limits Report, Revision 1

STI: 34726880

cc:

Regional Administrator, Region IV
U. S. Nuclear Regulatory Commission
1600 E. Lamar Blvd
Arlington, Texas 76011-4511

Lisa M. Regner
Senior Project Manager
U.S. Nuclear Regulatory Commission
One White Flint North (O9E01)
11555 Rockville Pike
Rockville, MD 20852

NRC Resident Inspector
U. S. Nuclear Regulatory Commission
P. O. Box 289, Mail Code: MN116
Wadsworth, TX 77483

NOC-AE-18003600
Enclosure 1

Enclosure 1

South Texas Project
Unit 1 Cycle 21 Core Operating Limits Report, Revision 2



SOUTH TEXAS PROJECT

Unit 1 Cycle 21

CORE OPERATING LIMITS REPORT

Revision 2

1.0 CORE OPERATING LIMITS REPORT

This Core Operating Limits Report for STPEGS Unit 1 Cycle 21 has been prepared in accordance with the requirements of Technical Specification 6.9.1.6. The core operating limits have been developed using the NRC-approved methodologies specified in Technical Specification 6.9.1.6.

The Technical Specifications affected by this report are:

- 1) 2.1 SAFETY LIMITS
- 2) 2.2 LIMITING SAFETY SYSTEM SETTINGS
- 3) 3/4.1.1.1 SHUTDOWN MARGIN
- 4) 3/4.1.1.3 MODERATOR TEMPERATURE COEFFICIENT LIMITS
- 5) 3/4.1.3.5 SHUTDOWN ROD INSERTION LIMITS
- 6) 3/4.1.3.6 CONTROL ROD INSERTION LIMITS
- 7) 3/4.2.1 AFD LIMITS
- 8) 3/4.2.2 HEAT FLUX HOT CHANNEL FACTOR
- 9) 3/4.2.3 NUCLEAR ENTHALPY RISE HOT CHANNEL FACTOR
- 10) 3/4.2.5 DNB PARAMETERS

2.0 OPERATING LIMITS

The cycle-specific parameter limits for the specifications listed in Section 1.0 are presented below.

2.1 SAFETY LIMITS (Specification 2.1):

- 2.1.1 The combination of THERMAL POWER, pressurizer pressure, and the highest operating loop coolant temperature (T_{avg}) shall not exceed the limits shown in Figure 1.

2.2 LIMITING SAFETY SYSTEM SETTINGS (Specification 2.2):

- 2.2.1 The Loop design flow for Reactor Coolant Flow-Low is 98,000 gpm.

2.2.2 The Over-temperature ΔT and Over-power ΔT setpoint parameter values are listed below:

Over-temperature ΔT Setpoint Parameter Values

- τ_1 measured reactor vessel ΔT lead/lag time constant, $\tau_1 = 8$ sec
- τ_2 measured reactor vessel ΔT lead/lag time constant, $\tau_2 = 3$ sec
- τ_3 measured reactor vessel ΔT lag time constant, $\tau_3 = 2$ sec
- τ_4 measured reactor vessel average temperature lead/lag time constant, $\tau_4 = 28$ sec
- τ_5 measured reactor vessel average temperature lead/lag time constant, $\tau_5 = 4$ sec
- τ_6 measured reactor vessel average temperature lag time constant, $\tau_6 = 2$ sec
- K_1 Overtemperature ΔT reactor trip setpoint, $K_1 = 1.14$
- K_2 Overtemperature ΔT reactor trip setpoint T_{avg} coefficient, $K_2 = 0.028/^\circ F$
- K_3 Overtemperature ΔT reactor trip setpoint pressure coefficient, $K_3 = 0.00143/psi$
- T' Nominal full power T_{avg} , $T' \leq 592.0$ $^\circ F$
- P' Nominal RCS pressure, $P' = 2235$ psig

$f_1(\Delta I)$ is a function of the indicated difference between top and bottom detectors of the power-range neutron ion chambers; with gains to be selected based on measured instrument response during plant startup tests such that:

- (1) For $q_t - q_b$ between -70% and $+8\%$, $f_1(\Delta I) = 0$, where q_t and q_b are percent RATED THERMAL POWER in the top and bottom halves of the core respectively, and $q_t + q_b$ is total THERMAL POWER in percent of RATED THERMAL POWER;
- (2) For each percent that $q_t - q_b$ is more negative than -70% , the ΔT Trip Setpoint shall be automatically reduced by 0.0% of its value at RATED THERMAL POWER; and
- (3) For each percent that $q_t - q_b$ is more positive than $+8\%$, the ΔT Trip Setpoint shall be automatically reduced by 2.65% of its value at RATED THERMAL POWER. (Reference 3.6 and Section 4.4.1.2 of Reference 3.7)

Over-power ΔT Setpoint Parameter Values

- τ_1 measured reactor vessel ΔT lead/lag time constant, $\tau_1 = 8$ sec
- τ_2 measured reactor vessel ΔT lead/lag time constant, $\tau_2 = 3$ sec
- τ_3 measured reactor vessel ΔT lag time constant, $\tau_3 = 2$ sec
- τ_6 measured reactor vessel average temperature lag time constant, $\tau_6 = 2$ sec
- τ_7 Time constant utilized in the rate-lag compensator for T_{avg} , $\tau_7 = 10$ sec
- K_4 Overpower ΔT reactor trip setpoint, $K_4 = 1.08$
- K_5 Overpower ΔT reactor trip setpoint T_{avg} rate/lag coefficient, $K_5 = 0.02/^\circ F$ for increasing average temperature, and $K_5 = 0$ for decreasing average temperature
- K_6 Overpower ΔT reactor trip setpoint T_{avg} heatup coefficient $K_6 = 0.002/^\circ F$ for $T > T''$, and $K_6 = 0$ for $T \leq T''$
- T'' Indicated full power T_{avg} , $T'' \leq 592.0$ $^\circ F$
- $f_2(\Delta I) = 0$ for all (ΔI)

2.3 SHUTDOWN MARGIN¹ (Specification 3.1.1.1):

The SHUTDOWN MARGIN shall be:

- 2.3.1 Greater than 1.3% $\Delta\rho$ for MODES 1 and 2*
*See Special Test Exception 3.10.1
- 2.3.2 Greater than the limits in Figure 2 for MODES 3 and 4.
- 2.3.3 Greater than the limits in Figure 3 for MODE 5.

2.4 MODERATOR TEMPERATURE COEFFICIENT (Specification 3.1.1.3):

- 2.4.1 The BOL, ARO, MTC shall be less positive than the limits shown in Figure 4.
- 2.4.2 The EOL, ARO, HFP, MTC shall be less negative than -62.6 pcm/°F.
- 2.4.3 The 300 ppm, ARO, HFP, MTC shall be less negative than -53.6 pcm/°F (300 ppm Surveillance Limit).

Where: BOL stands for Beginning-of-Cycle Life,
EOL stands for End-of-Cycle Life,
ARO stands for All Rods Out,
HFP stands for Hot Full Power (100% RATED THERMAL POWER),
HFP vessel average temperature is 592 °F.

- 2.4.4 The Revised Predicted near-EOL 300 ppm MTC shall be calculated using the algorithm from the document referenced by Technical Specification 6.9.1.6.b.10:

$$\text{Revised Predicted MTC} = \text{Predicted MTC} + \text{AFD Correction} - 3 \text{ pcm/°F}$$

If the Revised Predicted MTC is less negative than the COLR Section 2.4.3 limit and all of the benchmark data contained in the surveillance procedure are met, then an MTC measurement in accordance with S.R. 4.1.1.3b is not required.

2.5 ROD INSERTION LIMITS¹ (Specification 3.1.3.5 and 3.1.3.6):

- 2.5.1 All banks shall have the same Full Out Position (FOP) of either 256 or 259 steps withdrawn.
- 2.5.2 The Control Banks shall be limited in physical insertion as specified in Figure 5.
- 2.5.3 Individual Shutdown bank rods are fully withdrawn when the Bank Demand Indication is at the FOP and the Rod Group Height Limiting Condition for Operation is satisfied (T.S. 3.1.3.1).

¹ The Shutdown Margin and Rod Insertion limits account for the removal of RCCA D6 in Shutdown Bank A.

2.6 AXIAL FLUX DIFFERENCE (Specification 3.2.1):

- 2.6.1 AFD limits as required by Technical Specification 3.2.1 are determined by Constant Axial Offset Control (CAOC) Operations with an AFD target band of +5, -10%.
- 2.6.2 The AFD shall be maintained within the ACCEPTABLE OPERATION portion of Figure 6, as required by Technical Specifications.

2.7 HEAT FLUX HOT CHANNEL FACTOR (Specification 3.2.2):

- 2.7.1 $F_Q^{RTP} = 2.55$.
- 2.7.2 $K(Z)$ is provided in Figure 7.
- 2.7.3 The F_{xy} limits for RATED THERMAL POWER (F_{xy}^{RTP}) within specific core planes shall be:
- 2.7.3.1 Less than or equal to 2.102 for all cycle burnups for all core planes containing Bank "D" control rods, and
- 2.7.3.2 Less than or equal to the appropriate core height-dependent value from Table 1 for all unrodded core planes.
- 2.7.3.3 $PF_{xy} = 0.2$.

These F_{xy} limits were used to confirm that the heat flux hot channel factor $F_Q(Z)$ will be limited by Technical Specification 3.2.2 assuming the most-limiting axial power distributions expected to result for the insertion and removal of Control Banks C and D during operation, including the accompanying variations in the axial xenon and power distributions, as described in WCAP-8385. Therefore, these F_{xy} limits provide assurance that the initial conditions assumed in the LOCA analysis are met, along with the ECCS acceptance criteria of 10 CFR 50.46.

- 2.7.4 The F_{xy} limits from Section 2.7.3 above are not applicable in the following core plane regions as measured in percent of core height from the bottom of the fuel:
- 2.7.4.1 Lower core region from 0 to 15%, inclusive,
- 2.7.4.2 Upper core region from 85 to 100%, inclusive,
- 2.7.4.3 Grid plane regions at 22.4%, 34.2%, 46.0%, 57.8%, 69.5%, and 81.3%, (grid plane regions $\pm 2\%$, inclusive), and
- 2.7.4.4 Core plane regions within $\pm 2\%$ of core height (± 3.36 inches) about the bank demand position of the bank "D" control rods.
- 2.7.5 Core Power Distribution Measurement Uncertainty for the Heat Flux Hot Channel Factor
- 2.7.5.1 If the Power Distribution Monitoring System (PDMS) is operable, as defined in the Technical Requirements Manual Section 3.3.3.12, the core power distribution measurement uncertainty (U_{FQ}) to be applied to the $F_Q(Z)$ and $F_{xy}(Z)$ using the PDMS shall be calculated by:
- $$U_{FQ} = (1.0 + (U_Q/100)) * U_E$$

Where:

U_Q = Uncertainty for power peaking factor as defined in Equation 5-19 from the document referenced by Technical Specification 6.9.1.6.b.11

U_E = Engineering uncertainty factor of 1.03.

This uncertainty is calculated and applied automatically by the Power Distribution Monitoring System (PDMS).

2.7.5.2 If the moveable detector system is used, the core power distribution measurement uncertainty (U_{FQ}) to be applied to the $F_Q(Z)$ and $F_{xy}(Z)$ shall be calculated by:

$$U_{FQ} = U_{QU} * U_E$$

Where:

U_{QU} = Base F_Q measurement uncertainty of 1.05.

U_E = Engineering uncertainty factor of 1.03.

2.8 ENTHALPY RISE HOT CHANNEL FACTOR (Specification 3.2.3):

2.8.1 $F_{\Delta H}^{RTP} = 1.62$

2.8.2 $PF_{\Delta H} = 0.3$

2.8.3 Core Power Distribution Measurement Uncertainty for the Enthalpy Rise Hot Channel Factor

2.8.3.1 If the Power Distribution Monitoring System (PDMS) is operable, as defined in the Technical Requirements Manual Section 3.3.3.12, the core power distribution measurement uncertainty (U_{FAH}) to be applied to the $F_{\Delta H}$ using the PDMS shall be the greater of:

$$U_{FAH} = 1.04$$

OR

$$U_{FAH} = 1.0 + (U_{\Delta H}/100)$$

Where:

$U_{\Delta H}$ = Uncertainty for power peaking factor as defined in Equation 5-19 from the document referenced in Technical Specification 6.9.1.6.b.11.

This uncertainty is calculated and applied automatically by the Power Distribution Monitoring System.

2.8.3.2 If the moveable detector system is used, the core power distribution measurement uncertainty (U_{FAH}) shall be:

$$U_{FAH} = 1.04$$

2.9 DNB PARAMETERS (Specification 3.2.5):

2.9.1 The following DNB-related parameters shall be maintained within the following limits: ¹

2.9.1.1 Reactor Coolant System $T_{avg} \leq 595$ °F ²,

2.9.1.2 Pressurizer Pressure > 2200 psig ³,

2.9.1.3 Minimum Measured Reactor Coolant System Flow $> 403,000$ gpm⁴.

3.0 REFERENCES

- 3.1 Letter from J. M. Ralston (Westinghouse) to R. F. Dunn (STPNOC), "South Texas Project Electric Generating Station Unit 1 Cycle 21 Redesign Final Reload Evaluation" NF-TG-17-7, Rev. 1 (ST-UB-NOC-17003573, Rev. 1) dated April 12, 2017.
- 3.2 NUREG-1346, Technical Specifications, South Texas Project Unit Nos. 1 and 2.
- 3.3 STPNOC Calculation ZC-7035, Rev. 2, "Loop Uncertainty Calculation for RCS Tavg Instrumentation," Section 10.1.
- 3.4 STPNOC Calculation ZC-7032, Rev. 6, "Loop Uncertainty Calculation for Narrow Range Pressurizer Pressure Monitoring Instrumentation," Section 2.3, Page 9.
- 3.5 Letter from J. S Wyble (Westinghouse) to T. J. Jordan (STPNOC), "STP Nuclear Operating Company Units 1 & 2 Power Uprate PCWG Parameters," ST-WN-NOC-00-000072 dated December 15, 2000, STI 31218644.
- 3.6 Letter from J. M. Ralston (Westinghouse) to D. F. Hoppes (STPNOC), "South Texas Project Electric Generating Station Units 1 and 2 Documentation of the $f_i(\Delta I)$ Function in OTAT Setpoint Calculation," NF-TG-11-93 (ST-UB-NOC-11003215) dated November 10, 2011.
- 3.7 Document RSE-U1, Rev. 8, "Unit 1 Cycle 21 Reload Safety Evaluation and Core Operating Limits Report." (CR Action 15-23765-6)

¹ A discussion of the processes to be used to take these readings is provided in the basis for Technical Specification 3.2.5.

² Includes a 1.9 °F measurement uncertainty per Reference 3.3, Page 37.

³ Limit not applicable during either a Thermal Power ramp in excess of 5% of RTP per minute or a Thermal Power step in excess of 10% RTP. Per Technical Specification 3.2.5 Bases, this includes a 10.7 psi measurement uncertainty as read on the QDPS display, which is bounded by the 9.6 psi averaged measurement calculated in Reference 3.4.

⁴ Includes the flow measurement uncertainty of 2.8% from Reference 3.5.

Figure 1

Reactor Core Safety Limits - Four Loops in Operation

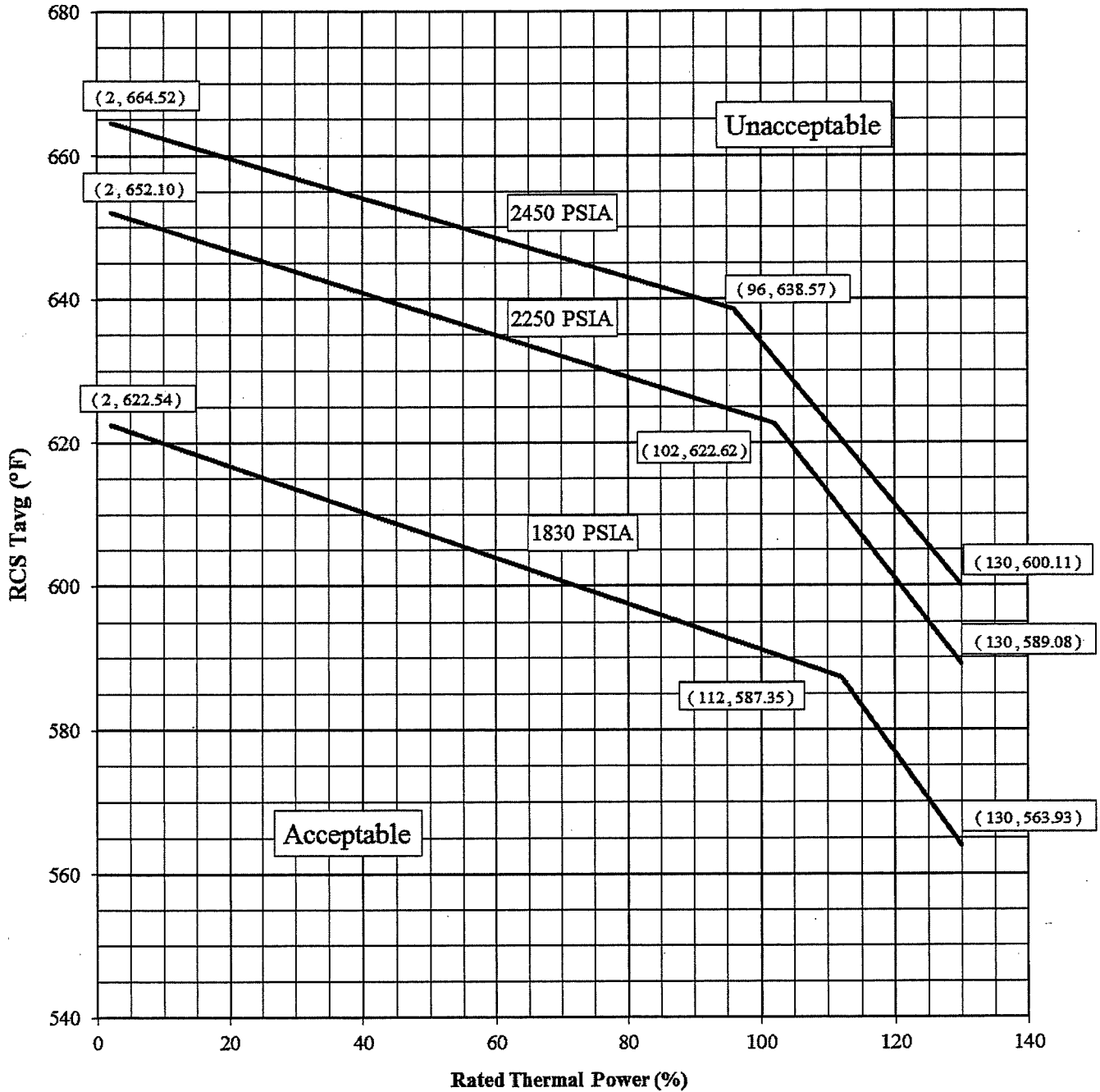


Figure 2

Required Shutdown Margin for Modes 3 & 4

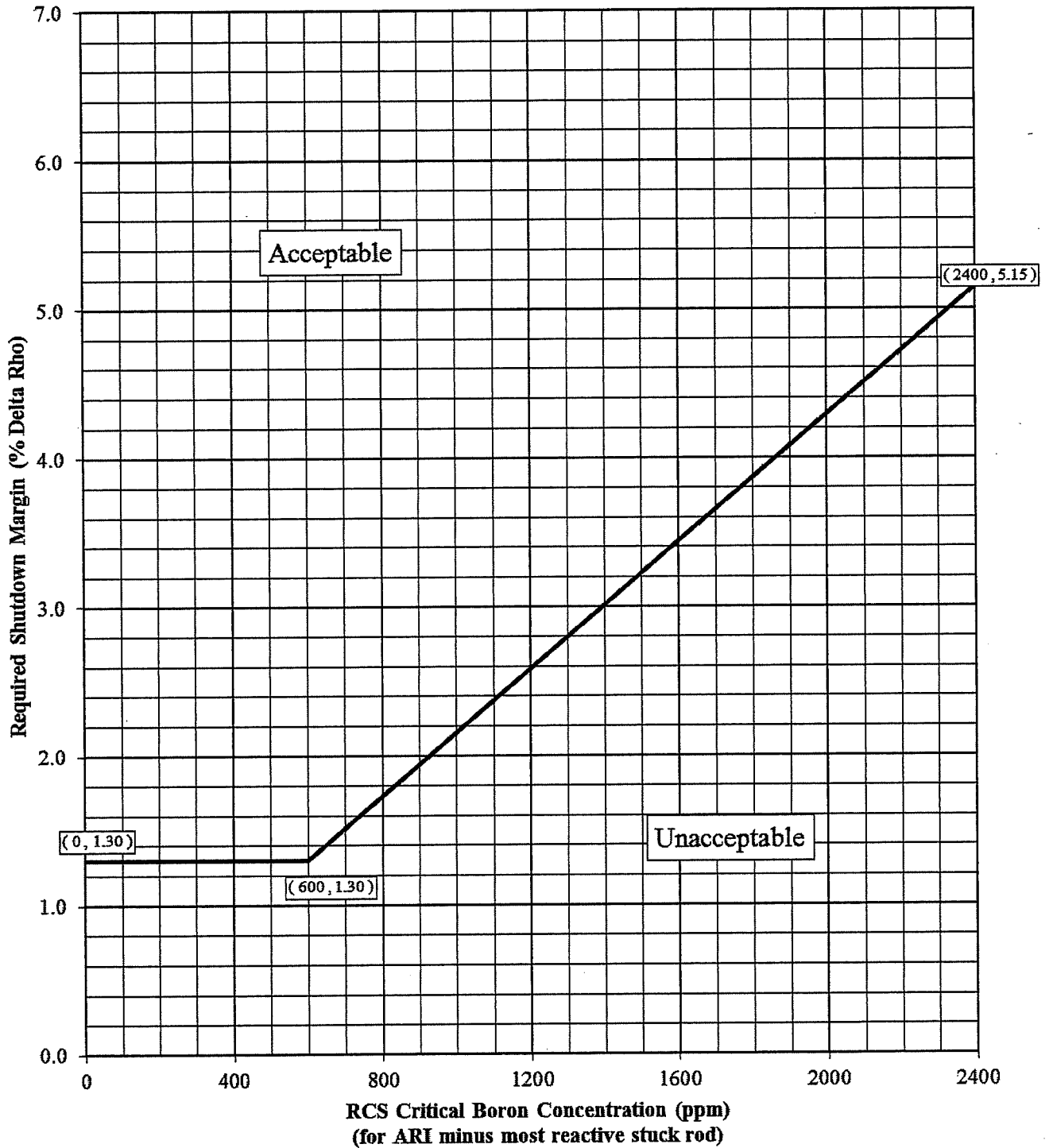


Figure 3

Required Shutdown Margin for Mode 5

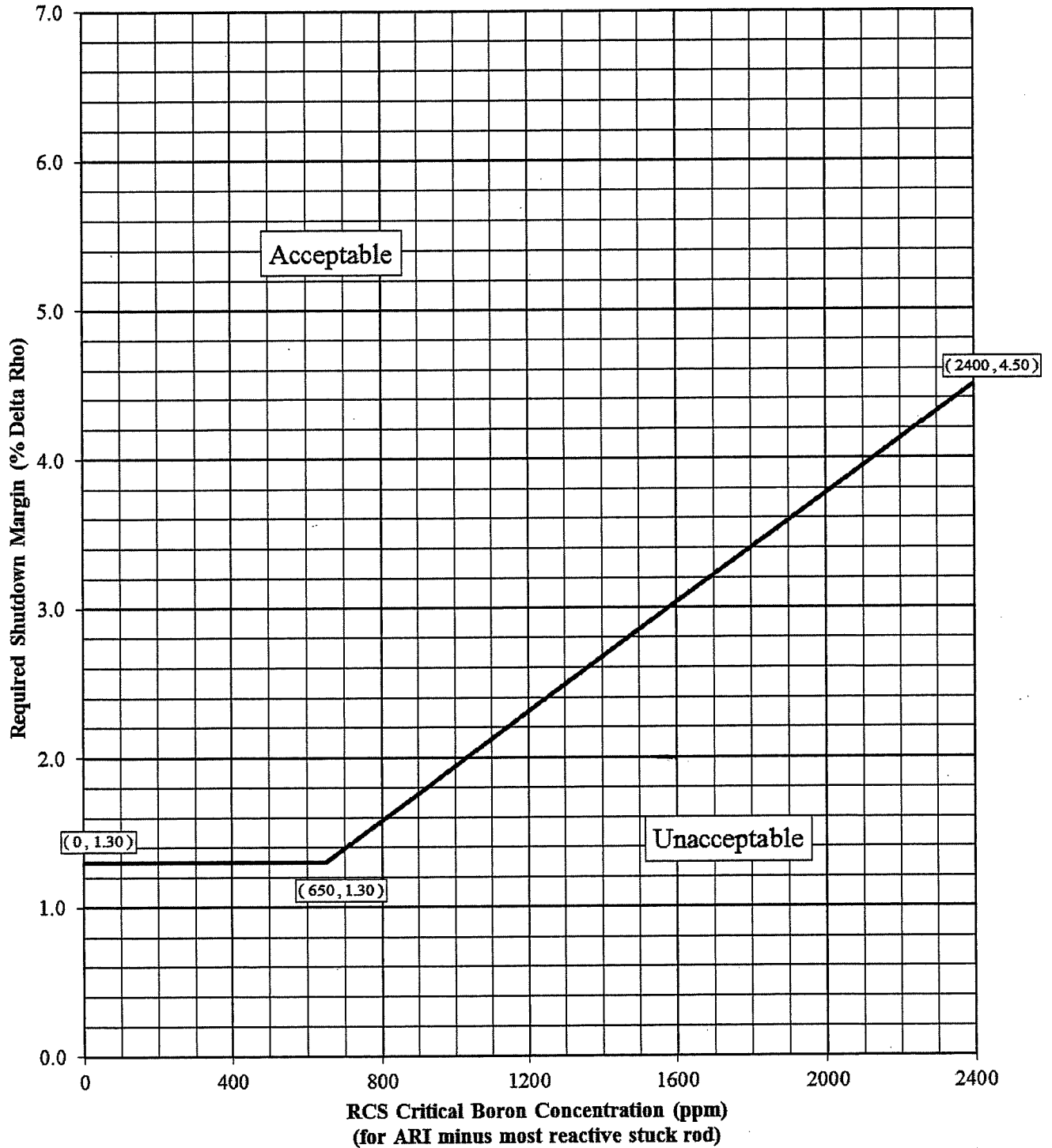


Figure 4

MTC versus Power Level

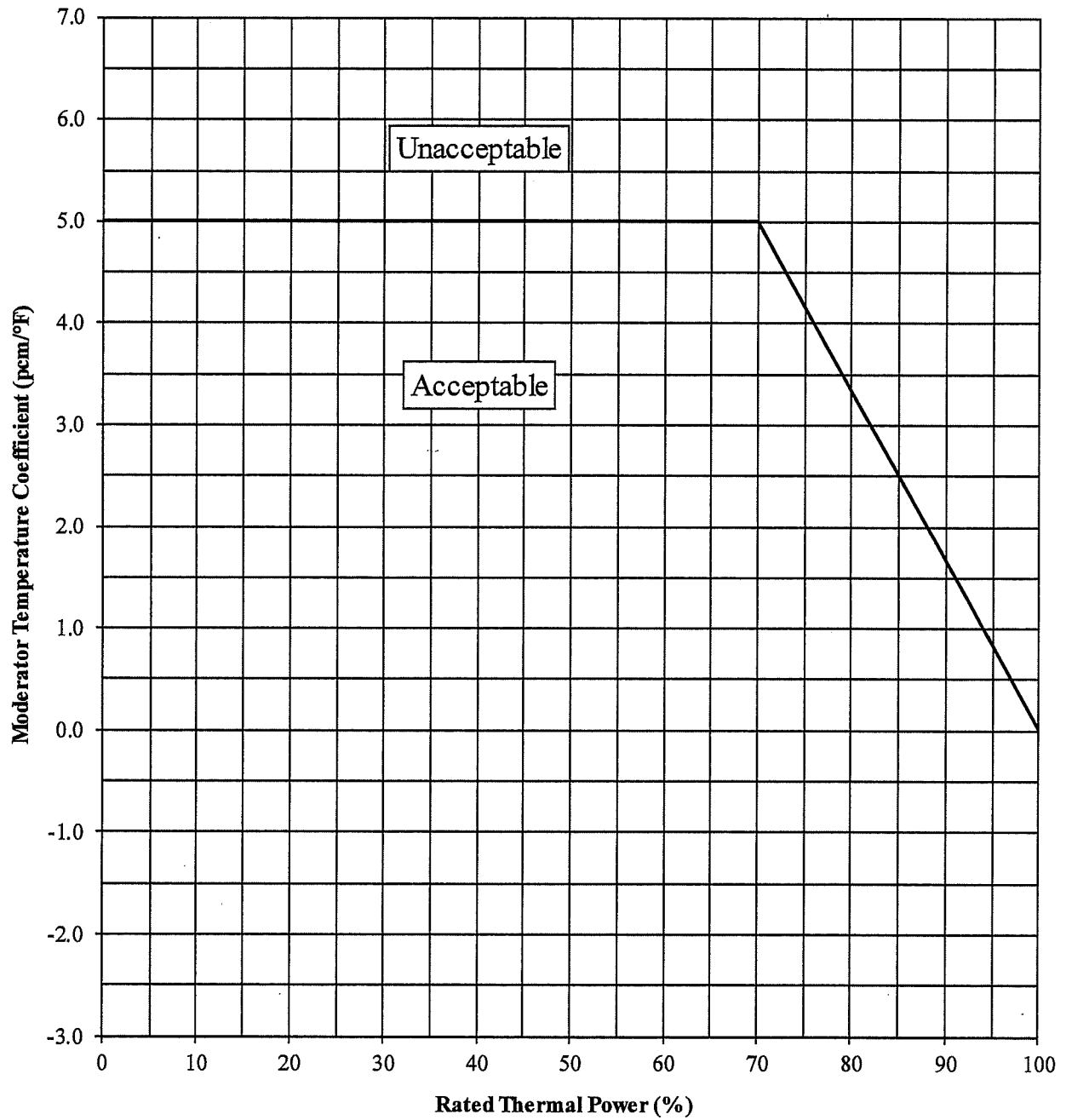


Figure 5

Control Rod Insertion Limits* versus Power Level

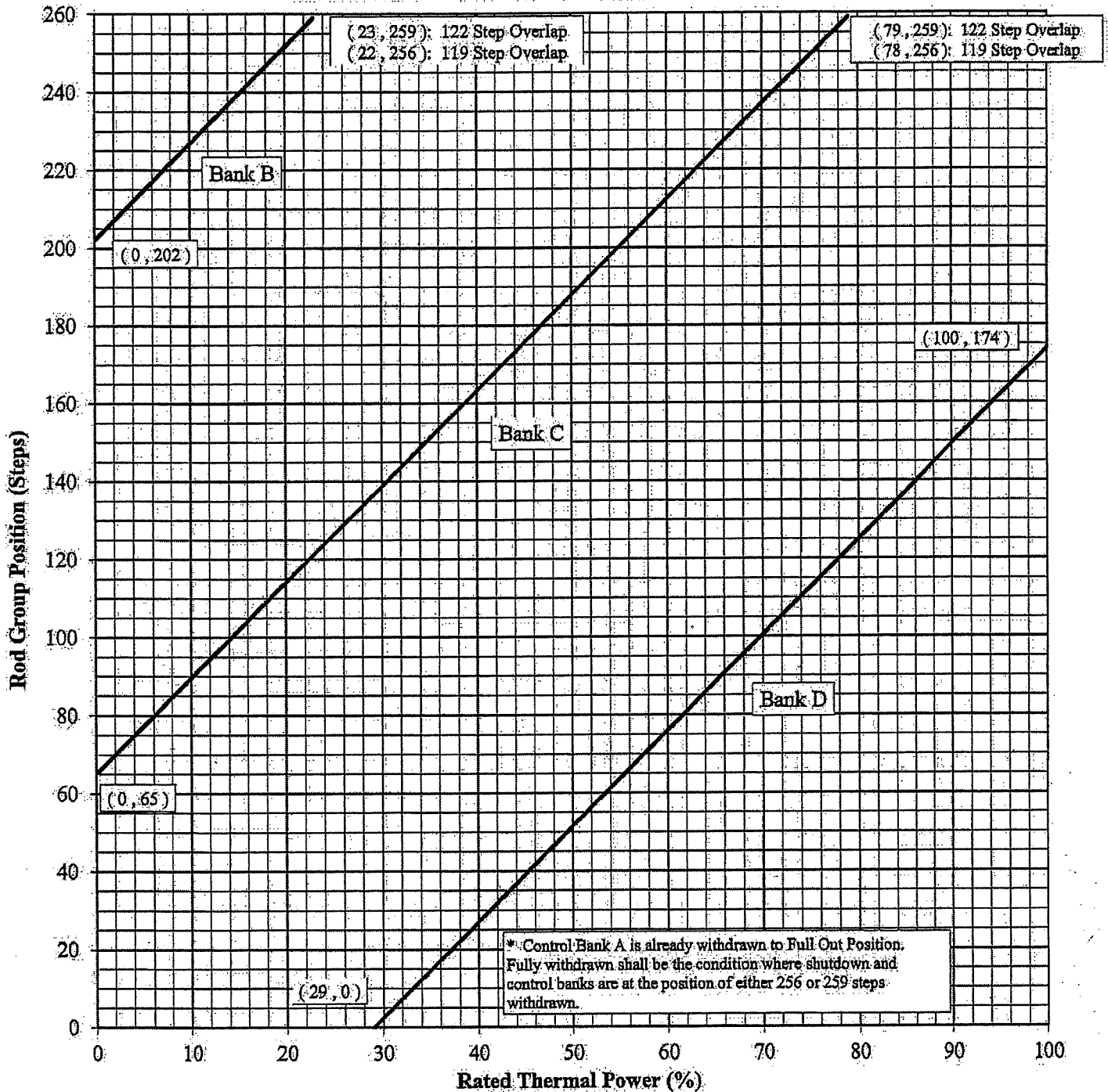


Figure 6

AFD Limits versus Power Level

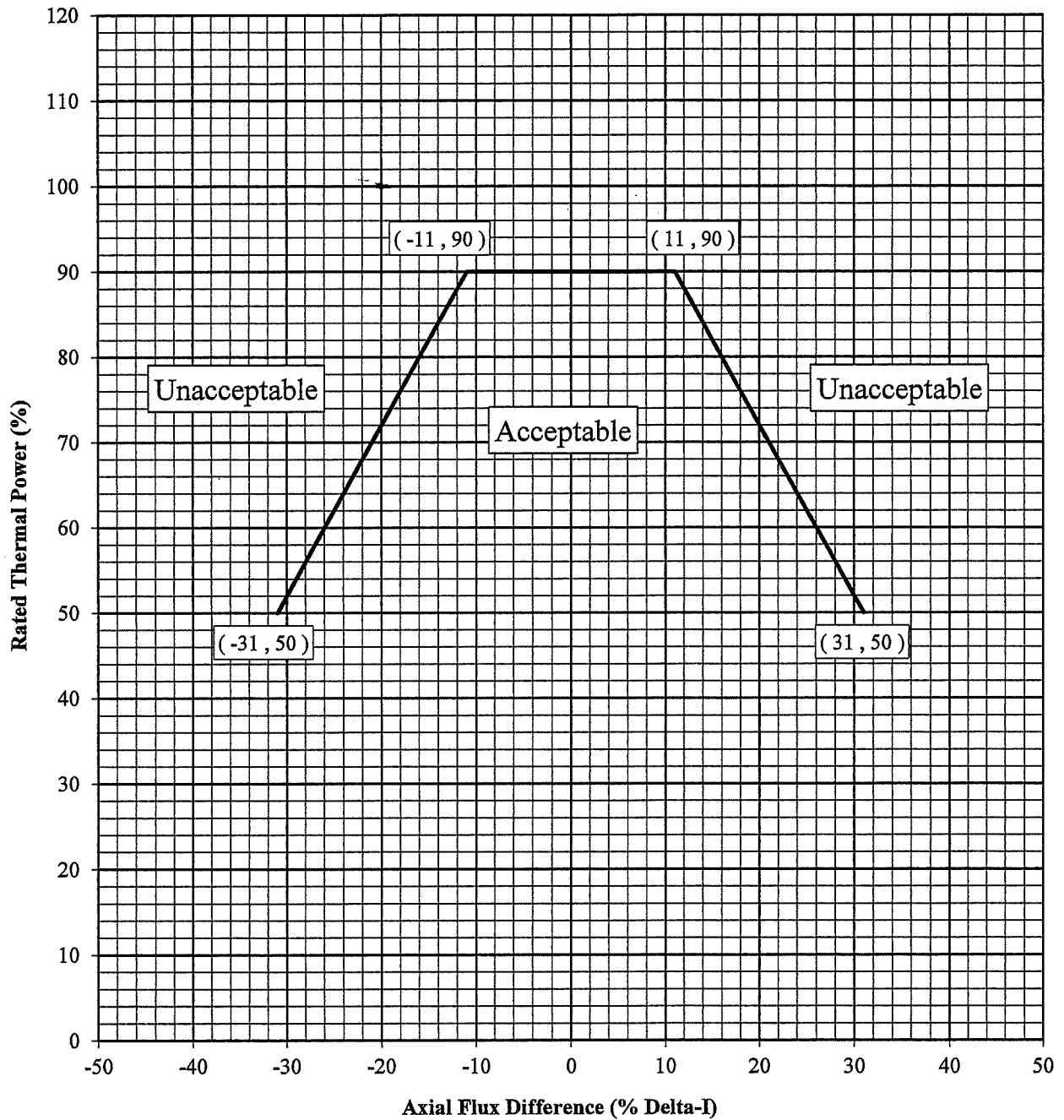


Figure 7

K(Z) - Normalized FQ(Z) versus Core Height

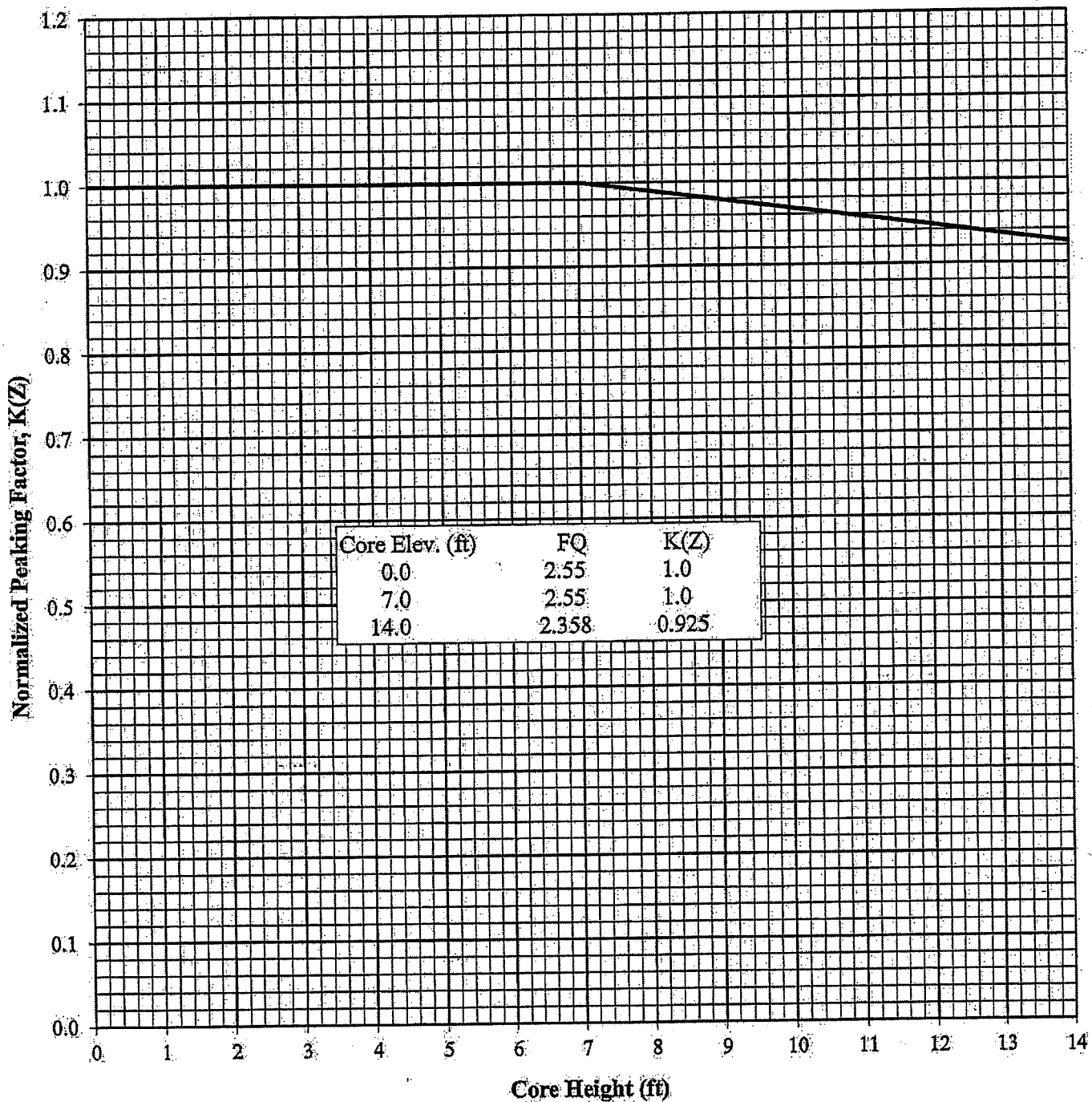


Table 1 (Part 1 of 2)
Unrodded F_{xy} for Each Core Height
for Cycle Burnups Less Than 10,000 MWD/MTU

Core Height (Ft.)	Axial Point	Unrodded Fxy	Core Height (Ft.)	Axial Point	Unrodded Fxy
14.0	1	7.401	6.8	37	1.982
13.8	2	5.801	6.6	38	2.031
13.6	3	4.200	6.4	39	2.008
13.4	4	2.815	6.2	40	1.953
13.2	5	2.534	6.0	41	1.924
13.0	6	2.276	5.8	42	1.956
12.8	7	2.204	5.6	43	1.967
12.6	8	2.186	5.4	44	1.973
12.4	9	2.120	5.2	45	2.019
12.2	10	2.066	5.0	46	2.083
12.0	11	2.039	4.8	47	2.096
11.8	12	2.048	4.6	48	2.042
11.6	13	2.075	4.4	49	1.975
11.4	14	2.061	4.2	50	1.985
11.2	15	2.017	4.0	51	1.984
11.0	16	1.984	3.8	52	1.973
10.8	17	1.972	3.6	53	1.981
10.6	18	1.964	3.4	54	2.024
10.4	19	1.934	3.2	55	2.050
10.2	20	1.950	3.0	56	1.992
10.0	21	1.994	2.8	57	1.939
9.8	22	2.004	2.6	58	1.943
9.6	23	1.934	2.4	59	1.947
9.4	24	1.913	2.2	60	1.955
9.2	25	1.908	2.0	61	1.988
9.0	26	1.903	1.8	62	2.048
8.8	27	1.909	1.6	63	2.049
8.6	28	1.929	1.4	64	1.957
8.4	29	1.987	1.2	65	1.895
8.2	30	2.038	1.0	66	1.937
8.0	31	1.999	0.8	67	2.254
7.8	32	1.937	0.6	68	3.025
7.6	33	1.934	0.4	69	4.318
7.4	34	1.955	0.2	70	6.145
7.2	35	1.950	0.0	71	9.182
7.0	36	1.940			

Table 1 (Part 2 of 2)
Unrodded Fxy for Each Core Height
for Cycle Burnups Greater Than or Equal to 10,000 MWD/MTU

Core Height (Ft.)	Axial Point	Unrodded Fxy	Core Height (Ft.)	Axial Point	Unrodded Fxy
14.0	1	6.408	6.8	37	2.210
13.8	2	5.134	6.6	38	2.246
13.6	3	3.860	6.4	39	2.213
13.4	4	2.756	6.2	40	2.155
13.2	5	2.530	6.0	41	2.121
13.0	6	2.280	5.8	42	2.113
12.8	7	2.139	5.6	43	2.101
12.6	8	2.070	5.4	44	2.088
12.4	9	2.002	5.2	45	2.105
12.2	10	1.991	5.0	46	2.139
12.0	11	2.001	4.8	47	2.133
11.8	12	2.029	4.6	48	2.075
11.6	13	2.061	4.4	49	2.027
11.4	14	2.055	4.2	50	2.022
11.2	15	2.029	4.0	51	2.009
11.0	16	2.015	3.8	52	1.993
10.8	17	2.026	3.6	53	1.994
10.6	18	2.033	3.4	54	2.028
10.4	19	2.043	3.2	55	2.050
10.2	20	2.073	3.0	56	1.992
10.0	21	2.119	2.8	57	1.939
9.8	22	2.137	2.6	58	1.925
9.6	23	2.104	2.4	59	1.907
9.4	24	2.076	2.2	60	1.879
9.2	25	2.088	2.0	61	1.889
9.0	26	2.099	1.8	62	1.936
8.8	27	2.110	1.6	63	1.965
8.6	28	2.127	1.4	64	1.943
8.4	29	2.166	1.2	65	1.956
8.2	30	2.201	1.0	66	2.067
8.0	31	2.166	0.8	67	2.434
7.8	32	2.133	0.6	68	3.163
7.6	33	2.134	0.4	69	4.275
7.4	34	2.146	0.2	70	5.814
7.2	35	2.157	0.0	71	8.515
7.0	36	2.169			

Enclosure 2

South Texas Project
Unit 2 Cycle 20 Core Operating Limits Report, Revision 1



SOUTH TEXAS PROJECT

Unit 2 Cycle 20

CORE OPERATING LIMITS REPORT

Revision 1

1.0 CORE OPERATING LIMITS REPORT

This Core Operating Limits Report for STPEGS Unit 2 Cycle 20 has been prepared in accordance with the requirements of Technical Specification 6.9.1.6. The core operating limits have been developed using the NRC-approved methodologies specified in Technical Specification 6.9.1.6.

The Technical Specifications affected by this report are:

- 1) 2.1 SAFETY LIMITS
- 2) 2.2 LIMITING SAFETY SYSTEM SETTINGS
- 3) 3/4.1.1.1 SHUTDOWN MARGIN
- 4) 3/4.1.1.3 MODERATOR TEMPERATURE COEFFICIENT LIMITS
- 5) 3/4.1.3.5 SHUTDOWN ROD INSERTION LIMITS
- 6) 3/4.1.3.6 CONTROL ROD INSERTION LIMITS
- 7) 3/4.2.1 AFD LIMITS
- 8) 3/4.2.2 HEAT FLUX HOT CHANNEL FACTOR
- 9) 3/4.2.3 NUCLEAR ENTHALPY RISE HOT CHANNEL FACTOR
- 10) 3/4.2.5 DNB PARAMETERS

2.0 OPERATING LIMITS

The cycle-specific parameter limits for the specifications listed in Section 1.0 are presented below.

2.1 SAFETY LIMITS (Specification 2.1):

- 2.1.1 The combination of THERMAL POWER, pressurizer pressure, and the highest operating loop coolant temperature (T_{avg}) shall not exceed the limits shown in Figure 1.

2.2 LIMITING SAFETY SYSTEM SETTINGS (Specification 2.2):

- 2.2.1 The Loop design flow for Reactor Coolant Flow-Low is 98,000 gpm.

2.2.2 The Over-temperature ΔT and Over-power ΔT setpoint parameter values are listed below:

Over-temperature ΔT Setpoint Parameter Values

- τ_1 measured reactor vessel ΔT lead/lag time constant, $\tau_1 = 8$ sec
 - τ_2 measured reactor vessel ΔT lead/lag time constant, $\tau_2 = 3$ sec
 - τ_3 measured reactor vessel ΔT lag time constant, $\tau_3 = 2$ sec
 - τ_4 measured reactor vessel average temperature lead/lag time constant, $\tau_4 = 28$ sec
 - τ_5 measured reactor vessel average temperature lead/lag time constant, $\tau_5 = 4$ sec
 - τ_6 measured reactor vessel average temperature lag time constant, $\tau_6 = 2$ sec
 - K_1 Overtemperature ΔT reactor trip setpoint, $K_1 = 1.14$
 - K_2 Overtemperature ΔT reactor trip setpoint T_{avg} coefficient, $K_2 = 0.028/^\circ F$
 - K_3 Overtemperature ΔT reactor trip setpoint pressure coefficient, $K_3 = 0.00143/psi$
 - T' Nominal full power T_{avg} , $T' \leq 592.0$ $^\circ F$
 - P' Nominal RCS pressure, $P' = 2235$ psig
- $f_1(\Delta I)$ is a function of the indicated difference between top and bottom detectors of the power-range neutron ion chambers; with gains to be selected based on measured instrument response during plant startup tests such that:
- (1) For $q_t - q_b$ between -70% and $+8\%$, $f_1(\Delta I) = 0$, where q_t and q_b are percent RATED THERMAL POWER in the top and bottom halves of the core respectively, and $q_t + q_b$ is total THERMAL POWER in percent of RATED THERMAL POWER;
 - (2) For each percent that $q_t - q_b$ is more negative than -70% , the ΔT Trip Setpoint shall be automatically reduced by 0.0% of its value at RATED THERMAL POWER; and
 - (3) For each percent that $q_t - q_b$ is more positive than $+8\%$, the ΔT Trip Setpoint shall be automatically reduced by 2.65% of its value at RATED THERMAL POWER. (Reference 3.6 and Section 4.4.1.2 of Reference 3.7)

Over-power ΔT Setpoint Parameter Values

- τ_1 measured reactor vessel ΔT lead/lag time constant, $\tau_1 = 8$ sec
 - τ_2 measured reactor vessel ΔT lead/lag time constant, $\tau_2 = 3$ sec
 - τ_3 measured reactor vessel ΔT lag time constant, $\tau_3 = 2$ sec
 - τ_6 measured reactor vessel average temperature lag time constant, $\tau_6 = 2$ sec
 - τ_7 Time constant utilized in the rate-lag compensator for T_{avg} , $\tau_7 = 10$ sec
 - K_4 Overpower ΔT reactor trip setpoint, $K_4 = 1.08$
 - K_5 Overpower ΔT reactor trip setpoint T_{avg} rate/lag coefficient, $K_5 = 0.02/^\circ F$ for increasing average temperature, and $K_5 = 0$ for decreasing average temperature
 - K_6 Overpower ΔT reactor trip setpoint T_{avg} heatup coefficient $K_6 = 0.002/^\circ F$ for $T > T'$, and $K_6 = 0$ for $T \leq T'$
 - T'' Indicated full power T_{avg} , $T'' \leq 592.0$ $^\circ F$
- $f_2(\Delta I) = 0$ for all (ΔI)

2.3 SHUTDOWN MARGIN (Specification 3.1.1.1):

The SHUTDOWN MARGIN shall be:

- 2.3.1 Greater than 1.3% $\Delta\rho$ for MODES 1 and 2*
*See Special Test Exception 3.10.1
- 2.3.2 Greater than the limits in Figure 2 for MODES 3 and 4.
- 2.3.3 Greater than the limits in Figure 3 for MODE 5.

2.4 MODERATOR TEMPERATURE COEFFICIENT (Specification 3.1.1.3):

- 2.4.1 The BOL, ARO, MTC shall be less positive than the limits shown in Figure 4.
- 2.4.2 The EOL, ARO, HFP, MTC shall be less negative than -62.6 pcm/ $^{\circ}$ F.
- 2.4.3 The 300 ppm, ARO, HFP, MTC shall be less negative than -53.6 pcm/ $^{\circ}$ F (300 ppm Surveillance Limit).

Where: BOL stands for Beginning-of-Cycle Life,
EOL stands for End-of-Cycle Life,
ARO stands for All Rods Out,
HFP stands for Hot Full Power (100% RATED THERMAL POWER),
HFP vessel average temperature is 592 $^{\circ}$ F.

- 2.4.4 The Revised Predicted near-EOL 300 ppm MTC shall be calculated using the algorithm from Technical Specification 6.9.1.6.b.10:

Revised Predicted MTC = Predicted MTC + AFD Correction - 3 pcm/ $^{\circ}$ F

If the Revised Predicted MTC is less negative than the COLR Section 2.4.3 limit and all of the benchmark data contained in the surveillance procedure are met, then an MTC measurement in accordance with S.R. 4.1.1.3b is not required.

2.5 ROD INSERTION LIMITS (Specification 3.1.3.5 and 3.1.3.6):

- 2.5.1 All banks shall have the same Full Out Position (FOP) of either 256 or 259 steps withdrawn.
- 2.5.2 The Control Banks shall be limited in physical insertion as specified in Figure 5.
- 2.5.3 Individual Shutdown bank rods are fully withdrawn when the Bank Demand Indication is at the FOP and the Rod Group Height Limiting Condition for Operation is satisfied (T.S. 3.1.3.1).

2.6 AXIAL FLUX DIFFERENCE (Specification 3.2.1):

- 2.6.1 AFD limits as required by Technical Specification 3.2.1 are determined by Constant Axial Offset Control (CAOC) Operations with an AFD target band of +5, -10%.
- 2.6.2 The AFD shall be maintained within the ACCEPTABLE OPERATION portion of Figure 6, as required by Technical Specifications.

2.7 HEAT FLUX HOT CHANNEL FACTOR (Specification 3.2.2):

- 2.7.1 $F_Q^{RTP} = 2.55$.
- 2.7.2 $K(Z)$ is provided in Figure 7.
- 2.7.3 The F_{xy} limits for RATED THERMAL POWER (F_{xy}^{RTP}) within specific core planes shall be:
 - 2.7.3.1 Less than or equal to 2.102 for all cycle burnups for all core planes containing Bank "D" control rods, and
 - 2.7.3.2 Less than or equal to the appropriate core height-dependent value from Table 1 for all unrodded core planes.
 - 2.7.3.3 $PF_{xy} = 0.2$.

These F_{xy} limits were used to confirm that the heat flux hot channel factor $F_Q(Z)$ will be limited by Technical Specification 3.2.2 assuming the most-limiting axial power distributions expected to result for the insertion and removal of Control Banks C and D during operation, including the accompanying variations in the axial xenon and power distributions, as described in WCAP-8385. Therefore, these F_{xy} limits provide assurance that the initial conditions assumed in the LOCA analysis are met, along with the ECCS acceptance criteria of 10 CFR 50.46.

- 2.7.4 The F_{xy} limits from Section 2.7.3 above are not applicable in the following core plane regions as measured in percent of core height from the bottom of the fuel:
 - 2.7.4.1 Lower core region from 0 to 15%, inclusive,
 - 2.7.4.2 Upper core region from 85 to 100%, inclusive,
 - 2.7.4.3 Grid plane regions at 22.4%, 34.2%, 46.0%, 57.8%, 69.5%, and 81.3%, (grid plane regions $\pm 2\%$, inclusive), and
 - 2.7.4.4 Core plane regions within $\pm 2\%$ of core height (± 3.36 inches) about the bank demand position of the bank "D" control rods.
- 2.7.5 Core Power Distribution Measurement Uncertainty for the Heat Flux Hot Channel Factor
 - 2.7.5.1 If the Power Distribution Monitoring System (PDMS) is operable, as defined in the Technical Requirements Manual Section 3.3.3.12, the core power distribution measurement uncertainty (U_{FQ}) to be applied to the $F_Q(Z)$ and $F_{xy}(Z)$ using the PDMS shall be calculated by:

$$U_{FQ} = (1.0 + (U_Q/100)) * U_E$$

Where:

U_Q = Uncertainty for power peaking factor as defined in Equation 5-19 from the document referenced by Technical Specification 6.9.1.6.b.11

U_E = Engineering uncertainty factor of 1.03.

This uncertainty is calculated and applied automatically by the Power Distribution Monitoring System (PDMS).

2.7.5.2 If the moveable detector system is used, the core power distribution measurement uncertainty (U_{FQ}) to be applied to the $F_Q(Z)$ and $F_{xy}(Z)$ shall be calculated by:

$$U_{FQ} = U_{QU} * U_E$$

Where:

U_{QU} = Base F_Q measurement uncertainty of 1.05.

U_E = Engineering uncertainty factor of 1.03.

2.8 ENTHALPY RISE HOT CHANNEL FACTOR (Specification 3.2.3):

2.8.1 $F_{\Delta H}^{RTP} = 1.62$

2.8.2 $PF_{\Delta H} = 0.3$

2.8.3 Core Power Distribution Measurement Uncertainty for the Enthalpy Rise Hot Channel Factor

2.8.3.1 If the Power Distribution Monitoring System (PDMS) is operable, as defined in the Technical Requirements Manual Section 3.3.3.12, the core power distribution measurement uncertainty (U_{FAH}) to be applied to the $F_{\Delta H}$ using the PDMS shall be the greater of:

$$U_{FAH} = 1.04$$

OR

$$U_{FAH} = 1.0 + (U_{\Delta H}/100)$$

Where:

$U_{\Delta H}$ = Uncertainty for power peaking factor as defined in Equation 5-19 from the document referenced in Technical Specification 6.9.1.6.b.11.

This uncertainty is calculated and applied automatically by the Power Distribution Monitoring System.

2.8.3.2 If the moveable detector system is used, the core power distribution measurement uncertainty (U_{FAH}) shall be:

$$U_{FAH} = 1.04$$

2.9 DNB PARAMETERS (Specification 3.2.5):

- 2.9.1 The following DNB-related parameters shall be maintained within the following limits (nominal values from Reference 3.1, as annotated below):¹
- 2.9.1.1 Reactor Coolant System $T_{avg} \leq 595 \text{ }^\circ\text{F}$ ²,
 - 2.9.1.2 Pressurizer Pressure $> 2200 \text{ psig}$ ³,
 - 2.9.1.3 Minimum Measured Reactor Coolant System Flow $> 403,000 \text{ gpm}$ ⁴.

3.0 REFERENCES

- 3.1 Letter from A. S. Ganey (Westinghouse) to R. F. Dunn (STPNOC), "South Texas Project Electric Generating Station Unit 2 Cycle 20 Final Reload Evaluation" NF-TG-18-12 (ST-UB-NOC-18003632) dated February 6, 2018.
- 3.2 NUREG-1346, Technical Specifications, South Texas Project Unit Nos. 1 and 2.
- 3.3 STPNOC Calculation ZC-7035, Rev. 2, "Loop Uncertainty Calculation for RCS Tavg Instrumentation," Section 10.1.
- 3.4 STPNOC Calculation ZC-7032, Rev. 6, "Loop Uncertainty Calculation for Narrow Range Pressurizer Pressure Monitoring Instrumentation," Section 2.3, Page 9.
- 3.5 Letter from J. S Wyble (Westinghouse) to T. J. Jordan (STPNOC), "STP Nuclear Operating Company Units 1 & 2 Power Uprate PCWG Parameters," ST-WN-NOC-00-000072 dated December 15, 2000, STI 31218644.
- 3.6 Letter from J. M. Ralston (Westinghouse) to D. F. Hoppes (STPNOC), "South Texas Project Electric Generating Station Units 1 and 2 Documentation of the $f_i(\Delta T)$ Function in OTAT Setpoint Calculation," NF-TG-11-93 (ST-UB-NOC-11003215) dated November 10, 2011.
- 3.7 Document RSE-U2, Rev. 8, "Unit 2 Cycle 20 Reload Safety Evaluation and Core Operating Limits Report." (CR Action 15-23765-7)

¹ A discussion of the processes to be used to take these readings is provided in the basis for Technical Specification 3.2.5.

² Includes a 1.9 °F measurement uncertainty per Reference 3.3, Page 37.

³ Limit not applicable during either a Thermal Power ramp in excess of 5% of RTP per minute or a Thermal Power step in excess of 10% RTP. Per Technical Specification 3.2.5 Bases, this includes a 10.7 psi measurement uncertainty as read on the QDPS display, which is bounded by the 9.6 psi averaged measurement calculated in Reference 3.4.

⁴ Includes the flow measurement uncertainty of 2.8% from Reference 3.5.

Figure 1

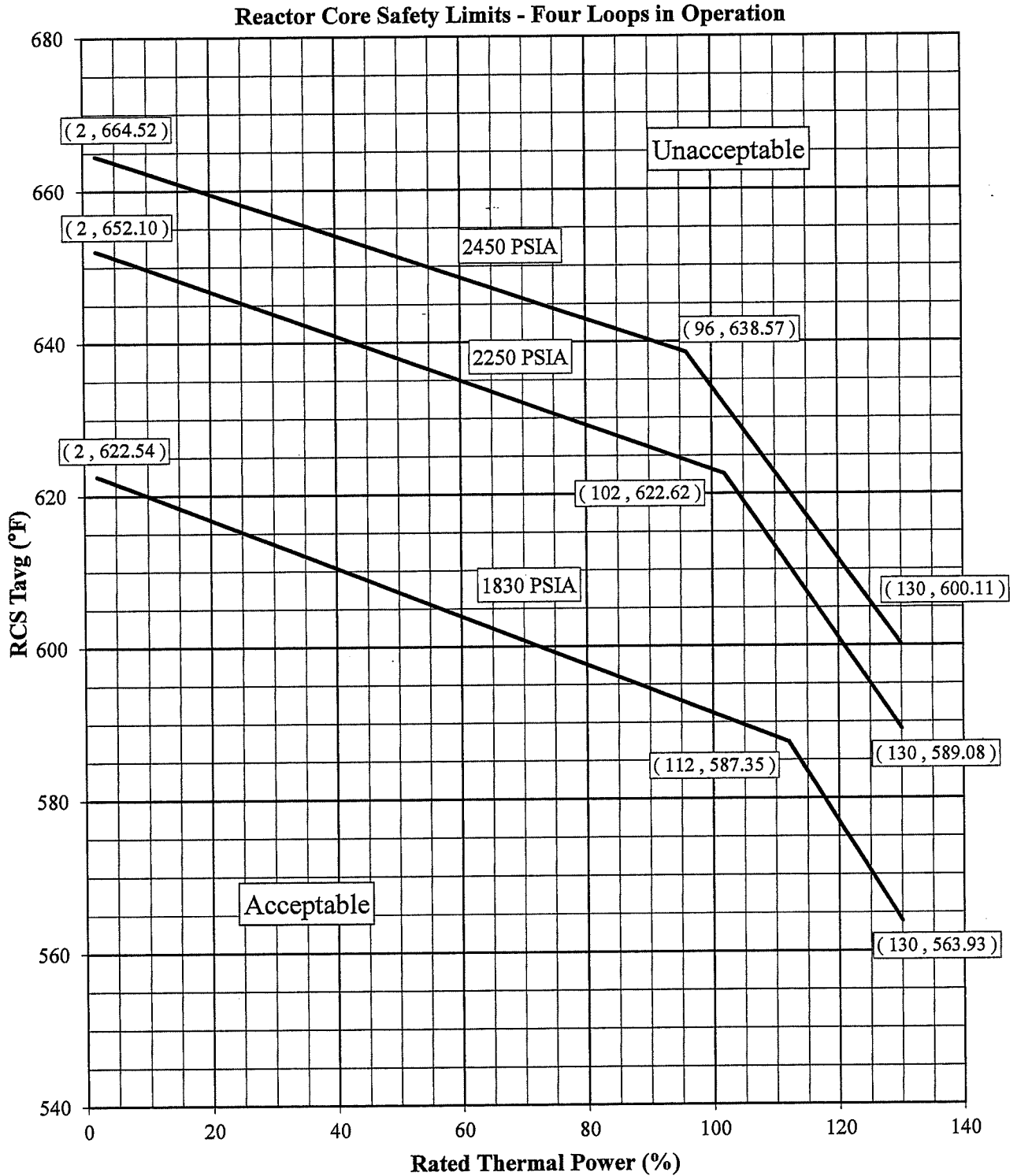


Figure 2

Required Shutdown Margin for Modes 3 & 4

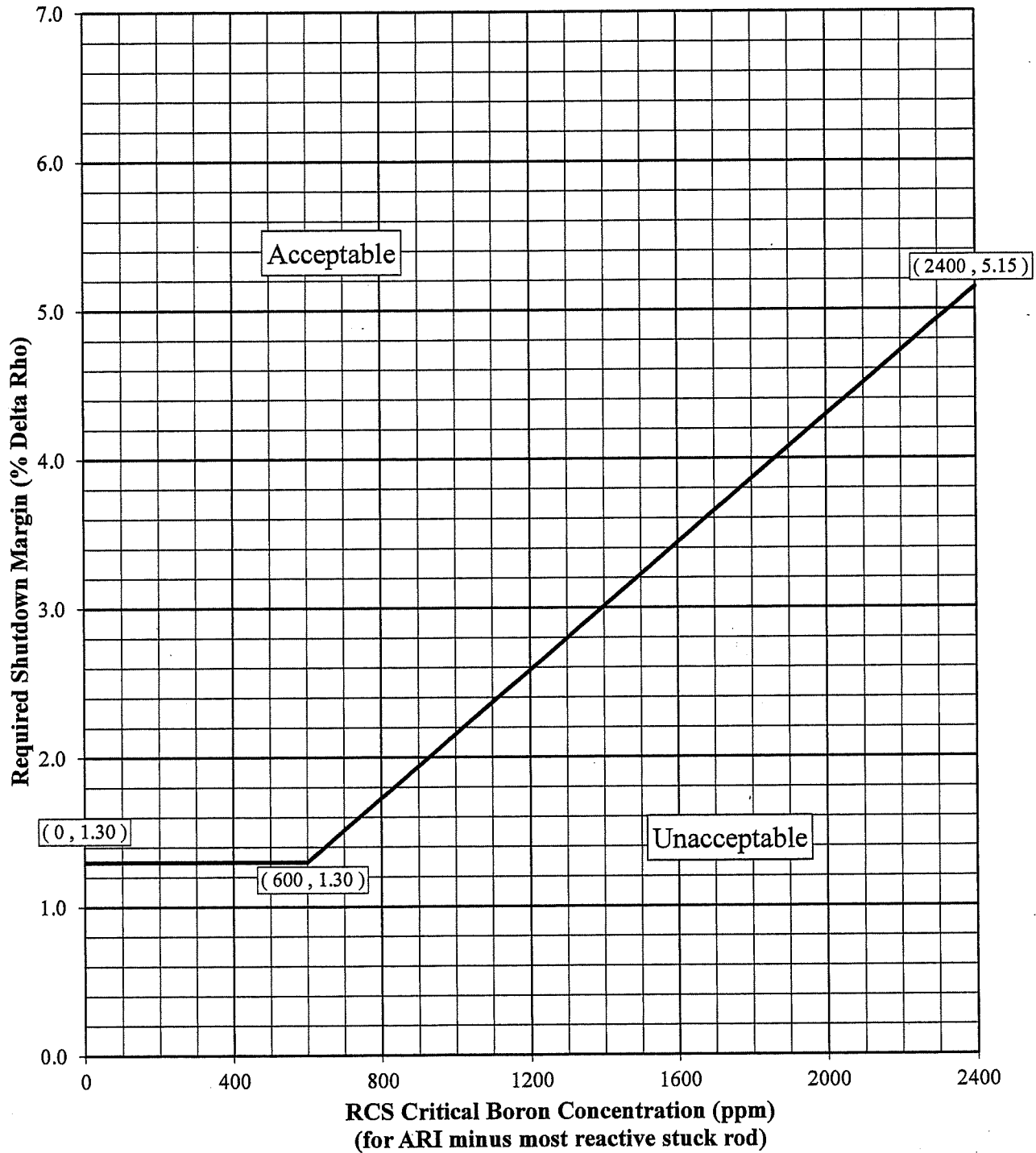


Figure 3

Required Shutdown Margin for Mode 5

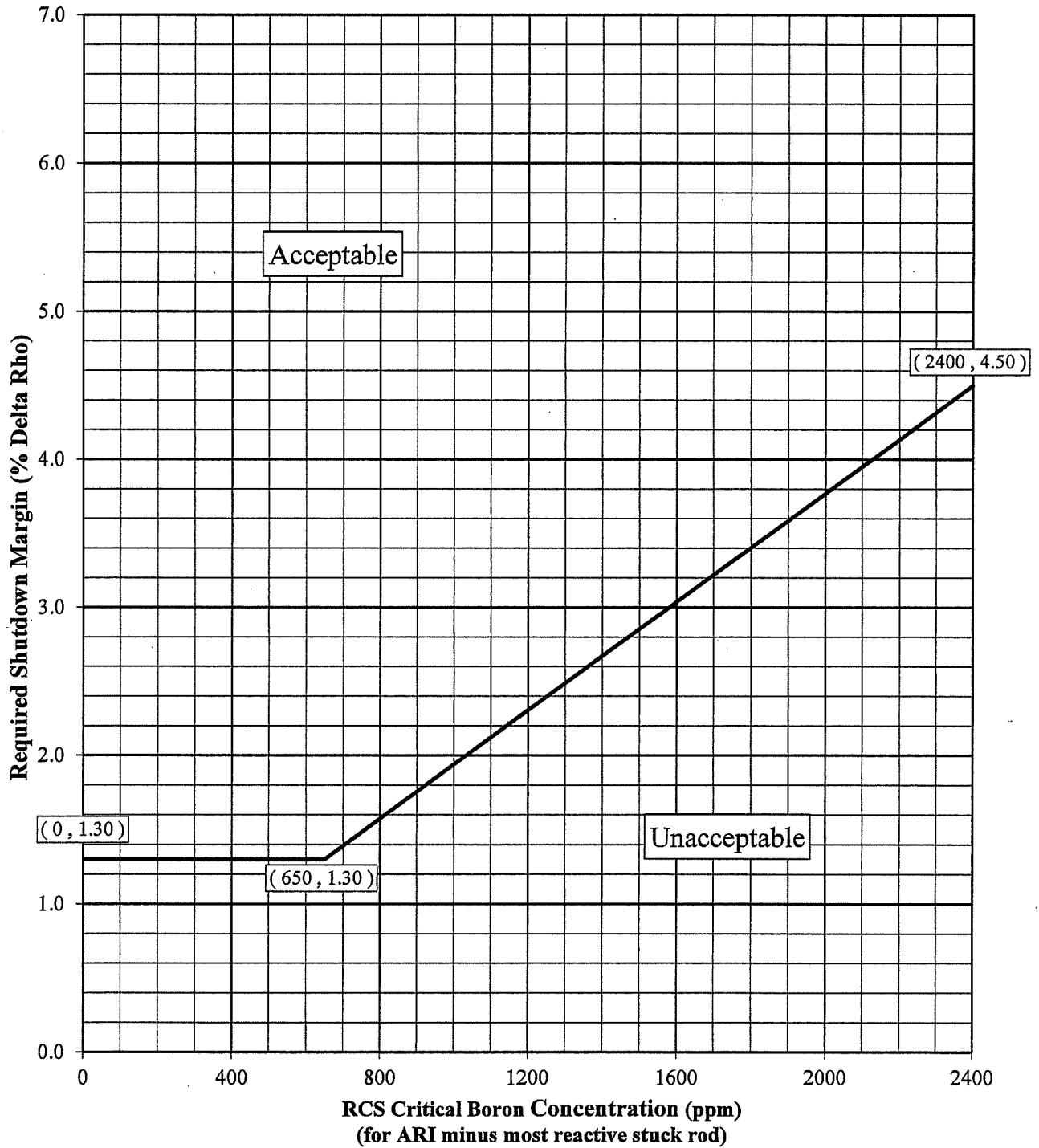


Figure 4

MTC versus Power Level

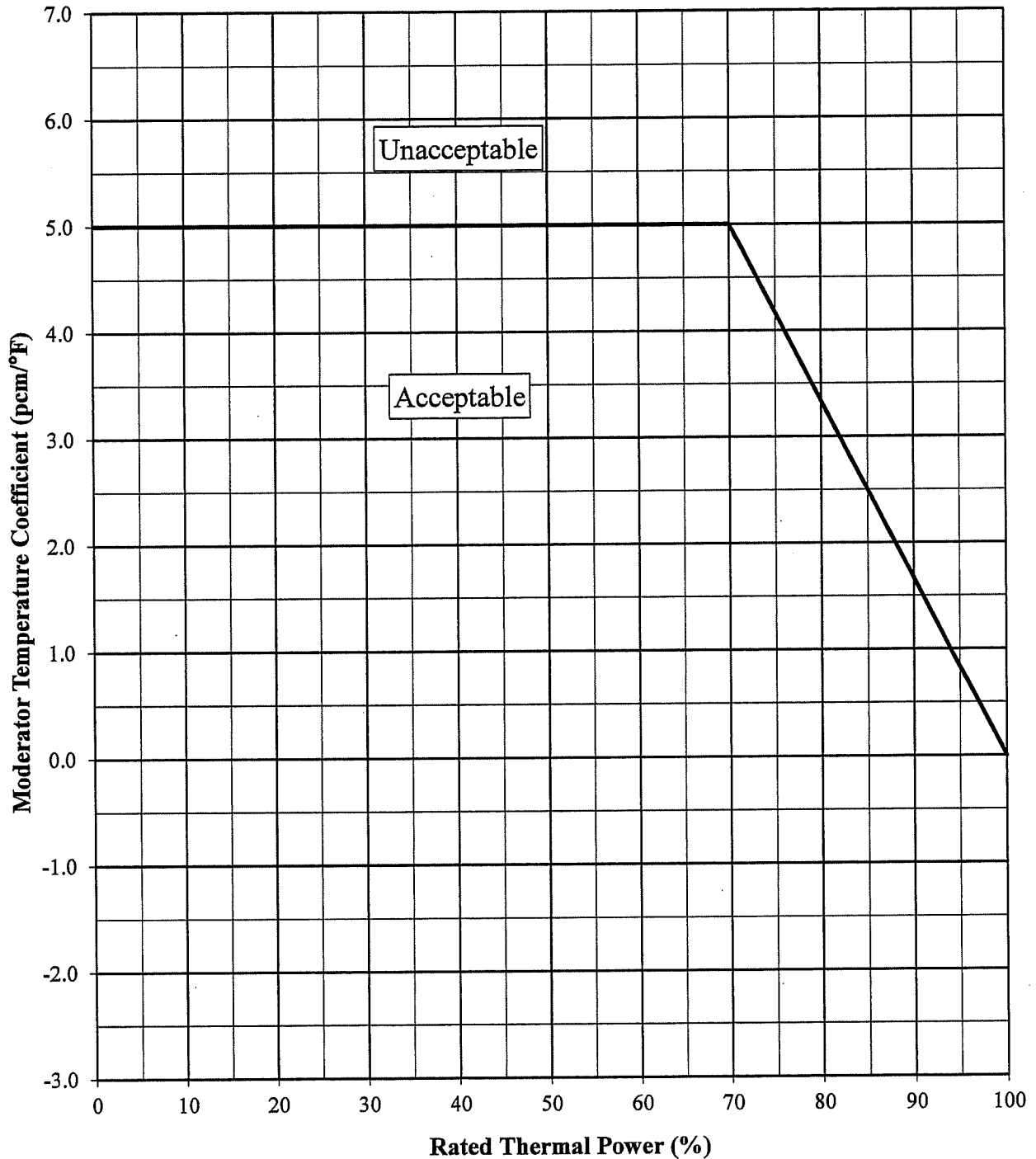


Figure 5

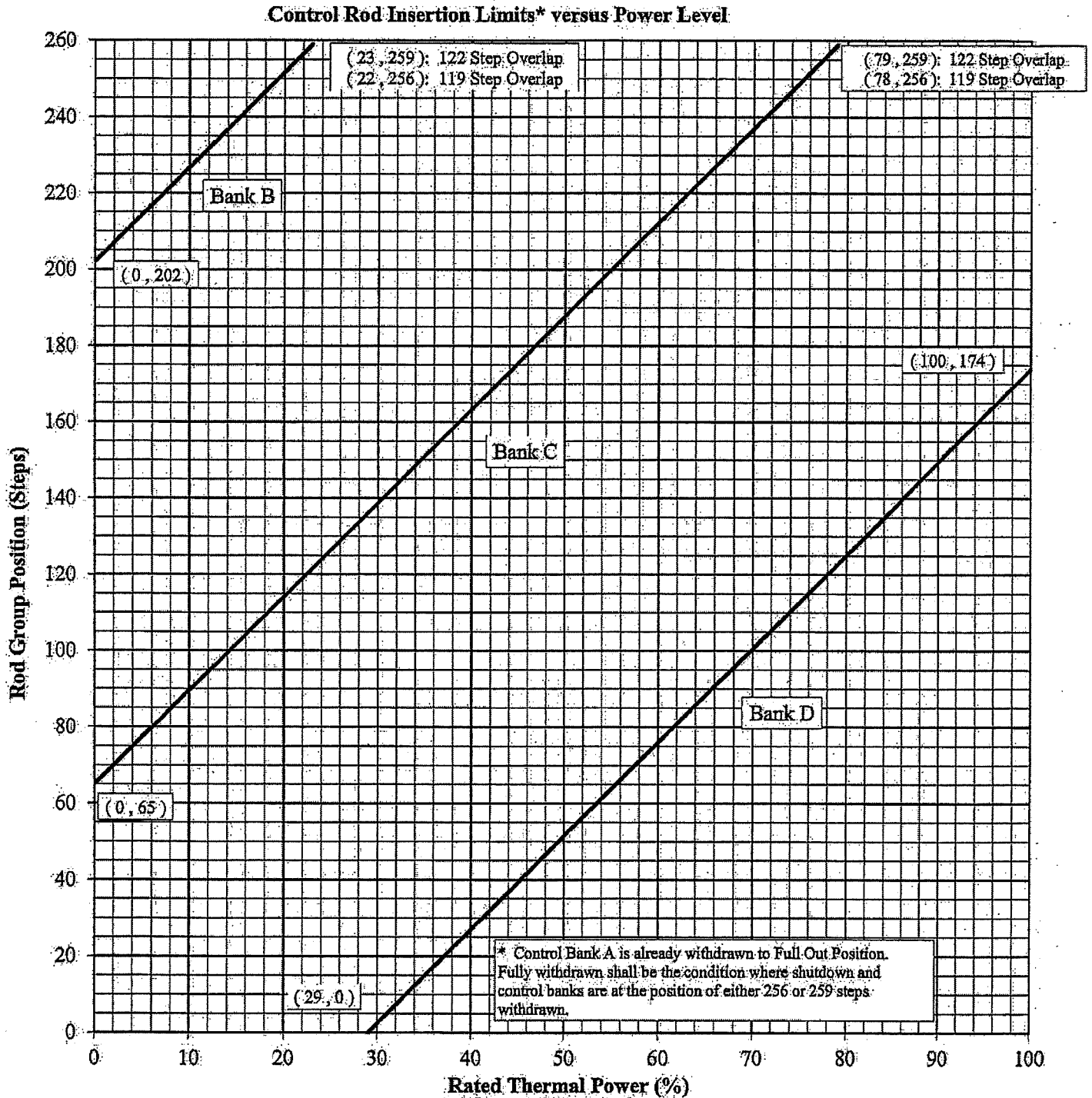


Figure 6

AFD Limits versus Power Level

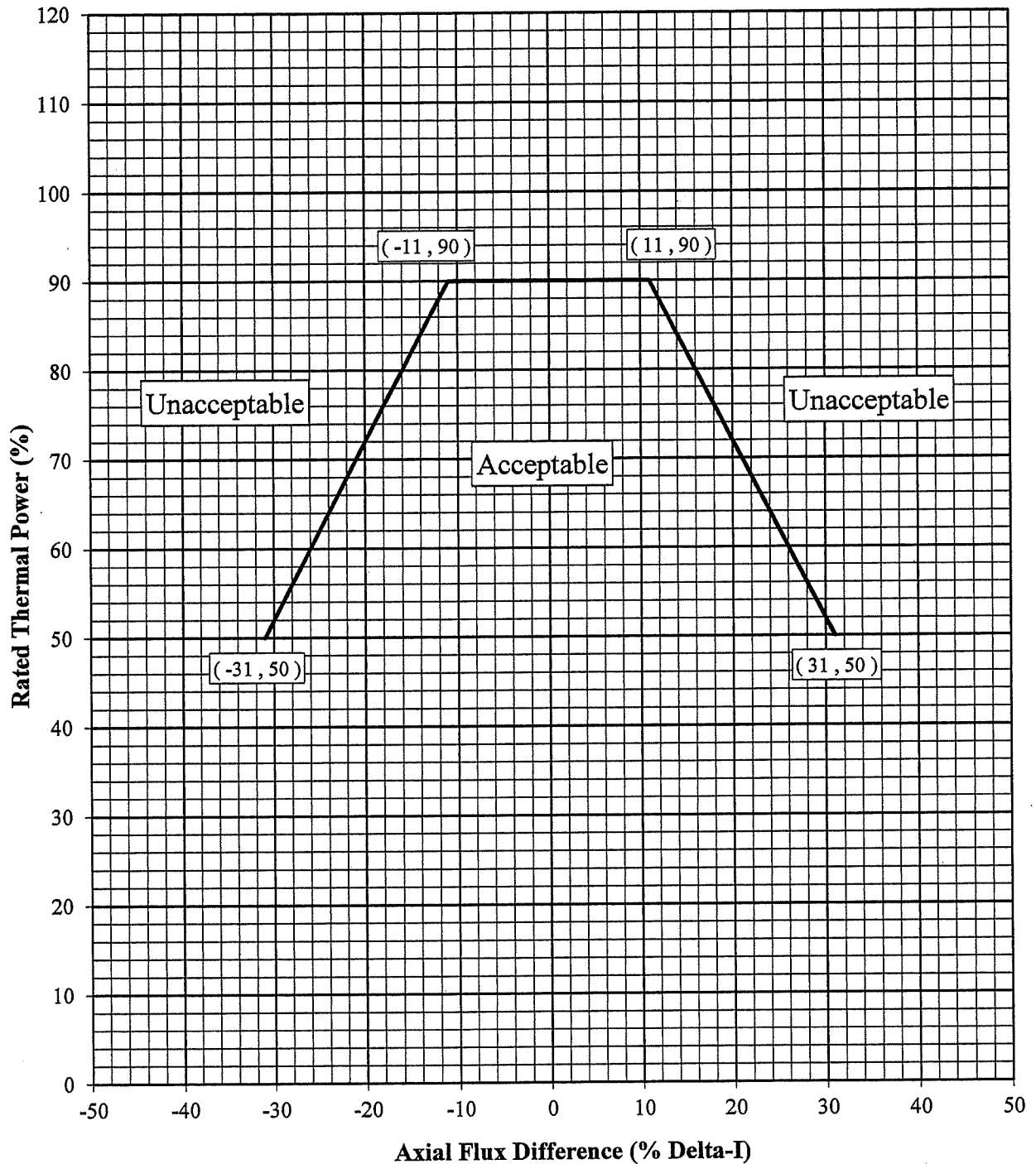
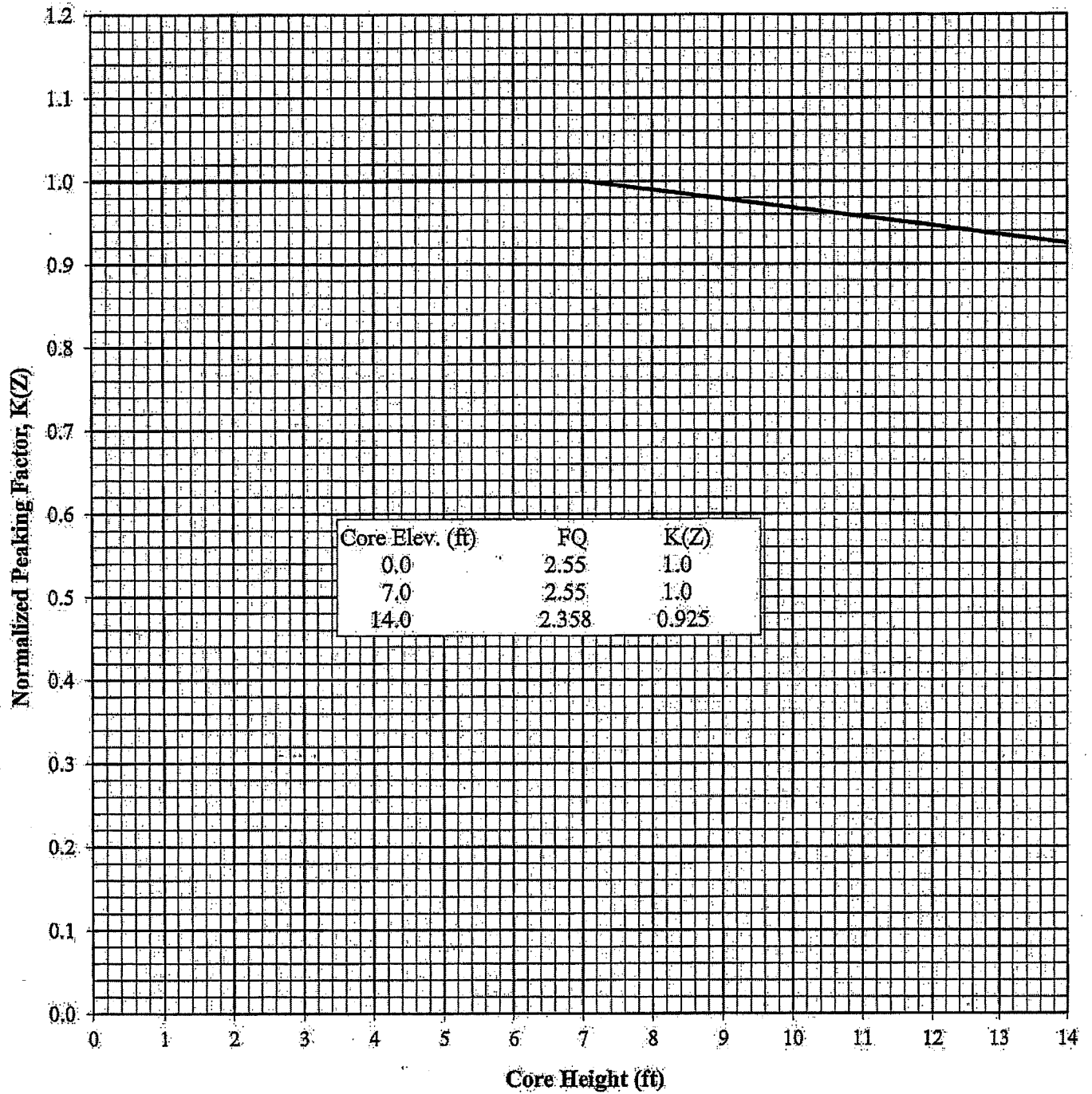


Figure 7

$K(Z)$ - Normalized FQ(Z) versus Core Height



**Table 1 (Part 1 of 2)
Unrodded F_{xy} for Each Core Height
for Cycle Burnups Less Than 10000 MWD/MTU**

Core Height (Ft.)	Axial Point	Unrodded F _{xy}	Core Height (Ft.)	Axial Point	Unrodded F _{xy}
14.0	1	7.129	6.8	37	1.979
13.8	2	5.560	6.6	38	2.046
13.6	3	3.993	6.4	39	2.017
13.4	4	2.657	6.2	40	1.943
13.2	5	2.474	6.0	41	1.906
13.0	6	2.191	5.8	42	1.939
12.8	7	2.096	5.6	43	1.948
12.6	8	2.097	5.4	44	1.948
12.4	9	2.049	5.2	45	1.993
12.2	10	1.987	5.0	46	2.065
12.0	11	1.948	4.8	47	2.084
11.8	12	1.960	4.6	48	2.027
11.6	13	2.005	4.4	49	1.959
11.4	14	1.992	4.2	50	1.975
11.2	15	1.944	4.0	51	1.977
11.0	16	1.913	3.8	52	1.963
10.8	17	1.905	3.6	53	1.969
10.6	18	1.894	3.4	54	2.017
10.4	19	1.869	3.2	55	2.051
10.2	20	1.881	3.0	56	1.995
10.0	21	1.931	2.8	57	1.944
9.8	22	1.944	2.6	58	1.947
9.6	23	1.881	2.4	59	1.951
9.4	24	1.859	2.2	60	1.922
9.2	25	1.863	2.0	61	1.897
9.0	26	1.865	1.8	62	1.915
8.8	27	1.872	1.6	63	1.916
8.6	28	1.893	1.4	64	1.824
8.4	29	1.959	1.2	65	1.750
8.2	30	2.023	1.0	66	1.780
8.0	31	1.987	0.8	67	2.068
7.8	32	1.936	0.6	68	2.763
7.6	33	1.931	0.4	69	3.936
7.4	34	1.941	0.2	70	5.599
7.2	35	1.936	0.0	71	8.325
7.0	36	1.925			

Table 1 (Part 2 of 2)
Unrodded Fxy for Each Core Height
for Cycle Burnups Greater Than or Equal to 10000 MWD/MTU

Core Height (Ft.)	Axial Point	Unrodded Fxy	Core Height (Ft.)	Axial Point	Unrodded Fxy
14.00	1	6.389	6.80	37	2.208
13.80	2	5.096	6.60	38	2.253
13.60	3	3.803	6.40	39	2.219
13.40	4	2.698	6.20	40	2.152
13.20	5	2.550	6.00	41	2.114
13.00	6	2.273	5.80	42	2.105
12.80	7	2.120	5.60	43	2.093
12.60	8	2.061	5.40	44	2.077
12.40	9	1.999	5.20	45	2.097
12.20	10	1.977	5.00	46	2.137
12.00	11	1.976	4.80	47	2.135
11.80	12	2.016	4.60	48	2.073
11.60	13	2.073	4.40	49	2.023
11.40	14	2.069	4.20	50	2.018
11.20	15	2.023	4.00	51	2.005
11.00	16	2.004	3.80	52	1.988
10.80	17	2.015	3.60	53	1.989
10.60	18	2.019	3.40	54	2.029
10.40	19	2.021	3.20	55	2.056
10.20	20	2.056	3.00	56	1.998
10.00	21	2.116	2.80	57	1.943
9.80	22	2.144	2.60	58	1.927
9.60	23	2.104	2.40	59	1.899
9.40	24	2.068	2.20	60	1.872
9.20	25	2.084	2.00	61	1.894
9.00	26	2.096	1.80	62	1.941
8.80	27	2.103	1.60	63	1.971
8.60	28	2.120	1.40	64	1.950
8.40	29	2.174	1.20	65	1.963
8.20	30	2.222	1.00	66	2.074
8.00	31	2.180	0.80	67	2.444
7.80	32	2.138	0.60	68	3.182
7.60	33	2.138	0.40	69	4.307
7.40	34	2.149	0.20	70	5.855
7.20	35	2.158	0.00	71	8.547
7.00	36	2.164			