

50-250(251)

NRC DISTRIBUTION FOR PART 50 DOCKET MATERIAL

FILE NUMBER

TO:
Mr. George Lear

FROM:
Florida Power & Light Company
Miami, Florida
Robert E. Uhrig

DATE OF DOCUMENT
1/3/78

DATE RECEIVED
1/11/78

LETTER
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DESCRIPTION

REACTOR VESSEL OVERPRESSURIZATION
DISTRIBUTION PER G. ZECH 10-21-76

(1-P)

PLANT NAME: Turkey Point Units 3 & 4
RJL 1/11/78

ENCLOSURE

Att. 1) Procedure for Evaluation of Maximum
Setpoint Overshoot Heat Input
Transients-

Att. 2) Supplement to the July 1977 Report -
Pressure Mitigating Systems, Transient
Analysis Results -

(2-P)+(1/4")

3 cys. OVERPRESSURE MITIGATING
RPT. TO THOSE INDICATED
ALL OTHER RECEIVE LTR
AND ATTACHMENT

SAFETY		FOR ACTION/INFORMATION	
BRANCH CHIEF:			
LIC. ASST.:	7 cys LTR	} LEAR	
PROJECT MANAGER:	w/1 cy RPT.		

INTERNAL DISTRIBUTION			
<input checked="" type="checkbox"/>	REG FILE w/RPT.		
<input type="checkbox"/>	NRC-PDR		
<input type="checkbox"/>	I & E (2)		
<input type="checkbox"/>	OELD		
<input type="checkbox"/>	GOSSICK & STAFF		
<input type="checkbox"/>	BOSNAK		
<input type="checkbox"/>	PAWLICKI		
<input type="checkbox"/>	NOVAK		
<input type="checkbox"/>	EISENHUT		
<input type="checkbox"/>	SHAO		
<input type="checkbox"/>	BAER		
<input type="checkbox"/>	BUTLER		
<input type="checkbox"/>	ZECH		

EXTERNAL DISTRIBUTION		CONTROL NUMBER	
LPDR:	w/RPT MIAMI FL 4		
TIC:			
NSIC:			
ACRS	16 cys HOLDING/SENT - 5A CAT B		

780110142
MAZ

REGULATORY DOCKET FILE COPY



FLORIDA POWER & LIGHT COMPANY

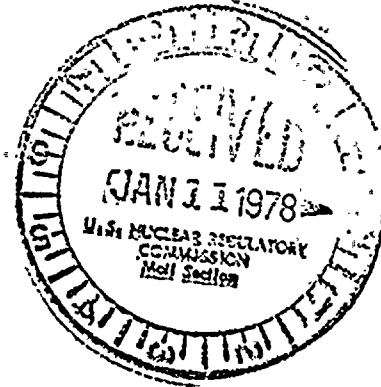
January 3, 1978

L-78-4

Office of Nuclear Reactor Regulation
Attention: Mr. George Lear, Chief
Operating Reactors Branch #3
Division of Operating Reactors
U. S. Nuclear Regulatory Commission
Washington, D.C. 20555

Dear Mr. Lear:

Re: Turkey Point Units 3 & 4
Docket Nos. 50-250 and 50-251
Overpressure Protection



In our October 18, 1977 (L-77-324) submittal on the Overpressure Mitigating System (OMS) for Turkey Point, setpoint selection for the pressurizer power operated relief valves (PORV's) was based upon a July 1977 Westinghouse analysis. The maximum setpoint overshoot for heat input transients was evaluated with a PORV setpoint of 500 psig, the only setpoint considered in the Westinghouse July analysis. A supplement to the July report has been prepared which permits us to evaluate the maximum setpoint overshoot with a PORV setpoint of 415 psig, the setpoint selected for Turkey Point for reactor coolant temperatures below 300 F. The supplement is attached.

The chosen PORV setpoint of 415 psig is 85 psi below the minimum NDT pressure of 500 psig. The maximum setpoint overshoot for heat input transients evaluated with a PORV setpoint of 415 psig increased from 14 psi at 100 F to 57 psi at 250 F. This is less than the margin to the minimum NDT pressure provided by the selected setpoint and confirms that the setpoint is conservative for heat input transients. The procedure for evaluating the setpoint overshoot is attached.

Very truly yours,

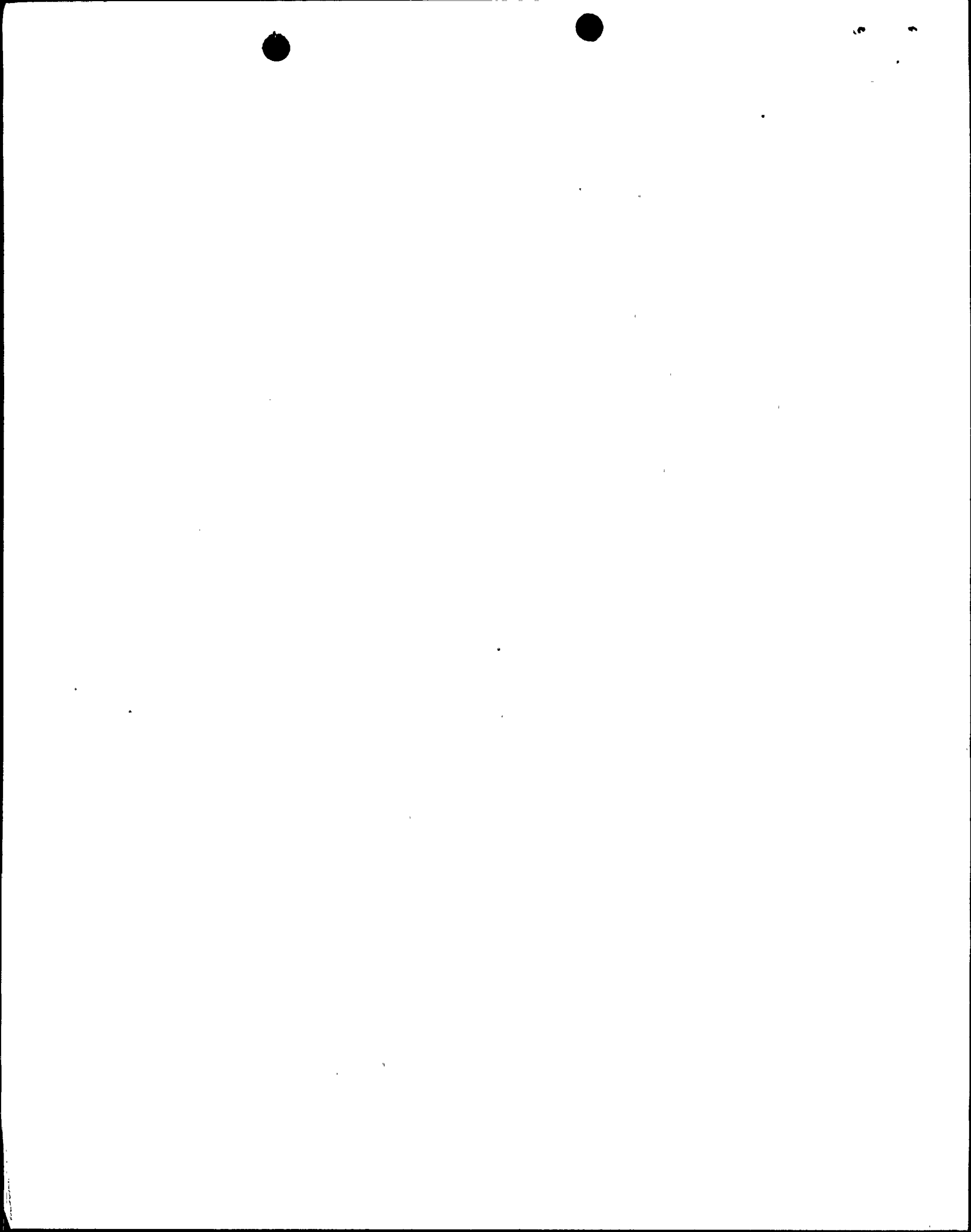
Robert E. Uhrig
Vice President

REU/MAS/lah

Attachments (2)

cc: James P. O'Reilly, Region II
Robert Lowenstein, Esquire

780110142



PROCEDURE FOR EVALUATION OF MAXIMUM SETPOINT OVERSHOOT
HEAT INPUT TRANSIENTS

Turkey Point Units 3 and 4 parameters

RCS Volume 9343 ft.³ (FSAR Table 4.1-1)
 S.G. Area 44,430 ft.² (FSAR Table 4.1-4)
 PORV opening time 2.0 sec. (Pre-op test 1000.16)
 Selected PORV setpoint 415 psig (below 300 F RCS temp.)

Figure and example numbers refer to the September 1977 supplement to the July 1977 report provided by Westinghouse.

- (1) Evaluate the effect of S.G. UA on pressure overshoot (ΔP) (Figures 14 thru 20).

$$\frac{\text{Turkey Point S.G. Area}}{\text{Reference S.G. Area}} = \frac{44,430 \text{ ft.}^2}{58,000 \text{ ft.}^2} = .766$$

Turkey Point UA = .766 Reference UA

Relief valve setpoint 400 psig, 3 second opening time:

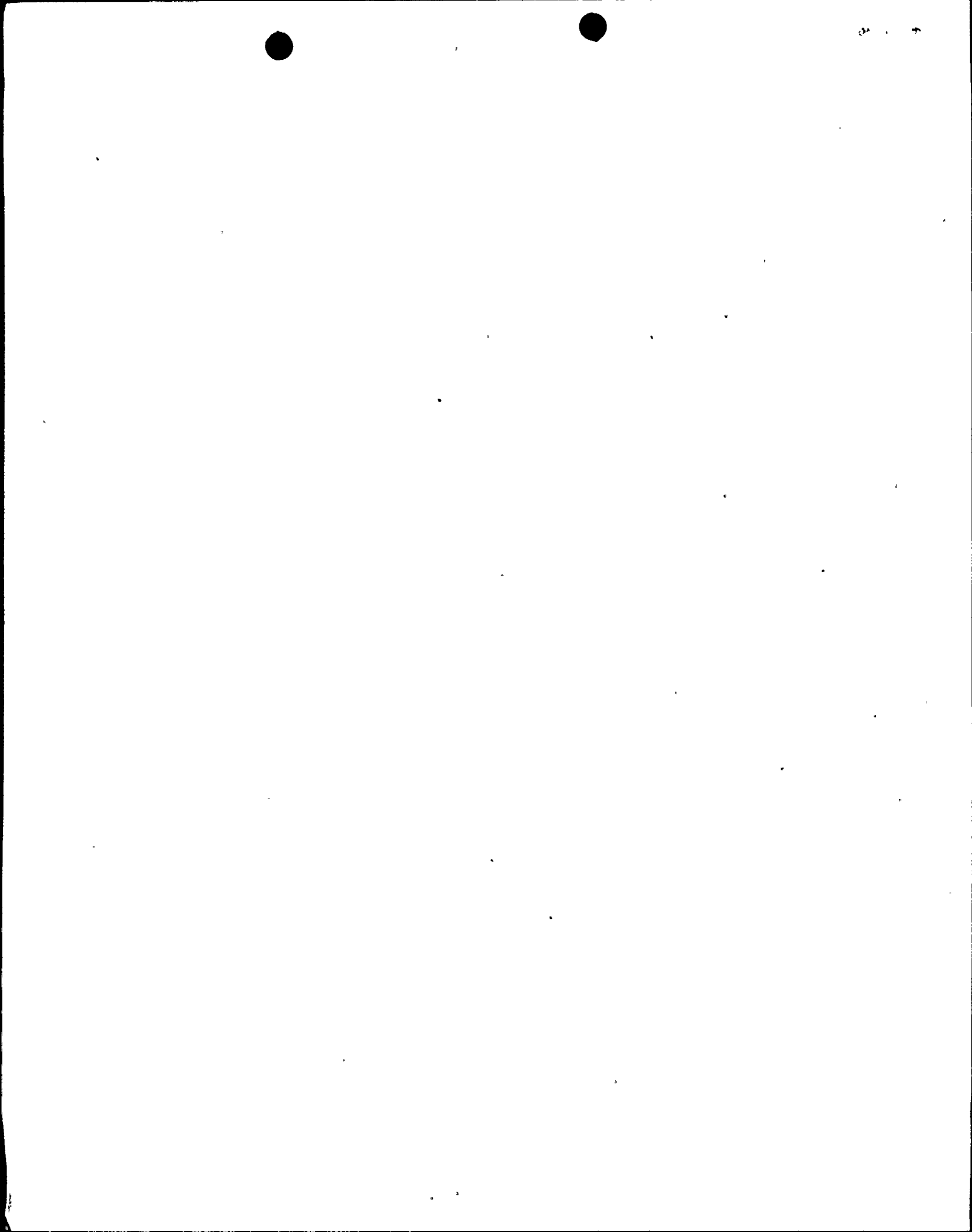
<u>Temp.</u>	<u>Figure 14³</u> <u>Vol. 6000 ft.³</u>	<u>Figure 15</u> <u>Vol. 13000 ft.³</u>
100°F	$\Delta P = 25 \text{ psi}$	$\Delta P = 16 \text{ psi}$
180°F	$\Delta P = 59 \text{ psi}$	$\Delta P = 51 \text{ psi}$
250°F	$\Delta P = 93 \text{ psi}$	$\Delta P = 72 \text{ psi}$

Relief valve setpoint 500 psig, 3 second opening time:

<u>Temp.</u>	<u>Figure 16³</u> <u>Vol. 6000 ft.³</u>	<u>Figure 17</u> <u>Vol. 13000 ft.³</u>
100°F	$\Delta P = 23 \text{ psi}$	$\Delta P = 21 \text{ psi}$
180°F	$\Delta P = 74 \text{ psi}$	$\Delta P = 53 \text{ psi}$
250°F	$\Delta P = 109 \text{ psi}$	$\Delta P = 91 \text{ psi}$

- (2) Evaluate the effect of RCS volume on pressure overshoot. By linear interpolation of results from (1) above (as in supplement example 4);
 RCS volume 9343 ft.³; 3 second opening time:

<u>Temp.</u>	<u>Setpoint 400 psig</u>	<u>Setpoint 500 psig</u>
100°F	$\Delta P = 21 \text{ psi}$	$\Delta P = 22 \text{ psi}$
180°F	$\Delta P = 55 \text{ psi}$	$\Delta P = 64 \text{ psi}$
250°F	$\Delta P = 83 \text{ psi}$	$\Delta P = 100 \text{ psi}$



- (3) Evaluate the effect of relief valve setpoint on pressure overshoot.
By linear interpolation of results from (2) above;
Relief valve setpoint 415 psig; RCS volume 9343 ft.³;
three second opening time:

<u>Temp.</u>	<u>Pressure Overshoot</u>
100°F	$\Delta P = 21$ psi
180°F	$\Delta P = 57$ psi
250°F	$\Delta P = 86$ psi

- (4) Evaluate the effect of valve opening time on pressure overshoot.
Figures 1 - 6 show pressure overshoot directly proportional to valve opening time.
Therefore, applying all Turkey Point parameters:

<u>Temp.</u>	<u>Pressure Overshoot</u>
100°F	$\Delta P = 14$ psi
180°F	$\Delta P = 38$ psi
250°F	$\Delta P = 57$ psi