

NRC DISTRIBUTION FOR PART 50 DOCKET MATERIAL

FILE NUMBER

TO: Mr V Stello

FROM: Florida Pwr & Light Co  
Miami, Fla  
R E Uhrig

DATE OF DOCUMENT  
2-2-77

DATE RECEIVED  
2-4-77

LETTER  
 ORIGINAL  
 COPY

NOTORIZED  
 UNCLASSIFIED

PROP

INPUT FORM

NUMBER OF COPIES RECEIVED

one signed

DESCRIPTION

Ltr re their 12-9-76 & 12-30-76 submittals  
.....trans the following:

1p

PLANT NAME: Turkey Pt 3 & 4

ENCLOSURE

ECCS Reevaluation Supplemental Information...  
submitted per NRC request.....

(40 cys encl rec'd)

11p **DO NOT REMOVE**

**ACKNOWLEDGED**

SAFETY

FOR ACTION/INFORMATION

ENVIRO

2-4-77

ehf

ASSIGNED AD:

BRANCH CHIEF:

PROJECT MANAGER:

LIC. ASST. :

*Leav (5)  
Elliott  
Parrish*

ASSIGNED AD:

BRANCH CHIEF:

PROJECT MANAGER:

LIC. ASST. :

INTERNAL DISTRIBUTION

<input checked="" type="checkbox"/> REG FILE	SYSTEMS SAFETY	PLANT SYSTEMS	SITE SAFETY &
<input checked="" type="checkbox"/> NRC PDR.	HEINEMAN	TEDESCO	ENVIRO ANALYSIS
<input checked="" type="checkbox"/> I-&-E (2)	SCHROEDER	BENAROYA	DENTON & MULLER
<input checked="" type="checkbox"/> OELD Ltr		LAINAS	
<input checked="" type="checkbox"/> GOSSICK & STAFF Ltr	ENGINEERING	IPPOLITO	ENVIRO TECH.
<input checked="" type="checkbox"/> MEPC-	MACARRY	KIRKWOOD	ERNST
<input checked="" type="checkbox"/> CASE Ltr	KNIGHT		BALLARD
HANAUER	SIHWEIL	OPERATING REACTORS	SPANGLER
HARLESS	PAWLICKI	STELLO	
			SITE TECH.
PROJECT MANAGEMENT	REACTOR SAFETY	OPERATING TECH.	GAMMILL
<input checked="" type="checkbox"/> BOYD Ltr	ROSS	EISENHUT	STEPP
P. COLLINS	NOVAK (3)	SHAO	HULMAN
HOUSTON	ROSZTOCZY	BAER	
PETERSON	CHECK	BUTLER	SITE ANALYSIS
MELTZ		GRIMES	VOLLMER
HELTEMES	AT & I		BUNCH
SKOVHOLT	SALTZMAN		J. COLLINS
	RUTBERG		KREGER

EXTERNAL DISTRIBUTION

CONTROL NUMBER

<input checked="" type="checkbox"/> LPDR: Miami, Fla	NAT. LAB:	BROOKHAVEN NAT. LAB.
<input checked="" type="checkbox"/> TIC:	REG V. IE	ULRIKSON (ORNL)
<input checked="" type="checkbox"/> NSIC:	LA PDR	
ASLB:	CONSULTANTS:	
<input checked="" type="checkbox"/> ACRS / 6 CYS HOLDING/SENT	As CAT B 2/4/77	

*1139*

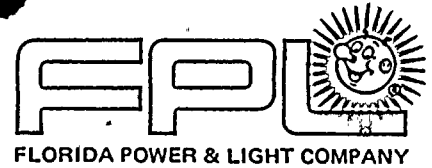
SECRET

.....

(Post Job type 1)

.....

.....



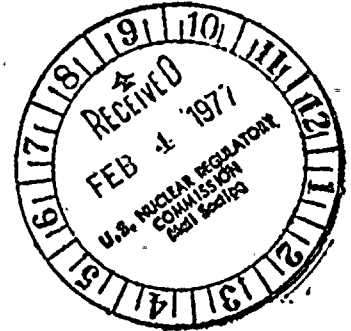
**Regulatory Docket File**

February 2, 1977  
L-77-38

Office of Nuclear Reactor Regulation  
Attention: Mr. Victor Stello, Director  
Division of Operating Reactors  
U. S. Nuclear Regulatory Commission  
Washington, D. C. 20555

Dear Mr. Stello:

Re: Turkey Point Units 3 and 4  
Docket Nos. 50-250 and 50-251  
ECCS Reevaluation  
Supplemental Information



ECCS information applicable to Turkey Point Units 3 and 4 has been submitted by Florida Power & Light Company in letters dated December 9, 1976 (L-76-419) and December 30, 1976 (L-76-438 and L-76-439).

Attached herewith is additional information requested by your staff.

Very truly yours,

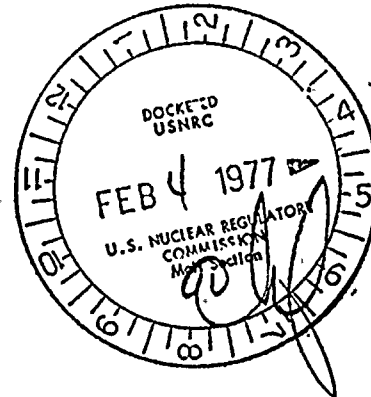
*Robert E. Uhrig*

Robert E. Uhrig  
Vice President

REU/MAS/cpc

Attachment

cc: Mr. Norman C. Moseley, Region II  
Robert Lowenstein, Esquire





ATTACHMENT

Re: Turkey Point Units 3 and 4  
Additional ECCS Information

QUESTION: Justify that the peak clad temperatures corresponding to different percentages of plugged steam generator tubes can be obtained by a linear interpolation, and submit a basis for the dependence of  $F_q$  on steam generator plugging.

ANSWER: Sensitivity studies were performed by Westinghouse in the early part of 1976 to determine, on a generic basis, the effect of plugged steam generator tubes on peak clad temperature (PCT) calculated during a LOCA. Three sets of runs were made, 1 each for a 2 loop plant, a 3 loop plant, and a 4 loop plant. The results were summarized and presented at an ACRS ECCS Subcommittee meeting. Plots of the results are shown in Figure 1. Figure 1 shows that the curves of  $\Delta PCT$  versus percent tube plugging are concave upward, which means that linearly interpolating between any two plugging levels results in a higher, or conservative, value of  $\Delta PCT$ .

Also, an answer given below to another question justifies the relationship between  $F_q$  and PCT (.01  $F_q$  per 10°F). Therefore, since " $F_q$  vs. PCT" is known, and "PCT vs. percent plugged tubes" is known, then the generic relationship between  $F_q$  and percent plugged tubes can be determined (Figure 2).



QUESTION: Submit the Westinghouse ECCS analyses which show that the decrease in accumulator water volume from 875 cubic feet to 825 cubic feet corresponds to 36°F rise in PCT.

ANSWER: Presented here is a discussion of the effect on the LOCA of a 50 cubic foot change in accumulator water volume.

To demonstrate the sensitivity of PCT to changes in accumulator water volume, specific analyses were made with accumulator water volumes of 825 and 875 cubic feet without changing other Turkey Point parameters. This resulted in a total change of PCT of 36°F because of the increase in downcomer water height and core inlet velocity.

The effectiveness of accumulators can be studied by inspecting Figures 1a and 1b, which are the downcomer water level and core water level plots, and Figures 2a and 2B, which are the core reflood water inlet velocity plots. The optimum accumulator water volume, based on previous studies, is generally a value that results in the downcomer being "almost" full when the accumulators empty.

From Figure 1a, when the accumulators empty, the downcomer height is about 9.5 feet for an initial water volume of 825 cubic feet per tank. Figure 1b indicates that increasing the initial water volume to 875 cubic feet per tank results in the downcomer being filled to 13.3 feet when the accumulators empty. This difference in accumulator performance during the accident results in a decrease in PCT from 2194°F for the core using 825 cubic feet initial accumulator water volume per tank to 2158°F for the case using 875 cubic feet.

The above delta change in peak clad temperature was obtained by explicitly modeling an increase in accumulator water volume for the Turkey Point units and can only be applied in the specified range. This response does not represent a generic sensitivity study.





QUESTION: Justify, by submitting the appropriate references to applicable sensitivity studies, the relationship between  $F_q$  and PCT ( $.01 F_q \rightarrow 10^\circ\text{F PCT}$ ).

ANSWER: The sensitivity in the ECCS analysis to changes in the total peaking factor has been determined from previous analysis performed by Westinghouse.

As presented in Reference 12 of the previous ECCS analysis (FPL letter L-76-419 of December 9, 1976) with core power equal to 2192 Mwt, it has been established that a conservative estimate of  $10^\circ\text{F}/0.01 F_q$  is appropriate for use on a generic basis as an interim measure.



FIGURE 1

Δ PEAK TAD TEMPERATURE °F

120  
100  
80  
60  
40  
20  
0

0 5 10

PERCENT STEAM GENERATOR PLUGGING

4-LOOP

2-LOOP

3-LOOP

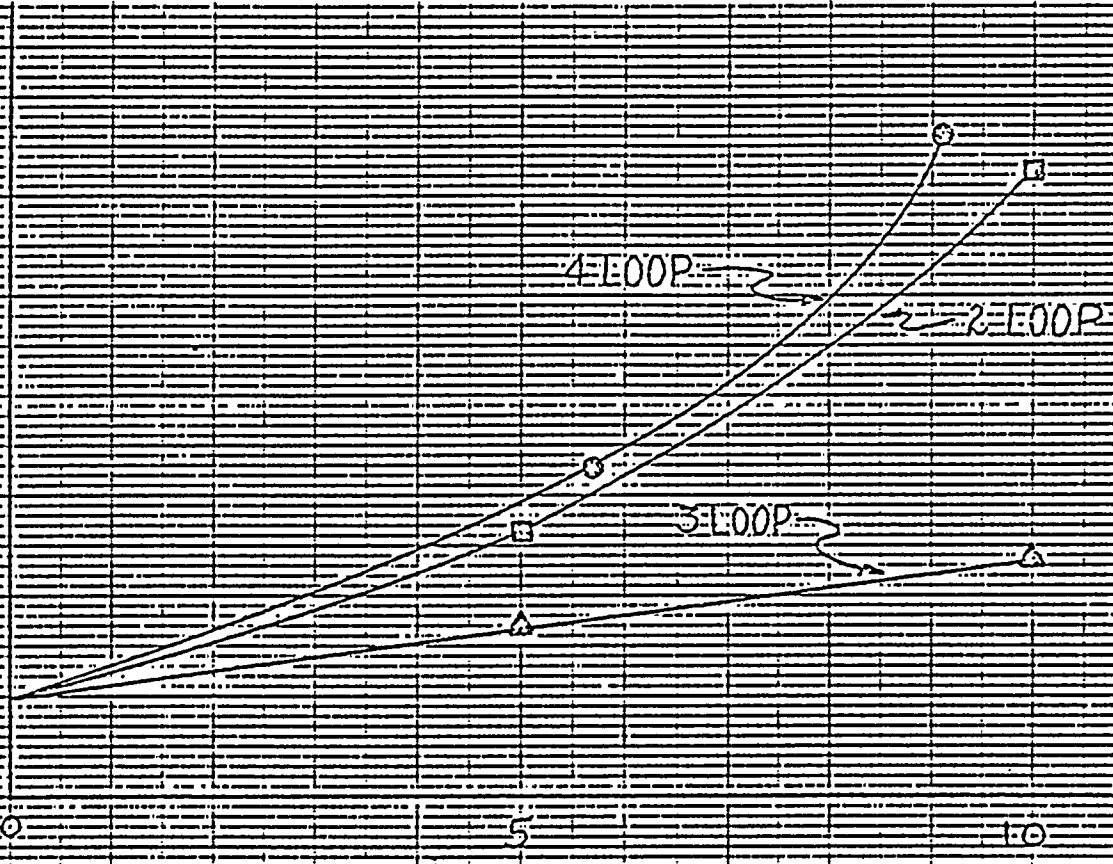
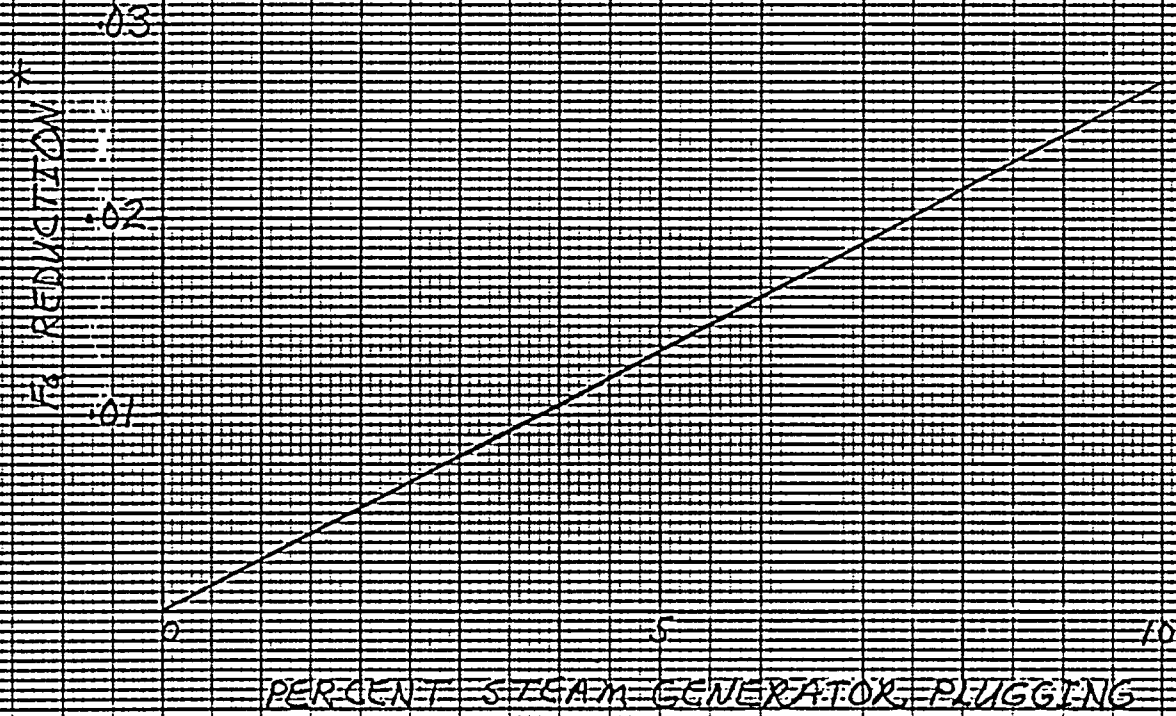




FIGURE 2



\* THE F<sub>0</sub> VALUES REPRESENT AMOUNT THAT MAX. ALLOWABLE F<sub>0</sub> MUST BE REDUCED IN ORDER TO ENSURE PGT LIMITS

TURKEY POINT (FPD) - 5 PERCENT UNIFORM - OCT75 MODEL  
DOUBLE ENDED GUILLOTINE - COLD LEG - CD=0.4  
WATER LEVEL(FT)

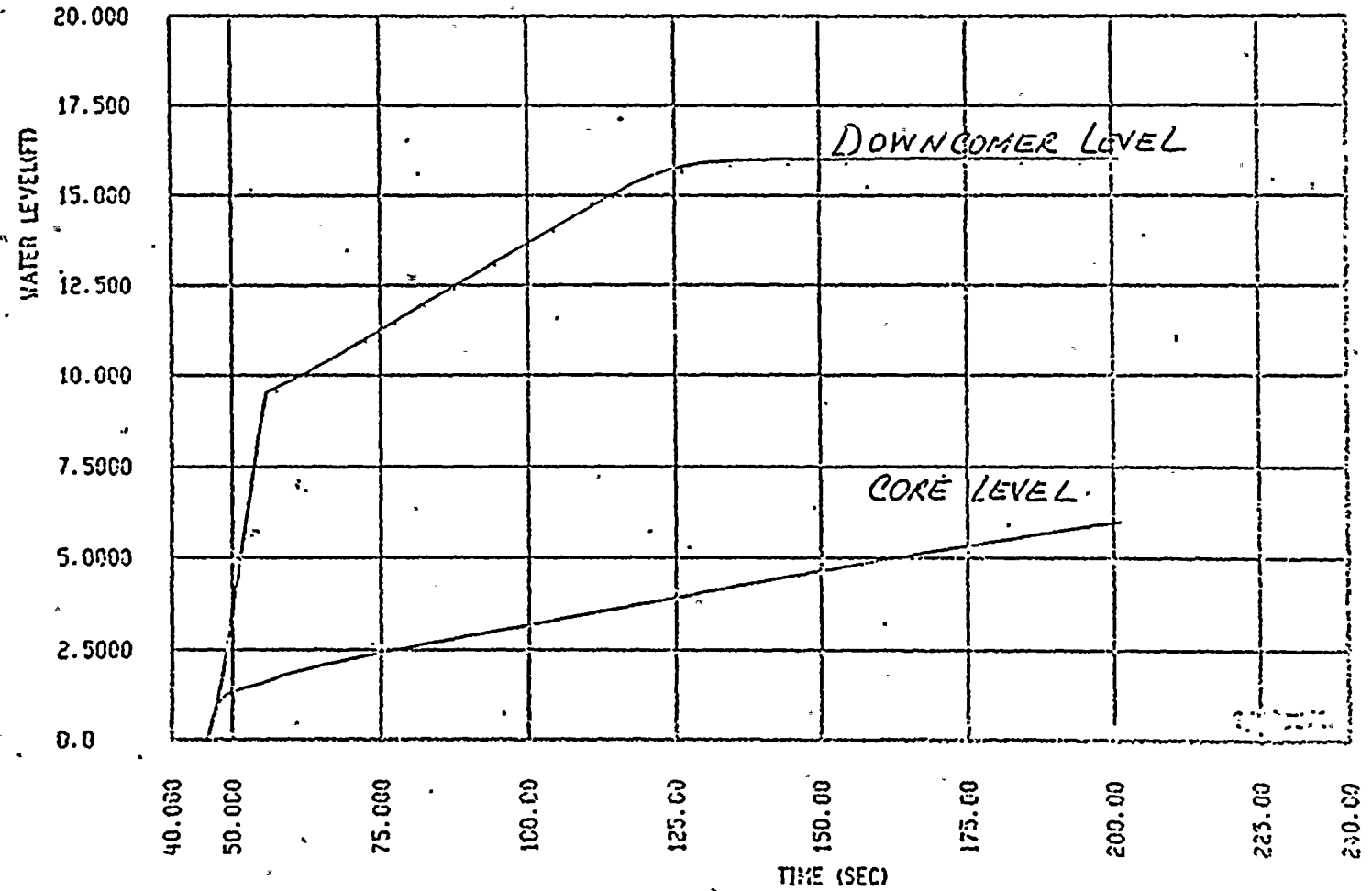


FIGURE 12 ACCUMULATOR WATER VOLUME, 825 FT<sup>3</sup> ...

TURKEY POINT (77) - 5 PERCENT URM - OCT75 MODEL  
DOUBLE ENDED GUILLOTINE - COLD LEG - CC=0.4  
WATER LEVEL (FT)

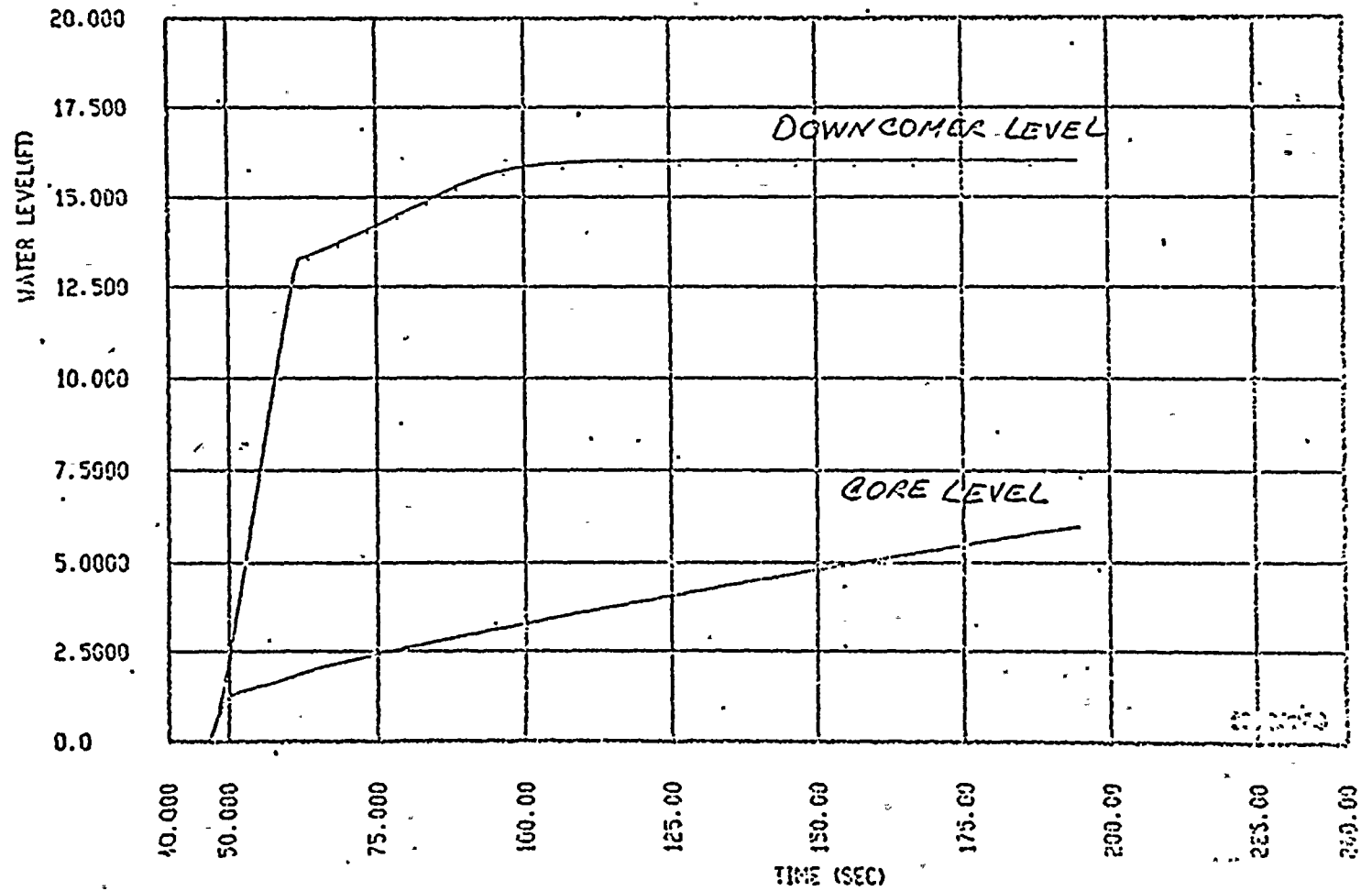


FIGURE 16 ACCUMULATOR WATER VOLUME, 875 FT<sup>3</sup>





TURKEY POINT (FPL) - 5 PERCENT UNRM - OCT75 MODEL  
DOUBLE ENDED GUILLOTINE - COLD LEG - CD=0.4  
FLOOD RATE(M/SEC)

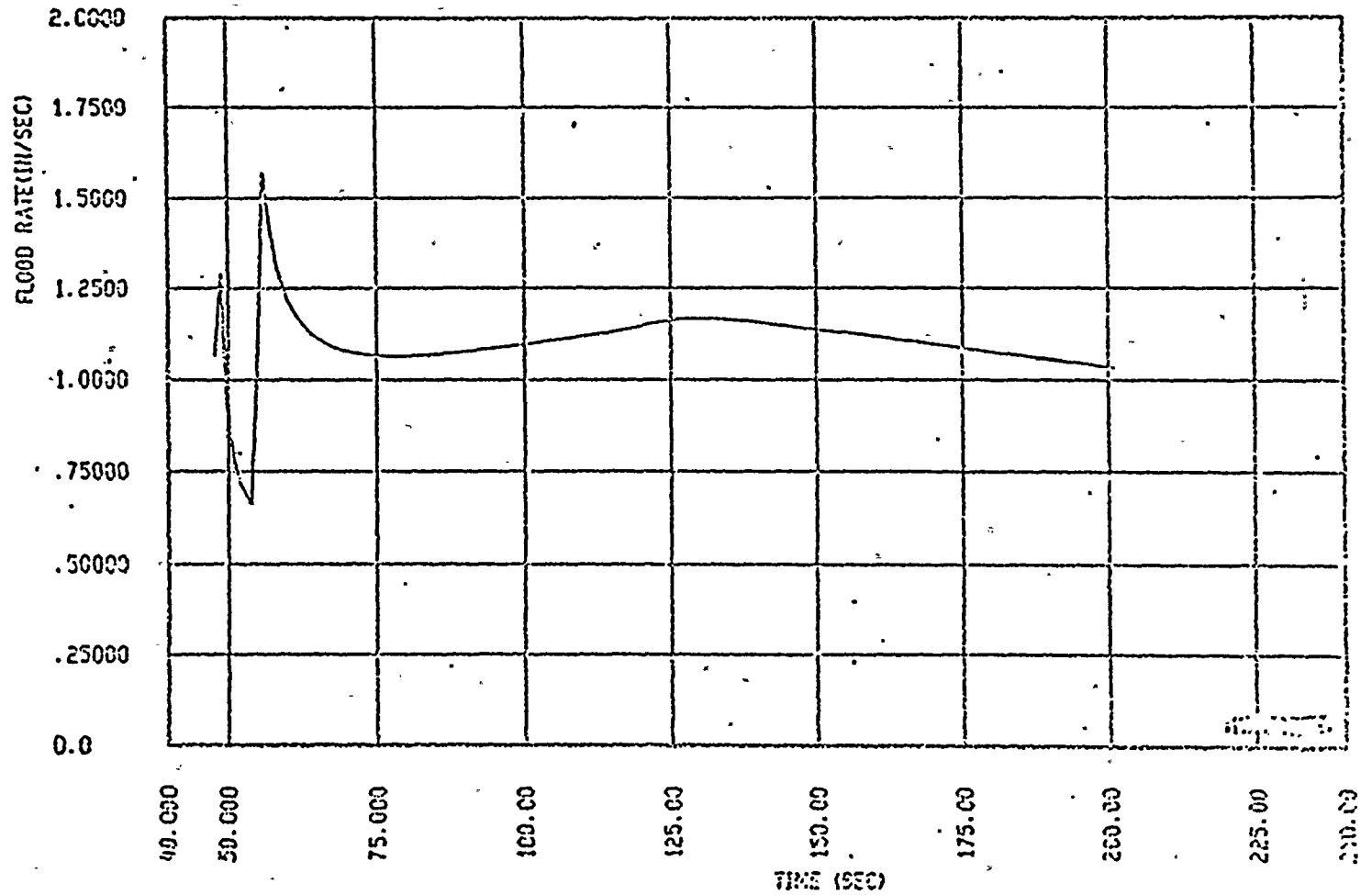


FIGURE 20 ACCUMULATOR WATER VOLUME, 8.25 FT<sup>3</sup>

TURKEY POINT (FPD) - 5 PERCENT UNFM - OCT75 MODEL  
DOUBLE ENDED CULLIGTINE - COLD LEG - CO-0.4  
FLOOD RATE (IN/SEC)

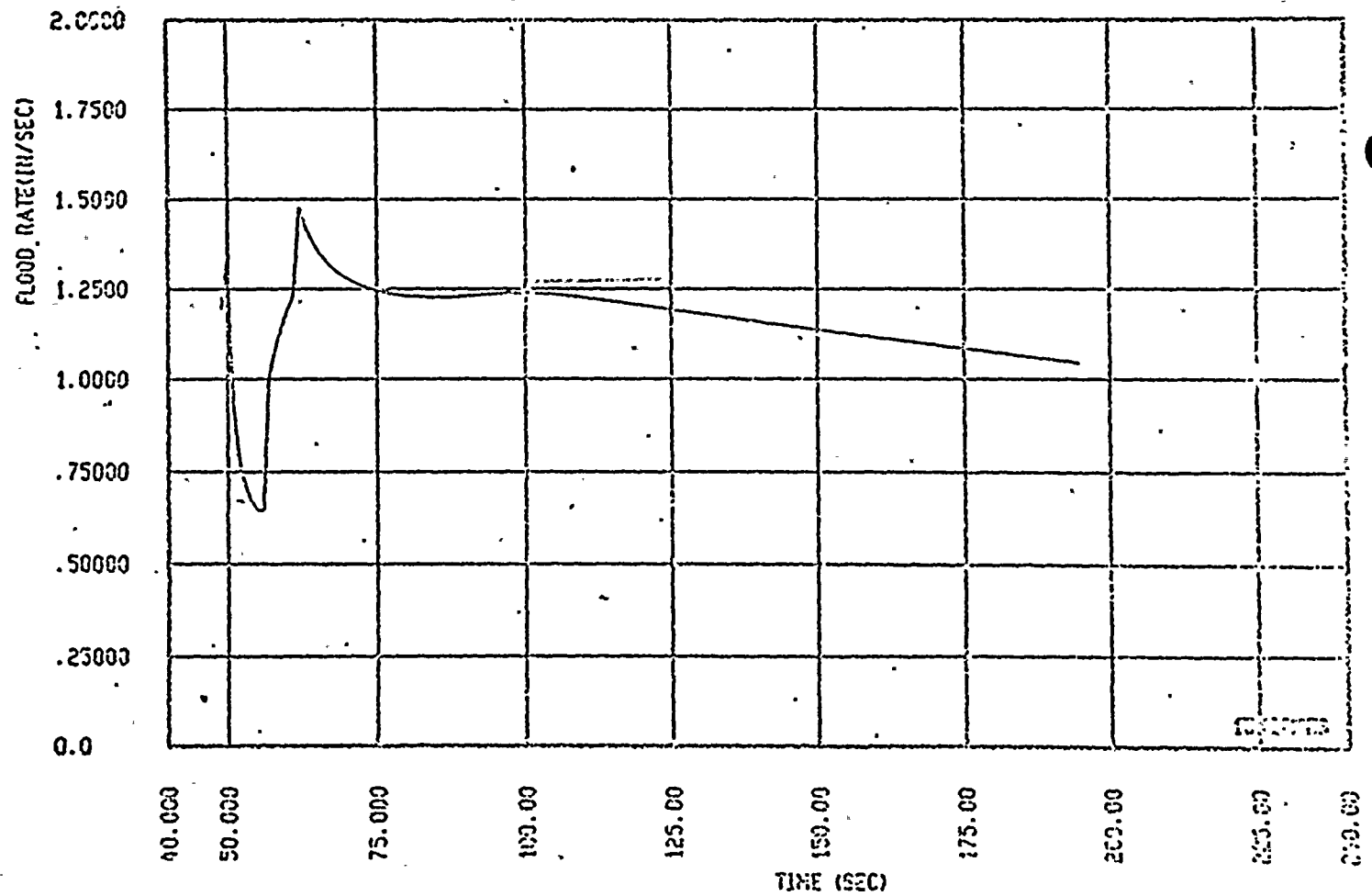


FIGURE 26 ACCUMULATOR WATER VOLUME, 875 FT<sup>3</sup>

