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FLORIDA POWER & LIGHT COMPANY

October 21, 1977 L-77-326



Office of Nuclear Reactor Regulation Attention: Mr. George Lear, Chief Operating Reactors Branch #3 Division of Operating Reactors U. S. Nuclear Regulatory Commission Washington, D. C. 20555

Dear Mr. Lear:

Re: Turkey Point Units 3 and 4 Docket Nos. 50-250 and 50-251 Reactor Vessel Material Information

Your letter of May 20, 1977 contained a Request for Information regarding the Reactor Vessel Material Surveillance Program at Turkey Point Units 3 and 4. On July 6, 1977 (L-77-211), we agreed to supply the information by October 22, 1977. The information you requested is attached.

Very truly yours,

Robert E. Uhrig

Vice President

REU/MAS/cpc

Attachment

cc: Mr. James P. O'Reilly, Region II Robert Lowenstein, Esquire

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TURKEY POINT UNIT NO. 3 REACTOR VESSEL MATERIAL SURVEILLANCE PROGRAM

- 1.) The estimated maximum fluence (E > 1 Mev) at the inner surface of the reactor vessel wall as of March 31, 1977 is 5.65×10^{18} n/cm².
- 2.) The effective full power years (EFPY) of operation accumulated as of March 31, 1977 is 2.87 EFPY.
- 3.) Fabrication of the reactor vessel was performed by the Babcock and Wilcox Company.
- 4.) a.) A sketch of the reactor vessel showing all materials in the beltline region is shown in Figure 1.
 - b.) Information on each of the welds in the beltline region is shown in Tables 1 through 4.
 - c.) Information on each of the forgings in the beltline region is shown in Tables 4 through 7.
- 5.) Information relative to weld and forging material included in the material surveillance program is shown in Tables 1 through 3 and 5 trough 7.

FIGURE 1

IDENTIFICATION AND LOCATION OF BELTLINE REGION MATERIAL IN THE TURKEY POINT UNIT NO. 3 REACTOR VESSEL



IDENTIFICATION OF REACTOR VESSEL TURKEY POINT UNIT NO. 3 REACTOR VESSEL BELTLINE REGION WELD MATERIAL

			Weld W	lire	Flu	IX			
Weld Location	Weld <u>Process</u>	Weld <u>Control No.</u>	Туре	<u>Heat No.</u>	Туре	Lot No.	Post Weld <u>Heat Treatment</u>		
Nozzle Shell to Inter. Shell	Submerged Arc	SA-1484	Mn Mo Ni	72442	Linde 80	8579	1100-1125°F-48 Hrs-FC		
Inter. Shell to Lower Shell	Submerged Arc	SA-1101	Mn Mo Ni	71249	Linde 80	8445	1100-1125°F-48 Hrs-FC		
Surveillance Weld	Submerged Arc	SA-1101	Mn Mo Ni	71249	Linde 80	8445	1125°F-10 1/4·Hrs-FC		

TABLE 2 CHEMICAL COMPOSITION OF VESSEL BELTLINE REGION WELD MATERIAL

	Weld Wire		Flux			Weight Percent							
Control No. SA-1484	<u>Type</u> Mn Mo Ni	<u>Heat No.</u> 72442	<u>Type</u> Linde 80	<u>Lot No.</u> 8579	<u>.08</u>	<u>P</u> .018	<u>5</u> .015	<u>Mn</u> 1.52	<u>Si</u> .42	<u>Mo</u> .39	<u>Ni</u> .64	<u>Cr</u> .06	<u>Cu</u> . 7
- SA-1101	Mn Mo Ni	71249	Linde 80	8445	.07	.021	.014	1.28	.52	.36	.57	.,17	.21
Surveillar	nce Weld				.076	.011	.018	1.26	.66	.42	.57	.14	.31

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TABLE 3 -

MECHANICAL PROPERTIES OF VESSEL BELTLINE REGION WELD MATERIAL

Weld Wire		<u> </u>		-T * Energy		RT*	Shelf				- •	
Туре	Heat No.	Туре	Lot No.	'NDT	at 10°F <u>ft-1b</u> ·	• <u>*</u>	Energy <u>ft-lb</u>	YS <u>ksi</u>	UTS <u>ksi</u>	Elong. <u>%</u>	RA <u>%</u>	
Mn Mo Ni	72442	Linde 80	8579	0	40,52,41	0			84.00	*****		
Mn Mo Ni	71249	Linde 80	8445	0	45,45,46	· 0	~~~~	68.63	84.26	28.5		
ce Weld				0	26,37,25 :	3	64.5	76.30	92.35	24.9	64.1	
1	<u>Weld</u> <u>Type</u> Mn Mo Ni Mn Mo Ni ce Weld	<u>Weld Wire</u> <u>Type Heat No.</u> Mn Mo Ni 72442 Mn Mo Ni 71249 ce Weld	<u>Weld Wire</u> <u>Type</u> <u>Heat No.</u> <u>Type</u> Mn Mo Ni 72442 Linde 80 Mn Mo Ni 71249 Linde 80 Mn Wo Ni	Weld WireFluxTypeHeat No.TypeLot No.Mn Mo Ni72442Linde 808579Mn Mo Ni71249Linde 808445Ice WeldIce WeldIce WeldIce Weld	Weld WireFluxT NDT*TypeHeat No.TypeLot No.°FMn Mo Ni72442Linde 8085790Mn Mo Ni71249Linde 8084450Ice Weld00	$\begin{tabular}{c c c c c c c c c c c c c c c c c c c $	$\begin{tabular}{c c c c c c c c c c c c c c c c c c c $	$\begin{tabular}{c c c c c c c c c c c c c c c c c c c $	Weld Wire Flux T_{NDT} Energy at 10°F RT_{NDT} Shelf Energy YS Type Heat No. Type Lot No. °F ft-1b °F ft-1b ksi Mn Mo Ni 72442 Linde 80 8579 0 40,52,41 0 Mn Mo Ni 71249 Linde 80 8445 0 45,45,46 0 68.63 ice Weld 0 26,37,25 3 64.5 76.30	Weld WireFluxT NDTT NDTEnergy at 10°FRT NDTShelf Energy $ft-1b$ VS UTS $ft-1b$ UTS ksi TypeHeat No.TypeLot No.°Fft-1b°Fft-1bksiksiMn Mo Ni72442Linde 808579040,52,41084.00Mn Mo Ni71249Linde 808445045,45,46068.6384.26Ice Weld026,37,25364.576.3092.35	Weld WireFluxT NDTT NDTEnergy at 10°FRT NDTShelf Energy ft-1bVS UTS KsiUTS KsiElong.TypeHeat No.TypeLot No.°F °Fft-1b°F ft-1bft-1bksiksi $\frac{1}{2}$ Mn Mo Ni72442Linde 808579040,52,41084.00Mn Mo Ni71249Linde 808445045,45,46068.6384.2628.5Ice Weld026,37,25364.576.3092.3524.9	Weld WireFluxT NDTT NDTEnergy at 10°FRT NDTShelf Energy $ft-1b$ UTS

*Estimated Per NRC Standard Review Plan Section 5.3.2.

TABLE 4

MAXIMUM END-OF-LIFE FLUENCE AT VESSEL INNER WALL LOCATIONS	
	Fluence
Shell Forging or Weld Location	<u>'n/cm²</u>
Nozzle Shell Forging	1.5×10^{18}
Nozzle Shell to Inter. Shell Circle Seam	0.5×10^{18}
Inter. Shell Forging	5.3×10^{19}
Inter. Shell to Lower Shell Circle Seam	5.3 x 10 ¹⁹
Lower Shell Forging	5.3 x 10 ¹⁹

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IDENTIFICATION OF VESSEL BELTLINE REGION SHELL FORGING MATERIAL

*			, Notoviol			•	
Component	Forging No.	<u>Heat No.</u>	Spec.	Supplier	<u>Austenitize</u>	Temper	Stress Relief
Nozzle Shell	122S146VA1	1225146	.A508 CL 2	Bethlehem	1550°F-11 HR-WQ	1220°F-22 HR-AC	1125°F-40 HR-FC
Inter. Shell	123P461VA1	123P461	A508 CL 2	Bethlehem	1550°F-13 HR-WQ	1210°F-18 HR-AC	1125°F-40 HR-FC
Lower Shell	123S266VA1	1235266	A508 CL 2	-Bethlehem	1550°F-13 HR-WQ	1210°F-18 HR-AC	1125°F-40 HR-FC
Surveillance M	laterial - Inter	. and Lower	Shell as Ab	ove Except St	ress Relieved by We	stinghouse	1125°F-10 1/4 HF

TABLE 6

CHEMICAL COMPOSITION OF VESSEL BELTLINE REGION SHELL FORGING MATERIAL

Forging No. 122S146VA1	<u>C</u> .22	<u>Mn</u> .64	<u>P</u> .010	<u>s</u> .013	<u>Si</u> .25	<u>Ni</u> .68	<u>Mo</u> .59	<u>Cr</u> .35	<u>v</u> . .03	<u>Co</u> .014	<u>Cu</u>
123P461VA1	.20	.65	.010	.010	.26	70	.62	.40	, Õ2	.011	.058*
123S266VA1	.20	.62	.010	.008	.20	.67	.59	38	.02	.016	.079*

*Analyses Performed by Westinghouse as Part of Surveillance Program

TABLE	7
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Forging No.		RT _{NDT} *	Shelf* Energy ft-lb	YS <u>ksi</u>	UTS <u>ksi</u>	Elong.	RA <u>%</u>	
122S146VA1	50.	50	98.5	64.0	85.5	26.0	69.95	-
123P461VA1	40	40	98.5	68.0	90.7	25.0	68.35	•
123S266VA1	30	30	117.5	58.1	83.4 .	28.0	71.40	•
123P461VA1	teo est	_ 40	94.0	64.4	96.2	26.1	70.35	Surveillance
123S266VA1 ·		30	96.0	57.4	92.6	26.1	70.70	Test Data

MECHANICAL PROPERTIES OF VESSEL BELTLINE REGION SHELL FORGING MATERIAL

*Estimated From Test Data in the Major Working Direction Per NRC Standard Review Plan Section 5.3.2

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TURKEY POINT UNIT NO. 4 REACTOR VESSEL

MATERIAL SURVEILLANCE PROGRAM

- 1.) The estimated maximum fluence (E > 1 Mev) of the inner surface of the reactor vessel as of March 31, 1977 is $4.79 \times 10^{18} \text{ n/cm}^2$.
- 2.) The effective full power years (EFPY) of operation accumulated as of March.31, 1977 is 2.43 EFPY.
- 3.) Fabrication of the reactor vessel was performed by the Babcock and Wilcox Co.
- 4.) a.) A sketch of the reactor vessel showing all materials in the beltline region is shown in Figure 1.
 - b.) Information on each of the welds in the beltline region is shown in Tables 1 through 4.
 - c.) Information on each of the forgings in the beltline region is shown in Tables 4 through 7.
- 5.) Information relative to weld and forging material included in the material surveillance program is shown in Tables 1 through 3 and 5 through 7.



IDENTIFICATION AND LOCATION OF BELTLINE REGION MATERIAL IN THE TURKEY POINT UNIT NO. 4 REACTOR VESSEL.



IDENTIFICATION OF REACTOR VESSEL TURKEY POINT UNIT NO.4 REACTOR VESSEL BELTLINE REGION WELD MATERIAL

	•	Weld Wire	Flux	. . .
Weld Location	Weld Weld Process <u>Control No.</u>	Type Heat N	o. Type Lot No.	Post Weld Heat Treatment
Nozzle Shell to Inter. Shell	Submerged Arc WF-70 Submerged Arc WF-67	Mn-Mo-Ni 72105 Mn-Mo-Ni 72442	Linde 80 8669 Linde 80 8669	1100-1150°F-48 HR 1100-1150°F-48 HR
Inter Shell to Lower Shell	Submerged Arc SA-1101	Mn-Mo-Ni 71249) Linde 80 8445	1100-1150°F-48 HR
Surveillance Weld	Submerged Arc SA-1094	Mn-Mo-Ni 71249) Linde 80 8457	1125°F-10 1/4 HR-FC

TABLE 2

CHEMICAL COMPOSITION OF VESSEL BELTLINE REGION WELD MATERIAL

	Weld Wire		Flux		Weight Percent								
Weld Control No. WF-70	<u>Type</u> Mn-Mo-Ni	<u>Heat No.</u> 72105	<u>Type</u> Linde 80	Lot No. 8669	<u>C</u> .070	<u>Mn</u> 1.60	<u>P</u> .014	<u>s</u> .011	<u>S1</u> .48	<u>N1</u> .46	<u>Mo</u> .40	<u>Cr</u>	<u>Cu</u> .27
WF-67	Mn-Mo-Ni	72442	Linde 80	8669	.064	1.49	.014	.017	.54 ;	.57	.41	.02	.2
SA-1101	Mn-Mo-Ni	71249	Linde 80	8445	.070	1.28	.021	.014	.52	.57	.36	.17	.21
SA-1094		71249	Linde 80	8457	.070	1.42	.020	.016	.51	.55	.49	.16	.23
Surveillan	ce Weld				.098	1.44	.014	.011	.50	.60	.36	.14	.30

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MECHANICAL PROPERTIES OF VESSEL BELTLINE REGION WELD MATERIAL

Mald	Weld Wire		F1	Flux T		T _{NDT} * Energy		Shelf	VC	UTC	Flong	D٨
Control No.	Туре .	<u>Heat No.</u>	Туре	<u>Lot No.</u>	۹DI F	ft-lbs	°F	ft-1b	ksi	<u>ksi</u>	<u><u>%</u></u>	кн <u>%</u>
WF-70	Mn-Mo-Ni	72105	Linde 80	8669	0	39,35,44	0		69.0	85.5	25,8	64.7
WF-67	Mn-Mo-Ni	72442	Linde 80	8669	0	29,35,30	0		64.0	81.5	31.3	65.8
SA-1101	Mn-Mo-Ni	71249	Linde 80.	8445	0	45,45,46	0	· 	68.6	84.3	28.5	معا هم فط
SA-1094	Mn-Mo-Ni	71249	Linde 80	8457 ·	0	38,34,52	0		72.5	86.0	26.7	65.1
Surveilla	nce Weld				0	29,39,36	0	66 ·	70.2 '	91 . 3	23.8	64.7

*Estimated Per NRC Standard Review Plan Section 5.3.2

TABLE 4

MAXIMUM END-OF-LIFE FLUENCE AT VESSEL INNER WA	LL LOCATIONS
· · ·	Fluence
Shell Forging or Weld Locations	n/cm ²
Nozzle Shell Forging	9.5 x 10 ¹⁸
Nozzle Shell to Inter. Shell Circle Seam	9.5 x 10 ¹⁸
Inter. Shell Forging	6.3 x 10 ¹⁹
Inter. Shell to Lower Shell Circle Seam	6.3×10^{19}
Lower Shell Forging	6.3 x 10 ¹⁹

'IDENTIFICATION OF VESSEL BELTLINE REGION SHELL FORGING MATERIAL

	•			Supplier Bethlehem	Heat Treatment			
<u>Component</u> Nozzle Shell	Forging No. 124S309VA1	<u>Heat No.</u> 124S309	Material <u>Spec.</u> A508 CL 2		<u>Austenitize</u> 1550°F-15 HR-WQ	<u>Temper</u> 1220°F-22 HR-FC	Stress Relief 1125°F-40 HR-FC	
Inter. Shell	123P481VA1	123P481	A508 CL 2	Bethlehem	1550°F-10 1/4HR-WQ	1210°F-18 HR-AC	1125°F-40 HR-FC	
Lower Shell	12S180VA1	1225180	A508 CL 2	Bethlehem	1550°F-10 1/2 HR-WQ	1200°F-18 HR-FC	1125°F-40 HR-FC	
Surveillance M	1125°F-10 1/2 HR-FC							

TABLE 6

CHEMICAL COMPOSITION OF VESSEL BELTLINE REGION SHELL FORGING MATERIAL

	·······	Weight Percent									-
Forging No.	<u><u> </u></u>	<u>Mn</u>	<u>P</u>	<u>s</u>	Si	<u>Ni</u>	Mo	<u>Cr</u>	<u>v</u>	<u>Co</u>	<u>Cu</u> `
124S309VA1	.20	.60	.010	.012	.27	.70	.57	.33	.02	.008	
123P481VA1	.21	.65	.010	.011	.25	.69	.59	· .33	. 02	.011	•••••
122S180VA1	.22	.60	.010	.009	.23	.74	.60	.34	.02	.013	
123P481VA1*	.22	.67	.010	.009	. 20 [*]	.71	.56	.33	.002	.017	.054
122S180VA1*	· .21	.67	.011	.009	.23	70	.56	.31	.001	.015	.056

*Surveillance Material Analysis Performed by Westinghouse.

Forging No.	T _{NDT} <u>°F</u>	RT _{NDT} *	Shelf* Energy <u>ft-lb</u>	YS <u>ksi</u>	UTS <u>ksi</u>	Elong. <u>%</u>	RA <u>%</u>	
124S309VA1	40	• 40	101	66.1	89.5	26.2	69.3	,
123P481VA1	50	50	93	71.0	93.2	25.0	67.2	
122S180VA1	40	40	97	72.2	92.7	24.0	66.9	
123P481VA1		50	88	68.5	90.1	25.4	68.1	Surveillance
122S180VA1		40	86	70.8	91.5	24.2	67.8	Test Data

*Estimated From Test Data in the Major Working Direction Per NRC Standard Review Plan Section 5.3.2

TABLE 7

MECHANICAL PROPERTIES OF VESSEL BELTLINE REGION SHELL FORGING MATERIAL