

NRC DISTRIBUTION FOR PART 50 DOCKET MATERIAL

TO: V. STELLO, JR.

FROM: FLORDIA POWER & LIGHT CO.  
MIAMI, FLORDIA  
R.E. UHRIG

DATE OF DOCUMENT  
1/3/77  
DATE RECEIVED  
1/10/77

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DESCRIPTION  
LTR. RE. THEIR 12/30/76 SUBMITTAL.....

PLANT NAME: TURKEY PT. # 3 & 4

ENCLOSURE  
RESULTS OF THE REVISED ECCS CALCULATIONS.....  
SUPPLEMENTAL INFORMATION.....

( 40 CYS. RECEIVED)  
( 20 PAGES)

**ACKNOWLEDGED**

**DO NOT REMOVE**

SAFETY	FOR ACTION/INFORMATION	ENVIRO	SAB 1/11/77
ASSIGNED AD:		ASSIGNED AD:	
BRANCH CHIEF:	LEAR (2)	BRANCH CHIEF:	
PROJECT MANAGER:		PROJECT MANAGER:	
LIC. ASST. :	PARRISH	LIC. ASST.:	

INTERNAL DISTRIBUTION			
<input checked="" type="checkbox"/> REG FILE	SYSTEMS SAFETY	PLANT SYSTEMS	SITE SAFETY &.....
<input checked="" type="checkbox"/> NRC PDR	HEINEMAN	TEDESCO	ENVIRO ANALYSIS
<input checked="" type="checkbox"/> I & E (2)	SCHROEDER	BENAROYA	DENTON & MULLER
<input checked="" type="checkbox"/> OELD		LAINAS	
<input checked="" type="checkbox"/> GOSSICK & STAFF	ENGINEERING	IPPOLITO	ENVIRO TECH
<input checked="" type="checkbox"/> MIPC	MACARRY	KIRKWOOD	ERNST
<input checked="" type="checkbox"/> CASE	KUIGHT		BALLARD
HANAUER	SIHWEIL	OPERATING REACTORS	SPANGLER
HARLESS	PAWLICKI	STELLO	
<input checked="" type="checkbox"/> DEYOUNG			SITE TECH.
<input checked="" type="checkbox"/> PROJECT MANAGEMENT	REACTOR SAFETY	OPERATING TECH:	GAMMILL
<input checked="" type="checkbox"/> BOYD	ROSS	EISENHUT	STEPP
<input checked="" type="checkbox"/> P. COLLINS	NOVAK (2)	SHAO	HULMAN
<input checked="" type="checkbox"/> HOUSTON	ROSZTOCZY	BAER	
<input checked="" type="checkbox"/> PETERSON	CHECK	BUTLER	SITE ANALYSIS
<input checked="" type="checkbox"/> MELTZ		GRIMES	VOLLMER
<input checked="" type="checkbox"/> HELTEMES	AT & I		BUNCH
<input checked="" type="checkbox"/> SKOVHOLT	SALTZMAN		J. COLLINS
	RUTBERG		KREGER

EXTERNAL DISTRIBUTION			CONTROL NUMBER
<input checked="" type="checkbox"/> LPDR: MIAMI, FL.	NAT. LAB:	BROOKHAVEN NAT. LAB.	<p>6CC</p> <p>176</p> <p>1</p>
<input checked="" type="checkbox"/> TIC:	REG V. IE	ULRIKSON (ORNL)	
<input checked="" type="checkbox"/> NSIC:	LA PDR		
<input checked="" type="checkbox"/> ASLB:	CONSULTANTS:		
<input checked="" type="checkbox"/> ACRS 16 CYS HOLDING/SENT			

**CATEGORY-B DOCUMENT**

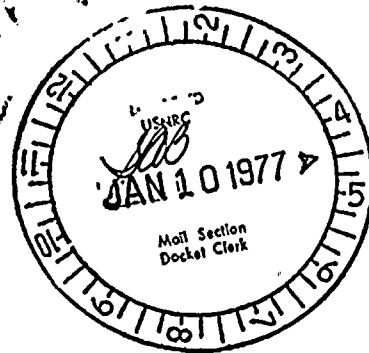
**FINFO ACRS**

ACCOMPLISHED

NOV 19 1957

Regulatory

File Cys



P. O. BOX 013100, MIAMI, FL 33101



FLORIDA POWER & LIGHT COMPANY

January 3, 1977  
L-77-1

Office of Nuclear Reactor Regulation  
Attn: Victor Stello, Jr., Director  
Division of Operating Reactors  
U. S. Nuclear Regulatory Commission  
Washington, D. C. 20555

Dear Mr. Stello:

Re: Turkey Point Units 3 and 4  
Docket Nos. 50-250 and 50-251  
ECCS Reevaluation  
Supplemental Information



On December 30, 1976, (L-76-438), Florida Power & Light Company forwarded the results of the revised ECCS calculations performed using a rated power level of 2200 MWt. Several of the pages in our December 30, 1976, transmittal have been revised to improve their clarity. A copy of the revised report is forwarded herewith.

Very truly yours,

Robert E. Uhrig  
Vice President

REU/GDW/hlc  
Attachment

cc: Norman C. Moseley, Region II  
Robert Lowenstein, Esq.

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TABLE 1

LARGE BREAK  
TIME SEQUENCE OF EVENTS  
STEAM GENERATOR  
10% TUBE PLUGGING

	<u>DECL</u> <u>(C<sub>D</sub>=0.4)</u> <u>(Sec)</u>
START	<u>0.0</u>
Reactor Trip Signal	<u>0.595</u>
S. I. Signal	<u>0.67</u>
Acc. Injection	<u>16.3</u>
End of Bypass	<u>27.52</u>
End of Blowdown	<u>27.66</u>
Bottom of Core Recovery	<u>46.59</u>
Acc. Empty	<u>61.02</u>
Pump Injection	<u>25.67</u>

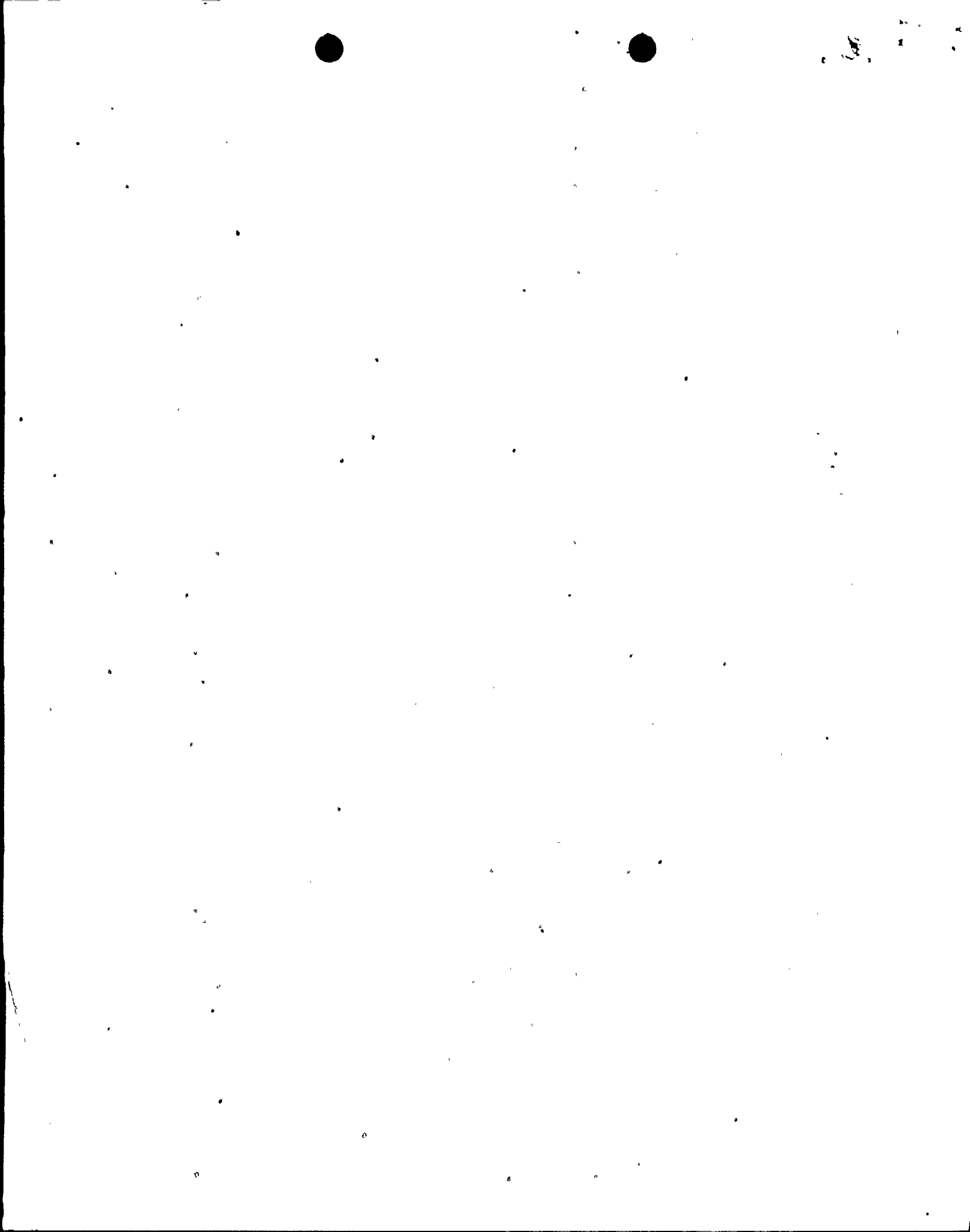


TABLE 2

LARGE BREAK  
STEAM GENERATOR  
10% TUBE PLUGGING

<u>Results</u>	<u>DECL</u> <u>(C<sub>D</sub>=0.4)</u>	
Peak Clad Temp. °F	<u>2190</u>	
Peak Clad Location Ft.	<u>6.0</u>	
Local Zr/H <sub>2</sub> O Rxn(max)%	<u>11.922</u>	
Local Zr/H <sub>2</sub> O Location Ft.	<u>6.0</u>	
Total Zr/H <sub>2</sub> O Reaction %	<u>&lt;0.3</u>	
Hot Rod Burst Time sec	<u>22.8</u>	
Hot Rod Burst Location Ft.	<u>6.0</u>	
<u>Calculation</u>		
Core Power Mwt 102% of		<u>2200</u>
Peak Linear Power kw/ft 102% of		<u>12.61</u>
Peaking Factor		<u>2.22</u>
Accumulator Water Volume (ft <sup>3</sup> )		<u>875</u> (per accumulator)
Fuel region + cycle analyzed	<u>Cycle</u>	<u>Region</u>
UNITS 3 and 4	<u>3</u>	<u>3</u>

TABLE 3 /

LARGE BREAK  
CONTAINMENT DATA (DRY CONTAINMENT)

NET FREE VOLUME	<u>1.55 x 10<sup>6</sup></u>	Ft <sup>3</sup>
INITIAL CONDITIONS		
Pressure	14.7	psia
Temperature	90	°F
RWST Temperature	39	°F
Service Water Temperature	63	°F
Outside Temperature	39	°F
SPRAY SYSTEM		
Number of Pumps Operating	2	
Runout Flow Rate	1450	gpm
Actuation Time	26	secs
SAFEGUARDS FAN COOLERS		
Number of Fan Coolers Operating	3	
Minimum Post Accident Initiation Time for Fan Coolers	26	secs



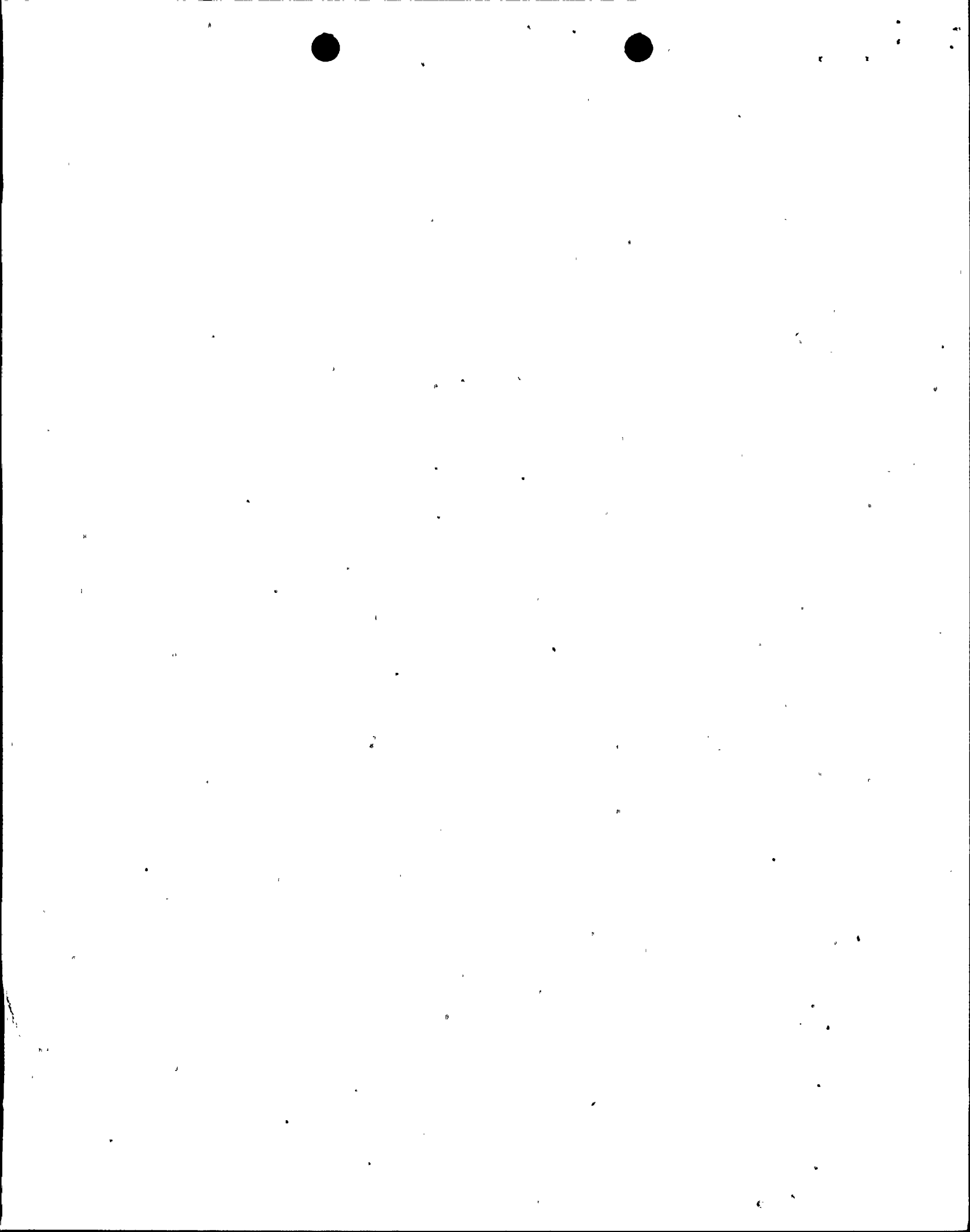


TABLE 3 (Continued)

LARGE BREAK  
CONTAINMENT DATA (DRY CONTAINMENT)

## STRUCTURAL HEAT SINKS

	<u>Thickness (In)</u>	<u>Area (Ft<sup>2</sup>)</u>
Steel	0.03	31,400
Steel	0.063	107,158
Steel	0.1	56,371
Steel	0.2	57,185
Steel	0.24	9,931
Steel	0.2898	---
Concrete	24.0	136,000
Steel	0.4896	23,677
Steel	0.6396	6,537
Steel	0.8904	4,915
Steel	1.256	27,802
Steel	1.56	5,307
Steel	2.0	668
Steel	2.75	1268.7
Steel	5.5	1277.4
Steel	9.0	260.4
Stainless	0.14	---
Concrete	24.0	14,392
Stainless	0.44	768
Stainless	2.126	3,704
Stainless	0.007	102,400
Concrete	24.0	59,132

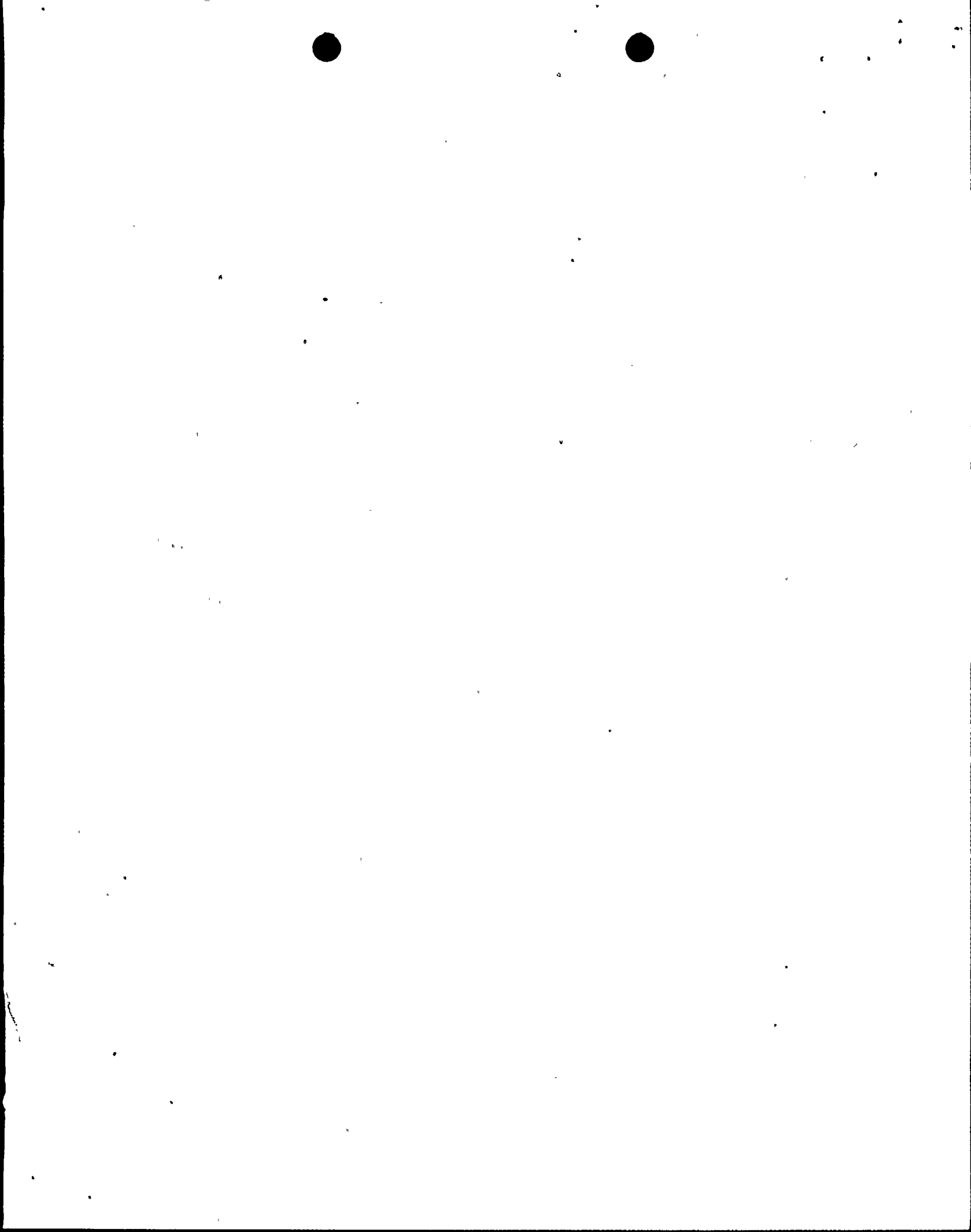


TABLE 4

REFLOOD MASS AND ENERGY RELEASES FOR  
LIMITING CASE DECLG ( $C_D=0.4$ ) AND  
10% STEAM GENERATOR TUBE PLUGGING

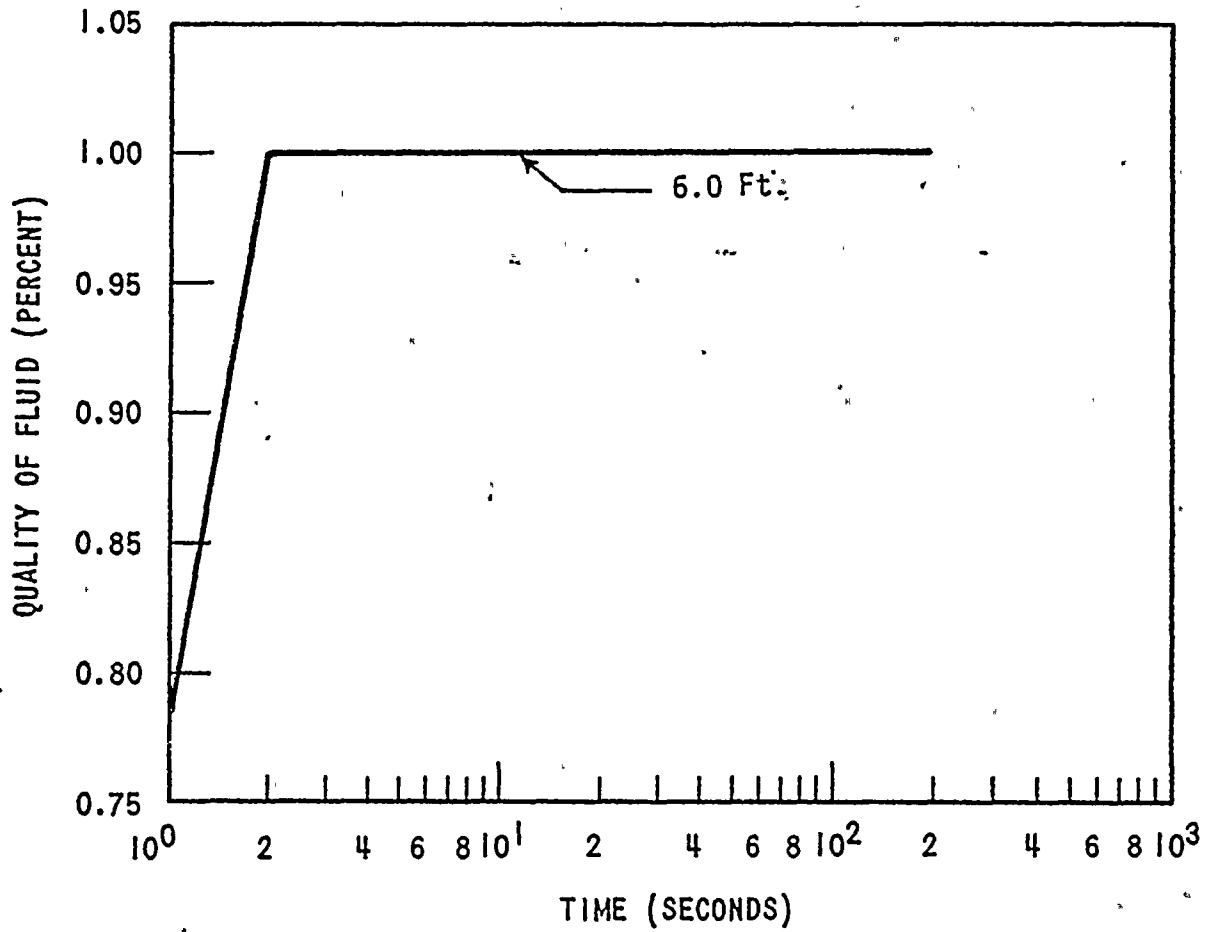
<u>TIME</u> <u>(SEC)</u>	<u>TOTAL MASS FLOWRATE</u> <u>(LBM/SEC)</u>	<u>TOTAL ENERGY FLOWRATE</u> <u>(<math>10^5</math> BTU/SEC)</u>
46.589	0.0	0.0
48.714	0.0415	0.0005
54.286	35.50	0.4614
64.436	95.65	1.189
77.136	98.17	1.219
92.136	103.9	1.280
107.936	220.9	1.603
124.236	263.2	1.678
159.236	274.8	1.607
197.536	281.5	1.514

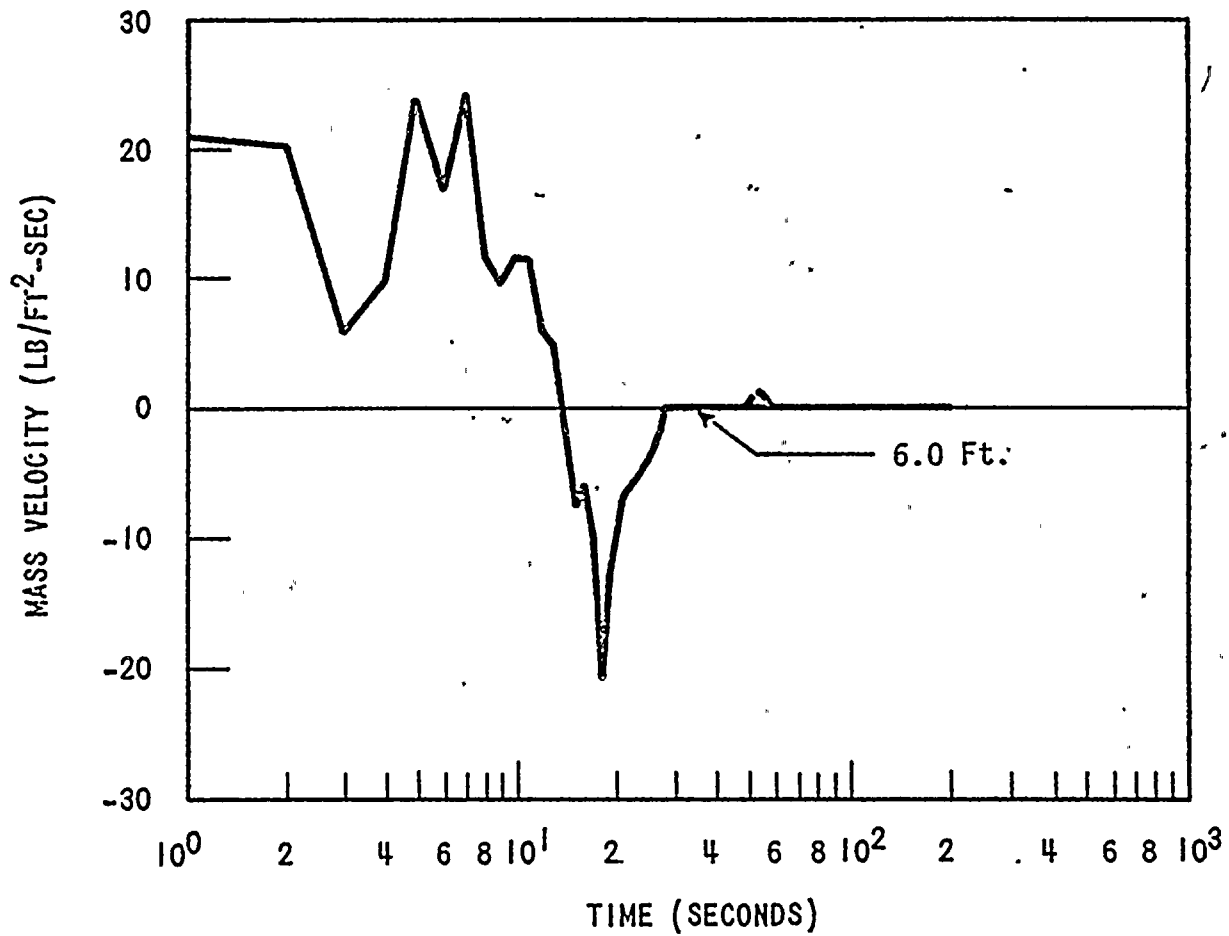


TABLE 5

BROKEN LOOP ACCUMULATOR FLOW TO CONTAINMENTFOR LIMITING CASE DECLG ( $C_D=0.4$ ) 10%STEAM GENERATOR TUBE PLUGGING

<u>TIME (SEC)</u>	<u>MASS FLOWRATE (LBM/SEC)</u>
0.0	0.0
0.02	2723.5
2.00	2276.0
4.00	1994.9
6.00	1793.1
8.00	1645.5
10.0	1526.4
15.0	1302.5
20.0	1137.8
25.0	1034.6
30.0	954.2
35.0	887.0
38.9	842.6

Figure 1 Fluid Quality - DECLG ( $C_D = 0.4$ )

Figure 2 Mass Velocity - DECLG ( $C_D = 0.4$ )





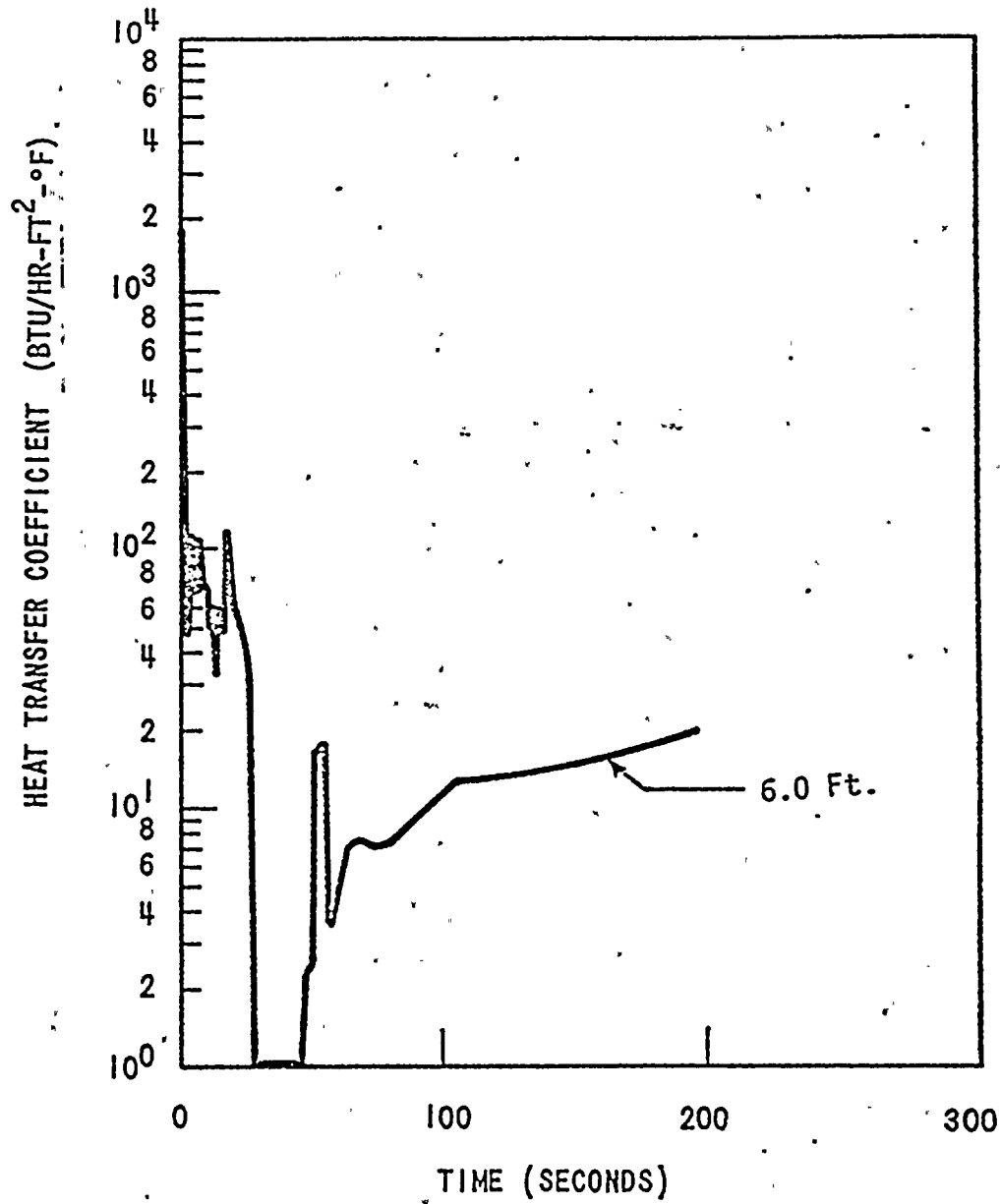


Figure 3 Heat Transfer Coefficient - DECLG ( $C_D = 0.4$ )



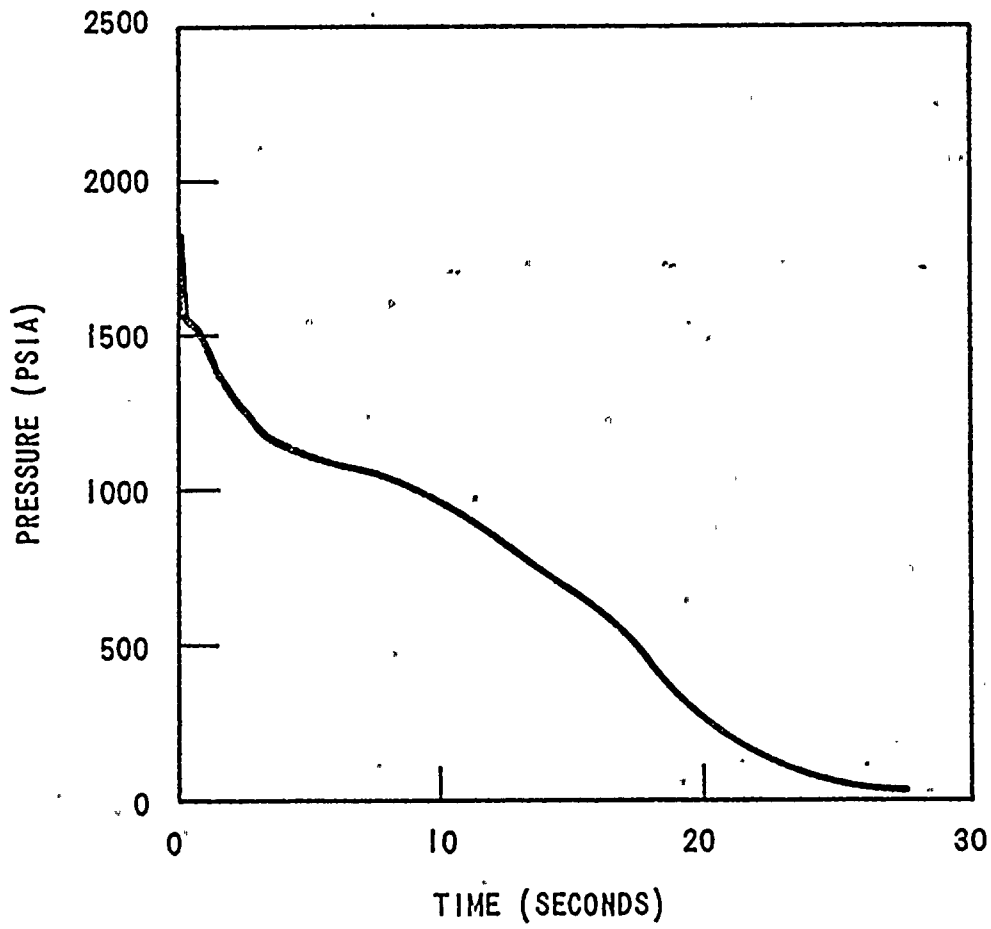


Figure 4 Core Pressure - DECLG ( $C_D = 0.4$ )

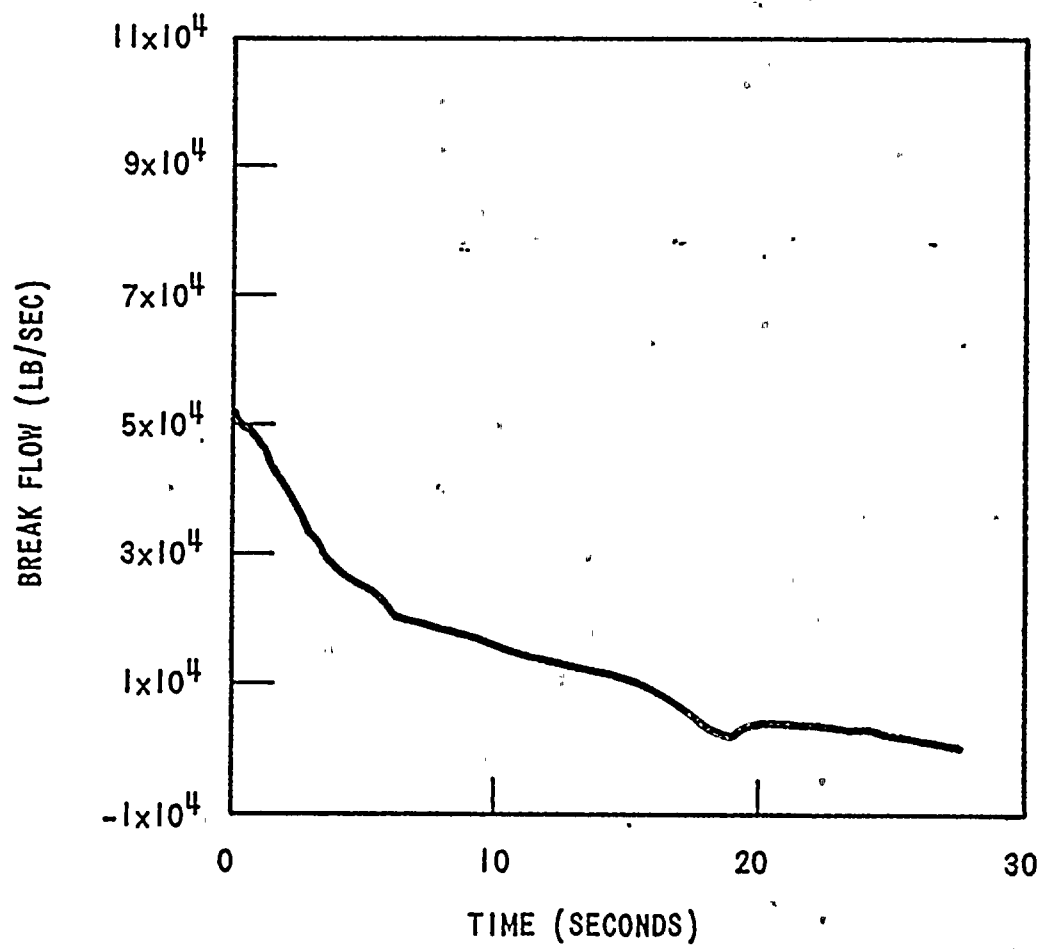


Figure 5 Break Flow Rate - DECLG ( $C_D = 0.4$ )

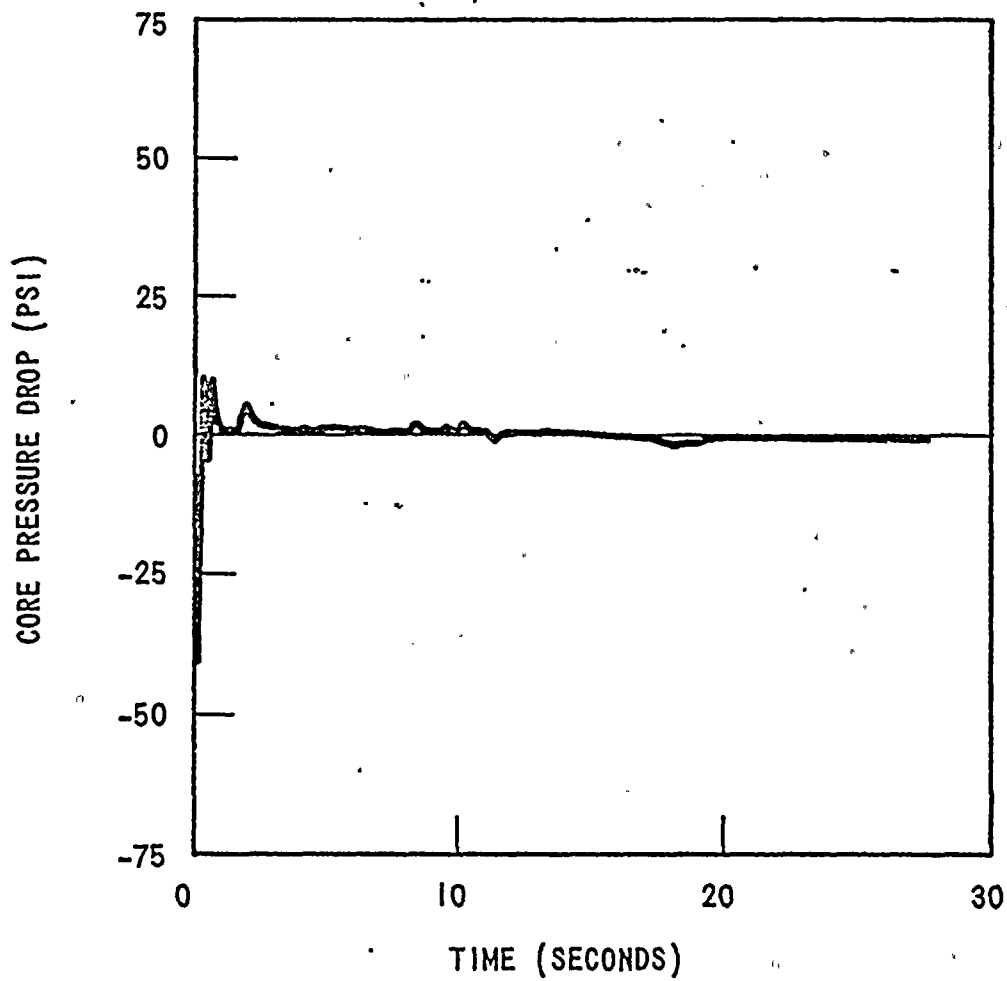


Figure 6 Core Pressure Drop - DECLG ( $C_D = 0.4$ )

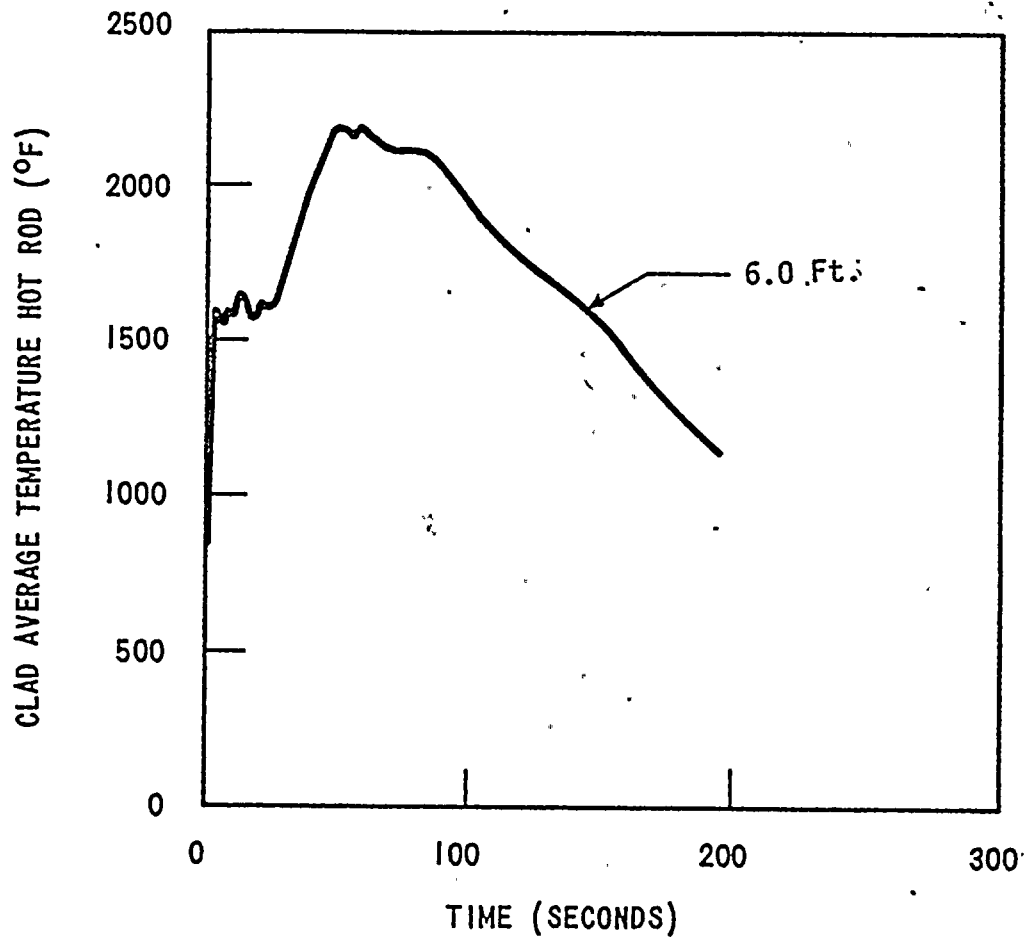


Figure 7 Peak Clad Temperature - DECLG ( $C_D = 0.4$ )

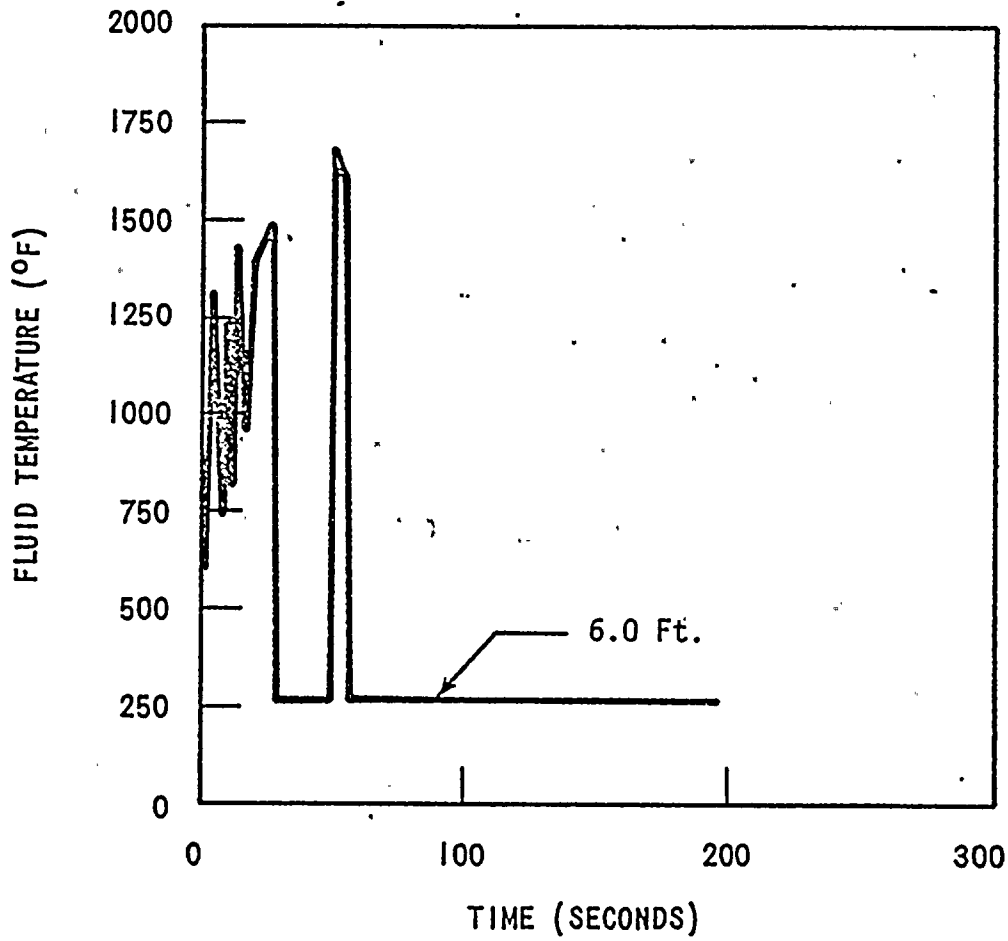


Figure 8 Fluid Temperature - DECLG ( $C_D = 0.4$ )



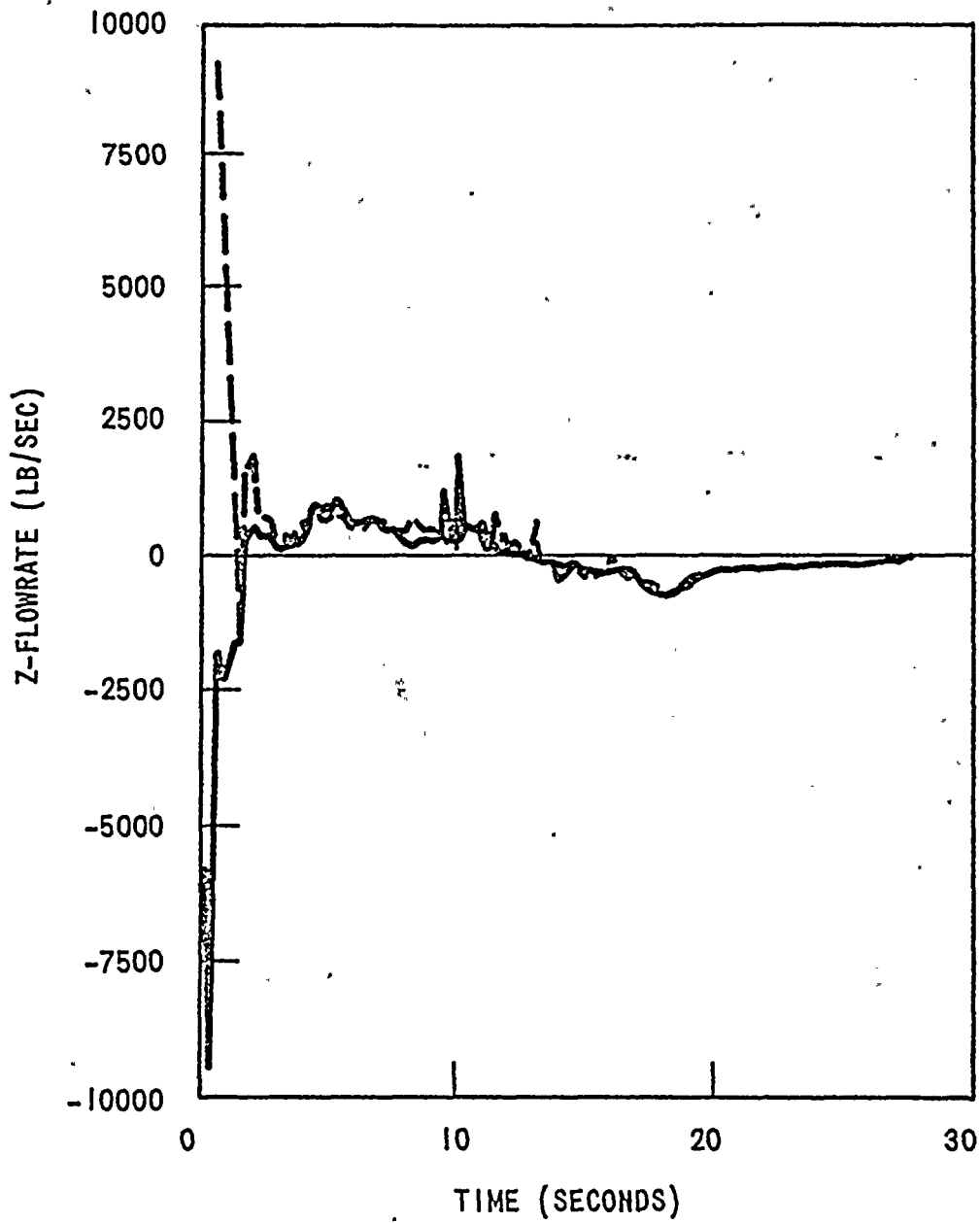


Figure 9 Core Flow - Top and Bottom - DECLG ( $C_D = 0.4$ )

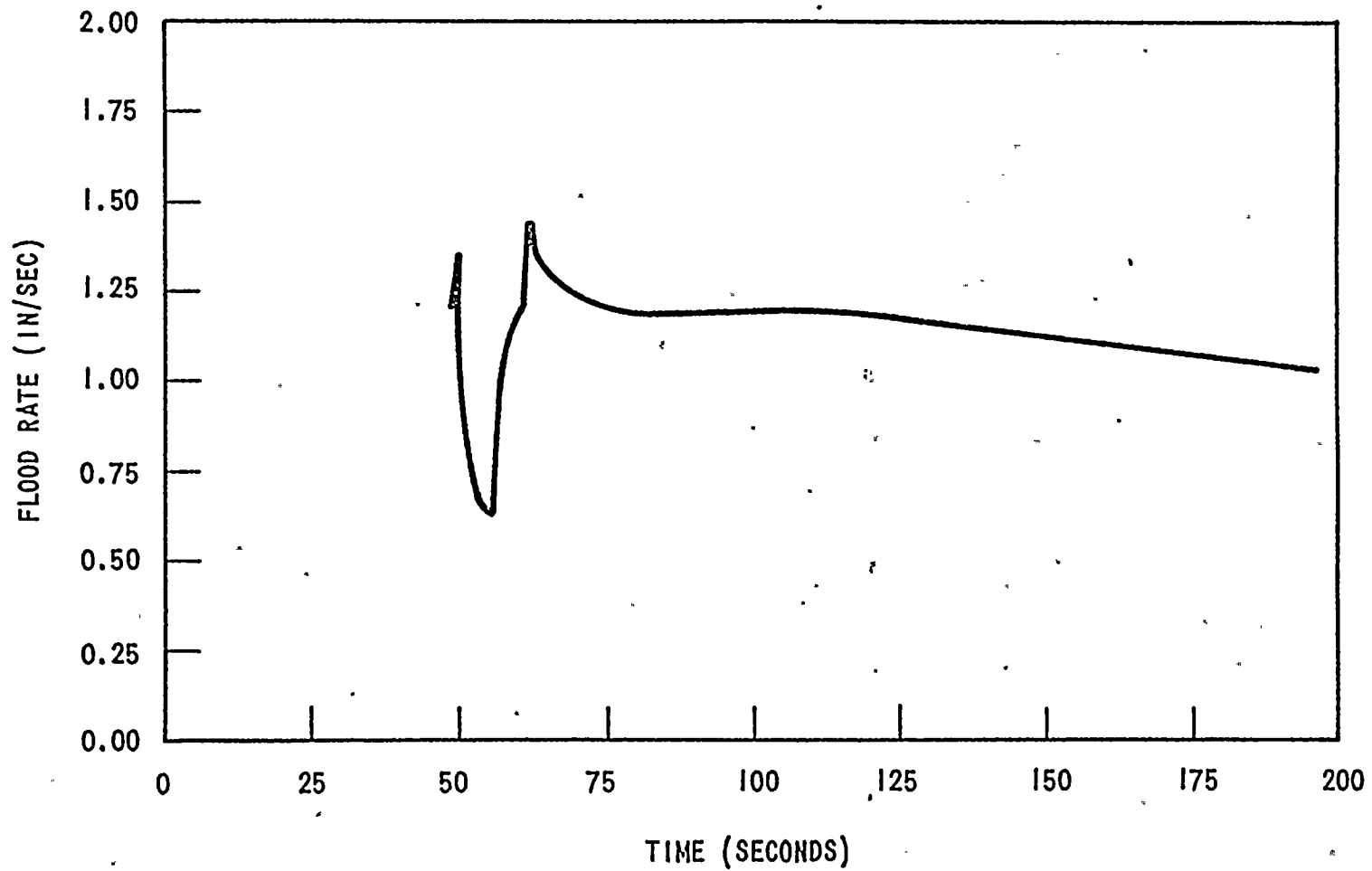


Figure 10 Reflood Transient - DECLG ( $C_D = 0.4$ )  
Core Inlet Velocity



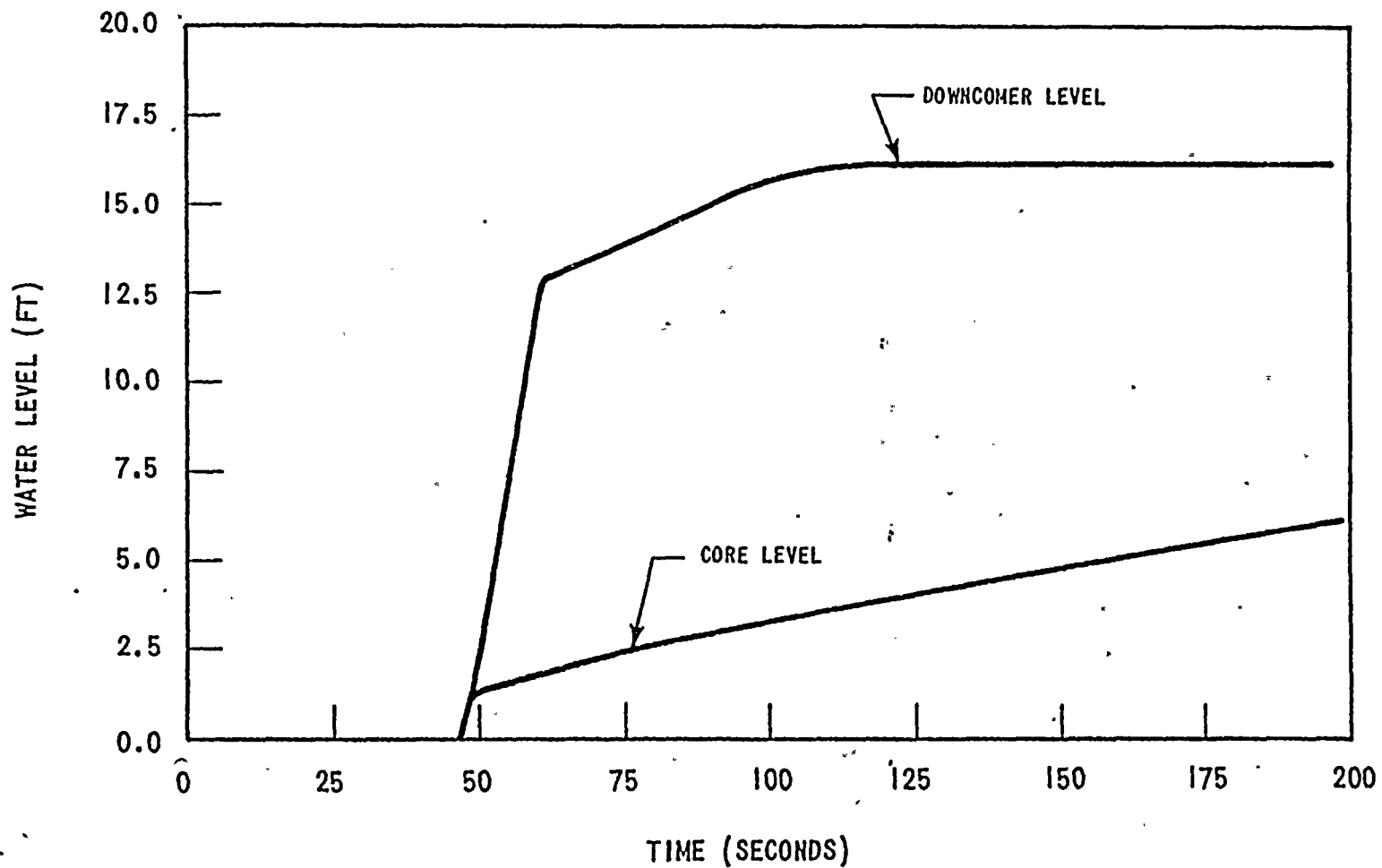


Figure 11 Reflood Transient - DECLG ( $C_D = 0.4$ )  
- Downcomer and Core Water Levels

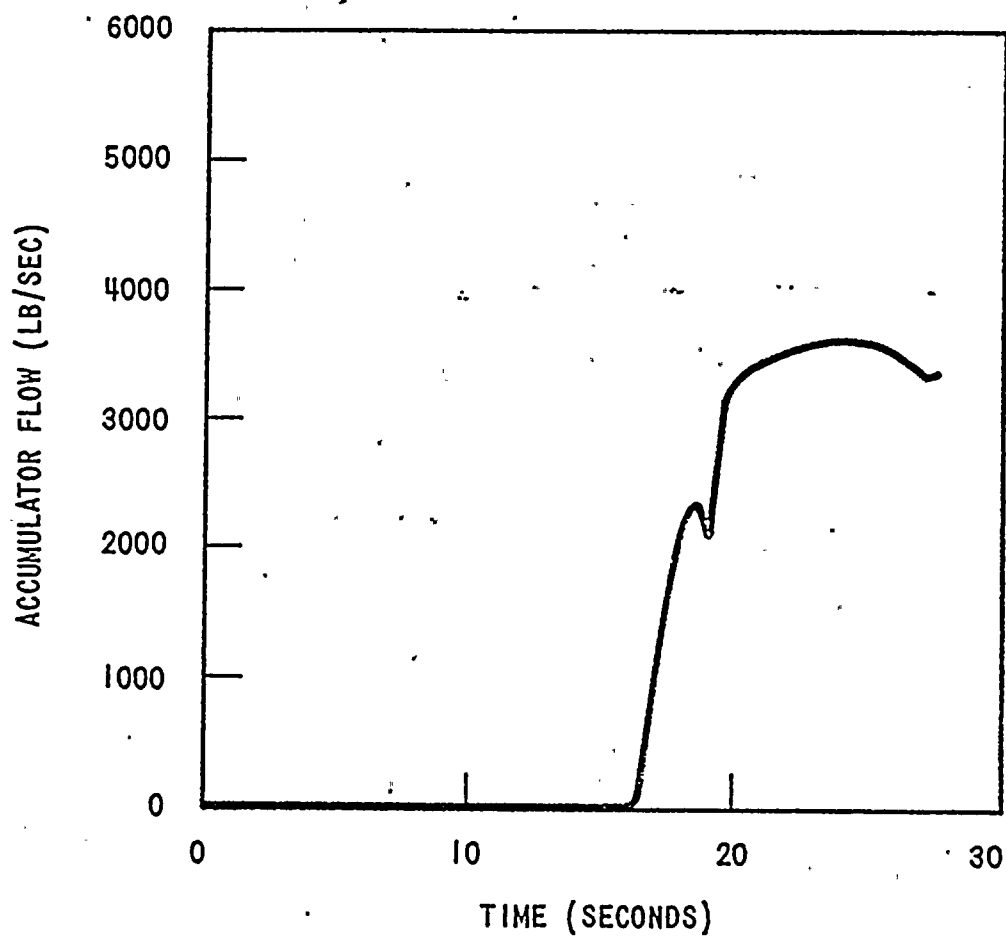


Figure 12 Accumulator Flow (Blowdown) - DECLG ( $C_D = 0.4$ )

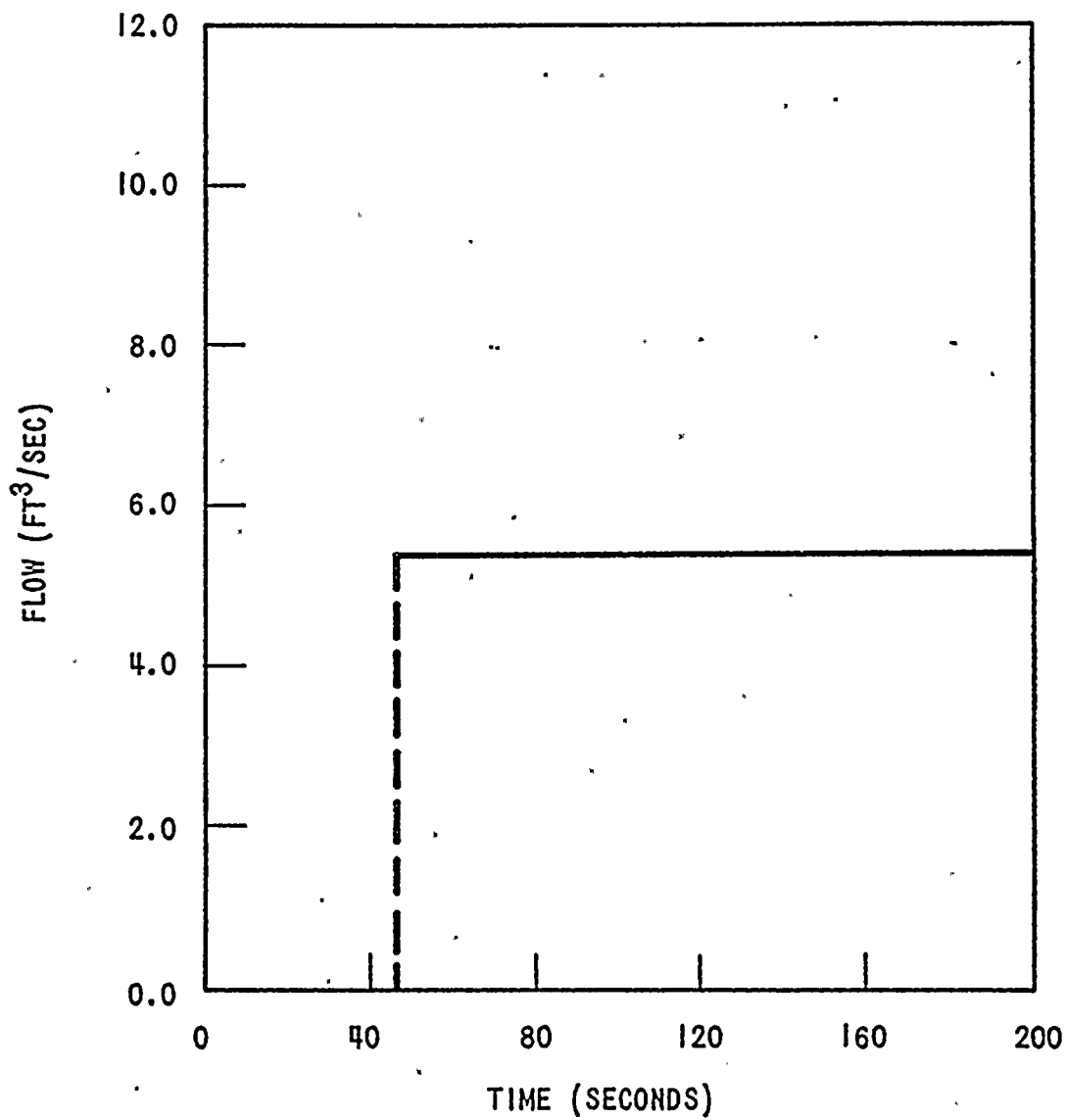


Figure 13 Pumped ECCS Flow (Reflood) - DECLG ( $C_D = 0.4$ )

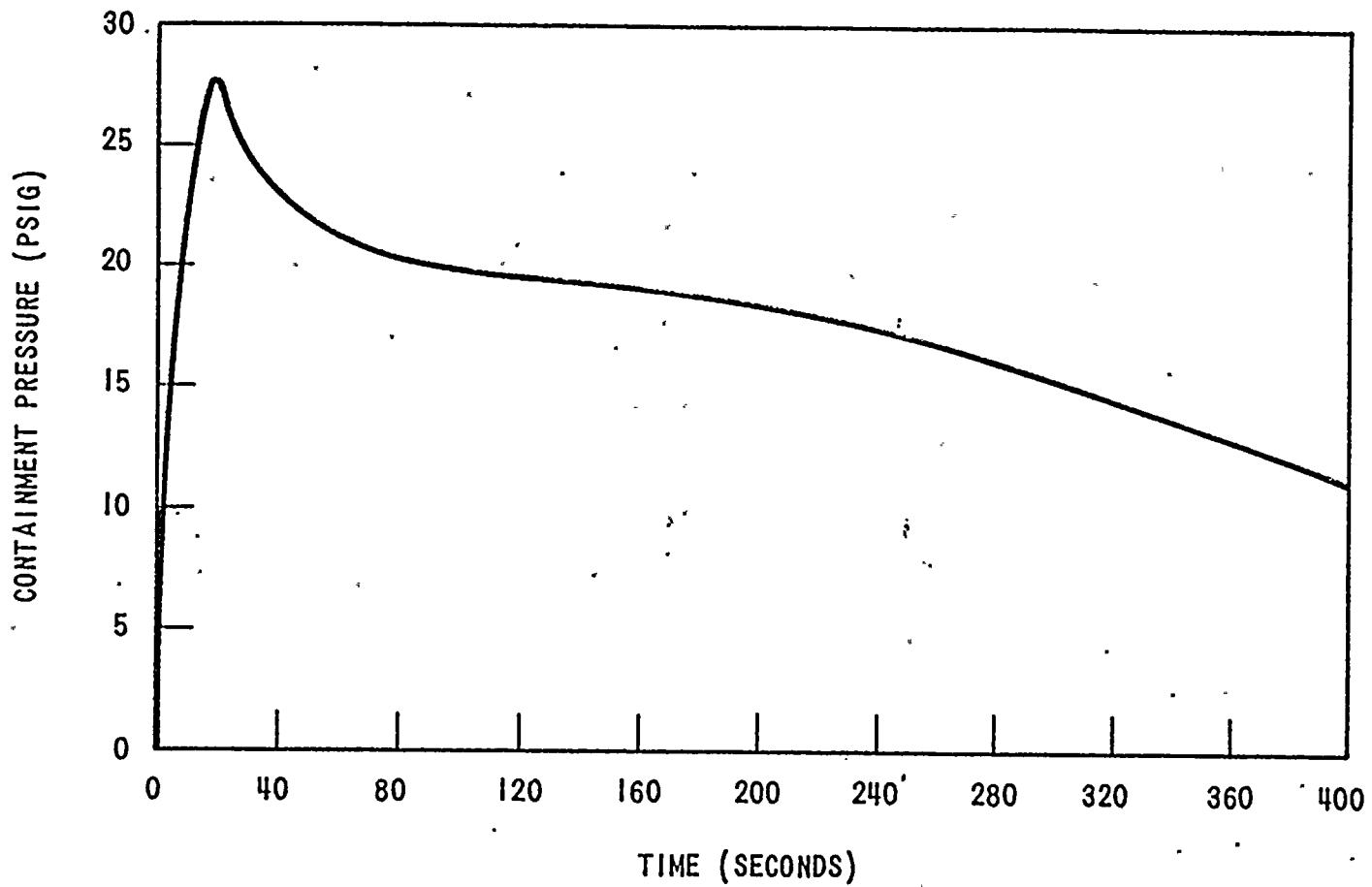


Figure 14 Containment Pressure - DECLG ( $C_D = 0.4$ )





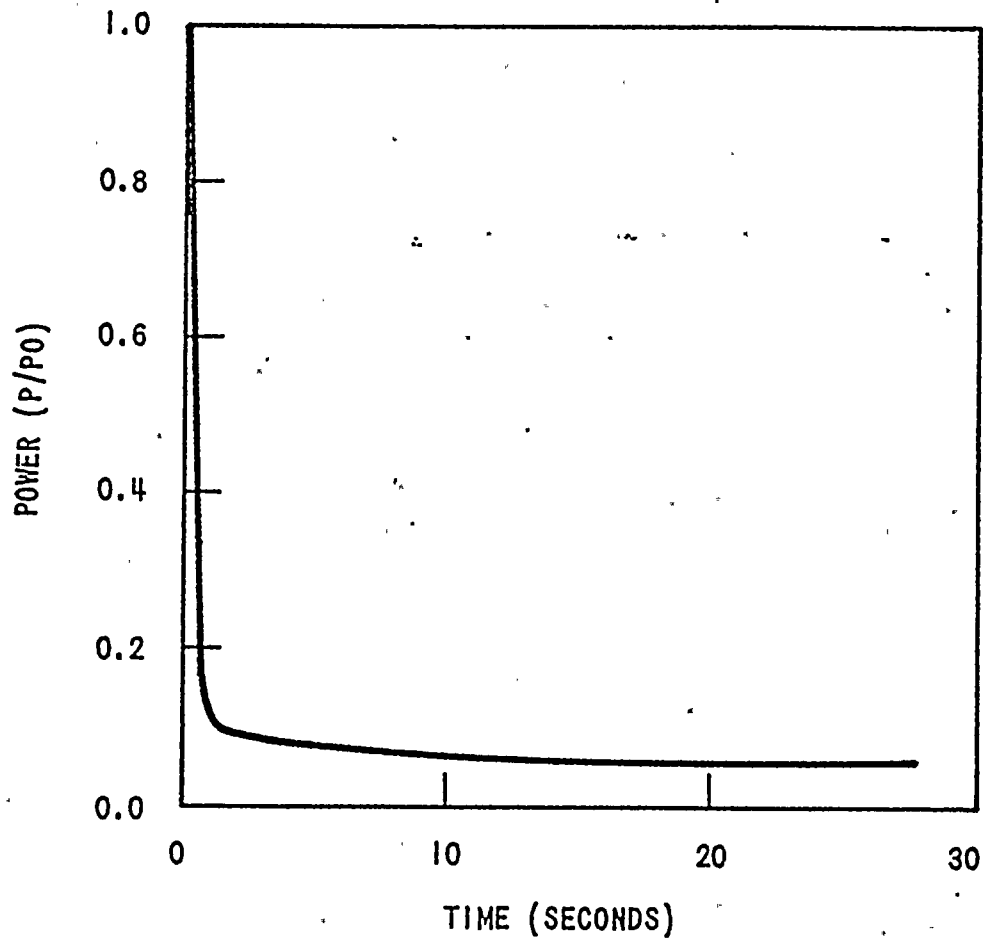


Figure 15 Core Power Transient - DECLG (C<sub>D</sub> = 0.4)



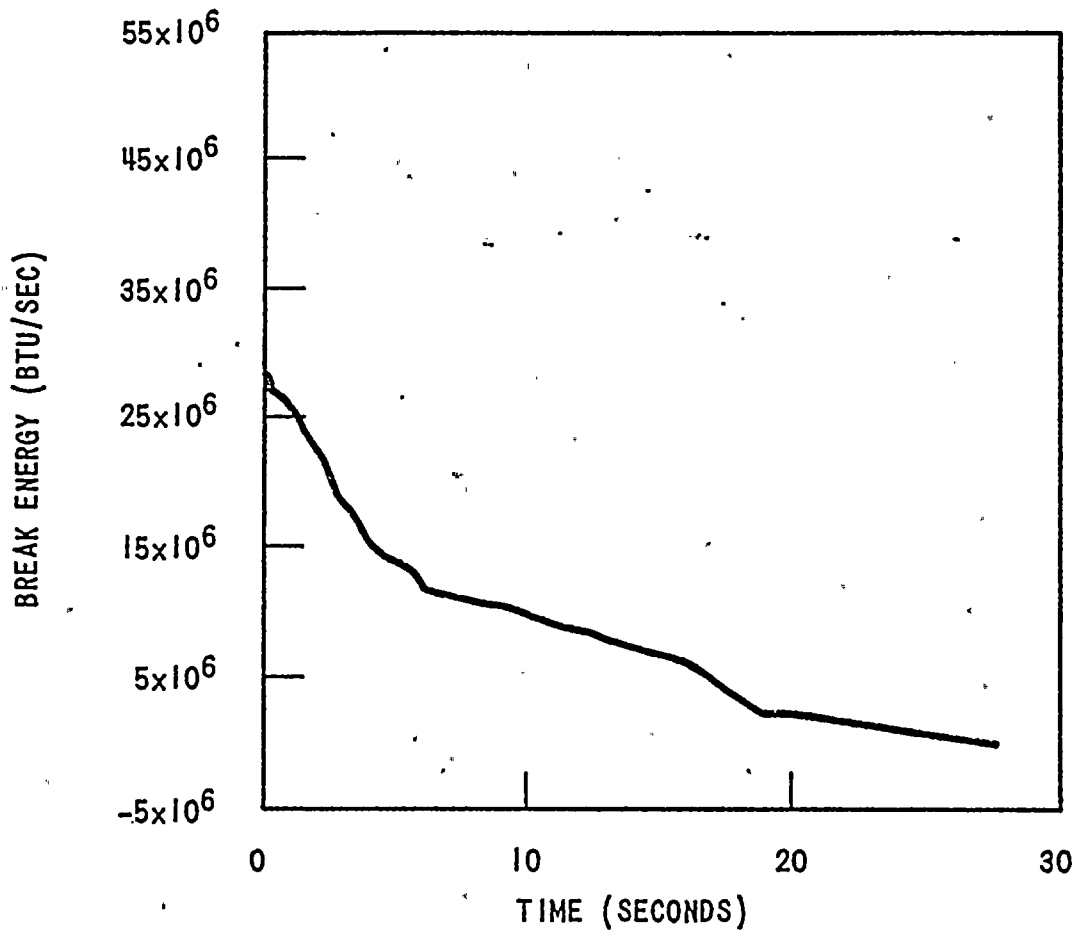


Figure 16 Break Energy Released to Containment

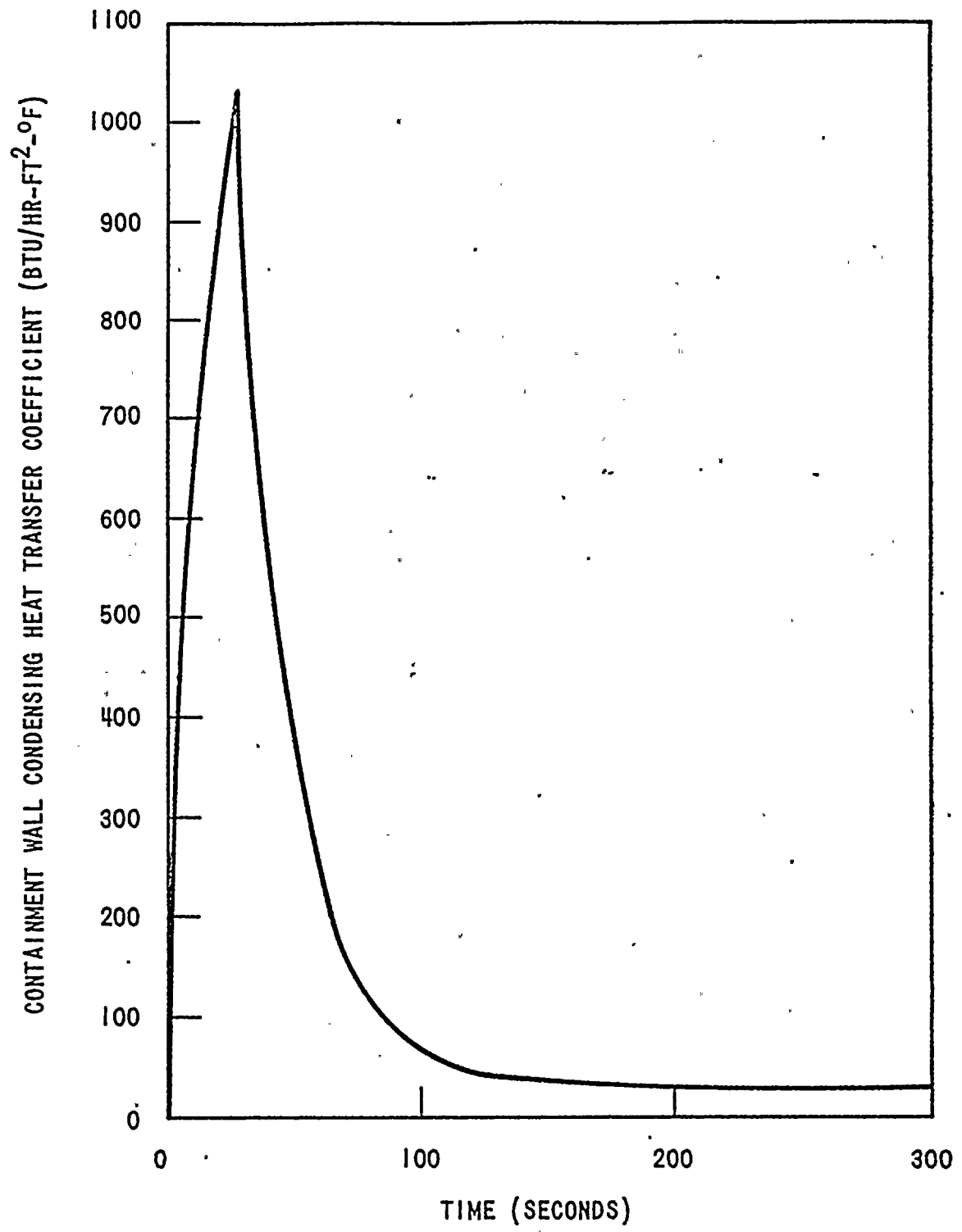


Figure 17 Containment Wall Condensing Heat Transfer Coefficient

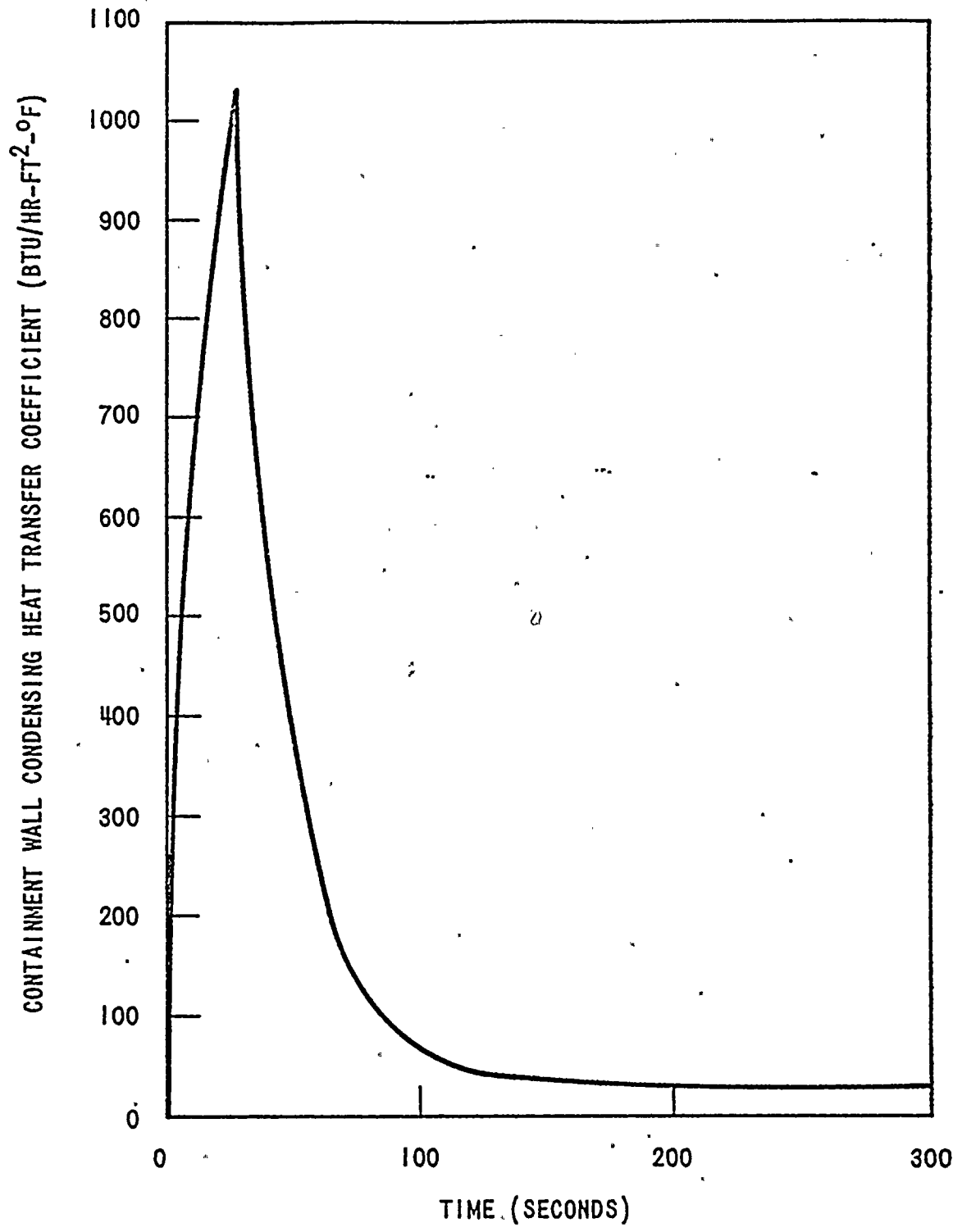


Figure 17 Containment Wall Condensing Heat Transfer Coefficient



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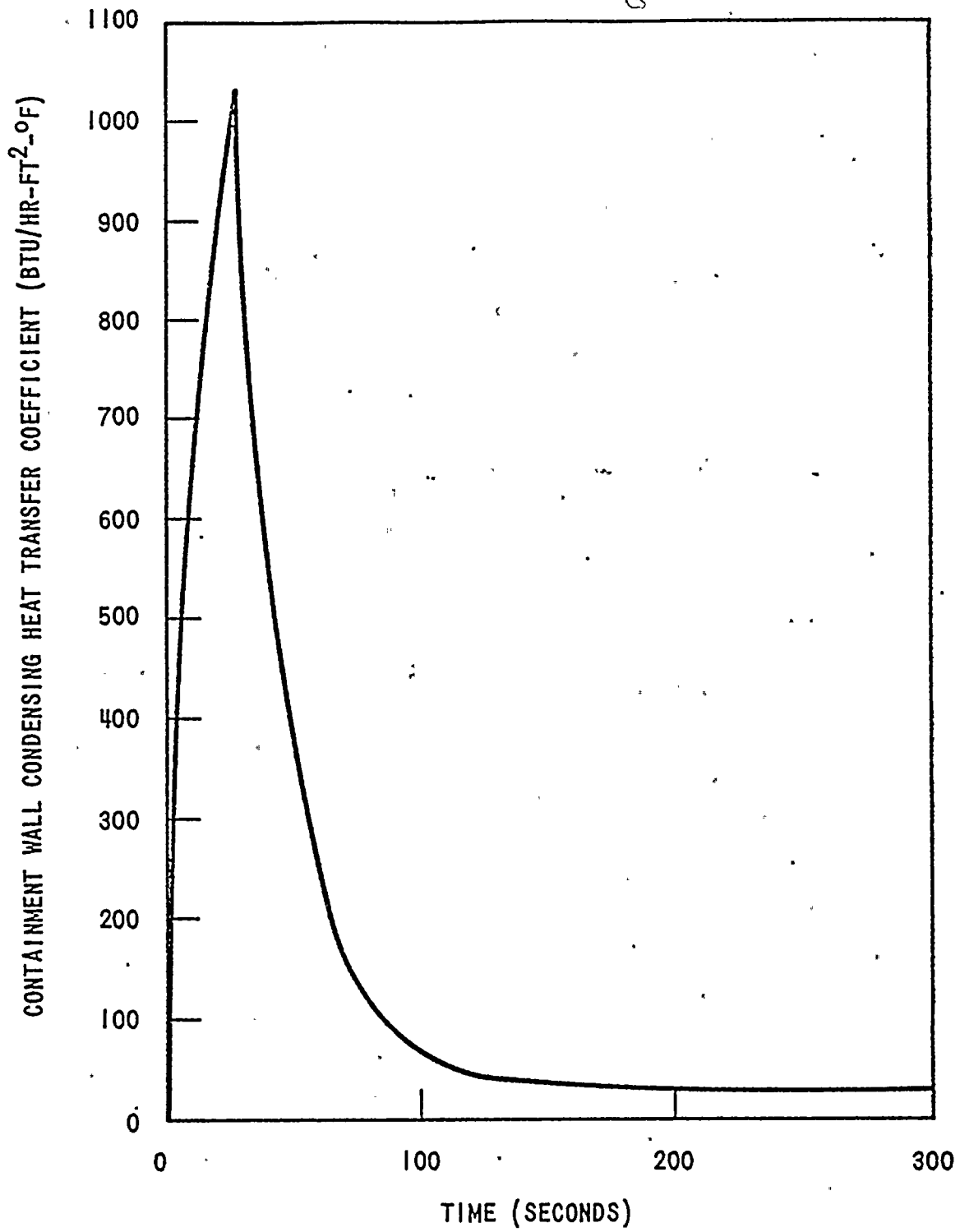


Figure 17 Containment Wall Condensing Heat Transfer Coefficient

