

REVISED REPORT ON THE REANALYSIS OF SAFETY-RELATED PIPING SYSTEMS

SURRY POWER STATION, UNIT 1 VIRGINIA ELECTRIC AND POWER COMPANY

January 1980

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Stone & Webster Engineering Corporation Boston, Massachusetts



VIRGINIA ELECTRIC AND POWER COMPANY, RICHMOND, VIRGINIA 23261

January 15, 1980

Mr. Harold R. Denton, Director Office of Nuclear Reactor Regulation U.S. Nuclear Regulatory Commission Washington, DC 20555

Serial No. 048 PSE&C/CMRjr:mac:wang

Docket No. 50-280

License No. DPR-32

Dear Mr. Denton:

### COMPLETION OF SHOW CAUSE ORDER REANALYSIS SURRY POWER STATION UNIT 1

The Virginia Electric and Power Company letter of December 21, 1979 (Serial No. 1158) gave notification of the completion of analysis associated with the 60 day time period designated in the Nuclear Regulatory Commission Order of August 22, 1979. The purpose of this letter is to transmit the results of that analysis in a format similar to our previous reports of June 5 and August 1, 1979. As stated in our December 21, 1979 letter, all modifications associated with the Order of August 22, 1979 will be completed by February 1, 1980.

The attached report concludes our detailed submittals on the design basis earthquake analysis associated with the March 13, 1979 Order to Show Cause for Unit 1. We will notify you when these modifications are completed.

If you have any questions, please contact us.

Very truly yours,

W. Z. Spencer Vice President - Power Station Engineering and Construction Services

Attachment

cc: Mr. Victor Stello, Director Office of Inspection & Enforcement

> Mr. James P. O'Reilly, Director Office of Inspection and Enforcement Region II

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### SECTION 1

### INTRODUCTION

The Nuclear Regulatory Commission (NRC) Order to Show Cause of March 13, 1979, required certain piping systems associated with Surry Power Station - Unit 1 to be reanalyzed, using an appropriate piping code to account for seismic loads. VEPCO complied with the order by the shutdown of Surry 1 within 48 hours.

The initial analysis effort to reanalyze these systems began immediately. Major decisions were made by VEPCO concerning the course of reanalysis. These actions had a major influence on the method in which the reanalysis was completed. These actions included:

1. The use of NUPIPE computer code for all dynamic reanalysis.

- The use of soil structure interaction (SSI) for the development of amplified response spectra (ARS) in dynamic reanalysis.
- 3. The award of a contract to obtain services of Quadrex (Nuclear Services Corporation) to complete a portion of the piping reanalysis.

4. The use of field-verified input into the pipe stress reanalysis.

On April 2, 1979, a letter was issued by the Nuclear Regulatory Commission clarifying the intent of the March 13, 1979, Show Cause Order. This letter contained specific information concerning exactly what information was required to allow the Show Cause Order to be lifted and the plant's return to operation. Among the requirements of the April 2, 1979, letter was a list of the material required for NRC review of reanalysis results and a plan for verification of dynamic analysis codes. This letter also requested response for the licensee concerning what methods of seismic analysis were employed for other systems within the show cause plants, and also, a listing of all piping systems affected by the Show Cause Order. VEPCO's response to this letter was Serial No. 220/040279, dated May 24, 1979 (Item 22, Appendix B).

The NRC letter of April 13, 1979 (Item 3, Appendix B), informed VEPCO that use of SSI techniques for the development of amplified response spectra utilizing an elastic half-space model would be acceptable for reevaluation of piping at Surry 1 and 2.

As the Show Cause analysis continued, SSI ARS were employed. The acceptability of SSI was obtained on May 25, 1979, in an NRC letter from D. Eisenhut (Item 5, Appendix B). The completion of documentation to support the staff review of SSI was supplied in the report, "Soil Structure

Interaction in Development of Amplified Response Spectra for Surry Power Station - Units 1 and 2." The date of this report is June 8, 1979 (Item 26, Appendix B).

Following the acceptability of the SSI ARS by the NRC, meetings were held both in the offices of Stone & Webster in Boston, Massachusetts, and the NRC in Bethesda, Maryland, to review the reanalysis completed and determine the acceptability of that reanalysis to allow interim plant operation. The reanalysis completed indicated that the computer code in question had no major effect on the ability of the piping systems to withstand earthquakes. Specific understandings were reached during these meetings, including evaluation of the Design Basis Earthquake (DBE), forming the basis for interim lifting of the show cause order and interim operation.

In order to develop a viable basis for interim operation of Surry Unit 1, the scope of reanalysis initially included some problems that used computer codes not addressed by the order to show cause. These were piping problems addressed by USNRC IE Bulletin 79-04 (Velan Valves). Also reanalyzed were SHOCK O/I piping problems. The reanalysis of these piping systems is being completed as part of IE Bulletin 79-14 reanalysis.

By June 5, 1979, the reanalysis had proceeded sufficiently to allow the issuance of "The Report on the Reanalysis of Safety-Related Piping Systems,

Surry Power Station - Unit 1," VEPCO Serial No. 453 (Item 24, Appendix B). This report outlined the pipe stress and pipe support analysis completed to date and requested interim operation of the unit, based on the minor hardware modifications identified as of that time. This submittal also included a summary of the conservatisms that were being factored into the reanalysis. This request for interim operation was refused.

As a result of the June 5, 1979, submittal, additional meetings were held with the NRC to discuss requirement for interim operation. It was then determined that the completion of the pipe stress analysis would be necessary in order to allow interim operation. Upon completion of the pipe stress analysis, a second submittal was issued on August 1, 1979, "Revised Report on the Reanalysis of Safety-Related Piping Systems, Surry Power Station - Unit 1," VEPCO Serial No. 453A (Item 31, Appendix B). Discussions and meetings between Stone & Webster, VEPCO, and the NRC (following this submittal) led to a letter written by VEPCO on August 21, 1979 (Item 32, Appendix B). This letter concluded that typical pipe support analysis was complete within the reactor containment and that certain systems outside the containment, as designated by the NRC, were also complete. This letter resulted in the lifting of the Show Cause Order by the Commission, on August 22, 1979 (Item 15, Appendix B).

Surry Unit 1 was not allowed to start up at this time, based on NRC Inspection and Enforcement (I&E) concerns about the acceptability of embedded anchor bolt

inspections required per I&E Bulletin 79-02 and the work completed to date on I&E Bulletin 79-14. The October 4, 1979, VEPCO letter, Serial No. 817 (Item 35, Appendix B), to the Commission on I&E Bulletins 79-14 and 79-02, was evaluated by I&E and interim start-up was granted following completion of specific activities outlined in that letter. Interim start-up of the plant occurred on October 25, 1979. This was after VEPCO committed to an expedited schedule for the reanalysis of all piping systems in accordance with I&E Bulletin 79-14.

The August 22, 1979, lifting of the Show Cause Order allowed VEPCO 60 days after startup to complete all DBE pipe support reanalysis outside the reactor containment building on the problems specifically addressed by the March 13, 1979, Order to Show Cause. At the end of the 60 day period, December 23, 1979, the provisions of the August 22, 1979, order were met as discussed in the VEPCO letter of December 21, 1979, Serial No. 1158 (Item 40, Appendix B).

The purpose of this report is to document the results of the DBE reanalysis during the 60 day interval in a format similar to the June 5 and August 1, 1979, reports. This report concludes detailed documentation of all aspects of the Design Basis Earthquake Show Cause reanalysis for Surry Power Station, Unit 1.

### SECTION 2

### PIPE STRESS RESULTS

A total of 63 pipe stress problems were originally analyzed by the PSTRESS/SHOCK 2 computer program that used algebraic summation and are therefore specifically addressed by the Show Cause Order. These stress problems were analyzed by two groups: Stone & Webster Engineering Corporation (S&W) in Boston, Massachusetts, and Nuclear Services Corporation (NSC) or Quadrex in Campbell, California, as indicated in the following table:

### PIPE STRESS PROBLEMS



Field-verified piping isometric drawings provide the basis for program inputs for the pipe stress reanalysis of the SHOCK 2 problems. The reanalysis is conducted using the NUPIPE computer program. NUPIPE calculates intra-modal seismic forces using a modified square root of the sum of the squares (SRSS)

technique which is always more conservative than the approved SRSS method, and an SRSS technique for inter-modal combination.

Additionally, in some cases, piping is analyzed utilizing amplified response spectra (ARS) that are developed using soil structure interaction techniques (SSI-ARS). The resultant stresses and loads are used to evaluate piping, supports, nozzles, and penetrations. In accordance with the NRC letter of May 25, 1979 to Virginia Electric and Power Company (VEPCO), the seismic inertial stresses typical loads computed using the SSI-ARS have been increased by a factor of 1.5 for the DBE condition.

All 63 SHOCK 2 problems have been reanalyzed and approved by S&W Engineering Assurance or NSC Quality Assurance. Table 2-1 for the Design Basis Earthquake shows the results for these 63 stress problems. In Table 2-1, the figures for Original Total Stress, at the point of maximum total stress in the pipe, and Original Seismic Stress, at the same point, are extracted from Table 3-1 of the "Seismic Design Review Equipment and Piping, Surry Power Station," dated September 15, 1971. The original calculations for the seismic design review report are no longer available; therefore, correlations were made to the original stresses in Table 3-1 on the basis of the MSK's.

In Table 2-1, the columns for New Total Stress, at the point of maximum total stress in the pipe, and New Seismic Stress, at the same point, were taken from

the NUPIPE computer runs with the seismic inertial stress magnified by a factor of 1.5 for runs using the SSI-ARS, per the NRC letter to VEPCO of May 25, 1979. Of the 63 problems in Table 2-1, 56 used the SSI-ARS and 7 used the original ARS.

The original total and original seismic stresses shown in Table 2-1 were computed using the SHOCK 2 programs for the original design conditions. The new total and new seismic stresses were computed by the NUPIPE program using different mass models and in some cases different ARS's than the original calculations. More importantly, the reanalyses were based on field-verified piping configurations in 1979, which in some cases differ from the original design conditions. For this reason, the new stresses and the original stresses in Table 2-1 are not comparable, as they do not necessarily represent the same physical conditions.

Table 2-2 summarizes the nozzles and penetrations evaluated under the reanalysis program. All of the 84 nozzles on problems originally analyzed by the SHOCK 2 program have been found acceptable by S&W. For those problems in which the SSI-ARS are used, the seismic inertial nozzle loads have been increased by a factor of 1.5 per the NRC letter of 25 May 1979.

The typical SHOCK 2 stress problems include 8 penetrations. The analyses of all penetrations have been completed. Table 2-4 lists all modifications to reduce nozzle and penetration loads.

Table 2-3 lists the hardware modifications necessary to bring the pipe stress analysis to within code allowables. Of the 63 SHOCK 2 problems reanalyzed, hardware modifications were made to 20 problems due to pipe stress. These modifications consisted of 63 added, modified, or deleted supports. No physical modifications to piping were required.

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# TABLE 2-1

### PIPE STRESS REEVALUATION SUMMARY DESIGN BASIS EARTHQUAKE

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Prob-			Line		Pipe	Stress	(psi)	
lem No	System <u>Name</u>	Iso. <u>No.</u>	Size (NPS)	Original Total*	Original Seísmíc×	New Total	New <u>Seísmic</u>	Allow- able
			.SHOCK2	Problems	-			
555	Low Head Safety Injection	122 D1	10'' 12''	29290	NA	10733	5311	30882
1555	Low Head Safety Injection	122 L1	12"	25290	NA	10036	3855	30882
706A	Low Head Safety Injection	122 H1	6"	18451	10707	15953	10024	30769
707A	Low Head Safety Injection	122 J1	6"	22436**	19577* <del>*</del>	19229	12556	33750(1)
708	Low Head Safety Injection	122 Kl	6"	20552 <b>*</b> *	NA	17489	10941	30769(1)
731A	Low Head Safety Injection	127 E1	8"	22671**	NA	12734	5393	29970(2,5)
731B	Low Head Safety Injection	127 E2	811	22671	NA	13470	2033	29970(2,5)
743	Low Head Safety Injection	127 F1	10"	24649* <del>*</del>	NA	14789	5496	33750
727	Low Head Safety Injection	127 C1 127 C2	6" 10"	28909**,	NA	29157	26678	29970
735	High Head Safet <b>y</b> Injection	127 G1 127 G2	4", 6" 8", 10"	23011	13220	19296	15708	31104(3)
525A 1525A	Containment & Recirculation Spray	123 Al	8'' 10''	11999	10866	6388 5596	3311 4275	33750 <b>(4)</b> 33750
546 <b>/</b> 560	Containment & Recirculation Spray	123 D1 123 E1	8" 10"	28209	24753	10751	`2291	32616(2)
546 <b>/</b> 5600	Containment & Recirculation Spray	123 F3,	8'' 10''	28209	24753	21279	2658	32616

# TABLE 2-1 (Cont)

### PIPE STRESS REEVALUATION SUMMARY DESIGN BASIS EARTHQUAKE

Prob-			Line 👘		Pipe	Stress	(psi)	
lem No	System <u>Name</u>	Iso. <u>No.</u>	Size (NPS)	Original Total¥	Original <u>Seismic×</u>	New <u>Total</u>	New <u>Seismic</u>	Allow- able
546⁄ 5620	Containment & Recirculation Spray	123 F2	8" 10" '	28209	24753	21003	2499	32616
548C	Containment & Recirculation Spray	123 H2	10"	15785* <del>*</del>	11241××	5610	2685	32616(\$)
547	Containment & Recirculation Spray	123 Cl	8" 10"	20953	5688	7451	5634	33750(5)
744 <b>/</b> 754	Containment & Recirculation Spray	123 J1	8"	26721**	NA	28136	16398	33750(*)
548A	Containment & Recirculation Spray	123 B1	8'' 10''	11955	11256	14927	11598	.33750 (\$)
548B	Containment & Recirculation Spray `	123 H1	10 <sup>11</sup>	28660	26790	17028	15505	32616
544	Containment & Recirculation Spray	123 G1 123 G2	10"	13402	6986	9211	6133	28485
544A	Containment & Recirculation Spray	123 R2	10"	12853	11256	6430	3556	29970
544B	Containment & Recirculation Spray	123 R1	10"	12853	11256	6448	4541	28485
751	Containment & Recírculation Spray	123 N1 123 N2	10"	6010	5169	7085	5206	28485
562	Containment & Recirculation Spray	123 F1 123 E2	10"	12610**	NA	28600	1962	32616(2,5)
745	Containment & Recirculation Spray	123 Kl	811	25702	24579	25394	2148	33750())
323A	Main Steam	100 D1	30"	13824	6343	12988	354	27000
322A	Main Steam	101 D1	30"	13031	5548	11546	852	27000
334A	Main Steam	102 D1	30"	18635	11082	15319	463	27000

# TABLE 2-1 (Cont)

### PIPE STRESS REEVALUATION SUMMARY DESIGN BASIS EARTHQUAKE

Prob-			Line		Pipe	Stress	(psi)	
lem <u>No.</u>	System <u>Name</u>	Iso. <u>No.</u>	Síze <u>(NPS)</u>	Original Total*	Original <u>Seismic×</u>	New <u>Total</u>	New <u>Seísmíc</u>	Allow- able
346	Main Steam	103 Al	30"	19970	12563	31663	14049	33750(7)
323B	Feedwater***	100 G1	14"	15829	590	12899	8061	27000
322B	Feedwater***	101 G1	14"	17927	13521	15432	878	27000
334B	Feedwater	102 G1	14"	16025	12281	17169	10791	27000
417	Auxiliary Feedwater	118 Al 118 A2	311	8568	NA	24530	14036	27000
607	Auxiliary Feedwater	118 G1 118 G2	411 611	18681	NA	18126 ,	5347	27000
636	Pressurizer Spray & Relief	125 Al	411	17671	9527	20304	13833	28800
630	Pressurízer Spray & Relíef	124 A1 124 A2	3", 4" 6", 12"	20500 <b>*</b> *	NA	29421	24839	30690(#)
540	Residual Heat Removal	117 Bl	3", 4" 6", 12"	14746**	3374**	19144	9020	25785
508	Resídual Heat Removal	117 Al 117 A2	10", 12", 14"	16627	12375	13203	8757	25785
465	Service Water	119 A1 119 A2 119 A3 119 A4	24"	19101	18285	6935	5826	21600
488⁄ 480	Component Cooling	112 C 112 Al	18"	26723 <b>*</b> *	NA	16263	13680	27000
507/ 481	Component Cooling	112 F1 112 B1	8'' 18''	26695**	NA	21499	19895	27000
614	Component Cooling	112 AE1 112 AE2 112 AE2	12" 18" 10", 6"	25448**	NA	20601	17575	27000
512	Component Cooling	112 AN1	18"	26792**	NA	17748	15621	27000

# TABLE 2-1 (Cont)

### PIPE STRESS REEVALUATION SUMMARY DESIGN BASIS EARTHQUAKE

Prob-					Line	3		Pipe	Stress	(psi)	
lem <u>No.</u>	Syster <u>Name</u>	n 	Iso. <u>No.</u>	- ·	Size (NPS	5)	Original <u>Total*</u>	Original <u>Seismic×</u>	New <u>Total</u>	New <u>Seismic</u>	Allow- able
603A	Component	Cooling	112	<b>S</b> 1	18"		18710	13461	5396	3554	27000
766	Component	Cooling	112 112	AR T	8"		10449**	NA	19041	17263	27000
605A	Component	Cooling	112 112	AA1 AA2	3", 18"	6",	12420	6727	20269	17990	27000 <sup>.</sup>
605B	Component	Cooling	112 112	AA1 AA2	3", 18"	6",	12420	6727	14775	11004	27000
509A/D	Component	Cooling	112	Gl	8", 18",	12" <b>,</b> 24"	26566* <del>*</del>	NA	20374	16992	27000
612	Component	Cooling	112	AKl	18"		17958**	NA	14034	9374	27000
1512	Component	Cooling	112	J	18"		26792 <b>*</b> *	NA	21455	19998	27000
2529/ 2527	Component	Cooling	112	AH	3", 8", 14",	6", 10", 18"	26701**	NA	18405	16809	27000
2526	Component	Cooling	112	AJ	2*2' 8'',	', 6", 10"	NA	NA	24840	16269	27000
517	Component	Cooling	112 112 112	M1 M2 M3	4", 8", 14",	6", 10", 18"	17958**	NA	14686	13239	27000
603B	Component	Cooling	112	S1	18"		18710	13461	5794	2624	27000
526C	Component	Cooling	112 112 112	L1 L2 L3	6" <b>,</b>	.8"	NA	NA	22573	22258	27000
527A/C	Component	Cooling	112 112	T1 T1	4", 8", 14"	6", 10",	10449**	NA	22803	21266	27000
509B	Component	Cooling	112	G2	8", 18",	12", 24"	26566**	NA	22705	19319	27000

### PIPE STRESS REEVALUATION SUMMARY DESIGN BASIS EARTHQUAKE

Prob-			Line		Pipe	Stress_	(psi)	
lem <u>No.</u>	System <u>Name</u>	Iso. <u>No.</u>	Size (NPS)	Original <u>Total*</u>	Original <u>Seísmíc*</u>	New Total	New <u>Seismic</u>	Allow- able
509C	Component Cooling	112 G3	8", 12", 18", 24"	26566**	NA	18862	16007	27000
CV1	Containment Vacuum	137 Al	8"	25750**	NA	16039	1824	27000
746	3" HP Steam	131 A1 131 B2 131 C3	3'' 4''	26766 <b>*</b> *	NA	18674	11200	27000 <sup>.</sup>
CF1	Fire Protection	144 Al	2", 6", 12"	22255 <b>*</b> *	NA	9911	8353	27000
CF2	Fire Protection	144 Bl	1 1/2", 2", 16"	10966**	3733**	5323	1190	27000
1040	Diesel Muffler Exhaust	143 Al	24"	11857 <b>*</b> *	NA	7340	6756	22500

### LEGEND:

\* Table 2-1 of Seismic Design Review Equipment and Piping Surry Power Station, September 1971, or

\*\* Subsequent reanalysis.

\*\*\* Max stress of feedwater inside reactor containment only. The flow diagram in the June 5, 1979 submittal is correct. The flow diagram in the August 1, 1979 submittal inadvertently included a small portion of feedwater. Piping outside the reactor containment is in error. Feedwater outside the reactor containment is part of the I&E 79-14 effort.

#### - TABLE 2-1 (Cont)

### PIPE STRESS REEVALUATION SUMMARY DESIGN BASIS EARTHQUAKE

Legend:

NA = Not Available

Allowable Stress = 1.8 S

New Total Stress = S + S + 1.5 S + S (for SSI/ARS)

New Seismic = 1.5 S (for SSI/ARS)

New Total Stress = S + S + S + S (original ARS)

New Seismic = S (original ARS)

### NOTE:

The original total\* and original seismic\* stresses shown in Table 2-1 were computed using SHOCK2 for the original design conditions. The new total and new seismic stresses were computed by the NUPIPE program using different mass models and, in some cases, different ARS's than the original calculations. More importantly, the reanalyses were based on field-verified, piping configurations in 1979, which, in some cases, differ significantly from the original design conditions. For this reason, the new stresses and the original stresses in Table 2-1 are not comparable, as they do not necessarily represent the same physical conditions.

DESCRIPTIVE NOTES (To explain differences between the August 1, 1979 table and table submitted in this report):

- 1. The high stress point occurs on a portion of the piping with a lower temperature therefore the higher allowable.
- 2. Pipe supports were added or modified to reduce loads on other existing supports. This stress analysis performed since the August 1, 1979 submittal.
- 3. The high stress point occurs on a portion of the piping with a higher temperature therefore the lower allowable.
- 4. In the original stress analysis both spray headers were considered as being similar therefore only one analysis made. As-built differences in pipe supports caused two separate pipe stress runs be made. This resulted in different hardware modifications due to pipe support analysis.
  - 5. System operating temperature revised therefore allowable stress changed accordingly.

6. Problem rerun with revised building displacements.

### PIPE STRESS REEVALUATION SUMMARY DESIGN BASIS EARTHQUAKE

- 7. Pipe stress problem rerun with enveloped ARS for 3-buildings. New run of record made in preparation for OBE support analysis.
- 8. Since the high stress point occurs at the point where two piping classes join, the lower allowable should be applied.

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9. Problem rerun with revised building displacements and modified NUPIPE model.

# TABLE 2-2

# NOZZLE AND PENETRATION SUMMARY SHOCK 2 PROBLEMS DESIGN BASIS EARTHQUAKE

System and <u>Prob. No.</u>	Total No. of Nozzles/ <u>Penetrations</u>	No. Accep- table Evaluation <u>(Complete)</u>	No. Under Evaluation	Modifi- cations or Additions <u>Required</u>	Vendor Confirmation Being Obtained
Low Head Safety <u>Injection</u>	· .				
555	1	1	0	0	Confirmed
1555	1	1	0	0	Confirmed
706A	0	NZA	N/A	N/A	N/A
707A	0	NZA	NZA	N/A	NZA
708	0	N/A	N/A	N/A	N/A
731A	0	N/A	NZA	N/A	N/A
731B	0	NZA	NZA	N/A	NZA
743	0	NZA	N/A	NZA	N/A
727	2	2	0	0	Confirmed
Hígh Head Safety <u>Injectíon</u>	•			`	
735	3	3	0	0	Confirmed
Containment Recirculation <u>Spray</u>			·		
525A/1525A	0	N/A	NZA	NZA	N/A
546/560	1	. 1	0	0	NZA
546/5600	0	N/A -	NZA	N⁄A	NZA
546/5620	0	N/A	N/A	N/A	N/A -

### NOZZLE AND PENETRATION SUMMARY SHOCK 2 PROBLEMS DESIGN BASIS EARTHQUAKE

System and <u>Prob. No.</u>	Total No. of Nozzles/ <u>Penetrations</u>	No. Accep- table Evaluation <u>(Complete)</u>	No. Under <u>Evaluation</u>	Modifi- cations or Additions <u>Required</u>	Vendor Confirmation Being Obtained
548C	1	1	0	0	N/A
547	· 0	NZA	N/A	N/A	N/A
744/754	1	1	0	0	Confirmed
548A	0	NZA	NZA	N⁄A	N/A
548B	1	1	0	0	N/A
544	2/2	2/2	0/0	0/0 .	N/A
544A	2	2	0	0	Confirmed
544B	. 2	2	0	0	Confirmed
751	2	2	0	0	N/A
562	1	1	0	. <b>O</b>	N/A
745	1	1	0	0	Confirmed
<u>Main Steam</u>			,		
323A	. 1/1	1/1	0/0	0/0	N/A
322A	1/1	1/1	0/0	0/0	N/A
334A	1/1	1/1	0/0	0/0	N/A
346	0/0	N⁄A	N/A	N/A	N/A
Feedwater					
323B	1/1	1/1	010	0/0	N/A
322B	1/1	1/1	0/0	0/0	N/A
334B	1/1	1/1	0/0	0/0	N/A

## NOZZLE AND PENETRATION SUMMARY SHOCK 2 PROBLEMS DESIGN BASIS EARTHQUAKE

System and <u>Prob. No.</u>	Total No. of Nozzles/ <u>Penetrations</u>	No. Accep- table Evaluation <u>(Complete)</u>	No. Under <u>Evaluation</u>	Modífi- cations or Additions <u>Required</u>	Vendor Confirmation Being <u>Obtained</u>
Aux. Feedwater	:	• .			
417	0	N/A	N⁄A	NZA	NZA
607	3	3	0	0	Confirmed
Pressurizer Spray & Relief	•				
636	1	1	0	0	Confirmed
630	5	5	0	0	Confirmed
Residual Heat <u>Removal</u>			·		
540	· 1	1	0	0	Confirmed
508	8	8	0	0	Confirmed
Service Water	,				
465	4	4	0	0	N/A
<u>Component Coolin</u>	g				
488/480	4	4	0	0	N/A
507/481	4	4	. 0	0	N/A
614	0	NZA	NZA	NZA	N⁄A
512	0	NZA	N/A	N⁄A	NZA
603A	1	1	0	. 0	Confirmed
766	2	2	0	0	NZA
605A	3	3	· 0	0	Confirmed

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# NOZZLE AND PENETRATION SUMMARY SHOCK 2 PROBLEMS DESIGN BASIS EARTHQUAKE

System and <u>Prob. No.</u>	Total No. cf Nozzles/ <u>Penetratíons</u>	No. Accep- table Evaluation <u>(Complete)</u>	No. Under <u>Evaluation</u>	Modifi- cations or Additions <u>Required</u>	Vendor Confirmation Being <u>Obtained</u>
605B	3	3	0	0	Confirmed
509A/D	. 3	3	0	0	N/A
612	2	2	0	0	Confirmed
1512	0	N⁄A	N⁄A	NZA	N/A
2527/2529	2	2	0	0	Confirmed
2526	0	N⁄A	NZA	N/A	NZA
527A/C	2	2	0	0	Confirmed
517	4	4 .	0	0	Confirmed
603B	1	1	0	0	Confirmed
526C	0	NZA	. NZA	NZA	NZA
509B	0	NZA	N/A	N∕A	N/A
509C	0	NZA	N/A	N/A	N/A
Containment <u>Vacuum</u>					
CV1	0	N/A	NZA	N/A	NZA .
<u>3" HP Steam</u>					
746	1	1	0	0	Confirmed
Fire Protection					
CF-1	0	N/A	N/A	NZA	NZA
CF-2	0	N/A	NZA -	NZA	NZA

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### NOZZLE AND PENETRATION SUMMARY SHOCK 2 PROBLEMS DESIGN BASIS EARTHQUAKE

System and Prob. No.	Total No. of Nozzles/ <u>Penetrations</u>	No. Accep- table Evaluation <u>(Complete)</u>	No. Under <u>Evaluation</u>	Modifi- cations or Additions <u>Required</u>	Vendor Confirmation Being Obtained
Diesel Muffler Exhaust					
1040	3	3	0	0	NZA

N/A = not applicable

# TABLE 2-3

# PIPE STRESS HARDWARE MODIFICATION SUMMARY

Problem <u>No.</u>	MKS <u>No.</u>	System	Overstressed Condition	Attributable	Resolution
334B	102G1,G2	FW	Thermal overstress	As-Built	Delete U-Bolt**
508	117A1	RHR	DBET overstressed RHR pump Discharge elbows and overloaded nozzles.	Seísmíc Reanal <b>ysís</b>	Six supports added to alleviate overstress condition.
540	117B1	RHR	<ol> <li>Thermal overstress due to support which was not included in original analysis.</li> </ol>	As-Built .	1. Delete NS & RH's.
			<ol> <li>Overstress in 2" line which was not included in original analysis.</li> </ol>		2. Add Anchor to 2" line.
548A	123B1	C&RS	DBEI overstress condition	As-Built	Addition of a horizontal snubber.
562	123E2	C&RS	DBEI overstress	As-Built	Addition of EW. Replace RH with SH. Replace SH with VC.
727	12701	LHSI	DBEI overstress	Seismic Reanalysis	Addition of an LSS.
735	127G1	HHSI	DBEI overstress	As-Built	Addition of two guides.
743	127F1	LHSI	DBEI overstress	As-Built	Shim existing constraint to VC/LC.
744/754	123J1	C&RS	DBEI overstress	As-Built	Modification and re- placement of constraints to reflect original analysis.
745	123K1	C&RS	DBEI overstress	As-Built	Modification and re- placement of constraints to reflect original analysis.
746	131A1 B2 C3	HP Steam	DBEI overstress	As-Built	Modification and addition of constraints to reflect original analysis.

### TABLE 2-3 (Cont)

### PIPE STRESS HARDWARE MODIFICATION SUMMARY

Problem <u>No.</u>	MKS <u>No.</u>	System		Overstressed Condition	Attributable To:	Resolution
488/480	122A1,C1	CCW	DBEI	overstress	As-built *	Add two guides to Problem 480 and two lateral restraints to Problem 488.
507/481	112B1,F1	CCW	DBEI	overstress	As-built *	Add two guides to Problem 481.
509A/D	112G	CCW	DBEI	overstress	As-built	Added one vertical restraint.
517	112M	CCW	DBEI	overstress	As-buílt Seísmíc Reanalysís	Seven restraint changes are required.
526C	112L	CCW	DBEI	overstress ,	Seismic Reanalysis	Added a lateral restraint and modify an SH to a rigid vertical constraint.
527A/C	112T	CCW	DBEI	overstress	As-built	Delete anchor A36 and shim supports.
605A	112AA	CCW	DBEI	overstress	As-built	Add four lateral ' restraints.
766	112AR	CCW	DBEI overs	overstress and thermal stress	As-built	Add horizontal guides and delete an axial restraint.
2527/2529	112	CCW	DBEI	overstress	As-built	Delete anchor and shim supports.

### NOTES:

\* The use of ARS curves causes higher acceleration levels than the procedure for below-grade structures formerly used as described in the Seismic Design Review revised September 15, 1971.

\*\* Due to Branch-Line Analysis

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RHR = Residual Heat Removal CCW = Component Cooling Water SH = Spring Hanger	
C&RS = Containment & Recirculating Spray System NS = North-South Constraint VC = Vertical Constra	int
LHSI = Low Head Safety Injection RH's = Rod Hangers LC = Lateral Constrai	nt
HHSI = High Head Safety Injection EW = East-West Constraint	

### TABLE 2-4

### HARDWARE MODIFICATION SUMMARY DUE TO NOZZLE AND PENETRATION OVERLOADING

Problem <u>No.</u>	<u>Overstress No.</u>	Attributable <u>To:</u>	Resolution
746	1-FW-P-2 inlet nozzle	As-Buílt⁄ thermal	Add vertical shock suppressor
746	l-FW-P-2 inlet nozzle	As-Built/ thermal	Add vertical shock suppressor
746	1-FW-P-2 inlet nozzle	As-Buílt/ thermal	Add spring hanger
746	1-FW-P-2 inlet nozzle	As-Buílt/ thermal	Add north/south shock suppressor
746	l-FW-P-2 inlet nozzle	As-Built/ thermal	Replace LC by spring hanger
746	1-FW-P-2 inlet nozzle	As-Built/ thermal	Add spring hanger
322B	Feedwater penetration	Seísmic reanalysis	Add guide
323B	Feedwater penetration	Seismic reanalysis	Add guide
334B	Feedwater penetration	Seísmic reanalysís	Add guide

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### SECTION 3

### PIPE SUPPORT RESULTS.

Tables 3-1A and 3-1B summarize the pipe supports evaluated in the reanalysis program. There are 944 supports (487 inside containment, 457 outside containment) on lines originally analyzed by SHOCK 2. All 944 pipe supports have been reanalyzed, and 137 pipe support hardware modifications have been identified. The modifications identified, due to pipe support analysis, are listed in Table 3-2.

In cases where SSI-ARS was used, the DBE seismic inertial reactions on supports are multiplied by 1.5. Anchor movements are not considered in the calculation of support stresses for the DBE conditions.

# TABLE 3-1A

# PIPE SUPPORT STATUS SUMMARY INSIDE CONTAINMENT - SHOCK 2

System and <u>Prob. No.</u>	Total No. of Supports	No. Accep- table (Evaluation <u>Complete)</u>	n No. Under <u>Evaluation</u>	Modifica- tions or Additions <u>Required</u> <u>Comme</u>	<u>nt</u>
Low Head Safety <u>Injection</u>				• •	
555	14	14	-	4	
706A	10	10	·· <del>-</del>	-	
707A	9	9	_	· –	
708	. 22	22	-	3	
1555	9	9	-	-	
Containment and Recircu- <u>lation Spray</u>					
525A/1525A	35	35	-	5	
544	12	12	-	2	
544A	6	. 6	-	-	
544B	6	6	-	1	
546/560	18	18	<u> </u>	6	
546/5600	11	11	_	2	
546/5620	11	11		1	
547	13	13	-	_	
548A	2	2	-	-	
548B	22	22	-	. 4	
548C	25	25	-	2	
562	19	19	· _	5	

# TABLE 3-1A (Cont)

### PIPE SUPPORT STATUS SUMMARY INSIDE CONTAINMENT - SHOCK 2

System and <u>Prob. No.</u>	Total No. of 	No. Accep- table (Evaluation <u>Complete)</u>	No. Under <u>Evaluation</u>	Modifica- tions or Additions <u>Required</u>	<u>Comment</u>
Main <u>Steam</u>	• •				
322A	5	5	~ .	-	
323A	17	17	-	<b>-</b> .	
334A	3	3	-	. –	
Feedwater					
322B	8	8	-	-	
323B	14	14	-	-	
334B	8	8	-	1	
Auxiliary <u>Feedwater</u>					
417	26	26		_	
Pressurizer Spray and <u>Relief</u>					
630	27	27	-	-	
636	33	33	-	1	
Residual Heat <u>Removal</u> ,		•			
508	50	50	-	3	
540	. 10	10	-	-	
<u>Service Water</u>					
465	8	8	-	1	

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# TABLE 3-1A (Cont)

# PIPE SUPPORT STATUS SUMMARY INSIDE CONTAINMENT - SHOCK 2

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System and Prob. No.	Total No. of <u>Supports</u>	No. Accep- table (Evaluation _Complete)	No. Under <u>Evaluation</u>	Modifica- tions or Additions <u>Required</u>	<u>Comment</u>
Component <u>Cooling</u>					
603A	7	7	-	3	
603B	5	. 5	-	2	
605A	17	17		3	
605B	10	10	-	2	
*					

### TABLE 3-1B

### PIPE SUPPORT STATUS SUMMARY OUTSIDE CONTAINMENT - SHOCK 2

System and Prob. No.	Total No. of 	No. Accep- table (Evaluation <u>Complete)</u>	No. Under <u>Evaluation</u>	Modífica- tions or Addítions <u>Required</u>	Comment
Low Head Safety <u>Injection</u>	,				
727	21	21	<b>_</b> ·	-	
731A	4	4	-	3	
731B	4	4	-	2	
743	5	5	-	-	
High Head Safety <u>Injection</u>					
735 3 Containment and Recircu- <u>lation Spray</u>	43	43	-	4	
744/754	10	10	-		
745	8	8	-	1	
751	6	6	-		
<u>Main Steam</u>		,			
346	54	54	·•• _	-	
Auxiliary Feedwater					
607	15	15	-	1	

# TABLE 3-1B (Cont)

# PIPE SUPPORT STATUS SUMMARY OUTSIDE CONTAINMENT - SHOCK 2

System and <u>Prob. No.</u>	Total No. of	No. Accep- table (Evaluation <u>Complete)</u>	No. Under Evaluation	Modifica- tions or Additions <u>Required</u>	<u>Comment</u>
Component Cooling					
488/480	26	26	<b>_</b>	5	
507/481	20	20	-	4	
509A/D	. 27	27	-	9	
509B	6	6	<u> </u>	3	
509C	2	2	_	-	
512	• 5	5		3	
517	34	34	-	. 7	
526C	11	11	-	3	
527A/C	13	13	-	3	
612	15	15	-	1	
614	14	14	-	8	
766	17	17	-	6	
1512	6	6	-	3	
2526	11	11	-	5	
2527/2529	. 14	14	-	4	
Containment <u>Vacuum</u>					
CV1	3	3	-	1	
<u>3" HP Steam</u>					
746	19	19	-	-	

### TABLE 3-1B (Cont)

### PIPE SUPPORT STATUS SUMMARY OUTSIDE CONTAINMENT - SHOCK 2

System and Prob. No.	Total No. of Supports	No. Accep- table (Evaluation <u>Complete)</u>	No. Under <u>Evaluation</u>	Modifica- tions or Additions <u>Required</u>	Comment
Fire Protec- tion	· ·				
CF1	10	10	-	5	
CF2	4	4	-	2	
<u>Diesel Muffler</u>					
1040	18	18	-	3	

### NOTES:

The number in the "Modifications" or "Additions" column are already included in the status shown in the "Acceptable (Complete)" column.

The number in the "Total Supports" column equals the number in the "Acceptable" plus the number in the "Under Evaluation" column.

The number in the "modifications" or "additions" columns does not include "modifications" or "additions" due to stress, nozzle/penetration, branch line analysis.

# TABLE 3-2

# PIPE SUPPORT HARDWARE MODIFICATION SUMMARY

Problem <u>No.</u>	Support	Description of Modification or <u>Overstressed Condition</u>	Modified Since August 21, 1979 Submittal	Attributable	Resolution
334B	PT 90	Snubber modification	No	Seismíc Reanalysis	Add horizontal shock suppressor.
465	H-21	Support member overstressed	No	As-built	Removed Support H-21.
508	H-42A	Snubbers over allowable	No	Seismic Reanalysis	Add horizontal snubber.
508	PT 26	Snubbers over allowable	No	Seísmíc Reanalysis	Add horizontal and vertical snubbers.
508	H-20	Weld over allowable	No	As-built	Modify support.
525A	H14	Prevents growth in one direction	No	As-built	Modify support.
525A	Н70	Support overloaded	No	As-built	Modífy support.
544	H34A	Overstressed with new loads	No	As-built	Redesigned and modified to VC-LC.
544	Н37А	Overstressed with new loads	No	As-built	Redesigned and modified to VC-LC.
544B	H46	Weld over stress allowable	No	As-built	Support modified.
548B	H87	No lateral restraint capability	No	As-built	Redesigned and modified support to receive lateral load.
548B	H72A H72B	6-way restraint not properly functioning	No	As-built	Redesigned (modified to 3-way restraint).
548B	H84	No lateral movement due to thermal and seismic	No	As-built	Restore to original configuration.
548B	H18A H18B	U-bolts overstressed	No	As-built	Redesigned and modified support by adding bracing member.
548C	H17A H17B H17C	Lugs overstressed on gang hanger - anchor	Νο	As-built	Redesigned and modified by removing attachments to relieve pipe overstress conditions.
548C	Н75	U-bolt subjected to lateral loads over allowable loads	No	As-built	Replace U-bolt with framed member.

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### TABLE 3-2 (Cont)

### PIPE SUPPORT HARDWARE MODIFICATION SUMMARY

Problem No,	Support No.	Description of Modification or Overstressed Condition	Modified Since August 21, 1979 Submittal	Attríbutable To:	Resolution
555	H10	Integral attachment overstressed	No	Seísmic Reanalysis	Add lateral shock suppressor.
555	H28	Horizontal and vertical structural member restraining pipe movement	No 3	Thermal Movement	Restore to original intent.
555	Н29	Vertical member restraining pipe motion	No	Thermal movement	Restore to original intent.
555	Н30	Vertical member restraining pipe motion	No	Thermal movement	Restore to original intent.
546/560	НЗ9Л НЗ9В	Integral attachment over- stressed for support H39A	No	As-built	Replace anchor by a 3-way restraint.
546/560	PT-185	Added due to H39A	No	As-built	Add vertical shock suppressor to reduce loads.
546/560	PT-208	Added due to H39A	No	As-built	Add lateral constraint.
546/560	PT-130	Added due to H39A	No	As-built	Add lateral constraint and vertical constraint.
546/560	PT-216	Added due to H39A	No	As-built	Add lateral constraint.
546/560	PT-310	Added due to H39A	No	As-built	Add lateral constraint.
562	Н26	Modified due to H39B. Inte- gral attachment overstressed for H39B.	Йо	As-built	Modify support by adding U-bolt.
562	H29A H29B	Modified due to H39B. Inte- gral attachment overstressed for H39B.	No	As-built	Modify 2-way support to 3-way support.
562	PT-265	Added due to H39B. Integral attachment overstressed for H39B.	No	As-built	Add lateral constraint. Reduce loads at anchor point.
562	PT-340	Modified due to H39B. Inte- gral attachment overstressed for H39B.	No	As-built	Modífy vertical constraint.

# • TABLE 3-2 (Cont)

### PIPE SUPPORT HARDWARE MODIFICATION SUMMARY

Problem <u>No.</u>	Support <u>No.</u>	Description of Modification or <u>Overstressed Condition</u>	Modified Since August 21, 1979 Submittal	Attributable To:	Resolution
562	PT-183	Added due to H39B. To reduce load on hanger H39B.	No	As-built	Add 2-way support.
546/5600	H15B	U-bolt modified to reduce loads on H17B	No	Seísmíc Reanalysís	Redesigned and modified ganghanger from 1-way (LC).
546/5600	PT-155	Added to reduce anchor loads	No	Seismic Reanalysis	Add LC-VC to reduce loads at anchor.
546/5620	PT-230	Added to reduce anchor loads	Νο	Seísmíc Reanalysís	Add LC-VC to reduce loads.
636	Н36	Plate overstressed	No	As-built	Modify anchor by adding gusset.
708	PT-1	Lateral load on U-bolt overstressed	No	As-built	Add lateral restraint.
708	H127	Member overstressed	No	As-built	Modify support to vertical and lateral constraint.
708	PT-380	Lateral restraint over- stressed	No	As-built	Modify support to vertical and lateral constraint.
1525A	PT-5000	Delete due to H-2	No	Seísmic Reanalysis	Delete axial support and 1-way LC to reduce anchor load.
1525A	PT-8000	U-bolt and frame over- stressed	No	Seismic Reanalysis	Modify frame.
1525A /	PT-5802	Hanger overloaded	No	Seísmic Reanalysís	Modify support.
603A	3,	Pipe straps overstressed	No	As-built	Add gussets to all and increase weld size.
603A	7	Pipe straps overstressed	Νο	As-built	Add gussets to all and increase weld size.
603A	5	Vertical restraint only re- quired, but support had	No .	As-built	Modify support to provide lateral clearance.

# TABLE 3-2 (Cont)

# PIPE SUPPORT HARDWARE MODIFICATION SUMMARY

Problem No.	Support <u>No.</u>	Description of Modification or <u>Overstressed Condition</u>	Modified Since August 21, 1979 Submittal	Attríbutable <u>To:</u>	Resolution
603B	13	Uplift restraint is re- quired, but support had negative vertical restraint only.	No :	As-built	Modify support to provide uplift restraint.
603B	10	Vertical support only re- quired, but support is a vertical restraint and lateral restraint.	No	As-built	Remove top and side members of support.
605B	4	Support members overstressed	Νο	As-built	Replace two W4x13 members with TS4x4x1/2.
605B	Н-2	Lateral clearance insufficient	Νο	Thermal movement	Modify restraint.
605A	PT-13	Need vertical restraint	No	As-built	Modify vertical support.
605A	2020	Delete lateral restraint	No	As-Built	Modify support.
605A	2005	Delete lateral restraint	No	As-Built	Modify support.
607	PT 335	U-Bolt overstressed	No	As-Built	Delete U-Bolt.
731A	SI-C-90	Support member overstressed	No	Seismíc Reanalysís	Add structural brace.
731A	PT 46	Integral attachment over- stressed	No	Seismic Reanalysis	Add N-S restraint. Gang Hanger Problem #731B Point #44.
731B	SI-C-91	Support member overstressed	No	Seismic Reanalysis	Add structural brace.
745	PT 45	Support overstressed	No	As-Built	Modify support.
731A	PT 38	Support overstressed	No	Seismic Reanalys <b>is</b>	Modífy support.
731B	PT 36	Support overstressed	No	Seismic Reanalysis	Modify support.
735	PT 20	Support overstressed	No	As-Built	Modify support.

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SURRY POWER STATION, UNIT 1

# TABLE 3-2 (Cont)

# PIPE SUPPORT HARDWARE MODIFICATION SUMMARY

Problem <u>No.</u>	Support <u>No.</u>	Description of Modification or <u>Overstressed Condition</u>	Modified Since August 21, 1979 Submittal	Attributable	Resolution
735	PT 35	Support overstressed	No	As-Built	Modify support.
735	PT 50	Support overstressed	No	As-Built	Modify support.
735	PT 60	Ganged support overstressed	Note 2. Yes	As-Built	Modify support.
480/488	1	Integral attachment	Note 1. Yes	Seismic Reanalysis	Modify support by adding welds.
480/488	2,10,16 Gang	Weld overstressed	Note 1. Yes	Seismic Reanalysis	Modify support by adding welds.
480/488	3,11,17 Gang	Integral attachment overstressed	Note l. Yes	Seismíc Reanalysis	Modify support by increasing trunnion size.
507	1	Integral attachment overstressed	Note 1. Yes	Seismic Reanalysis	Modify support by remoding trunnion and adding frame.
507	4 <b>,9,</b> 15 Gang	Support overstressed	Note 1. Yes	As-Buílt	Modify support by replacing u-bolt and adding new members.
507	5,10,16 Gang	U-bolt overstressed	Note 1. Yes	Seismic Reanalysis	Modify support by adding stiffners.
507	6,11,17 Gang	Support members and weld overstressed	Note 1. Yes	Seismic Reanal <b>ysis</b>	Modify support by replacing U-bolt and adding new members.
509AD	5	U-bolt and weld over- stressed	Note 1. Yes	As-Built	Modify support by replacing U-bolt and adding frame.
509AD	7	U-bolt and support . overstressed	Note 1. Yes	Seísmic Reanalysís	Modify support by redesigning.
509AD	8,9,13	Support overstressed (ganged with H5, Pro. #517, H5, Pro. #1512)	Note 1. Yes	Seísmíc Reanalysís	Modify support by replacing vs with vc.
509AD	15	U-bolt and support overstressed	Note 1. Yes	Seismic Reanalysis	Modify support by adding strut.
509AD	4,20, 24,42	Uplift restraint required	Note 1. Yes	Seismic Reanalysis	Modify support by vs with vc.

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# SURRY POWER STATION, UNIT 1

# TABLE 3-2 (Cont)

# PIPE SUPPORT HARDWARE MODIFICATION SUMMARY

Problem No.	Support <u>No.</u>	Description of Modification or <u>Overstressed Condition</u>	Modified Since August 21, 1979 Submittal	Attributable	Resolution
509AD	22	Support overstressed	Note 1. Yes	Seismíc Reanalysís	Modify support by removing trunnion and providing frame.
509AD	47	Support overstressed	Note 1. Yes	As-Built	Modify support by adding new sliding plate.
509AD	44	Uplift restraint required	Note 1. Yes	Thermal Movement	Modify vc to vs.
509AD	45,46	Support overstressed	Note 1. Yes	Seísmic Reanalysis	Modify support to provide uplift restraint.
517	1	Integral welded attachments overstressed	Note 1. Yes	Seísmíc Reanalysís	Add pad, add braces.
517	16	Integral attachments overstressed	Note 1. Yes	Seísmíc Reanalysís	Modify support by relocating trunnion.
517	21	Support overstressed	Note 1. Yes	Seísmíc Reanalysís	Modify support by adding stiffeners.
517	22	Support member over- stressed.	Note 1. Yes	Seismic Reanalysis	Modify support.
517	25	Support overstressed	Note 1. Yes	Seismic Reanalysis	Replace RM with strut.
517	27	Support overstressed	Note 1. Yes	Seismic Reanalysis	Replace rod hanger by sway strut.
517	28,35	Weld overstressed	Note 1. Yes	As-Built	Modify support by adding brace.
526C	4	Support overstressed (ganged with H8 Pro. #527AC)	Note 1. Yes	As-Built	Modify support by adding stiffeners.
526C	6	Integral attachment overstressed	Note 1. Yes	Seísmic Reanalysis	Replace support by clamp anchor assembly.
526C	11	Integral attachment overstressed	Note 1. Yes	Seísmic Reanalysis	Modify support by relocating trunnion.
527AC	1	Support member over- stressed	Note 1. Yes	Seísmíc Reanalysis	Modify support by adding base plates.

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# TABLE 3-2 (Cont)

# PIPE SUPPORT HARDWARE MODIFICATION SUMMARY

Problem No.	Support No.	Description of Modification or <u>Overstressed Condition</u>	Modified Since August 21, 1979 Submittal	Attributable To:	Resolution
527AC	3	U-bolt overstressed	Note 1. Yes	As-Built	Modify support by replacing u-bolt and adding frame.
527AC	4	Support overstressed	Note 1. Yes	Seismic Reanalysis	Modífy support.
1512	3	Support overstressed	Note 1. Yes	Seismic Reanalysis	Add sway strut for side load.
1512	6	Support overstressed	Note 1. Yes	Seísmíc Reanalysís	Modify support by replacing U-bolt.
1512	7	Support overstressed	Note l. Yes	Seísmíc Reanalysis	Modify support by adding plates.
2527	3	U-bolt overstressed	Note 1. Yes	Seismic Reanalysis	Modify support by replacing U-bolt and adding welded frame.
2527	5	Support overstressed	Note 1. Yes	Seísmic Reanalysis	Replaced with new support.
2527	7	U-bolt overstressed	Note 1. Yes	Seísmic Reanalysis	Modify support by replacing U-bolt.
2529	13	Clevís overstressed	Note 1. Yes	Seísmic Reanalysis	Replace clevis with rod and clamp.
1040	PT 57	Additional support	Note 1. Yes	As-Built	Add l vertical snubber Diesel 1.
	PT 57	Additional support	Note 1. Yes	As-Buílt	Add 1 vertical snubber Diesel 2.
	PT 57	Additional support	Note 1. Yes	As-Built	Add 1 vertical snubber Diesel 3.
CVI	PT 38	Support overstressed	Note 1. Yes	As-Built	Modífy support.
CF-1	1	Bolts and structure overstressed	Note 1. Yes	Seísmíc Reanalysis	Add brace (S&W) increase weld size.
	2	Support overstressed	Note 1. Yes	Seismic Reanalysis	Sway struts added.
	5	Uplift problem	Note 1. Yes	Seismic Reanalysis	Remove angle, add sway strut.

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SURRY POWER STATION, UNIT 1

# TABLE 3-2 (Cont)

# PIPE SUPPORT HARDWARE MODIFICATION SUMMARY

Problem <u>No.</u>	Support	Description of Modification or <u>Overstressed Condition</u>	Modified Since August 21, 1979 Submittal	Attributable	Resolution
	13	Uplift problem	Note l. Yes	Seísmíc Reanalysís	Replace rod hanger with sway strut.
	14	Uplift problem	Note 1. Yes	Seismic Reanalysis	Replace rod hanger with sway strut.
CF-2	2	U-bolt overstressed	Note 1. Yes	Seismíc Reanalysis	Replace with frame.
	4	Weld overstressed	Note 1. Yes	Seísmíc Reanalysis	Added weld and gusset plater.
488	21	Improper support	Note 1. Yes	Seísmic Reanalysís	Add baseplate and shims.
	22	Weld and bolts overstressed	Note 1. Yes	Seísmíc Reanalysis	Increase weld, add brace (S&W).
509B	6	Weld overstressed	Note 1. Yes	Seismíc Reanalysís	Increase weld.
·	19	Integral welded attachment overstressed	Note 1. Yes	Seïsmic Reanalysis	Add pad, brace (S&W).
	28	U-bolt overstressed	Note 1. Yes	Seísmic Reanalysís	
512	3	Structure, weld and U-bolt overstressed	Note 1. Yes	Seísmic Reanalysis	Remove support, add frame w/brace.
	6	Structure, weld and U-bolt overstressed	Note 1. Yes	Seísmíc Reanalysís	Modífy support, rémove support, add frame.
·	8	Integral welded attachment overstressed	Note 1. Yes	Seismic Reanalysis	Add pad, add braces.
612	4	Structure and weld over- stressed	Note 1. Yes	Seismic Reanalysis	Shorten stanchion.
614	1	Structure overstressed ganged with H27 Pro. #509B	Note 1. Yes	Seísmic Reanalysis	
	2	Structure and U-bolt	Note 1. Yes	Seismic	Replace U-bolt w/frame, add brace.

# TABLE 3-2 (Cont)

# PIPE SUPPORT HARDWARE MODIFICATION SUMMARY

Problem <u>No.</u>	Support <u>No.</u>	Description of Modification or <u>Overstressed Condition</u>	Modified Since August 21, 1979 Submittal	Attributable To:	Resolution
		overstressed		Reanalysís	
	. 5	Support structure over- stressed (ganged with H31, Pro. #509B, H7 Pro. #512)	Note l. Yes	Seismic Reanalysis	Revise IWA; add lateral brace and closure plate to column.
	7	Structure and U-bolt overstressed	Note 1. Yes	Seismic Reanalysis	Replace U-bolt w/beams, add brace.
	8	Improper support	Note 1. Yes	As-Built	Restrain pipe in correct direction.
	9	Structure overstress	Note 1. Yes	Seísmíc Reanalysís	Add gussets.
	10	Integral welded attachment overstressed	Note 1. Yes	Seismic Reanalysis	Replace exist. support w/1WA and frame to floor.
	13	Uplift restraint required	Note 1. Yes	Seismic Reanalysis	Replace vs by vc.
766	5	Support structure and weld overstressed (ganged with H39, Pro. #517)	Note 1. Yes	Support Reanalysis	Modífy support.
	7	Support, structure over- stress (ganged with H32, Pro. #517)	Note 1. Yes	Support Reanalysis	Modífy support.
	8	Support uplift over- stress problem (ganged with H33, Pro. #517)	Note 1. Yes	Support Reanalysis	Modify support.
	9	Support weld overstressed and uplift (ganged with H34, Pro. #517)	Note 1. Yes	Support Reanalysis	Reanalyzed and restrain uplift.
	14	U-bolt, welds and structure overstressed	Note 1. Yes	Support Reanalysis	Remove U-bolt, add frame and brace.
	15	Structure and weld over- stress	Note 1. Yes	Support Reanalysis	Add braces.

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### TABLE 3-2 (Cont)

### PIPE SUPPORT HARDWARE MODIFICATION SUMMARY

Problem <u>No.</u>	Support	Description of Modification or <u>Overstressed Condition</u>	Modified Since August 21, 1979 Submittal	Attributable To:	Resolution
2526	1	Support overstress (ganged with H4, Pro. #512, H2, Pro. #2529)	Note l. Yes	Seísmíc Reanalysis	Modify support.
	6	Integral welded attachment overstressed	Note 1. Yes	Seísmic Reanalysís	Add pad.
	9	Uplift problem	Note 1. Yes	Seismic Reanalysis	Replace rod hanger with sway strut.
	18	Vertical, lateral, axial restraint required by pipe stress due to H2O overstress	Note l. Yes	Seismic Reanal <b>ysis</b>	Replace rod hanger w/frame, add lugs to modified support.
	20	Integral welded attachment overstressed	Note 1. Yes	Seismic Reanalysís	Rerun NUPIPE revise H18, and replace IWA w/(2) IWAs.

### NOTES:

Modification outside containment.
 Modified prior to interim operation as required per August 22, 1979 order.

# APPENDIX A

# CROSS REFERENCE OF MKS, FM, FP, PROBLEM NO., SYSTEM

# APPENDIX A

# CROSS REFERENCE OF MKS, FM, FP, PROBLEM NO., SYSTEM

<u>MKS</u>	FM	<u>FP</u>	<u>Problem</u>	System
100D1 101D1 102D1 103A1 103A2	1148-FM-14 11448-FP-1 11448-FM-14 11448-FM-14 11448-FM-14	11448-FP-1 11448-FP-1 11448-FP-1 11448-PP-1 11448-PP-1 11448-PP-1	323A 322A 334A 346 346	Maín Steam Maín Steam Maín Steam Maín Steam Maín Steam
131A1 131B2 131C3	11448-FM-14 11448-FM-14 11448-FM-14	11448-FP-5 11448-FP-5 11448-FP-5	746 746 746	3" Hígh Press Steam 3" High Press Steam 3" Hígh Press Steam
100G1 101G1 102G1	11448-FM-18 11448-FM-18 11448-FM-18	11448-FP-2 11448-FP-2 11448-FP-2	323B 322B 334B	Feedwater Feedwater Feedwater
118A1 118A2 118G1 118G2	11448-FM-18 11448-FM-18 11448-FM-18 11448-FM-18	11448-FP-2 11448-FP-2 11448-FP-2 11448-FP-2 11448-FP-2	417 417 607 607	Aux Feedwater Aux Feedwater Aux Feedwater Aux Feedwater
119A1 119A2 119A3 119A4	11448-FM-21 11448-FM-21 11448-FM-21 11448-FM-21	11448-FP-4 11448-FP-4 11448-FP-4 11448-FP-4	465 465 465 465	Service Water Service Water Service Water Service Water
112A1 112B1 112C1 112F1 112G2 112G3 112G3 112G4 112J1 112L1 112L2 112L3 112L1 112L2 112L3 112M1 112M2 112M1 112T1 112T2 112T3 112A1 112AA1 112AA2	11448-FM-22 11448	11448-FP-16 11448-FP-16	480 481 448 507 509AD 509B 509C 509AD 1512 526C 526C 526C 526C 517 517 517 517 603A&B 527A/C 527A/C 605A&B	Component Cooling Component Cooling

# APPENDIX A (Cont)

CROSS REFERENCE OF MKS, FM, FP, PROBLEM NO., SYSTEM

<u>_MKS</u>	FM	FP	Problem	System
112AE1 112AE2 112AH1 112AH2 112AJ1 112AJ2 112AK1 112AK1 112AK1 112AK1 112AK1 112AK1 112AK1 112AK1 112AK1 112AK1 122K1 122K1 122K1 122K1 122K1 122C1 127C1 127C2 127E1 127F1	11448-FM-22 11448-FM-22 11448-FM-22 11448-FM-22 11448-FM-22 11448-FM-22 11448-FM-22 11448-FM-22 11448-FM-22 11448-FM-22 11448-FM-22 11448-FM-106 1148-FM-106 1148-FM-106 1148-FM-106 1148-FM-106 1148-FM-106 1148-FM-106 1148-FM-106 1148-FM-106 1148-FM-106 1148-FM-106 1148-FM-106 1148-FM-106 1148-FM-106 1148-FM-106 1148-FM-106 1148-FM-106 1148-FM-106 11	11448-FP-16 11448-FP-16 11448-FP-16 11448-FP-16 11448-FP-16 11448-FP-16 11448-FP-16 11448-FP-16 11448-FP-16 11448-FP-16 11448-FP-3, 10 11448-FP-3, 10 11448-FP-3, 10 1448-FP-60 11448-FP-60 11448-FP-5, 10 11448-FP-5, 10 11448-FP-5, 10	614 614 2529 2529 2526 2526 617 2527 512 766 766 555 706A 707A 707A 707A 707A 707A 7555 727 727 727 731A 731B 743	Component Cooling Component Cooling Low Head Safety INJ Low Head Safety INJ
127G1 127G2	11448-FM-105, 106 11448-FM-105, 106	11448-FP-10 11448-FP-10	735 735	High Head Safety INJ High Head Safety INJ
123A1 123A2 123B1 123C1 123C1 123C1 123E1 123F2 123F1 123F2 123F3 123G1 123G2 123H1 123H2 123H1 123H1 123N1 123N1 123N1 123R1 123R2	11448-FM-101A 11448-FM-101A 11448-FM-101A 11448-FM-101A 11448-FM-101A 11448-FM-101A 11448-FM-101A 11448-FM-101A 11448-FM-101A 11448-FM-101 1148-FM-101 1148-FM-101 1148-FM-101 1148-FM-101 1148-FM-101	11448-FP-13 11448-FP-13 11448-FP-13 11448-FP-13 11448-FP-13 11448-FP-13 11448-FP-13 11448-FP-13 11448-FP-13 11448-FP-13 11448-FP-13 11448-FP-13 11448-FP-5, 60 11448-FP-60 11448-FP-13 11	525A 1525A 548A 547 546/560 562 562 546/5620 546/5620 546/6500 544 548B 548C 744/754 745 751 544B 544A	Cont&Recirc Spray Cont&Recirc Spray

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# APPENDIX A (Cont)

# CROSS REFERENCE OF MKS, FM, FP, PROBLEM NO., SYSTEM

<u>MKS</u>	FM	FP	<u>Problem</u>	System
117A1	11448-FM-104	11448-FP-12	508	Residual Heat RMVL
117A2	11448-FM-104	11448-FP-12	508	Residual Heat RMVL
117B1	11448-FM-104	11448-FP-3, 12	540	Residual Heat RMVL
124A1	11448-FM-103	11448-FP-9	630	Pressurizer Spray/Relief
124A2	11448-FM-103	11448-FP-9	630	Pressurizer Spray/Relief
125A1	11448-FM-103	11448-FP-9	636	Pressurizer Spray/Relief
137A1	11448-FM-85	11448-FP-19, 20, 74	CV1	Containment Vacuum
137A2	11448-FM-85	11448-FP-19, 20, 74	CV1	Containment Vacuum
143A1	Not Applicable	11448-FB-25	1040	Diesel Muffler Exhaust
144A	11448-FB-45A	11448-FB-3	CF1	Fire Protection
144B	11448-FB-45A	11448-FB-3	CF2	Fire Protection

# APPENDIX B

# CORRESPONDENCE WITH NRC

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### APPENDIX B

### CORRESPONDENCE WITH NRC

The following is a listing of correspondence with the NRC related to the reanalysis effort.

Item <u>No.</u>	Date	<u>Sígnature</u>	Addressee	Letter No./Subject
			NRC_	TO VEPCO
1 ·	3/13/79	Denton	Proffitt	Show Cause Order
2	4/2/79	Stello	Proffitt	Addendum to Show Cause Order
3	4/13/79	Stello	Proffitt	Use of Soil Structure Interaction Techniques
4	5/18/79	Stello	Proffitt	Request for Further SSI Information
5	5/25/79	Eisenhut	Proffitt	Factor Adjustment to SSI Calculated Stresses
6	7/18/79	O'Reilly	Proffitt	Information Pertaining to I.E. Bulletin No. 79-14, Revision 1
7	8/15/79	O'Reilly	Proffitt	Letter of Guidance on I.E. Bulletin No. 79-14
8	8/27/79	Denton	Proffitt	Lifting of Suspension Required by the Order to Show Cause
9	10/5/79	O'Reilly	Proffitt	Confirmation of Concurrence
10	10/23/79	Murphy	Proffitt	Refers to NRC Inspection of Sept. 10-13 and Sept. 19-21, 1979
11	10/24/79	Murphy	Proffitt	Refers to NRC Inspection of Sept. 13-14, 1979
12	10/25/79	Murphy	Proffitt	Refers to NRC Inspection of Sept. 26-28, 1979
13	11/15/79	Eisenhut	Proffitt	Refers to Soil Structure Interaction
			VEPC	<u>O_TO_NRC</u>
14	3/30/79	Spencer	Denton⁄ Stello	198/Initial Response to Show Cause Order

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### APPENDIX B (CONT)

### CORRESPONDENCE WITH NRC

Item				
<u>No.</u>	Date	<u>Signature</u>	<u>Addressee</u>	Letter No./Subject
15	4/19/79	Stallings	O'Reilly	270/LER 79-010/013L-0
16	4/23/79	Spencer	O'Reilly	289/Response to I.E. Bulletin No. 79-07
17	4/24/79	Spencer	O'Reilly	288/Response to I.E. Bulletin No. 79-07
18	4/27/79	Spencer	Denton⁄ Stello	311/Transmittal to Two Sample Problems to EG&G
19	5/2/79	Stallings	Denton	Observations on Reanalysis Effort
20	5/2/79	Spencer	Stello	260/Submittal of SSI Information
21	5/22/79	Ragone	Hendrie	Comments on Moratorium/Surry Reanalysis
22	5/24/79	Spencer	Stello	Response to NRC Letter of 4/2/79
23	5/24/79	Spencer	Stello	Response to NRC Letter of 5/18/79
24	6/5/79	Spencer	Denton	Submittal of Report on Reanalysis
25	6/8/79	Spencer	Denton	Additional Information, Report on Reanalysis of Piping
26	6/8/79	Spencer	Stello	Soil Structure Interaction Report
27	6/12/79	Spencer	Denton	Modification Information, Reanalysis of Piping Systems
28	6/15/79	Spencer	Denton	Schedule and Support Information
29	6/19/79	Spencer	Denton	Support Modifications
30	6/25/79	Spencer	Denton	Support Information, Reanalysis of Piping Systems
31	8/1/79	Spencer	Denton	Submittal of Revised Report on Analysis
32	8/21/79	Spencer	Denton	Analysis Completion of Designated Supports - Outside Containment

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### APPENDIX B (CONT)

### CORRESPONDENCE WITH NRC

Item <u>No.</u>	Date	<u>Signature</u>	<u>Addressee</u>	Letter No./Subject			
33	10/4/79	Spencer	O'Reilly	Response to NRC Letter of 7/2/79			
34	10/3/79	Proffitt	Denton	Seismic Analysis of Piping Systems			
35	10/4/79	Spencer	O'Reilly	Response to I.E. Letter Dated 9/7/79			
36	10/15/79	Spencer	O'Reilly	Extension of I.E. Bulletin 79-14 Deadline			
37	11/28/79	Spencer	Denton	Seismic Analysis of Piping Systems			
38	12/7/79	Spencer	O'Reilly	Response to NRC Letter of 11/8/79			
39	12/13/79	Spencer	Denton	Show Cause Order Reanalysis			
40	12/21/79	Spencer	O'Reilly	Show Cause 60 Days Analysis Completion			
S&W TO NRC							
41	3/22/79	Kennedy	Denton	Transmittal of S&W Computer Programs			
42	3/30/79	Jacobs	Herring	Submittal of Computer Outputs			
43	4/3/79	Jacobs	Bezler	Submittal of Benchmark Problem to Brookhaven National Laboratory			
44	4/6/79	Kennedy	Denton	Transmittal of S&W Computer Programs			
45	4/6/79	Jacobs	Stello	Plan for Verification of Dynamic Analysis Codes			
46	4/11/79	Jacobs	Bezler	Submittal of Computer Outputs			
47	4/13/79	Jacobs	Stello	Update and Status of Verification Plan for Dynamic Analysis Codes			
48	4/18/79	Jacobs	Hartman	Submittal of Computer Outputs			
49	4/27/79	Jacobs	Bezler	Submittal of Benchmark Problems			
50	4/27/79	Jacobs	Stello	Status of Verification Plan for Dynamic Analysis Codes			
51	5/8/79	Rossier	Neighbors	Draft Outline of SSI-ARS Report			

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### APPENDIX B (CONT)

# CORRESPONDENCE WITH NRC

<u>No.</u>	Date	<u>Signature</u>	Addressee	Letter No./Subject
52	5/9/79	Kennedy	Stello	Reference SHOCK O Program
53	5/11/79	Kennedy	Stello	Reference SHOCK 0 Program
5 <sup>.</sup> 4	5/14/79	Kennedy	Denton	Proprietary Computer Codes
5.5	6/4/79	Jacobs	Bezler	Submittal of Benchmark Problems
56	6/12/79	Jacobs	Bezler	Submittal of Benchmark Problems
57	9/6/79	Allen	Stello	Response to NRC Letter of 8/10/79

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