

NOTES: Prepared in June 2015 with latest update by JRWhite in July 2015 (and again in March 2017)
 This file focuses on the flow distribution calculation - all axial power info in separate file
 Here we do calc for both the UMLRR and WPI fuel elements
 For the bypasses, all the cases have 5 ribs, 4 control blades, and 1 RegBlade
 We also do a calc based on only flow area for comparison purposes
 Basic geometry parameters and assumptions are tabulated at the top and then the PLTEMP input is prepared below
 This file is based on the original work done by JRWhite back in 1991 for the HEU to LEU conversion.
 Added the power-to-flow plot on 7/30/15
 Reviewed in March 2017 -- Fixed a couple of typos in the comments and changed the # channels from 19 to 18 in the min flow area calc for the fuel channels.
 This was modified to account for the fact that the two end channels are only approximately 1/2 the size of the interior channels (19 full channels was simply not correct).
 This change only affected the flow area distribution for the no-friction case (Tables 8 and 9 in the safety analysis report), but this was only used for comparison purposes anyway.
 Thus, this change does not affect any of the results and conclusions from the PLTEMP full-core analysis.

Fuel Assembly Info (units => centimeters)

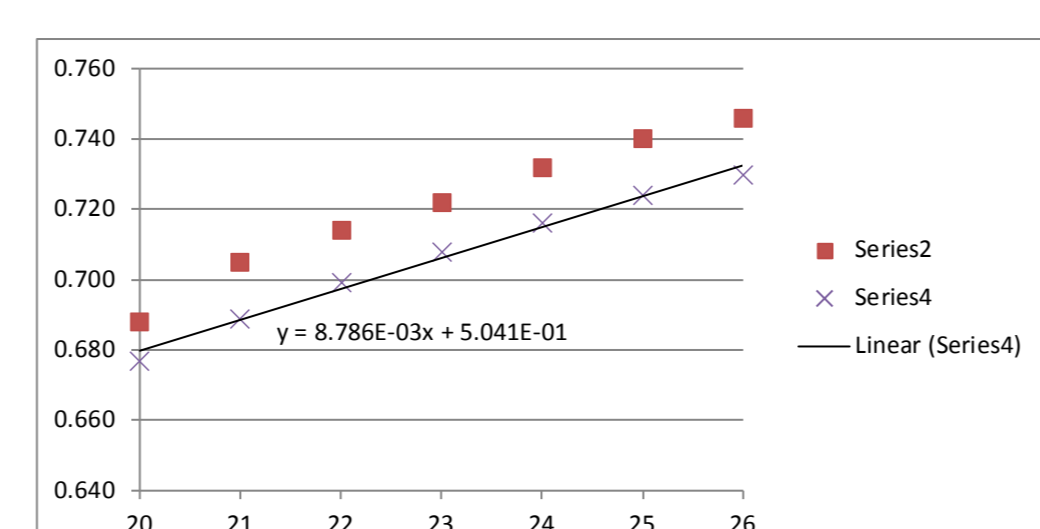
	UMLRR	WPI					
fuel	top channel area (assume 2.6" x 2.6")	43.613	43.613				
	top channel length (about 4.5" for top end box)	11.430	11.430	# fuel assy	fuel	UMLRR Flow Areas (cm ²)	total
	plate height	63.500	62.548	20	704.435	88.595	106.819
	channel width	6.604	6.706	21	739.657	88.595	106.819
	channel thickness	0.296	0.271	22	774.879	88.595	106.819
	bottom channel area (assume 2.6" x 2.6")	43.613	43.613	23	810.101	88.595	106.819
	bottom channel length (about 6" for grid plate)	15.240	15.240	24	845.323	88.595	106.819
	min flow area	35.222	32.698	25	880.544	88.595	106.819
				26	915.766	88.595	106.819
							10.068
rod basket	flow area (1.87" diameter hole)	17.719	17.719				
	length (35")	88.900	88.900	# fuel assy	fuel	UMLRR Normalized Flow Areas	total
	min flow area	17.719	17.719	20	0.774	0.097	0.117
				21	0.783	0.094	0.113
				22	0.790	0.090	0.109
				23	0.798	0.087	0.105
				24	0.804	0.084	0.102
				25	0.811	0.082	0.098
				26	0.817	0.079	0.095
							0.011
control blade	shroud area (10.844 x 0.75)	52.471	52.471				
	blade area (10.65 x 0.375)	25.766	25.766	# fuel assy	fuel	WPI Flow Areas (cm ²)	total
	top control in flow area (shroud - blade)	26.705	26.705	20	653.957	88.595	106.819
	top length (30")	76.200	76.200	21	686.655	88.595	106.819
	middle control out flow area	52.471	52.471	22	719.353	88.595	106.819
	middle length (21")	53.340	53.340	23	752.050	88.595	106.819
	bottom (10.844 x 4.7) -- very conservative since ignore holes	32.882	32.882	24	784.748	88.595	106.819
	bottom length (6")	15.240	15.240	25	817.446	88.595	106.819
	min flow area	26.705	26.705	26	850.144	88.595	106.819
							0.124
regblade	shroud area (2.465 x 2.465)	39.201	39.201				
	blade area (2.125 x 2.125)	29.133	29.133	# fuel assy	fuel	WPI Normalized Flow Areas	total
	top control in (shroud - blade)	10.068	10.068	20	0.761	0.103	0.124
	top length (26")	66.040	66.040	21	0.770	0.099	0.120
	middle control out	39.201	39.201	22	0.778	0.096	0.116
	middle length (25")	63.500	63.500	23	0.785	0.093	0.112
	bottom (grid box)	43.613	43.613	24	0.792	0.089	0.108
	bottom length (6")	15.240	15.240	25	0.799	0.087	0.104
	min flow area	10.068	10.068	26	0.805	0.084	0.101
							0.012

PLTEMP Data for LEU Core Flow Distribution Calculation

case description	umlr_flow21	wpi_flow21
Card 0100		
ANAME		
Card 0200		
IB		
ICHF		
NCTYP		
NEDIT		
NAXDIN		
NELPRT		
Card 0300		
NELF		
NF		
WCGES		
FB		
FQ		
FH		
Card 0301		
EZJ1		
Card 0302		
AF		
DF		
LF		
ZF		
Card 0302		
AF		
DF		
LF		
ZF		
Card 0303		
FCOEF		
FEXPC		
Card 0304		
NCHNF		
IDF		
IDC		
UDEN		
UNFUEL		
CLAD		
TALM		
Card 0305		
AFF		
DFP		
PERF		
XIF		
Card 0305		
AFF		
DFP		
PERF		
XIF		
Card 0306		
CIRCF		
Card 0307		
FACFP		
Card 0400		
NCRS		
NC		
WCGES		
Card 0401		
AC		
DC		
LC		
ZC		
Card 0402		
FCOEF		
FEXPC		
Card 0400		
NCRS		
NC		
WCGES		
Card 0401		
AC		
DC		
LC		
ZC		
Card 0401		
AC		
DC		
LC		
ZC		
Card 0402		
FCOEF		
FEXPC		
Card 0400		
NCRS		
NC		
WCGES		
Card 0401		
AC		
DC		
LC		
ZC		
Card 0401		
AC		
DC		
LC		
ZC		
Card 0402		
FCOEF		
FEXPC		
Card 0500		
DPO		
DDP		
DPMAX		
POWER		
TIN		
P		
Card 0600		
ITER		
CONV		
ETA		
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NN		
ZR		
QVZ		
Card 0702		
NUK		
Card 0703		
NI		
NIJ		
NKK		

Summary Results

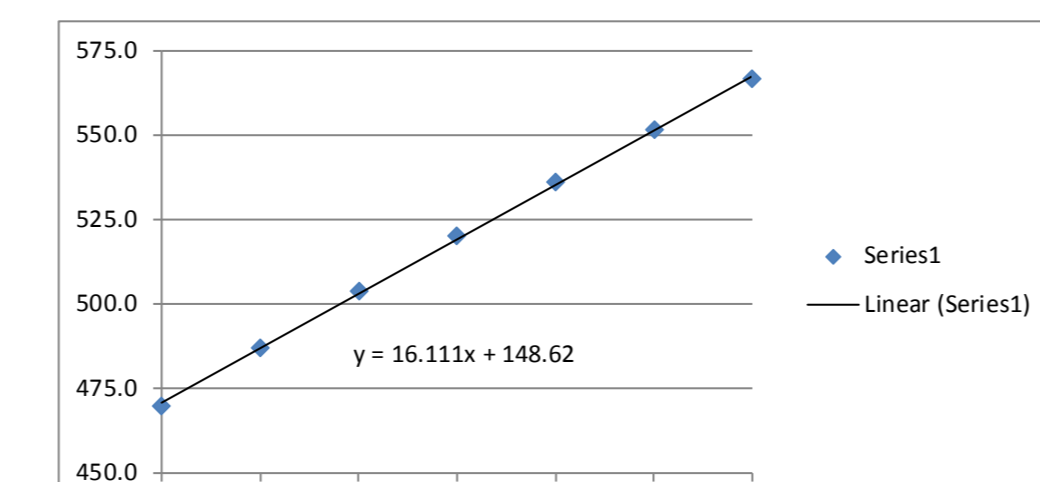
	UMLRR Assembly	WPI Assembly
# fuel assy	flow area calc	PLTEMP calc
20	0.783	0.688
21	0.792	0.705
22	0.799	0.714
23	0.806	0.722
24	0.813	0.732
25	0.819	0.740
26	0.825	0.746



Note: To do the documentation for this work I decided to treat this conversion factor a little differently. I wrote it as wassy = 0.0630 (FN) Qupm (gpm) where N = Nassy and F = 0.50 + 0.0088N

Let's use these to compute some of the same data as before (just as a check)

Prot (kW)	1000	1700	1600	1400	1300
# fuel assy	20	20	20	20	20
kW/assy	50.0	50.0	50.0	50.0	50.0
F	0.676	0.676	0.676	0.676	0.676
gpm/assy	55.8	55.8	55.8	55.8	55.8
wchan (kg/s)	0.201	0.201	0.195	0.188	0.182
UMLRR	1.028E+03	1.075E+03	9.975E+02	9.624E+02	9.323E+02
WPI	1.107E+03	1.075E+03	9.975E+02	9.624E+02	9.323E+02



Note: the power to flow ratio vs Nassy is also of interest. As the #assy increases, the power per assy decreases (for constant Prot), but the flow rate per assy also decreases. Thus, addressing how the power to flow (kW/gpm) changes is important.

