



UNITED STATES
NUCLEAR REGULATORY COMMISSION
REGION I
631 PARK AVENUE
KING OF PRUSSIA, PENNSYLVANIA 19406

CENTRAL FILES

Docket No. 50-272

OCT 29 1979

Public Service Electric and Gas Company
ATTN: Mr. F. W. Schneider
Vice President - Production
80 Park Place
Newark, New Jersey 07101

Gentlemen:

The enclosed IE Bulletin 79-17, Revision 1 is forwarded to you for action. A written response is required. If you desire additional information regarding this matter, please contact this office.

Sincerely,

for Robert V. Callan
Boyce H. Grier
Director

Enclosures:

1. IE Bulletin No. 79-17, Revision 1 w/Attachment
2. List of IE Bulletins Issued in the Last Six Months

CONTACT: L. E. Tripp
215-337-5282

cc w/encls:

F. P. Librizzi, General Manager - Electric Production
E. N. Schwalje, Manager - Quality Assurance
R. L. Mittl, General Manager - Licensing and Environment
H. J. Midura, Manager - Salem Generating Station

CCP
A02

7911150078 Q

ENCLOSURE 1

UNITED STATES
NUCLEAR REGULATORY COMMISSION
OFFICE OF INSPECTION AND ENFORCEMENT
WASHINGTON, D.C. 20555

SSINS No.: 6820
Accession No.: 7908220157
3

IE Bulletin No. 79-17
Revision 1
Date: October 29, 1979
Page 1 of 5

PIPE CRACKS IN STAGNANT BORATED WATER SYSTEMS AT PWR PLANTS

Description of Circumstances:

IE Bulletin No. 79-17, issued July 26, 1979, provided information on the cracking experienced to date in safety-related stainless steel piping systems at PWR plants. Certain actions were required of all PWR facilities with an operating license within a specified 90-day time frame. R1
R1
R1
R1

After several discussions with licensee owner group representatives and inspection agencies it has been determined that the requirements of Item 2, particularly the ultrasonic examination, may be impractical because of unavailability of qualified personnel in certain cases to complete the inspections within the time specified by the Bulletin. To alleviate this situation and allow licensees the resources of improved ultrasonic inspection capabilities, a time extension and clarifications to the bulletin have been made. These are referenced to the affected items of the original bulletin. R1
R1
R1
R1
R1
R1
R1

During the period of November 1974 to February 1977 a number of cracking incidents have been experienced in safety-related stainless steel piping systems and portions of systems which contain oxygenated, stagnant or essentially stagnant borated water. Metallurgical investigations revealed these cracks occurred in the weld heat affected zone of 8-inch to 10-inch type 304 material (schedule 10 and 40), initiating on the piping I.D. surface and propagating in either an intergranular or transgranular mode typical of Stress Corrosion Cracking. Analysis indicated the probable corrodents to be chloride and oxygen contamination in the affected systems. Plants affected up to this time were Arkansas Nuclear Unit 1, R. E. Ginna, H. B. Robinson Unit 2, Crystal River Unit 3, San Onofre Unit 1, and Surry Units 1 and 2. The NRC issued Circular No. 76-06 (copy attached) in view of the apparent generic nature of the problem.

During the refueling outage of Three Mile Island Unit 1 which began in February of this year, visual inspections disclosed five (5) through-wall cracks at welds in the spent fuel cooling system piping and one (1) at a weld in the decay heat removal system. These cracks were found as a result of local boric acid buildup and later confirmed by liquid penetrant tests. This initial identification of cracking was reported to the NRC in a Licensee Event Report (LER) dated May 16, 1979. A preliminary metallurgical analysis was performed by the licensee on a section of cracked and leaking weld joint from the spent fuel cooling system.

The conclusion of this analysis was that cracking was due to Intergranular Stress Corrosion Cracking (IGSCC) originating on the pipe I.D. The cracking was localized to the heat affected zone where the type 304 stainless steel is sensitized (precipitated carbides) during welding. In addition to the main through-wall crack, incipient cracks were observed at several locations in the weld heat affected zone including the weld root fusion area where a miniscule lack of fusion had occurred. The stresses responsible for cracking are believed to be primarily residual welding stresses in as much as the calculated applied stresses were found to be less than code design limits. There is no conclusive evidence at this time to identify those aggressive chemical species which promoted this IGSCC attack. Further analytical efforts in this area and on other system welds are being pursued.

Based on the above analysis and visual leaks, the licensee initiated a broad based ultrasonic examination of potentially affected systems utilizing special techniques. The systems examined included the spent fuel, decay heat removal, makeup and purification, and reactor building spray systems which contain stagnant or intermittently stagnant, oxygenated boric acid environments. These systems range from 2 1/2-inch (HPCI) to 24-inch (borated water storage tank suction), are type 304 stainless steel, schedule 160 to schedule 40 thickness respectively. Results of these examinations were reported to the NRC on June 30, 1979 as an update to the May 16, 1979 LER. The ultrasonic inspection as of July 10, 1979 has identified 206 welds out of 946 inspected having UT indications characteristic of cracking randomly distributed throughout the aforementioned sizes (24"-14"-12"-10"-8"-2" etc.) of the above systems. It is important to note that six of the crack indications were reportedly found in 2 1/2-inch diameter pipe of the high pressure injection lines inside containment. These lines are attached to the main coolant pipe and are nonisolable from the main coolant system except for check valves. All of the six crack indications were found in two high pressure injection lines containing stagnated borated water. No crack indications were found in high pressure injection lines which were utilized for makeup operations.

Recent data reported from Three Mile Island Unit 1 indicates that the extent of IGSCC experienced in stainless steel piping at that facility may be more limited than originally stated above. Of the 1902 total welds originally inspected 350 contained U.T. indications which required further evaluation. These 350 welds have been reinspected with a second U.T. procedure which purportedly provides better discrimination between actual cracks and geometrical reflectors. Hence, the licensee now estimates that approximately 38 of the 350 welds contain IGSCC and the remaining welds, including those in high pressure injection and decay heat lines, contain only geometrical reflectors. Further metallurgical analysis of these welds is required to verify the adequacy of the U.T. procedures and to determine the nature of the cracking.

For All Pressurized Water Reactor Facilities with an Operating License:

1. Conduct a review of safety related stainless steel piping systems within 30 days of the date of this Bulletin (July 26, 1979) to identify systems and portions of systems which contain stagnant oxygenated borated water. These systems typically include ECCS, decay/residual heat removal, spent fuel pool cooling, containment spray and borated water storage tank (BWST-RWST) piping. R1

For this review, the term "stagnant, oxygenated borated water systems" refers to those systems serving as engineered safeguards having no normal operating functions and contain essentially air saturated borated water where dynamic flow conditions do not exist on a continuous basis. However, these systems must be maintained ready for actuation during normal power operations. Where your definition for stagnant differed from the one given above please supplement your previous response within 30 days of this Bulletin revision. R1

- (a) Provide the extent and dates of the hydrotests, visual and volumetric examinations performed per 10 CFR 50.55a(g) (Re: IE Circular No. 76-06 attached) of identified systems. Include a description of the non-destructive examination procedures, procedure qualifications and acceptance criteria, the sampling plan, results of the examinations and any related corrective actions taken.
 - (b) Provide a description of water chemistry controls, summary of chemistry data, any design changes and/or actions taken, such as periodic flushing or recirculation procedures to maintain required water chemistry with respect to pH, B, Cl⁻, F⁻, O₂.
 - (c) Describe the preservice NDE performed on the weld joints of identified systems. The description is to include the applicable ASME Code sections and supplements (addenda) that were followed, and the acceptance criterion.
 - (d) Facilities having previously experienced cracking in identified systems, Item 1, are requested to identify (list) the new materials utilized in repair or replacement on a system-by-system basis. If a report of this information and that requested above has been previously submitted to the NRC, please reference the specific report(s) in response to this Bulletin.
2. All operating PWR facilities shall complete the following inspection on the stagnant piping systems identified in Item 1 at the earliest practical date not later than twelve months from the date of this bulletin revision. Facilities which have been inspected in accordance with the original Bulletin, Sections 2(a) and 2(b) satisfy the requirements of this Revision. R1
R1
R1
R1
R1

- (a) Until the examination required by 2(b) is completed a visual examination shall be made of all normally accessible welds of the engineered safety systems at least monthly to verify continued systems integrity. Similarly, the normally inaccessible welds, shall be visually examined during each cold shutdown. R1
R1
R1
R1
R1

The relevant provisions of Article IWA 2000 of ASME Code Section XI and Article 9 of Section V are considered appropriate and an acceptable basis for this examination. For insulated piping, the examination may be conducted without the removal of insulation. During the examination particular attention shall be given to both insulated and noninsulated piping for evidence of leakage and/or boric acid residues which may have accumulated during the service period preceding the examination. Where evidence of leakage and/or boric acid residues are detected at locations, other than those normally expected, (such as valve stems, pump seals, etc.) the piping shall be cleaned (including insulation removal) to the extent necessary to permit further evaluation of the piping condition. In cases where piping conditions observed are not sufficiently definitive, additional inspections (i.e., surface and/or volumetric) shall be conducted in accordance with Item 2.(b). R1
R1
R1
R1
R1
R1
R1
R1
R1
R1
R1
R1
R1
R1

- (b) An ultrasonic examination shall be performed on a representative sample of circumferential welds in normally accessible portions of systems identified by 1 above. It is intended that the sample number of welds selected for examination include all pipe diameters within the 2 1/2-inch to 24-inch range with no less than a 10 percent sampling being taken. The approach to selection of the sample shall be based on the following criteria: R1
R1
R1
R1
R1
R1
R1

- (1) Pipe Material Chemistry - As a first consideration, those welds in austenitic stainless steel piping (Types 304 and 316 ss) having 0.05 to 0.08 wt. % carbon content based on available material certification reports. R1
R1
R1
R1
- (2) Pipe Size and Thickness - An unbiased mixture of pipe diameters and actual wall thickness distributed among both horizontal and vertical piping runs shall be included in the sample. R1
R1
R1
- (3) System Importance - The sample welds shall focus the examination primarily on those systems required to function in the emergency core cooling mode and secondly, on the containment spray system. R1
R1
R1

The U.T. examination sample may be focused on noninsulated piping runs. The evaluation shall cover the weld root fusion zone and a minimum of 1/2 inch on the pipe I.D. (counterbore area) on each side of the weld. The procedure(s) for this examination shall be essentially R1
R1
R1
R1

*Normally accessible refers to those areas of the plant which can be entered during reactor operation. R1
R1

in accordance with ASME Code Section XI, Appendix III and Supplements of the 1975 Winter Addenda, except all signal responses shall be evaluated as to the nature of the reflectors. Other alternative examination methods, combination of methods, or newly developed techniques may be used provided the procedure(s) have a proven capability of detecting stress corrosion cracking in austenitic stainless steel piping. R1
R1
R1
R1
R1

For welds of systems included in the sample having pipe wall thickness of 0.250 inches and below, visual and liquid penetrant surface examination may be used in lieu of ultrasonic examination. R1
R1
R1

- (c) If cracking is identified during Item 2(a) and 2(b) examinations, all welds in the affected system, shall be subject to examination and repair considerations. In addition, the sample welds to be examined on the remaining normally accessible noninsulated piping shall be increased to 25 percent using the criteria outlined in paragraph 2(b). In the event that cracking is identified in other systems at this sampling level, all accessible and inaccessible welds of the systems identified in item 1 shall be subject to examination. R1
R1
R1
R1
R1
R1
3. Identification of cracking in one unit of a multi-unit facility which causes safety-related systems to be inoperable shall require immediate examination of accessible portions of other similar units which have not been inspected under the ISI provisions of 10 CFR 50.55a(g) unless justification for continued operation is provided.
4. Any cracking identified shall be reported to the Director of the appropriate NRC Regional Office within 24 hours of identification followed by a 14 day written report.
5. Provide a written report to the Director of the appropriate NRC Regional Office within 30 days of the date of this bulletin revision addressing the results of your review if required by Item 1. Provide a schedule of your inspection plans in response to Item 2(b) in those cases in which the inspections have not been completed. R1
R1
R1
R1
R1
6. Provide a written report to the Director of the appropriate NRC Regional Office within 30 days of the date of completion of the examinations required by Items 2(a), 2(b), or 2(c) describing the inspection results and any corrective actions taken. R1
R1
R1
R1
7. Copies of the reports required by Items above shall also be provided to the Director, Division of Operating Reactors, Office of Inspection and Enforcement, Washington, D.C. 20555.

Approved by GAO, B180225 (R0072), clearance expires 7/31/80. Approval was given under a blanket clearance specifically for identified generic problems.

Attachment:
IE Circular No. 76-06

November 26, 1976
IE Circular No. 76-06

**STRESS CORROSION CRACKS IN STAGNANT, LOW PRESSURE STAINLESS
PIPING CONTAINING BORIC ACID SOLUTION AT PWR's**

DESCRIPTION OF CIRCUMSTANCES:

During the period November 7, 1974 to November 1, 1975, several incidents of through-wall cracking have occurred in the 10-inch, schedule 10 type 304 stainless steel piping of the Reactor Building Spray and Decay Heat Removal Systems at Arkansas Nuclear Plant No. 1.

On October 7, 1976, Virginia Electric and Power also reported through-wall cracking in the 10-inch schedule 40 type 304 stainless discharge piping of the "A" recirculation spray heat exchanger at Surry Unit No. 2. A recent inspection of Unit 1 Containment Recirculation Spray Piping revealed cracking similar to Unit 2.

On October 8, 1976, another incident of similar cracking in 8-inch schedule 10 type 304 stainless piping of the Safety Injection Pump Suction Line at the Ginna facility was reported by the licensee.

Information received on the metallurgical analysis conducted to date indicates that the failures were the result of intergranular stress corrosion cracking that initiated on the inside of the piping. A commonality of factors observed associated with the corrosion mechanism were:

1. The cracks were adjacent to and propagated along weld zones of the thin-walled low pressure piping, not part of the reactor coolant system.
2. Cracking occurred in piping containing relatively stagnant boric acid solution not required for normal operating conditions.
3. Analysis of surface products at this time indicate a chloride ion interaction with oxide formation in the relatively stagnant boric acid solution as the probable corrodant, with the state of stress probably due to welding and/or fabrication.

The source of the chloride ion is not definitely known. However, at ANO-1 the chlorides and sulfide level observed in the surface tarnish film near welds is believed to have been introduced into the piping during testing of the sodium thiosulfate discharge valves, or valve leakage. Similarly, at Ginna the chlorides and potential oxygen

November 26, 1976

availability were assumed to have been present since original construction of the borated water storage tank which is vented to atmosphere. Corrosion attack at Surry is attributed to in-leakage of chlorides through recirculation spray heat exchange tubing, allowing buildup of contaminated water in an otherwise normally dry spray piping.

ACTION TO BE TAKEN BY LICENSEE:

1. Provide a description of your program for assuring continued integrity of those safety-related piping systems which are not frequently flushed, or which contain nonflowing liquids. This program should include consideration of hydrostatic testing in accordance with ASME Code Section XI rules (1974 Edition) for all active systems required for safety injection and containment spray, including their recirculation modes, from source of water supply up to the second isolation valve of the primary system. Similar tests should be considered for other safety-related piping systems.
2. Your program should also consider volumetric examination of a representative number of circumferential pipe welds by non-destructive examination techniques. Such examinations should be performed generally in accordance with Appendix I of Section XI of the ASME Code, except that the examined area should cover a distance of approximately six (6) times the pipe wall thickness (but not less than 2 inches and need not exceed 8 inches) on each side of the weld. Supplementary examination techniques, such as radiography, should be used where necessary for evaluation or confirmation of ultrasonic indications resulting from such examination.
3. A report describing your program and schedule for these inspections should be submitted within 30 days after receipt of this Circular.
4. The NRC Regional Office should be informed within 24 hours, of any adverse findings resulting during nondestructive evaluation of the accessible piping welds identified above.
5. A summary report of the examinations and evaluation of results should be submitted within 60 days from the date of completion of proposed testing and examinations.

November 26, 1976

This summary report should also include a brief description of plant conditions, operating procedures or other activities which provide assurance that the effluent chemistry will maintain low levels of potential corrodants in such relatively stagnant regions within the piping.

Your responses should be submitted to the Director of this office, with a copy to the NRC Office of Inspection and Enforcement, Division of Reactor Inspection Programs, Washington, D.C. 20555.

Approval of NRC requirements for reports concerning possible generic problems has been obtained under 44 U.S.C 3152 from the U.S. General Accounting Office. (GAO Approval B-180255 (R0062), expires 7/31/77.)

ENCLOSURE 2

LISTING OF IE BULLETINS
ISSUED IN LAST SIX MONTHS

Bulletin No.	Subject	Date Issued	Issued To
79-10	Requalification Training Program Statistics	5/11/79	All Power Reactor Facilities with an OL
79-11	Faulty Overcurrent Trip Device in Circuit Breakers for Engineered Safety Systems	5/22/79	All Power Reactor Facilities with an OL or CP
79-12	Short Period Scrams at BWR Facilities	5/31/79	All GE BWR Facilities with an OL
79-01A	Environmental Qualification of Class 1E Equipment (Deficiencies in the Environmental Qualification of ASCO Solenoid Valves)	6/6/79	All Power Reactor Facilities with an OL or CP
79-02 (Rev 1)	Pipe Support Base Plate Design Using Concrete Expansion Anchor Bolts	6/21/79	All Power Reactor Facilities with an OL or CP
79-13	Cracking in Feedwater System Piping	6/25/79	All PWRs with an OL (for Action), All Other Power Reactor Facilities with an OL or CP (For Information)
79-14	Seismic Analysis for As-Built Safety Related Piping Systems	7/2/79	All Power Reactor Facilities with an OL or CP

LISTING OF IE BULLETINS
ISSUED IN LAST SIX MONTHS (CONTINUED)

Bulletin No.	Subject	Date Issued	Issued To
79-15	Deep Draft Pump Deficiencies	7/11/79	All Power Reactor Facilities with an OL or CP
79-14 (Revision 1)	Same Title as 79-14	7/18/79	Same as 79-14
79-16	Vital Area Access Controls	7/30/79	All Holders of and Applicants for Reactor Operating Licenses
79-17	Pipe Cracks in Stagnant Borated Water Systems at PWR Plants	7/26/79	All PWR Power Reactor Facilities with an OL
79-05C&06C	Nuclear Incident at Three Mile Island - Supplement	7/26/79	All PWR Power Reactor Facilities with an OL
79-18	Audibility Problems Encountered on Evacuation	8/7/79	All Power Reactor Facilities with an OL
79-19	Packaging Low-Level Radioactive Waste for Transport and Burial	8/10/79	All Power and Research Reactors with OL, all Fuel Facilities (except Uranium Mills), and certain Materials Licensees
79-20	Same Title as 79-19	8/13/79	Certain Materials Licensees
79-21	Temperature Effects on Level Measurements	8/13/79	All Power Reactor Facilities with an OL or CP

LISTING OF IE BULLETINS
ISSUED IN LAST SIX MONTHS (CONTINUED)

Bulletin No.	Subject	Date Issued	Issued To
79-14 (Supplement)	Same Title as 79-14	8/15/79	Same as 79-14
79-02 (Rev 1) (Supplement No. 1)	Same Title as 79-02	8/20/79	Same as 79-02 (Rev 1)
79-13 (Rev 1)	Cracking in Feedwater System Piping	8/30/79	All Designated Applicants for OLs
79-22	Possible Leakage of Tubes of Tritium Gas Used in Timepieces for Luminosity	9/5/79	Each Licensee who Receives Tubes of Tritium Gas in Timepieces for Luminosity
79-14 (Supplement No. 2)	Same as Title 79-14	9/7/79	Same as 79-14
79-23	Potential Failure of Emergency Diesel Generator Field Exciter Transformer	9/12/79	All Power Reactor Facilities with an OL or CP
79-24	Frozen Lines	9/27/79	All Power Reactor Facilities which have either OLs of CPs and are in late stage of construction
79-13 (Rev. 2)	Cracking in Feedwater System Piping	10/17/79	All PWRs with an OL and Designated Applicants (for Action), All Other Power Reactor Facilities with an OL or CP (for Information)