REACTOR CONTAINMENT BUILDING INTEGRATED LEAK RATE TEST BROWNS FERRY NUCLEAR PLANT UNIT 3

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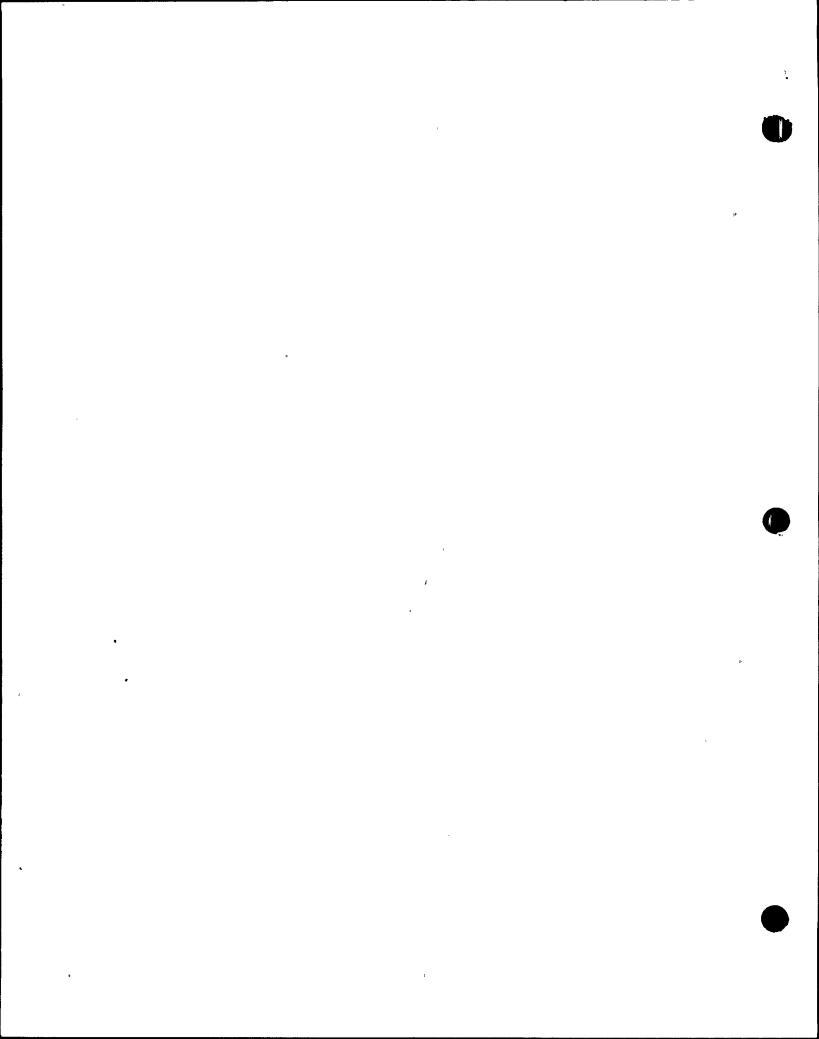
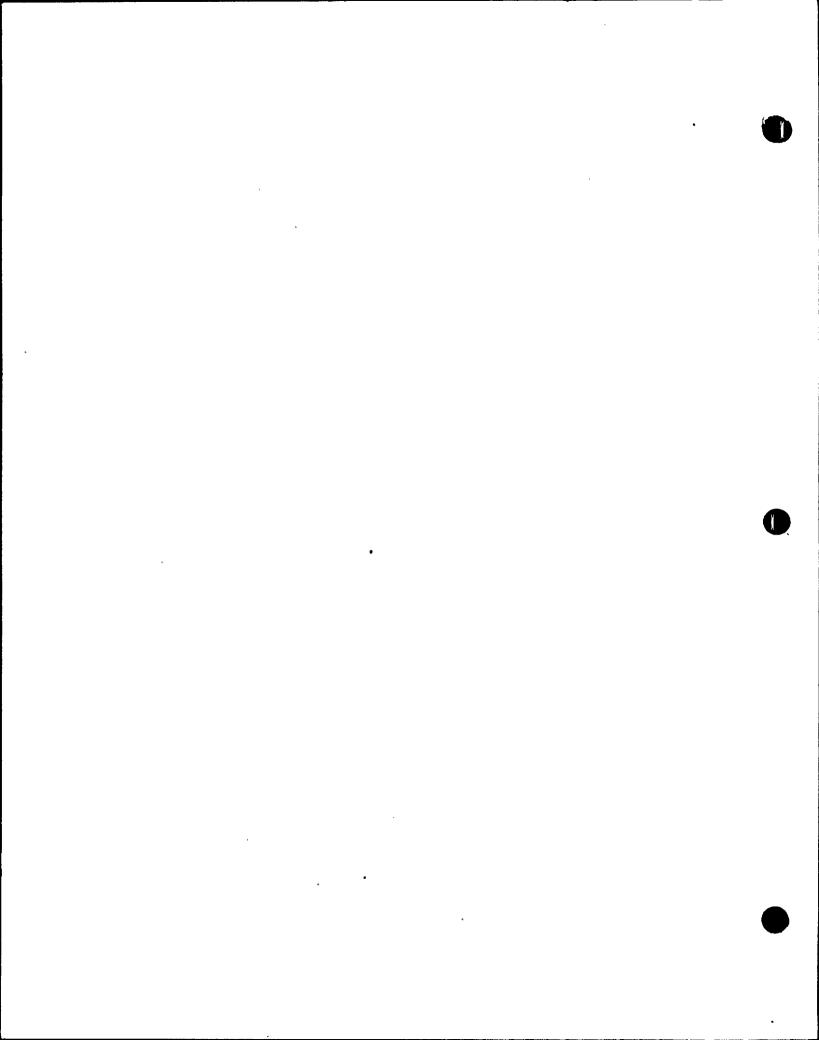


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1.0 INTRODUCTION

This report contains the summary technical analysis of the Reactor Building Containment Integrated Leak Rate Test (CILRT) conducted on Browns Ferry Nuclear Plant (BFN) Unit 3 November 6-7, 1995. As prescribed in BFN Technical Specification 4.7.A.2, the leakage of air from the boundary forming the reactor building primary containment is limited to 2.0 percent by weight of the containment air mass per day at a pressure of Pa, 49.6 psig. This test was conducted in accordance with the requirements of Title 10, Code of Federal Regulations (CFR), Part 50, Appendix J, which is implemented by BFN Surveillance Instruction (SI) 3-SI-4.7.A.2.a-f. Guidance for the procedure implemented by the SI was provided by the American National Standard for Containment Testing, ANS 145.4-1972, the American Nuclear Society Standard for Containment Testing, ANS 56.8, and the procedure outlined in Bechtel Topical Report, "Testing Criteria for Integrated Leakage Rate Testing of Primary Containment Structures for Nuclear Power Plants" (BN-TOP-1, Revision 1).

BFN Unit 3 is a 3,293-megawatt thermal, boiling water reactor employing a steel pressure suppression containment. The Final Safety Analysis Report defines the calculated peak accident pressure, Pa, to be 49.6 psig. The reactor containment building is divided into two major compartments—the drywell, enclosing the reactor and the forced recirculation system, and a pressure suppression pool chamber. These two compartments are connected by blowdown pipes that terminate below the suppression pool level. Vacuum breakers are provided to ensure that the suppression chamber is never pressurized with respect to the drywell. For the performance of this CILRT, these vacuum breakers were mechanically locked open to ensure pressure equalization between the drywell and the suppression chamber.

This report outlines the objectives, principal events, special equipment, and analysis of the test results for the CILRT completed on November 7, 1995, on BFN Unit 3. In addition, a summary of local leak rate tests conducted since the previous CILRT is included in Appendix M.

2.0 SUMMARY

A CILRT was conducted on BFN Unit 3 November 6-7, 1995, in preparation for return to power operation following an extended shutdown period (~ 10.5 years). The CILRT was successfully completed in 10 hours and 14 minutes and included 63 data samples.

The calculated Total Time Leak Rate (TTLR) was 0.8562 percent of containment air mass per day (% /day). The associated reportable As Found 95 percent upper confidence limit (UCL), which includes the type B and C leakage for testable penetrations in service at the time of the CILRT, was 1.0645 % /day. The As Left 95 percent UCL was the same since no adjustments were necessary during the performance of the test.

The Mass Leak Rate (MLR) for the CILRT was 0.91106 % /day. The associated reportable As Found and As Left 95 percent UCL was 0.92275 %/day. These values reflect the adjustment provisions as described for TTLR.

3.0 TEST PURPOSE AND RESULTS

3.1 TEST PURPOSE

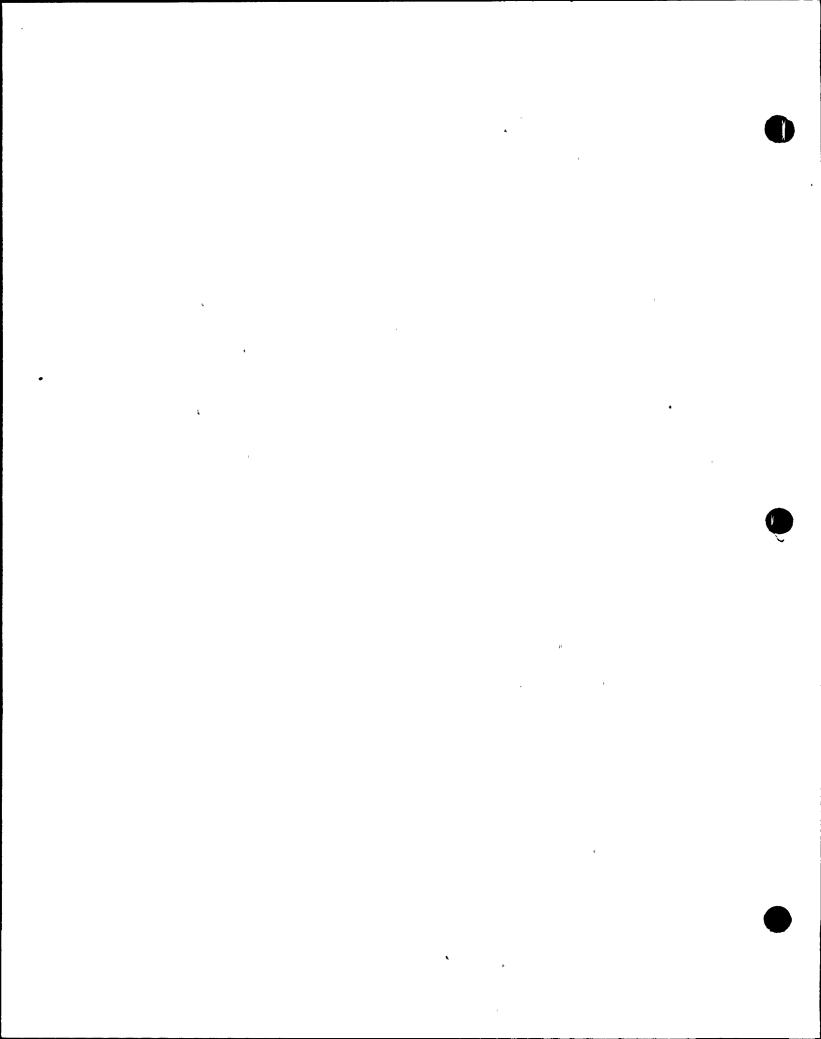
The primary objective of the CILRT was to demonstrate the leak-tight integrity of the Unit 3 reactor containment for return to power operation.

For BFN Unit 3, the leak-tight integrity is defined in Technical Specifications to be that the leakage of air from containment is not to exceed 1.5 % /day at peak accident pressure, P_a .

3.2 TEST RESULTS

The following table presents the test results with appropriate adjustments in leak rates as indicated by the notations. Evaluation of the Instrument Selection Guide and statistical analysis of proposed Regulatory Guide MS-021-5 are also presented. Additional tabular data on the CILRT and verification test results are presented in Appendices C and E.

The Total Time Leak Rate results, required by BN-TOP-1, Revision 1, for short duration tests, represent 70.9 percent of the allowable 1.5 percent of containment air mass, as described under Technical Specification 4.7.A.2. Agreement as prescribed by BN-TOP-1 between the CILRT and the verification test was -0.852 percent, which is well within the \pm 25 percent L_a required by Technical Specifications.



During the stabilization period, the primary containment was tested for unidentified leakage with a soap solution using Technical Instruction 3-TI-173. Leakage was identified at several instrument tubing compression fittings on panels 3-25-306 and 3-25-307, and minor packing leakage was identified on several valves which are tested as part of the CILRT boundary. The magnitude of these leakage paths was insufficient to preclude the successful performance of the CILRT, so the locations of these leaks were noted in 3-TI-173, and repairs were deferred until after completion of the CILRT and verification tests. These repairs were subsequently performed during the primary containment depressurization period. Since no convenient provisions for locally quantifying these leaks existed, no adjustment was made in the CILRT results to reflect the improvement realized by these repairs.

The leak-tight integrity of BFN Unit 3 was accurately measured and recorded by a computer-based instrumentation and data acquisition system. The acquisition system provided reliable, immediate calculations of the test data, thereby allowing test engineers to continuously monitor all instrumentation and test parameters.

Table of CILRT and Verification Test Results

TTLR = Total Time Leak Rate MLR = Mass Leak Rate

Post Test ISG = 0.16357 %/ day (1) (25 percent L_a = 0.5 %/ day)

CILRT (As Found = As Left)

 Calculated
 With 95% UCL

 TTLR
 0.85617 % /day
 1.06352 % /day (2)

 MLR
 0.91106 % /day
 0.92275 % /day (2)

CILRT Test Duration 10 Hours 14 Minutes CILRT Number of Samples 63 CILRT Sample Span 68 to 130

Verification Test

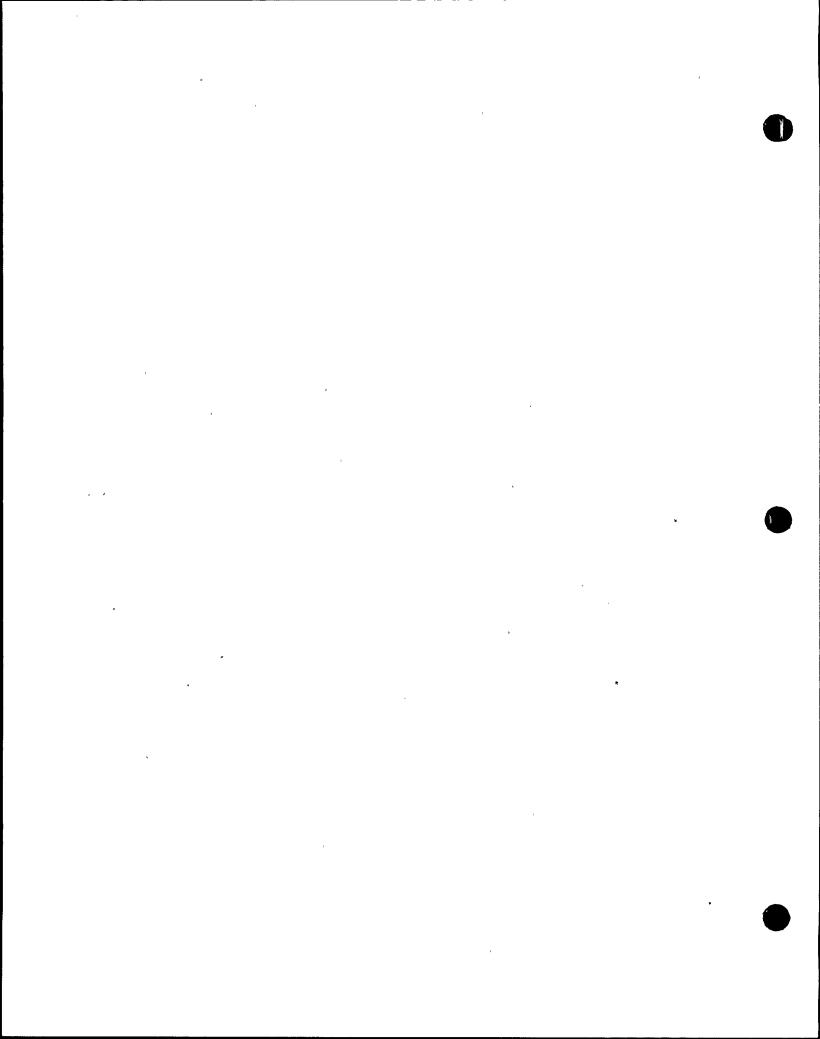
TTLR Agreement -0.852% (3) MLR Agreement 0.156% (3)

Verification Test Duration <u>5</u> Hours <u>19</u> Minutes Verification Number of Samples <u>59</u> Verification Sample Span <u>139</u> to <u>197</u>

Extended ANSI Statistical Analysis for CILRT (satisfaction of equations 1.1 or 1.2 and 2.1 is required)

Equation 1.1 0.2128 < 1 Satisfied 1.2 0.1506 < 1 Satisfied 2.1 1.5745 > 1 Satisfied

- (1) See Appendix G for ISG plot
- (2) Reflects leakage of systems in service during the CILRT of 0.0034 percent per day. See Appendix H for calculation.
- (3) See Appendix F for agreement calculations.



4.0 CONDUCT OF TEST

Prior to the start of the CILRT, local leak rate tests (LLRT) were conducted on the containment closures (hatches with resilient seals, bellows, and electrical penetrations) in accordance with surveillance instructions 3-SI-4.7.A.2.g-1 and 3-SI-4.7.A.2.g-2 (series). LLRTs were conducted on valves forming the boundary of the primary containment in accordance with Surveillance Instructions 3-SI-4.7.A.2.g-3/(series) and 3-SI-4.7.A.2.i-3/(series), with all valves meeting satisfactory leakage requirements prior to the performance of the CILRT.

The Residual Heat Removal (RHR) and the Core Spray (CS) safety systems were aligned to allow exposure to the CILRT test pressure. Water levels in the reactor vessel and the pressure suppression chamber were monitored for unexpected or unusual changes during the test sequence, but were intentionally not controlled with makeup or letdown (See Appendix L). The levels were allowed to change in response to possible internal system leakage (i.e., leakage from the reactor vessel to the pressure suppression chamber via safety system piping) or possible external system leakage (i.e., from primary containment via the RHR and CS external piping). This test configuration provides a means to reflect any water leakage from these systems external to the primary containment boundary (via displacement) in the CILRT measured leak rate.

This CILRT was performed with the reactor vessel head installed and torqued. The Reactor Coolant System (RCS) temperature was maintained between 100 and 110°F to ensure minimal stress in the reactor vessel head flange region. Maintaining this RCS temperature required periodic operation of the RHR system in the shutdown cooling mode. This resulted in a perturbation in the air temperature in the drywell each time the RHR shutdown cooling mode was entered (approximately every 4 hours). This perturbation is reflected on the temperature, pressure, and mass graphs, and in the tabular data presented in the Appendices.

Although the maximum permissible exposure temperature for temperature sensors used with the CILRT measuring and data acquisition system is 390°F, the normal measuring range is 0-114°F. Five specially modified sensors were calibrated to allow temperature measurements up to 130°F. These five modified sensors were installed in the drywell area immediately above and below the vessel head flange in anticipation of possible elevated temperatures. However, maximum temperatures remained well below the 114°F threshold.

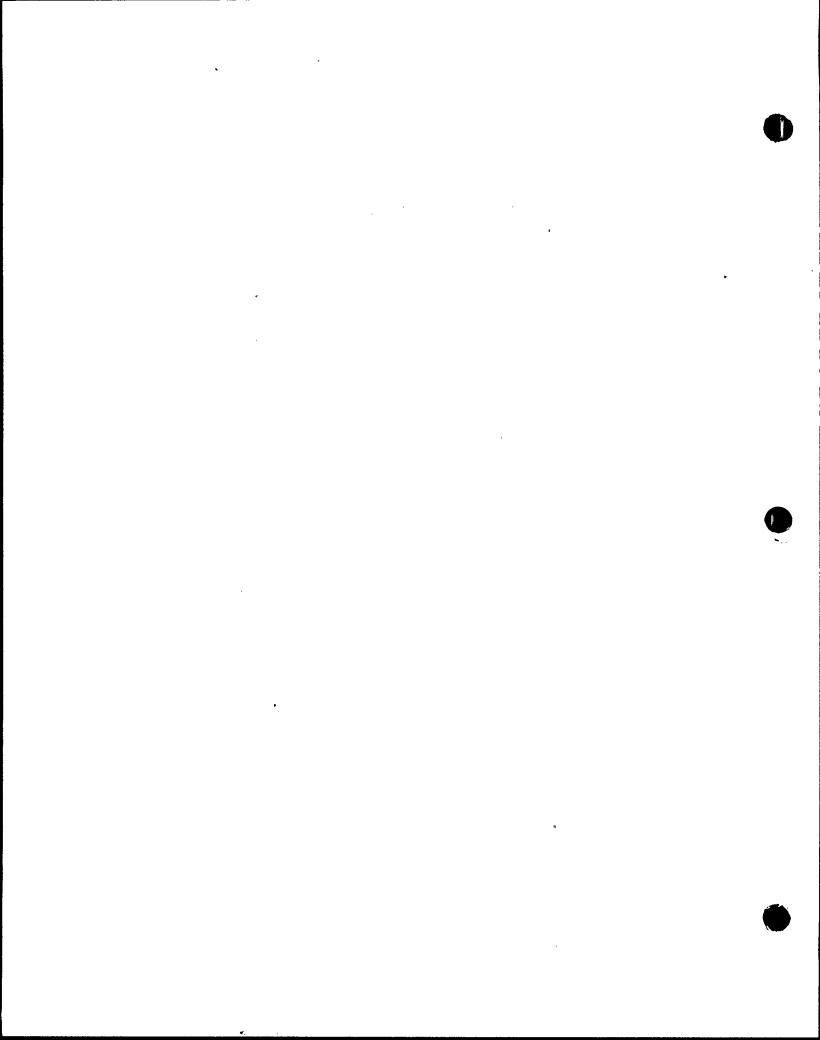
Pressurization of the primary containment was accomplished in approximately 6 hours. Pressurization began at 0626 hours on November 6, 1995 and was complete at 1338 hours.

The required 4 hour stabilization was begun on November 6 at 1343 hours, following completion of the isolation of penetration X-48 and venting of the pressurization line, and completed at 1752 hours (see Appendix A for stabilization phase acceptance criteria).

Evaluation of the containment environment parameters indicated that the temperature distribution was comparable to that of past BFN tests. The overall containment conditions stabilized rapidly during stabilization phase. This was attributed, in part, to a controlled pressurization rate which reduced temperature variations and the effects of ingassing. Another identifiable contributing factor—was the containment ventilation configuration (no forced ventilation), which—reduced spot heat sources due to blower operation).

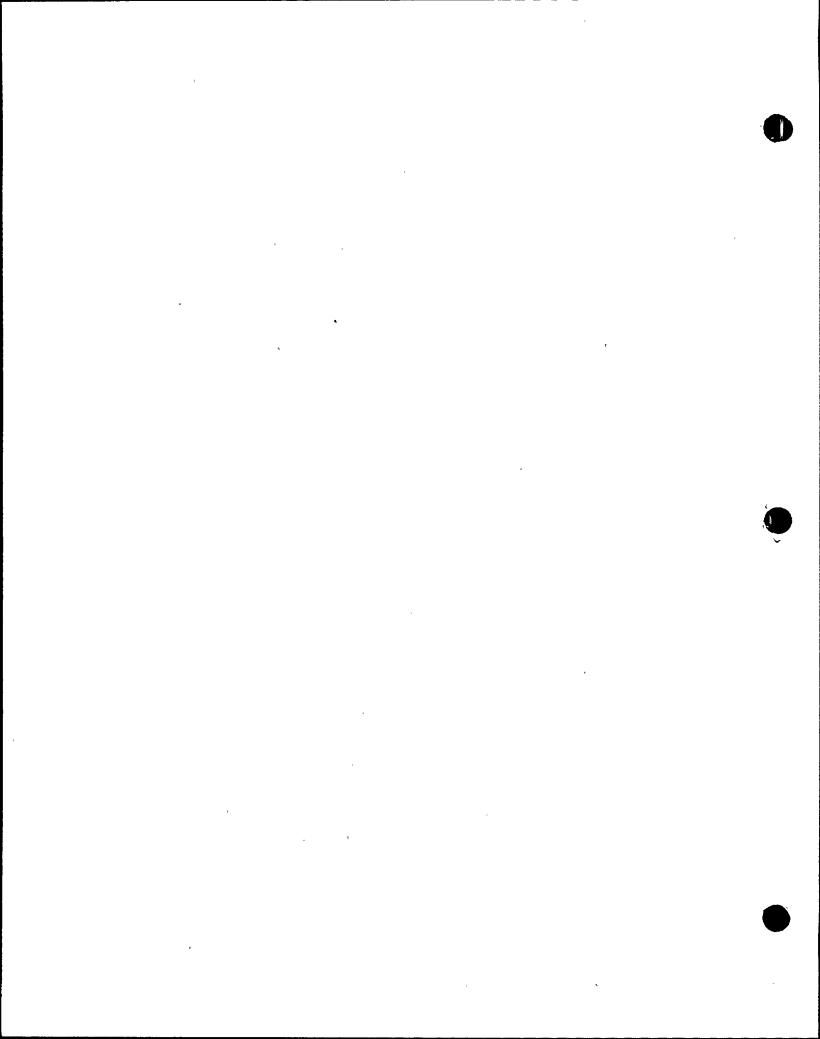
At 1802 hours, the CILRT test phase was initiated. The 10 hour and 14 minute, 63 samples test proceeded relatively uneventfully, with conditions remaining stable, with the exception of the regularly spaced perturbations caused from the periodic operation of RHR shutdown cooling. The reactor vessel water level slowly decreased at a rate of 0.9 inches per hour throughout the test, while the suppression chamber water level increased at 0.05 inches per hour. The amount of increase in the suppression chamber water level was approximately equal to the vessel level decrease and confirmed that leakage out of the test boundary was essentially zero. The CILRT test phase was concluded at 0416 hours on November 7,1994, in accordance with BN-TOP-1, Revision 1. The linearity of the CILRT was confirmed by statistical evaluation as described in ANSI 56.8.

Subsequent to the conclusion of the CILRT test phase, a leak of 18.2 SCFM (approximately L_a) was imposed on the primary containment. The primary containment was allowed to stabilize for 1 hour after introduction of this leak before beginning the verification test. The 5 hour and 14 minute verification test was initiated at 0547 hours on November 7 and was completed at 1106 hours. No additional perturbations occurred during this period, and the required agreement between this test and the CILRT was attained immediately.

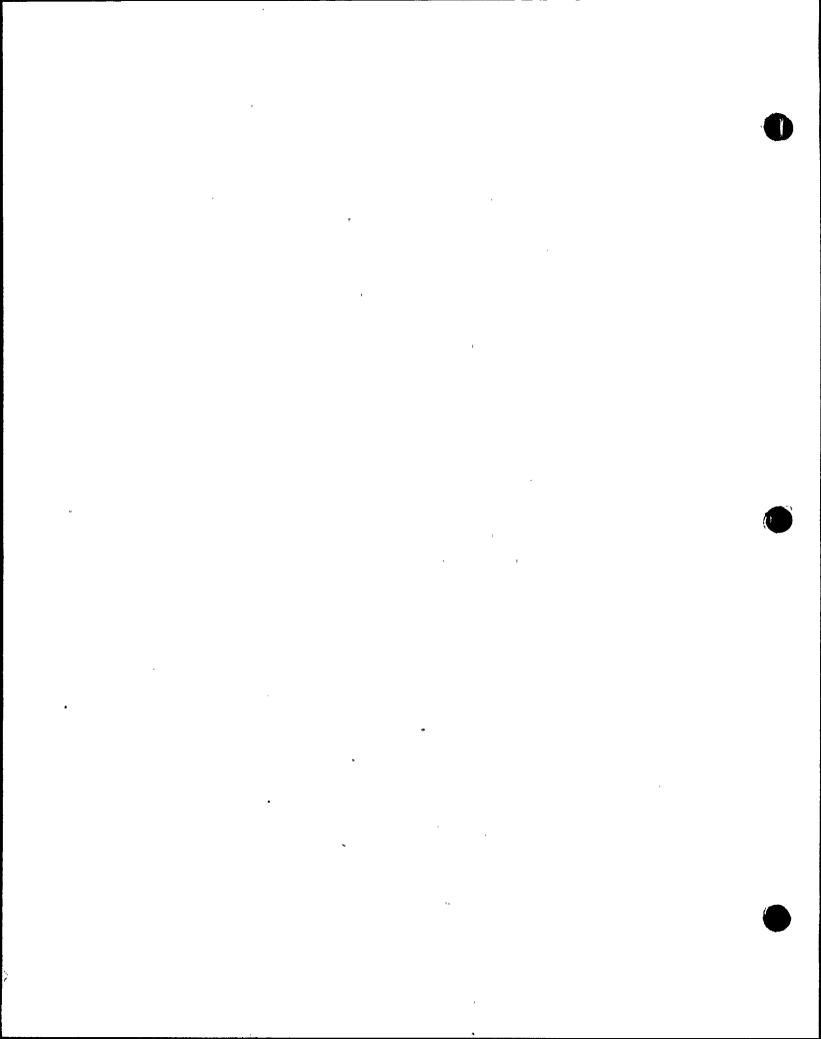


The following gives a chronological listing of events associated with the CILRT.

11/5/95		
	0930	CILRT Management Pretest Briefing given by F. Nilsen at morning meeting.
11/5/95	2300	Operations Pretest Briefing given by K. Green at Operations shift-turnover meeting.
11/6/95	0521	Completed pretest briefings with Operations and all personnel associated with test.
1/6/95	0626	Began pressurization of primary containment.
11/6/95	0645	Observed that two pressure gauges were not responding to increase in pressure. Discovered fitting problem at tubing to Drywell compartment. Stopped pressurization to correct.
1/6/95	0703	Resumed pressurization.
1/6/95	0732	Regulated air-compressor cooling water to increase discharge air temperature from 65-68°F to approximately 75°F to minimize impact on containment temperature.
1/6/95	0831	Reactor water level at 111.7 inches.
1/6/95	0833	Containment pressure at ~ 27.0 psia. Atmospheric pressure at ~ 14.5 psia.
1/6/95	0915	Briefed oncoming Operations shift.
1/6/95	0955	Containment pressure at 24.48 psig.
1/6/95	1025	Notified by Operations that Torus water level had dropped 2.7 inches since start of pressurization. Investigation in progress.
1/6/95	1100	Torus Level Indicators 3-LE-64-54 and 3-LE-66-64 are new instruments. They read the actual torus water level incorrectly when the torus is pressurized, but they will correctly reflect changes in the water level. Initial and final water levels will be recorded using an associated sight glass, and these level indicators will be monitored for changes during the test sequence.
	1/6/95 1/6/95 1/6/95 1/6/95 1/6/95 1/6/95 1/6/95 1/6/95	1/6/95 0703 1/6/95 0732 1/6/95 0831 1/6/95 0833 1/6/95 0915 1/6/95 0955 1/6/95 1025



11/6/95	1200	Containment pressure at ~ 41 psig. Air-compressor discharge at 58 psig and 78°F.
11.6.95	1230	Drywell temperature sensor TS-21 overranging occasionally and may have to be eliminated from the data base. This will require re-assignment of associated humidity sensor HS-5. Will monitor.
11/6/95	1259	Containment pressure at 62.27 psia, Atmospheric pressure at 14.45 psia.
11/6/95 	1302	Operations Keith Nichols reported that actual torus level was -4.75 inches (approximately the same level as when pressurization began).
11/6/95	1318	Containment pressure at 64.25 psia. Notified compressor operators to shut down one compressor.
11/6/95	1338	Notified compressor operators to shut down remaining compressor. Pressurization complete. Containment pressure at 65.23 psia. Atmospheric pressure at 14.43 psia.
11/6/95	1343	Began stabilization at sample number 44. Began performance of leak-checking portion of 3-TI-173.
11/6/95	1515	Deleted TS-21 due to overranging. Reset volume fractions and reassigned HS-5 to TS-22.
11/6/95	1639	Leak checks per 3-TI-173 progressing satisfactorily. Completed Core Spray pump shaft seal leakage tests. Small leak found on one pump (3A). Inspected Bonnet on 3-FCV-75-57.
11/6/95	1700	Drywell temperature sensor TS-14 overranged at sample 38 and at sample 46, then remained stable for the last 3.5 hours. Will mask reading for those two samples.
11/6/95	1707	Notified of a small leak on excess-flow check valve 3-ECKV-3-816. Will repair following test completion.



11/6/95	1730	Leakage found on instrument tubing joints in two locations. Leakage inspected and determined to be acceptable for performance of CILRT. These leaks will be repaired following the CILRT test sequence while pressure is still on containment. (These leaks are not locally testable).
11/6/95	1752	Terminated stabilization phase at sample 68. Stabilization length was 4 hours, 9 minutes. Stabilization criteria satisfied. Delta T values were: Avg. 4 hour = 0.452°F, Avg. last hour = 0.244°F
11/6/95	1802	Began test phase at sample number 69. Notified Operations to began hourly readings of water levels.
11/6/95	1840	Obtained water level from torus level sight glass. Torus level at -4.5 inches
11/6/95	1935	Removed TS-14 from data base due to sporadic overranging. Adjusted volume fractions and re-assigned HS-3 to TS-13.
11/6/95	2300	K. Green attended the Operations turnover meeting and gave update on CILRT status.
11/6/95	2310	Containment leak rate trending slightly upward.
11/7/95	0200	Control Rod Drive (CRD) 22-43 is leaking. Leak appears to be the directional control valve.
11/7/95	0203	Eight hours have elapsed since beginning test. The calculated TTLR is increasing very slightly. Cannot terminate due to Technical Specification requirement.
11/7/95	0210	Operations obtained torus water level from sight glass on 3-LE-64-54. Level at -4 5/8 inches.
11/7/95	0210	Operations contacted test director concerning isolating (CRD) leak. Since containment leak rate was acceptable leak, Operations was advised not to isolate to prevent changing test conditions and voiding test.
11/7/95	0416	Terminated Test phase at sample 130. Test duration was 10 hours, 14 minutes. All acceptance criteria met.

11/7/95 0440	Setting up for Verification Test phase. Operations obtained torus water level from sight glass on 3-LE-64-54. Level at -4 5/8 inches.
11/7/95 0447	Established an imposed leakage of 18.2 scfm on containment for verification test at Sample number 133. Contacted RADCON to obtain a grab sample of leak discharge.
11/7/95 0547	Completed required stabilization period with imposed leak. Started Verification test phase at sample 139.
11/7/95 0700	F. Nilsen attended Operations shift turnover meeting and gave test status update.
11/7/95 1014	UNIC-04 placed in procedure to correct flowrate meter 3-FI-64-132 reading from fpm to cfm. This meter is used during the depressurization of containment.
11/7/95 1106	Completed Verification test phase at sample 197 Test duration was 5 hours, 19 minutes. All BN-TOP-1, Revision 1, criteria met.
11/7/95 1106	Notified Maintenance department to repair leaks found during performance of 3-TI-173.
11/7/95 1220	Temporary mechanical valve stops used to provide positive control of depressurization path valve positions have been installed in ventilation valves 3-FCV-64 -29 and 3 FCV-64-30 but are binding severely. Will remove and lubricate threaded stems.
11/7/95 1245	Temporary mechanical valve stops lubricated and reinstalled in ventilation valves 3-FCV-64 -29 and 3-FCV-64-30. Began depressurization.
11/7/95 1500	Attended Operations shift turnover meeting and gave test status update. Depressurization in progress-containment pressure at 20.6 psig.
11/7/95 1642	Containment depressurization completed.

5.0 MEASUREMENTS AND CALCULATIONS

5.1 Test Equipment

Appendix J lists the range, accuracy, and repeatability of the special test equipment used in the Unit 3, Cycle 6 CILRT. Test instrumentation received pretest calibration checks. The test instruments were calibrated by the TVA Central Laboratories using traceable standards.

5.2 Sensor Location

Appendix J lists the volumetric weighting factor for each instrument based on the two-compartment model used for this test. The associated figures indicate sensor locations. The pressure sensors were divided so that two sensors measured each compartment through penetrations X-25 and X-205. Utilizing two sensors per compartment allows removal of any one malfunctioning pressure gauge during the test while continuing to accurately monitor containment pressure. An additional pressure gauge measured barometric pressure at the test station. Twenty-nine temperature sensors and seven humidity sensors measured conditions in the Drywell compartment, and six temperature sensors and three humidity sensors measured conditions in the Torus compartment. Using this number of sensors in each compartment yields precise measurements of all areas of each compartment and provides adequate margin to allow several malfunctioning sensors in each compartment to be deleted from the test calculations without compromising the test results. Two Drywell compartment temperature sensors were removed from the test data base due to sporadic overranging. The first sensor (TS-21) was removed during the stabilization phase and the second (TS-14) was removed approximately one and one-half hours into the test phase. In each case, the volume fractions were adjusted so that the remaining temperature sensors represented 100% of the compartment volume, and re-assignments were made so that the readings of the humidity sensors affected (HS-5 and HS-3) were correlated with an appropriately located temperature sensor (TS-22 and TS-13).

5.3 Computer-Based Data Acquisition and Data Reduction

The test data measured by the special test instrumentation during the BFN Unit 3 CILRT was automatically scanned and collected by a PC computer system and then reduced. The computer produced immediate statistical and graphical results of the containment test parameters, including temperature, pressure, vapor pressure, mass, MLR, and TTLR plots. These calculated results were reported automatically to the test director as data was collected. Appendix I depicts the functional relationship between the special test instrumentation and the PC computer system.

All calculations performed by the computer system were in conformance with the procedures outlined in ANS 56.8, ANSI 45.2-1972, and/or Bechtel Topical report BN-TOP-1, Revision 1.

Software used by the PC was purchased from Duke Engineering Company. Source listing for all computer programs are on file with the Plant Operating Systems group in Chattanooga, Tennessee. Additional software Commercial Dedication, Software Description, and User's manuals are located in the BFN Technical Support organization.

5.4 Containment Model

A two-compartment model was used to represent the Unit 3 containment.

The first compartment was the drywell which was subdivided into five segments. A constant volume mode was used with a volume of 164,170.2 ft³ representing the drywell volume. Twenty-nine temperature, 7 relative humidity, and two pressure instruments were used to determine the ambient conditions in the drywell.

The second compartment was the pressure suppression chamber (torus). Due to the uniformity of atmospheric conditions in the torus, this compartment consisted of only one segment. Again, a constant volume mode was used, amounting to 136,629.5 ft³. Six temperature, 3 relative humidity, and 2 pressure instruments were used in the torus compartment.

6.0 ANALYSIS OF TEST DATA

6.1 Instrument Assessment

The total complement of instruments for both the drywell and torus was 35 temperature, 10 relative humidity, 4 containment pressure, and one flow instrument. In addition, 1 pressure and one temperature instrument was used to monitor atmospheric conditions. Two temperature sensors, as discussed in paragraph 5.2, were the only instruments that malfunctioned during the entire test interval.

6.2 <u>Discussion of Graphical and Tabular Results for the CILRT and Verification</u> Phases

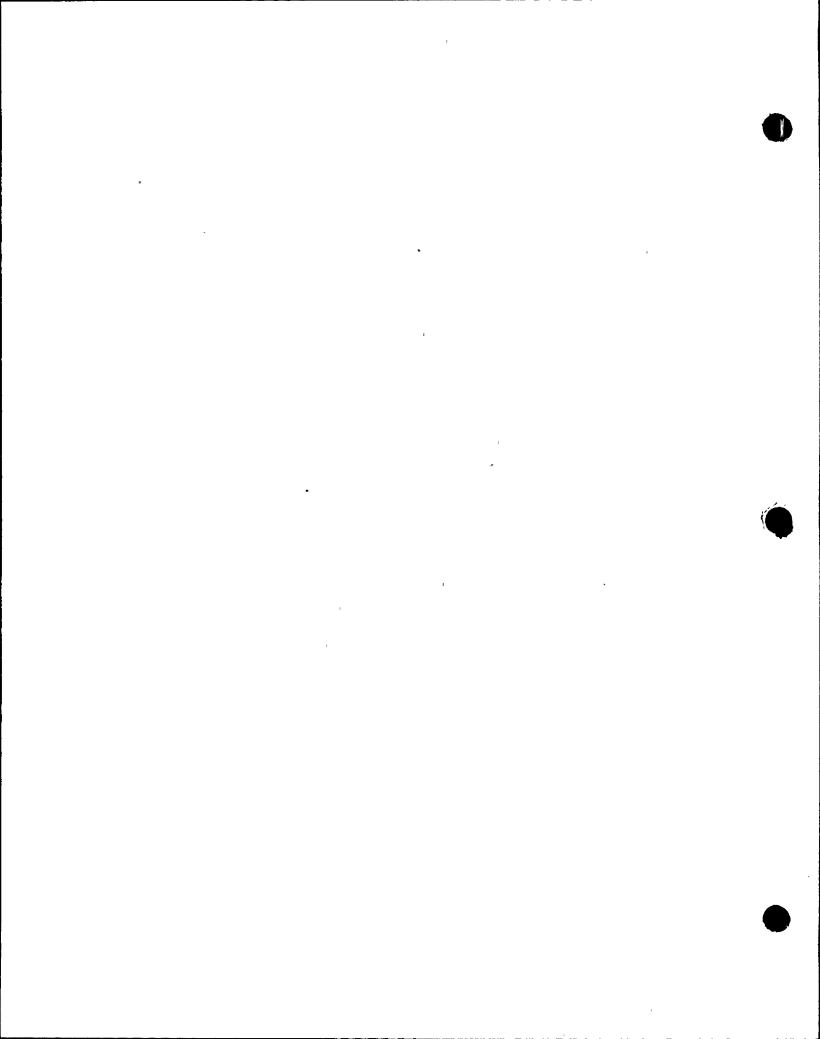
The CILRT and verification test phases were markedly uneventful. The CILRT was completed in 10 hours and 14 minutes with 63 samples collected. The measured, measured mean, calculated, and delta calculated leak rates were all converging. The extrapolated value of the leak rate was 0.93996 percent per day.

The verification test was also without incident. 59 samples were taken after allowing the verification imposed flow to stabilize for 1 hour. The verification test was concluded in 5 hours and 19 minutes and agreement was satisfactory.

During the CILRT phase and the verification test phase the water levels in the reactor vessel and torus were allowed to fluctuate without make-up to either vessel. The reactor vessel level decreased slightly (16.7 inches during the combined CILRT and verification test periods) while the torus level increased slightly (~ 0.2 inches during the same period) indicating that no measurable leakage was occurring out of the RHR and CS systems. (See Appendix L for water tabular data)

6.3 <u>Discussion of agreement (Verification Test)</u>

Since this test was conducted in accordance with BN-TOP-1, Revision 1, the verification flow was allowed to stabilize for approximately 1 hour prior to starting the verification phase of testing. The verification test ran 5 hours and 19 minutes, which is approximately one-half of the CILRT duration of 10 hours and 14 minutes. The verification test summary is contained in Appendix F.



Agreement between the verification test and CILRT test results was attained immediately and held constant throughout the verification test. This phase was completed in the minimum time required by BN-TOP-1 criteria.

6.4 Discussion of the Determination of the "As Found" Leakage Rate.

BFN Unit 3 was shut down in March, 1985, prior to the August issuance of IE Notice 85-71. The concept of "leakage savings" was not practiced by industry or inforced by NRC prior to issuance of this Notice. Although it was the in-house policy at BFN to perform As-Found leak rate tests, this practice was performed at that point in time to obtain information used for maintenance purposes, rather than obtaining leak rates for regulatory reporting. After the shutdown of Unit 3, it was anticipated that these As-Found tests would be performed prior to component maintenance. However, the lengthy delay of unit restart (ten and one-half years) resulted in deviations from normal practice, and not all components were tested prior to maintenance or modification. Therefore, an exact As-Found value for total minimum path or maximum path LLRT leakage is not available for the Unit 3, Cycle 6 extended shutdown period. However, since the unit only operated for about 3 months (November, 28,1984 to March 7, 1985) the As Found maximum path value can be approximated as the As Left maximum path LLRT total from the previous Unit 3, Cycle 5 refueling outage. Using maximum path leakage totals to approximate "leakage savings" is conservative and would result is an addition of only 0.02 percent per day(~11.5 SCFH) to the As Found CILRT results shown in this report. This addition is insignificant and would not impact the acceptability of the test results.

The Unit 3 CILRT As-Found leak rate value presented in this report reflects the total leak rate of the unit at the time of performance of the CILRT, including leakage from systems required to be in service during the test. No "leakage savings" is considered.

7.0 CONCLUSIONS

The reactor building containment integrated leak rate test performed on BFN Unit 3, cycle 6, recorded a calculated TTLR of 0.85617 percent of containment air mass per day, which clearly demonstrates the leak-tight integrity of Unit 3. The total 95 percent TTLR UCL As-Found and As-Left value of 1.06351 percent per day was less than 71 percent of that allowed by Technical Specifications.

The technique of multi-compartment modeling coupled with a computer-based data acquisition system yielded immediate results that accurately measured and displayed the Unit 3 containment leak rate.

APPENDIX A

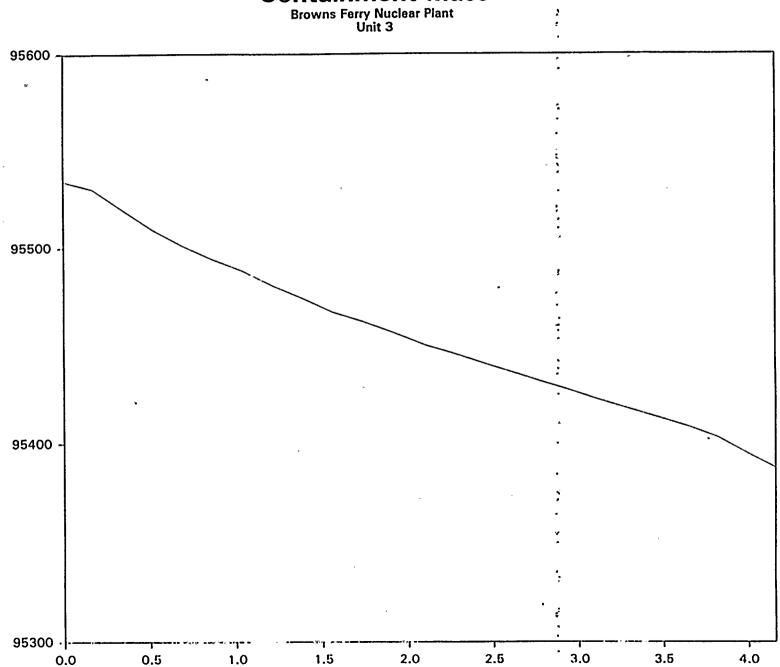
Stabilization Phase

Graphs and Tabular Data

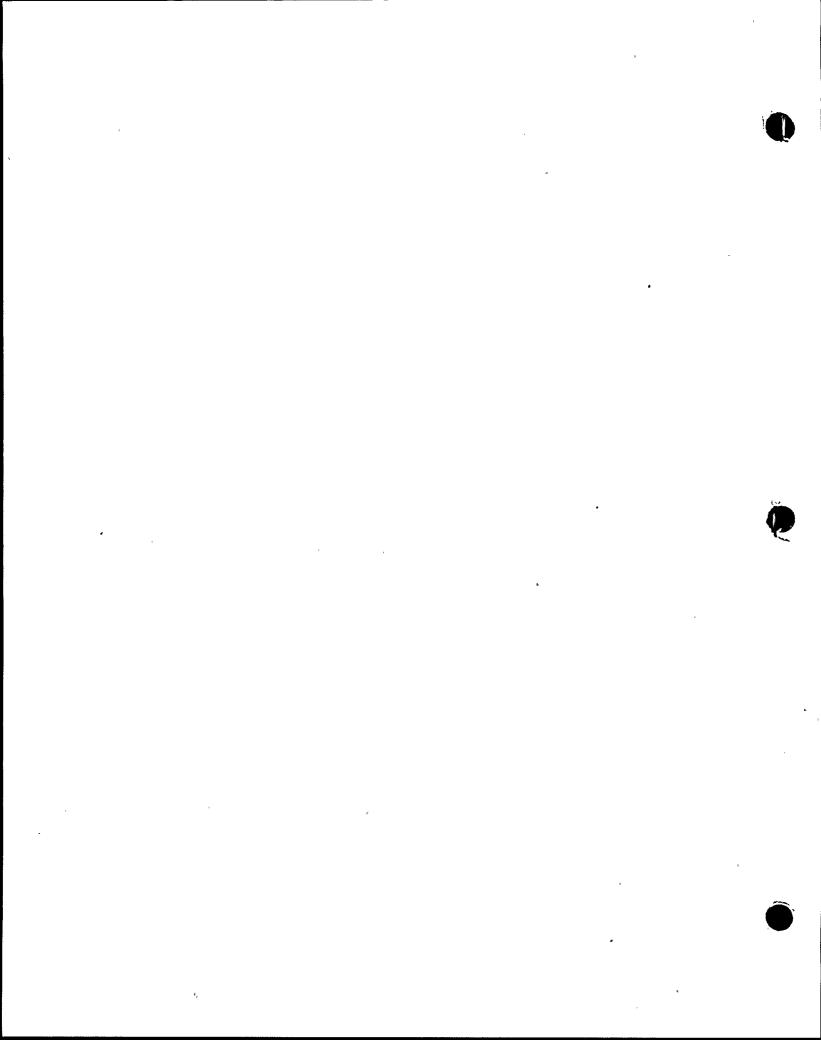
Contents: Temperature stabilization criteria - Samples 44 to 67

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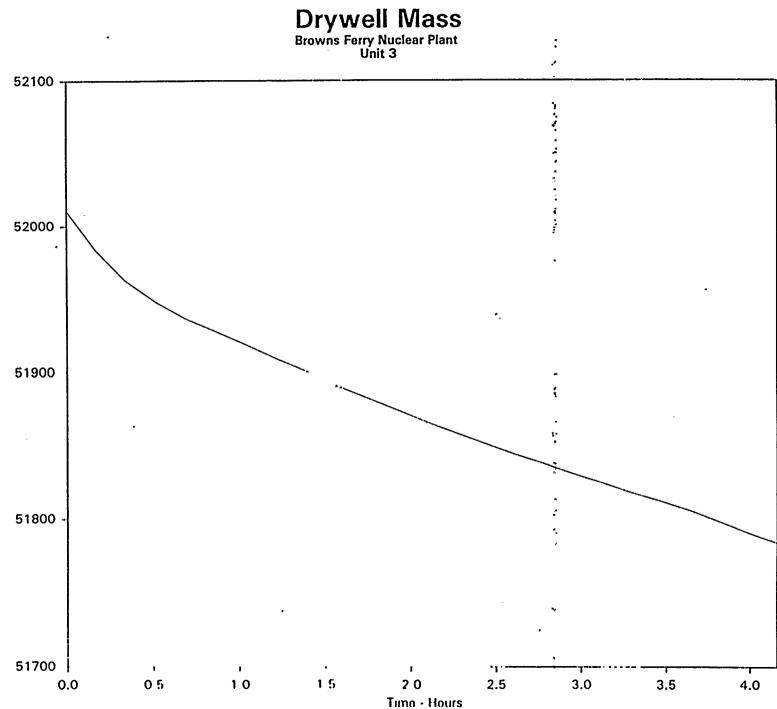
Containment Mass



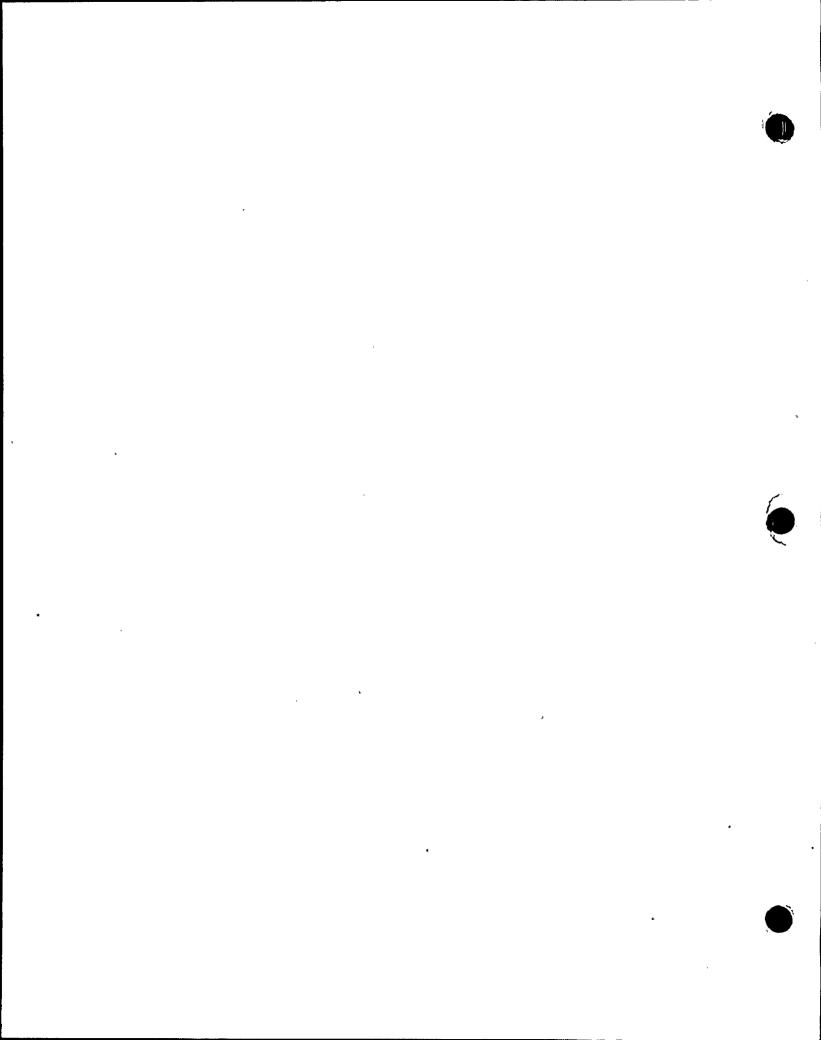
Time - Hours





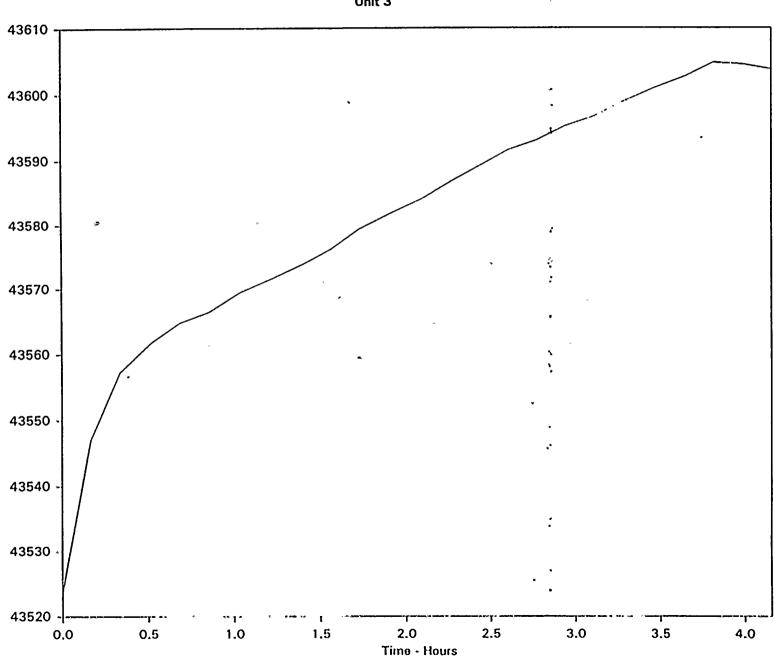


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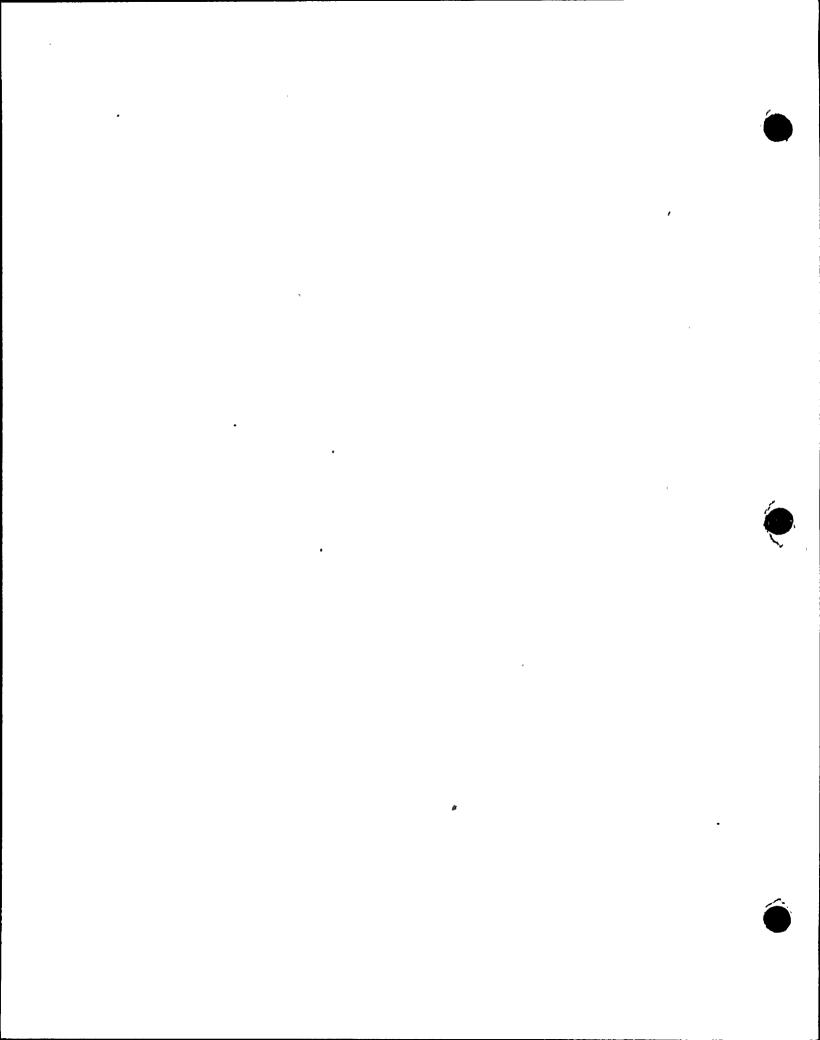


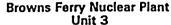


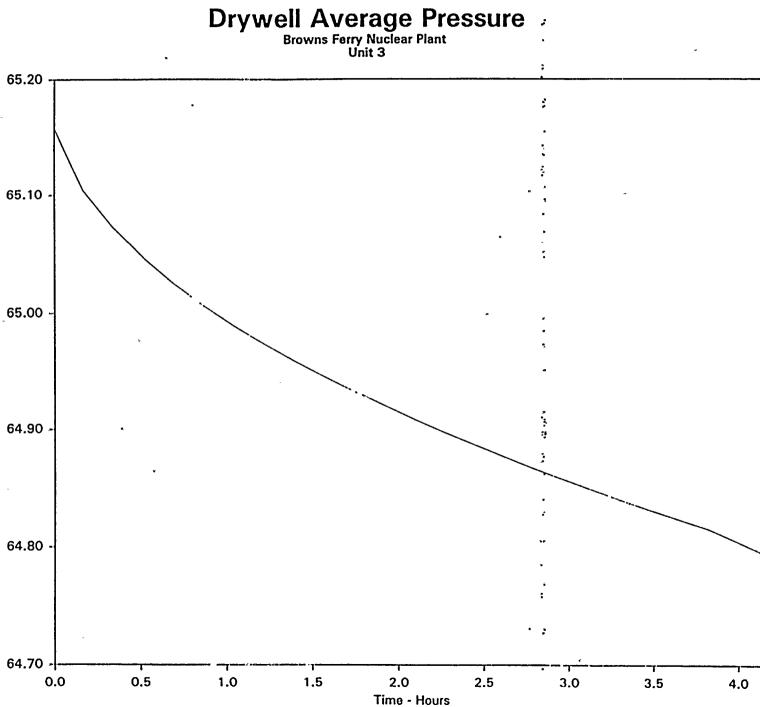
Torus Mass Browns Ferry Nuclear Plant Unit 3

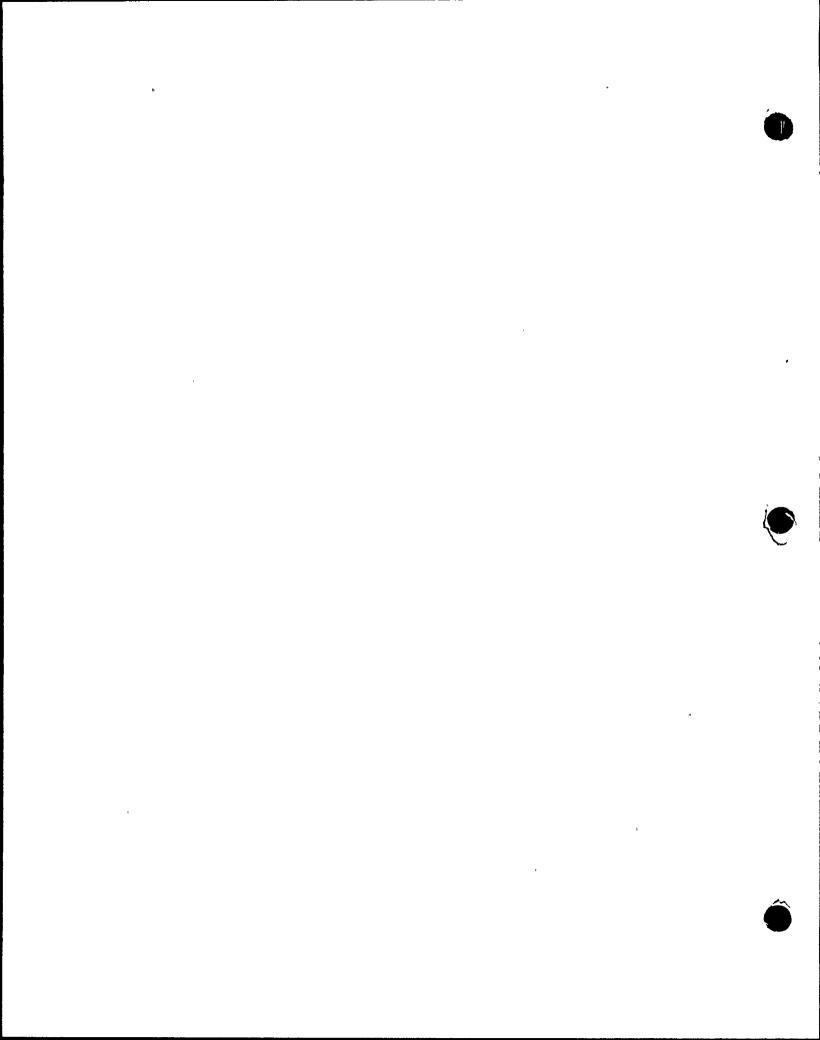


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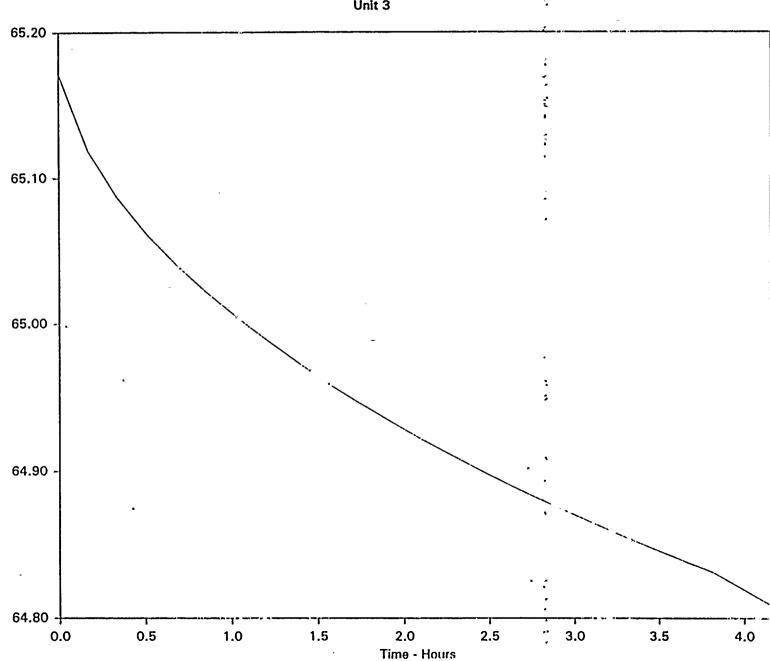






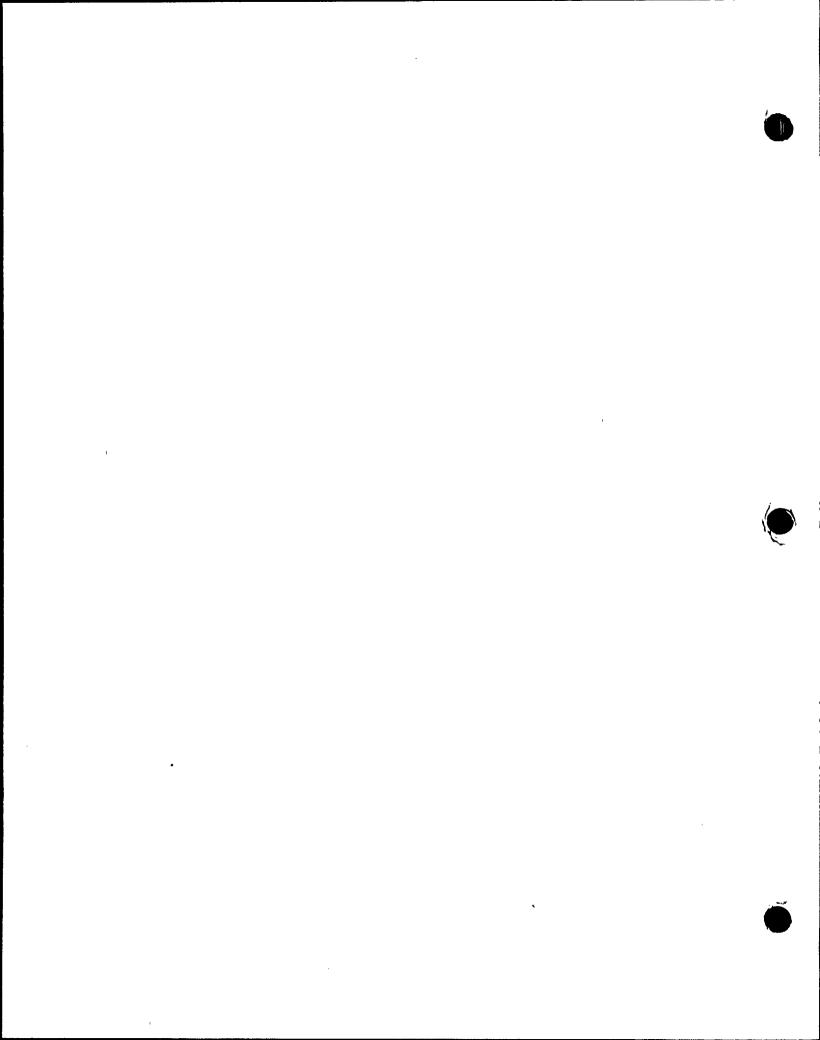


Torus Average Pressure Browns Ferry Nuclear Plant Unit 3

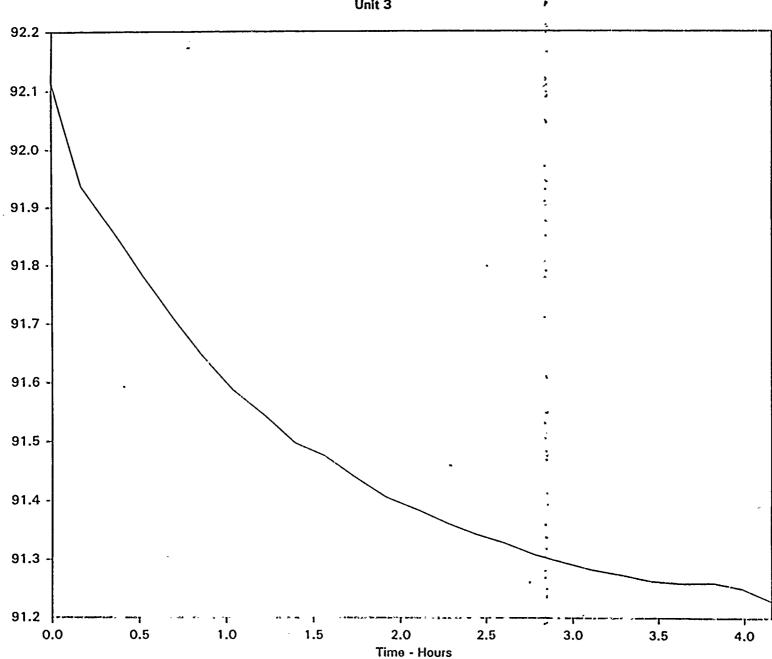


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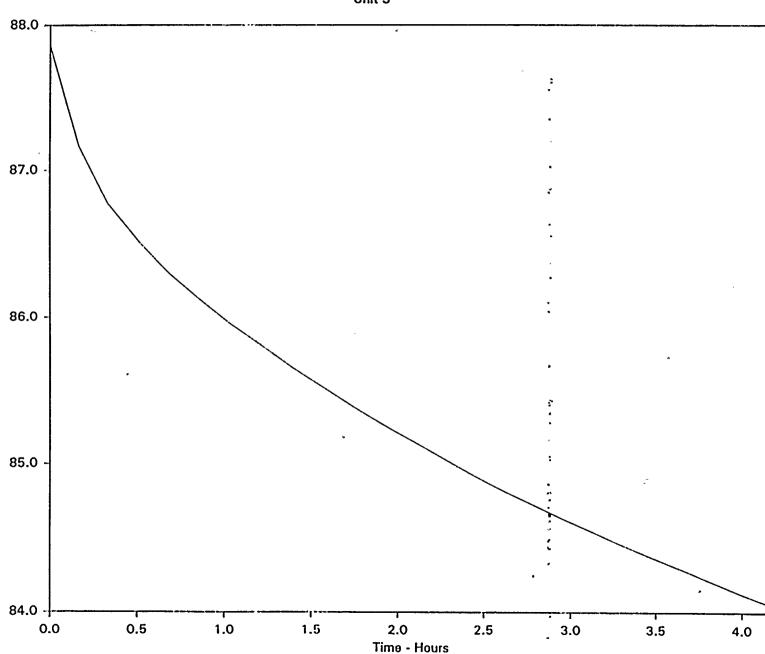
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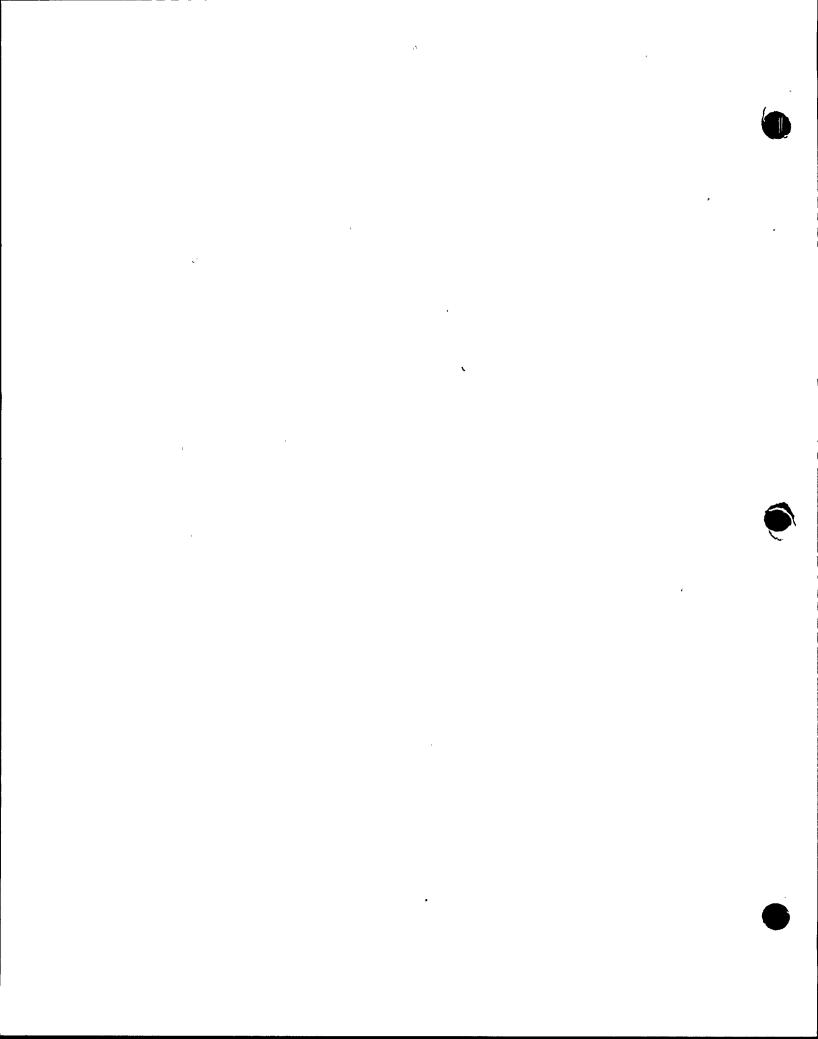
Drywell Average Temperature Browns Ferry Nuclear Plant Unit 3



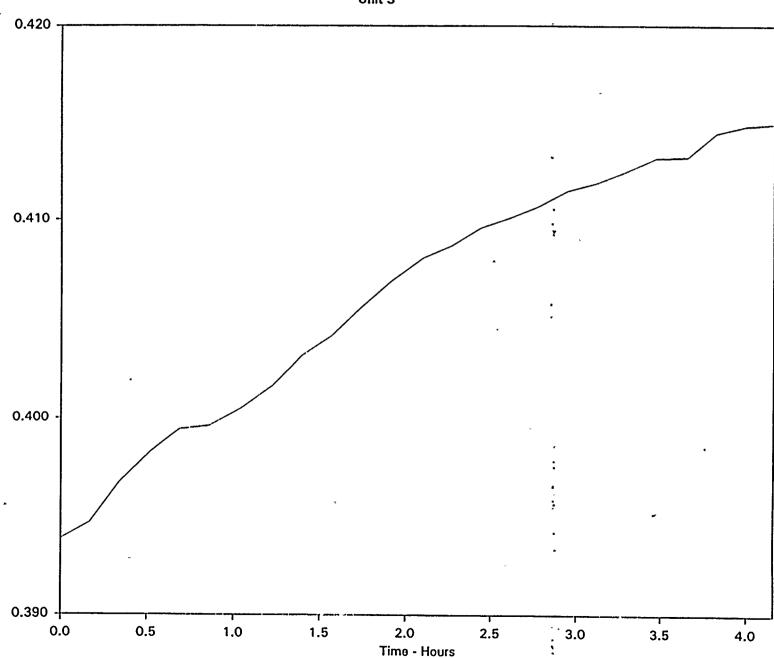


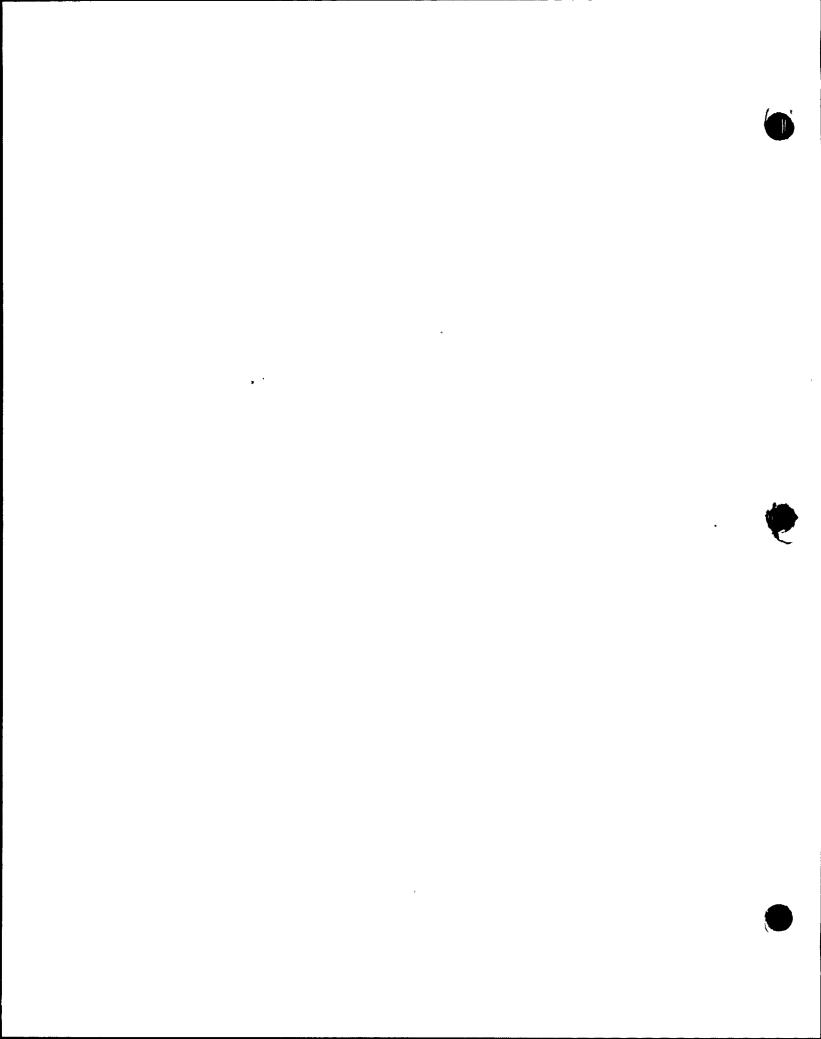


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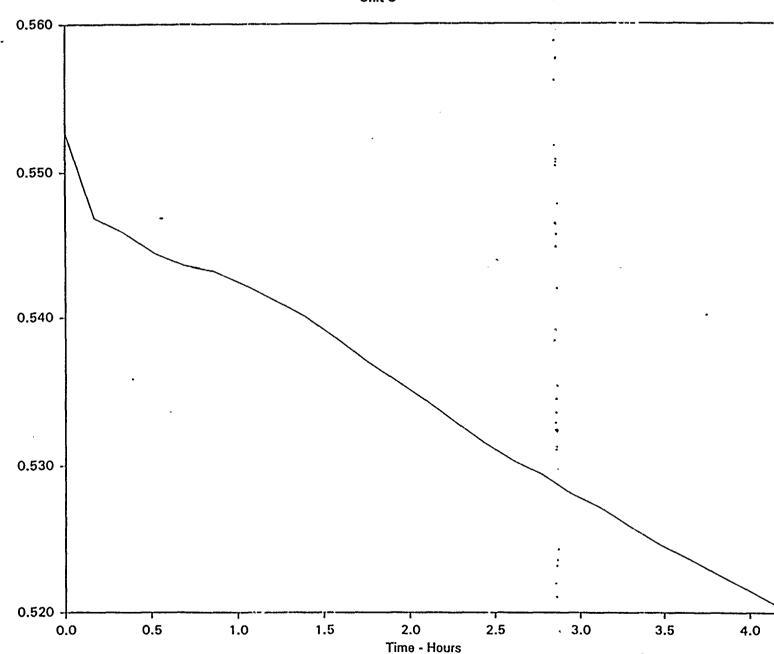


Drywell Average Vapor Pressure Browns Ferry Nuclear Plant Unit 3







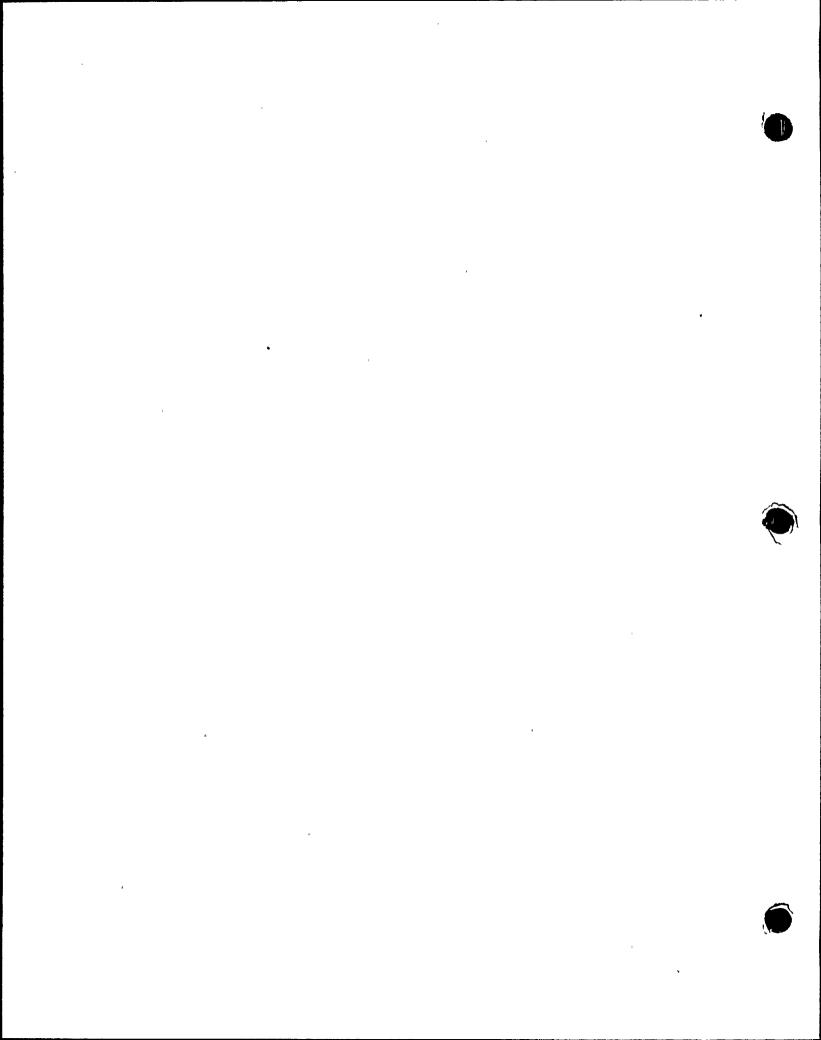


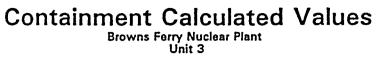
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Containment Calculated Values Browns Ferry Nuclear Plant Unit 3

Page 1 of 2

RDG	TIME	•	MASS	TEMP	VAPOR PRESS	PRESSURE
44	16:43:23	Drywell Torus TOTAL	52010.59 43523.58 95534.17	92.113 87.862	0.3938 .0.5527	65.1584 65.1719
45	16:53:29	Drywell Torus TOTAL	51983.15 43546.98 95530.13	91.937 87.165	0.3946 0.5468	65.1044 65.1185
.,, 46	1,7:03;34	, Drywell, , , Torus TOTAL	51962.79 43557.32 95520.11	91,865 86.777	.0.3967 0.5458	65.0727 . 65.0869
47	17:14:40	Drywell Torus TOTAL	51947.50 43561.82 95509.32	91.782 86.503	0.3983 0.5444	65.0455 65.0599
48	17:24:46	Drywell ' Torus TOTAL	51936.35 43564.81 95501.16	91.712 86.297	0.3994 0.5436	65.0246 65.0391
49	17:34:52	Drywell Torus TOTAL	51928.04 43566.41 95494.45	91.647 86.128	0.3996 0.5432	65.0068 65.0212
50	17:45:57	Drywell Torus TOTAL	51918.59 43569.43 95488.01	91.587 85.948	0.4005 0.5422	64.9889 65.0034
51	17:57:03	Drywell Torus TOTAL	51908.56 43571.51 95480.07	91.542 85.793	0.4017 0.5411	64.9724 64.9870
52	18:07:09	Drywell Torus TOTAL	51900.24 43573.67 95473.92	91.497 85.655	0.4031 0.5400	64.9582 64.9728
53	18:17:15	Drywell Torus TOTAL	51891.04 43576.10 95467.14	91.476 85.527	0.4041 0.5386	64.9452 64.9598
54	18:27:20	Drywell Torus TOTAL	51883.36 · 43579.31 95462.67	91.441 85.395	0.4055 0.5371	64.9330 64.9475
55	18:38:26	Drywell Torus TOTAL	51875.04 43581.78 95456.83	91.406 85.267	0.4069 0.5357	64.9200 64.9346
56	18:49:32	Drywell Torus TOTAL	51866.29 43584.06 95450.35	91.384 85.145	0.4081 0.5343	64.9076 64.9222
57	18:59:38	Drywell Torus TOTAL	51859.32 43586.68 95446.00	91.362 85.035	0.4087 0.5329	64.8971 64.9117





Page 2 of 2

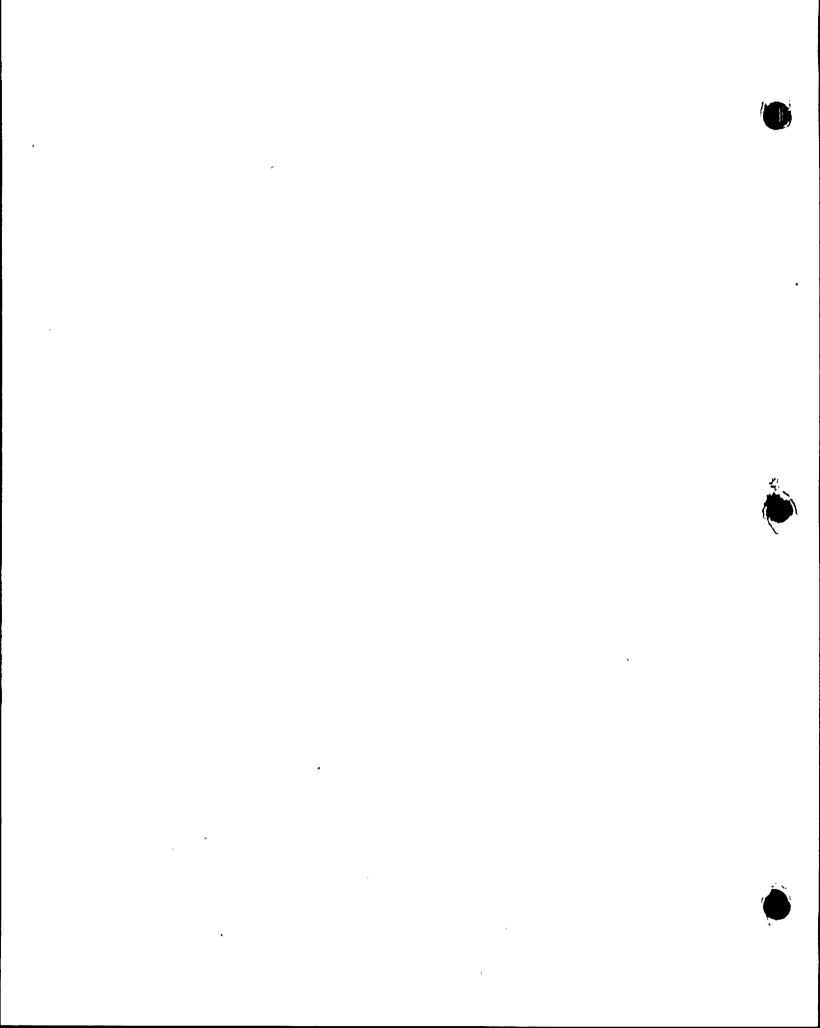
RDG TIME		MASS	TEMP	VAPOR PRESS	PRESSURE
58 19:09:44	Drywell Torus TOTAL	51852.06 43589.10 95441.17			
59 19:19:49	Drywell Torus TOTAL	51845.07 43591.48 95436.56			
60 .19:29:55	. Drywell Torus TOTAL	51838.78 43592.97 95431.75			
61 19:40:01	Drywell Torus TOTAL	51832.02 43595.17 95427.19			
62 19:50:07	Drywell Torus TOTAL	51825.78 43596.68 95422.45			
63 20:00:13	Drywell Torus TOTAL	51819.21 43598.83 95418.04			
64 20:11:18	Drywell Torus TOTAL	51812.58 43600.88 95413.46			
65 20:22:24	Drywell Torus TOTAL	51805.88 43602.65 95408.53			
66 20:32:30	Drywell Torus TOTAL	51798.59 43604.72 95403.31			
67 20:42:36	Drywell Torus TOTAL	51790.77 43604.49 95395.26			
68 20:52:42	Drywell Torus TOTAL	51783.99 43603.72 95387.71			

BN-TOP-1 Temperature Stabilization Browns Ferry Nuclear Plant Unit 3

Page 1 of 1

Containment

TIME	TEMP	AVE. DT OVER LAST 2 HOURS	RATE OF DT CHANGE OVER LAST 2 HOURS
t	т	$\left \frac{T_{t} - T_{t-2}}{2}\right $	
HOURS	٥F	°F/HR	°F/HR/HR
HOURS 16:43 16:53 17:03	90.182 89.769 89.554 89.384 89.252 89.140 89.025 88.931 88.694 88.617 88.550 88.488 88.430 88.374 88.322 88.271 88.322 88.271 88.322 88.271 88.322 88.3181 88.322 88.3181	0.630 0.551 0.498 0.458 0.427 0.417 0.386 0.365 0.343 0.314 0.306 0.291	0.623 0.352 0.262 0.195 0.170 0.152 0.126 0.119 0.106 0.108 0.098 0.098
20:52	87.969	0.283	0.072



Mass Point Temperature Stabilization Browns Ferry Nuclear Plant Unit 3 Containment

Page 1 of 1

1	2	3	4	(5)
TIME	TEMP	AVE. DT OVER LAST 4 HOURS	AVE. DT OVER LAST HOUR	
t	т	[<u>T_t - T_{t-4}</u>]	T _t - T _{t-1}	5 = 3 - 4
HOURS	٥F	°F/HR	°F/HR	°F/HR
				11



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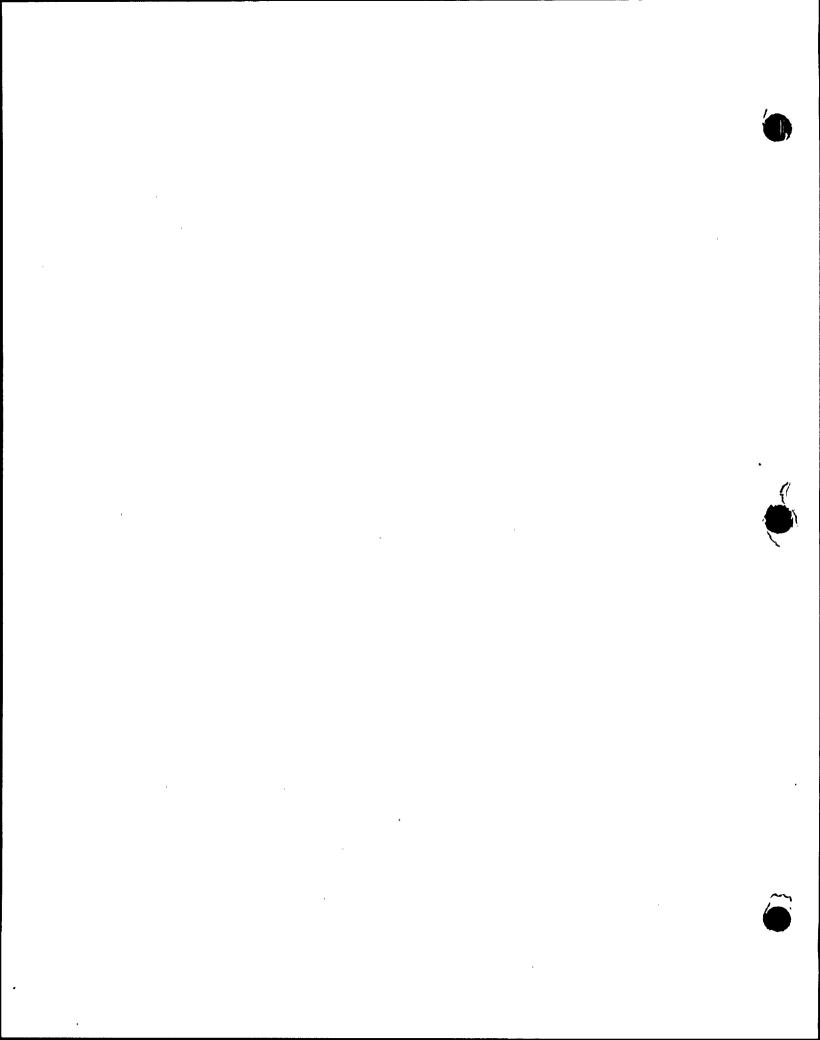
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APPENDIX B

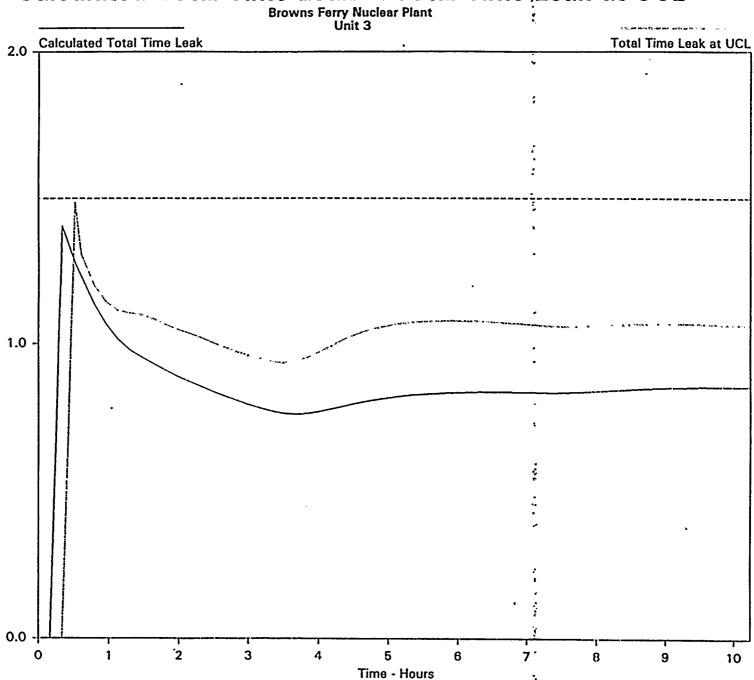
CILRT Test Phase Graphs

(samples 68 to 130)

Conte	nts:	<u>Page</u>
the graph graph with a second of the		
	Containment Total Time Leak Rate & UCL	30
	Containment Mass Point Leak Rate & UCL	31
	Total Containment Mass	32
	Drywell Mass	33
J	Torus Mass	34
	Drywell Average Pressure .	35
	Torus Average Pressure	36
	Drywell Average Temperature	37
	Torus Average Temperature	38
	Drywell Average Vapor Pressure	39
х	Torus Average Vanor Pressure	40



Calculated Total Time Leak & Total Time Leak at UCL

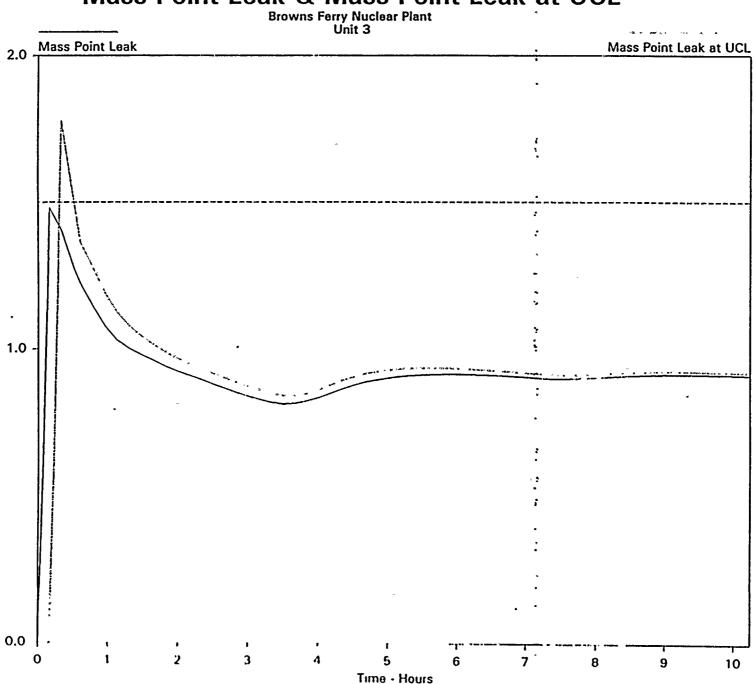


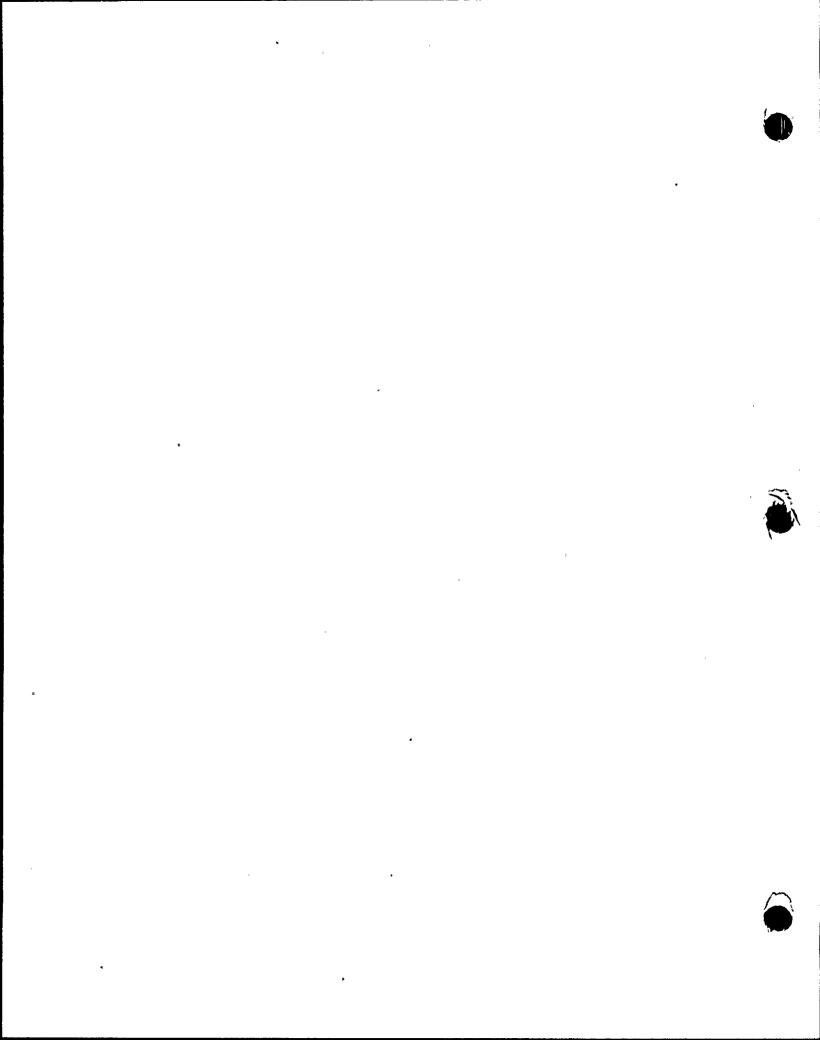


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Mass Point Leak & Mass Point Leak at UCL

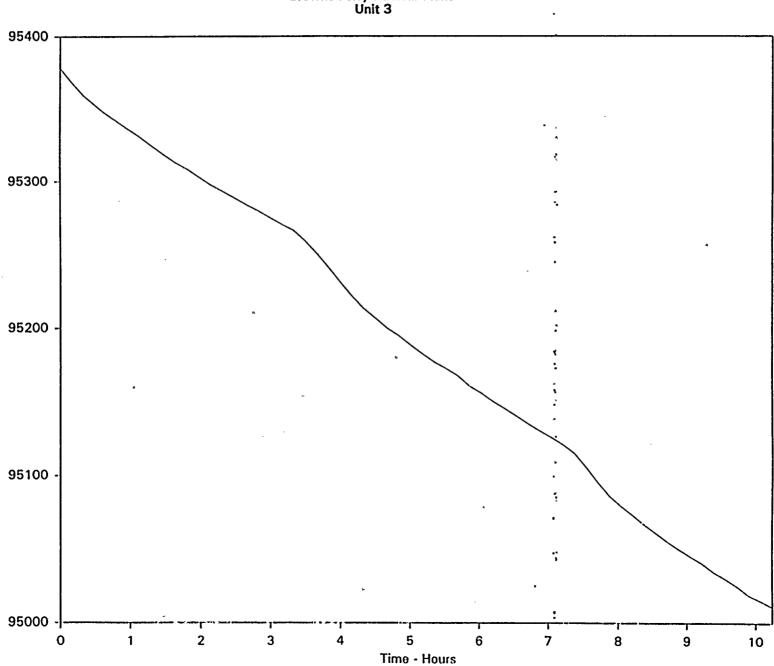




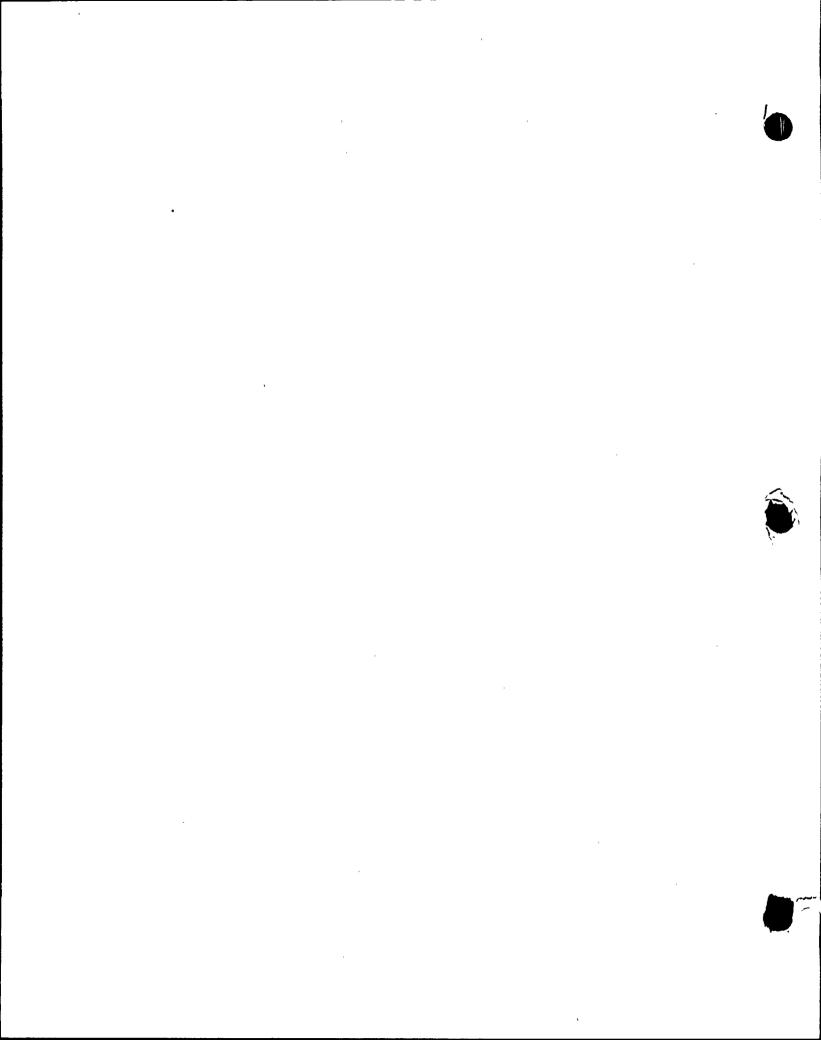


Containment Mass

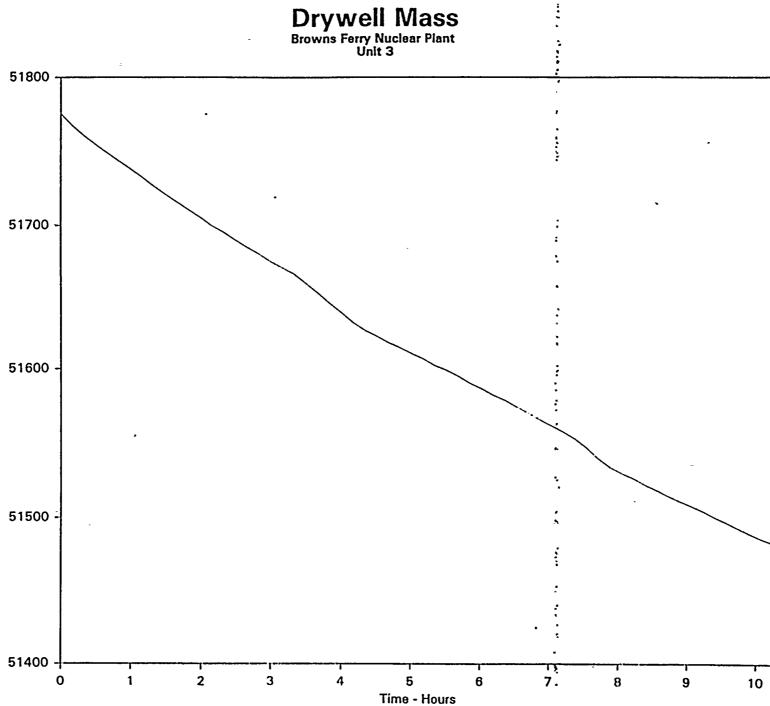
Browns Ferry Nuclear Plant Unit 3



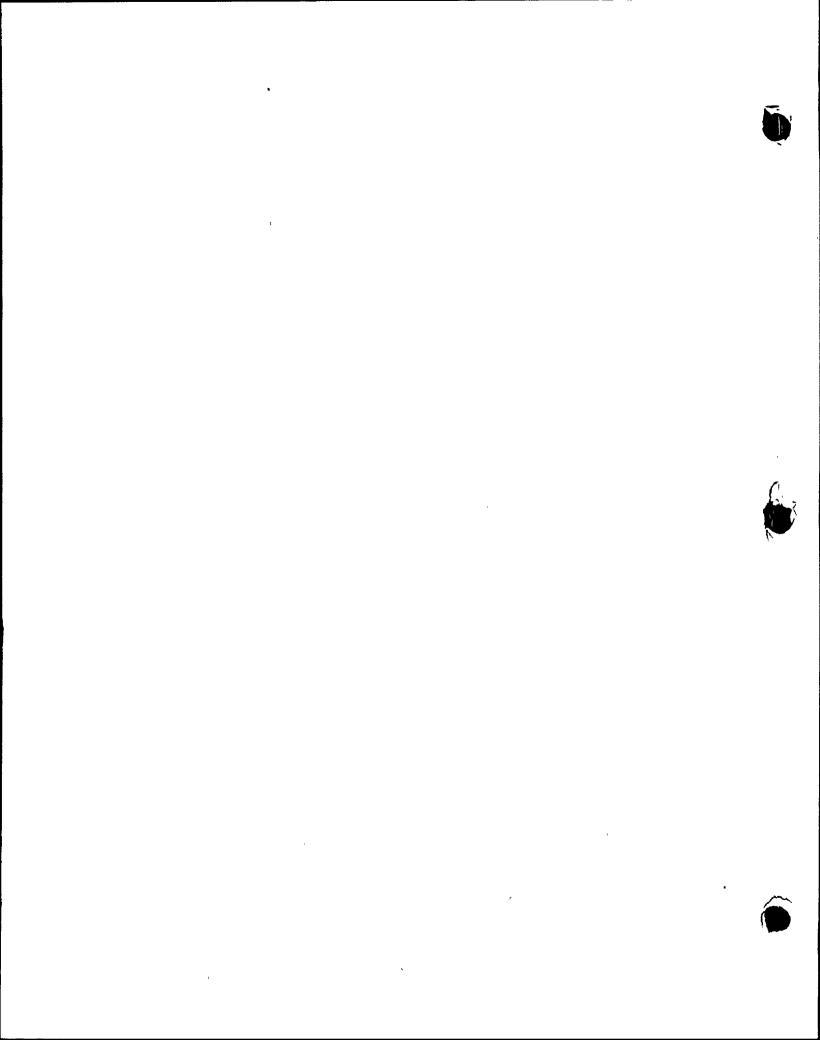
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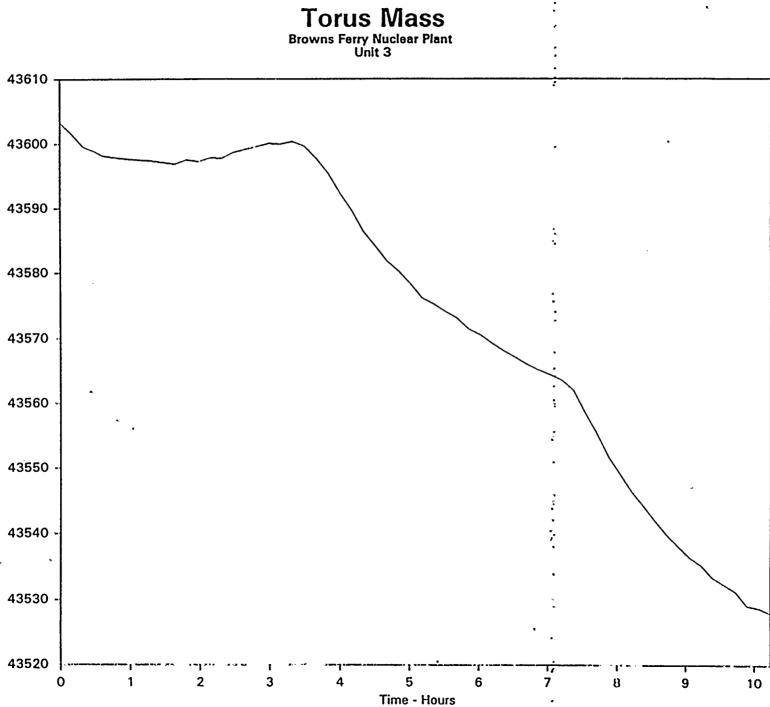




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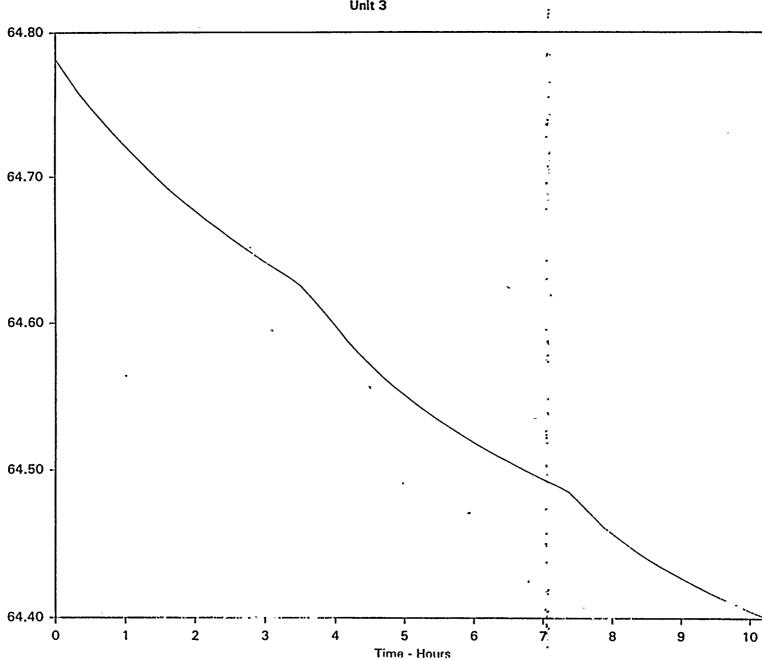
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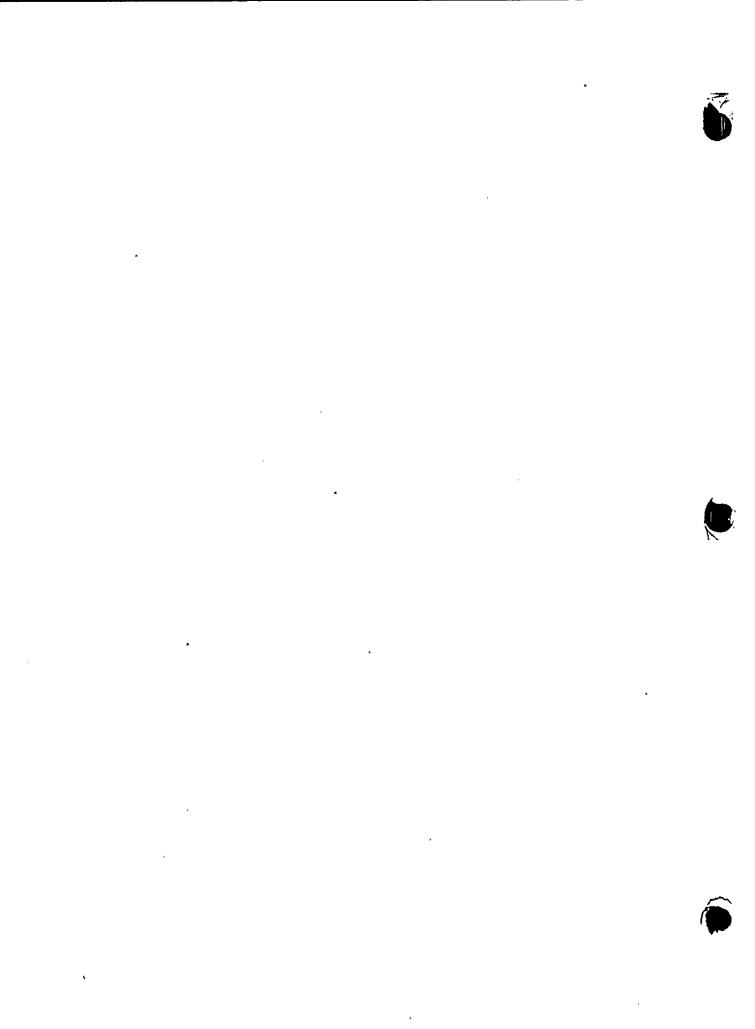




Drywell Average Pressure Browns Ferry Nuclear Plant Unit 3



CILRT TEST PHASE

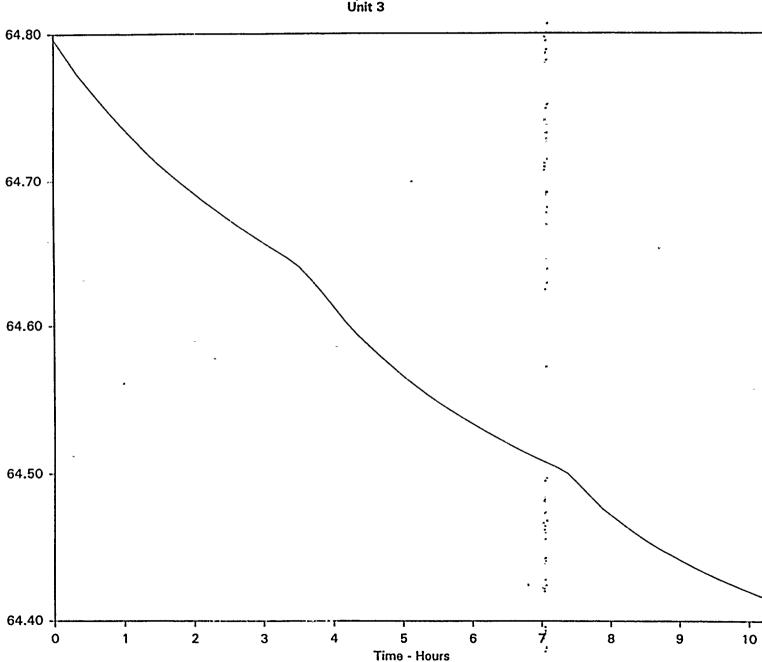


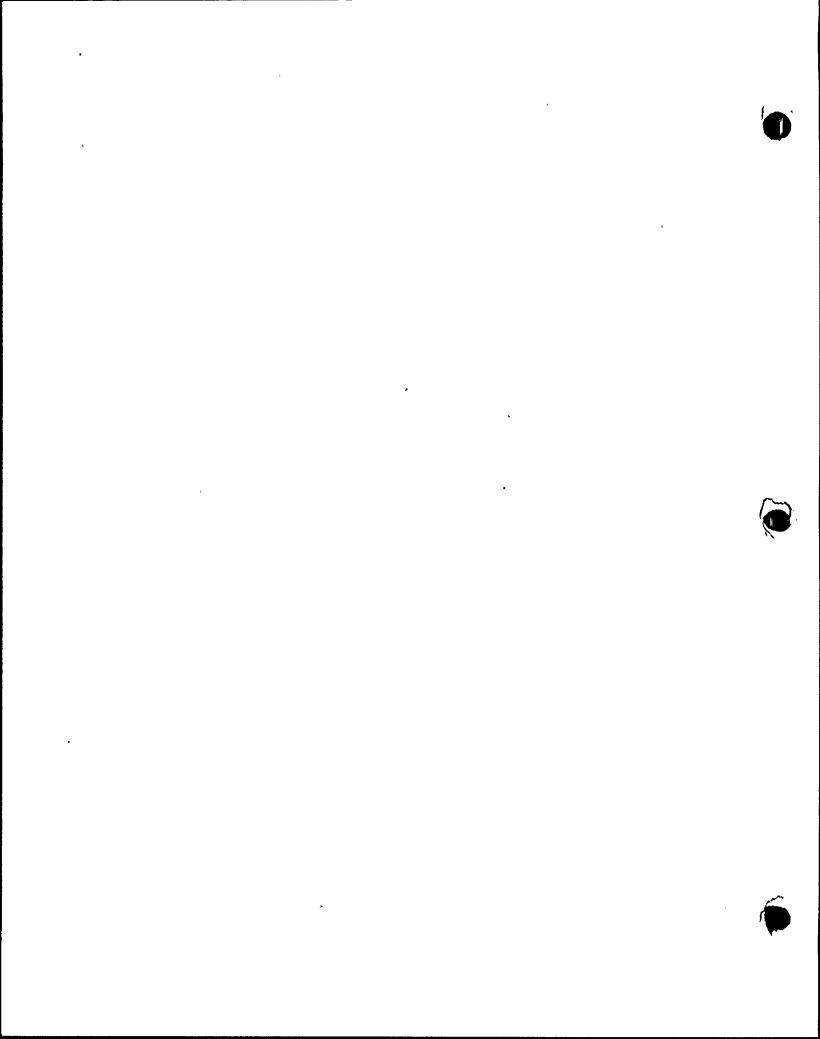
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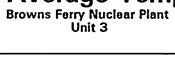
Torus Average Pressure Browns Ferry Nuclear Plant Unit 3

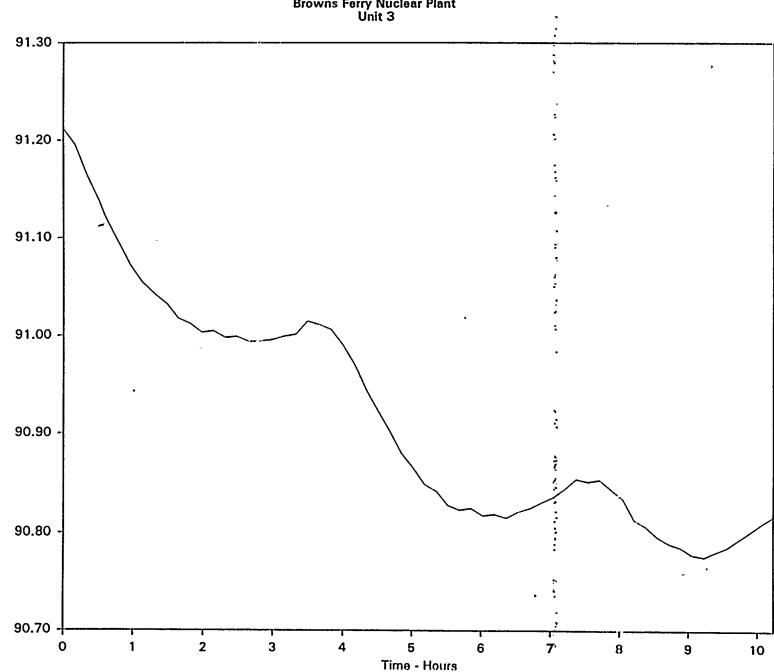






Drywell Average Temperature Browns Ferry Nuclear Plant Unit 3





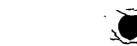


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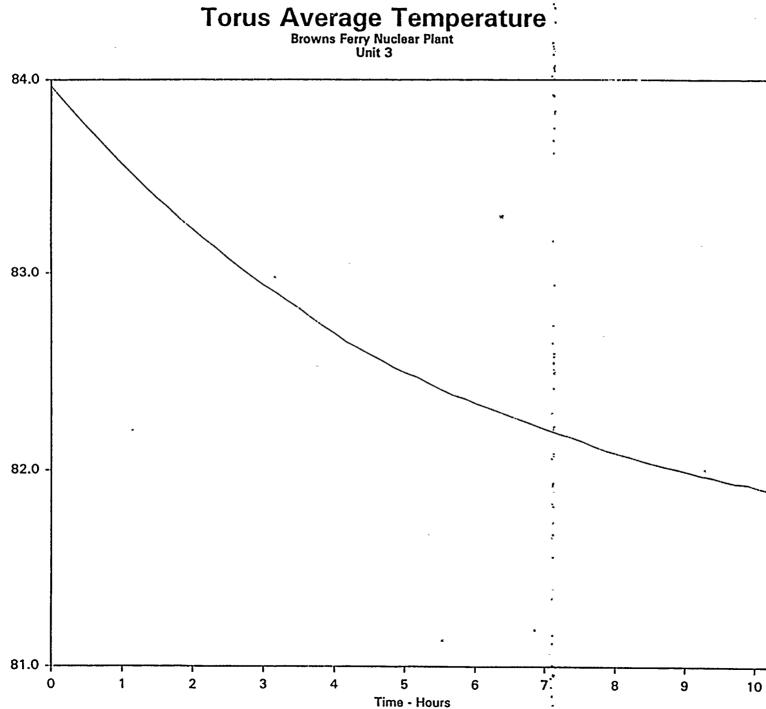
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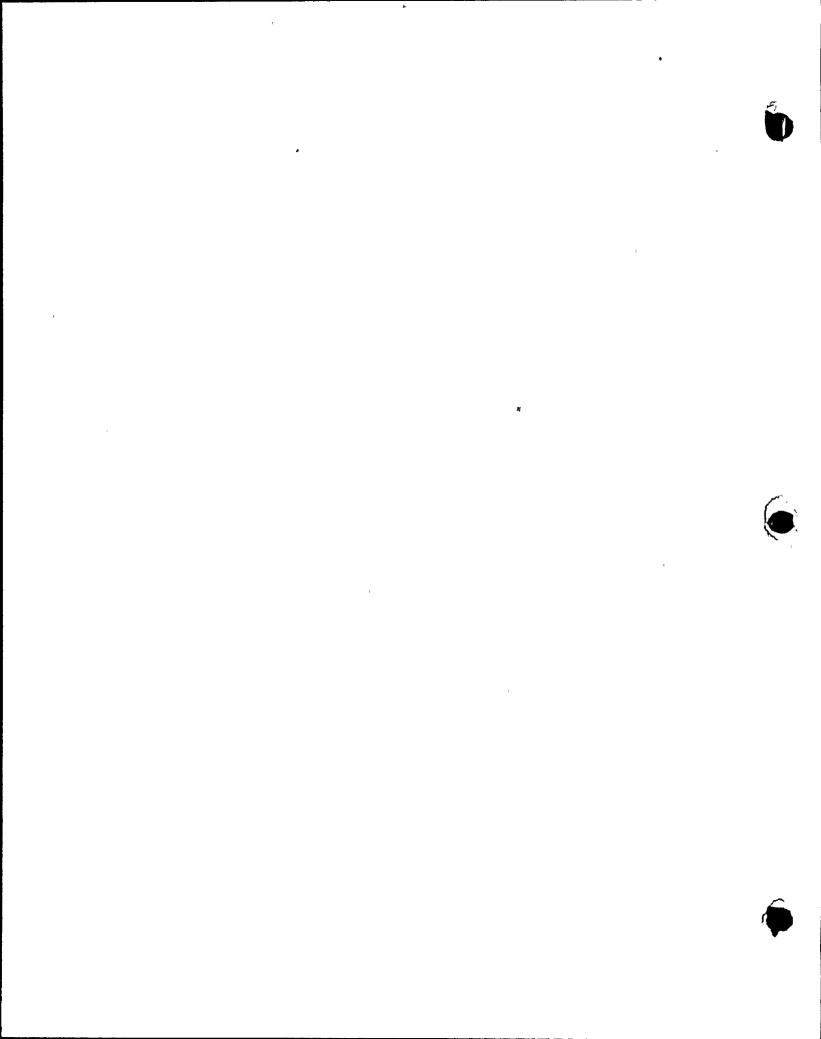
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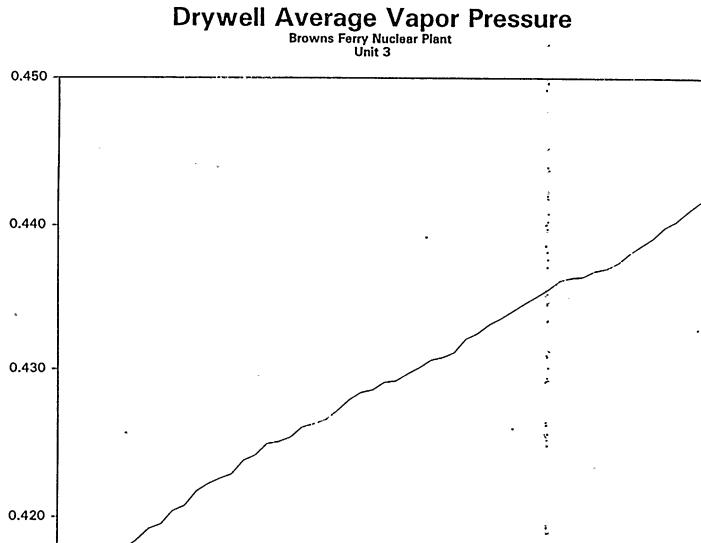








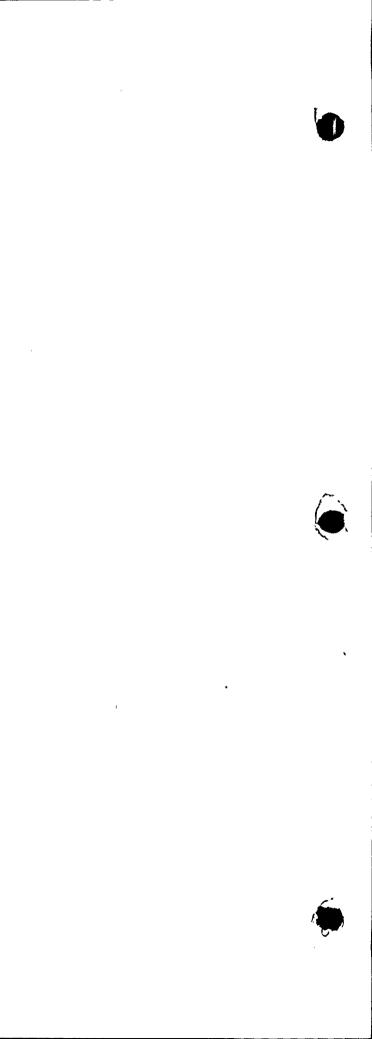




Time - Hours

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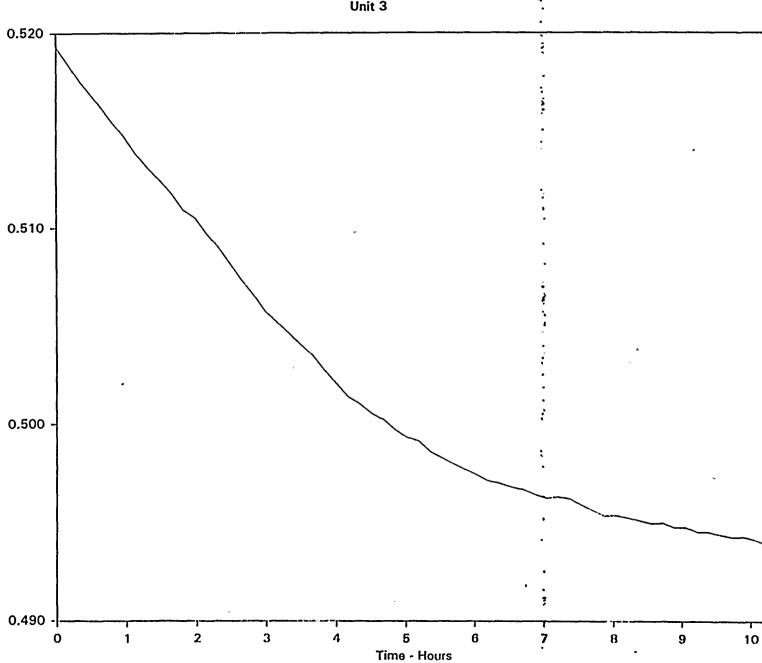


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Torus Average Vapor Pressure Browns Ferry Nuclear Plant Unit 3





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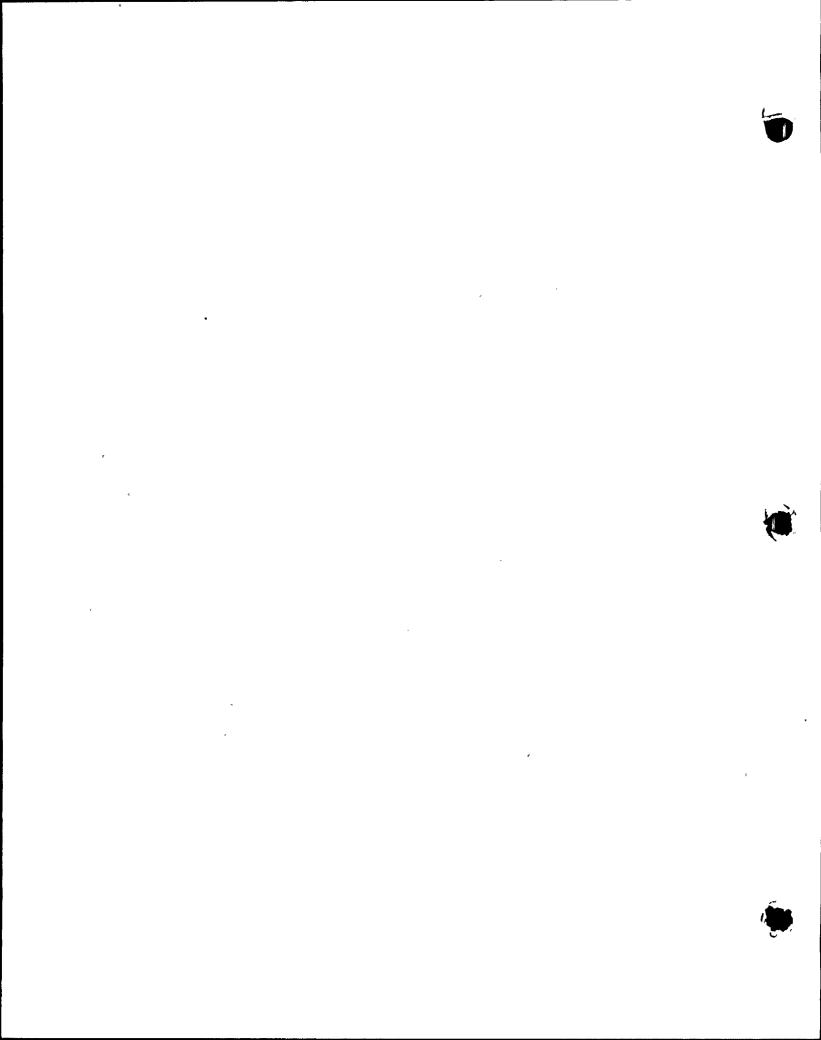
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APPENDIX C

CILRT Test Phase Tabular Data

(samples 68 to 130)

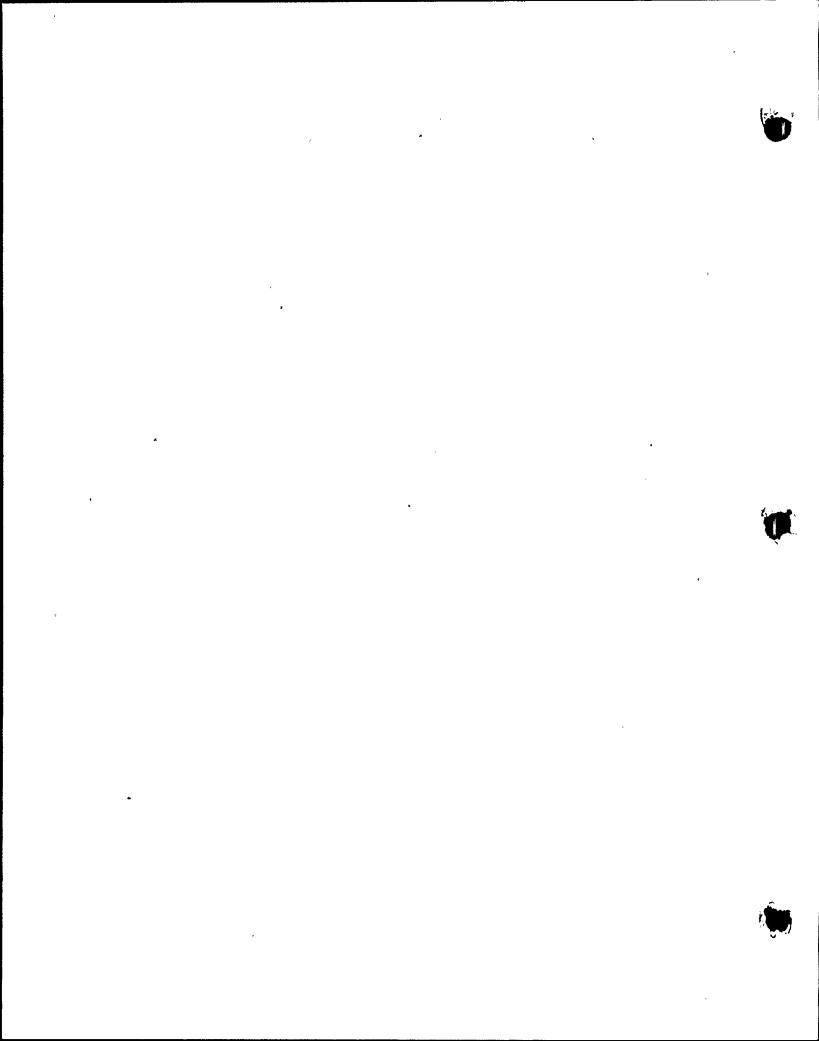
Contents:		<u>Page</u>
	CILRT Total Time Leak Rate Analysis	42
	CILRT Mass Point Leak Rate Analysis	44
	BN-TOP-1 Termination Criteria	46
	CILRT Mass Point Termination Criteria	47
	CILRT Containment Calculated Values	49



Page 1 of 2

Total Time Leak Rate Analysis Browns Ferry Nuclear Plant Unit 3

RDG	TIME (MINUTES)	MEASURED LEAK (WT %/DAY)	CALCULATED LEAK (WT %/DAY)	UCL LEAK (WT %/DAY)
69 70 71 72 73	0.00 10.10 20.20 31.30 36.47	1.480974 1.405476 1.266608 1.231309	1.405476 1.275059 1.2277.77	1.486497 1.304901
74	47.52	1.145211	1.134577	1.197491
75	57.62	1.091352	1.067916	1.143241
76	67.72	1.054852	1.016918	1.112397
77	78.82	1.036872	0.978081	1.102714
78	88.90	1.020993	0.953804	1.096254
79	99.00	1.000184	0.931637	1.083354
80	109.10	0.972956	0.908701	1.063222
81	119.20	0.960181	0.889552	1.047858
82	129.30	0.947023	0.872787	1.034568
83	139.38	0.928243	0.856205	1.019521
84	149.48	0.909589	0.839637	1,003318
85	159.58	0.894976	0.824015	0.987984
86	169.68	0.879511	0.808877	0.972830
87	179.77	0.870198	0.795381	0.959959
88	189.87	0.861251	0.783119	0.948698
89	199.97	0.849322	0.771286	0.937592
90	210.07	0.861303	0.764032	0.934182
91	220.17	0.881297	0.761809	0.939364
92	230.25	0.904832	0.764260	0.952207
93	240.35	0.928264	0.770439	0.970519
94	250.45	0.948538	0.779232	0.991685
95	260.55	0.959950	0.788887	1.012081
96	270.63	0.960992	0.797802	1.028893
97	280.73	0.962510	0.806088	1.043072
98	290.83	0.955550	0.812732	1.053184
99	300.93	0.953954	0.818634	1.061337
100	311.02	0.951553	0.823801	1.067759
101	321.12	0.947106	0.828043	1.072345
102	331.22	0.937545	0.830895	1.074515
103	341.32	0.931710	0.832946	1.075370
104	351.43	0.933765	0.835142	1.076423
105	361.53	0.925752	0.836410	1.076058
106	371.63	0.923392	0.837428	1.075347
107	381.73	0.917515	0.837863	1.073832
108	391.82	0.914330	0.838053	1.072016
109	401.92	0.910813	0.837966	1.069878
110	412.02	0.906254	0.837543	1.067338
111	422.12	0.901533	0.836800	1.064433



Total Time Leak Rate Analysis Browns Ferry Nuclear Plant Unit 3

Page 2 of 2

RDG	TIME (MINUTES)	MEASURED LEAK (WT %/DAY)	CALCULATED LEAK (WT %/DAY)	UCL LEAK (WT %/DAY)
112	432.20	0.898085	0.835893	1.061372
113	442.30	0.898146	0.835123	1.058569
114	452.40	0.910181	0.835516	1.057421
115	462.50	0.923184	0.837040	1.057926
116	472.60	0.934335	0.839435	1.059726
117	482.68	0.936811	0.841926	1.061642
118	492.78	0.936068	0.844229	1.063262
. 119	502.88	0.936823	0.846483	1.064797
120	512.98	0.935239	0.848514	1.065992
121	523.07	0.934571	0.850412	1.066991
122	533.17	0.932058	0.852038	1.067607
123	543.27	0.928345	0.853333	1.067765
124 ·	553.37	0.924167	0.854290	1.067471
125	563.45	0.923163	0.855160	1.067081
126	573.55	0.919158	0.855731	1.066314
127	583.65	0.916154	0.856099	1.065305
128	593.75	0.916076	0.856472	1.064334
129	603.85	0.910166	0.856468	1.062900
130	613.93	0.904978	0.856166	1.061117



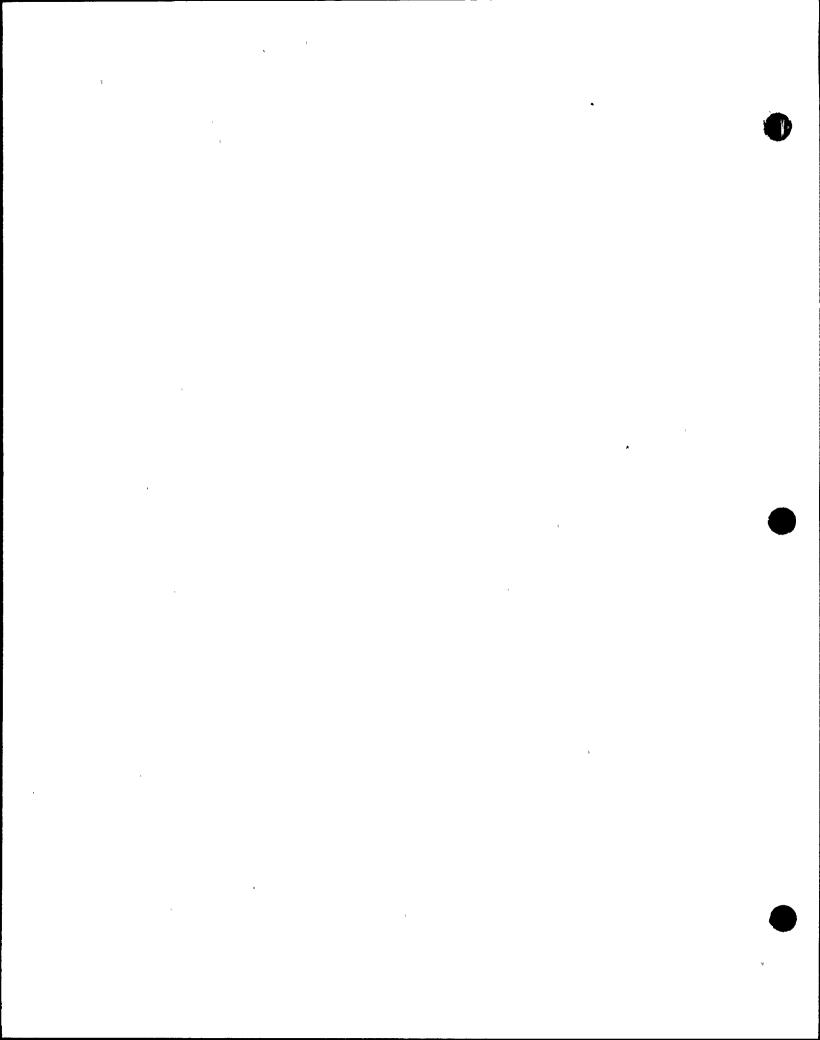


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Mass Point Leak Rate Analysis Browns Ferry Nuclear Plant Unit 3

Page 1 of 2

RDG	TIME (MINUTES)	NORM. MASS	MEASURED LEAK (WT %/DAY)	UCL LEAK (WT %/DAY)
69 70 71 72 73	0.00 10.10 20.20 31.30 36.47	1.000000 0.999896 0.999803 0.999725 0.999688	1.480974 1.405478 1.270295 1.221265	1.778417 1.496087 1.362384
74 75 76 	47.52 57.62 67.72 78.82 88.90	0.999622 0.999563 0.999504 0.999432 0.999370	1.142417 1.078264 . 1.031056 1.001103 0.980539	1.272263 1.191702 1.127073 1.079079 1.044650
79	99.00	0.999312	0.961881	1.016620
80	109.10	0.999263	0.941131	0.990729
81	119.20	0.999205	0.924748	0.969371
82	129.30	0.999150	0.910675	0.951096
83	139.38	0.999102	0.895917	0.933692
84	149.48	0.999056	0.880632	0.916860
85	159.58	0.999008	0.866178	0.901089
86	169.68	0.998964	0.851971	0.885944
87	179.77	0.998914	0.839633	0.872292
88	189.87	0.998864	0.828685	0.859916
89 90 91 92 93	199.97 210.07 220.17 230.25 240.35	0.998821 0.998744 0.998653 0.998553	0.817931 0.813236 0.814979 0.822396 0.834112	0.848040 0.840910 0.840229 0.846614 0.859164
94	250.45	0.998350	0.848449	0.875502
95	260.55	0.998263	0.862964	0.891754
96	270.63	0.998194	0.875497	0.904886
97	280.73	0.998124	0.886486	0.915853
98	290.83	0.998070	0.894604	0.923105
99	300.93	0.998006	0.901326	0.928751
100	311.02	0.997945	0.906738	0.932955
101	321.12	0.997888	0.910703	0.935604
102	331.22	0.997844	0.912604	0.936086
103	341.32	0.997792	0.913373	0.935502
104	351.43	0.997721	0.914427	0.935331
105	361.53	0.997676	0.914174	0.933931
106	371.63	0.997617	0.913654	0.932360
107	381.73	0.997568	0.912391	0.930166
108	391.82	0.997512	0.910875	0.927811
109	401.92	0.997458	0.909093	0.925285
110	412.02	0.997407	0.906942	0.922492
111	422.12	0.997357	0.904449	0.919463



Mass Point Leak Rate Analysis Browns Ferry Nuclear Plant Unit 3

Page 2 of 2

	RDG TI	ME (MINUTES)	NORM. MASS	MEASURED LEAK (WT (A)	UCL LEAK (WT %/DAY)
,	112	432.20	0.997304	0.901825	0.916372
	113	442.30	0.997241	0.899533	0.913602
	114	452.40	0.997141	0.899022	0.912481
	115	462.50	0.997035	0.900189	0.913118
	116	472.60	0.996934	0.902608	0.915211
se, e se e	117	482.68	0.996860	0.905110	0.917434
	118	492.78	0.996797	0.907312	0.919328
	119	502.88	0.996728	0.909416	0.921133
	120	512.98	0.996668	0.911169	0.922559
	121	523.07	0.996605	0.912710	0.923765
	122	533.17	0.996549	0.913861	0.924561
	123	543.27	0.996498	0.914537	0.924865
	124	553.37	0.996449	0.914739	0.924696
	125	563.45	0.996388	0.914835	0.924440
	126	573.55	0.996339	0.914538	0.923813
	127	583.65	0.996287	0.913984	0.922957
	128	593.75	0.996223	0.913479	0.922164
	129	603.85	0.996183	0.912466	0.920920
	130	613.93	0.996142	0.911060	0.919351

BN-TOP-1 Termination Criteria

Browns Ferry Nuclear Plant Unit 3 Page 1 of 1

BN-TOP-1 Termination Criteria Evaluation for Reading # 130

1. The Trend Report based on Total Time calculations shall indicate that the magnitude of the calculated leak rate is tending to stabilize at a value less than the maximum allowable leak rate (<.75La).

Required Value: 1.500000, %/day, Actual Value: 0.856166 %/day

(Note: The magnitude of the calculated leak rate may be increasing slightly as it tends to stabilize. In this case the average rate of increase of the calculated leak rate shall be determined from the accumulated data over the last five hours or last twenty data points, whichever provides the most points. Using this average rate, the calculated leak rate can then be linearly extrapolated to the 24th hour data point. If this extrapolated value of the calculated leak rate exceeds 75% of the maximum allowable leak rate (La) then the leak rate test is continued.)

Required Value: 1.500000 %/day Actual Value: 0.939964 %/day

2. The end of test upper 95% confidence limit for the calculated leak rate based on Total Time calculations shall be less than the maximum allowable leak rate (<.75La).

Required Value: 1.500000 %/day Actual Value: 1.061117 %/day

3. The mean of the measured leak rates based on Total Time calculations over the last five hours of test or last twenty data points, whichever provides the most data, shall be less than the maximum allowable leak rate (<.75La).

Required Value: 1.500000 %/day Actual Value: 0.923193 %/day

4. Data shall be recorded at approximately equal intervals and in no case at intervals greater than one hour.

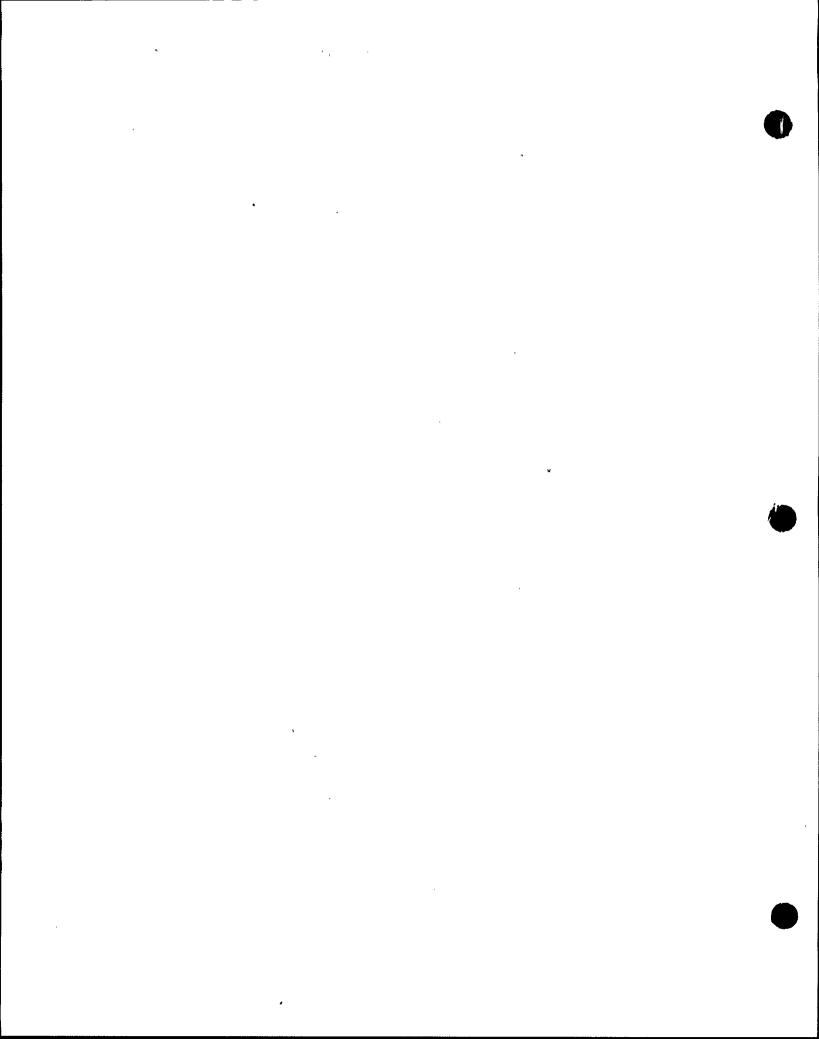
Required Interval: <=1 hr Maximum Actual Interval: 0.19 hr

5. At least twenty (20) data points shall be provided for proper statistical analysis.

Required # Data Points: > = 20 Actual Data Points: 62

6. In no case shall the minimum test duration be less than six (6) hours.

Required Minimum Duration: 6 hr Actual Duration: 10.2 hr



Mass Point Termination Criteria Browns Ferry Nuclear Plant Unit 3

RDG	TIME	MP UCL %/day	Curv 11	Curv 111	Curv 12	Scat 21
69 70 71 72 73	0.00 10.10 20.20 31.30 36.47	0.0000 0.0000 1.7784 1.4961 1.3624	0.3105 3.6894	27.1827 24.3021	- - 89.9864 75.3850	0.0000 1.0000 1.1254 1.2107 1.2441
74 75 76 77 78 ·	47.52 57.62 67.72 78.82	1.2723 1.1917 1.1271 1.0791	10.9491 11.9522 9.1679 4.8551	20.4870 17.0825 13.8720 10.2768 7.9209	57.7076 44.7689 34.5840 24.8526 18.₹689	1.3300 1.3915 1.4428 1.4872
79	99.00	1.0166	4.1530	6.5511	15.2442	1.5347
80	109.10	0.9907	5.8624	5.9601	13.5972	1.5601
81	119.20	0.9694	6.9320	5.2691	11.8376	1.5818
82	129.30	0.9511	7.8073	4.6669	10.3493	1.6014
83	139.38	0.9337	9.9932	4.3272	9.4678	1.6218
84	149.48	0.9169	13.6001	4.1361	8.9260	1.6435
85	159.58	0.9011	17.8426	3.9526	8.4213	1.6647
86	169.68	0.8859	23.3567	3.8093	8.0157	1.6863
87	179.77	0.8723	27.2274	3.6002	7.4950	1.7060
88	189.87	0.8599	29.3555	3.3719	6.9541	1.7244
89	199.97	0.8480	32.8290	3.1931	6.5255	1.7428
90	210.07	0.8409	19.1766	2.7550	5.6080	1.7521
91	220.17	0.8402	6.8607	2.1130	4.3075	1.7496
92	230.25	0.8466	1.8814	1.3586	2.7872	1.7355
93	240.35	0.8592	0.2675	0.5823	1.2066	1.7128
94	250.45	0.8755	0.0134	-0.1381	0.2897	1.6856
95	260.55	0.8918	0.3643	-0.7149	1.5190	1.6594
96	270.63	0.9049	0.9705	-1.0957	2.3540	1.6385
97	280.73	0.9159	1.7279	-1.3422	2.9120	1.6213
98	290.83	0.9231	2.4217	-1.4344	3.1349	1.6096
99	. 300.93	0.9288	3.0751	-1.4589	3.2080	1.6003
100	311.02	0.9330	3.6154	-1.4330	3.1665	1.5930
101	321.12	0.9356	3.9241	-1.3620	3.0207	1.5878
102	331.22	0.9361	3.7552	-1.2344	2.7425	1.5855
103	341.32	0.9355	3.3483	-1.0911	2.4259	1.5846
104	351.43	0.9353	3.1094	-0.9795	2.1799	1.5832
105	361.53	0.9339	2.5981	-0.8453	1.8806	1.5834
106	371.63	0.9324	2.1340	-0.7233	1.6085	1.5838
107	381.73	0.9302	1.6129	-0.5978	1.3277	1.5851
108	391.82	0.9278	1.1666	-0.4831	1.0716	1.5867
109	401.92	0.9253	0.7870	-0.3773	0.8354	1.5885
110	412.02	0.9225	0.4637	-0.2759	0.6098	1.5908
111	422.12	0.9195	0.2145	-0.1791	0.3949	1.5935
112	432.20	0.9164	0.0618	-0.0916	0.2016	1.5963
113	442.30	0.9136	0.0046	-0.0238	0.0523	1.5987
114	452.40	0.9125	0.0007	-0.0087	0.0190	1.5989
115	462.50	0.9131	0.0139	-0.0361	0.0793	1.5969
116	472.60	0.9152	0.0953	-0.0900	0.1982	1.5930
117	482.68	0.9174	0.2529	-0.1395	0.3077	1.5891

Mass Point Termination Criteria Browns Ferry Nuclear Plant Unit 3

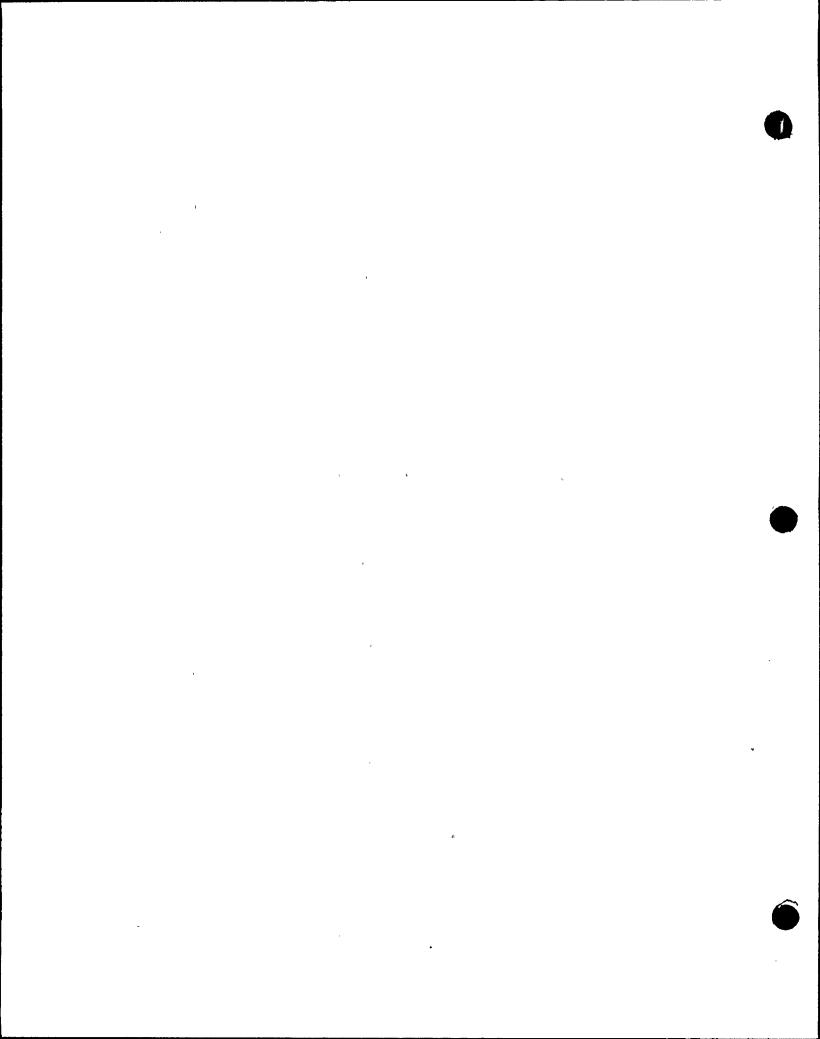
Page 2 of 2

RDG	TIME	MP UCL %/day	Curv 11	Curv 111	Curv 12	Scat 21	
118	492.78	0.9193	0.4505	-0.1763	0.3899	1.5856	
119	502.88	0.9211	0.6913	-0.2068	0.4581	1.5823	
120	512.98	0.9226	0.9265	-0.2262	0.5018	1.5795	
121		0.9238	1.1579	-0.2388	0.5306	1.5770	
122	533.17	0.9246	1.3314	-0.2418	0.5379	1.5750	
123	543.27	0.9249	1.4011	-0.2346	0.5222	1.5737	
124	553.37	0.9247	1.3485	-0.2185	0.4863	1.5729	
125	563.45	0.9244	1.2739	-0.2018	0.4493	1.5723	
126	573.55	0.9238	1.0997	-0.1791	0.3986	1.5722	
127	58365	0.9230	0.8805	-0.1536,,,	0.3416	1,5724	• • • • • • • • • • • • • • • • • • • •
128	593.75	0.9222	0.7040	-0.1315	0.2924	1.5725	
129	603.85	0.9209	0.4538	-0.1019	0.2264	1.5733	
130	613.93	0.9194	0.2128	-0.0679	0.1506	1.5745	

Containment Calculated Values
Browns Ferry Nuclear Plant
Unit 3

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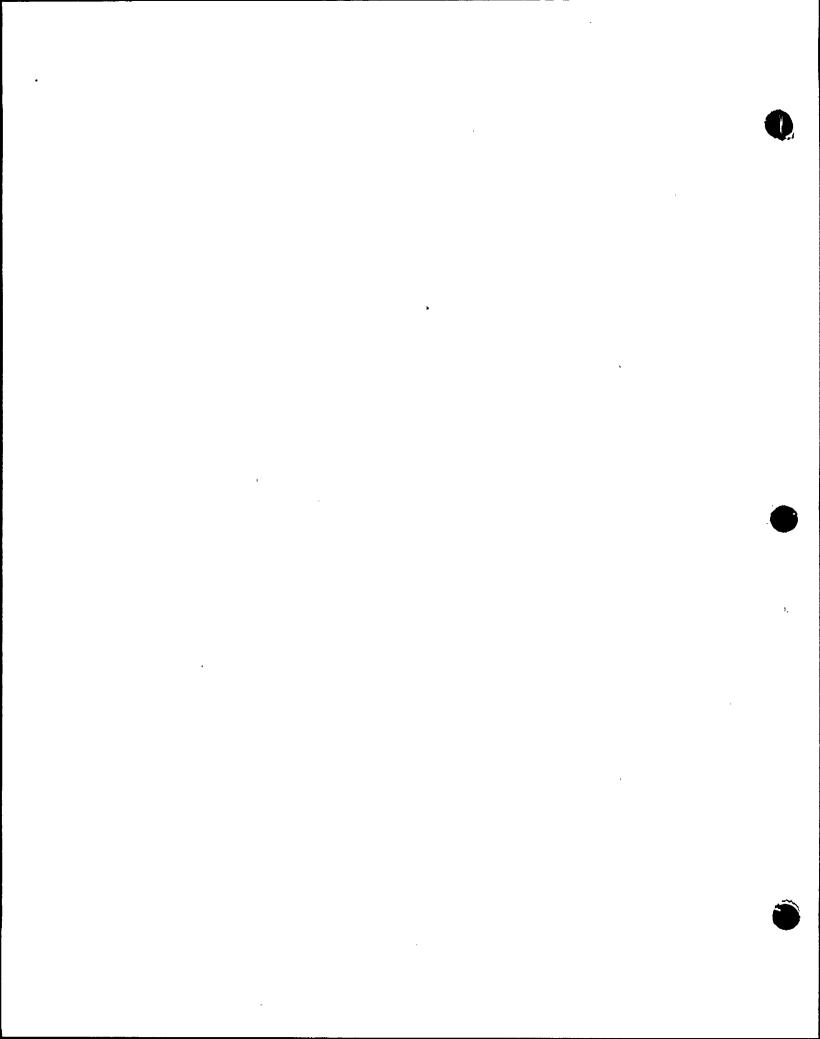
RDG	TIME	•	MASS	TEMP	VAPOR PRESS	PRESSURE
69	21:02:48	Drywell Torus TOTAL	51775.38 43603.31 95378.69	91.212 83.968	0.4154 0.5193	64.7818 64.7964
70	21:12:54	Drywell Torus TOTAL	51767.21 43601.57 95368.78	91.196 83.898	0.4155 0.5185	64.7699 64.7848
	21;23:00	Drywell Torus TOTAL	51760.34 43599.55 95359.88	91.165	0.4158 0.5176	64.7581 64.7729
[*] 72	21:34:06	Drywell Torus TOTAL	51753.70 43598.73 95352.43	91.137 83.755	0.4164 0.5168	64.7472 64.7620
73	21:39:16	Drywell Толиs TOTAL	51750.74 43598.21 95348.95	91.121 83.722	0.4170 0.5164	64.7422 64.7569
74	21:50:19	Drywell Torus TOTAL	51744.73 43597.92 95342.65	91.096 83.647	0.4173 0.5155	64.7320 64.7467
75	22:00:25	Drywell Torus TOTAL	51739.34 43597.70 95337.04	91.073 83.582	0.4178 0.5148	64.7232 64.7380
76	22:10:31	Drywell Torus TOTAL	51733.81 43597.56 95331.38	91.055 83.520	0.4184 0.5139	64.7149 64.7296
77	22:21:37	Drywell Torus TOTAL	51727.13 43597.43 95324.56	91.043 83.452	0.4192 0.5131	64.7059 64.7206
78	22:31:42	Drywell Torus TOTAL	51721.39 43597.18 95318.57	91.032 83.393	0.4195 0.5125	64.6979 64.7127
79	22:41:48	Drywell Torus . TOTAL	51716.20 43596.91 95313.10	91.018 83.342	0.4205 0.5118	64.6907 64.7055
80	22:51:54	Drywell Torus TOTAL	51710.81 43597.57 95308.38	91.012 83.282	0.4208 0.5110	64.6837 64.6985
81	23:02:00	Drywell Torus TOTAL	51705.55 43597.33 95302.88	91.003 83.232	0.4218 0.5105	64.6771 64.6918
82	23:12:06	Drywell Torus TOTAL	51699.75 43597.84 95297.58	91.005 83.178	0.4223 0.5097	64.6705 64.6854



Containment Calculated Values Browns Ferry Nuclear Plant Unit 3

Page 2 of 5

RDG	TIME		MASS	TEMP	VAPOR PRESS	PRESSURE
83	23:22:11	Drywell Torus TOTAL	51695.18 43597.81 95292.99			
84	23:32:17	Drywell Torus TOTAL	51689.94 43598.69 95288.63			
85	23:42:23	Drywell _ , , , , Torus TOTAL	51684.96 43599.13 95284.09			
86	23:52:29	Drywell Torus TOTAL	51680.26 43599.58 95279.84			
87	00:02:34	Drywell - Torus TOTAL	51675.01 43600.07 95275.08			
88	00:12:40	Drywell Torus TOTAŁ	51670.40 43599.98 95270.38			
89	00:22:46	Drywell Torus TOTAL	51665.86 43600.34 95266.20			
90	00:32:52	Drywell Torus TOTAL	51659.22 43599.63 95258.85			
91	00:42:58	Drywell Torus TOTAL	51652.39 43597.78 95250.17			
92	00:53:03	Drywell Torus TOTAL	51645.25 43595.45 95240.70			
93	01:03:09	Drywell Torus TOTAL	51638.58 43592.33 95230.91			
94	01:13:15	Drywell Torus TOTAL	51631.77 43589.57 95221.34			
95	01:23:21	Dryweli Torus TOTAL	51626.66 43586.37 95213.03			
96	01:33:26	Drywell Torus TOTAL	51622.27 43584.15 95206.43			



Containment Calculated Values Browns Ferry Nuclear Plant Unit 3

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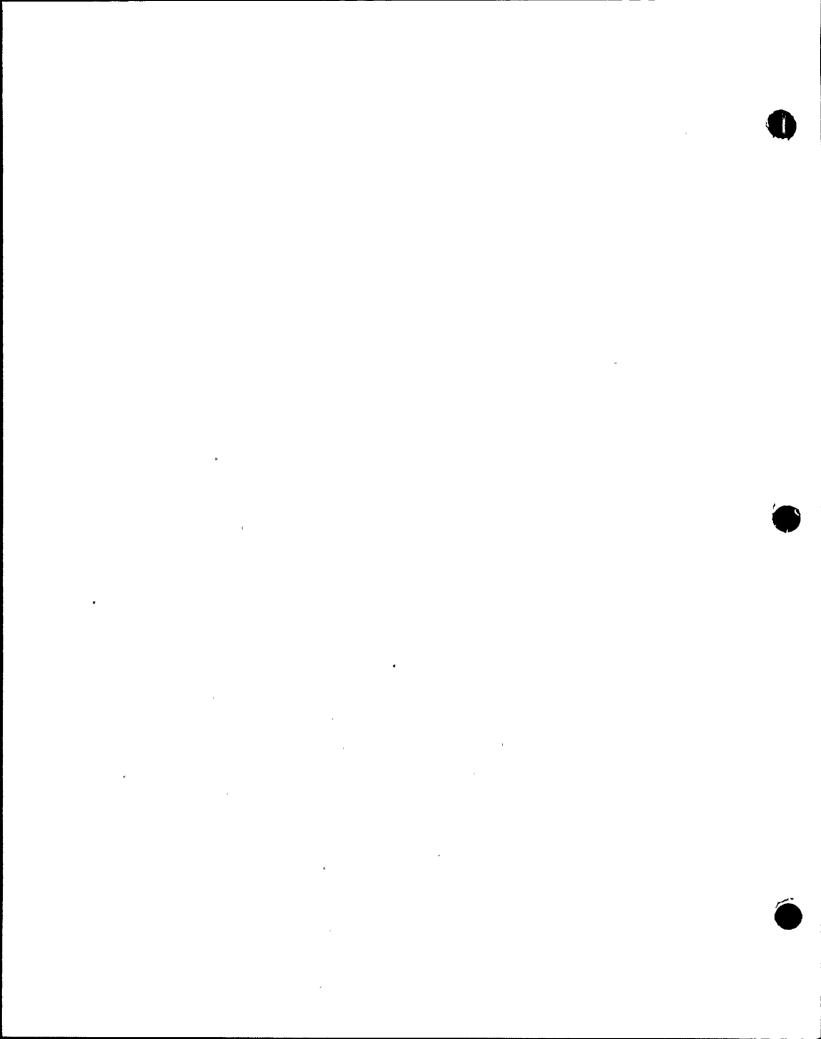
RDG TIME		MASS	TEMP	VAPOR PRESS	PRESSURE
97 01:43:32	Drywell Torus TOTAL	51617.86 43581.85 95199.72			
98 01:53:38	Drywell Torus TOTAL	51614.36 43580.26 95194.62			
99 02:03:44,	Drywell Torus TOTAL	51610.26 43578.28 95188.54			
100 02:13:49	Drywell Torus TOTAL	51606.57 43576.09 95182.67			
101 02:23:55	Drywell . Torus TOTAL	51602.09 43575.16 95177.25			
102 02:34:01	Drywell Torus TOTAL	51598.93 43574.08 95173.01			
103 02:44:07	Drywell Torus TOTAL	51594.96 43573.09 95168.06			
104 02:54:14	Drywell Torus TOTAL	51589.98 43571.36 95161.33			
105 03:04:20	Drywell Torus TOTAL	51586.49 43570.52 95157.01			
106 03:14:26	Drywell Torus TOTAL	51582.16 43569.23 95151.39			
107 03:24:32	Drywell Torus TOTAL	51578.64 ³ 43568.06 95146.70			
108 03:34:37	Drywell Torus TOTAL	51574.32 43567.08 95141.40			
109 03:44:43	Drywell Torus TOTAL	51570.21 43566.01 95136.22			
110 03:54:49	Drywell Torus TOTAL	51566.24 43565.14 95131.37			

Containment Calculated Values

Page 4 of 5

Browns Ferry Nuclear Plant Unit 3

RDG	TIME		MASS	TEMP .	VAPOR PRESS	PRESSURE
111 04	:04:55	Drywell Torus TOTAL	51562.21 43564.42 95126.63			
112 04	:15:00	Drywell Torus TOTAL	51558.04 43563.55 95121.60			
113 04		Drywell ·· Torus TOTAL	51553.56 43562.01 95115.57	90.854 82.172	0.4364 0.4962	64.4855 64.5003
114 04	:35:12	Drywell Torus . TOTAL	51547.38 43558.57 95105.96			
115 04	:45:18	Drywell . Torus TOTAL	51540.40 43555.48 95095.88			
116 04	:55:24	Drywell Torus TOTAL	51534.46 43551.76 95086.22			
117 05	:05:29	Drywell Torus TOTAL	51530.19 43549.00 95079.18			
118 05	:15:35	Drywell Torus TOTAL	51526.82 43546.34 95073.16			
119 05	:25:41	Drywell . Torus TOTAL	51522.44 43544.21 95066.65			
120 05	:35:47	Drywell Torus TOTAL	51518.90 43542.02 95060.92			
121 05	:45:52	Drywell Torus TOTAL	51514.98 43539.92 95054.90			
122 05	:55:58	Drywell Torus TOTAL	51511.40 43538.14 95049.54			
123 06	:06:04	Drywell Torus TOTAL	51508.19 43536.45 95044.64			
124 06	:16:10	Drywell Torus TOTAL	51504.73 43535.23 95039.96			



Containment Calculated Values Browns Ferry Nuclear Plant Unit 3

RDG TIME		MASS ,	TEMP	VAPOR PRESS	PRESSURE
125 06:26:15	Drywell Torus TOTAL	51500.79 43533.37 95034.16			
126 06:36:21	Drywell Torus TOTAL	51497.17 43532.34 95029.51			
127 06:46:27	Drywell Torus TOTAL	51493.29 			
128 06:56:33	Drywell Torus TOTAL	51489.33 . 43529.09 95018.42			
129 07:06:39	Drywell Torus TOTAL	51485.92 43528.73 95014.66			
130 07:16:44	Drywell Torus TOTAL	51482.74 43527.95 95010.69			

APPENDIX D

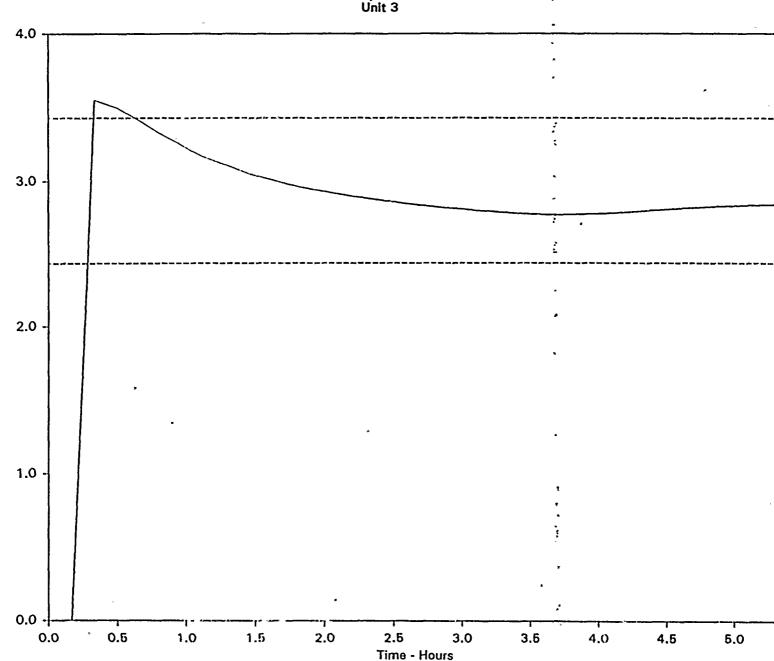
Verification Test Phase Graphs

(samples 139 to 197)

Contents:	<u>Page</u>
Containment Total Time Leak Rate with Agreement Limits	55
Containment Mass Point Leak Rate with Agreement Limits	56
Total Containment Mass	57
Drywell Mass	58
Torus Mass	59
Drywell Average Pressure	60
Torus Average Pressure	61
Drywell Average Temperature	62
Torus Average Temperature	63
Drywell Average Vapor Pressure .	64
Torus Average Vapor Pressure	65

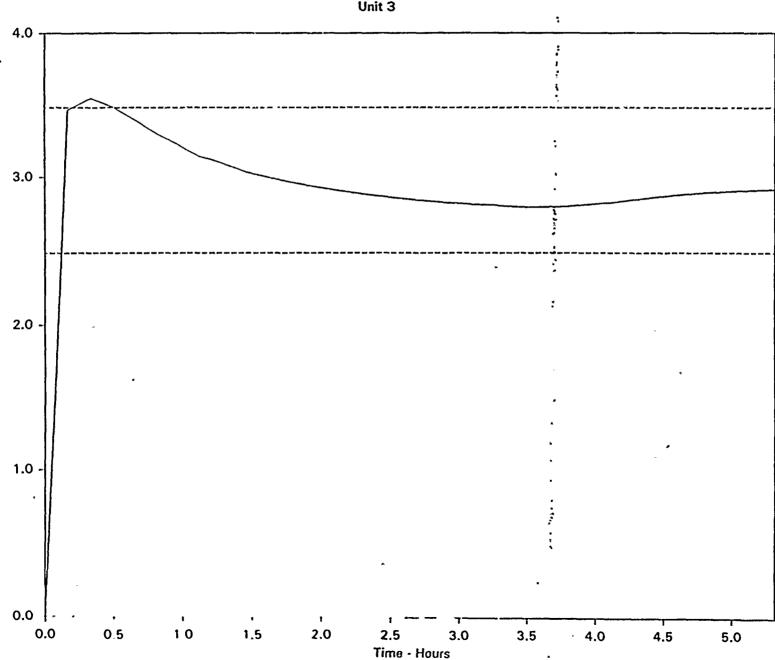
Calculated Total Time Leak

Browns Ferry Nuclear Plant Unit 3

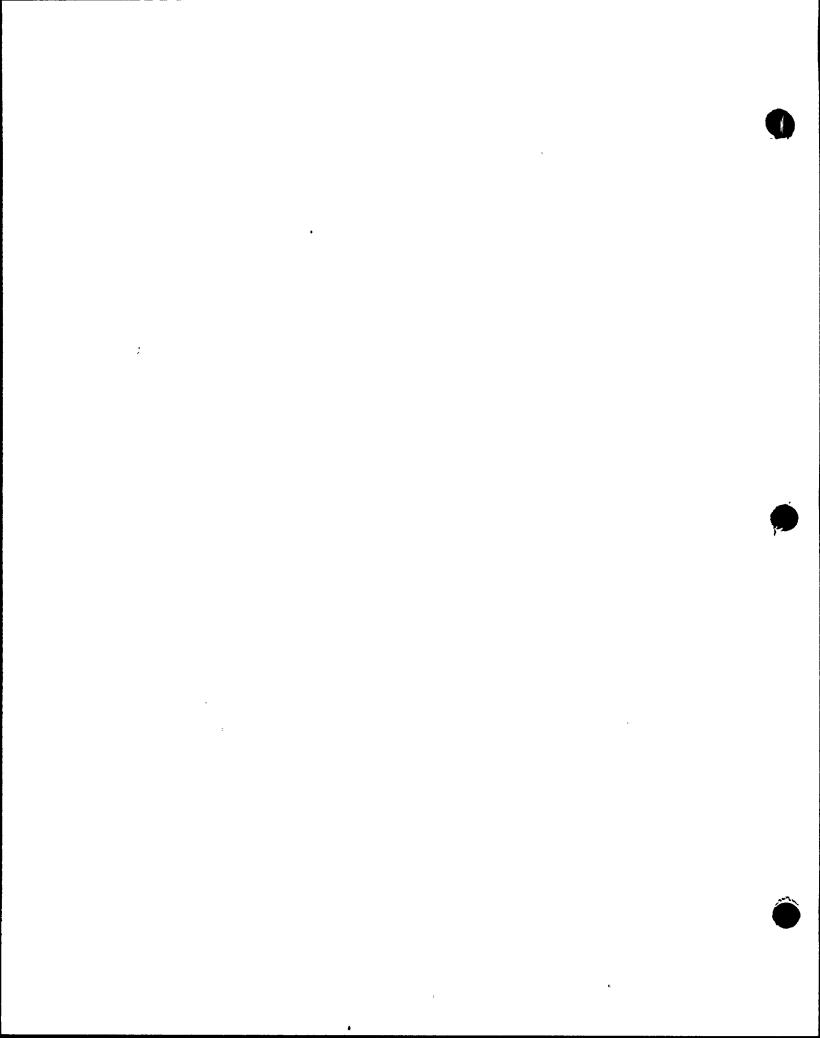




Browns Ferry Nuclear Plant Unit 3

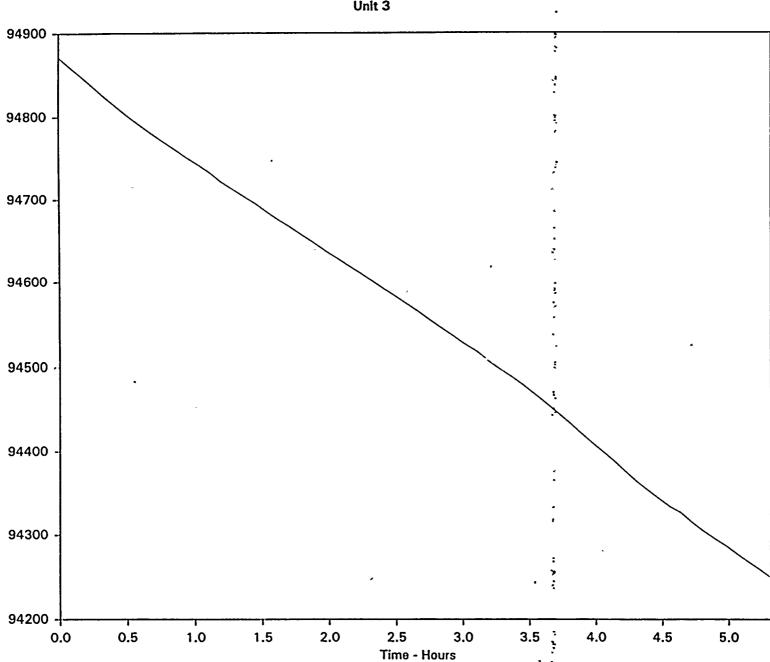


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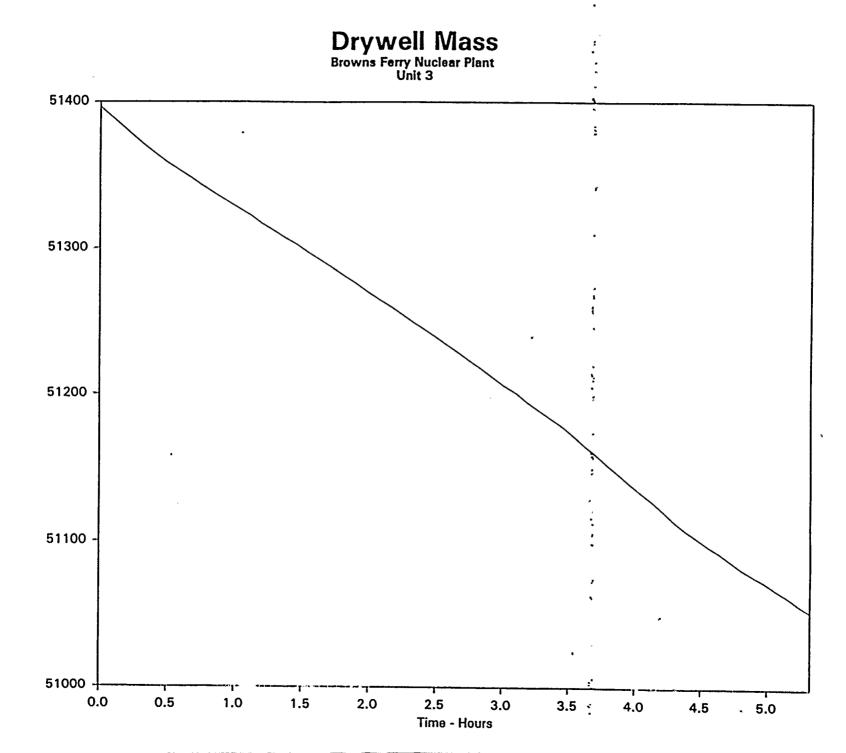


Containment Mass

Browns Ferry Nuclear Plant Unit 3

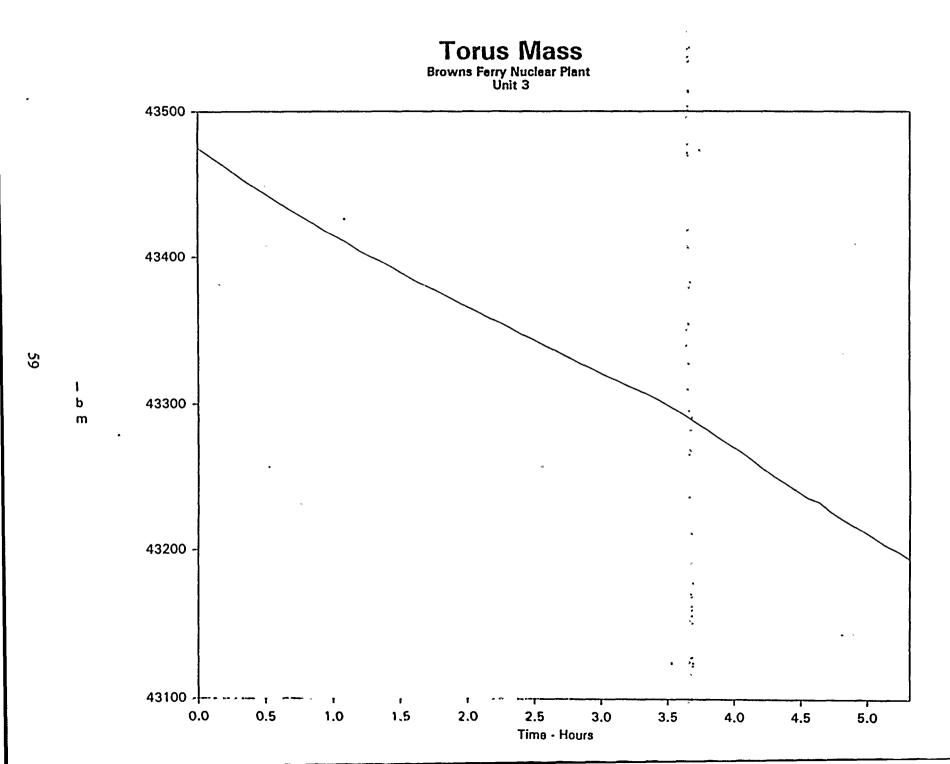


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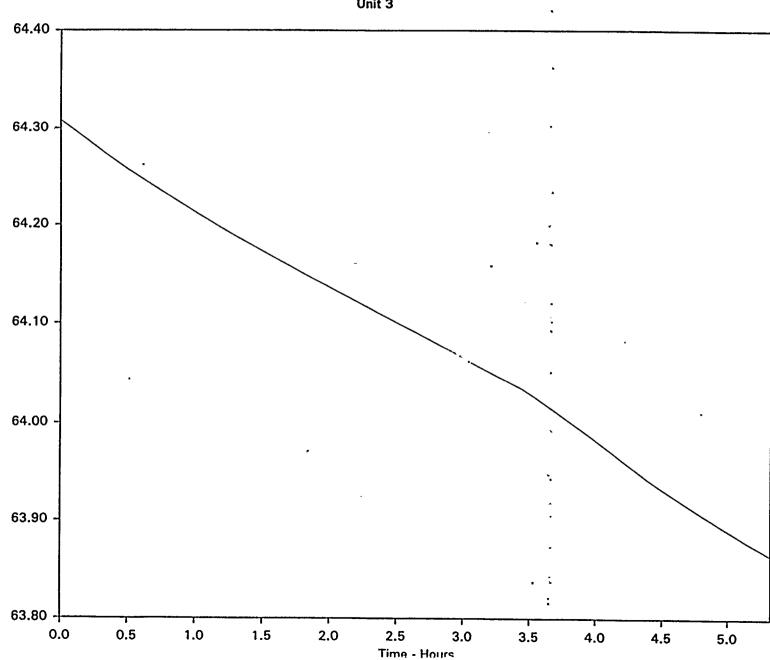


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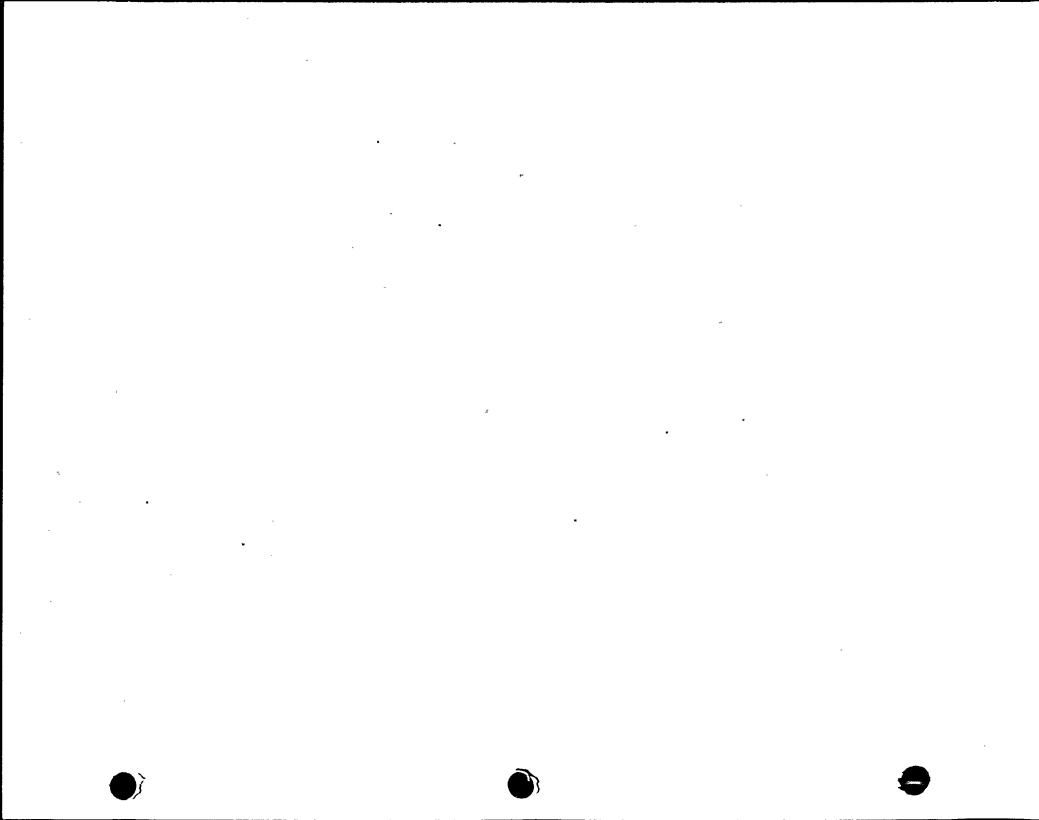


Drywell Average Pressure Browns Ferry Nuclear Plant Unit 3

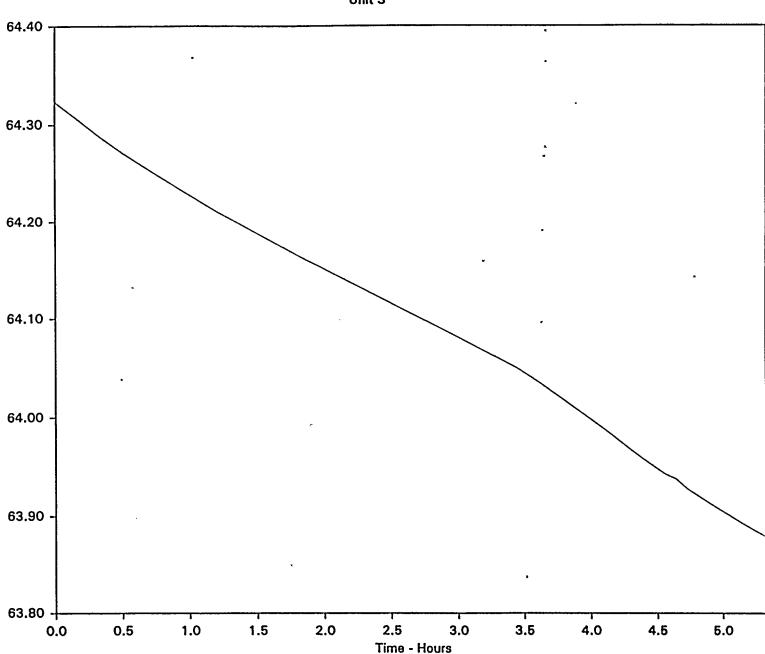


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Torus Average Pressure Browns Ferry Nuclear Plant Unit 3

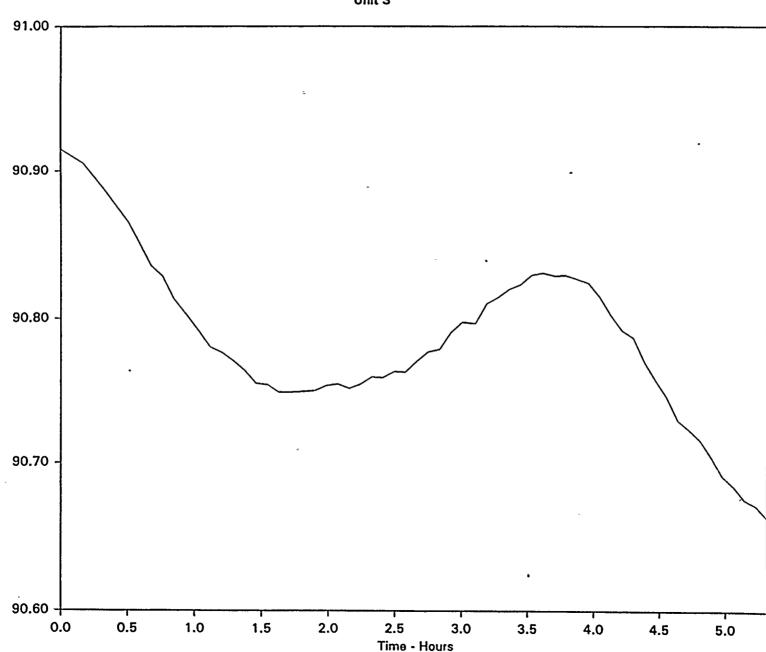


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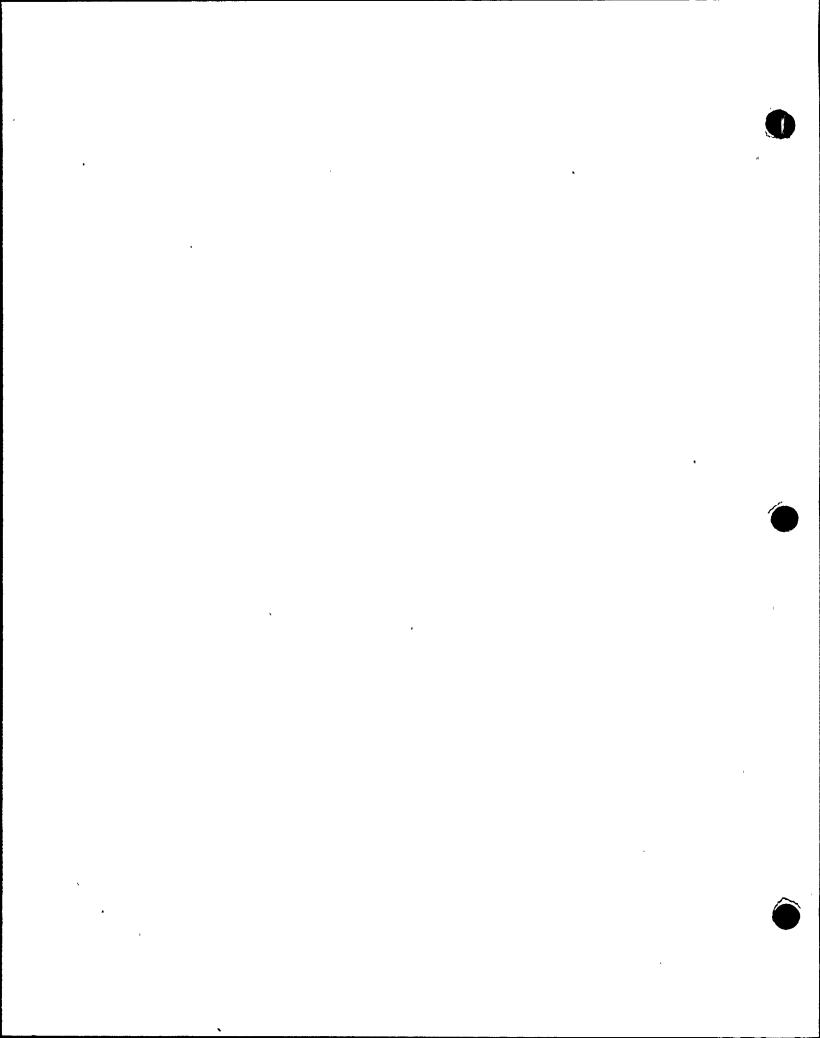
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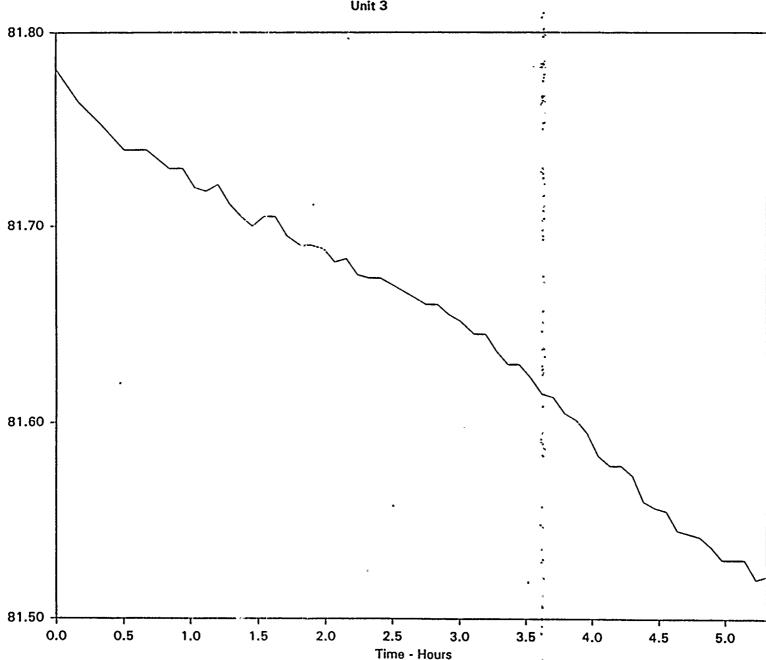
Drywell Average Temperature Browns Ferry Nuclear Plant Unit 3



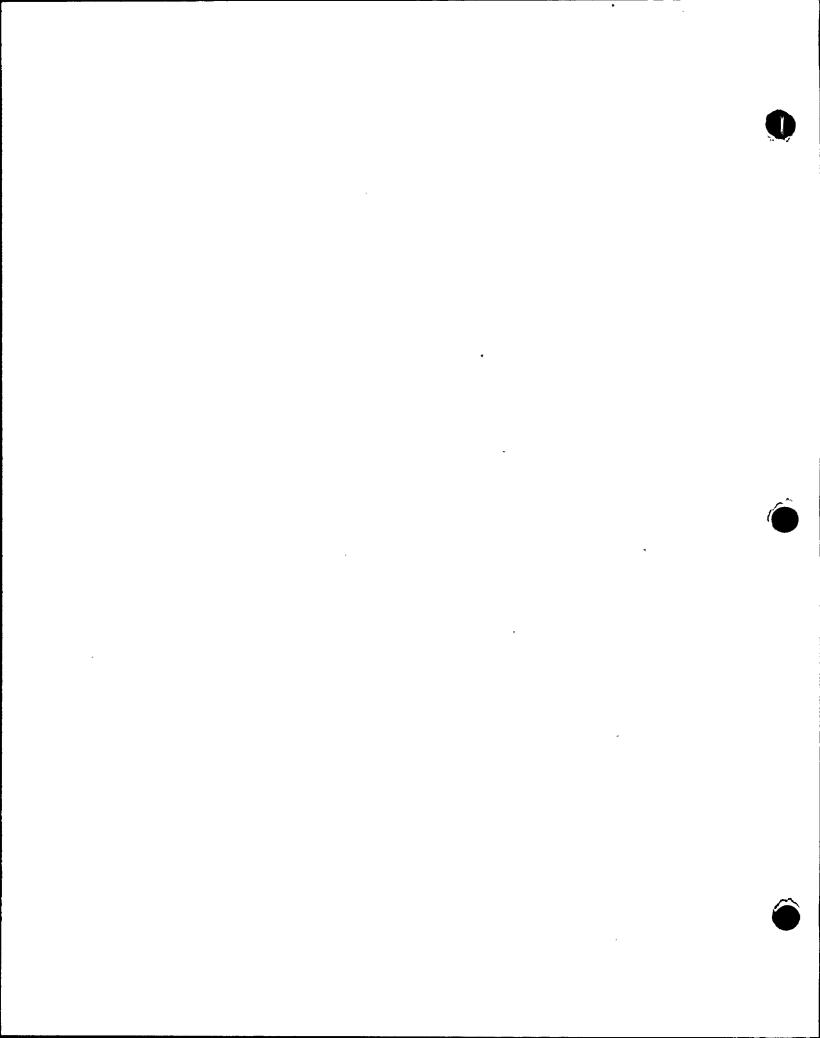
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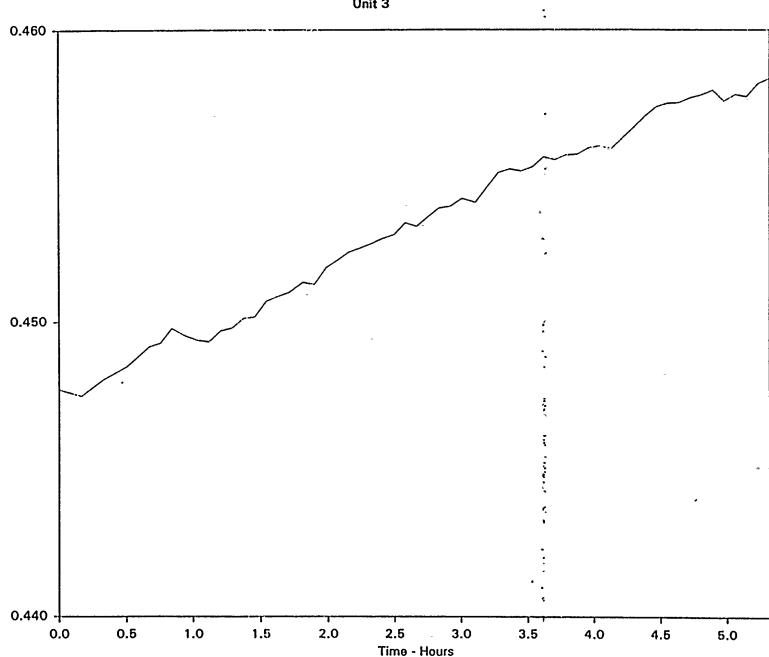
Torus Average Temperature: Browns Ferry Nuclear Plant Unit 3



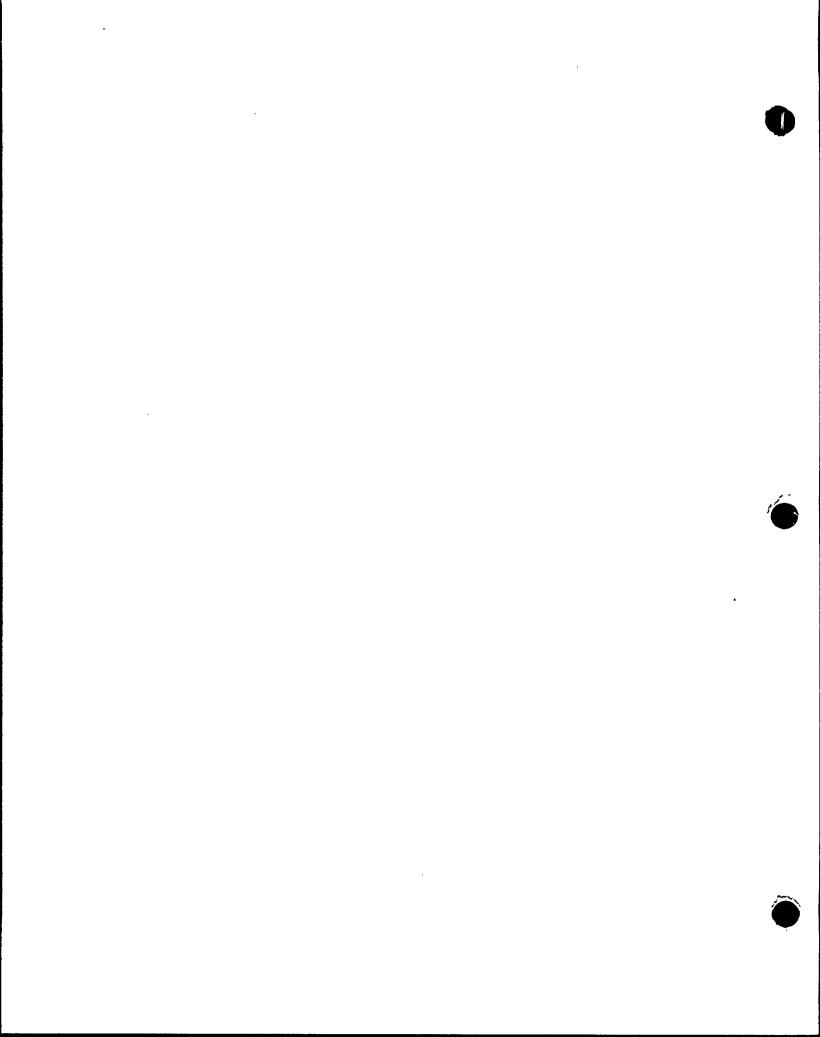
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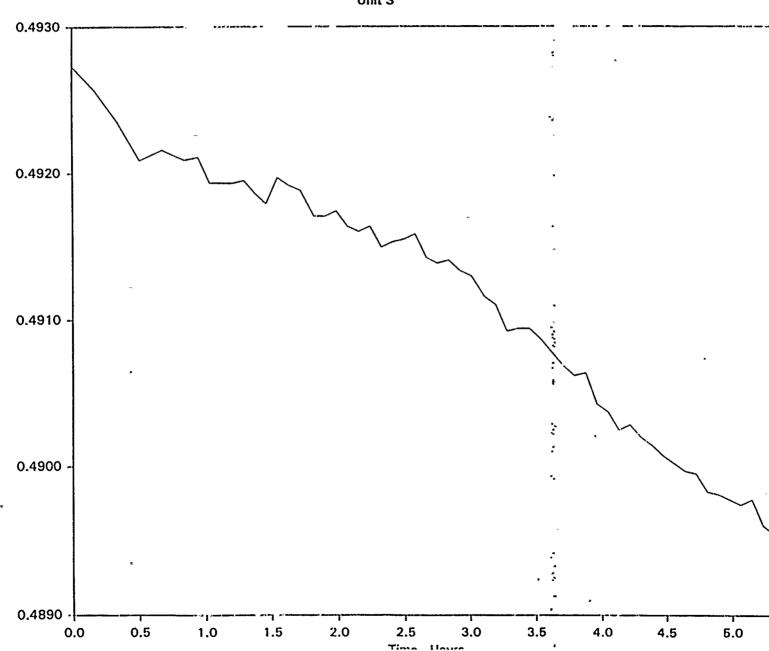
Drywell Average Vapor Pressure Browns Ferry Nuclear Plant Unit 3



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Torus Average Vapor Pressure Browns Ferry Nuclear Plant Unit 3

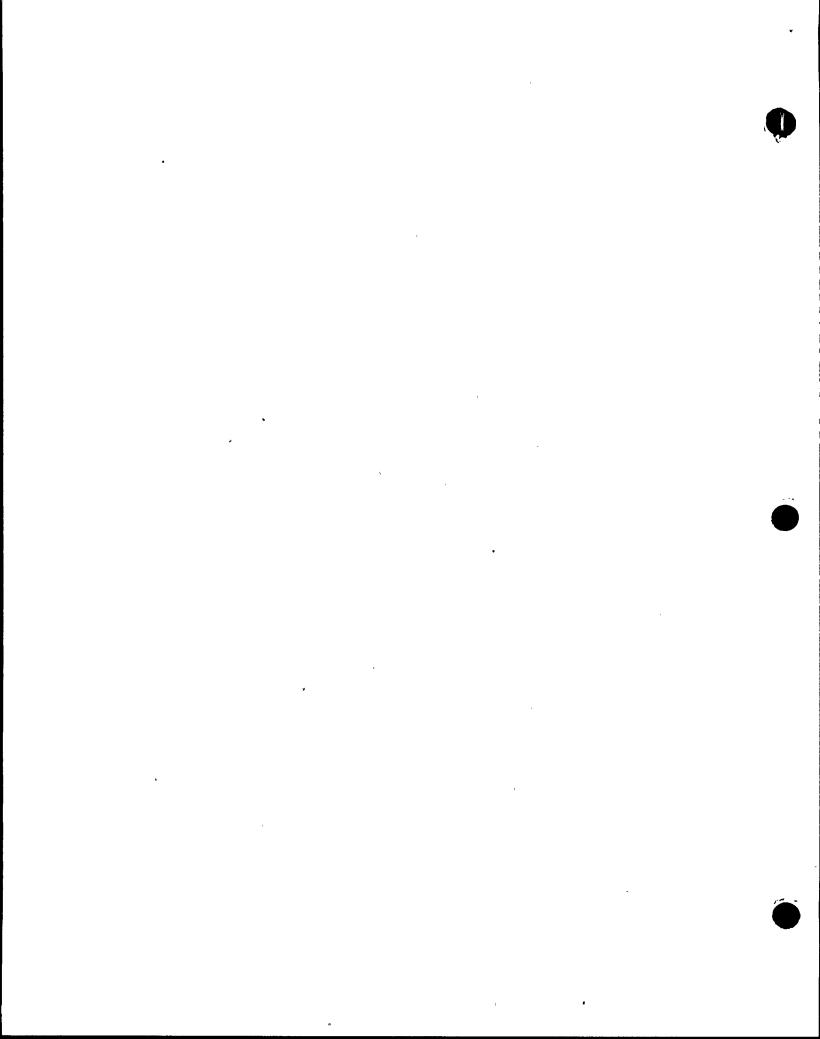


APPENDIX E

Verification Test Phase Tabular Data

(samples139 to 197)

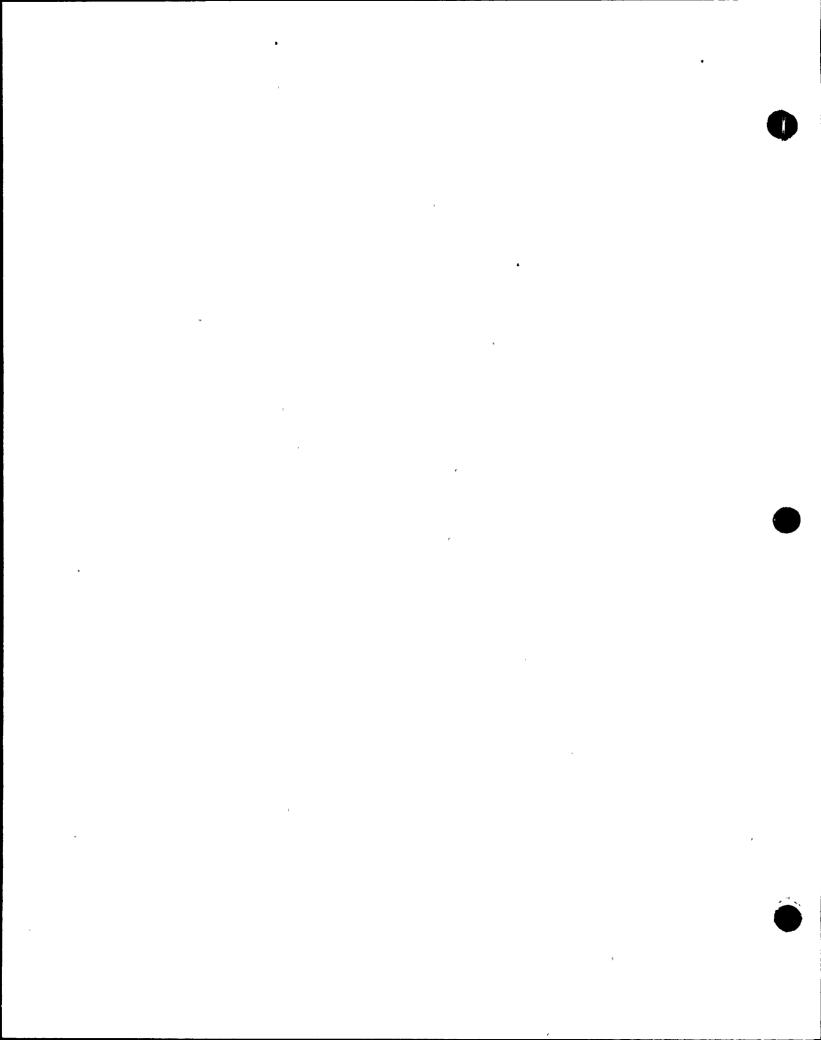
Contents:	•	<u>Page</u>
	Verification Total Time Leak Rate Analysis	67
	Verification Mass Point Leak Rate Analysis	69
	Verification Containment Calculated Values	71



Total Time Leak Rate Analysis
Browns Ferry Nuclear Plant
Unit 3

Page 1 of 2

RDG	TIME (MINUTES)	MEASURED LEAK (WT %/DAY)	CALCULATED LEAK (WT %/DAY)	UCL LEAK (WT %/DAY)
139	0.00	•	•	•
140	10.10	3.467233	•	•
141	20.20	3.549774	3.549774	•
142	30.28	3.469550	3.496700	4.140368
143	40.38	3.365340	3.405089	3.754550
143	40.36	3.305340	3.403065	3./54550
144	45.48	3.326937	3.355488	3.587435
145	50.62	3.278164	3.307921	3.493057
446		· 3.234726 .	- 3.258166	. 3.41.5860
147	61.97	3.180637	3.210106	3.351930
148	67.08	3.148010	3,167354	3.295210
149	72.27	3.158886	3,139690	3.257283
150	77.45	3.120935	3.109435	3.218039
151	82.55	3.092211	3.080081	3.181518
152	87.65	3.059388	3.050001	3.145331
153	92.75	3.065604	3.028190	3.122830
.55	32.73	, 0,000004	0.020100	0.122000
154	97.85	3.048226	3.007604	3.102309
155	102.95	3.024102	2.986573	3.080594
156	109.05	3.008887	2.962494	3.057875
157	114.13	2.998517	2.946016	3.043502
158	119.23	2.995010	2.932017	3.033466
		,		
159	124.32	2.979502	2.918068	3.022402
160	129.42	2.967644	2.904617	3.011633
161	134.50	2.953964	2.891412	3.000584
162	139.60	2.948198	2.879480	2.991495
163	144.70	2.938725	2.868121	2.982862
164	149.78	2.930432	2.857461	2.974902
165	154.88	2.921502	2.847172	2.967152
166	159.98	2.914087	2.837453	2.959966
167	165.07	2.909641	2.828652	2.953966
168	170.18	2.905451	2.820495	2.948801
169	175.28	2.901830	2.813124	2.944556
170	180.47	2.899856	2.806308	2.941132
171	186.48	2,884686	2.796219	2.933586
172	191.62	2,889730	2.790808	2.931535
173	196.70	2.881169	2.785342	2.928748
174	201.82	2.873585	2.779683	2.925324
175	206.92	2.869092	2.774316	2.922076
176	212.02	2.879014	2.770616	2.921640
177	217.12	2.889946	2.768489	2.923840
177			2.767763	
1/8	222.20	2.900490	2./0//03	2.928252
179	227.30	2.913092	2.768392	2.934851
180	232.40	2,924540	2.770169	2.943097
181	237.48	2.936725	2.773074	2.952873
			— · • • · ·	



Total Time Leak Rate Analysis Browns Ferry Nuclear Plant Unit 3

Page 2 of 2

	RDG '	TIME (MINUTES)	MEASURED LEAK (WT %/DAY)	CALCULATED LEAK (WT %/DAY)	UCL LEAK (WT %/DAY)
	182 183 184 185 186	242.58 247.68 252.77 257.87 262.95	2.942904 2.950414 2.966628 2.981625 2.984327	2.776389 2.780222 2.785282 2.791286 2.797213	2.962729 2.972899 2.984860 2.998062 3.010283
./	187 188 189	268.05 273.13 278.23 283.33 288.42	2.985484 2.986618 2.971013 2.982597 2.983900	2.802885 2.808375 - 2.812370 2.817047 2.821617	3.021367 3.031520 ,3.038434 3.046321 3.053691
	192 193 194 195 196	293.52 298.62 303.70 308.80 313.90	2.980227 2.972417 2.971977 2.969631 2.966145	2.825680 2.829007 2.832184 2.835049 2.837568	3.059917 3.064661 3.068993 3.072699 3.075742
:	197	318.98	2.964229	2.839886	3.078373

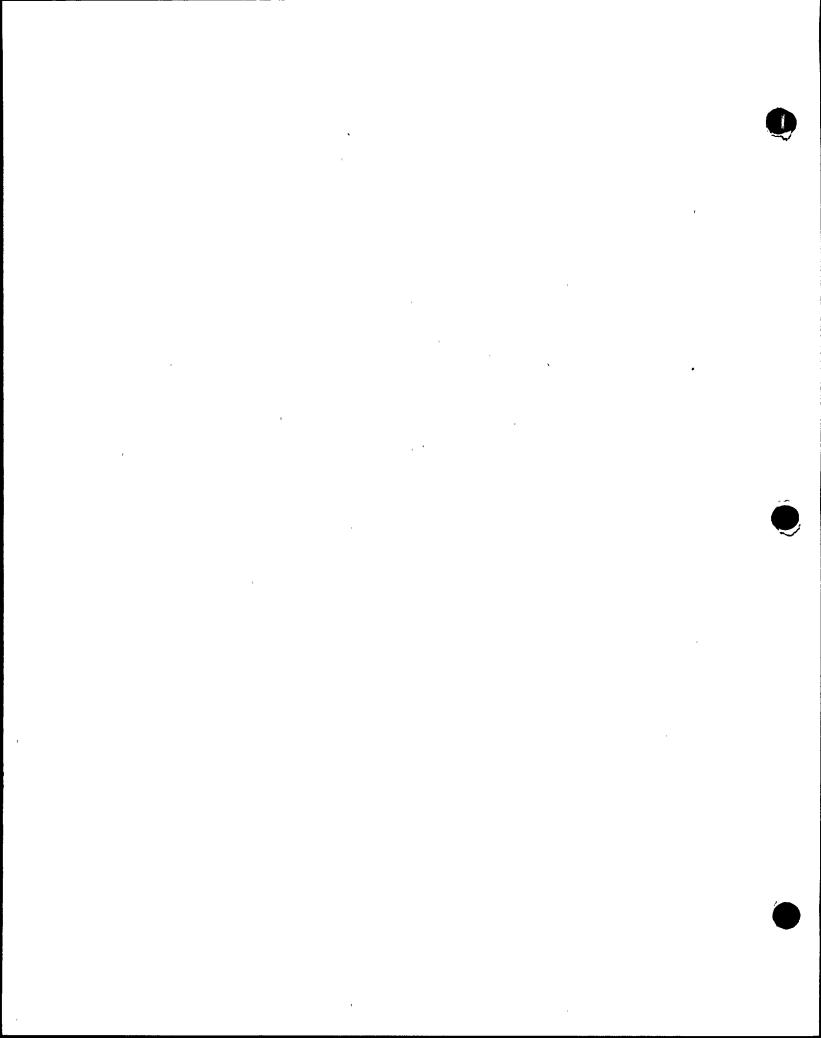
Mass Point Leak Rate Analysis Browns Ferry Nuclear Plant Unit 3

RDG	TIME (MINUTES)	NORM. MASS	MEASURED LEAK (WT %/DAY)	UCL LEAK (WT %/DAY)
139 140 141 142 143	0.00 10.10 20.20 30.28 40.38	1.000000 0.999757 0.999502 0.999270 0.999056	3.467233 3.549767 3.485860 3.386444	3.957495 3.611337 3.533530
144	45.48	0.998949	3.334020	3.455293
145	50.62	0.998848	3.285578	3.398040
146	56.72	0.998726	3.238509	3.345909
147	61.97	0.998631	3.187955	3.297139
148	67.08	0.998533	3.144050	3.250589
149	72.27	0.998415	3.120902	3.215002
150	77.45	0.998321	3.092508	3.180164
151	82.55	0.998227	3.063801	3.147222
152	87.65	0.998138	3.033384	3.114814
153	92.75	0.998025	3.014337	3.089489
154	97.85	0.997929	2.996045	3.066043
155	102.95	0.997838	2.976232	3.042752
156	109.05	0.997721	2.957605	3.020696
157	114.13	0.997623	2.941462	3.001063
158	119.23	0.997520	2.928961	2.984695
159	124.32	0.997428	2.916089	2.968743
160	129.42	0.997333	2.903791	2.953745
161	134.50	0.997241	2.891470	2.939202
162	139.60	0.997142	2.880920	2.926316
163	144.70	0.997047	2.870922	2.914202
164	149.78	0.996952	2.861592	2.902907
165	154.88	0.996858	2.852642	2.892182
166	159.98	0.996762	2.844285	2.882156
167	165.07	0.996665	2.836971	2.873160
168	170.18	0.996566	2.830545	2.865075
169	175.28	0.996468	2.824939	2.857848
170	180.47	0.996366	2.820293	2.851592
171	186.48	0.996264	2.814126	2.844228
172	191.62	0.996155	2.810137	2.838796
173	196.70	0.996064	2.805680	2.833113
174	201.82	0.995973	2.800974	2.827349
175	206.92	0.995877	2.796533	2.821913
176	212.02	0.995761	2.794539	2.818698
177	217.12	0.995643	2.794775	2.817727
178	222.20	0.995524	2.796855	2.818784
179	227.30	0.995402	2.800804	2.822059
180	232.40	0.995280	2.806192	2.827162
181	237.48	0.995157	2.812913	2.834023

Mass Point Leak Rate Analysis Browns Ferry Nuclear Plant Unit 3

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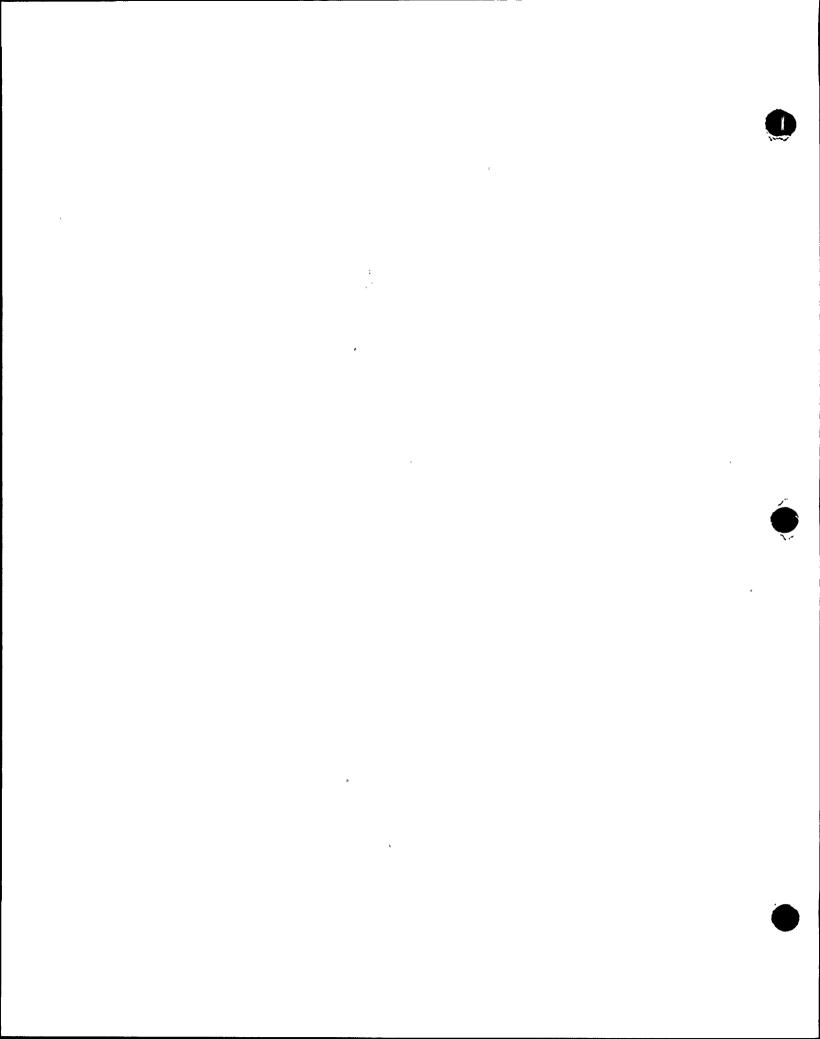
RDG	TIME (MINUTES)	NORM. MASS	MEASURED LEAK (WT %/DAY)	UCL LEAK (WT %/DAY)
182 183 184 185 186	242.58 247.68 252.77 257.87 262.95	0.995042 0.994925 0.994793 0.994661 0.994550	2.819971 2.827483 2.836496 2.846662 2.856307	2.841335 2.849245 2.859181 2.870635 2.881217
187 188 189. 190	268.05 273.13 278.23 283.33 288.42	0.994443 0.994335 0.994259 0.994131 0.994024	2.865293 2.873677 .2.8795.66 2.886336 2.892728	2.890813 2.899566 2.905133 2.911834 2.918080
192 193 194 195 196	293.52 298.62 303.70 308.80 313.90	0.993925 0.993836 0.993732 0.993632 0.993534	2.898226 2.902469 2.906364 2.909743 2.912535	2.923252 2.926962 2.930306 2.933097 2.935263
197	318.98	0.993434	2.914953	2.937051



Containment Calculated Values Browns Ferry Nuclear Plant Unit 3

Page 1 of 5

RDG	TIME		MASS	TEMP	VAPOR PRESS	PRESSURE
139	08:47:40	Drywell Torus TOTAL	51396.32 43475.08 94871.40	90.915 81.782	0.4477 0.4927	64.3085 64.3231
140	08:57:46	Drywell Torus TOTAL	51383.58 43464.75 94848.33	90.905 81.765	0.4475 0.4926	64.2913 64.3058
141.	09:07:52	, Drywell , , Torus TOTAL	51370.49 43453.67 94824.16	90,886 81.753	0.4481 0.4924	64.2733 64.2880
142	09:17:57	Drywell Torus TOTAL	51358.63 43443.55 94802.18	90.865 81.740	0.4485 0.4921	64.2566 64.2712
143	09:28:03	Drywell ' Torus TOTAL	51348.65 43433.21 94781.86	90.836 81.740	0.4492 · 0.4922	64.2415 64.2562
144	09:33:09	Drywell Torus TOTAL	51343.18 43428.53 94771.71	90.829 81.735	0.4493 0.4921	64.2340 64.2487
145	09:38:17	Drywell Torus TOTAL	51338.17 43423.91 94762.08	90.813 81.730	0.4498 0.4921	64.2265 64.2412
146	09:44:23	Drywell Torus TOTAL	51332.59 43417.94 94750.53	90.802 81.730	0.4495 0.4921	64.2180 64.2325
147	09:49:38	Drywell Torus TOTAL	51327.66 43413.89 94741.55	90.791 81.720	0.4494 0.4919	64.2105 64.2252
148	09:54:45	Drywell Torus TOTAL	51323.08 43409.19 94732.27	90.780 81.718	0.4493 0.4919	64.2035 64.2181
149	09:59:56	Drywell Torus TOTAL	51317.09 43403.91 94721.00	· 90.776 81.722	0.4497 0.4919	64.1960 64.2108
150	10:05:07	Drywell Torus TOTAL	51312.12 43400.04 94712.15	90.771 81.712	0.4498 0.4919	64.1892 64.2039
151	10:10:13	Drywell Torus TOTAL	51307.13 43396.10 94703.23	90.764 81.705	0.4501 0.4919	64.1825 64.1973
152	10:15:19	Drywell Torus TOTAL	51302.68 43392.05 94694.73	90.755 81.700	0.4502 0.4918	64.1761 64.1907



Containment Calculated Values Browns Ferry Nuclear Plant Unit 3

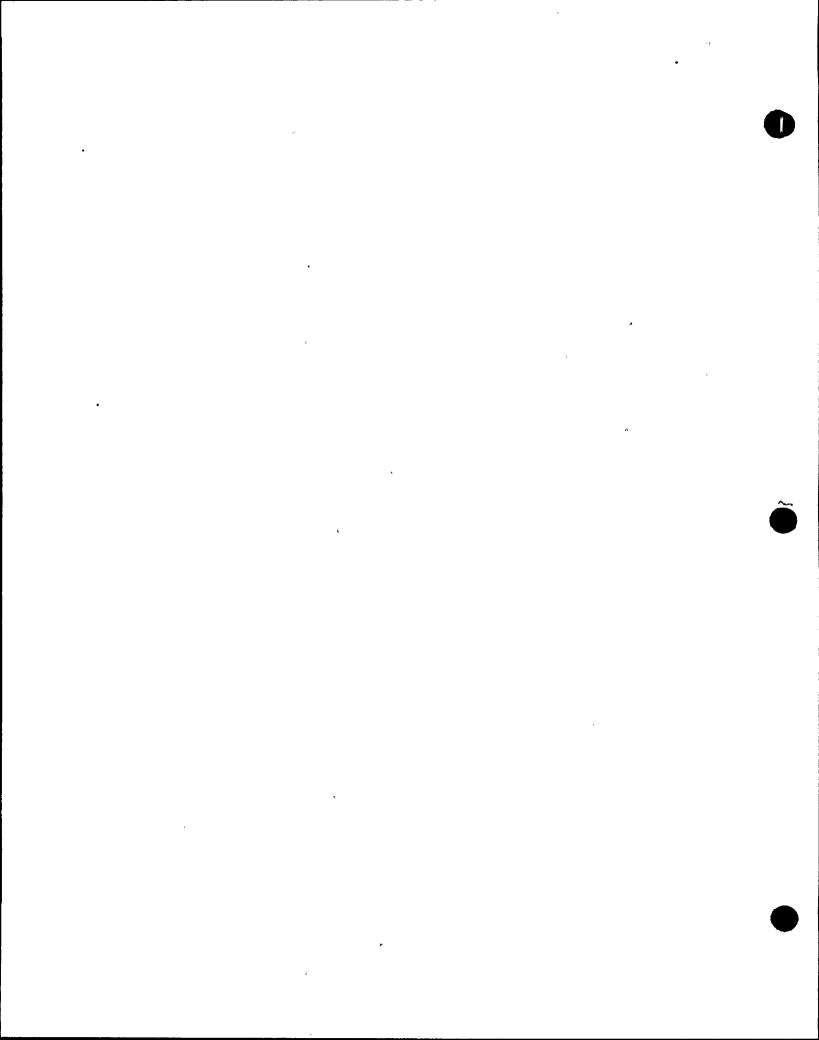
Page 2 of 5

RDG TIME			MASS	TEMP	VAPOR PRESS	PRESSURE
153 10:20:25	Drywell Torus TOTAL		51297.00 43387.07 94684.07			
154 10:25:31	Drywell Torus TOTAL		51292.18 43382.71 94674.89			
15510:30:37	··Drywell- Torus TOTAL	ege eg geg	51287.04 43379.25 94666.29		_	
156 10:36:43	Drywell Torus TOTAL	•	51280.60 43374.62 94655.23			
157 10:41:48	Drywell Torus TOTAL		51275.56 43370.37 94645.93			
158 10:46:54	Drywell Torus TOTAL		51269.84 43366.29 94636.13			
159 10:51:59	Drywell Torus TOTAL		51264.63 43362.74 94627.37			
160 10:57:05	Drywell Torus TOTAL		51259.83 43358.54 94618.37			
161 11:02:10	Drywell Torus TOTAL		51254.55 43355.10 94609.64			
162 11:07:16	Drywell Torus TOTAL		51249.08 43351.17 94600.25	-		
163 11:12:22	Drywell Torus TOTAL		51244.19 43347.06 94591.25	81.673		
164 11:17:27	Drywell Torus TOTAL		51238.89 43343.33 94582.22			
165 11:22:33	Drywell Torus TOTAL		51233.77 43339.52 94573.29			
166 11:27:39	Drywell Torus TOTAL		51228.41 43335.84 94564.25	81.663		

Containment Calculated Values Browns Ferry Nuclear Plant Unit 3

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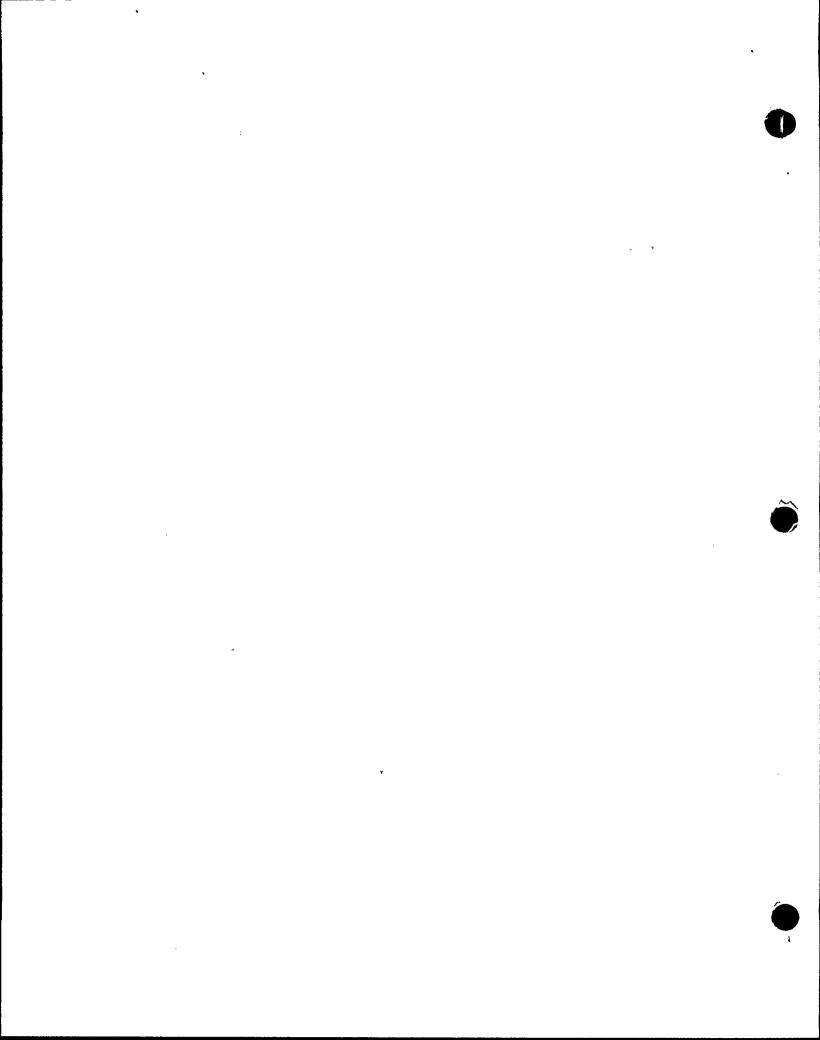
RDG	TIME		, MASS	TEMP	VAPOR PRESS	PRESSURE
167	11:32:44	Drywell Torus TOTAL		.86 90.777 .11 81.660		
168	11:37:51	Drywell Torus TOTAL		.56 90.779 .08 81.660 .64		
· 169-	11:42:57"-	· ··Drywell · Torus TOTAL		.72 90 790 .58 81.655 .29		
170	11:48:08	Drywell Torus TOTAL		.97 90.797 .64 81.652 .62		
171	11:54:09	Drywell Torus TOTAL		.45 90.797 .54 81.645 .99		
172	11:59:17	Drywell Torus TOTAL		.07 90.810 .52 81.645 .59		
173	12:04:22	Drywell Torus TOTAL		.60 90.814 .43 81.637 .03		
174	12:09:29	Drywell Torus TOTAL		.36 90.820 .96 81.630 .32		
175	12:14:35	Drywell Torus TOTAL		.34 90.823 .94 81.630 .28		
176	12:19:41	Drywell Torus TOTAL		.77 90.829 .48 81.623 .25		
177	12:24:47	Drywell Torus TOTAL		.09 90.831 .93 81.615 .02		
178	12:29:52	Drywell Torus TOTAL		.05 90.829 .74 81.613 .79		
179	12:34:58	Drywell Torus TOTAL		.23 90.829 .93 81.605 .16		
180	12:40:04	Drywell Torus TOTAL		.98 90.827 .64 81.602 .62		



Containment Calculated Values Browns Ferry Nuclear Plant Unit 3

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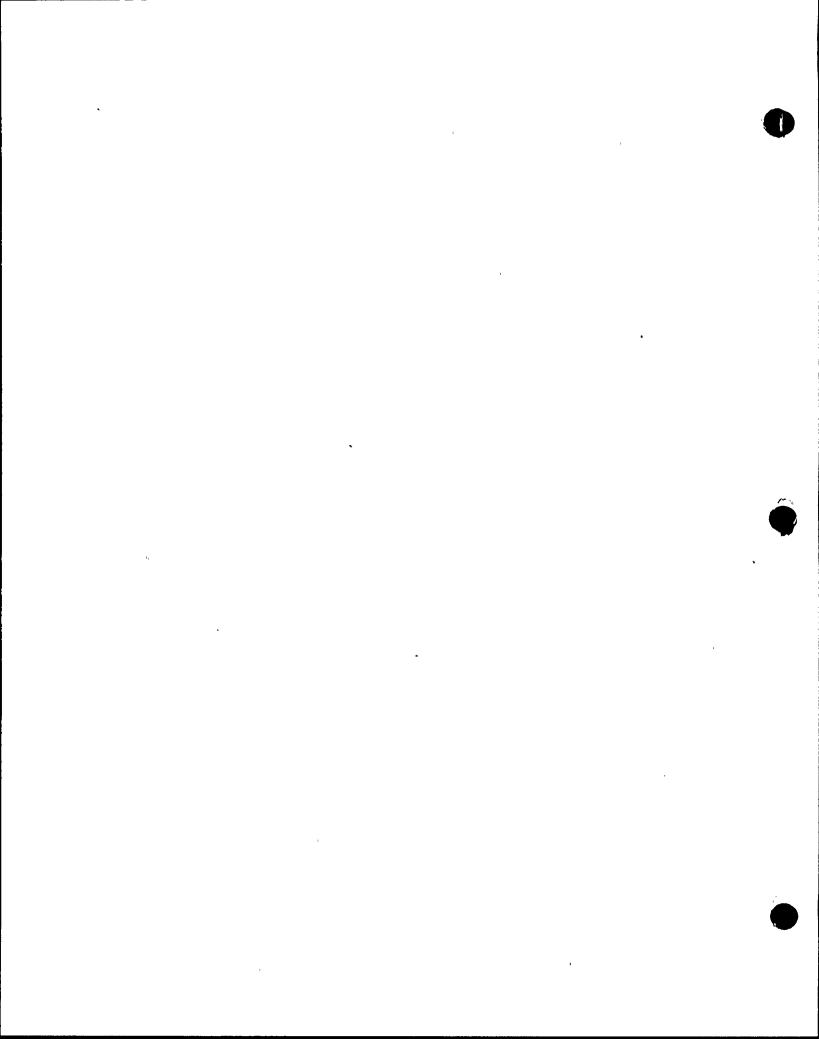
RDG	TIME	•	MASS	TEMP	VAPOR PRESS	PRESSURE
181	12:45:09	Drywell Torus TOTAL	51139.29 43272.62 94411.92			
182	12:50:15	Drywell Torus TOTAL	51133.26 43267.80 94401.06			
183	12:55:21·	Torus TOTAL	- 51127.56 43262.39 94389.95			
184	13:00:26	Drywell Torus TOTAL	51121.03 43256.34 94377.37			
185	13:05:32	Drywell Torus TOTAL	51114.09 43250.77 94364.85			
186	13:10:37	Drywell Torus TOTAL	51108.36 43246.04 94354.40			
187	13:15:43	Drywell Torus TOTAL	51103.09 43241.08 94344.17			-
188	13:20:48	Drywell Torus TOTAL	51097.93 43236.03 94333.97			
189	13:25:54	Drywell Torus TOTAL	51093.40 43233.39 94326.79			
190	13:31:00	Drywell Torus TOTAL	51087.79 43226.86 94314.65			
191	13:36:05	Drywell Torus TOTAL	51082.41 43222.00 94304.41			
192	13:41:11	Drywell Torus TOTAL	51077.59 43217.51 94295.09			
193	13:46:17	Drywell Torus TOTAL	51073.36 43213.26 94286.62			
194	13:51:22	Drywell Torus TOTAL	51068.24 43208.51 94276.75			



Containment Calculated Values Browns Ferry Nuclear Plant Unit 3

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RDG	TIME		MASS	TEMP	VAPOR PRESS	PRESSURE
195 13	3:56:28	Drywell Torus TOTAL	51063.56 43203.68 94267.24			
196 14	:01:34	Drywell Torus TOTAL	51058.01 43199.97 94257.98			
· *197·/24	:06:39-	Torus TOTAL	51053:18 43195.27 94248.45			



APPENDIX F

Verification Analysis Summary

TTLR reported during Verification Test (%/day): 2.839886

MLR reported during Verification Test (%/day): 2.914953

TTLR reported during CILRT (%/day): 0.856166

MLR reported during CILRT (%/day): 0.91,1060

Imposed Leak (%/day) 2.000770

Maximum Allowable Leak Rate (%/day) 2.000000

% Agreement = $LR_v - LR_j - LR_c$ L_a

where:

LR_v = the calculated leakage rate measured during the verification test

LR_i = the imposed leakage rate during the verification test

LR_c = the calculated leakage rate measured during the CILRT

L_a = the allowable leakage from containment

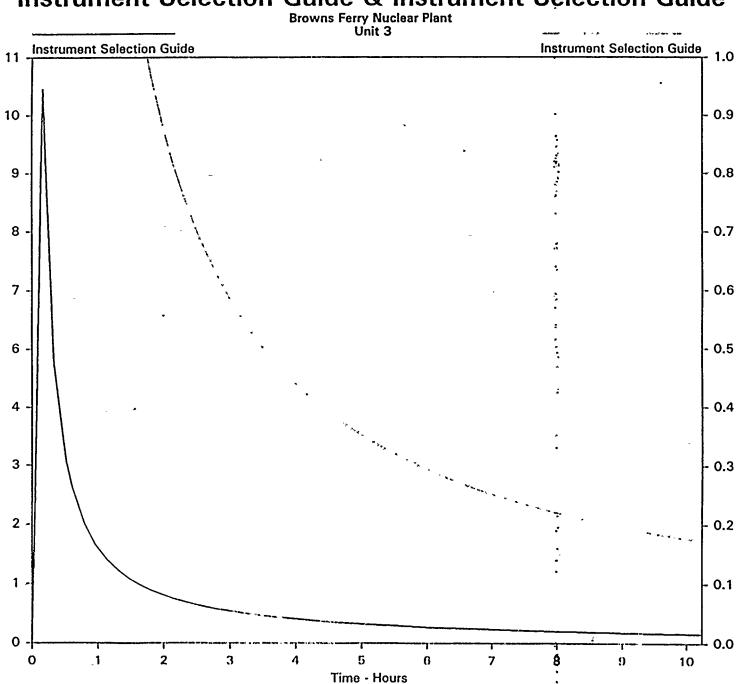
TTLR Agreement:

-0.852 %

MLR Agreement:

0.156 %

Instrument Selection Guide & Instrument Selection Guide



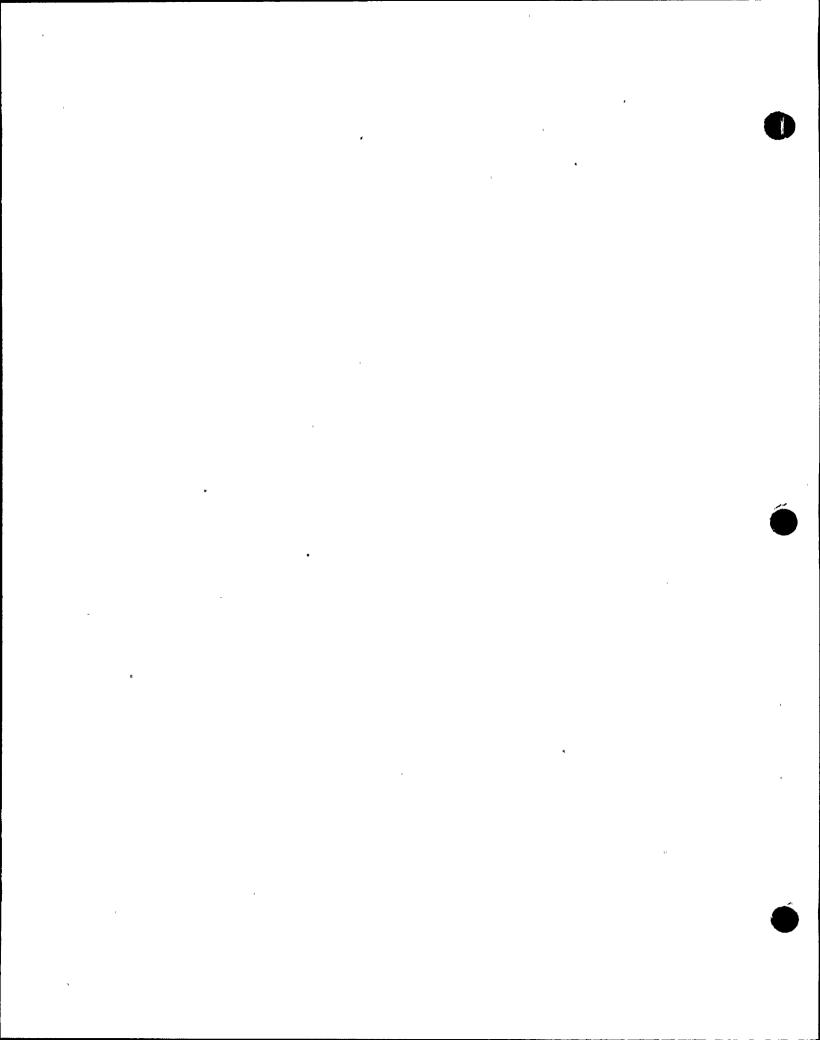
APPENDIX H

Penetrations Not Vented During the CILRT (in service or available for service)

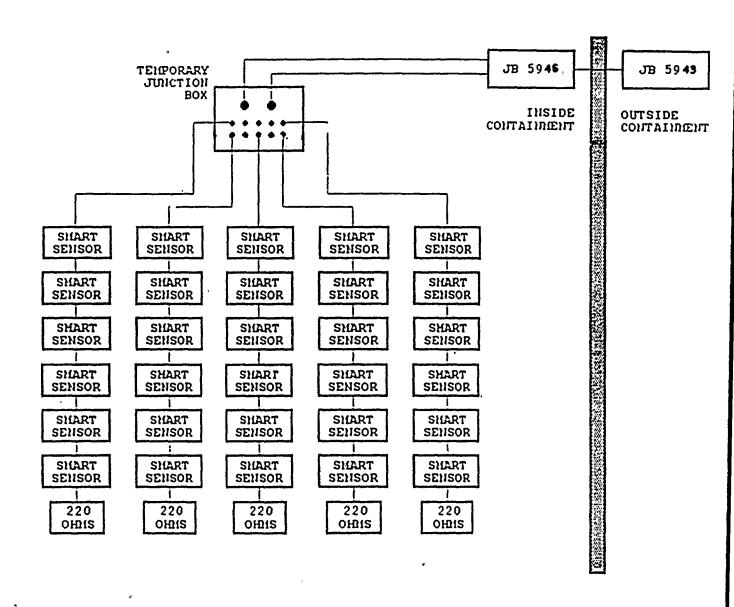
Penetration Number	<u>Description</u>	Leak Rate in SCFH	Percent per Day Added to UCL
X-9B	"B" Feedwater, Reactor Water Cleanup Return, Control Rod Drive Return,Reactor Core Injection Cooling	0.5384`	0.0010
X-12	Residual Heat Removal Shutdown Cooling suction	0.0004	0.0000
X-14	Reactor Water Cleanup Suction	0.0000	0.0000
X-18	Floor & Equipment Sump Drain	0.7329	0.0013
X-19	Floor & Equipment Sump Drain	0.0000	0.0000
X-42	Standby Liquid Control	0.5763	0.0011
	Total Leakage	1.8480	0.0034

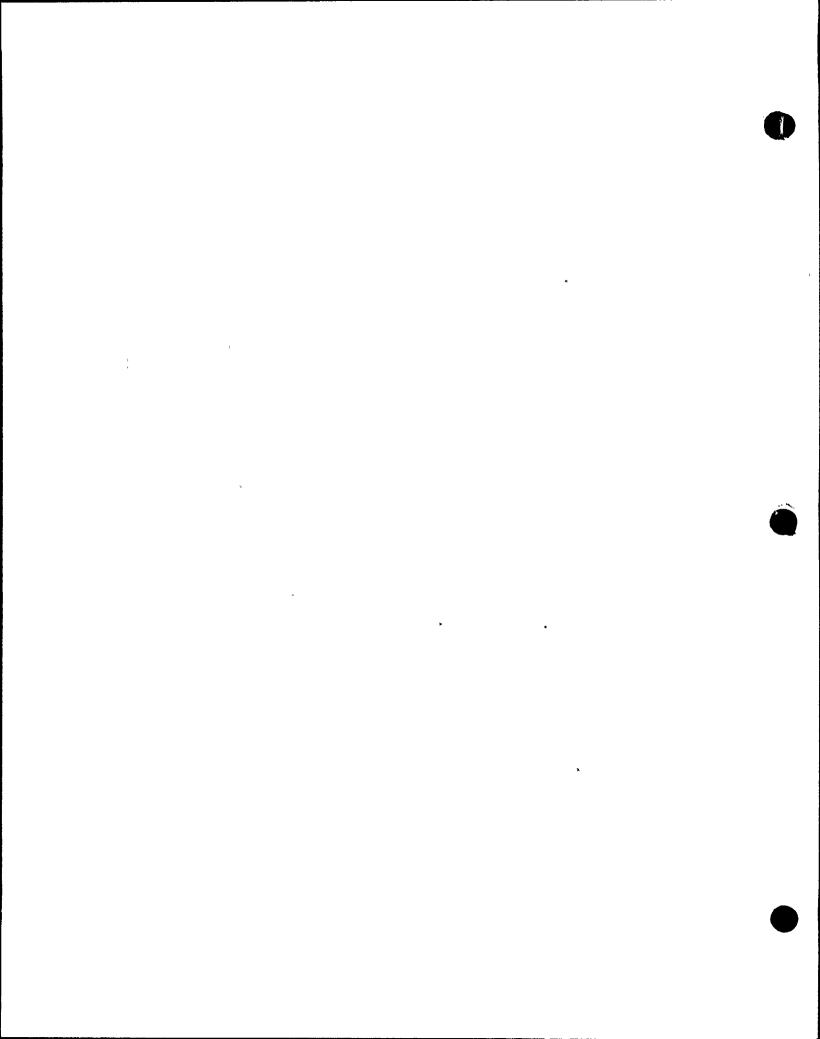
APPENDIX I

Computer System Block Diagram (Typical)

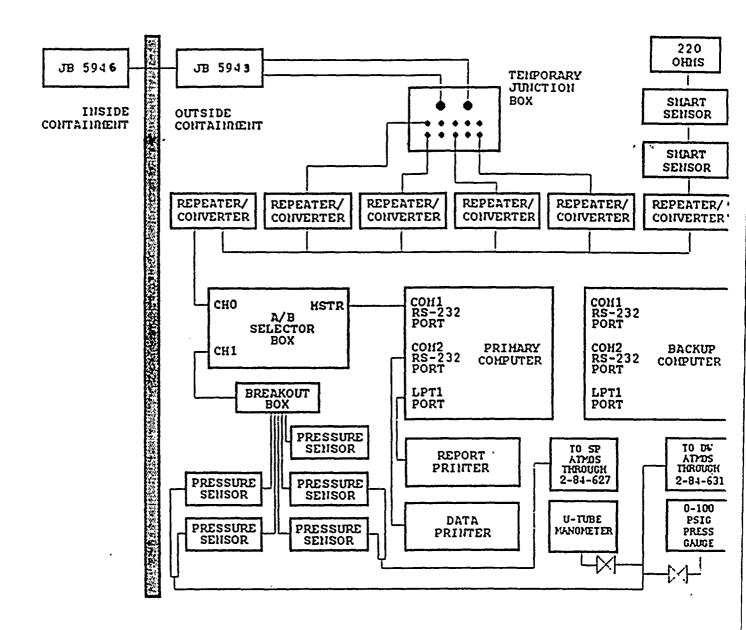


Computer System Block Diagram (Typical)





Computer System Block Diagram (Typical)



APPENDIX J

Compartment Parameters and Instrument Locations

COMPARTMENT PARAMETERS

, opo.a.a.a. (00		_		Instrumen	ŧ			
	Segment	Segment	Number of	Volume F	raction			
Compartment	Number	Volume (ft ³⁾	Instruments	Initial	Final			
Drywell	1	8,300.87	1	0.050563	*******			
(TS 1-29)	11	50,332.38	8	0.038323	0.043798			
,	111	64,058.92	8	0.048775	0.055743			
	IV ,	33,378.15	. 9 .	0.022590	` <u>`</u>			
	V	8,099.86	3	0.016446				
Torus (TS 30-35)	IX	136,629.53	6	0.166667				
Relative Humidity (10 Instruments)								
Drywell	VI (I+II)	58,633.25 64,058.92	3 2	0.119045 0.195099				
(HS 1-7)	III VII (IV&V)	41,478.01	2	0.195099				

Pressure (4 Instruments)

IX

Torus

(HS 8-10)

Temperature (35 Instruments)

Drywell (PS 1-2)	VIII	164,170.18	2	0.500000	
Torus (PS 3-4)	IX	136,629.53	2	0.500000	

136,629.53 3

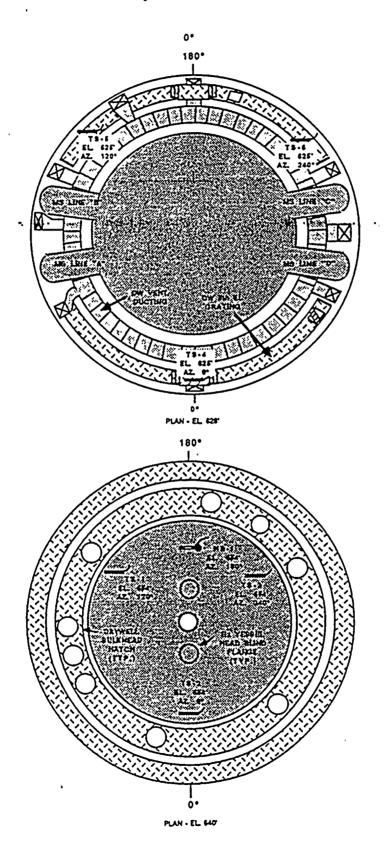
0.333333

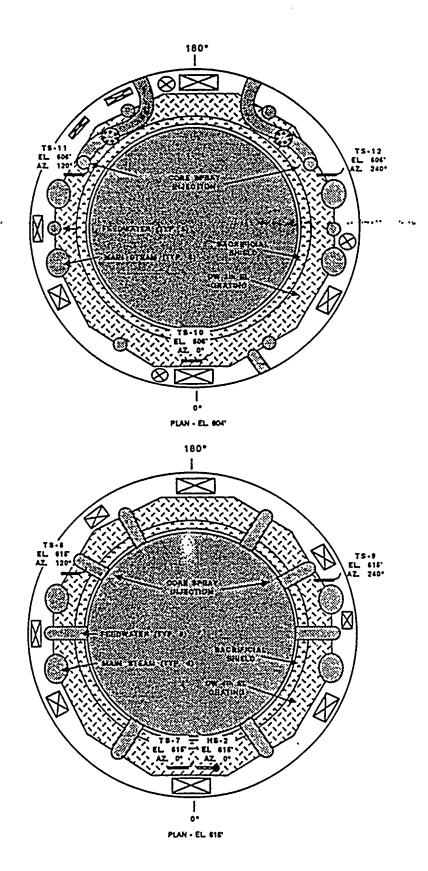
Compartment Volume Weights

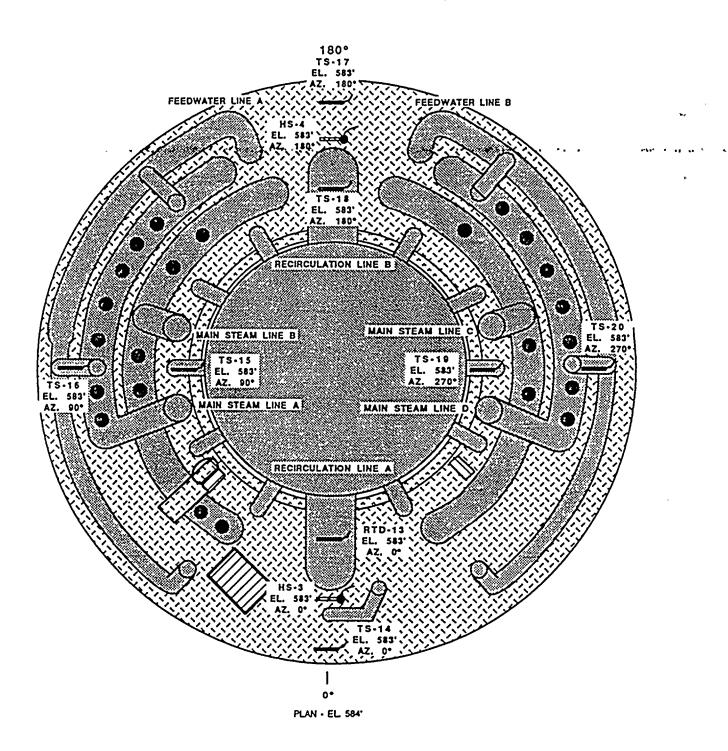
Containment <u>Compartment</u>	Volume (ft³)	Volumetric <u>Weight</u>
Drywell	164,170.18	0.545779
Torus	136,629.53	0.454221
3 C	a sylvation for the	profite and
Total Containment	300,799.71	1.000000

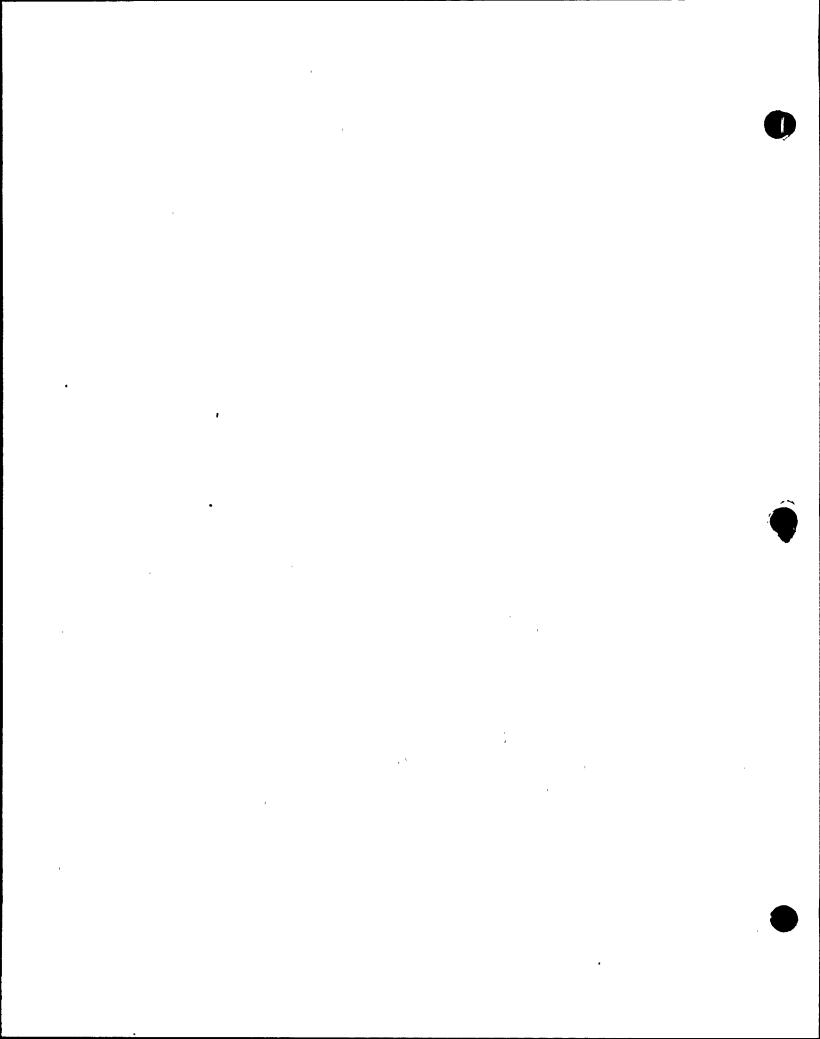
HS/TS Associations

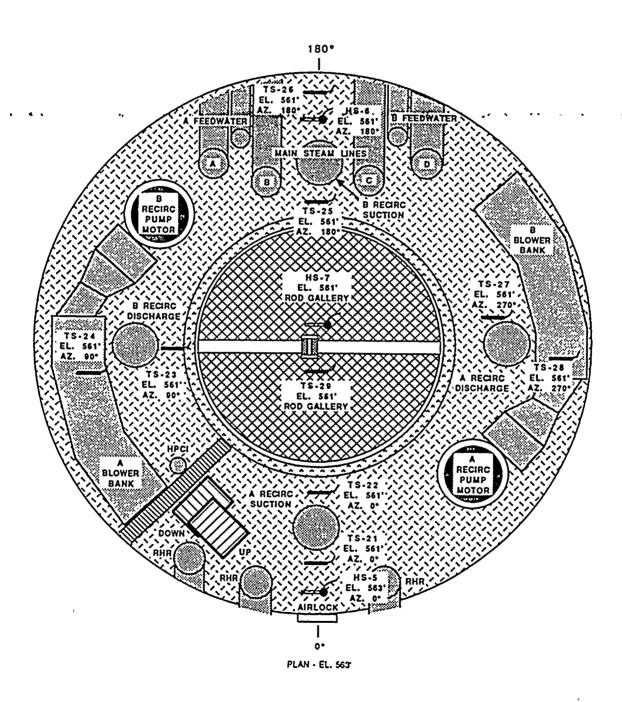
Humidity Sensor	Temperature Sensor
HS 1	TS 1
HS 2	TS 7
HS 3	TS 13
HS 4	TS 17
HS 5	TS 22
HS 6	TS 26
HS 7	TS 29
HS 8	TS 30
HS 9	TS 32
HS 10	TS 34

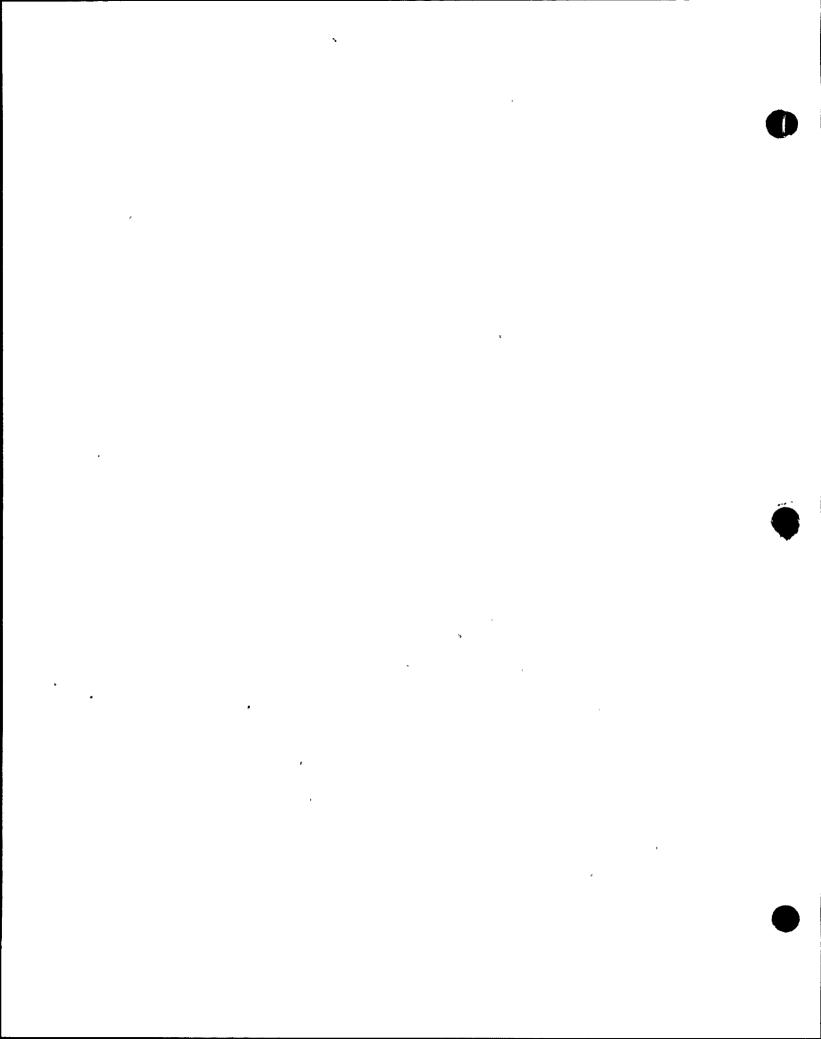




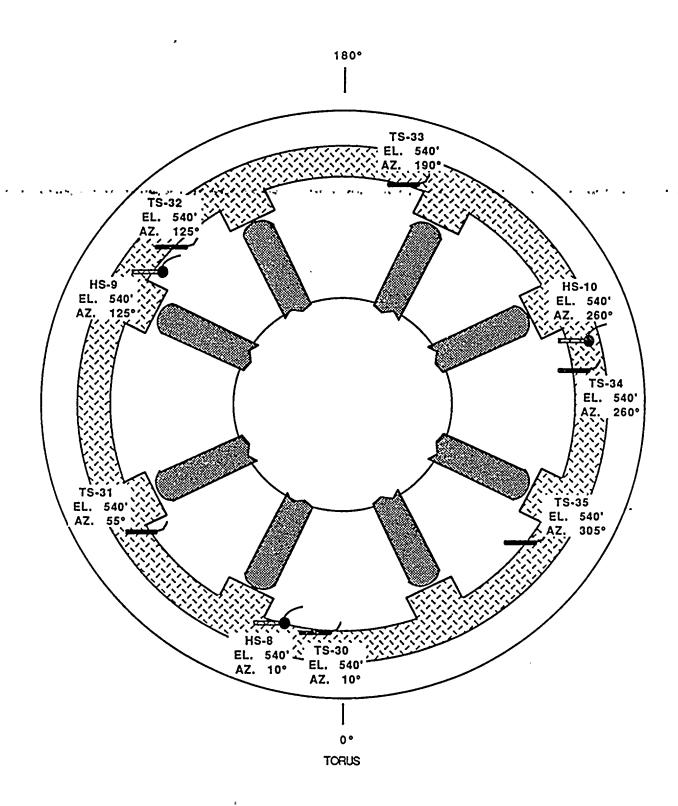








Torus Instrument Locations



APPENDIX K

INSTRUMENT SPECIFICATIONS

Measured <u>Parameter</u>	Manufacturer 'N and Model No.	lumber Used	Instrument S	pecifications
Containment Temperature	Graftel Model No. 9202 LT	30	Range: Accuracy: Repeatability	0-114°F <u>+</u> 0.24°F y: 0.01°F
Containment Temperature	Graftel Model No. 9202	5	Range: Accuracy: Repeatability	32-130°F ±0.24°F 7: 0.01°F
Containment Relative Humidity	Graftel Model No. 9203	10	Range: Accuracy: Repeatability	17-100% RH <u>+</u> 2°F dewpoint /: 0.1°F
Containment Pressure	Paroscientific Model No. 760-100A	4	Range: Accuracy: Repeatability	0-100 psia <u>+</u> 0.015% F.S. : <u>+</u> 0.005% F.S.
Verification Flow	Teledyne-Hastings Mass Flow Meter Model AHL-25	1	Range: Accuracy: Repeatability	0-25 SCFM ±2% F.S. ±0.5% F.S.
Atmospheric Temperature	Graftel Model No. 9202 LT	1	Range: Accuracy: Repeatability	0-114°F <u>+</u> 0.24°F : 0.01°F
Atmospheric Pressure	Paroscientific Model No. 760-100A	4	Range: Accuracy: Repeatability	0-100 psia ±0.015% F.S. : <u>+</u> 0.005% F.S.

APPENDIX L

Water Level Readings

CILRT Test Phase

<u>Time</u>	Reactor Vessel (2-L-3-55)	Suppression Chamber (2-L-64-54)	Drywell Floor Drain Sump	Drywell Equipment <u>Drain Sump</u>
1830	101.0	-6.5	13.0	18.0
1930	, 100,3	. . 6.6	13.0	_~ 18.0
2030	99.7	-6.6	13.0	18.0
2130	99.0	-6.7	13.0	18.0
2230	97.0	-6.9	13.0	18.0
2330	96.4	- 6.9	13.0	18.0
0030	95.7	- 6.9	13.0	19.0
0130	94.9	-7.0	13.0	19.0
0230	93.2	<i>-</i> 7.0	13.0	19.0
0330	92.6	-7.0	13.0	19.0
0430	92.0	- 7.0	13.0	19.0

Verification Test Phase

<u>Time</u>	Reactor Vessel (2-L-3-55)	Suppression Chamber (2-L-64-66)	Drywell Floor <u>Drain Sump</u>	Drywell Equipment <u>Drain Sump</u>
0530	91.0	-6.9	13.0	19.0
0630	89.1	-6.9	13.0	19.0
0730	88.2	-7.0	13.0	19.0
0830	87.7	-7.0	13.0	19.0
0930	86.7	-7.0	13.0	19.0
1030	85.0	-6.8	13.0	19.0
1130	84.3	-6.7	13.0	20.0

APPENDIX M

Summary of Local Leak Rate Tests

Introduction

Appendix J to 10 CFR 50 and BFN Technical Specifications (TS) require that the total leakage from all penetrations subject to type B and C testing be less than 0.60 L_a for return to power operations. In addition, TS 4.7.A.2.i requires that the main steam isolation valve leakage be less than 11.5 SCFH, and TS 4.7.A.2.g requires water-tested valves in the water seal system to provide a leakage limiting boundary which will ensure 30-day maintenance of the seal system inventory. TS 4.7.A.2.g also requires that water-tested valves in seismic Class I lines be tested and reported but not included in the leakage total. In the following listing, leak rates are given in SCFH for air/nitrogen-tested components, and in CFH for water-tested components. Water-tested valves in the seal system are denoted by "W" after the description, and water-tested valves in seismic Class I lines are denoted by "W/S". Valves which do not have these designations are air-tested valves.

Summary

These tests were conducted during the period from the cycle 4 CILRT until the cycle 6 CILRT. Testing was performed in accordance with plant-approved Surveillance Instructions 3-SI-4.7.A.2.g-1 through 3-SI-4.7.A.2.i.3/1.d.2, which are on file at the plant site. The Cycle 5 and Cycle 6 outage totals are summarized below. Individual component tests and leak rates are also listed.

The Unit 3, Cycle 6 shut down period began in March, 1985. Although it was BFN's inhouse policy to perform As-Found leak rate tests, this practice was performed at that point in time to obtain information used for maintenance purposes, rather than obtaining leak rates for regulatory reporting. After the shutdown of Unit 3, it was anticipated that these As-Found tests would be performed prior to component maintenance. However, the lengthy delay of unit restart (ten and one-half years) resulted in deviations from normal practice, and not all components were tested prior to maintenance or modification. Therefore, an exact As-Found value for minimum path or maximum path total LLRT leakage is not available for the Unit 3, Cycle 6 shutdown period. However, since the unit only operated for about 3 months during Cycle 6 (November 28, 1984 to March 9, 1985) the, As Found maximum path value can be approximated as the As Left maximum path LLRT total from the previous refueling outage.

Leakage through the Main Steam System (system 01) primary containment isolation valves (measured by LLRT's) caused the Cycle 5 LLRT As Found total to exceed 0.6La.

• • Modifications performed on the Main Steam and Main Steam Drain isolation valves during the Cycle 5 and Cycle 6 outages should significantly improve the leakage performance of these valves as has been demonstrated by similar modificatrions on Unit 2.

Unit 3 Cycle 5

	As Found (Max.Path)	As Left (Max.Path)	T.S. Limit
Type B & C Total Leak Rate (SCFH)	, 5080.3905 ,	. 116.1660	655.9 (60% L _a)
Seal System Total Leak Rate (CFH)	22.1512	0.3172	28.65

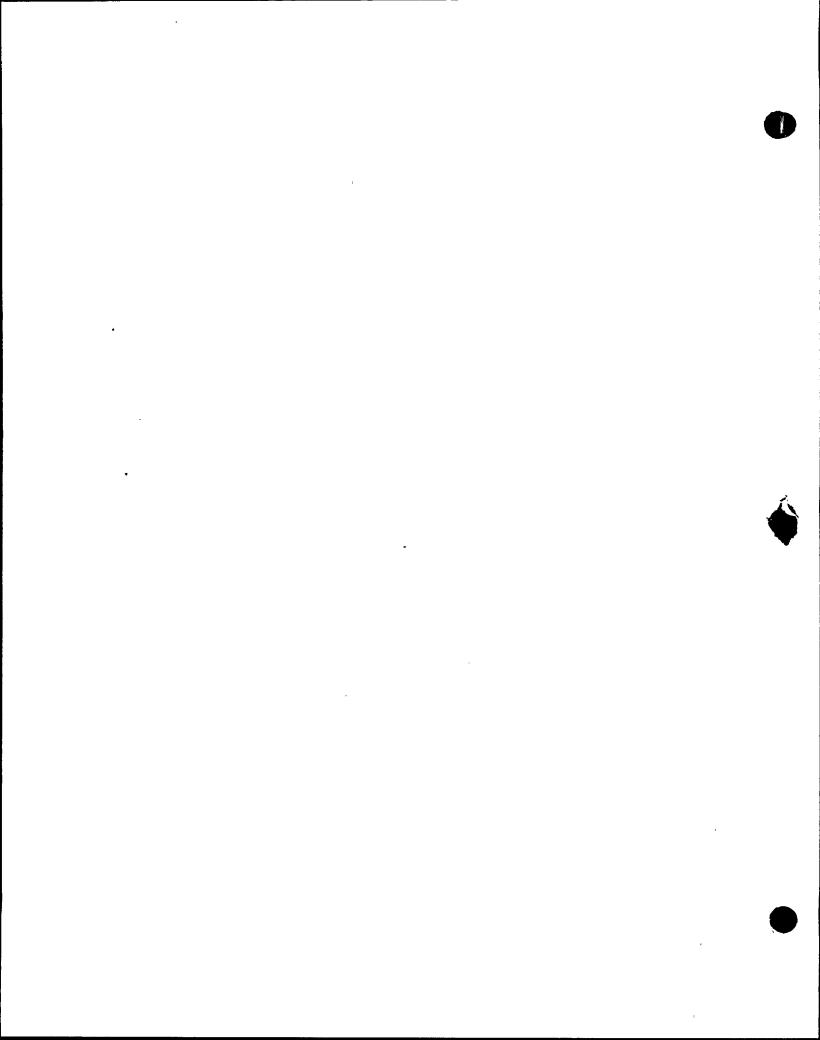
Unit 3 Cycle 6

	As Found (Max,Path)	As Left (Max.Path)	T.S. Limit
Type B &C Total Leak Rate (SCFH)	N/A	104.7270	655.9 (60% L _a)
Seal System Total Leak Rate (CFH)	N/A	0.9923	28.65

Type B Testing Summary

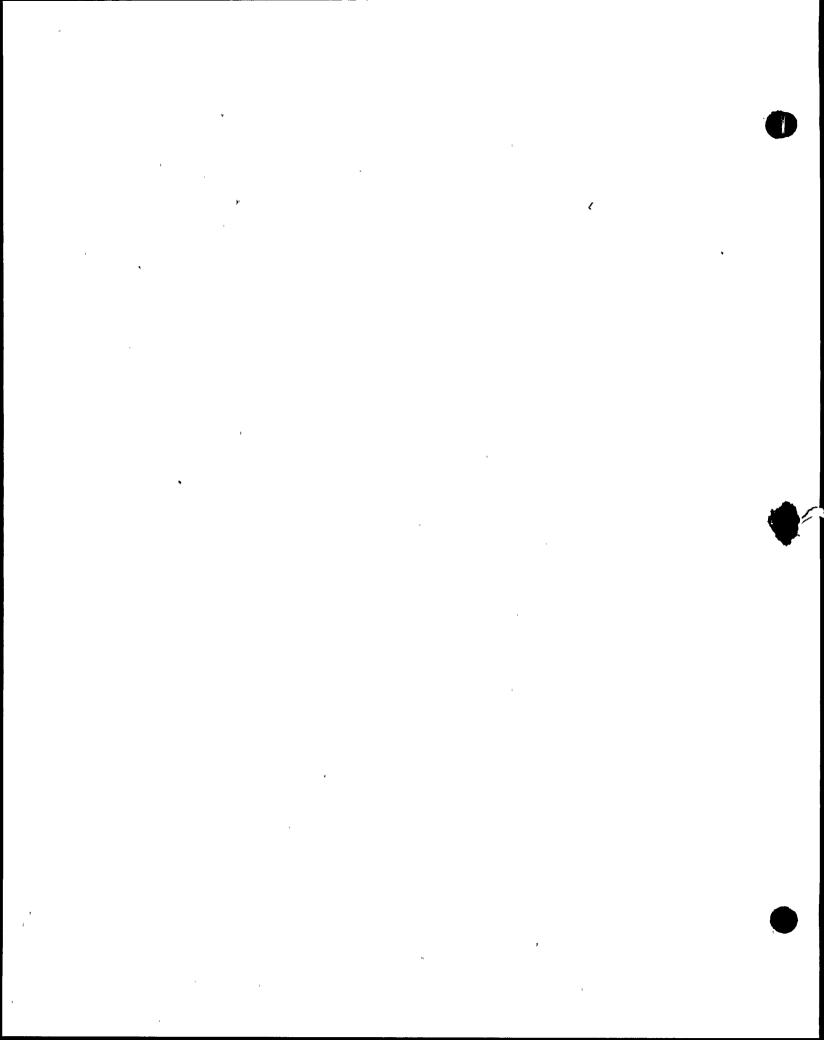
Personnel Air Lock

<u>Penetration</u>	Component Description		Leak Rate	Date Tested
X-2	Personnel Airlock		4.5573	01/23/83
4.1) //2 ³ , // ⁴ / 4 * *	a la la segui pers		2.8467	
			36.3709	10/14/84
			12.9469	10/19/84
			2.8602	11/27/84
			46.7044	12/16/84
			43,7000	02/13/85
			107.0159	04/13/85
			82.9788	04/13/85
			62.8054	08/21/86
			36.7216	11/06/95

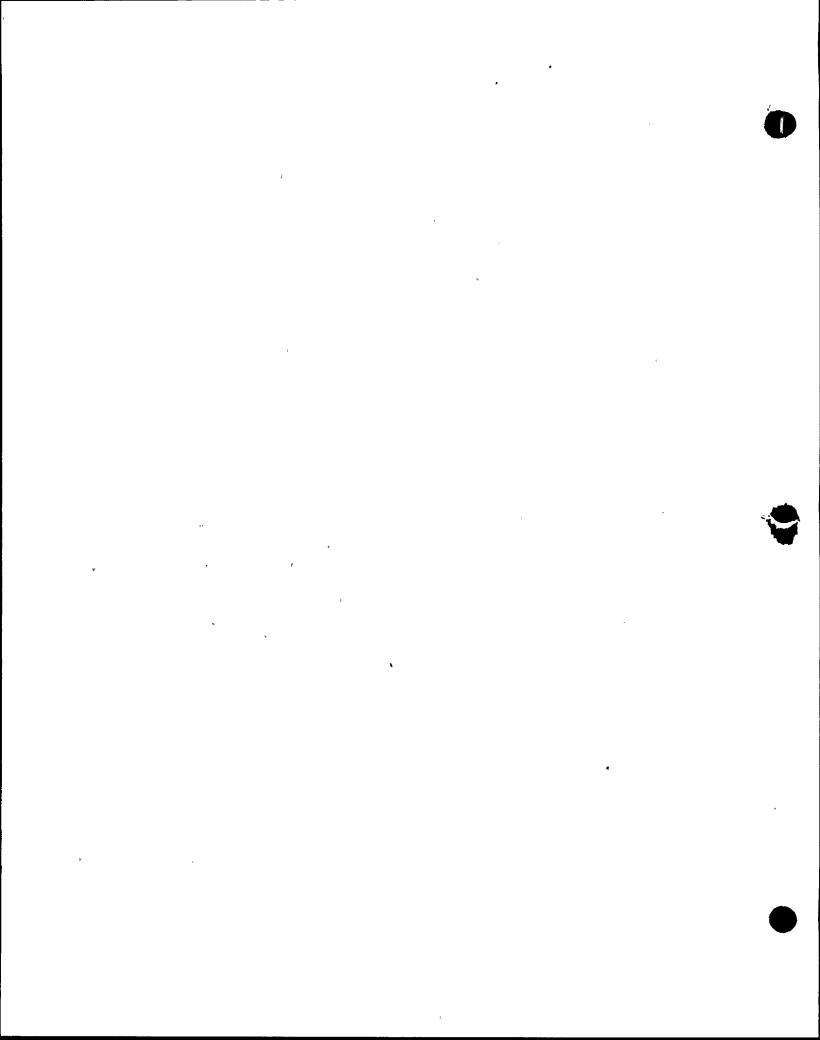


Bellows

<u>Penetration</u>	Component Description	Leak Rate	Date Tested
X-7A	MS Line A Inboard Bellows	0.0000 0.0002	05/30/84 07/19/95
	MS Line A Outboard Bellows	0.0000 0.0000	05/30/84 07/19/95
X-7B	MS Line B Inboard Bellows	0.0000 0.0013	05/30/84 07/19/95
• • •	MS Line B Outboard Bellows	0.0005 0.0009	05/30/84 07/19/95
X-7C	MS Line C Inboard Bellows	0.0000 0.0009	05/24/84 07/20/95
	MS Line C Outboard Bellows	0.0005 0.0005	05/24/84 07/20/95
X-7D	MS line D Inboard Bellows	0.0000 0.0006	05/31/84 07/20/95
	MS Line D Outboard Bellows	0.0010 0.0007	05/31/84 07/20/95
X-8	MS Drain Line Inboard Bellows	0.0003 [*] 0.0001	05/30/84 07/21/95
	MS drain Line Outboard Bellows	0.0000 0.0000	05/30/84 07/21/95
X-9A	A Feedwater Line Inboard Bellows	. 0.0001 0.0000	05/31/84 07/21/95
	A Feedwater Line Outboard Bellows	0.0000 0.0000	05/31/84 07/21/95

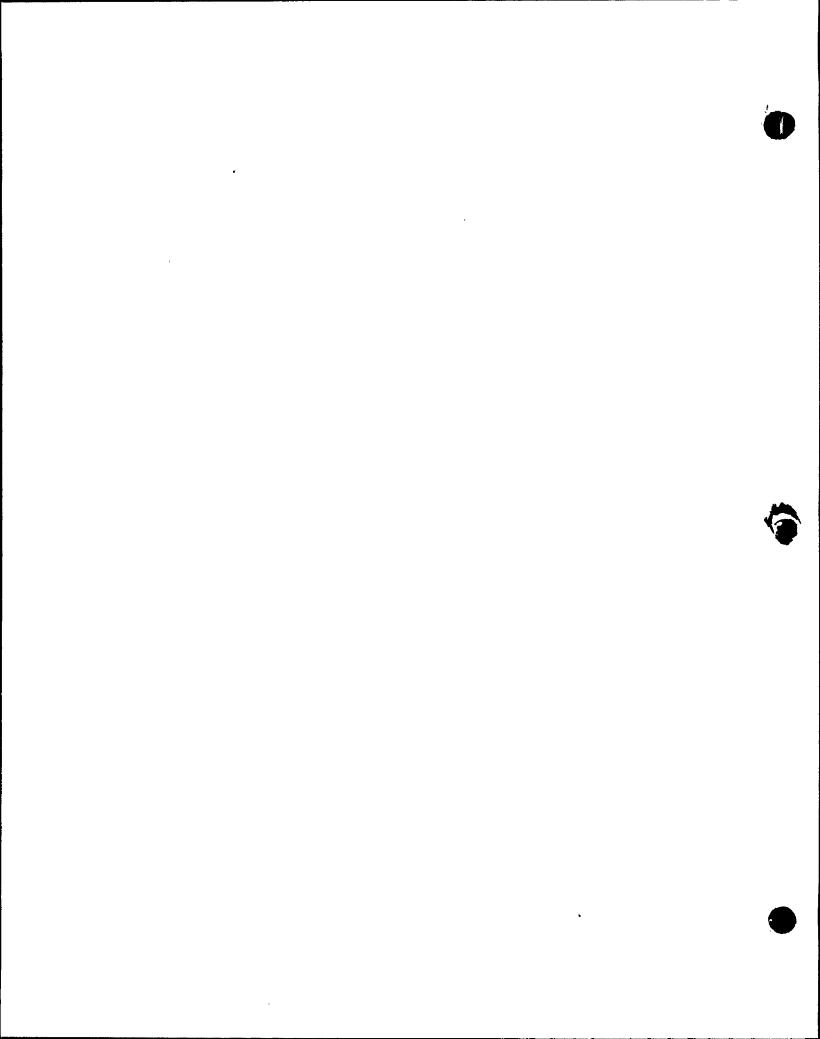


Penetration	Component Description	Leak Rate	Date Tested
X-9B	B Feedwater Line Inboard Bellows	0.0000 0.0001	05/24/84 07/22/95
	B Feedwater Line Outboard Bellows	0.0000 0.0001	05/24/84 07/22/95
X-10	RCIC Steam Supply Inboard Bellows	0.0003 0.0001	05/31/84 07/22/95
N 40 - 1 - 1 - 1 - 1	RCIC Steam Supply Outboard Bellows	0.0001 0.0001	05/31/84 07/22/95
X-11	HPCI Steam Supply Inboard Bellows	0.0002 0.0006	06/07/84 07/24/95
	HPCI Steam Supply Outboard Bellows	0.0003 0.0001	06/07/84 07/24/95
X-12	RHR SDC Suction Inboard Bellows	0.0004 0.0002	06/01/84 07/22/95
	RHR SDC Suction Outboard Bellows	0.0004 0.0002	06/01/84 07/22/95
. X-13A ,	RHR LPCI Inboard Bellows	0.0000 0.0005	06/01/84 07/22/95
	RHR LPCI Outboard Bellows	0.0000 0.0002	06/01/84 07/22/95
X-13B	RHR LPCI Inboard Bellows	0.0000 0.0005	05/31/84 07/22/95
	RHR LPCI Outboard Bellows	0.0000 0.0012	05/31/84 07/22/95
X-14	RWCU Suction Inboard Bellows	0.0001 0.0001	06/03/84 07/25/95
	RWCU Suction Outboard Bellows	0.0002 0.0000	06/03/84 07/25/95



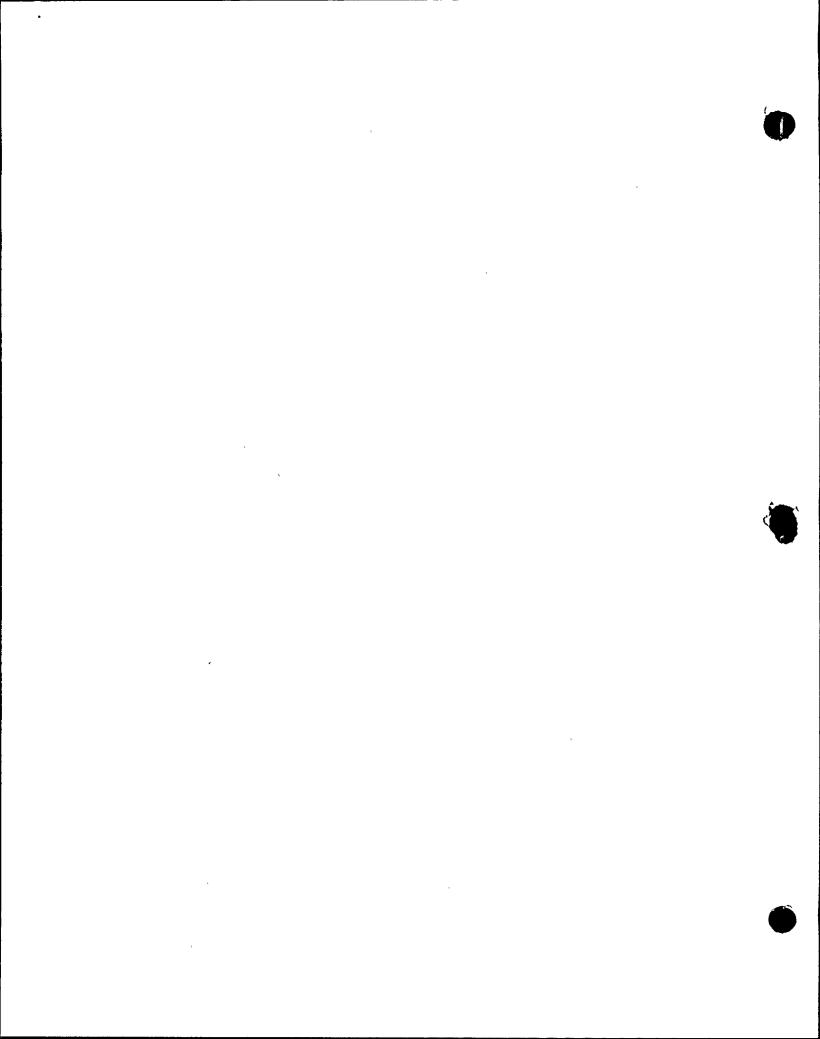
<u>Penetration</u>	Component Description	Leak Rate	Date Tested
X-16A	CS Injection Inboard Bellows	0.0002 0.0000	06/02/84 07/24/95
- *	CS Injection Outboard Bellows	0.0001 0.0000	06/02/84 07/24/95
X-16B	CS Injection Inboard Bellows	0.0003 0.0010	06/01/84 07/24/95
, Marro - 24 to 11	CS Injection Outboard Bellows	0.0001 . Q.0008	06/01/84 07/24/95
X-17 ¹	RHR Head Spray Inboard Bellows	0.0001	06/01/84
	RHR Head Spray Outboard Bellows	0.0001	06/01/84

¹ Bellows and line removed and penetration sealed during Cycle 6 outage

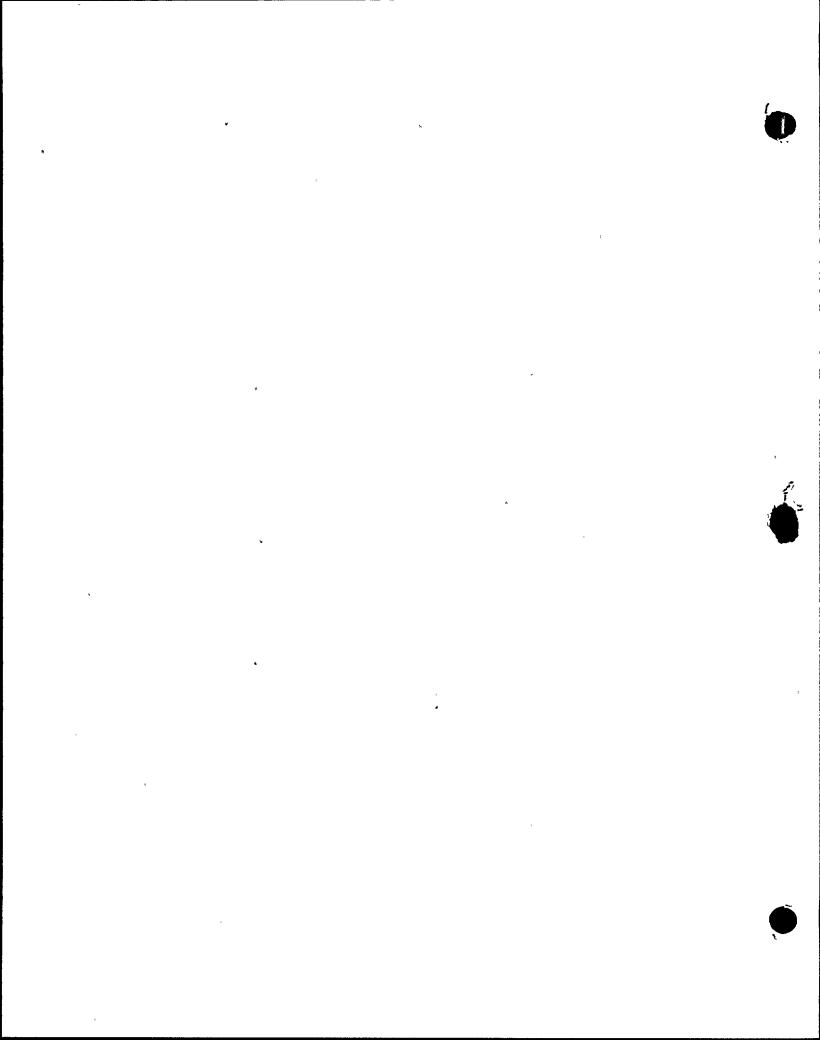


Electrical Penetrations

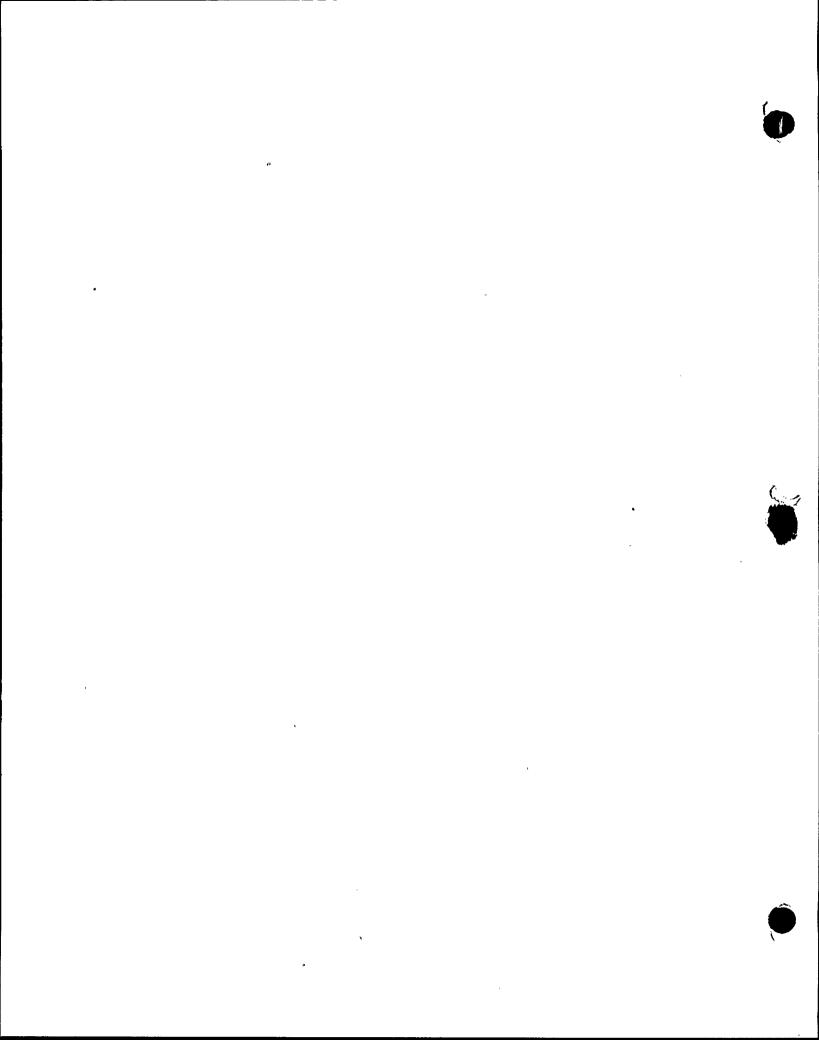
Penetration	Component Description	Leak Rate	Date Tested
X-100A	I&C Electrical Penetration	0.0229 0.0234 0.0077	09/16/83 05/18/84 07/28/95
X-100B	Neutron monitor Electrical Penetration	0.0229 0.0467 0.0385	09/16/83 05/18/84 07/26/95
,X . 100 C , 7,	Neutron monitor Electrical Penetration · · ·	0.0245 - 0.0375 0.0556	09/18/83 05/19/84 07/28/95
X-100D	Neutron monitor Electrical Penetration .	0.0000 0.0876 0.0062	09/18/83 05/19/84 07/28/95
X-100E	Neutron monitor Electrical Penetration	0.0305 0.0000 0.0309	09/18/83 05/19/84 07/28/95
X-100F	Neutron monitor Electrical Penetration	0.0000 0.0376 0.0371	09/18/83 05/18/84 07/28/95
X-100G	Neutron monitor Electrical Penetration	0.0230 0.0779 0.0309	09/17/83 05/18/84 09/17/95
X-101A	RCP POWER Electrical Penetration	0.0789 0.0000	05/20/84 09/07/95
X-101B	RCP POWER Electrical Penetration	0.0813 0.0187	05/20/84 07/27/95
X-101C	RCP POWER Electrical Penetration	0.0228 0.0287 0.0000 0.0356	09/17/83 05/20/84 05/22/84 11/02/95



<u>Penetration</u>	Component Description	Leak Rate	Date Tested
X-101D	RCP POWER Electrical Penetration	0.0000	09/17/83
		0.0330 0.0000	05/20/84 07/27/95
X-102	Thermocouple Electrical Penetration	0.0076	09/16/83
	,	0.0547 0.0154	05/18/84
		0.0154	07/25/95
X-103	CRD Pos. Ind. Electrical Penetration	0.0123 0.0313	09/18/83 05/18/84
te , • / 21 gg ••	and the second of the second o	0.037.1	07/28/95 · ·
X-104A	I&C Electrical Penetration	0.0194	09/17/83
		0.0198	05/18/84
		0.0196	07/26/95
X-104B	CRD Pos. Ind. Electrical Penetration	0.0129	09/18/83
		0.0527	05/18/84
	•	0.0261	07/25/95
X-104C	Neutron Monitor Electrical Penetration	0.0000	09/16/83
		0.0659	05/17/84
		0.0391	07/26/95
X-104D	Thermocouple Electrical Penetration	0.0061	09/18/83
=		0.0000	05/23/84
		0.0031	07/28/95
X-104E	I&C Electrical Penetration	0.0257	09/18/83
		0.0133	05/19/84
		0.0000	07/28/95
X-104F	I&C Electrical Penetration	. 0.0000	09/18/83
		0.0001	05/19/84
	•	0.0001	07/28/95
X-105B	RCP POWER Electrical Penetration	0.0125	05/20/84
		0.0000	07/27/95
X-105C	RCP POWER Electrical Penetration	0.0000	09/18/83
		0.0389	05/20/84
1		0.0000	07/27/95



Penetration	Component Description	Leak Rate	Date Tested
X-106A	CRD Pos. Ind. Electrical Penetration	0.0000 0.0467 0.0540	09/17/83 05/18/84 07/26/95
X-106B	Neutron Monitor Electrical Penetration	0.0152 0.0078 0.0232	09/16/83 05/17/84 07/25/95
X-107A	Neutron Monitor Electrical Penetration	0.0305 0.0701 . 0.0000.	09/16/83 05/17/84 07/26/95 -
X-107B	Neutron Monitor Electrical Penetration	0.0299 0.0382 0.0680	09/16/83 05/17/84 07/26/95
X-108A	Power Electrical Penetration	0.0000 0.0001 0.0001	09/18/83 05/22/84 07/27/95
X-108B	CRD Pos. Ind. Electrical Penetration	0.0129 0.0659 0.0325	09/18/83 05/18/84 07/28/95
X-109	CRD Pos. Ind. Electrical Penetration	0.0129 0.0000 0.0131	09/16/83 05/22/84 07/26/95
X-110A	Power Electrical Penetration	0.0064 0.0329 0.0131	09/17/83 05/22/84 07/27/95
X-110B	CRD Pos. Ind. Electrical Penetration	. 0.0185 0.0627 0.0185	09/18/83 05/18/84 07/28/95
X-219	PSC Vacuum Breaker Electrical Penetratio	n 0.0001 0.0001	05/22/84 07/27/95



Resilient Seals

Penetration	Component Description	Leak Rate	Date Tested
X-1A	Equipment Hatch	0.4746 0.0093	. 09/08/83 10/10/95
X-1B	Equipment Hatch	0.0275 0.0016 0.0011	09/08/83 09/14/84 10/08/95
X-4	DW Head Access Hatch	0.0000 .0.0007 <i>z. z</i> .	07/11/84 09/30/95
X-6 ,	CRD Hatch	0.1981 0.0002 0.0004	09/15/83 09/11/84 10/10/95
X-35A	TIP Indexer Flange	0.0000 0.0000 0.0001	05/21/84 09/14/84 08/06/95
X-35B	TIP Indexer Flange	0.0000 0.0001	05/21/84 08/06/95
X-35C	TIP Indexer Flange	0.0000 0.0000 0.0000 0.0001	05/21/84 09/07/84 09/14/84 08/06/95
X-35D	TIP Indexer Flange	0.0000 0.0001	05/21/84 08/06/95
X-35E	TIP Indexer Flange	0.0000 . 0.0001	05/21/84 08/06/95
`X-35F	TIP Indexer Purge Flange	0.0001 0.0000 0.0000 0.0001	05/21/84 09/07/84 09/14/84 08/06/95
X-35G	Spare	0.0001 0.0000 0.0001	05/21/84 09/07/84 08/06/95



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Penetration	Component Description	Leak Rate	Date Tested
X-47	Power Operations Test Flange	0.0000 0.0003	06/03/84 10/10/95
X-200A	Torus Access Hatch	0.0042 0.0000 0.0007	09/12/83 09/15/84 11/06/95
X-200B	Torus Access Hatch	0.0000 0.0002 0.0003	09/12/83 09/10/84 09/30/95
X-213A ¹	Torus Drain Flange	0.0001 0.0037 0.0000 0.0000	09/15/83 05/05/84 10/15/84 09/30/95
N/A	Drywell Head	0.0516 0.0268 0.0282	09/08/83 09/23/84 11/05/95
N/A	Shear Lug @ 0° Azmith	0.0004 0.0009	06/03/84 09/28/95
N/A	Shear Lug @ 45° Azmith	0.0001 0.0000	06/03/84 09/28/95
N/A	Shear Lug @ 90° Azmith	0.0000 8000.0	06/03/84 09/28/95
N/A	Shear Lug @ 135° Azmith	0.0000 0.0015	06/04/84 09/28/95
N/A	Shear Lug @ 180° Azmith	. 0.0000 0.0000	06/04/84 09/28/95
N/A .	Shear Lug @ 225° Azmith	0.0000 0.0022	06/04/84 09/28/95

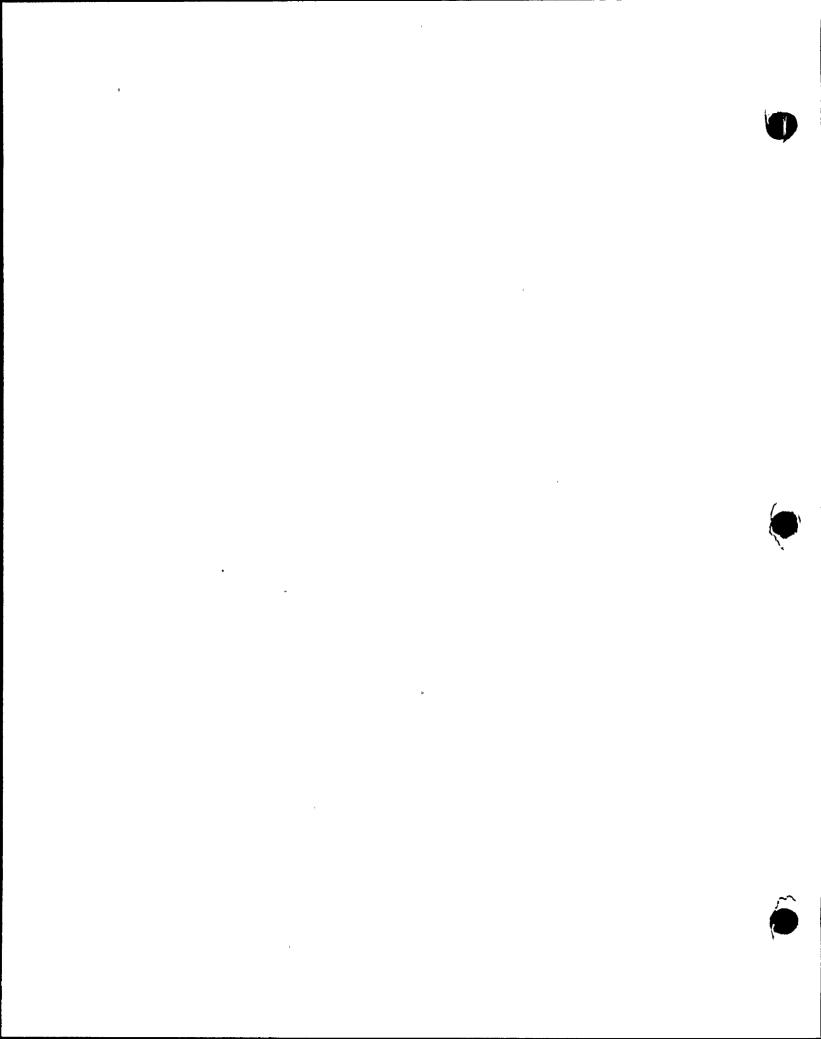
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¹ Flange seal-welded during Cycle 6 outage

Penetration	Component Description	Leak Rate	Date Tested
N/A	Shear Lug @ 270° Azmith	0.0000 0.0000	06/03/84 09/28/95
N/A	Shear Lug @ 315° Azmith	0.0000 0.0026	06/03/84 09/28/95

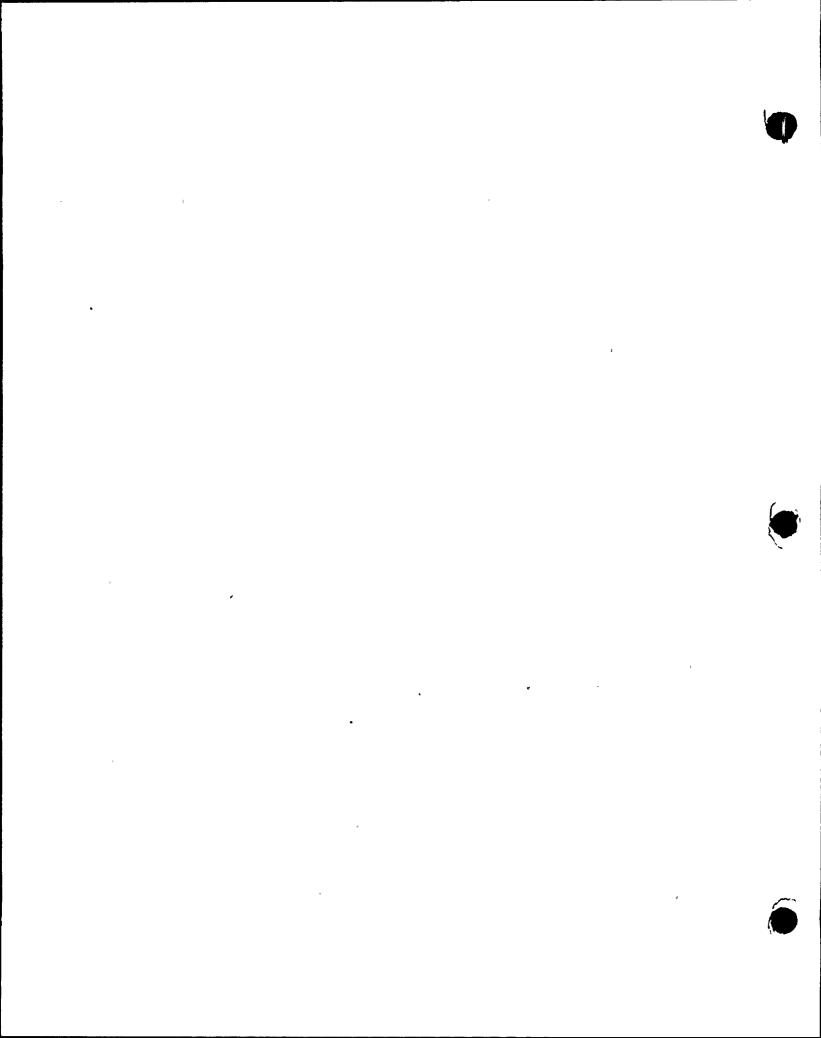
Type C Testing Summary

Penetration	Valve No.	Description	Leak Rate	Date Tested
X-7A	3-FCV-1-14/1	5"A" Main Steam Line MSIVs	2615.5389 6.8072 7.9440 0.0000	09/17/83 06/07/84 06/17/84 10/18/95
X-7B	3-FCV-1-26/27	"B" Main Steam Line MSIVs	7.0563 7.8765 7.0845 5.2861	09/18/83 05/15/84 05/15/84 10/33/95
X-7C	3-FCV-1-37/38	"C" Main Steam Line MSIV'S	37.5728 3.7306 2.2638	09/18/83 05/25/84 10/18/95
	3-FCV-1-37	"C" Main Steam Line I.B. MSIV	2.2049	03/14/84
	3-FCV-1-38	"C" Main Steam Line O.B. MSIV	35.3679 1.5126	03/14/84 05/25/84
X-7D	3-FCV-1-51/52	"D" Main Steam Line MSIVs	2652.7217 9.7966 0.1246	09/18/83 05/31/84 10/25/95
	3-FCV-1-51	"D" Main Steam Line I.B. MSIV	5.4108 5.4108	05/31/84 11/02/84
	3-FCV-1-52	"D" Main Steam Line O.B. MSIV	4.3858	05/31/84
X-8	3-FCV-1-55/56	Main Steam Drain Isolation Valves .	139.5777 0.0000	09/01/83 07/02/84
	3-FCV-1-55	Main Steam Drain I.B. Isolation Valve	0.0000	10/07/95
•	3-FCV-1-56	Main Steam Drain O.B. Isolation Valve	0.0000	10/07/95



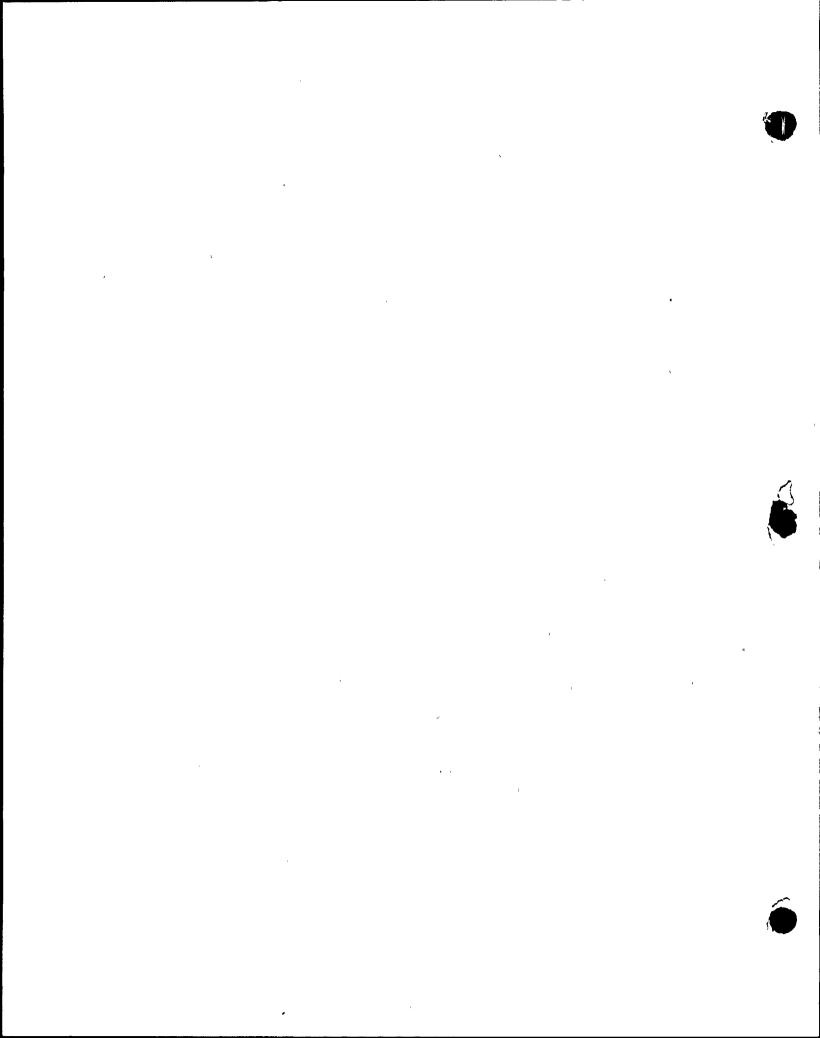
Penetration.	Valve No.	Description	Leak Rate	Date Tested
X-9A	3-CKV-3-558	"A" Feedwater O.B. Isolation Valve	9.1154 11.2151 6.2849	02/16/84 09/07/84 09/14/95
	3-CKV-3-554	"A" Feedwater I.B. Isolation Valve	0.0000 8.3457	02/16/84 09/07/84
	3-FCV-73-44 ¹	HPCI Tie-in to "A" Feedwater O.B. Isolation Valve	1.5643 0.0000	02/17/84 09/08/84 、
	,3-FCV-73-45	HPCI Tie-in to "A" Feedwater O.B. Isolation Valve	0.0000 8.3457 7.7180	02/16/84 - 09/07/84 09/18/95
	3-CKV-69-624	Reactor Water Clean-up Return Tie-in To "A" Feedwater O.B. Isolation Valve	0.0000 0.0000	02/17/84 09/09/84
	3-CKV-69-628 ²	Reactor Water Clean-up Return Tie-in To "A" Feedwater O.B. Isolation Valve	0.0000	09/18/95
X-9B	3-CKV-3-572	"B" Feedwater O.B. Isolation Valve	1.9320 3.3576	04/26/84 09/20/95
	3-CKV-3-568	"B" Feedwater I.B. Isolation Valve	6.5900 0.0006	04/26/84 09/20/95
	3-CKV-69-579	Reactor Water Clean-up Return Tie-in To "B" Feedwater O.B. Isolation Valve	2.3979	04/26/84
	3-FCV-71-39 ³	RCIC Tie-in to "B" Feedwater O.B. Isolation Valve	0.0000	04/26/84

Isolation valve designation removed during cycle 6 outage.
 New designated isolation valve replaced 3-CKV-69-624 during cycle 5 outage.
 Isolation valve designation removed during cycle 6 outage.



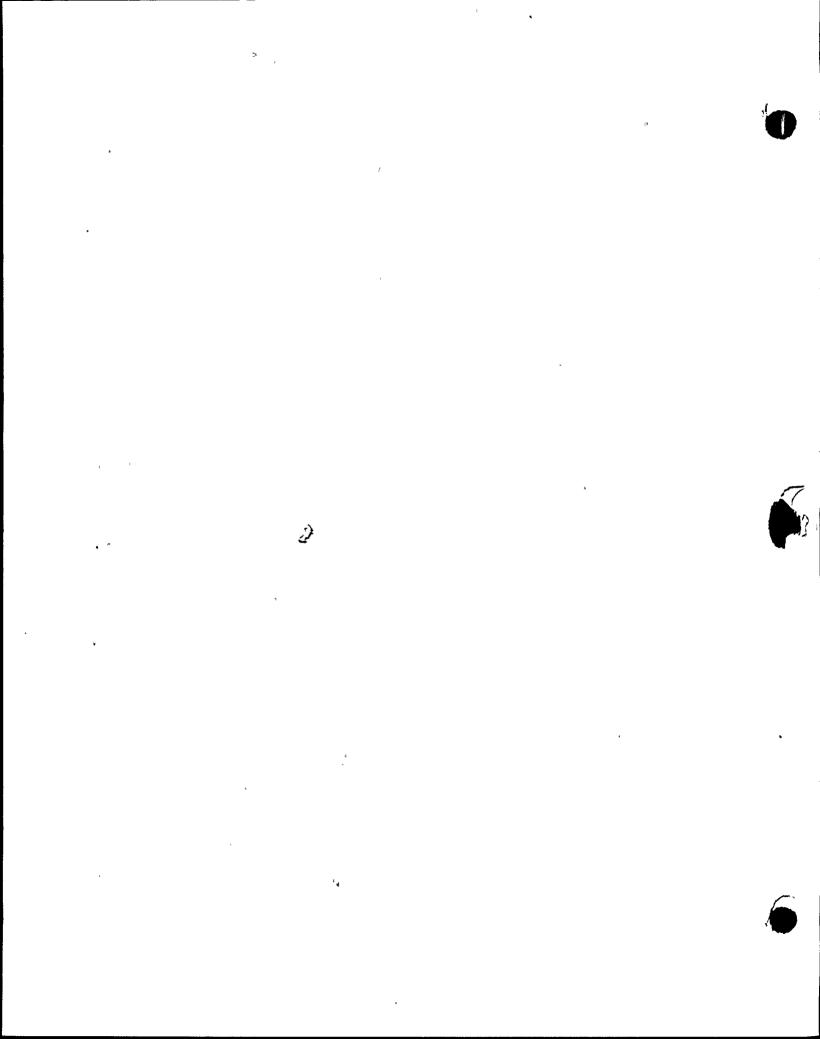
Penetration	Valve No.	Description	Leak Rate	Date Tested
X-9B (cont.)	3-CKV-69-629 ¹	Reactor Water Clean-up Return Tie-in To "B" Feedwater O.B. Isolation Valve	0.5302	09/20/95
	3-FCV-71-40	RCIC Tie-in to "B" Feedwater O.B. Isolation Valve	6.5900 0.0000	04/26/84 09/20/95
	3-CKV-85-576	CRD Return Tie-in to "B" Feedwater O.B. Isolation Valve	0.1940	04/26/84
X-10,	3-FCV-71-2/3	RCIC Steam Supply Isolation . Valves	0.2529 26.2549 0.1219 0.0000	09/17/83 05/17/84 06/13/84 10/08/95
X-11	3-FCV-73-2/3 /81	HPCI Steam Supply Isolation Valves	2.2129 0.0000 0.9155	09/18/83 05/17/84 11/01/95
X-12	3-FCV-74-47	RHR Shutdown Cooling Suction I.B. Isolation Valve	1.2465 0.0000	03/21/84 09/13/95
	3-FCV-74-48	RHR Shutdown Cooling Suction O.B. Isolation Valve	0.0000 2.3629	03/21/84 09/13/95
	3-CKV-74-661/ 662	RHR Shutdown Cooling Suction Bypass Isolation Valve	0.0000 0.1296	03/21/84 09/13/95
X-13A	3-FCV-74-53	RHR Loop 1 LPCI O.B. Isolation Valve (W/S)	0.0630 0.0225 0.0788	09/10/84 11/08/84 08/31/95
	3-FCV-74-54	RHR Loop 1 LPCI I.B. Isolation Valve (W/S)	44.1899 2.0409 1.4516 0.6750	01/18/84 04/19/84 10/08/84 08/31/95

¹ New designated isolation valve replaced 3-CKV-69-579 and 3-CKV-85-576 during cycle 6 outage



Penetration	Valve No.	Description	Leak Rate	Date Tested
X-13B	3-FCV-74-67	RHR Loop 2 LPCI O.B. Isolation Valve (W/S)	0.1017 2.7000 0.0158 0.0225	01/18/84 03/24/84 09/18/84 08/29/95
	3-FCV-74-68	RHR Loop 2 LPCI I.B. Isolation Valve (W/S)	40.5000 3.6269 27.0000 0.3555 0.1238	01/17/84 01/31/84 09/18/84 09/30/84 08/29/95
X-14	3-FCV-69-1	Reactor Water Cleanup I.B. Isolation Valve	0.3703 5.3323 0.0000	09/08/83 06/05/84 09/20/95
	3-FCV-69-2	Reactor Water Cleanup O.B. Isolation Valve	0.3703 1.2583 2.5378	09/08/83 06/05/84 09/20/95
X-16A	3-FCV-75-25	CS Loop 1 Injection O.B. Isolation Valve (W/S)	0.0141 0.1377 0.0281	02/15/84 09/09/84 05/24/95
	3-FCV-75-26	CS Loop 1 Injection I.B. Isolation Valve (W/S)	40.5000 0.2295 1.0506 0.0169	02/15/84 02/17/84 09/09/84 05/24/95
X-16B	3-FCV-75-53	CS Loop 2 Injection O.B. Isolation Valve (W/S)	0.0000 0.0180 0.0028	03/07/84 09/07/84 06/07/95
X-16B	3-FCV-75-54	CS Loop 2 Injection I.B. Isolation Valve (W/S)	0.0018 0.0247 2.1131	03/07/84 09/07/84 09/14/95
X-17 ¹	3-FCV-74-77/7	8 RHR Head Spray	0.0000	03/29/84
X-18	3-FCV-77-2A/ 2B	Drywell Floor Drain Sump Isolation Valves	0.3243 0.0000	09/18/83 05/20/84

¹ Line Removed and Sealed during Cycle 6 outage

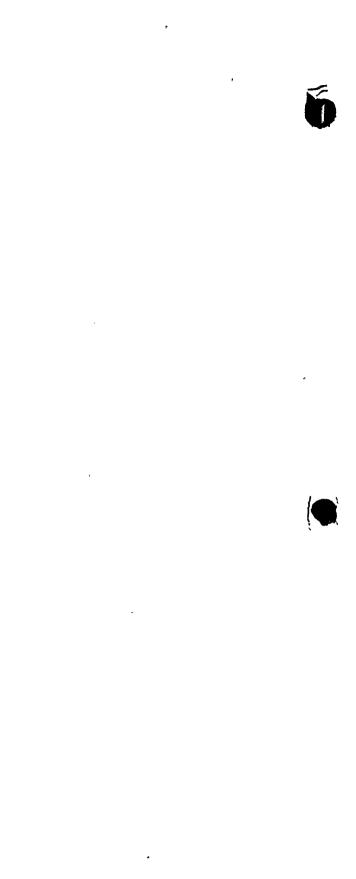


	Penetration	_Valve No.	Description	Leak Rate	Date Tested
•	X-18 (cont.)	3-FCV-77-2A	Drywell Floor Drain Sump I.B. Isolation Valve	4.0333	10/07/95
	H	3-FCV-77-2B	Drywell Floor Drain Sump O.B. Isolation Valve	0.7329	10/07/95
," <i>,</i>	X-19		Drywell Floor Drain Sump Isolation Valves	0.0584 0.0000	09/18/83 05/20/84
*** * * * * * * * * * * * * * * * * * *	, <u>, , , , , , , , , , , , , , , , , , </u>	3-FCV-77-15A	Drywell Equipment Sump Drain I.B. Isolation Valve	. 0.1461	10/06/95
		3-FCV-77-15B	Drywell Equipment Drain Sump O.B. Isolation Valve	0.0000	10/06/95
	X-20	3-ISV-2-1192	Demin. Water I.B. Isolation Valve	0.5594 0.9099	09/11/83 09/10/95
		3-CKV-2-1383	Demin. Water O.B. Isolation Valve	0.0000 0.0000	09/11/83 09/10/95
<u>.</u>	X-21	3-CKV-33-785	Service Air I.B. Isolation Valve	0.0381 0.1400 0.0000	09/11/83 05/18/84 09/24/95
		3-ISV-33-1070	Service Air O.B. Isolation Valve	0.0042 0.0000 0.6627	09/12/83 05/18/84 09/24/95
	X-22	3-CKV-32-336	Control Air I.B. Isolation Valve	0.0000 1.2168	05/18/84 09/17/95
		3-CKV-32-2163	Control Air O.B. Isolation Valve	0.0000	05/18/84
		3-FSV-84-49/ ¹ 686	Containment Atmosphere Dilution Tie-in to Control Air	0.0000 0.1574	09/16/95 09/17/95
	X-23	3-FCV-70-47 ²	Reactor Building Closed Cooling Water Isolation Valve	0.0000	09/18/95

¹ Valves added during Cycle 6 outage.2 Valves added to test program during Cycle 6 outage

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Penetration	Valve No.	Description	Leak Rate	Date Tested
X-24	3-CKV-70-506 ¹	Reactor Building Closed Cooling Water Isolation Valve	4.7043	09/18/95
X-25	3-FCV-64-18 Flange	Ventilation Supply Isolation Valve I.B. Flange	0.0002 0.0002	09/19/84 09/21/95
	3-FCV-76-18 Flange Isolati	Drywell Inerting Supply on Valve I.B. Flange	0.0000 0.0004	05/23/84 09/07/95
	3-FSV-84-8A	Flange ²	0.0000	06/04/84
	3-FSV-84-8D	Flange ²	0.0000	06/04/84
	3-FSV-84-8A/ ³ 600	CAD Isolation Valves	132.0000 0.0000	09/12/83 10/02/84
	3-FSV-84-8A	CAD I.B. Isolation Valve	0.0340	08/09/95
	3-CKV-84-600	CAD O.B. Isolation Valve	0.0166	08/09/95
	3-FSV-84-8D/ ³ 602	CAD Isolation Valves	132.0000 1.7143	09/12/83 10/04/84
	3-FSV-84-8D	CAD I.B. Isolation Valve	0.0031	08/09/95
	3-CKV-84-602	CAD O.B. Isolation Valve	0.0200	08/09/95
X-25/ 205		Ventilation Supply Isolation Valves	4.7941 6.8909 3.8101	09/13/83 09/26/84 09/21/95
		Containment Inerting Supply Isolation Valves .	0.0000 0.00000 0.0000 0.2346	09/13/83 05/05/84 06/06/84 09/21/95

Valves added to test program during Cycle 6 outage
 Valve arrangement modified during Cycle 6 outage. Flange no longer tested.
 Modification Performed to allow valves to be individually tested during Cycle 6.

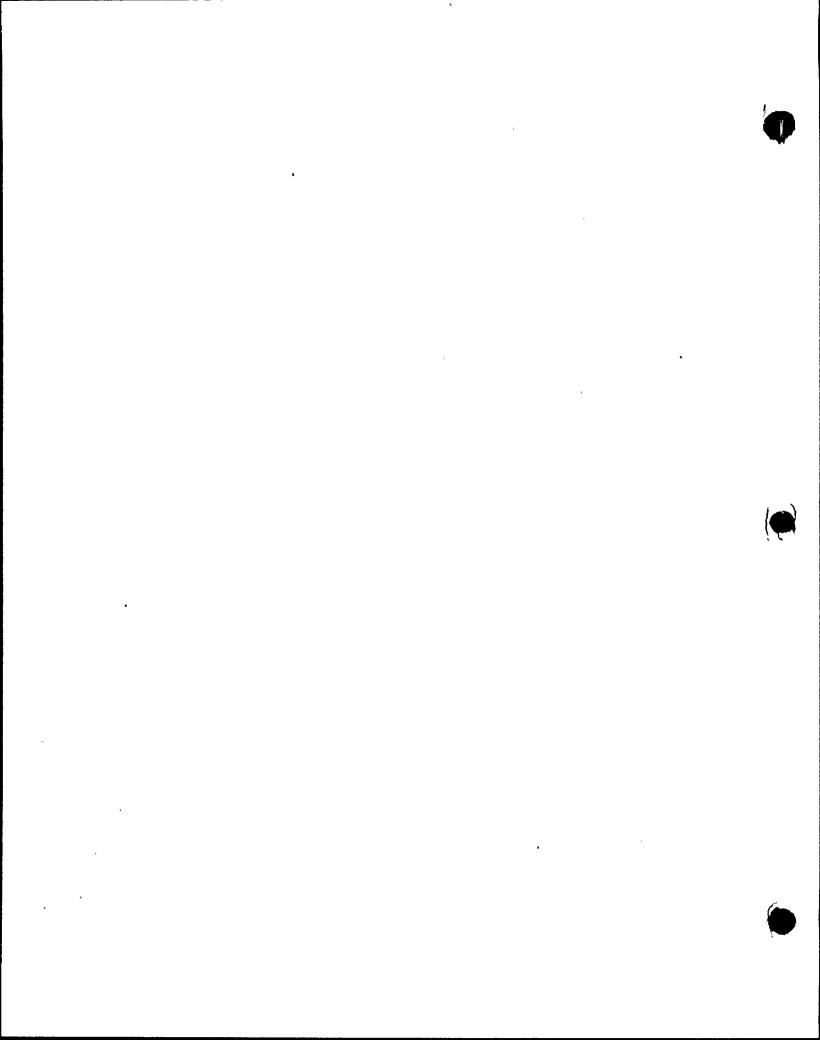


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Penetration	Valve No.	Description	Leak Rate	Date Tested
X-26	3-FCV-64-29 Flange	Ventilation Exhaust Isolation Valve I.B. Flange	0.0028 0.1589 0.0000	09/08/84 09/08/84 10/09/95
X-26	3-FCV-64-31 Flange	Ventilation Exhaust Isolation Valve I.B. Flange	0.0000 0.0000 0.0001	09/08/84 10/04/84 09/21/95
X-26/ 231	30/32/33/84-19	Ventilation Exhaust Isolation Valves	86.8340 23.7464 3.7297	09/14/83 10/13/84 10/09/95
	3-FCV-64-31/3- /139/140/84-20	4Ventilation Exhaust Isolation Valves	3 4.0922 7.2047 3.9963	09/13/83 10/05/84 10/26/95
X-27E	23-FSV-76-51 ¹	H ₂ O ₂ Sampling I.B. Isolation Valve	0.0000 0.0081	09/19/83 05/22/84
	23-FSV-76-52 ¹	H ₂ O ₂ Sampling I.B. Isolation Valve	0.0000 0.0081	09/19/83 05/22/84
X-27F	23-FSV-76-49	H ₂ O ₂ Sampling I.B. Isolation Valve (Analyzer A, Drywell Sample)	0.0000 0.0000 0.0000	09/19/83 05/22/84 10/08/95
	3-FSV-76-50	H ₂ O ₂ Sampling O.B. Isolation Valve (Analyzer A, Drywell Sample)	0.0000 0.0000	09/19/3 10/08/95
X-35A	3-FCV-94-501	TIP Isolation Valve	1.5518 0.0986 0.0993	05/21/84 10/10/84 08/08/95
X-35B	3-FCV-94-502	TIP Isolation Valve	0.9330 0.2780	05/21/84 08/07/95
X-35C	3-FCV-94-503	TIP Isolation Valve	4.9355 0.0000	05/21/84 10/10/84
1 Valves ren	noved during Cy	cle 6 outage	0.0664	08/07/95



Penetration	Valve No.	Description	Leak Rate	Date Tested
X-35D	3-FCV-94-504	TIP Isolation Valve	0.0000 0.0081	05/21/84 08/07/95
X-35E	3-FCV-94-505	TIP Isolation Valve	0.0000 0.0396	05/21/84 08/07/95
X-35F	3-CKV-76-234	TIP Nitrogen Purge Isolation Valve	0.8886 0.0000	05/21/84 10/10/84
	3-CKV-76-653 ¹	TIP Nitrogen Purge Isolation Valve		08/06/95
X-37C	3-CKV-68-508	CRD Seal Water to RCP "A" I.B. Isolation Valves	0.9957 0.0000 0.0000 0.0000	09/17/83 03/13/84 09/08/84 09/11/95
	3-CKV-68-550	CRD Seal Water to RCP "A" O.B. Isolation Valves	401.7110 0.0000 0.0000 0.0000	09/17/83 03/13/84 09/08/84 09/11/95
X-38C	3-CKV-68-523	CRD Seal Water to RCP "B" I.B. Isolation Valves	19.7078 0.0000 0.0000 0.0000	09/17/83 03/13/44 09/08/84 09/09/95
	3-CKV-68-555	CRD Seal Water to RCP "B" O.B. Isolation Valves	73.6851 0.0000 0.0000 0.0000	09/17/83 03/13/44 09/08/84 09/09/95
X-39A	3-FCV-74-74/7	5 ² RHR Loop 2 Containment Spray Isolation Valves	0.0900	03/23/84
	3-FCV-74-74	RHR Loop 2 Containment Spray O.B. Isolation Valve (W/S)	0.0141	08/24/95
	3-FCV-74-75	RHR Loop 2 Containment Spray I.B. Isolation Valve (W/S)	0.2588	08/24/95

Valve 3-CKV-76-234 replaced by CKV-76-653 during Cycle 6 outage.
 Test method tested valves separately during Cycle 6 outage.

	Penetration	Valve No.	Description	Leak Rate	<u>DateTested</u>
	X-39B	3-FCV-74-60/6	1 ¹ RHR Loop 1 Containment Spray O.B. Isolation Valve (W/S)	2.0083	04/19/84
	['] X-39B	3-FCV-74-60	RHR Loop 1 Containment Spray O.B. Isolation Valve (W/S)	0.0619	09/29/95
٠,		3-FCV-74-61	RHR Loop 1 Containment Spray I.B. Isolation Valve (W/S)	0.8571	09/29/95
ayer alon to		3-FSV-43-70 ²	Post-Accident Sampling Isolation Valve.	0.0000	10/17/95
	X-41	3-FCV-43-13	RCP Sample I.B. Isolation Valve	0.3614 0.4218	03/29/84 10/08/95
		3-FCV-43-14	RCP Sample O.B. Isolation Valve	0.5477 0.0000	03/29/84 10/03/95
	X-42	3-CKV-63-525	Standby Liquid Control I.B. Isolation Valve	0.0000 0.5763	03/21/84 07/28/95
		3-CKV-63-526	Standby Liquid Control O.B Isolation Valve	0.0000 0.7608	03/21/84 07/12/95
	X-48	3-FCV-32-62/63	3 Drywell Control Air Suction Isolation Valves	0.0000 1.2271	03/28/84 09/05/95
	X-50A/D		V ³ Radiation Monitoring Suction . Isolation Valves	0.0000 0.0514	09/11/83 05/17/84
		3-FSV-90-254A	Radiation Monitoring Suction I.B. Isolation Valve	0.0000	09/15/95
		3-FSV-90-254E	Radiation Monitoring Suction I.B. Isolation Valve	0.0000	09/15/95

Test method tested valves separately during Cycle 6 outage.
 Valve added during Cycle 6 outage.
 Valves replaced with new valves during Cycle 6 outage

Penetration	Valve No.	Description	Leak Rate	Date Tested
X-50A/D (cont.)	3-FSV-90-255	Radiation Monitoring Suction O.B. Isolation Valve	0.0000	09/15/95
X-50B	3-CKV-32-2516	6 ¹ Control Air I.B. Isolation Valve	0.4300	09/14/95
	3-CKV-32-252	¹ Control Air O.B. Isolation Valve	0.0000	09/14/95
	3-FSV-84-48/ ¹ 683	Containment Atmosphere Dilution Tie-in to Control Air	0.1006	09/14/95
X-50C, ,,		N ² Radiation Monitoring Return B O.B. Isolation Valve	0.4217 0.4161	.09/11/83 05/17/84
1	3-FSV-90-257A	Radiation Monitoring Return O.B. Isolation Valve	0.0000	09/15/95
•	3-FSV-90-257E	Radiation Monitoring Return I.B. Isolation Valve	0.0000	09/15/95
X-52B	3-FSV-76-59	H ₂ O ₂ Sampling I.B. Isolation Valve (Analyzer A, Drywell Sample)	0.0000 0.0000 0.0000	09/19/83 06/21/84 08/15/95
	3-FSV-76-60	H ₂ O ₂ Sampling O.B. Isolation Valve (Analyzer A, Drywell Sample)	0.0000 0.0000 0.0051	09/19/83 06/21/84 08/15/95
X-52C	3-FCV-76-61	H ₂ O ₂ Sampling I.B. Isolation Valve (Analyzer B, Drywell Sample)	0.0000 0.0000	09/19/83 06/21/84
	3-FCV-76-62	H ₂ O ₂ Sampling O.B. Isolation Valve (Analyzer B, Drywell Sample)	0.0000 0.0000	09/19/83 06/21/84
X-205	3-FCV-64-19	Ventilation Supply Isolation Valve I.B. Flange	0.0000 0.0000 0.0001	09/08/84 10/04/84 09/21/95

Valve added during Cycle 6 outage.
 Valves replaced with new valves during Cycle 6 outage

Penetration	Valve No.	Description	Leak Rate	Date Tested
X-205 (cont.)	3-FCV-64-20/ 800	Reactor Building-to-Torus Vacuum Breaker Isolation Valves	0.0000 0.0000 1.0749	09/13/83 09/10/84 10/01/95
	3-FCV-64-20	Reactor Building-to-Torus Vacuum Breaker Isolation Valve I.B. Flange		09/06/84 10/01/95
	3-FCV-64-21/ 801	Reactor Building-to-Torus Vacuum Breaker Isolation Valves	0.0000 0.3268 0.0000	09/13/83 09/18/84 10/20/95
	3-FCV-64-21	Reactor Building-to-Torus Vacuum Breaker Isolation Valve I.B. Flange	0.0024 0.0000	09/06/84 10/20/95
		Hardened Wetwell Vent Isolation Valves	1.7670	08/26/95
	3-FCV-64-222 ¹	Hardened Wetwell Vent I.B. Isolation Valve Flange	0.0000	08/26/95
	3-FCV-76-19 Flange	Torus Inerting Supply Isolation Valve I.B. Flange	0.0000 0.0000	05/23/84 09/07/95
	3-FSV-84-8B/ ² 601	CAD Isolation Valves	0.0000 0.0000	09/12/83 10/08/84
	3-FSV-84-8B	CAD I.B. Isolation Valve	0.0672	08/09/95
	3-CKV-84-601	CAD O.B. Isolation Valve	0.0148	08/09/95
	3-FSV-84-8C/ ² 603	CAD Isolation Valves .	0.0000 0.0701 0.1253	09/12/83 10/02/84 10/08/84
	3-FSV-84-8C	CAD I.B. Isolation Valve	0.2750	08/09/95
	3-CKV-84-603	CAD O.B. Isolation Valve	0.0064	08/09/95

Line and valves added during Cycle 6 outage
 Modification performed to allow valves to be individually tested during Cycle 6.

Penetration	Valve No	Description ·	Leak Rate	Date Tested
X-205	3-FSV-84-8B ¹	Flange	0.0000 0.0000	06/07/84 10/08/84
	3-FSV-84-8C ¹	Flange	0.0000 0.0000 0.0000	06/04/84 09/28/84 10/15/84
X-210A	3-CKV-12-738 ²	Auxiliary Boiler Tie-in to torus I.B. Isolation Valve (W)	0.0079 0.0073	09/11/83 05/19/84
	3-CKV-12-741 ²	Auxiliary Boiler Tie-in to torus O.B. Isolation Valve (W)	0.0152 0.0076	09/11/85 05/19/84
X-210A	3-FCV-71-34 ³	RCIC Minimum Flow I.B. Isolation Valve (W)	0.0000	09/06/95
X-210A	3-CKV-71-547 ³	RCIC Minimum Flow O.B. Isolation Valve (W)	0.0000	09/06/95
X-210B	3-FCV-73-30 ³	HPCI Minimum Flow I.B. Isolation Valve (W)	0.0000	09/24/95
	3-CKV-73-559 ³	HPCI Minimum Flow O.B. Isolation Valve (W)	0.0000	09/24/95
X-211A	3-FCV-74-57/ 58/59	RHR Loop 1 Torus Spray Isolation Valves (W/S)	37.3846 0.0900 0.0630 0.3853	11/19/83 11/20/83 05/31/84 09/26/95
X-211B	3-FCV-74-71/ 72/73	RHR Loop 2 Torus Spray Isolation Valves (W/S)	0.5175 0.2412 3.3986	11/06/83 06/06/84 08/25/95
X-212		RCIC Turbine Exhaust Isolation Valves	8.5263 0.0072 3.5470	09/13/83 09/06/84 09/06/95

Valve arrangement modified during Cycle 6 outage. Flange no longer tested.
 Valves removed and line permanently terminated during Cycle 6 outage.
 Added to test program during Cycle 6 outage.



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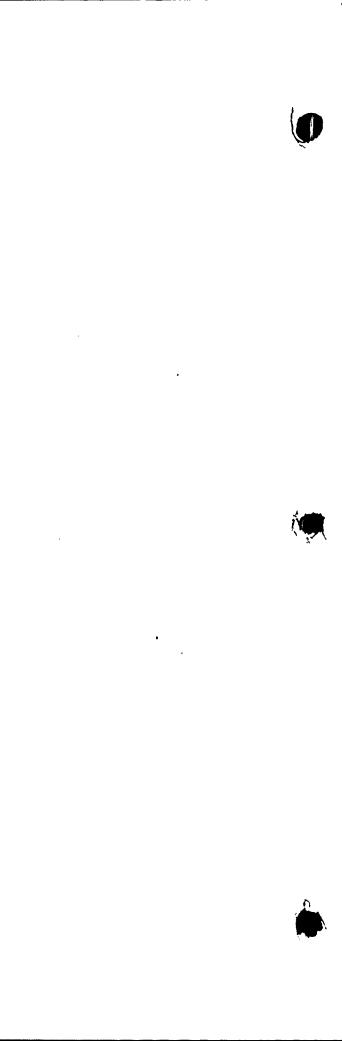
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	Penetration	Valve No.	Description	Leak Rate	Date Tested
	X-212 (cont.)	3-HCV-71-14 ¹ Bonnet	RCIC Turbine Exhaust I.B. Isolation Valve Bonnet Flange	0.0000	09/06/95
		3-HCV-71-14 ¹ Packing	RCIC Turbine Exhaust I.B. Isolation Valve Packing	0.0000	09/06/95
	X-213B	3-ISV-74-722	Torus Drain Isolation Valve (W)	2.9847 0.0699	09/12/83 05/05/84
۹.	y ** m*		Torus Drain Isolation Valve Blind Flange (W)	0.1260	09/11/95
	X-214	3-ISV-73-23/ 603	HPCI Turbine Exhaust Isolation Valves	16.2000 0.3375 0.1635 7.9192	09/14/83 01/09/84 09/08/84 09/19/95
		3-ISV-73-23 ¹ Bonnet	HPCI Turbine Exhaust I.B. Isolation Valve Bonnet	0.0000	09/19/95
		3-ISV-73-23 ¹ Packing	HPCI Turbine Exhaust I.B. Isolation Valve Packing	0.0000	11/07/95
	X-218	3-FCV-71-59/ ¹ 597/598/ 599/600/601 Bonnet & Pac	RCIC Turbine Exhaust Vacuum Breaker Line Valves Bonnet/Packing	0.0000 3	09/17/95
	X-220	3-FCV-73-64/ ¹ 633/634/ 635/636/642 Bonnet & Pac	HPCI Turbine Exhaust Vacuum Breaker Line Valves Bonnet/Packing king	0.0000 3	09/17/95
	X-221	3-SHV-71-32/ 592	RCIC Vacuum Pump Discharge Isolation Valves (W)	0.0076 0.0563 0.0038	09/13/83 05/20/84 09/15/95
		3-SHV-71-32 ¹ Bonnet & Packing	RCIC Vacuum Pump Discharge I.B. Isolation Valve Bonnet and Packing	0.0000	09/15/95

¹ Added to test program during Cycle 6 outage.



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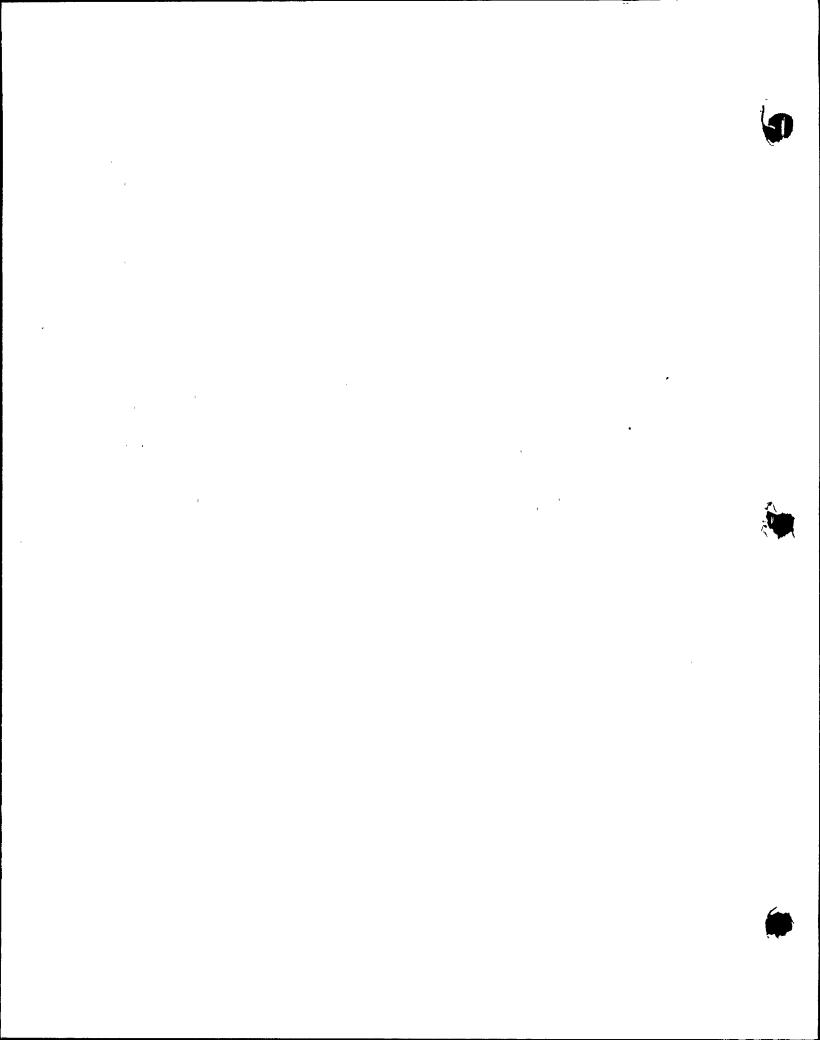
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	Penetration	Valve No.	Description	Leak Rate	Date Tested
	X-222	3-ISV-73-24/ 609	HPCI Turbine Exhaust Drain Isolation Valves	0.0113 0.0000 0.0492	09/14/83 05/20/84 08/21/95
	X-222 (cont.)	3-ISV-73-24 ¹ Bonnet & Packing	HPCI Turbine Exhaust Drain I.B. Isolation Valve Bonnet and Packing	0.0000	11/07/95
٠.	X-225A		RHR Sample I.B. Isolation Valve	0.0051 0.0000	09/13/83 05/19/84.
		3-FSV-43-28B ²	RHR Sample O.B. Isolation Valve	0.0000 0.0000	09/13/83 05/19/84
	X-225B	3-FSV-43-29A ²	RHR Sample I.B. Isolation Valve	0.0030 0.0038	09/13/83 05/19/84
		3-FSV-43-29B ²	RHR Sample O.B. Isolation Valve	0.0000 0.0127	09/13/83 05/19/84
	X-226	3-FCV-73-26 ¹	HPCI Torus Suction I.B. Isolation Valve (W)	0.7033	10/17/95
		3-FCV-73-27 ¹	HPCI Torus Suction O.B. Isolation Valve (W)	0.7594	10/17/95
	X-227A	3-FCV-71-17 ¹	RCIC Torus Suction I.B. Isolation Valve (W)	0.0000	09/10/95
		3-FCV-71-18 ¹	RCIC Torus Suction O.B. Isolation Valve (W)	0.0126	10/05/95
		3-FCV-75-57/58	CS Torus Drain Isolation Valves (W)	0.0135 0.0000 0.0000 0.0338	02/17/84 02/17/84 09/09/84 08/22/95

Added to test program during Cycle 6 outage.
 Isolation boundary changed, valve removed from program during Cycle 6 Outage



Penetration	Valve No.	Description	Leak Rate	Date Tested
X-228	3-HCV-2-1143	¹ Demin. Water to Torus	0.0438	09/11/83
X-229A ²	3-FSV-76-5 ⁷³	H₂O₂ Sampling I.B. Isolation Valve (Analyzer A, Sample Return to Torus)	0.1541)	09/12/95
	3-FSV-76-58 ³	H ₂ O ₂ Sampling O.B. Isolation Valve (Analyzer A, Sample Return to Torus		09/12/95
X-229B ²	3-FSV-76-57 ³	H₂O₂ Sampling I.B. Isolation Valve (Analyzer A, Sample Return to Torus)	0.0000	06/03/84
1 M. W. K. F.	3-FSV-76-58 ³	H₂O₂ Sampling O.B. Isolation Valve (Analyzer A, Sample Return to Torus		 06/03/84
X-229C	3-FSV-76-53 ⁴	H ₂ O ₂ Sampling I.B. Isolation Valve	0.0000	06/03/84
	3-FSV-76-54 ⁴	H ₂ O ₂ Sampling O.B. Isolation Valve	0.0000	06/03/84
X-229D⁵	3-FSV-76-55 ³	H ₂ O ₂ Sampling I.B. Isolation Valve (Analyzer A, Torus Sample)	0.0000	06/02/84
· ·	3-FSV-76-56 ³	H ₂ O ₂ Sampling O.B. Isolation Valve (Analyzer A, Torus Sample)	0.0000	06/02/84
X-229G	3-FSV-76-67 ³	H₂O₂ Sampling I.B. Isolation Valve (Analyzer B, Sample Return to Torus	0.0000 3)0.0983	09/12/95 06/03/84
	3-FSV-76-68 ³	H ₂ O ₂ Sampling O.B. Isolation Valve (Analyzer B, Sample Return to Torus		06/03/84 09/12/95

¹ Valve removed and line permanently terminated during Cycle 6 outage.

² Line changed from X-229B to X229A during Cycle 6 outage

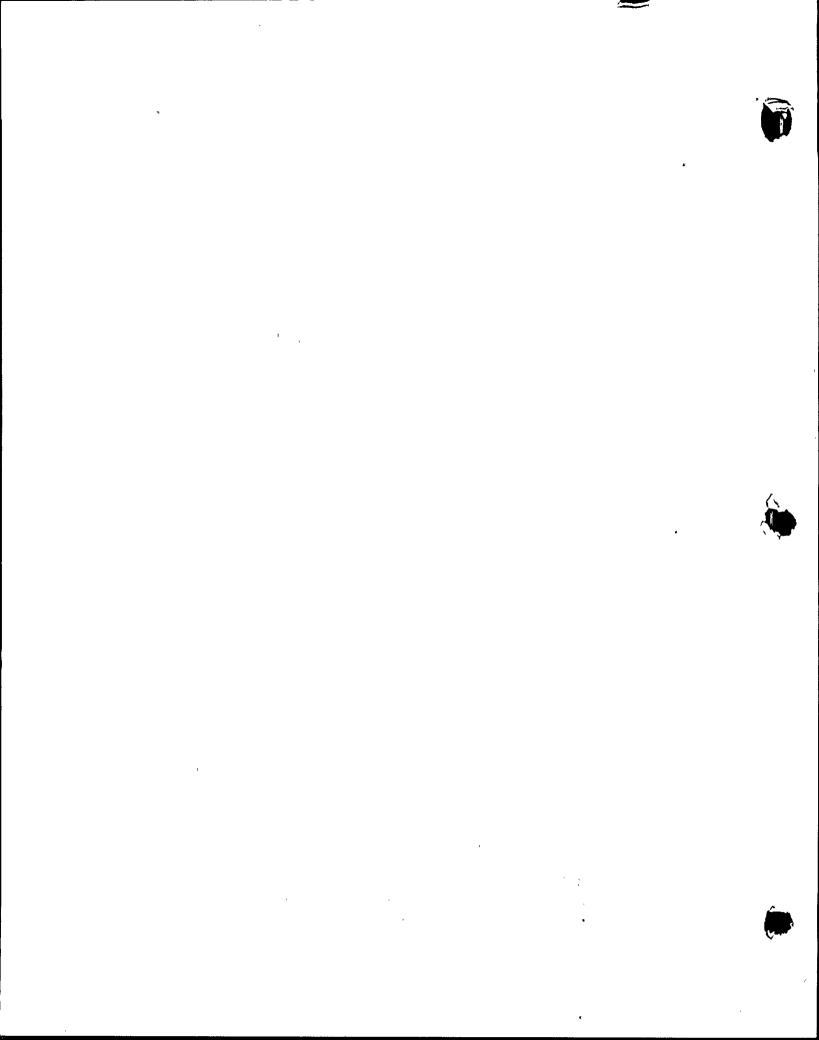
³ Valves installed during Cycle 5 outage

⁴ Valves installed during Cycle 5 outage, removed during Cycle 6 outage

⁵ Line changed from X-229D to X229N during Cycle 6 outage

Penetration	Valve No.	Description	Leak Rate	Date Tested
X-229J	3-FSV-76-63 ⁴	H ₂ O ₂ Sampling I.B. Isolation Valve	0.0769	06/03/84
•	3-FSV-76-64 ⁴	H ₂ O ₂ Sampling O.B. Isolation Valve	0.0000	06/03/84
	3-FSV-43-40 ⁶	Post-Accident Sampling Isolation Valve	0.1670	10/11/95
	3-FSV-43-42 ⁶	Post-Accident Sampling Isolation Valve	0.4630	10/11/95
X-229K ⁷	3-FSV-76-65 ³	H ₂ O ₂ Sampling I.B. Isolation Valve (Analyzer B, Torus Sample)	0.2060	06/02/84 . ·
	3-FSV-76-66 ³	H ₂ O ₂ Sampling O.B. Isolation Valve (Analyzer B, Torus Sample)	0.2321 0.0983	06/02/84 06/03/84
X-229N ⁵	3-FSV-76-55 ³	H ₂ O ₂ Sampling I.B. Isolation Valve (Analyzer A, Torus Sample)	0.1571	08/15/95
	3-FSV-76-56 ³	H₂O₂ Sampling O.B. Isolation Valve (Analyzer A, Torus Sample)	0.1546	08/15/95
X-229P ⁷	3-FSV-76-65 ³	H ₂ O ₂ Sampling I.B. Isolation Valve (Analyzer B, Torus Sample)	0.0001	08/14/95
	3-FSV-76-66 ³	H ₂ O ₂ Sampling O.B. Isolation Valve (Analyzer B, Torus Sample)	0.0487	08/14/95
X-231	3-FCV-64-32	Ventilation Exhaust Isolation Valve I.B. Flange	0.0041 0.0427 0.0000	09/06/84 09/08/84 10/09/95
X-231	3-FCV-64-34	Ventilation Exhaust Isolation Valve I.B. Flange	0.0000 0.1588	09/06/84 10/26/95

<sup>Valves installed during Cycle 5 outage
Valves installed during Cycle 5 outage, removed during Cycle 6 outage
Line changed from X-229D to X229N during Cycle 6 outage
Valves installed during Cycle 6 outage
Line changed from X-229K to X229P during Cycle 6 outage</sup>



<u>Penetration</u>	Valve No.	Description	Leak Rate	Date Tested
N/A	3-FSV-43-50 ¹	Post-Accident Sampling Isolation Valve (W)	0.0075	09/11/95
N/A	3-FSV-43-56 ¹	Post-Accident Sampling Isolation Valve (W)	0.0045	09/11/95
N/A	3-CKV-74-792 ²	RHR Loop 1 keep fill O.B. Isolation Valve (W)	0.0000	09/06/95
N/A	3-CKV-74-804 ²	RHR Loop 1 keep fill I.B. Isolation Valve (W)	0.0047	09/06/95
N/A		RHR Loop 2 keep fill O.B. Isolation Valve (W)	0.0030	09/17/95
N/A	3-CKV-74-803 ²	RHR Loop 2 keep fill I.B. Isolation Valve (W)	0.0038	09/17/95
N/A	3-CKV-75-606 ²	CS Loop 1 keep fill I.B. Isolation Valve (W)	0.0000	05/18/95
N/A	3-CKV-75-610 ²	CS Loop 2 keep fill O.B. Isolation Valve (W)	0.0084	05/18/95
N/A	3-CKV-75-607 ²	CS Loop 1 keep fill O.B. Isolation Valve (W)	0.0059	07/11/95
N/A .	3-CKV-75-609 ²	CS Loop 2 keep fill I.B. Isolation Valve (W)	0.0047	07/11/95

¹ Valves installed during Cycle 6 outage2 Valves added to to test program during Cycle 6 outage

