CAROLINA POWER & LIGHT COMPANY

SHEARON HARRIS NUCLEAR POWER PLANT

PLANT OPERATING MANUAL

VOLUME 6

PART 7

PROCEDURE TYPE:

Inservice Inspection Program (ISI)

NUMBER:

ISI-203

TITLE:

ASME Section XI Pump and Valve Program Plan

REVISION 6

EFFECTIVE APR 0 5 1989 **APPROVED:** 3/27/87 Signature Date

TITLE:

890505

400

89051601 PDR ADC

SUDDORT ECH MANAGER

MAR 2 9 1989 HNP DOCUMENT SERVICES

· ·

Page 1 of 244

0S2

Table of Contents

Sect	ion			Page
1.0	PIRP	OSE		5
2.0	DEEE	RENCES		8
3 0	DEGD	ONSTRUCT	FQ	8
<i>x</i> 0	DEEL	NTTTONS / AR	BERTATIONS	ă
5 0	DECI	CDIDE	u u	9
7.0	E 1	Dofinitio		3
	2.1	Conceral D	us slief for Durne	
	J.2 5 3	General A	eller for Fumps	11
	J.J	General A	Burn Mart Dramer	<u>, 12</u>
	2.4	Inservice	The last rogram	13
		5.4.1	Introduction	13
		5.4.2	Pump 1ST Program Plan Concept	13
	•	2.4.3	Code Interpretation	15
		5.4.4		12
		5.4.5	Pump Table Nomenclature	15
		5.4.6	Pump Test Table Notes	16
		5.4.7	Pump Test Table	18
		5.4.8	Pump Relief Request	19
	5.5	Inservice	Valve Test Program	26
		5.5.1	Introduction	26
		5.5.2	Valve IST Program Plan Concept	26
	v	5.5.3	Code Interpretation	26
		5.5.4	Valve Table Nomenclature	34
		5.5.5	Valve Test Table Format	37 ്
	5.6	Valve Tes	t Tables and Relief Request	39
		5.6.1`	Containment HVAC	40
		5.6.2	Reactor Aux. Bldg. HVAC	46
		5.6.3	Control Room HVAC	49
		5.6.4	Fuel Bldg. HVAC	54
	•	5.6.5	Switchgear and Protection Room HVAC	57
		5.6.6	Main Steam	60.
		5.6.7	Feedwater	72
		5.6.8	Auxiliary Feedwater	77
		5.6.9	Condensate	93
		5.6.10	Service Water	98
		5.6.11	Containment Spray	109
		5.6.12	Steam Generator Blowdown	116
		5.6.13	Process Sampling	119 /
		5.6.14	D.G. Fuel Oil Transfer	124
		5.6.15	Rad. Monitor and H2 Analyzer	127
		5.6.16	D.G. Starting Air	131
		5.6.17	Demineralized Water.	134
		5.6.18	CTMT. Sump Drains	138
		5.6.19	Service Air	141
		5.6.20	Instrument Air	145
٠		5.6.21	Fuel Pool Cooling	152
		5.6.22	Emergency Screen Wash	156
		5.6.23	Fire Protection	159
		5.6.24	Essential Chilled Water	163
		5.6.25	Reactor Coolant •	171
		5.6.26	CVCS	179

ISI-203 Rev. 6

Page 2 of 244

0\$2

J

Í

Table of Contents (Continued)

Section Page Safety Injection 202 5.6.27 5.6.28 CTMT. Waste Processing 219 Component Cooling Water 5.6.29 222 Residual Heat Removal 5.6.30 236 5.6.31 CTMT. Integrated Leakage Detection 241 6.0 DIAGRAMS/ATTACHMENTS 244

Page³ of 244

0S2



List of Effective Pages

1 - 244

Page

052

Revision

6

.

.

,

•

•

.

· · · ·

.

· ·

•

Page 4 of 244

ISI-203 Rev. 6 -

1.0 PURPOSE

OS2

1.1 Introduction

This document presents the Program Plan for Inservice Testing (IST) of pumps and valves at the Shearon Harris Nuclear Power Plant (SHNPP) in compliance with the requirements of 10CFR50.55a. 10CFR50.55a(g) specified that the Section XI Pump and Valve Inservice Testing Program shall be initiated at the start of commercial operation of the facility. Further, the Program Plan must conform to the requirements of the Code edition and addenda in effect no more than twelve months prior to the date of issuance of the operating license. This program plan has been prepared to the requirements of the ASME Boiler and Pressure Vessel Code, Section XI, Subsections IWP and IWV, 1983 Edition through the Summer 1983 Addenda.

This plan will then be in effect for the first 120 month interval. It will be updated for each subsequent 120 month interval to conform to the Code Edition and Addenda in effect no more than twelve months prior to the start of the interval.

1.2 Basis

In addition to the reference Code edition and addenda, these Program Plans have been prepared in compliance with the NRC guidance contained in "Guidance for Preparing Pump and Valve Testing Program Descriptions and Associated Relief Requests Pursuant to 10CFR50.55a(g)" and the November 1981 Draft Regulatory Guide "Identification of Valves for Inclusion in Inservice Testing Programs." These three documents provide the basis for selection of components, test requirements, relief requests, and format.

All information except individual valve maximum stroke times, requested by the reference documents has been included in this Program Plan. Maximum stroke times for valves have been determined from the pre-operational test program, Technical Specifications, system operational considerations and manufacturers information. Since individual valve maximum stroke times may require revision after modification, repair or maintenance, SHNPP has elected to exclude them from the Program Plan submittal. Maximum stroke times will be established prior to the end of the first refueling outage and will be maintained in the appropriate test procedures.

1.3 General Program Plan Concept

The Program Plan specifies Section XI testing requirements for components providing, either by action or position, a safetyrelated function. By definition, a safety-related function is one that is needed to:

1.3	General	Program	Plan	Concept	(Continued)	
-----	---------	---------	------	---------	-------------	--

- 1. Mitigate the consequences of an accident
- 2. Shut down the reactor to the cold shutdown condition
- 3. Maintain the reactor in a safe shutdown condition

Plant Technical Specifications, special manufacturer's tests, system operating conditions, etc., may dictate additional components which should be included in the overall plant testing program, but whose functions fall outside the criteria above, and are not addressed by this Program Plan.

Section XI requires quarterly testing of all components unless it is impractical to do so. This program specifies quarterly testing of pumps and valves unless it has been determined that such testing would:

- 1. Be impractical due to system or component design
- 2. Render a safety-related system inoperable
- 3. Cause a reactor scram or turbine trip
- 4. Require significant deviations from normal operations
- 5. Require entry into inaccessible plant areas
- 6. Increase the possibility of an inter-system LOCA

Excluded from exercising during normal operations are all valves which, if exercised, could place the plant in an unsafe condition. Cases where valve exercising could compromise plant safety include:

- 1. All values whose failure in a non-conservative position during the cycling test would cause a loss of system function will not be exercised. Values in this category would typically include all non-redundant values in lines such as single discharge line from the refueling water storage tank, or accumulator discharge lines. Other values may fall into this category under certain system configurations or plant operating modes. For example, when one train of a redundant system such as ECCS is inoperable, non-redundant values in the remaining train should not be cycled since their failure would cause a loss of total system function.
- 2. All valves, whose failure to close during a cycling test would result in a loss of containment integrity will not be tested. Valves in this category would typically include all valves in containment penetrations where the redundant valve is open and inoperable.

İSI-203 Rev. 6

Page 6 of 244

0S2

· · · · · · · ·

۰ ۲

.

.

1.3 General Program Plan Concept (Continued)

3. All valves, which when cycled, could subject a system to pressures in excess of their design pressures. It is assumed for purpose of a cycling test, that one or more of the upstream check valves has failed unless positive methods are available for determining the pressure or lack thereof on the high pressure side of the valve to be cycled. Valves in this category would typically include the isolation valves of the residual heat removal/shutdown cooling system and, in some cases certian ECCS valves.

Each component excluded from quarterly testing has been analyzed to determine when appropriate testing may be performed. If exercising of a valve is not practical during plant operation, the Code allows part-stroke exercising during normal plant operation, and full-stroke exercising at cold shutdown.

Since the Code allows testing at cold shutdown, this program does not request relief for those valves for which testing is delayed until cold shutdown.

The Valve IST Program Plan does provide a justification for the delay of testing until cold shutdown. These justifications are prepared in a format similar to relief requests, and are included following the Valve Test Tables for each system.

Where it has been determined that testing is not practical during plant operation, or at cold shutdown, a specific relief request has been prepared. Each specific relief request provides justification for not performing the Code required testing, and provides appropriate alternative testing.

In addition to specific relief requests, general relief requests which address specific Code requirements found to be impractical for this site have been prepared. Because of the general nature of these relief requests, and the number of components involved, they are presented in separate sections and are not repeated in the individual system sections.

Cold Shutdown and Refueling as used in this test program includes mode changes going into and coming out of plant Technical Specification defined modes 5 and 6. Because of unique system operating conditions, it will be necessary to perform some tests during mode change. For example, a steam driven turbine scheduled for testing at cold shutdown can not be tested during mode 5 when there is no steam available. In this case, testing will be performed during a mode change when sufficient steam is available.

1.4 Organization

The Pump and Valve Inservice Testing Program Plan is organized into three independent sections, each of which can be removed from the Program Plan for review. Sections 5.1 - 5.3 present the general program commitment basis, the conceptual framework used in developing the Program Plans, and general relief requests for Code requirements found to be impractical for this site. Section 5.4 deals specifically with the Pump Test Program, and Sections 5.5 -5.6 deal specifically with the Valve Test Program.

Sections 5.4 - 5.6 are formatted in a manner to aid review. Each section summarizes the basis and concepts used to formulate the Pump and Valve Testing Program. Pump testing requirements are summarized in a single Pump Test Table attached to Section 5.4. Valve test requirements are summarized in Valve Test Tables attached to Section 5.6. The Valve Test Tables are arranged into separate attachments for each system. Where quarterly testing has been found to be impractical, either a justification for delay of test to cold shutdown, or a relief request, is provided following the appropriate Pump or Valve Test Tables. In those cases where additional discussion of the test requirements for a component is needed, the remarks column of the Test Table contains a Note Number. These Notes may be found following the Valve Test Tables for each system.

2.0 REFERENCES

- 1. ASME Boiler and Pressure Vessel Code, Section XI, 1983 Edition through Summer 1983 addenda.
- 2. Code of Federal Regulations, Title 10, Part 50.55a(g).
- 3. SHNPP Technical Specifications, Section 4.0.5.

3.0 RESPONSIBILITIES

ISI-203 Rev. 6

3.1 <u>Technical Support Unit</u>

The Technical Support Unit is responsible for overall administration of the program including:

- 1. Determination of the program plan scope.
- 2. Revision of the program plan as necessary based on plant design changes.
- 3. Preparation of reports as necessary.
- 4. Requesting relief from testing for components that cannot be tested during plant operation.

3.1 <u>Technical Support Unit</u> (Continued)

- 5. Determining acceptance criteria.
- 6. Trending and review of test results.
- 3.2 Operations Unit
 - 1. Preparation and performance of surveillance test procedures that implement the program requirements.
 - 2. Evaluation of test results based on acceptance criteria determined by the Technical Support Unit.

3.3 Administrative Section

1. Maintaining test records consistent with the requirements of reference 2.1.

4.0 DEFINITIONS/ABBREVIATIONS

- 1. ASME American Society of Mechnical Engineers.
- 2. CFR Code of Federal Regulations.

5.0 PROCEDURE

The following is a detailed description of the ASME Section XI pump and valve program as implemented at SHNPP. The format is consistent with NRC recommendations.

5.1 Definitions

The terms below, when used in the Inservice Testing Program Plan, are defined as follows:

Quarterly:

Cold Shutdown:

An interval of 92 days for testing components which can be tested during normal plant operation.

Testing delayed until cold shutdown will commence as soon as cold shutdown condition is achieved, but no later than 48 hours after achieving cold shutdown. Testing will continue until all tests are complete, or the plant is ready to return to power. Completion of testing is not a prerequisite to return to power, and any testing not completed at one cold shutdown will be performed during subsequent cold shutdowns before the refueling outage. No cold shutdown testing will be performed on any components tested less than 92 days prior

ISI-203 Rev. 6

Page 9 of 244

5.1 <u>Definitions</u> (Continued)

to achieving cold shutdown. The 48 hour interval will not hold for planned cold shutdowns where all required testing will be completed.

Testing delayed to refueling will be , performed during the normal scheduled refueling shutdown before returning to power operation.

> Category C safety and relief valves (IWV-3511), Category D explosive actuated valves (IWV-3610) and Category D rupture disks (IWV-3620) are periodically tested as defined in the appropriate Code Sections.

Any valve which acts as an isolation boundary between the high pressure Reactor Coolant System and a system having a lower operating or design pressure.

ion: Any valve which performs a containment isolation function and is included in the Appendix J, Type C, Local leak Rate Test program.

> Any value which is required to change position to accomplish its safety-related function.

> Any value which is not required to change position to accomplish a specific function and for which the Code does not require operability testing.

Refueling:

Period:

Pressure Isolation:

Containment Isolation:

Active:

Passive:



5.2 General Relief Requests for Pumps

This section requests relief from specific requirements of Section XI found to be impractical for this site. Since they are general in nature, and pertain to a number of components, this section requests general relief as presented below.

General Relief Request:

PG-1

Pumps:

All centrifugal pumps

IWP-3100-2).

Differential pressure alert and required action ranges (Table

Test Requirements:

Basis for Relief:

Alternate Testing:

Pump overpressure is an indicator of pump clogging or improper maintenance and as such is an important test parameter to measure. However, small positive increases in measured differential pressure across a centrifugal pump are most likely not a significant indicator of pump degradation. Adherence to the Code specified alert and required action ranges could result in unnecessary pump testing and repair. In order to preclude unnecessary testing and repair, pump differential pressure will be measured and expanded alert and required action ranges used.

In lieu of the Code specified values, the high side acceptance range will be 1.05 times the reference pump differential pressure. The high side alert and required action ranges will be 1.05 to 1.07 and > 1.07 times the reference pump differential pressure respectively.



ISI-203 Rev. 6

Page 11 of 244

5.3 General Relief Requests for Valves

This section requests relief from specific requirements of Section XI found to be impractical for this site. Since they are general in nature, and pertain to a number of components, this section requests general relief as presented below.

General Relief Request:

VG-1

A, B

seconds or less.

Component:

Category:

Code Requirements:

Basis for Relief:

Alternate Testing:

IWV-3417 requires corrective action if the measured stroke time for a valve which normally strokes in ten seconds or less increases by fifty percent from the last measured stroke time. IWV-3413 allows measurement to the nearest second for stroke times of ten seconds or less.

Rapid actuating power operated valves with stroke times of 2

For rapid actuating power operated valves the application of the above criteria could result in requiring corrective action when the valves are functioning normally. These valves are generally small air and solenoid operated valves which because of their size and actuator types stroke very quickly. Operating history on this type of valve indicates that they generally either operate immediately or fail to operate in a reasonable length of time. The intent of the referenced . Code sections is to track valve stroke time as a means of detecting valve degradation. This type of valve does not lend itself to this tracking technique.

A maximum stroke time of two seconds will be specified for each rapid actuating valve. If the measured valve stroke time is two seconds or less it will be considered as acceptable and no corrective action will be required. If the measured

Page 12 of 244



.

.

c

5.3 General Relief Requests for Valves (continued)

valve stroke time exceeds two seconds it will be considered inoperable and appropriate corrective action will be taken.

5.4 Inservice Pump Test Program

5.4.1 Introduction

This section presents the Program Plan for Inservice Testing of safety-related Pumps at Unit 1 of the Shearon Harris Nuclear Power Plant, in compliance with the requirements of 10CFR50.55a. This Program Plan has been prepared to the requirements of the ASME Boiler and Pressure Vessel Code, Section XI, Subsection IWP, 1983 Edition through the Summer 1983 Addenda.

5.4.2 Pump IST Program Plan Concept

The Pump Program Plan specifies Section XI testing requirements for all ASME Class 1, 2 and 3 pumps provided with an emergency power source, and which are required for safety-related system operation. Test requirements determined to be impractical for a large number of pumps have been addressed in Section I under General Relief Requests for Pumps. In addition to those General Relief Requests, this section includes requests for relief from Code requirements found to be impractical for specific pumps. Each relief request provides justification for deviation from the Section XI specified test, and proposes appropriate alternate testing.

5.4.3 Code Interpretation

A number of items in Subsection IWP of the Code are subject to interpretation. The interpretations of a number of general items encountered in preparing the Pump Test Program Plan are provided below.

Pump Test Data within the Required Action Range (Table IWP-3100-2)

When test results show deviations greater than allowed by Table IWP-3100-2, the instruments involved may be checked for accuracy and the test rerun. If the second test provides results falling within the required action range, appropriate corrective action must be initiated. This corrective action may be either replacement, repair, or analysis to demonstrate that the condition does not impair pump operability, and that the pump will still fulfill its safety-related function. If the analysis verifies that the pump is operable, a new set of reference values will be established. If the instrumentation is checked, and the test rerun with results in the acceptable range, the first set of test results will be discarded, and the second set retained.



ISI-203 Rev. 6

Analysis of Data within 96 Hours (IWP-3220)

All Code required test parameters will be reviewed within 96 hours after completion of test to verify that they do not fall within the required action range. Those that fall within the required action range will be processed as described above. Those that do not fall within the required action range will be analyzed within four working days after completion of test. This fulfills the intent of the Code to require immediate action on pumps falling within the required action range and allows orderly reduction of data taken on weekends or holidays, when sufficient staff may not be available to perform the Code required analysis.

Scope of Tests (IWP-3300)

Section IWP-3300 requires that each inservice test measure and observe all the quantities in Table IWP-3100-1 except bearing temperature, which shall be measured at least once a year. The Code assumes that each pump installation can be instrumented to obtain the specified quantities. In some installations it is not possible to provide instrumentation to obtain Code specified quantities. For example, submerged pumps cannot be instrumented to measure inlet pressure and observation of proper lubricant level or pressure is not possible for a greased bearing pump. In some cases it is possible to substitute an alternate method. For example, inlet pressure for a submerged pump can be calculated by measuring the head of water relative to the pump suction. This program does not request relief from Section XI testing for those quantities which cannot be obtained due to pump design or installation. Explanatory notes have been used in the Pump Test Table when Section XI testing is not possible due to pump design or installation.

ISI-203 Rev. 6

5.4.4 Pump List

Pumps' required for safety-related operation for this site are as follows:

SYSTEM	DWG. NO. R	EV.NO.	NO. of PUMPS
Auxiliary Feedwater	S-0545	16	3
Emergency Service Water	S-0547	14	2
S. W. Booster	S-0547	14 -	2
Containment Spray	S-0550	9	2
D.G. Fuel Oil Transfer	S-0563 .	5	2
Emerg. S.W. Intake Screen Wash	S-0808	6	2
Chilled Condenser Water	S-0998 SO2 S-0999 SO2	6 6	2
S.I. Charging	S-1305	9	3
Boric Acid Transfer	s-1307	4	2
Component Cooling Water	S-1319	7	3
Residual Heat Removal	s-1324	7	2
Spent Fuel Pool Cooling	S-0805	5	2

5.4.5 Pump Table Nomenclature

The following abbreviations have been used in the Pump Test Table:

N	Ħ	Rotative Speed
Pi	-	Inlet Pressure (Before and after pump start)
DP	₽.	Differential Pressure Across Pump
Q£	a,	Flow Rate
V.	Ħ	Vibration Amplitude
ть	=	Bearing Temperature
1	=	Quarterly



0S2

5.4.5 Pump Table Nomenclature (Continued)

2

3

- = Cold Shutdown
- · = Refueling
- X = Measurement/Observation per IWP
- L = Lubricant Level or Pressure
- PR = Relief Request

5.4.6 Pump Test Table Notes

In the Pump Test Table, the test parameters to be measured or observed, and the test frequency are identified. Footnotes 1 through 9 refer to amplifications, deviations, and exceptions to the Code requirements and are further discussed below:

- 1. Pump with constant speed drive, speed is not measured since test will be performed at nominal motor nameplate speed as required by Section XI, IWP-3100.
- 2. Inlet pressure to be calculated from the inlet liquid level. The liquid level will be measured while establishing and verifying Reference Data sets, and used as information during subsequent test analysis.
- 3. Bearing temperature measurement not required (IWP-4310) since bearings are in the pumped fluid flow path.
- 4. Bearing temperatures to be measured once a year as stipulated by Section XI, IWP-3300.
- 5. Lubricant level or pressure not observed because of bearing lubrication désign.
- 6. Any one of three component cooling or three charging pumps is an installed spare. One pump is normally running, the second is aligned as an automatic backup to the operating pump and the third pump is electrically disconnected. In the event of failure of the operating pump, the second pump automatically starts and the installed spare is electrically connected and valved in as the reserve pump. The normally operating and reserve pump will be tested. The installed spare is required to be-tested only when it is connected to the system.
- 7. Quarterly testing of the motor driven pumps is performed using pump recirculation flow through a small diameter recirculation line. A full flow test will be performed on the way to cold shutdown.

ISI-203 Rev. 6

Page 16 of 244

5.4.6 <u>Pump Test Table Notes</u> (Continued)

- 8. Quarterly testing of the steam driven pump is performed using pump recirculation flow through a small diameter recirculation line. A full flow test will be performed on the way to cold shutdown.
- 9. Pump and motor are an integral unit with no bearings in the pump. Motor upper bearing will be treated as if it were a pump bearing. Motor bearing has installed vibration monitoring, temperature measurment and are water lubricated.



ISI-203 Rev. 6

5.4.7

PUMP TEST TABLE

- PUMP LIST					MEASURED PARAMETERS							
System	Pump 1.D.	P & 1.D.	Coord.	Class	Test Freq.	N	PI	DP	Qf	,v	Ть (4)	L
AUXILIARY FEEDWATER	1A-SA 1B-SB 1X-SAB	S-0545	J-7 J-8 J-9	3 3 3	1,2 (7) 1,2 (7) 1,2 (8)	(1) (1) X	× × ×	x x x	X X X	X X X	PR-1 PR-1 PR-1	X · X X
EMERGENCY SERVICE WATER	1A-SA 1B-SB	S-0547	C-3 C-3	3 3	, 1 1	(1) (1)	(2) X	X PR-8 X PR-8	X PR-8 X PR-8	××	(3) (3)	(5) (5)
D.G. FUEL OIL TRANSFER	IÀ-SA 18-SB	S-0563	F-2 F-7	3	1 1	(1) (1)	x x	x x	PR-2 PR-2	×.	PR-3 PR-3	X X
EMERG. S.W. INTAKE SCREEN WASH	1A-SA 1B-SB	S-0808	C-12 C-15	3 3	1 1	(1) (1)	x x	x x	x x	× ×	PR7 PR7	× ×
CHILLED CONDENSER WATER	1A-SA 18-SB -	S-0998 SO S-0999 SO	C-9 C-9	3 3	1 1	(1) (1)	x x	x x	x x	× ×	PR-7 PR-7	x x
S.I. CHARGING	1A-SA 18-SB 1C-SAB	S-1305	H-9 J-9 K-9	2 2 2	1 (6) 1 (6) 1 (6)	(1) (1) (1)	× × ×	x x x	x x x	x x x	PR-7 PR-7 PR-7	x x x
BORIC ACID TRANSFER	1A-SA 18-SB	S-1307	D-8 G-8	2	1,2 PR-7 1,2 PR-7	(1) (1)	x x	.x x	PR-5 PR-5	x x	PR-6 PR-6	PR-6 PR-6
COMPONENT COOLING WATER	1A-SA 1B-SB 1C-SAB	S-1319	F-7 L-7 I-7	3 3 3	1 (6) 1 (6) 1 (6)	(1) (1) (1)	× × ×	X PR-8 X PR-8 X PR-8	X PR-8 X PR-8 X PR-8	× × ×	PR-7 PR-7 PR-7	x x x
RESIDUAL HEAT REMOVAL	1A-SA 1B-SB	S-1324	L-11 1-11	2 2	1 1	(1) (1)	× ×	x x	x	(9) (9)	(9) (9)	(9) (9)
SPENT FUEL POOL COOLING	1A-SA 1B-SB	S-0805	H-10 K-10	3 3	1	(1) (1) (1)	× ×	× ×	x x	× ×	PR-7 PR-7	(5) (5)
CONTAINMENT SPRAY	1A-SA 18-SB	S-550	F-8 K-8	2 2	1	(1) (1)	× ×	× ×	x x	(9) (9)	(9) (9)	(9) (9) -
S.W. BOOSTER	1A-SA 18-SB	S-0547	H-6 H-15	3 3	1	(i) (i)	× ×	x x	X X	× ×	(3) (3)	(5) (5)

. ISI-203 Rev. 6 Page 18 of 244

Pump Relief Request

PUMP RELIEF REQUEST

<u>PR-1</u>

3

System:

1A-SA, 1B-SB, 1X-SAB

Auxiliary Feedwater

Pump:

Class:

Function:

Test Requirements:

Basis for Relief:

Alternate Testing:

Provide Auxiliary Feedwater to the Steam Generators on loss of Main Feedwater.

Measure Bearing Temperature (IWP-4300).

Quarterly pump testing is performed using a pump recirculation line back to the CST. In this mode of operation the temperature of the pumped fluid is constantly increasing and operation is limited to a maximum of one hour. IWP-3500(b) requires the pumps be operated until bearing temperature stability is achieved, but for no less than thirty minutes. Since the pumped fluid temperature is constantly increasing, bearing temperature will not reach stability in one hour. In addition, good operating procedure will limit operation of the pumps in this mode to as short a time as possible to preclude pump degradation. When the pumps are full flow tested at cold shutdown or refueling the length of operation is dictated by plant operating conditions and it can not be guaranteed that plant conditions will allow operation of each pump until bearing temperature stabilizes without significant impact on normal plant operations.

Pump differential pressure, flow and vibration measurments will be used to evaluate pump performance.

5.4.8

ISI-203 Rev. 6

Page 19 of 244

<u>PR-2</u>

System:

Pump:

Diesel Generator Fuel Oil Transfer

Measure pump flow rates to the requirements of Table IWP-3100-2.

tanks to the Day Tanks.

pump operation.

IA-SA, IB-SA

3

Class:

Function:

Test Requirements:

Basis for Relief:

Alternate Testing:

with the allowable ranges of test quantities of Table IWP-3100-2. Flow rate will be calculated from observed change in Day Tank level during

Transfer Diesel Fuel Oil from the Storage

There are no system design provisions for direct flow measurements. Flow rate will be calculated from measured change in Day Tank level during pump operation. This method is not accurate enough to comply

Page 20 of 244

P

0S2

PUMP RELIEF REQUEST

PR-3

Diesel Fuel Oil Transfer

tank to the day tank.

System:

Pump:

1A-SA, 1B-SB

stabalizes.

3

Class:

Function:

Test Requirements:

Basis for Relief:

Alternative Testing:

Per IWP-3500(b), when the measurement of bearing temperature is required, each pump shall be run for a minimum of thirty minutes until bearing temperature

Transfer diesel fuel oil from the storage

Diesel Fuel Oil Pump running time is dictated by interlock circuitry and administrative limits corresponding to allowable Day Tank levels. The interlocks, which control automatic transfer pump operation, limit operation of the pumps below minimun allowable or above maximum allowable tank levels. Operation of the pumps with tank levels above maximum allowable is precluded by administrative controls and alarms. The time required to fill the tank from minimum level to maximum level is less than thirty minutes.

Bearing condition will be evaluated by pump bearing vibration measurments.

0S2

PUMP RELIEF REQUEST

<u>PR-5</u>

Boric Acid Transfer

System: .

Pump:

Class:

1A-SA, 1B-SB

2

Function:

Test Requirements:

Basis for Relief:

Alternate Testing:

Transfer of concentrated Boric Acid from the Boric Acid Tank to the CVCS.

Quarterly measurement of pump flow rate.

There are no system design provisions for measurement of flow rate in the flow path used for quarterly pump testing. To utilize the system flow meter would require a test flow path which would transfer highly concentrated Boric Acid form the Boric Acid Tank to the CVCS. The addition of large amounts of concentrated Boric Acid during cold shutdown would have a significant adverse effect on CVCS operation. And would require the removel and processing of the added Boron prior to returning the plant to operation. This procedure would have a significant impact on systems operation and could cause delay in returning the plant to operation.

The pumps will be run quarterly using the pump minimum flow line. During quarterly testing both inlet and differential pressure will be measured. Flow will be measured through the emergency boration path when borating on the way to cold shutdown.





ø

,

,

,

· · · · ·

.

.

1

PUMP RELIEF REQUEST

PR-6

Boric Acid Transfer

Transfer of concentrated Boric Acid from

These pumps are Model GVHS-10K Pumps made by Chempump Division of the Crane Co. This type of pump has no bearings in the pump and is a integral unit with the motor. The pump bolts directly onto the integral motor end housing flange, such that the motor bearings are completely inclosed. Motor bearings are lubricated and cooled by diverting a portion of pump flow through the motor and back to the

lubrication are associated with the motor would not provide any information about

the Boric Acid Tank to the CVCS.

observe lubrication level.

pump suction. All cooling and

Measure pump bearing temperature and

System:

Pump:

0S2

1A-SA, 1B-SB

2

Class:

Function:

Test Requirements:

Basis for Relief:

Alternate Testing:

None

the pump.

ISI-203 Rev. 6

Page 23 of 244



<u>PR-7</u>

System:

Pump:

Class:

Function:

Test Requirements:

Basis for Relief:

Alternate Testing:

Chilled Condenser Water, S.I. Charging, Component Cooling Water and Spent Fuel Pool Cooling, ESW Intake Screen Wash.

1A-SA, 1B-SB (Chilled Cond. Water); 1A-SA, 1B-SB, 1C-SAB (S.I. Charging); 1A-SA, 1B-SB, 1C-SAB (C.C.W.); 1A-SA, 1B- SB (SFPC); 1A-SA, 1B-SB (ESW Intake Screen Wash)

2,3

HVAC Chilled Water, Safety Injection and Cooling Water for safety-related equipment.

Measure bearing temperature (IWP-4300).

These pumps have no installed instrumentation to measure bearing temperature. Measurement of temperature of the pump bearing housing would not be indicative of actual bearing temperature because of temperature gradients caused by operation of space coolers, pump. location, pumped fluid, etc. The once a year measurement will not provide significant information about pump condition. The long pump running time required to achieve temperature stability could result in unnecessary wear on the pumps and result in increased pump maintenance and repair. Deletion of this measurement will not have significant affect on the pump monitoring program, since other required test parameters are being measured.

Pump differential pressure, flow and vibration will be used to monitor pump performance.

ISI-203 Rev. 6

Page 24 of 244

PUMP RELIEF REQUEST

<u>PR-8</u>

Cooling Water

1C-SAB (C.C.W.)

3

System:

Pump:

Class:

Function:

•Test Requirements:

Basis for Relief:

Alternate Testing:

Provide cooling water to safety-related equipment.

Emergency Service Water; Component

1A-SA, 1B-SB (E.S.W.); 1A-SA, 1B-SB,

Article IWP-3100 requires that pumps be tested in a fixed resistance system or that the resistance of the system varied until either the measured differential pressure or flow rate equals the corresponding value.

These systems do not have an installed pump test line and system operating conditions will not allow adjusting system resistance without significant impact on plant operations. These are. variable resistance systems that experience a wide swing in loads and configuration. Depending on plant operating conditions and climatic conditions the cooling requirements can range from minimum cooling loads to 100 percent and many of the loads are automatically placed in operation in response to local temperature requirements. Because of these normal operating requirements it is not possible to specify a particular flow path that can be repeated for each pump test.

Pump testing will be performed with the system in the as-found operating configuration and the test results compared with a curve of reference values which establishes the relationship between flow and differential pressure in a band around the design point.

ISI-203 Rev. 6

Page 25 of 244

5.5 Inservice Valve Test Program

-5.5.1 Introduction

This section presents the Program Plan for Inservice Testing of Valves at the Shearon Harris Nuclear Power Plant, in compliance with the requirement of 10CFR50.55a. This Program Plan has been prepared to the requirements of the ASME Boiler and Pressure Vessel Code, Section XI, Subsection IWV, 1983 Edition through the Summer 1983 Addenda.

5.5.2 Valve IST Program Plan Concept

The Valve Test Program Plan was developed to verify the operability of safety-related systems. The valves addressed are those whose operability is essential to safety-related system operation. Section XI valve testing is then specified for each of these valves to verify individual valve operability. The Program Plan specifies either Section XI or alternate testing, as appropriate, for all valves which perform a safety-related function.

Valves are selected for inclusion in the test program based on a review of all plant systems. This review identifies those systems performing safety-related functions. Each safety-related system is then analyzed to determine which valves are essential to the safety-related operation of the system. These valves are investigated to determine whether Section XI testing can be performed during normal operation. Those valves for which quarterly testing is determined to be inappropriate are analyzed further to determine if Code allowed testing at cold shutdown is possible. If so, a justification for delay of test to cold shutdown is provided following the appropriate Valve Test Tables. Relief requests describing appropriate alternative testing, and justifying exclusion from Section XI testing, have been prepared for valves which cannot be tested quarterly or during cold shutdown, and are provided following the appropriate Valve Test Tables.

5.5.3 Code Interpretation

A number of items in Subsection IWV of the Code are subject to interpretation. The interpretations of a number of general items encountered in preparing the Valve Test Program Plan are provided below.

ISI-203 Rev. 6



•

4

•

Relief Valves:

The Code requires testing of pressure relief values in accordance with ASME/ANSI OM-1 1981. The relief values designated for test are only those which perform a system pressure relief function. Thermal relief values, whose only function is to protect components or piping from thermal expansion are not included in the IST program. Where a relief value performs both a system and a thermal relief function it has been included as testable. A number of thermal relief values have been included in the value test tables to comply with a North Carolina State Requirement for testing of relief values which protect pressure vessels. SHNPP has elected to include these thermal relief values in their Section XI test program. All relief values included to comply with North Carolina State Regulations are so noted in the value test tables.

Passive Valves:

The reference Code excludes valves used only for operating convenience and/or maintenance from testing. Also, the Code defines passive valves but specifies no operability test requirements. This program defines as passive power operated valves which do not have to change position, but whose position has a direct bearing on safety-related system operation. Manual flow path maintenance and system alignment valves are excluded. Manual passive Containment Isolation and pressure isolation valves have been included for leak testing only.

System Test Valves:

Power operated values included in a system to align the system for testing are included for Section XI testing if their position is critical to safety-related system operation. The system analysis postulates that the system is in a test mode when the initiation signal occurs. All values, including those used only for testing, which must respond to the initiation signal, are included in the test program.

Pressure and Flow Control Valves:

The reference Code excludes valves which perform pressure or flow control functions. This program excludes them unless they also perform a system safety-related response function such as automatic closure on system initiation. The program addresses these valves by specifying testing of the safety-related function, and excluding the normal pressure or flow control functions. These valves will be stroke timed if they are equipped with valve test provisions or if a repeatable exercising method is possible.



Automatic Power Operated Valves:

Power operated valves which receive an automatic signal on system initiation are included in the program.

Remote Power Operated Valves:

The program includes power operated values activated by remote switches if they are required to change position to align a system for safety-related operation, terminate safety-related system operation, or provide containment isolation capability during the long term post-LOCA operating mode.

Normal vs. Safety-Related System Operation:

Valves in systems which have both normal and safety-related operating modes are included in the program only if they perform a safety-related function. Valves which provide normal system operation control and whose position has no effect on safety-related operation are excluded from the program.

Dual Function Valves:

Valves which provide more than one function are tested for their safety-related function only. Valves with multiple safety-related functions are tested for each function.

Simple Check Valves:

This Program Plan considers any check valve to be a simple check valve if it has no means of changing position other than by reversal of fluid flow direction. Simple check valves are tested to verify operability in the safety-related flow direction. Normally closed simple check valves which must open are tested to verify full opening with forward flow. Normally open simple checks which must close on cessation of flow are tested to verify closure on cessation of forward flow. Normally closed simple check valves which remain closed on system initiation are tested to verify absence of reverse flow. Normally open simple check valves which are required to remain open, are tested to verify full flow in the forward direction. Simple check valves which are required to cycle open and closed are tested to verify full opening with forward flow and closure on loss of forward flow.

Manual Stop Check Valves:

Manual stop check valves are tested to verify operability in the safety-related flow direction. If the manual operator is withdrawn, the valve operates as a simple check in the forward flow direction and is tested as a simple check. Reverse flow closure is verified as a simple check, if possible, or by use of the manual operator. ISI-203 Rev. 6





Page 28 of 244

Testable Check Valves:

Check values equipped with manual exercisers will be tested as a simple check, or by exercising using the manual exercising device. Check values equipped with a power operator installed for the sole purpose of exercising the value for operability will be tested as a simple check, or by use of the power operator.

Power Operated Stop Check Valves:

Testing of power operated stop check values is based on the function of the operator. If the value operator is always withdrawn, and the value operates as a simple check value except during maintenance, the value is tested as a simple check. If the operator is normally withdrawn, such that the value operates as a simple check in the forward direction, and the operator provides positive closure, it is tested as a simple check in the forward direction, and exercised closed using the operator. In addition to exercising, the operator will be timed and fail safe actuation tested as appropriate.

Pump Discharge Check Valves:

As a minimum, pump discharge check valves in safety-related systems will be forward flow exercised. In addition, reverse flow closure will be verified when failure of the valve to close could result in a substantial reduction of system performance. Such a potential exists with parallel pumps connected to common suction and discharge headers. If the check valve on the idle pump fails to close, a significant amount of system flow could be diverted back through the idle pump to the suction header.

System Piping Keep Fill Check Valves:

Keep fill lines are those lines attached to ECCS system piping whose function is maintenance of system water inventory to preclude water hammer. Forward flow operability is verified by a system check of water inventory performed at least quarterly. Reverse flow closure verification is performed only if failure of the valve to close could result in a significant reduction of ECCS system operation.

Check Valve Full/Partial Stroke:

In most cases full design flow through a check valve requires less than full mechanical valve movement. As used in this program, the term full stroke refers to the ability of the valve to pass design flow, and not the full mechanical stroking. Forward flow full stroke operability testing will be by any method that verifies the valve capable of passing design flow. Any test that verifies less than full design flow capability is considered as a partial stroke test.

ISI-203 Rev. 6





Category A (Containment Isolation Valve) Leak Testing:

All values specified for Appendix J, Type C, Local Leak Rate testing are included in the Value IST Program as Category A values. Appendix J, Type C, value local leak rate testing fulfills the intent of Articles IWV-3420 through IWV-3425 and will be performed in lieu of Section XI testing. Analysis of leakage rates and corrective actions requirements of IWV-3426 and IWV-3427 will be performed. The Program plan reflects the current list of values receiving Appendix J, Type C testing. Any future change to that list will be incorporated into the value test program.

Category A (Pressure Isolation Valve) Leak Testing:

All values designated as pressure isolation values in Table 3.4-1 of plant Technical Specifications are considered to perform a pressure isolation function between the Reactor Coolant System and a low pressure system and are included in the Value IST Program as Category A values. These values will be tested to the requirements specified in IWV-3420. Any change to the list of pressure isolation values in Technical Specifications will automatically be incorporated into the Value Test Program.

Category A (Containment and Pressure Isolation Valve) Leak Testing:

Valves which perform both a containment isolation and a pressure isolation function are included in the Valve IST Program Plan as Category A Valves. These valves will be tested to requirements of both Appendix J and Section XI.

Category A (Pressure Isolation) Valve Operability Testing:

Reactor Coolant System pressure isolation valves will be demonstrated operable in accordance with plant Technical Specification 4.4.6.2.2 by verifying leakage to be within specified limits:

- 1. At least once per 18 months,
- Prior to entering Mode 2 whenever the plant has been in Cold Shutdown for 72 hours or more and if leakage testing has not been performed in the previous 9 months,
- Prior to returning the value to service following maintenance, repair or replacement work on the value, and
- 4. Within 24 hours following value actuation due to automatic or manuel action or flow through the value.





Locked Valves:

0S2

This program plan classifies as locked valves only those which are physically restrained from movement (i.e., chain and padlock), or sealed (i.e., wire and seal) in position. Keylocked valves are not considered to be physically locked. This program plan makes no distinction between locked and non-locked manual valves and considers both to be passive.

Maximum Stroke Times:

Maximum stroke times have been developed based on actual observed times obtained during on-going pre-operational testing and operational test data for valves which can not be timed under repeatable test conditions during the pre-operational testing. These times along with manufactures data and Technical Specifications have been used to specify maximum stroke times for each valve prior to the end of the first refueling outage. Where actual stroke times are much less than Technical Specification values the limiting value of maximum stroke time will be determined from actual observed values, but at no time will maximum stroke time exceed Technical Specification values. A plant criteria has been developed for determining values of maximum stroke times from measured values as follows:

- 1. Stroke time greater than 10 Seconds 2 X baseline
- 2. Stroke time greater than 2 seconds 3 X baseline but equal to or less than 10 seconds
- 3. Stroke time equal to or less than 2 seconds 2 seconds

Values of maximum stroke times will be maintained separate from this document. This will allow for changes in maximum stroke times necessitated by changing test conditions, repairs, maintenance, modifications, etc., without requiring revision of the approved Valve Test Program Plan.

Valve Position Indicator Verification:

IWV-3300 requires that all valves with remote position indicators shall be observed at least once every two years to verify that valve operation is accurately indicated. It is the intent of this program that such verification will be performed on all valves included in this program which have remote position indicators.



İSI-203 Rev. 6

Valve Stroke Direction:

Valves will be stroked and timed in their safety-related direction(s). For example, a motor operated test valve whose safety-related operation is to close on system initiation will only be exercised and timed closed. If the valve must operate in both directions for safety-related system operation, it will be exercised and timed in both directions.

Valve Fail Safe Direction:

Valves will be tested to verify operability of the fail safe operator in the direction that the valve travels to perform its safety-related function. Valves equipped with fail safe operators for convenience only and which do not have to change position on loss of power for adequate safety-related operation will not be fail safe tested.

Temperature Inter-Locked Valves:

Valves which open and close in response to local temperature controls will not be tested unless they are inter-locked to system operation. For example, temperature inter-locked valves on local area heat exchangers will not be tested unless they are interlocked to go open/closed on system initiation for safety-related operation.

Check Valve Disassembly:

Valve disassembly is utilized as an alternative for check valves where it has been determined that testing is impractical. A sampling plan is used for groups of check valves which are identical (ie. same manufacturer, type, size, etc.) in construction and for which the system operating environment is the same. The sampling plan selects one valve from each group for disassembly during each refueling outage. If the selected valve passes inspection a second valve is selected for disassembly at the next refueling, etc., until the group has been completed or until such time that sufficient inspections have been performed to justify an alternate sampling plan. For those cases where disassembly indicates that there are no valve problems, a new relief request may be prepared to perform less frequent inspections:

Failure of the selected value to pass inspection will initiate additional value disassembly as specified by the appropriate relief request.

ISI-203 Rev. 6

Page 32 of 244

æ

0S2
. .

5.5.3 <u>Code Intepretation</u> (Continued)

The visual inspection of disassembled values includes verification that the value is capable of full stroke operation. All values specified for disassembly are of the bolted bonnet design. For values with hinge pins in the value body, full stroke operability will be verified by manually exercising the value through a complete cycle. For values with hinge pins in the removable bonnet such that the value internals are removed from the value body during disassembly direct verification of full stroke operability by manually exercising is not possible. For these values, full stroke operability will be by verification of full stroke travel of value internals for evidence of wear, binding, etc. and by stringent value reassembly procedures.

Containment Entry:

Entry into the Containment structure during normal operation or cold shutdown is strictly regulated by plant operating procedures. Because of environmental and ALARA considerations, entry is made only for tasks that are absolutely necessary for plant operation and duration inside the Containment is limited to as-short-as-possible. Because of this, valve testing that would require entry into Containment to perfrom special testing is considered to be beyond the scope of Section XI and is delayed to refueling.



5.5.4 Valve Test Table Nomenclature

The following abbreviations have been used in the Valve Test Table.

Valve Type	Actuator Type
BF - Butterfly Valve	AO - Air
BA '- Ball Valve	PO - Piston
CK - Check Valve	EH - Electro-Hydraulic
DA - Diaphragm Valve	MA - Manual
GL - Globe Valve	MO - Motor
GA - Gate Valve	NO - Nitrogen
ND - Needle Valve	SA - Self
RG - Regulator Valve	SO - Solenoid
RL - Relief Valve	
SK - Spring Check Valve	Stroke Direction
3W - Three Way Valve	0 - Open
PG - Plug Valve	C - Closed
Normal Position	Check Valve Test Direction
0 - Open	FF - Forward Flow
C - Closed	BS - Reverse Flow
LO - Locked Open	1

LC - Locked Closed

TH - Throttled

LT - Locked throttled

ISI-203 Rev. 6

Page 34 of 244

5.5.4 Valve Test Table Nomenclature (Continued)

Test Requirements

- FS Full Stroke Exercise Valve for operability in accordance with Article IWV-3412.
- FC Exercise valve with a fail-safe actuator to the closed position in accordance with Article IWV-3415.
- FO Exercise valve with a Fail-safe actuator to the open position in accordance with Article IWV-3415.
- LC Leak Test per both Appendix J, Type C, and Section XI (both pressure and containment isolation function).
- LJ Leak Test per Appendix J, Type C, in Accordance with Appendix J of 10 CFR 50 (containment isolation function only).
- LK Leak Test per Section XI, in accordance with Article IWV-3420 (pressure isolation function only).
- PE Partial Stroke Exercise in accordance with Article IWV-3412.
- PV Passive Valve as defined by Article IWV-2100.
- RD Rupture Disk as defined by Article IWV-3620.
- RL Relief Valve in accordance with Article IWV-3512.
- TS Stroke Time valve in accordance with Article IWV-3413 for valves with maximum stroke times specified in Plant Technical Specifications.
- TM Stroke Time valve in accordance with Article IWV-3413 for valves other than those with maximum stroke times specified in Plant Technical Specifications.
- PI Valve with remote position indication verified in accordance with Article IWV-3300.
- DS Valve will be disassembled and visually inspected as described in the Relief Request.
 - SP A special valve test procedure in lieu of Section XI testing, and described in the Relief Request.

0S2



Test Frequency

0S2

- 1 Once per 92 days
- 2 Testing performed during cold shutdown (but no sooner than 92 days) in accordance with Article IWV-3412.

NOTE: Testing may be performed during plant operating modes between normal operation and Tech. Spec. defined cold shutdown conditions.

- 3 Once per refueling outage
- <u>NOTE</u>: Testing may be performed during plant operating modes between normal operation and Technical Specification defined refueling conditions.
- 4 Tested during the time period defined in: IWV-3511 and ANSI/ASME OM-1 - 1981 (safety and relief valves) IWV-3620 (rupture disks)
- 5 Once per 2 Years in accordance with Article IWV-3300.



ISI-203 Rev. 6

Valve No.	Unique number assigned to each valve.
Class and Dwg. Coor.	The ASME valve class and drawing reference location. This is a two line entry with the class on the first line and drawing coordinate on the second line.
Valve Cat.	Valve category as defined in Subsection IWV-2200.
Size (in.) and Type	A two line entry with the first being the valve size in inches, and the second the valve type.
Actu. Type	The type of operator used to change valve position. For dual function valves this will be a two line entry. For example, a locked open stop check valve is entered as self actuating on one line, and manual on the other.
Norm. Posit.	The valve position during normal plant operation.
Test Req.	The test requirements which apply to the valve. For dual function valves, multiple line entries of applicable tests which correspond to actuator type.
Stroke Direct.	This a multiple line entry for safety- related stroke direction. If both directions are safety-related, two lines are used. This column also includes direction for positive closure power operated check valves.
Check Valve Test Direction	Direction of check valve operability verification. May be a two line entry if valve operability is safety-related in both directions.
C.S. Just. or Relief Req. No.	Reference number of the cold shutdown justification or relief request located following the Valve Test Tables for each system.
C.S. or Alt. Test Perf.	Cold shutdown or alternate testing which is being performed in lieu of the Code specified quarterly testing.
ISI-203 Rev. 6	Page 37 of 244



٠,

5.5.5	Valve	Test	Table	Format	(Continued)

Valve No. (continued)	Unique number assigned to each valve
Remarks	Key to notes providing amplifying
• _	remarks. These notes are located prior to the Valve Test Tables.

Rev. No.

This column records the document revision number for each valve.

System	Dwg. No.	Rev. No.	Section
Containment HVAC	2165-S-1017	1	5.6.1
Reactor Aux. Bldg. HVAC	2168-G-517 SO3	9	5.6.2
Control Room HVAC	2168-G-517 S04	8	5.6.3
Fuel Bldg. HVAC	2168-G-533	10	5.6.4
Switchgear and Protection Room HVAC	2168-G-517 S05	- 11	5.6.5
Main Steam	2165-5-542	· 12 ´	5.6.6
Feedwater	2165-S-544	14	5.6.7
Auxiliary Feedwater	2165-S-544	14	5.6.8
Condensate	2165-8-545	16	5.6.9
Service Water	2165-5-547 2165-5-588 2165-5-936	14 8 10	5.6.10
Containment Spray	2165-S-550	9	5.6.11
Steam Generator Blowdown	2165-S-551	6	5.6.12
Process Sampling	2165-8-551 2165-8-552	6 7	5.6.13
D.G. Fuel Oil Transfer	2165-S-563	5	5.6.14
Rad. Monitor and H2 Analizer	2165-S-605	7	5.6.15
D.G. Starting Air	2165-S-633	4	5.6.16
Demineralized Water	2165-S-799	5	5.6.17

. ISI-203 Rev. 6

Page 38 of 244





5.5.5 Valve Test Table Format (Continued)

	I		
System	Dwg. No.	Rev. No.	Section '
CTMT. Sump Drains	2165-S-685	8	5.6.18
Service Air	2165-S-800	5	5.6.19
Instrument Air	2165-S-801	12	5.6.20
	2165-5-1017	1	
Fuel Pool Cooling	2165-S- <u>5</u> 61	4	5.6.21
	2165-S-805	5	
Emergency Screen Wash	2165-S-808	6	5.6.22
Fire Protection	2165-S-888	3	5.6.23
Essential Chilled Water	2165-S-998	3	5.6.24
¥	2165-S-998 SO2	× 6	
•	2165-5-999	2	
	2165-8-000 802	–	
	2103-3-333 302	0	
Reactor Coolant	2165-S-1301	6	5.6.25
CVCS	2165-5-1303	7	5.6.26
	2165-S-1303 SOI	. 3	
	2165-S-1303 S02	2	
ĩ	2165-S-1304	9	
	2165-S-1305	9	
	· 2165-S-1306	6	
	2165-S-1307	. 4	
Safety Injection	2165-S-1308	7	5.6.27
	2165-S-1309	10	
	2165-S-1310	6	•
CTMT. Waste Processing	2165-S-1313	4	5.6.28
Component Cooling Water	2165-S-1319	7	5.6.29
•	2165-S-1320	0	
5	2165-S-1321	5	
	2165-S-1322	3	
	2165-S-1322 SOI	. 2	
Residual Heat Removal	2165-S-1324	7	5.6.30
CTMT. Integrated Leakage Detection	2166-5-916	1	5.6.31

5.6 Valve Test Tables and Relief Requests



Page 39 of 244

052

•

PUMP AND VALVE INSERVICE TESTING PROGRAM PLAN

FOR

SHEARON HARRIS NUCLEAR POWER PLANT

SECTION 5.6.1

VALVE TEST TABLES AND RELIEF REQUESTS

FOR

CONTAINMENT HVAC

DWG. NO. 2165-S-1017

<u>NO.</u>	NOTE
1.	Containment Vacuum relief Containment isolation valves.
2.	Post-accident Hydrogen Purge Back-up to Recombiners. Valves are maintained closed except for Post-LOCA Hydrogen Purge.
3.	Normal Containment Purge and Make-up Isolation Valves. Plant Tech. Spec. 3.6.1.7 allows these valves to be opened for safety-related reasons only in Modes 1-4.
4.	Containment Isolation Valves for Pre-Entry Purge. Valves are incapable of closing against accident flow. Plant Tech. Spec. 3.6.1.7 requires maintaining these valves closed during normal operation.
5.	Valve numbers have been revised as follows: 2CB-B1 = 1CB-2 2CP-B1 = 1CP-9 2CB-B2 = 1CB-6 2CP-B4 = 1CP-7 2CB-V1 = 1CB-3 2CP-B3 = 1CP-10 2CB-V2 = 1CB-7 2CP-B6 = 1CP-3 2CM-B4 = 1CM-4 2CP-B5 = 1CP-5 2CM-B5 = 1CM-2 2CP-B8 = 1CP-1 2CM-B6 = 1CM-5 2CP-B7 = 1CP-4

6.

Containment Isolation Valve

2CP-B2 = 1CP-6

COLD SHUTDOWN TEST JUSTIFICATION

CS-1

System:

0S2

Containment HVAC

1CP-1,4,7,10

Valve:

Category:

A

2

· Class:

ASME Section XI Quarterly Test Requirements:

Cold Shutdown Test Justification:

Quarterly Part Stroke Testing:

Cold Shutdown 'Testing: Exercise, Time and Fail.

If these values were open during LOCA, the value operators are incapable of closing the values against the accident flow conditions. Plant Technical Specifications (3.6.1.7) require maintaining these values closed and sealed closed during plant operating modes 1,2,3 and 4.

Valves are administratively close and sealed closed during normal operations.

Exercise, time and fail.

ISI-203 Rev. 6

Page 42 of 244

•

v

ĩ

,

VALVE

RELIEF REQUEST

Containment HVAC

1CB-3,7 :1CM-7

<u>RV-1</u>

System:

Valve:

0S2

Category:

Class:

AC 2

Function:

Test

Requirements:

Basis for Relief:

Alternate Testing:

Containment Vacuum Relief Isolation Check Valves (1CB-3,7), and Hydrogen Purge Make-up Isolation Valve (1CM-7).

Verify forward flow operability and reverse flow closure.

There are inside Containment simple check valves and do not have position verification capability. To verify forward flow operability using system fluid would require injecting large quantities of air into the Containment and would result in a Containment overpressurization condition. The only practical method to verify forward flow operability is by mechanically exercising the valve disk through a complete cycle by hand. Entry into Containment during cold shutdown is limited by plant procedures to perform only necessary repair and maintenance work. In cases of short shutdowns caused by problems external to the Containment there may be no entry made into the Containment: The only method available to verify reverse flow closure is by valve leak rate testing during Appendix J. Type C. Testing at refueling.

Verify forward flow operability by using a manual exercising procedure yia a spring scale at Refueling. Verify reverse flow closure during Appendix J, Type C, Testing at Refueling.

ISI-203 Rev. 6

Page 43' of 244

SHEARON HARRIS NUCLEAR POWER PLANT VALVE TEST TABLE

÷



DWG. NO. 2165-	<u>S-1017</u>					·		·				
VALVE NUMBER	CLASS AND DWG. COOR.	VALVE (CAT.)	SIZE (IN.) AND TYPE	ACTU. TYPE	NORM. POSIT.	TEST REQ.	STROKE DIRECT.	CHECK VALVE TEST DIRECT.	C.S. JUST. OR RELIEF REQ.NO.	C.S. OR ALT. TEST PERF.	REMARKS	REV. NO.
í íc8-2	2 G-4	A	24 BF	AO	c	' FS-1 TS-1 FC-1 PI-5 LJ-3	С 0	<u>L</u>	L,		NOTE 1,5	_
108-3	2 G-6	AC	24 CK	SA	C	FS-1 85-1 LJ-3		FF 8S	RV-1 RV-1	SP-3 SP-3	NOTE 1,5	Ĩ
103-6	2 H-4	^ .	24 BF	AO	C	FS-1 TS-1 FC-1 P1-5 LJ-3	C O				NOTE 1,5	
108-7	2 H-6	AC	24 CK	SA .	C	FS-1 BS-1 LJ-3		FF BS	RV-1 RV-1	SP-3 SP-3	NOTE 1,5	
1 CH-2	2 8 -5	A	3 BF	AO	C	FS-1 TM-1 FC-1 P1-5 LJ-3	C			2	NOTE ·2,5,6	
1CH-4	2 8-4	۸	3 BF	MA	LC	PV LJ-3		2	-		NOTE 2,5,6	
104-5	2 H-4	٨	3 BF	ма	LC	PV LJ-3	•				NOTE 2,5,6	-
104-7	2 H -6	ĨĂĊ	3 CK	SA	C	FS-1 BS-1 LJ-3	· ·	FF BS	RV-1 RV-1	SP-3 SP-3	NOTE 2,5,6	
1CP-1	2 D-4	A	42 BF	AO	С ,	FS-1 TS-1 FC-1 P1-5 LJ-3	C		CS-1 CS-1 CS-1	FS-2 TS-2 FC-2	NOTE 4,5	ĸ



Page 44 of 244

5

•*

0S2

.

SHEARON HARRIS NUCLEAR POWER PLANT VALVE TEST TABLE

SYSTEM: CONTAINMENT HVAC

DWG. NO. 2165-5-1017 C.S. c.s. ACTU. CLASS VALVE SIZE NORM. TEST STROKE CHECK JUST. OR REMARKS VALVE NUMBER AND (CAT.) (IN.) TYPE POSIT. REQ. DIRECT. VALVE OR ALT. AND DWG. TEST RELIEF TEST COOR. TYPE DIRECT. REQ.NO. PERF. 1CP-3 2 0/C C 8 AO FS-1 NOTE 3,5 Α 8F E-4 TS-1 FC-1 PI-5 LJ-3 1CP-4 2 42 AO . С FS-1 С CS-1 FS-2 NOTE 4.5 A D-6 BF TS-1 CS-1 • TS-2 FC-1 FC-2 CS-1 PI-5 LJ-3 1CP-5 0/C 2 8 AO FS-1 **C** -NOTE 3,5 A BF E--6 TS-1 FC-1 PI-5 LJ-3 1CP-6 0/C FS-1 С NOTE 3,5 2 8 · AO A F-5 BF TS-1 FC-1 PI-5 LJ-3 1CP-7 2 C FS-1 С CS-1 NOTE 4,5 Α 42 AO FS-2 F-5 BF TS-1 CS-1 TS-2 FC-1 CS-1 FC-2 P1-5 LJ-3 1CP-9 2 0/C FS-1 С NOTE 3,5 8 AO A 8F F-6 TS-1 FC-1 PI-5 . LJ-3 NOTE 4,5 1CP-10 C FS-1 CS-1 2 42 AO С FS-2 Α F-6 8F TS-1 TS-2 CS-1 FC-1 FC-2 CS-1 P1-5 LJ-3

Page 45 of 244

REV.

NO.

0S2



1

.

I

2

. .

đi

PUMP AND VALVE INSERVICE TESTING PROGRAM PLAN

FOR

SHEARON HARRIS NUCLEAR POWER PLANT

SECTION 5.6.2

VALVE TEST TABLES AND RELIEF REQUESTS

FOR

REACTOR AUXILIARY BUILDING (RAB) HVAC

DWG. NO. 2165-G-517 S03





. •

.

٦

n N

I.

ه

b

٠

,

Í	

SYSTEM: RAB HVAC

NO.

NOTE

NONE

ISI-203 Rev. 6

SHEARON HARRIS NUCLEAR POWER PLANT VALVE TEST TABLE

SYSTEM: RAB HVAC

		-	
DWG.	NO.	2168-G-517	S03

VALVE NUMBER	CLASS AND DWG. COOR.	VALVE (CAT.)	SIZE (IN.) AND TYPE	ACTU. TYPE	NORM. POSIT.	TEST REQ.	STROKE DIRECT.	CHECK VALVE TEST DIRECT.	C.S. JUST. OR RELIEF REQ.NO.	C.S. OR ALT. TEST PERF.	REMARKS	REV. NO.
3AV-BISA-1	3 F-14	B	20 BF	МО	С	FS-1 TH-1 P1-5	0	*	+			
3AV-82SA-1	3 F-17	B	20 BF	MO	С	FS-1 TM-1 PI-5	0		r			ji.
3AV- B 3SB-1	3 E-14	B	6 BF	МО	C	FS-1 TM-1 P1 -5	0 .			,		
3AV-8488-1	3 G-14	B	20. BF	Ю	С	FS-1 TM-1 PI-5	0					•
3AV-8558-1	3 G-17	8	20 BF	мо	С	FS-1 TM-1 P1-5	0	•	• و بر	v		
3AV-865A-1	3 G-14	B	6 8F	мо	С	FS-1 TM-1 P1-5	0					•
3AV-V3-1	3 E-14	C	6 .CK	SA	C	FS-1	I	FF	,	*		
3AV-V4-1	3 G-14	C	6 CK	SA	С	FS-1		FF				

 \cap

`

PUMP AND VALVE INSERVICE TESTING PROGRAM PLAN

FOR

SHEARON HARRIS NUCLEAR POWER PLANT

SECTION 5.6.3

VALVE TEST TABLES AND RELIEF REQUESTS

FOR

CONTROL ROOM HVAC

DWG. NO. 2165-G-517 S04



ISI-203 Rev. 6

.

/

I

NO.

1.

NOTE

Verification of reverse flow is not necessary since the intake valves are interlocked with blower operation and are closed when the blowers are idle.

ISI-203 Rev. 6

.

.

•

2

×

, , , ,

SHEARON HARRIS NUCLEAR POWER PLANT VALVE TEST TABLE

.

SYSTEM: CONTROL ROOM HVAC

DWG. NO. 2168-G-517 SO4

VALVE NUMBER	CLASS AND DWG. COOR.	VALVE (CAT.)	SIZE (IN.) AND TYPE	ACTU. TYPE	NORM. POSIT.	TEST REQ.	STROKE DIRECT.	CHECK VALVE TEST DIRECT.	C.S. JUST. OR RELIEF REQ.NO.	C.S. OR ALT. TEST PERF.	REMARKS	REV. NO.
3CZ-B1SA-1	3 H-2	B	16 BF	Ю	0	FS-1 TM-1 P1-5	C				4	, ,
3CZ-B2SB-1	3 H-2	В	16 BF	мо	0	FS-1 TM-1 P1-5	C				,	
3CZ-B3SA-1	3 E-2	B	12 BF	мо	0	FS-1 TM-1 P1-5	C				4	
3CZ-8458-1	3 E-2	8	12 BF	ю	0	FS-1 TM-1 PI-5	C					•
3CZ-89SA-1	3 N-5	8	12 BF	MO	С	FS-1 TM-1 PI-5	0					
3CZ-B10SB-1	3 N-5	B	12 BF	МО	C	FS-1 TM-1 P1-5	0					
3CZ-B11SA-1	3 N-11	B	12 BF	мо	C	FS-1 TM-1 P1-5	0					
3CZ-B12SB-1	3 N-11	B	12 BF	мо	C	FS-1 TM-1 P1-5	0					
3CZ-B13SA-1	3 B-4	B	30 BF	мо	с _	FS-1 TM-1 P1-5	: c`	×			×	





.

Page 51 of 244

.

SHEARON HARRIS NUCLEAR POWER PLANT VALVE TEST TABLE

SYSTEM: CONTROL ROOM HVAC

DWG. NO. 2168-G-517 SO4

010. 10. 2100-	3-317	<u> </u>										
VALVE NUMBER	CLASS AND DWG. COOR.	VALVE (CAT.)	SIZE (IN.) AND TYPE	ACTU. TYPE	NORM. POSIT.	TEST REQ.	STROKE DIRECT.	CHECK VALVE TEST DIRECT.	C.S. JUST. OR RELIEF REQ.NO.	C.S. OR ALT. TEST PERF.	REMARKS	REV. NO.
3CZ-814SB-1	3 B-4 -	8	30 BF	мо	С	FS-1 TM-1 PI-5	Ċ		•			
3CZ-B17SA-1	3 G-2	B	36 8F	Ю	C	FS-1 TM-1 P1-5	C		5	-		
3CZ-B18SB-1	3 G-2	B	36 BF	Ю	С	FS-1 TM-1 P1-5	C					
3CZ-B19SA-1	- 3 H-7	8	20 BF	но .	C	FS-1 TM-1 P1-5	0	·				•
3CZ-82058-1	3 H-8	8	20 BF	МО	C	FS-1 TM-1 PI-5	0					
3CZ-821SA-1	3 К-б	B	20 BF	мо	с	FS-1 TM-1 PI-5	0					
3CZ-822SB-1	3 К-7	8	20 BF	мо	C	FS-1 TM-1 PI-5	0	-				ŧ
3CZ-823SA-1	3 . L - 6	8	20 BF	мо	С	FS-1 TM-1 PI-5	0					
3CZ-824S8-1	'3 L-7	8	20 BF	Ю	С	FS-1 TM-1 PI-5	ŏ					Å



•

2

.

. .

٠ .

i -



SHEARON HARRIS NUCLEAR POWER PLANT VALVE TEST TABLE

SYSTEM: CONTROL ROOM HVAC

DWG. NO. 2168-G-517 SO4

VALVE NUMBER	CLASS AND DWG. COOR.	VALVE (CAT.)	SIZE (IN.) AND TYPE	ACTU. TYPE	NORM. POSIT.	TEST REQ.	STROKE DIRECT.	CHECK VALVE TEST DIRECT.	C.S. JUST. OR RELIEF REQ.NO.	C.S. OR ALT. TEST PERF.	REMARKS	REV.
- 3CZ-825SA-1	3 G-4	B	36 BF	мо	0/C	FS-1 TM-1 P1-5	0					
3CZ-82658-1	3 H - 4	В	36 BF	мо	0/C	FS-1 TM-1 PI-5	0					
3CZ-V15A-1	3 L-7	Ċ	6 CK	SA	С	FS-1		FF			NOTE 1	
3CZ-V2SB-1	3 L-7	C	6 CK	sa .	C	FS-1		FF			NOTE 1	•



0S2

ı

• •

,

•

*

•

PUMP AND VALVE INSERVICE TESTING PROGRAM PLAN

FOR

SHEARON HARRIS NUCLEAR POWER PLANT

SECTION 5.6.4

.

VALVE TEST TABLES AND RELIEF REQUESTS

• FOR

FUEL BUILDING HVAC

DWG. NO. 2165-G-533



đ

. . •

.

•

- , .

P

SYSTEM: FUEL BUILDING HVAC

NO.

NOTE

NONE



.

SHEARON HARRIS NUCLEAR POWER PLANT VALVE TEST TABLE

SYSTEM: FUEL BUILDING HVAC

DWG. NO. 216-G-533

VALVE NUMBER	CLASS AND DWG. COOR.	VALVE (CAT.)	SIZE (IN.) AND TYPE	ACTU. TYPE	NORM. POSIT.	TEST REQ.	STROKE DIRECT.	CHECK VALVE TEST DIRECT.	C.S. JUST. OR RELIEF REQ.NO.	C.S. OR ALT. TEST PERF.	REMARKS	REV. NO.
3FV- 8 2SA-1-	4 3 G-14	B	24 BF	но	С	FS-1 TM-1 P1-5	0	•				
3FV-84S8-1-	4 3 F-14	B	24 BF	MO	C	FS-1 TM-1 PI-5	0					





. .

.

,

3

ı.

ι

, r

8

ف

ł

. .



.

PUMP AND VALVE INSERVICE TESTING PROGRAM PLAN

FOR ,

SHEARON HARRIS NUCLEAR POWER PLANT

SECTION 5.6.5

VALVE TEST TABLES AND RELIEF REQUESTS

FOR

,

SWITCHGEAR AND PROTECTION ROOM HVAC

DWG. NO. 2165-G-517 S05

ISI-203 Rev. 6

Page 57 of 244
SYSTEM: SWITCHGEAR AND PROTECTION ROOM HVAC

NO.

1. Valves close and Blowers shutdown on a SIS signal.

NOTE



SYSTEM: SWTCHGR & PROT. ROOM HVAC

DWG. NO. 2168-G-517 S05

VALVE NUMBER	CLASS AND DWG. COOR.	VALVE (CAT.)	SIZE (IN.) AND TYPE	ACTU. TYPE	NORM. POSIT.	TEST REQ.	STROKE DIRECT.	CHECK VALVE TEST DIRECT.	C.S. JUST. OR RELIEF REQ.NO.	C.S. OR ALT. TEST PERF.	REMARKS	REV. NO.
3CZ-85SA-1	3 L-3	B	12 8F	мо	0	FS-1 TM-1 P1-5	С		·		NOTE	1
3CZ-86SB-1	3 L-3	β.	12 8F	МО	0	FS-1 TM-1 PI-5	C				NOTE	1
3CZ-87SA-1	3 K-10	B	12 BF	мо	0	FS-1 TM-1 P1-5	C		t p T		· NOTE	1
3CZ-8888-1	3 K-9	В	12 BF -	мо	, 0	FS-1 TM-1 PÍ-5	C	•			NOTE	1

0S2



PUMP AND VALVE INSERVICE TESTING PROGRAM PLAN

FOR

SHEARON HARRIS NUCLEAR POWER PLANT

SECTION 5.6.6

VALVE TEST TABLES AND RELIEF REQUESTS

FOR

MAIN STEAM

DWG. NO. 2165-S-542

ISI-203 Rev. 6

Page 60 of 244

•
۵
,

0S2

SYSTEM:	MAIN STEAM	· ,
	NO.	NOTE
	1.	Main Steam to Auxiliary Feedwater Turbine Trip and Throttle Valves.
	2.	Main Steam Sample Valves.
	3.	Main Steam Relief Valves.
	4.	Main Steam Power Operated Relief Valves. Valves are Nitrogen supplied, electro/hydrolic operated gate valves.
	5.	Main Steam to Auxiliary Feedwater Turbine Line Block Valves.
, ,	6.	Main Steam Supply to Auxiliary Feedwater Turbine Line Check Valves. Partial forward flow operability is verified by Turbine operation. Reverse flow closure is required to prevent steam flow between the Main Steam lines when line block valves are open (both block valves open on system isolation).
	7	Main Steam Line Isolation Valves. Valve operators are designed to perform a partial stroke closed test with full steam flow.
	8.	Bypass Line Valves around the Main Steam Line Isolation Valves.
	9.	Steam Generator Blowdown Isolation Valves.



e.

И

.

. .

COLD SHUTDOWN TEST JUSTIFICATION

CS-1

System: -

Valve:

MAIN STEAM

1MS-58,60,62

В

2

Category:

Class:

ASME Section XI Quarterly Test Requirements:

Cold Shutdown Test Justification:

Quarterly Part Stroke Testing:

Cold Shutdown Testing: Exercise, Time and Fail.

Exercising these valves during normal operation would cause a decrease in Main Steam line pressure and an increase in secondary system steam demand, resulting in a serious self imposed plant transient. This transient could result in a forced plant shutdown.

Valves are full stroke on initiation and can not be partial stroke exercised.

Exercise, time and fail.

0S2



COLD SHUTDOWN TEST JUSTIFICATION

CS-2

1MS-80,82,84

System:

MAIN STEAM

В

2

Valve:

Category:

Class:

ASME Section XI Quarterly Test Requirements:

Cold Shutdown Test Justification:

Quarterly Part Stroke Testing:

Cold Shutdown Testing: Exercise, Time and Fail.

Exercising these valves during normal operation isolates one line of steam flow to the Turbine and would cause a severe pressure transient in the Main Steam line which could result in a forced plant shutdown. Reducing power level to perform testing without causing a transient would significantly impact plan operations and power production.

Valves are equipped with a partial stroke closed exerciser and will be partial stroke exercised Quarterly.

Exercise, time and fail.



VALVE

RELIEF REQUEST

<u>RV-1</u>

MAIN STEAM

1MS-G

В

3

Category:

Class:

System:

Valve:

Function:

Auxiliary feedwater steam driven turbine Governing Valve (1MS-G)

Measure stroke time Quarterly.

turbine. Operability is

Test Requirements:

Basis for Relief:

Alternate Testing:

control signals. Proper operation of this valve will be verified during turbine testing. No stroke time testing will be performed.

The purpose of this valve is to regulate

adequately demonstrated by proper turbine operation. Valve position is steam line pressure and turbine speed dependent and therefore will not repeatedly throttled to the same position. During turbine operation this valve moves in response to

steam flow to the AFW steam driven

0S2



Page 64 of 244



VALVE

RELIEF REQUEST

<u>RV-2</u>

MAIN STEAM

С

3

System:

0S2

Valve: 1MS-7.1,73

Category:

Class:

Function:

Test Requirements:

Basis for Relief:

Main Steam to Auxiliary Feedwater Pump Turbine Line Check Valves.

Verify forward flow and reverse flow closure.

The only possible method to verify forward flow operability is by running the Auxiliary Feedwater Pump Turbine at full flow conditions. The quarterly pump test is performed with flow through a minimum flow line which is not a full flow test. These check valves are also safety-related to prevent cross-flow between the Main Steam lines when the upstream motor operated valves are open (both motor operated valves open on initiation of Auxiliary Feedwater). To verify reverse flow closure would require blanking (the turbine stop valve is not a leak tight valve) the turbine line, injecting fluid into the line and monitoring upstream of the valves for evidence of gross leakage. Upstream of these valves are the Main Steam lines and Steam Generators. Because of the long time to perform this test and the large volume of waste water involved, it is not a practical test method.

Page 65 of 244

•

٠

.

۰ •



Alternate Testing:

0S2

Both valves will be partial flow exercised in the forward direction quarterly during Auxiliary Feedwater Pump testing and one of the Check valves will be disassembled at Refueling and visually inspected. Alternate valves will be inspected at each Refueling, unless the inspected valve fails to pass inspection. If either valve fails to pass inspection the other valve will also be disassembled and inspected.

Both valves will be full flow exercised in the forward direction on a cold shutdown frequency when the full flow test on the Turbine Driven Aux Feed Pump is performed.



.

SYSTEM: MAIN STEAM

DWG. NO. 2165-5-542

	VALVE NUMBER	CLASS AND DWG. COOR.	VALVE (CAT.)	SIZE (IN.) AND TYPE	ACTU. TYPE	NORM. POSIT.	TEST REQ.	STROKE DIRECT.	CHECK VALVE TEST DIRECT.	C.S. JUST. OR RELIEF REQ.NO.	C.S. OR ALT. TEST PERF.	REMARKS	REV. NO.
-	1HS-G	3 N-1	8.	'4 GL	EH	ο	FS-1 TM-1	o C		RV-1	sp-1	NOTE 1	
	iks-t	3 N-1	B	4 GT	ŴО	0	FS-1 TM-1 PI-5	0 C	•			NOTE 1	
	[·] 1HS-25	2 D-2	B	1 GA	AO .	0/C	FS-1 TM-1 FC-1 P1 -5	C				NOTE 2	
	1HS-27	2 G-2	B,	1 GA	AO	́ 0/C	FS-1 TM-1 FC-1 P1-5	С				NOTE 2	•
	1HS-29	2 K-2	8	1 GA	AO	0/C	FS-1 TM-1 FC-1 P1-5	C ·		,		NOTE 2	
•	1HS-43	2 C-3	C RL	8X10	SA	C .	RL-4			•		NOTE 3	
	1MS-44	2 G-3	C	8X10 RL	SA	C	_ RL-4			¥	1	NOTE 3	
	1MS-45	2 J-3	C	8X10 RL	SA	C	RL-4					NOTE 3	
	1MS-46	2 C-4	"C	8X10 RL	SA	C	RL-4	:				NOTE 3	2





Page 67 of 244

IS

SYSTEM: MAIN STEAM

DWG. NO. 2165-5-542

VALVE NUMBER	CLASS AND DWG. COOR.	VALVE (CAT.)	SIZE (IN.) AND TYPE	ACTU. TYPE	NORM. POSIT.	TEST REQ.	STROKE DIRECT.	CHECK VALVE TEST DIRECT.	C.S. JUST. OR RELIEF REQ.NO.	C.S. OR ALT. TEST PERF.	REMARKS	REV. NO.
- 1MS-47 .	2 G-4	C	8X10 RL	SA	C	· RL-4			•		NOTE 3	
` 1MS-48	2 J-4	C	8X10 RL	SA	C	RL-4					NOTE 3	
1MS-49	2 C-5	C	8X10 RL	SA <u></u>	C	RL-4			-		NOTE 3	
1MS-50	2 G -5	C	8X10 RL	SA	C	RL-4			۰.		NOTE 3	
1MS-51	2 J-5	C	8X10 RL	SA	C	RL-4					NOTE 3	·
1MS-52	2 C-6	C	8X10 RL	SA	C	RL-4					NOTE 3	
1MS-53	2 G-6	C	8X10 RL	SA	C	RL-4					NOTE 3	
1MS-54	2 J-6	°C	8X10 RL	SA	C	RL-4			•		NOTE 3	
1MS-55	2 C-6	C	8X10 RL	SA	с _.	RL-4				1	NOTE 3	



i I IÎ

SYSTEM: MAIN STEAM

DWG. NO. 2165-5-542

VALVE NUMBER	CLASS AND DWG. COOR.	VALVE (CAT.)	SIZE (IN.) AND TYPE	ACTU. TYPE	NORM. POSIT.	TEST REQ.	STROKE DIRECT.	CHECK VALVE TEST DIRECT.	C.S. JUST. OR RELIEF REQ.NO.	C.S. OR ALT. TEST PERF.	REMARKS	REV.
- 1MS-56	2 G -6	C	8X10 RL	SA	C	RL-4					NOTE 3	,
1MS-57	2 J-6	С	8X10 RL	SĂ	с .	RL-4					NOTE 3	
1MS-58	2 C-8	BC	8 GA	eh No	C	FS-1 TM-1 FC-1 P1-5	0 C	1	CS-1 CS-1 CS-1	FS-2 TM-2 FC-2	NOTE 4	
1MS-60	2 F-8	BC	8 GA	eh No	C	FS-1 TM-1 FC-1 P1-5	O C		CS-1 CS-1 CS-1	FS-2 TM-2 FC-2	NOTE 4	•
1MS-62	2 J-8	BC	8 GA	eh . No	С	FS-1 TM-1 FC-1 PI-5	0 C		CS-1 CS-1 CS-1	FS-2 TM-2 FC-2	NOTE 4	-
1MS-70	2 H-7	B	6 GA	мо	, C -	FS-1 TM-1 P1-5	o C		•		NOTE 5	
ĮMS-71	3 H-7	C	6 CK	SA	С	FS-1 BS-1		FF BS	RV-2 RV-2	PE-1 DS	NOTE 6	
1MS-72	2 K-7	8	6 GA	мо	C	FS-1 TM-1 P1-5	0 C				NOTE 5	a
1MS-73	3 K-7	C	6 CK	SA	C	FS-1 BS-1		FF BS	RV-2 RV-2	PE-1 DS	NOTE 6	





0S2



*

. ,

,

•

SYSTEM: MAIN STEAM

DWG. NO. 2165-S-542 c.s. c.s. CLASS VALVE SIZE ACTU. NORM. TEST STROKE CHECK JUST. OR REMARKS REV. VALVE NUMBER AND (CAT.) (IN.) TYPE POSIT. REQ. DIRECT. VALVE OR ALT. OWG. AND TEST RELIEF TEST NO. COOR. TYPE DIRECT. REQ.NO. PERF. 2 B 1MS-80 34 PO 0 FS-1 С CS-2 FS-2 NOTE 7 D-9 GL TS-1 CS-2 TS-2 . FC-1 CS-2 FC-2 PI-5 PE-1 . 1HS-81 2 в 3 -AO С FS-1 C NOTE 8 D-9 GA TS-1 FC-1 PI-5 1MS-82 2 8 34 PO С FS-1 С FS-2 CS-2 NOTE 7 G-9 GL TS-1 CS-2 TS-2 FC-1 CS-2 FC-2 P1-5 PE-1 1**MS-83** 2 В 3 AO С FS-1 C NOTE 8 H-9 GA TS-1 FC-1 P1-5 1**MS-8**4 2 8 34 PO 0 FS-1 С CS-2 FS-2 NOTE 7 J-9 GL TS-1 CS-2 TS-2 FC-1 CS-2 FC-2 PI-5 PE-1 1MS-85 2 8 3 AO С FS-1 C NOTE 8 K-9 GA . TS-1 FC-1 PI-5 IMS-231 2 8 2 AO 0/C FS-1 С NOTE 9 E-8 GL TS-1 FC-1 P1-5 ۰. 1MS-266 2 В 2 AO 0/C FS-1 C, NOTE 9 1-8 GL TS-1 FC-1 PI-5 1MS-301 2 В 2 AO 0/C FS-1 С NOTE 9 L-8 GL TS-1 FC-1 PI-5

Page 70 of 244

0S2

ų

SYSTEM: MAIN STEAM

DWG. NO. 2165-5-542

VALVE NUMBER	CLASS AND DWG. COOR.	VALVE (CAT.)	SIZE (IN.) AND TYPE	ACTU. TYPE	NORM. POSIT.	TEST REQ.	STROKE DIRECT.	CHECK VALVE TEST DIRECT.	C.S. JUST. OR RELIEF REQ.NO.	C.S. OR ALT. TEST PERF.	REMARKS	REV.
1MS-336	3 M-4	B	2 GL	AO	0	FS-1 TM-1 FC-1 P1-5	C					
1MS-354	3 N-5	B	2 GL	AO	0	FS-1 TH-1 FC-1 PI-5	С					

Page 71 of 244



PUMP AND VALVE INSERVICE TESTING PROGRAM PLAN

FOR

SHEARON HARRIS NUCLEAR POWER PLANT

SECTION 5.6.7

VALVE TEST TABLES AND RELIEF REQUESTS

FOR

FEEDWATER

DWG. NO. 2165-5-544



ISI-203 Rev. 6

_er,

OS2

SYSTEM:	FEEDWATER	
	NO.	NOTE
	•	

1.	Feedwater Isolation Valves, close on isolation signal. Valves are equipped with partial stroke operators for testing at full flow.
2.	Chemical Addition Isolation Valves.
3	Foodmator Toolation Value Purses Value



COLD SHUTDOWN TEST JUSTIFICATION

cs-1

System:

Feedwater

- B

2

Valve:

1FW-159,217,277

,

Category:

Class:

ASME Section XI Quarterly Test Requirements:

Cold Shutdown Test Justification:

Quarterly Part Stroke Testing:

Cold Shutdown Testing: Exercise, Time and Fail.

Exercising these values closed during normal operation would result in a loss of Feedwater to the associated Steam Generator. Isolation of Feedwater flow during normal operation would cause a severe Steam Generator operating transient which could result in a forced plant shutdown and/or Reactor trip.

Valves'are equipped with partial stroke exercisers. Each valve will be exercised to it's 90% open position and back to the full open position.

Exercise, Time and Fail.



.

,

SYSTEM: FEEDWATER

DWG. NO. 2165-5-544

VALVE NUMBER	CLASS AND DWG. COOR.	VALVE' (CAT.)	SIZE (IN.) AND TYPE	ACTU. TYPE	NORM. POSIT.	TEST REQ.	STROKE DIRECT.	CHECK VALVE TEST DIRECT.	C.S. JUST. OR RELIEF REQ.NO.	C.S. OR ALT. TEST PERF.	REMARKS	REV.
1FW-159	2 8-6	8	16 GA	EH	. 0	FS-1 TS-1 FC-1 P1-5	C` 	•	CS-1 CS-1 * CS-1	FS-2 TS-2 FC-2 PE-1	NOTE 1	· · · · · · · · · · · · · · · · · · ·
1FW-163	2 B-6	B	1 GA	AO	0/C	FS-1 TM-1 FC-1 P1-5	. C	·			NOTE 2	. (*) ² - (* 14
1FW-165	2 8-5	В	1 GA	AO	• 0/C	FS-1 TM-1 FC-1 P1-5	C		ı		NOTE 2	•
1FW-217	2 D-4	8	16 GA	EH	0	FS-1 TS-1 FC-1 PI-5	Ċ	a 11	CS-1 CS-1 CS-1	FS-2 TS-2 FC-2 PE-1	NOTE 1	
1FW-221	2 D-4	B	1 GA	AO	0/C	FS-1 TM-1 FC-1 PI-5	C				NOTE 2	
1FW-223	2 D-4	8	1 GA	AO	0/C	FS-1 TM-1 FC-1 PI-5	C	,			NOTE 2	



Page 75 of 244

.

SYSTEM: FEEDWATER

NWG.	NO.	21	165-	5-54	1

		1			-	· · · · ·		1	1				
	VALVE NUMBER	CLASS AND DWG	VALVE (CAT.)	SIZE (IN.) AND	ACTU. TYPE	NORM. POSIT.	TEST REQ.	STROKE DIRECT.	CHECK VALVE TEST	C.S. 'JUST. OR RELIEE	C.S. OR ALT. TEST	REMARKS	REV.
'	·	COOR.		TYPE					DIRECT.	REQ.NO.	PERF.		NO.
	1FW-277	2 5-4	8	16 GA	EH	0	FS-1	С		CS-1	FS-2	NOTE 1	
	A			on			FC-1 PI-5			CS-1	FC-2 FC-1	-	
	1FW-279	2 E-4	8	1. GA	AO	0/C	FS-1 TH-1	C			ŗ	NOTE 2	
							FC-1 PI-5						
	1FW-281	2 E-3	B	1 GA	AO	0/C	FS-1 TM-1 FC-1 PI-5	C ,				NOTE 2	
	1FW-307	2 B-6	B	3 GA	AO	тн [́]	FS-1 TM-1 FC-1 P1-5	С			•	NOTE 3	
	1FW-313	2 D-4	B	3 GA [*]	AO	тн	FS-1 TH-1 FC-1 P1-5	C	- •			NOTE 3	×
	1FW-319	2 F-4	B	3 GA	AO	тн	FS-1 TM-1 FC-1 P1-5	С		к Ξ	•	NOTE 3	
	. 5												



.

•

ù,

.

,

x

4 1

PUMP AND VALVE INSERVICE TESTING PROGRAM PLAN

FOR

SHEARON HARRIS NUCLEAR POWER PLANT

SECTION 5.6.8

VALVE TEST TABLES AND RELIEF REQUESTS

· FOR

AUXILIARY FEEDWATER

DWG. NO. 2165-S-544

.

...



• •

.

.

.

.



SYSTEM: AUXILIARY FEEDWATER

NO.

1.

2.

3.

Auxiliary Feedwater Bypass Line to Condensate Storage Tank Line Check Valve. Failure to close would not degrade system operation.

NOTE

- Pump Recirculation to the Condensate Storage Tank Isolation Valve.
- Motor Driven Auxiliary Feed Pump Discharge Check Valve. Reverse flow closure necessary to preclude diversion of flow back across idle pump.
- 4.

Motor Driven Pump Discharge Pressure Control Valves. Valves are installed in the discharge lines of the motor driven pumps and regulate pump discharge pressure to prevent pump damage caused from a runout condition. The valves prevent pump runout by automatically throttling as Steam Generator pressure decreases. Valves are normally open when the system is in standby and automatically throttle in responce to line pressure on initiation.

Motor Driven and Steam Driven Pump Discharge Flow Control Valves. Each of the six Pump discharge lines contains a remote-manually controlled flow control valve. Flow from 0 to 100 Percent is manually selected using remote control logic switches. In addition to flow control, the valve control logic causes the valves to close in each Steam Generator Feedwater Header if a Feedwater Header rupture or Main Steam Header rupture occurs.

6.

7.

5.

Pump Discharge Line Check Valves. Valves prevent cross flow between the motor driven and steam driven pump discharge headers and reverse flow from the Steam Generators back through the pumps. Each flow path contains two check valves in series.

Auxiliary Feedwater Motor-operated Isolation Valves. Valves allow for isolation of each header for maintenance or header rupture.

ISI-203 Rev. 6

Page 78 of 244

, ,

i

· • •

.

ł	

NO.	NOTE
8.	Auxiliary Feedwater Isolation From Normal Feedwater Valves.
9.	Auxiliary Feedwater Isolation From Normal Feedwater Check Valves.
10.	Auxiliary Feedwater Inlet to Steam Generator Check Valves.
11.	Chemical Addition Valves. Valves are normally closed when the system is idle. Chemicals are added as necessary when the system is in operation.





COLD SHUTDOWN TEST JUSTIFICATION

CS-1

System:

Valve:

0S2

Auxiliary Feedwater

1AF-64,81,102

В

2

Category:

Class:

ASME Section XI Quarterly Test Requirements:

Cold Shutdown Test Justification:

Quarterly Part Stroke Testing:

Cold Shutdown[.] Testing. Exercise, Time and Fail.

These six inch valves are normally open and supply eighteen percent of the normal Feedwater to the Steam Generators. Exercising during normal operation would cause Steam Generator transients and would have a significant undesirable effect on plant operations.

Valves are full stroke on initiation and can not be partial stroke exercised.

Exercise, Time and Fail.



ų

:

· #

2

•

.

.

.

-



operability is by operating the motor driven Auxiliary Feedwater pumps and injecting relatively cold condensate water directly into the hot Steam Generators. The introduction of cold water into the hot Steam Generators during normal operation would result in large thermal shock to the Feedwater Nozzles which could cause cracking of the nozzles. In addition, to test Auxiliary Feedwater during normal operation would require starting the Auxiliary Feedwater pumps and securing the normal Feedwater System flow, which would have an adverse effect on Steam Generator water level control and could cause a forced plant shutdown. Quarterly pump testing is done through the pump recirculation lines and the downstream flow control valves automatically close so that the pumps are essentially isolated from each other and reverse flow closure of these pump discharge check valves can not be verified until full Auxiliary Feedwater flow is injected into the Steam Generators.

Verify forward flow operability and reverse flow closure on a cold shutdown frequency when full flow test is performed on motor driven auxiliary feed pumps.

Alternate Testing:

System:

Valve:

Class:

Test

Relief:



ISI-203 Rev. 6

Page 81 of 244

.

۵ ٦ F

. i

. .

•

. à

a.

•

COLD SHUTDOWN TEST JUSTIFICATION

CS-3

System:

Auxiliary Feedwater

В

3

1AF-19,34,49,50,51,129,130,131

Valve:

Category: Class:

Function:

1AF-19,34: Auxiliary Feedwater Pump Discharge Pressure Control Valves. 1AF-49,50,51,129,130,131: Auxiliary Feedwater Pump Discharge Flow Control Valves.

[.]Test Requirement:

Basis for Relief:

Alternate Testing:

Exercise, Time, and Fail

Position of these valves is automatically modulated during pump operation to control Auxiliary Feedwater flow rate. To test these valves would require use of control logic defeating methods, such as temporary jumpers. In order to minimize the impact on the auxiliary feedwater system by forcing these valves to their non fail safe position, valve testing will be performed on a cold shutdown frequency.

Exercise; time and fail on a cold shutdown frequency.



COLD SHUTDOWN TEST JUSTIFICATION

CS-4

C

3

System:

Auxiliary Feedwater

1AF-54,73,92,201,202,203

discharge check valves:

Valve:

Category:

Class:

Function:

Test Requirements:

Basis for Relief:

Alternate Testing:

Verify forward flow operability.

Motor driven Auxiliary Feedwater Pump

The only way to verify forward flow operability is by operating the motor driven Auxiliary Feedwater pumps and injecting relatively cold condensate water directly into the hot Steam Generators. The introduction of cold water into the hot Steam Generators during normal operation would result in large thermal shock to the Feedwater Nozzles and could cause cracking of the nozzles. In addition, to test the Auxiliary Feedwater during normal operation would require starting the Auxiliary Feedwater pumps and securing the normal Feedwater System flow, which would have an adverse effect on Steam Generator water level control and could cause a forced plant shutdown.

Verify full forward flow operability at cold shutdown when the Auxiliary Feedwater Pumps are being full flow tested.



CS-5

С

3,

valves.

System:

Valve:

Auxiliary Feedwater

1AF-117, 136, 142, 148, 204, 205, 206

Steam driven Auxiliary Feedwater pump line to Steam Generator series check

Category:

Class:

Function:

Test Requirement:

Basis for Relief:

Verifiy forward flow operability.

These valves can only be forward flow operability tested by operation the steam driven pumps and injecting full flow into the Steam Generators, which can not be done during normal operations (See CS-2). The only source of steam to the steam driven turbine is from the Main Steam System. To operate the turbine requires that the Steam Generators be producing sufficient steam to drive the turbine. Control of Steam Generator water level when producing steam is much more critical than during the refilling process, where the motor operated pumps are tested. To perform flow testing during steam production would have a significant impact on Steam Generator water level control on all three Steam Generators, would require a significant amount of startup time and could result in a forced plant shutdown.

Alternate Testing:

Perform full forward flow operability testing of these values during full steam driven pump testing on a cold shutdown frequency when the impact on plant operations will be minimized.



COLD SHUTDOWN JUSTIFICATION

CS-6

1AF-117

C

3

Auxiliary Feedwater

System: Valve:

_

Category: Class:

Function:

Test Requirements:

Basis for Relief:

The system has no design provision for verification of reverse flow closure. The only possible test method involes pressurizing the downstream section of pipe and monitoring an upstream tap for evidence of gross leakage performing this at power could result in a loss of steam generator level control and could cause a plant shutdown.

1C-SAB Discharge Check Valve

Verify reverse flow closure.

Alternate Testing: Verify reverse flow closure on a cold shutdown frequency when test can be performed with little impact on plant condition.

ISI-203 Rev. 6

Page 85 of 244
RELIEF REQUEST

<u>RV-1</u>

Auxiliary Feedwater

System:

1AF-65, 84, 103

Valve:

. Class:

Category:

С

2

Function:

Auxiliary Feedwater Isolation From Normal Feedwater Line Check Valves.

Test Requirements:

Basis for Relief:

Alternate Testing:

Verify reverse flow closure.

The system has no design provision for verification of reverse flow closure. The only possible test method involes pressurizing the downstream section of pipe and monitoring an upstream tap for evidence of gross leakage. This method involves filling and draining large segments of the system. Because of the time involved, ALARA consideration and large amounts of wastes, it is not practical to perform testing execpt at refueling. The only other alternative testing is to disassemble and visually inspect each valve.

One valve will be disassembled and visually inspected at each refueling, and alternate valves will be done during subsequent refuelings. Failure to pass inspection will initiate disassembly and inspection of the other two valves.



τ.

VALVE

RELIEF REQUEST

RV-2

Auxiliary Feedwater

204, 205, 206

1AF-201, 202, 203

C

3

System:

Valve:

Category:

Class:

Function:

Test Requirement:

Basis for Relief:

Alternate Testing:

Auxiliary Feedwater Pump Discharge Line to Feedwater Line Check Valves.

Verifiy reverse flow closure.

The system has no design provision for verification of reverse flow closure. The only possible test method involes pressurizing the downstream section of pipe and monitoring an upstream tap for evidence of gross leakage. This method involves filling and draining large segments of the system. Because of the time involved, ALARA consideration, and large amounts of wastes, it is not practical to perform testing execpt at refueling. The only other alternative testing is to disassemble and visually inspect each valve.

During normal plant operation The valves 1AF-201, 202, 203, 204, 205, and 206 will be verified to be in the closed position through the continual monitoring of installed temperature elements. Unacceptable conditions require action in accordance with Plant Operating Procedure. In addition 1 valve off of the Motor Driven Train and 1 valve off Turbine Driven Train will be disassembled and inspected at each refueling, and alternate valves will be done during subsequent refuelings. Failure to pass inspection will initiate disassembly and inspection of the other valves on the same train.

052

Page 87 of 244

SYSTEM: AUXILIARY FEEDWATER

DWG. NO. 2165-5-544

			The second second second second second second second second second second second second second second second se				_					
VALVE NUMBER	CLASS AND DWG.	VALVE (CAT.)	SIZE (IN.) AND	АСТИ. ТҮРЕ	NORM. POSIT.	TEST REQ.	STROKE DIRECT.	CHECK VALVE TEST	C.S. JUST. OR RELIEF	C.S. OR ALT. TEST	REMARKS	REV.
	COOR.		TYPE					DIRECT.	RĘQ.NO.	PERF.		1.01
1AF-4	3 N-6	С	2 CK	• SA	C	FS-1		FF			NOTE 1	_ !
ÌAF-5	3 N-6	B	2 GL	мо	0	FS-1 TM-1 P1-5	C				NOTE 2	
1AF-16	3 L-6	C	4 CK	SA	С	FS-1 85-1		FF BS	CS-2 CS-2	FF-2 85-2	NOTE 3	
1AF-19	3 K-6	В	4 GL	EH	0	FS-1 F0-1 P1-5			CS-3	FS-2 F0-2	NOTE 4	•
1AF-23	3 N-9	C	2 CK	SA	C	FS-1		FF	•		NOTE 1	
1AF-24	3 N-9	B	2 GL	мо	0	FS-1 TM-1 P1-5	Ċ				NOTE 2	
1AF-31	3 L-8	C	4 CK	SA	C	FS-1 BS-1		FF BS	CS-2 CS-2	FF-2 85-2	NOTE 3	
1AF-34	3 K-8	8	4 GL	EH	0	FS-1 F0-1 P1-5			CS-3	FS-2 F0-2	NOTE 4	
1AF-49	3 - J - 6	B	4 GL	EH	· 0	F0-1 P1-5 FS-1 TM-1	C		CS-3	F0-2 FS-2 TM-2	'NOTE 5	

ISI-203 Rev. 6

.

•

•

*

SYSTEM: AUXILIARY FEEDWATER

DWG. NO. 2165-	<u>s-544</u>				•					<u> </u>		
VALVE NUMBER	CLASS AND	VALVE (CAT.)	SIZE	· ACTU. TYPE	NORM. POSIT.	TEST REQ.	STROKE	CHECK	C.S. JUST. OR	C.S. OR ALT.	REMARKS	REV.
	DWG. COOR.		AND, TYPE			ه. 		TEST DIRECT.	RELIEF REQ.NO.	TEST PERF.		NO.
1AF-50	3 J-7	В	4 GL	EH	0	F0-1 FS-1 TH-1	C		CS-3	F0-2 TM-2 FS-2	NOTE 5	
1AF-51	3 J-8	8	4 GL	ЕН	0	P1-5 F0-1 FS-1	C		CS-3	F0-2 FS-2	NOTE 5	
1AF-54	,	C	4	SA	С	PI-5		FF	CS-4	FF-2	NOTE 6	
145 FF	F-6	•	СК		0	F6_1	0			•• -	NOTE 7	
186-22	2 F-6	В	4 GA	мо	Ū	75-1 TS-1 PI-5	C				NOTE 7	
1AF-64	2 C-6	B	6 GA	AO	0 、	FS-1 TM-1 FC-1 P1-5	С		CS-1 CS-1 CS-1	FS-2 TM-2 FC-2	NOTE 8	
1AF-65	2 C-6	С	6 СК	SA	0	FS-1		BS	RV-1	DS SP-3	NOTE 9	
1AF-68	2 C-2	C	6 CK	SA ,	0	FS-1		FF		, *	NOTE 10	•
1AF-73	3 [.] H-7	C	4 CK	SA	C	FS-1		FF	CS-4	FF-2	NOTE 6	
1AF-74	2 G-7	B	. 4 GA	МО	°O	FS-1 TS-1 P1-5	Ç	•			NOTE 7	

ISI-203 Rev. 6

. × 、 ч Ч r a

SYSTEM: AUXILIARY FEEDWATER

DWG. NO. 2165-5-544

	<u> </u>				r							
	1	1							C.S.	c.s.		
	CLASS	VALVE	SIZE	ACTU.	NORM.	TEST	STROKE	CHECK	JUST.	OR	REMARKS	REV.
.VALVE NUMBER	AND	(CAT.)	(IN.)	TYPE	POSIT.	REQ.	DIRECT.	VALVE	OR	ALT.		
	DWG.		AND			-		TEST	RELIEF	TEST		NO.
1	COOR.	•	TYPE					DIRECT.	REO.NO.	PERF		
				-								
· · · · · · · · · · · · · · · · · · ·								·	· · ·			
1AF-81	2	В	6	AO	0	FS-1	С		CS-1	FS-2	NOTE 8	
	E7		GA			TM-1		1	CS-1	TM-2		
						FC-1			CS-1	FC=2		
					•	P1-5						
					,							
1AF-84	່ 2	С	6	SA	0.	FS-1		BS	RV-1	פת	WOTE O	
	E-5		СК							SP-3		
						,			•	51 -5		
1AF-87	2	С	6	SA	0	FS-1		FF			NOTE 10	
	K-2		Ċĸ		•			••				
							٠				•	
1AF-92	3	С	4	SA	С	FS-1		FF	CS-4	FF-2	NOTE 6	
	1-8	۴	ĊK		-			••		11-2	NOTE O	
			+								a	•
1AF-93	2	B	4	мо	ດ່	ES-1	C	*			NOTE 7	,
	H-8	-	GA		•	' TS-1	U		•		, MUIC /	
						PI-5						
			•			11-5						
1AF-102	2	в	6	AO	0	ES-1	C		1-23	55-2	NOTE O	
	F-4	-	GA		•	TM-1	U		00-1 00-1	FJ-2 TV-2	MOLE O	
	• •					FC-1				1M-2		
						FC-1 D1_5			ယ-I	FC-2		
						r (=)						
1AF-103	2	C	6	C A	٥	E		DC	DV 1	00		
	- -	Ŭ	CY CY	34	v	r3-1		53	KV-1	05	NOTE 9	
	F - 4		^{cn}							SP-3		
1AF-106	2	c	6	CA	•	56-1		~~				
174 ×100	6-2	5	о су.	37	v	r3 - 1		rr			NOTE 10	
	0-2			·								
1AF-110	٦	c	2	SA	c	56-1						
	N-11	U	- CY	37	U	r3 -1		rr			NOTE 1	
	11 11		UN			•						





Page 90 of 244

.

0S2

۰ ۱

, , . v

,

,

SYSTEM: AUXILIARY FEEDWATER

DWG. NO. 2165-5-544 c.s. c.s. • REV. CLASS VALVE SIZE ACTU. NORM. TEST STROKE CHECK JUST. OR REMARKS VÁLVE NUMBER AND (CAT.) (IN.) TYPE POSIT. REQ. DIRECT. VALVE OR ALT. DWG. AND TEST RELIEF TEST NO. COOR. TYPE DIRECT. REQ.NO. PERF. С 1AF-117 C FS-1 FF FF-2 3. 6 SA CS-5 NOTE 6 L-10 CK 8S-1 **8**S CS-6 3 EH 0 F0-1 CS-3 F0-2 1AF-129 8 4 С NOTE 5 J-9 GL FS-1 FS-2 , TH-1 TM-2 PI-5 3 8 EH 0 F0-1 F0-2 NOTE 5 1AF-130 4 C CS-3 J-10 GL FS-1 FS-2 -TH-1 TM-2 PI-5 EH 3 0 F0-1 CS-3 F0-2 NOTE 5 1AF-131 в 4 C J-1,1 GL FS-1 FS-2 TH-1 TM-2 P1-5 3 1AF-136 С 4 SA C FS-1 FF CS-5 FF-2 NOTE 6 F-6 CK 1AF-137 2 8 4 MO 0 FS-1 С NOTE 7 F-6 GA TS-1 PI-5 FF-2 1AF-142 4 SA C FS-1 FF 3 С CS-5 NOTE 6 H-9 CK 2 0 ' FS-1 С NOTE 7 1AF-143 4 МО В TS-1 H-9 GA P1-5 1AF-148 3 °C 4 SA C FS-1 FF CS-5 FF-2 NOTE 6 . H**-7** CK 1AF-149 2 8 4 MO 0 FS-1 С NOTE 7 G-7 GA TS-1 . P1-5 2 C FS-1 NOTE 11 1AF-153 B 1 AO C 8-4 GA TH-1 - FC-1 . P1-5

' ISI-203 Rev. 6

Page 91 of 244

0S2 .

•

SYSTEM: AUXILIARY FEEDWATER

DWG. NO. 2165-5-544 c.s. c.s. . ACTU. TEST STROKE REV. CLASS VALVE SIZE NORM. CHECK JUST. OR REMARKS VALVE NUMBER DIRECT. AND (CAT.) (IN.) TYPE POSIT. REQ. VALVE OR ALT. DWG. AND TEST RELIEF TEST NO. DIRECT. REQ.NO. COOR. TYPE PERF. . 1AF-155 2 FS-1 С NOTE 11 В 1 ٨٥ C B-3 GA TH-1 FC-1 P1-5 •2 C` 1AF-157 FS-1 8 1 AO C NOTE 11 GA TH-1 G-4 FC-1 PI-5 1AF~159 2 FS-1 B 1 ٨0 C С NOTE 11 TH-1 G-3 GA FC-1 P1-5 2 ' FS-1 Ċ 1AF-161 1 С 8 ٨0 NOTE 11 -GA TH-1 K-4 FC-1 P1-5 1AF-163 2 8 1 AO С FS-1 С NOTE 11 K-3 GA _TM-1 FC-1 PI-5 1AF-201 FS-1 CS-4 FF-2 NOTE 9 3 SA C FF C 4 H-5 CK 8S-1 **8**\$ RV-2 DS 4 ' 1AF-202 3 FS-1 FS CS-4 FF-2 C SA C NOTE 9 1-8 8S-1 RV-2 DS CX **BS** • FF-2 1AF-203 3 - C 4 SA C **FS-1** FS CS-4 NOTE 9 • 1-6 CK 8S-1 BS RV-2 DS . . FF-2 1AF-204 3 C 4 SA C FS-1 FS CS-5 NOTE 9 H-7 CK 8S-1 . BS RV-2 OS 1AF-205 3 , C 4 SA С FS-1 FS CS-5 FF-2 NOTE 9 H-10 CK 8S-1 **B\$** RV-2 DS 1AF-206 3 C 4 SA С FS-1 FS CS-5 FF-2 NOTE 9 BS RV-2 CX BS-1 DS H-11 . ..

ISI-203 Rev. 6

Page 92 of 244

0S2

•

•

,

4

r

, ,

•

1

•

PUMP AND VALVE INSERVICE TESTING PROGRAM PLAN

FOR

SHEARON HARRIS NUCLEAR POWER PLANT

SECTION 5.6.9

VALVE TEST TABLES AND RELIEF REQUESTS

FOR

CONDENSATE

DWG. NO. 2165-S-545

SYSTEM:	CONDENSATE	
Ŀ	<u>NO.</u>	NOTE
•	1.	Condensate Storage Tank to Auxiliary Feedwater Pump Inlet Check Valves. Reverse flow closure required to prevent flow of service water into the Condensate Storage Tank.
	2.	Relief Valves which protect the Low Pressure Suction piping from back leakage across the Pump Discharge Check Valves.

ISI-203 Rev. 6

Page 94 of 244

COLD SHUTDOWN TEST JUSTIFICATION

CS-1

System:

Valve:

Condensate

1CE-36,46,56

Category:

Class:

Function:

Condensate Storage Tank to Auxiliary Feedwater Pump Inlet Check Valves.

Test Requirements: Verify forward flow operability.

С

3

Basis for Relief:

Alternate Testing:

The only way to verify full forward flow operability is by operating the motor driven Auxiliary Feedwater pumps and injecting relatively cold condensate water directly into the hot Steam Generators. The introduction of cold water into the Steam Generators during normal operation would result in large thermal shock to the Feedwater Nozzles and could cause cracking of the

nozzles. In addition to test the Auxiliary Feedwater during normal operation would require starting the Auxiliary Feedwater pumps and securing the normal Feedwater System flow, which would have an adverse effect on Steam Generator water level control and could cause a forced plant shutdown.

Valves will be partial stroke exercised during quarterly pump testing with flow through the small pump recirculation line back to the Condensate Storage Tank. Valves will be full flow exercised on the way to cold shutdown when the Aux. Feed System is in operation.

ISI-203 Rev. 6

RELIEF REQUEST

RV-1

Condensate

C

3

System:

0S2 ·

1CE-36,46,56

Valve:

Category:

Class:

Function:

Condensate Storage Tank to Auxiliary Feedwater Pump Inlet Check Valve which prevents back-flow from the Service Water System into the Condensate Storage Tank.

Test Requirements:

Basis for Relief:

Alternate Testing:

Verify reverse flow closure.

These valves are in the line from the Condensate Storage Tank to the Auxiliary Feedwater Pump Inlet and are upstream from the ross-tie with the Service Water System. In this location the valves prevent back-flow from the Service Water System into the Condensate Storage Tank. The only possible method to verify reverse flow closure would be by monitoring for a increase in tank level. This technique is not possible in this case because of the volume of the tank and the normal level changes which occur during normal operation.

One valve will be disassembled and visually inspected at refueling and alternate valves will be done during subsequent refuelings. Only one valve will be inspected at a refueling unless it fails to pass inspection. Failure to pass inspection will initiate disassembly and inspection of the other two valves.

Page 96 of 244.

(

SHEARON HARRIS NUCLEAR POWER PLANT . VALVE TEST TABLE

SYSTEM: CONDENSATE

DWG. NO. 2165-5-545

VALVE NUMBER	CLASS AND DWG. COOR.	VALVE (CAT.)	SIZE (IN.) AND TYPE	ACTU. TYPE	NORM. , POSIT.	TEST REQ.	STROKE DIRECT.	CHECK VALVE TEST DIRECT.	C.S. JUST. OR RELIEF REQ.NO.	C.S. OR ALT. TEST PERF.	REMARKS	REV.
1CE-36	3 H-7	C	6 CK	SA	C	FS-1 FS-1 BS-1	* <u> </u>	FF FF BS	CS-1 CS-1 RV-1	FF-2 PE-1 DS	NOTE 1	
1CE-46	3 H-8	C	6 CK	SA	C	FS-1 FS-1 BS-1		FF FF BS	CS-1 CS-1 RV-1	FF-2 PE-1 DS	NOTE 1	
1CE-56	3 H-9	с	8 CK	SA	C	FS-1 FS-1 BS-1		FF FF BS	CS-1 CS-1 RV-1	FF-2 PE-1 DS	NOTE 1	
1CE-1157	3 1-7	C	1X1 RL	SA	С	RL-4		¥			NOTE 2	•
1CE-1 158	3 1-8	C	IX1 RL	SA	C	RL-4					NOTE 2	
1CE-1159	3 1-9	С	1X1 RL	SA	C	RL-4		đ	,		NOTE 2	

PUMP AND VALVE INSERVICE TESTING PROGRAM PLAN

FOR

SHEARON HARRIS NUCLEAR POWER PLANT

SECTION 5.6.10

VALVE TEST TABLES AND RELIEF REQUESTS

FOR

SERVICE WATER

DWG. NO. 2165-S-547 2165-S-588 2165-S-936

Page 98 of 244

ISI-203 Rev. 6

`

4

x

0S2

		•
SYSTEM:	SERVICE WATER	•
	NO.	NOTE
	1.	Pump Discharge Check Valves. Valves prevent backflow through the pumps.
	2.	CTMU Pump Inlet Isolation Valves.
,	3.	Cross-tie to Normal Service Water Isolation Valves.
	4.	Valves Close to Isolate Non-Safety- Related Loads.
	5.	Thermal Relief Valve added to Program to comply with North Carolina State Requirements.
	6.	Emergency Service Water to Containment Fan Coolers Check Valve. Reverse flow closure to prevent drain back from the coolers.
·	7.	Emergency Service Water to Containment Fan Coolers Isolation Valves.
	8.	Orifice Bypass Valve. 'Valve closes on system initiation.
	9.	Back-up Water Supply to the Auxiliary Feedwater Pumps.
	10 .	Charging Pump Oil Cooler Check Valves. Reverse flow closure is not required to prevent cross-flow between Emergency Service Water Headers. Valves are 1 1/2 inch and if they fail to close the amount of water diverted from the operating to non-operating header would not be great enough to cause significant degradation of system operation.
	11	Normal Service Water to the Non-Safety- Related Containment Fan Coolers. Can only be tested when the Emergency Service Water system is in operation with flow

12.

Normal Service Water to Non-Safety-Related Containment Fan Coolers inside Containment Isolation Check Valve. Reverse flow closure for Containment isolation.

through the Emergency Containment Fan Coolers Containment Isolation Valve.



SYSTEM: SERVICE WATER

0S2

NO.

NOTE

Return Header Isolation Valves.

14.

13.

Normal CTMUP and ESW Water soures for ESW Intake Structure Fan Coolers. Valves are controlled by local temperature elements and as such are temperature control valves, exempt from Section XI test requirements. Normal CTMUP isolates and ESW source initiates on loss of site power or LOCA condition. Valves are tested for fail-safe operation only.



Page 100 of 244

فه

• • ,

۰

. ,

×

VALVE

RELIEF REQUEST

<u>RV-1</u>

System:

SERVICE WATER

AC

2

Valve: 1SW-233

Category:

Basis for Relief:

Class:

Function:

Normal Service Water System Inside Containment Isolation Check Valve

Test Requirements:

Verify reverse flow closure.

The only method available to verify reverse flow closure is by valve leak testing during Appendix J, Type C, Testing at refueling.

Alternate Testing:

Reverse flow closure will be verified during Appendix J, Type C, Testing at refueling.



0S2

SYSTEM: SERVICE WATER

DWG. NO. 2165-5-547

VALVE NUMBER	CLASS AND DWG. COOR.	VALVE (CAT.)	SIZE (IN.) AND TYPE	ACTU. TYPE	NORM. POSIT.	TEST REQ.	STROKE DIRECT.	CHECK VALVE TEST DIRECT.	C.S. JUST. OR RELIEF REQ.NO.	C.S. OR ALT. TEST PERF.	REMARKS	REV. NO.
- 15W-9	3 E-2	С	30 CK	SA	C	FS-1 85-1		FF BS			NOTE 1	
1SW-10	3 E3	C	30 CK	SA	C	FS-1 85-1		FF BS			NOTE 1	
15W-20	3 F-1	8	3 BA	P0 _.	0/C	FS-1 TM-1 F0-1 PI-5	0				NOTE 2	
1SW-23	3 F-4	B	3 BA	PO	0/C	FS-1 TH-1 F0-1 P1-5	0				NOTE 2	
1SW-39	3 I-1	B	30 BF	мо	0/C	FS-1 TM-1 81-5	0 C				NOTE 3	

0S2

• 1

SYSTEM: SERVICE WATER

DWG. NO. 2165-S-547

VALVE NUMBER	CLASS AND DWG. COOR.	VALVE (CAT.)	SIZE (IN.) AND TYPE	ACTU. TYPE	NORM. POSIT.	TEST REQ.	STROKE DIRECT.	CHECK VALVE TEST DIRECT.	C.S. JUST. OR RELIEF REQ.NO.	C.S. OR ALT. TEST PERF.	REMARKS	REV. NO.
15W-40	3 I-2	B	30 BF	Ю	0/C	FS-1 TM-1 PI -5	. 0 C				NOTE 3	4
15W-60 -	3 1-6	C	3/4X1 RL	RL 🕚	С	RL-4					NOTE 5	
1SW-86	3 F-6	С	14 - CK	, SA	0/C	FS-1 BS-1		FF BS			NOTE 6	•
1SW-91	2 C-6	B	8 BF	мо	0	FS-1 TS-1 P1-5	0 C		1		NOTE 7	•
15W-92 .	2 C-7	8	8 BF	МО	0	FS-1 TS-1 PI-5	0 . C				NOTE 7	•
1SW-97	2 C-8	8	8 8F.	MO	0	FS-1 TS-1 PI-5	0. C				NOTE 7	
1SW-98	2 C-9	B	8 BF	мо	0	FS-1 TS-1 P1-5	o C				NOTE 7	
1SW-95	2 C-8	C ,	IXI‡ RL	SA	С	RL-4					NOTE 5	
1SW-96	2. C-9	C	1X1 1 RL	SA	С	RL-4					NOTE 5	•







,

SHEARON HARRIS NUCLEAR POWER PLANT VALVE TEST TABLE

SYSTEM: SERVICE WATER

0S2

DWG. NO. 2165-5-547

	224 17		\$175	ACTU	NOON	TEST	STOOKE	OUE OV	C.S.	C.S.		
VALVE NUMBER	AND	(CAT.)		TYPE	POSIT	PEO	DIRECT	VALVE	1051.		REMARKS	REV.
	DWG	(031.)		1165	FUSTI.	REQ.	DIRECT.	TECT		ALI.		
-	C008.	•	TYPE				1	DIRECT	RELIEF	1251		NO.
	000111							DIRECI.	REV.NU.	PERF.	•	
- 1SW-109	2	в	8	мо	0	ES-1	0				NOTE 7	
	C-12	-	8F		, U	TS-1	Ċ				NUTE /	
				,		PI-5	Ŭ					
`												
1SW-110	2	в	8	мо	0	FS-1	0				NOTE 7	
	C-13		BF			TS-1	Ċ					
						PI-5	-					
1SW-116	3	В	14	AO	0	FS-1	С				NOTE 8	
	H-7		BF			TM-1						
		•				FC-1						
						P1-5						
												•
1SW-118	3	в	14	AO	0	FS-1	C				NOTE 8	
	G-13		8F			TM-1						
						FC-1						
			-			PI-5						
	-	-										
124-121	،د م	в	8	мо	C	FS-1	0				NOTE 9	
	1-8		BF			TM-1	С					
-						P1-5						
1SW-123	3	8	8	мо	. с	ES-1	0			-	NOTE O	
	J-8		8F		-	TM-1	c					
•						P1-5	•			•		
							n					
1SW-124	3	в	8	МО	C	FS-1	0				NOTE 9	
		1-8		BF		TM-1	С					
						P1-5					•	
	•											
1SW-126	3	8	8	мо	C	FS-1	0				NOTE 9	
	1-8		BF			TM-1	ç					
						P1-5	•					
1SW-127	3	B	8	мо	C	ES-1	0.				NOTE O	
	1-9	-	BF		v	. J=1	Ċ				WULE A	
	• •					PI-5	C					

ISI-203 Rev. 6

SYSTEM: SERVICE WATER

DWG. NO. 2165-S-547

DWG. NO. 2165-	<u>-547</u>					-						
VALVE NUMBER	CL'ASS AND DWG. COOR.	VALVE (CAT.)	SIZE (IN.) AND TYPE	ACTU. TYPE	NORM. POSIT.	TEST REQ.	STROKE DIRECT.	CHECK VALVE TEST DIRECT.	C.S. JUST. OR RELIEF REQ.NO.	C.S. OR ALT. TEST PERF.	REMARKS	REV.
 1SW-129	3 I-9	В	8 BF	МО	C	FS-1 TM-1 P1-5	o C				NOTE 9	N
1SW-130	3 1-9	В	8 BF	мо	С	FS-1 TM-1 P1-5	0 C				NOTE 9	
15W-132	3 J-10	B	8 BF	мо	С	FS-1 TM-1 P1-5	0 C	· .			NOTE 9	
1SW-141	3 H-8	C	1 1/2 CK	SA	0/C	FS-1,		FF			NOTE 10	•
1Ś₩-143	3 H-9	· C	1 1/2 CK	sa sa	0/C	FS-1		FF	•		NOTE 10	
1SW-152	3 H-10	C	1 1/2 CK	SA	0/C	FS-1		FF			NOTE 10	
1SW-154	3 H-11	C	1 1/2 CK	SA	0/C	FS-1		FF			NOTE 10	
1SW-163	3 H-11	C	1 1/2 CK*	SA	0/C	FS-1		FF			NOTE 10	
1SW-165	3 H-12	C	1 1/2 CK	SA	0/C	FS-1		FF			NOTE 10	, ,
1SW-107	2 C-12	C	1X1 1 RL	SA	с	RL-4					NOTE 5	
1SW-108	2 C-13	C	1X1 1 RL	SA	C	RL-4	•	-			NOTE 5	,



SYSTEM SERVICE WATER

DWG. NO. 2165-5-547

<u> </u>	<u> </u>						· · · · · · · · · · · · · · · · · · ·					
VALVE NUMBER	CLASS AND DWG. COOR.	VALVE (CAT.)	SIZE (IN.) AND TYPE	ACTU. TYPE	NORM. POSIT.	TEST REQ.	STROKE DIRECT.	CHECK VALVE TEST DIRECT.	C.S. JUST. OR REL1EF REQ.NO.	C.S. OR ALT. TEST PERF.	REMARKS	REV. NO.
ISW-171	3 F-11	С	3/4X1 RL	SA	С	RL-4	•	Ŧ			NOTE 5	
1SW-179	3 I-15	B	4 GA	PO	0	FS-1 TM-1 FC-1 PI-5	С				NOTE 4	
1SW-180	3 I-15	B	4 GA	PO	0	FS-1 TM-1 FC-1 P1 -5	C				NOTE 4	
1SW-204	3 K-16	B	4 GA	P0	0	FS-1 TM-1 FC-1 P1-5	С				NOTE 4	•
15W-206	3 K-16	В	4 GA	P0	0 .	FS-1 TM-1 FC-1 P1-5	С	,			NOTE 4	
, 15 W-220	3 F-6	.с	14 CK	SA	0/C	FS-1 BS-1		FF BS	х,		NOTE 6	1
1SW-225	2 C-14	B	8 8F	мо	0	FS-1 TS-1 PI-5	0 C				NOTE 7	
ISW-227	2 C-14	B	8 BF	MO	0	FS-1 TS-1 P1-5	O C	•			NOTE 7	
15W-231	2 C-15	A	12 8F	AO	0	FS-1 TS-1 FC-1 P1-5 LJ-3	C.		,	٩	NOTE 11	

ISI-203 Rev. 6

۱

Page 106 of 244

£

τ. .

۰ ۲ ۲ ۲ ۲

SYSTEM: SERVICE WATER

DWG. NO. 2165-5-547

JIG: IQ: 2103-	-3-341						1					
VALVE NUMBER	CLASS AND DWG. COOR.	VALVE (CAT.)	SIZE (IN.) AND TYPE	ACTU. TYPE	NORM. POSIT.	TEST REQ.	STRÓKE DIRECT.	CHECK VALVE TEST DIRECT.	C.S. JUST. OR RELIEF REQ.NO.	C.S. OR ALT. TEST PERF.	REMARKS	REV. NO.
1SW-233	2 C-15	AC	12 CK	SA	0	FS-1 LJ-3		BS	RV-1	SP-3	NOTE 12	
1SW-240	2 D-17	۸	12 BF	AO	0	FS-1 TS-1 FC-1 P1-5 LJ-3	С	·	-		NOTE 11	
1SW-242	2 E-17	A	12 BF	AO	0	FS-1 TS-1 FC-1 PI-5 LJ-3	С				NOTE 11	•
1SW-257	3 I-13	C	3/4X1 RL	SA	c	RL-4					NOTE 5	
- 1SW-270	3 K-16	B	30 BF	Ю	С	FS-1 TM-1 P1-5,	o C				NOTE 13	
1SW-271	3 J-16	B	30 BF	мо	C `	FS-1 TM-1 P1-5	0 C				NOTE 13	•
15 ₩-274 ,	3 L-16	В	30 8F	мо	0	FS-1 TM-1 P1-5	0 C				NOTE 13	
1SW-275	3 L-16	B	30 8F	МО	0	FS-1 TM-1 P1-5	0 ·				NOTE 13	
1S₩-276	3 M∸15	8	36 BF	МО	0	FS-1 TM-1 P1-5	o C				NOTE 13	



ſ



Page 107 of 244

SYSTEM: SERVICE WATER

DWG. NO. 2165-5-588

VALVE NUMBER	CLASS AND DWG. COOR.	VALVE (CAT.)	SIZE (IN.) AND TYPE	ACTU. TYPE	NORM. POSIT.	TEST REQ.	STROKE DIRECT.	CHECK VALVE TEST DIRECT.	C.S. JUST. OR RELIEF REQ.NO.	C.S. OR ALT. TEST PERF.	REMARKS	REV. NO.
1MP-70	3 C-18	B	• 2 GL	SO	0	FC-1 PI-5	C	<u></u>		<u>.</u>	NOTE 14	
1MP-71	3 C-19	B	2 GL	SO	Ģ	FC-1 1 P1-5	C				NOTE 14	
1SW-1000	3 C-18	8	2 GL	SO	С	F0-1 P1-5	0				NOTE 14	
1SW-1001	3 C-19	B	2 GL	SO	C	F0-1 P1-5	0				NOTE 14	
1SW-150	3 F-8	C	3/4X1 RL	SA	C	RL-4	v			1	NOTE 5	•
1SW-160	3 F-8	С	3/4X1 RL	SA	C	RL-4			2		NOTE 5	

PUMP AND VALVE INSERVICE TESTING PROGRAM PLAN

FOR

SHEARON HARRIS NUCLEAR POWER PLANT

SECTION 5.6.11

VALVE TEST TABLES AND RELIEF REQUESTS

.

FOR

CONTAINMENT SPRAY

DWG. NO. 2165-S-550





N

SYSTEM:	CONTAINMENT SP	RAY
	NO.	NOTE
	.1.	Relief Valve which protects Safety-Related Equipment.
۶	2.	NaOH Additive Valves. Valves open on CSAC signal and close on low tank level.
	3.	CTMT Spray Eductor Test Valves. Valves close on system initiation.
	4.	RWST to Pump Inlet Block Valves. Valves close on switch over to recirculation mode.
	5.	RWST to Pump Inlet Check Valves. Test line is large enough to verify full design forward flow. The Recirculation and RWST Block Valves are interlocked and can not be open at the same time. Thus, reverse flow closure of these check valves is not required.
×	6.	Pump Test Line to RWST Block Valves. Valves close on system initiation.
	7• ·	Containment Isolation Valves.
	8.	NaOH Injection Check Valves. Reverse flow closure is required to separate headers, since both motor operated block valves open on initiation.
	9.	Containment Sump Isolation Valves. Valves open for Recirculation operating mode and close for CTMT isolation. Cycling will drain system water into the Stainless Steel sumps.
	10.	Spring loaded check values used as vacuum brakers on the Spray Additive Tank. Values open with a 0.17 Psid (maximum) across the values. They will be treated and tested in a manner similar to relief values. At each refueling, one of the values will be tested. Failure of value to pass test will result in other value being tested.

C

ISI-203 Rev. 6

,
COLD SHUTDOWN TEST JUSTIFICATION

CS-1

System:

CONTAINMENT SPRAY

1CT-102,105

В

2

Valves.

Valve:

Category:

Class:

Function:

;

Test Requirements:

Basis for Relief:

Exercise and Time

Exercising these valves, even with the in-line block valves closed, would result in a small amount of water being drained into the Containment Sump. This highly oxygenated, stagnant water could result in excessive corrosion of the sump structure. The amount of water is insufficient to insure adequate pump NPSH so it can not be removed with the system pumps. There are no provisions for removing the water except by a temporary sump pump and entering the sump to hand dry the wetted surfaces.

Containment Recirculation Sump Isolation

Alternate Testing:

Exercise and Time at cold shutdown when sump water can be removed.



VALVE

RELIEF REQUEST

RV-1

System:

CONTAINMENT SPRAY

reverse flow closure.

Containment Spray System Inside Containment Isolation Check Valves.

Verify forward flow operability and

AC

2

Valve: 1CT-53,91

Category:

Class:

Function:

Test Requirements:

Basis for Relief:

Alternate Testing:

Since there is no test recirculation line the only way to verify forward flow operability would be by using the pumps and injecting a large quantity of water into the Containment. Spraying the Containment would result in extensive damage to safety-related equipment located inside Containment. Using air as a test medium is not practical since large segments of the system would have to be drained and high pressure air pumped into the system through a small test connection. The amount of air that could be injected using this method would be insufficient to verify full stroke opening and could result in an overpressurization of the Containment structure. The only method available to verify leak testing during Appendix J. Type C, testing at refueling.

One of the valves will be disassembled and visually inspected at refueling. Valve inspections will alternate with subsequent refuelings. Failure to pass inspection will initiate disassembly and inspection of the other valve. Reverse flow closure will be verified during Appendix J, Type C, valve leak testing at refueling.

ISI-203 Rev. 6

Page 112 of 244



CONTAINMENT SPRAY SYSTEM:

DWG. NO. 2165-	<u>-5-550</u>		_,	<u></u>								
VALVE NUMBER	CLASS AND	VALVE	SIZE	ACTU. TYPE	NORM. POSIT.	TEST REQ.	STROKE DIRECT	CHECK	C.S. JUST. OR	C.S. OR ALT.	REMARKS	REV.
	DWG. COOR.		AND TYPE					TEST DIRECT.	RELIEF	TEST PERF.		NO.
	3 B-9	Ċ	1X1.2 RL	\$ SA	C	RL-4					NOTE 1	
1CT-11	3	8 [,]	2,	Ю	С	FS-1	0				NOTE 2	
	1-12	2	GL	••-	-	TH-1	C				···· .	
			-			P1-5						
ICT-12	3	в	2	ю	С	FS-1	0				NOTE 2	
	H - 12	2	GL			TH-1	C					
					-	PI-5						
1CT-24	2	8	2	HO	Ċ	FS-1	C	•			NOTE 3	
	H-14	,	GL			. TH-1						•
		ž	•	,		P1-5						·
1CT-25	2	8	2	Ю	C.	FS-1	C				NOTE 3	-
	H-14	,	GL			TH-1						8
						P1-5						
1CT-26	2	в	12	Ю	D	FS-1	C			لد	NOTE 4	
	F-15	,	GA			TH-1						
	•					PI-5	Ŀ	6				
1CT-27	, 2	С	12	SA	C	FS-1	• ^	FF			NOTE 5	,
*	F-14	1 .	CK					•				•
1CT-47	2	8	6	но	С	FS-1	C				NOTE 6	
	E-5		GA			TH-1						
						P1-5						
1CT-50	2	A	8	, но	С	FS-1	0				NOTE 7	
	F-4		GA			TS-1	C					
		• >		•		P1-5	•					
						レリーン	•					



ISI-203 Rev. 6

Page 113 of 244

0S2 `

SYSTEM: CONTAINMENT SPRAY

DWG. NO. 2165-5-550

VALVE NUMBER	CLASS AND DWG. COOR.	VALVE (CAT.)	SIZE (IN.) AND TYPE	ACTU. TYPE	NORM. POSIT.	test Req.	STROKE DIRECT.	CHECK VALVE TEST DIRECT.	C.S. JUST. OR RELIEF REQ.NO.	C.S. OR ALT. TEST PERF.	REMARKS	REV.
- 1CT-53	2 F-3	AC .	8 CK	SA	С	FS-1 BS-1 LJ-3		FF BS	RV-1 RV-1	DS SP-3	NOTE 7	
1CT-62	2 H-8	С	2 CK	SA	C	FS-1 BS-1		FF BS		,	NOTE 8	
1CT-65	2 J-8	C	2 CK	SA	C	FS-1 85-1		FF BS			NOTE 8	
1CT-71	2 K-16	B	12 GA	мо	. 0	FS-1 TM-1 P1-5	С		Ŀ.		NOTE 4	•
1CT-72	2 K-15	C	12 CK	SA	C	FS-1		FF			NOTE 5	
1CT-88	2 K-4	A	8 GA	мо	C	FS-1 TS-1 PI-5 LJ-3	O C				NOTE 7	
1CT-91	2 K-3	AC	8 CK	SA	C	FS-1 BS-1 LJ-3		FF BS	- RV-1 RV-1	ds SP-3	NOTE 7	·
1CT-95	2 L-5	8	6 GA	НО	С ,	FS-1 TM-1 P1-5	C		•	ī	NOTE 6	
1CT-102	2 H-7	8 - ·	12 GA	МО	Ċ ,	FS-1 TM-1 P1-5	o C	:	CS-1 CS-1	FS-2 TM-2	NOTE 9, 7	•

ISI-203 Rev. 6

Page 114 of 244

0\$2

SYSTEM: CONTAINMENT SPRAY

DWG. NO. 2165-S-550

	VALVE NUMBER	CLASS AND DWG. COOR.	VALVE (CAT.)	SIZE (1N.) AND TYPE	ACTU. TYPE	NORM. POSIT.	TEST REQ.	STROKE DIRECT.	CHECK VALVE TEST DIRECT.	C.S. JUST. OR RELIEF REQ.NO.	C.S. OR ALT. TEST PERF.	REMARKS	REV. NO.
	1CT-105	2 N-7	В	12 GA	мо	С	FS-1 TM-1 P1-5	o C		CS-1 CS-1	FS-2 TM-2	NOTE 9,7	
	1VB-1 (1CT-E017)	3 A-8	C	2 CK	SA	C	FS-1		FF	ł		NOTE 10 '	•
•	1VB-2 (1CT-E018)	3 A-8	C	2 CK	SA	. C	FS-1		FF			NOTE 10	

FOR

SHEARON HARRIS NUCLEAR POWER PLANT

SECTION 5.6.12

.

٠

.

VALVE TEST TABLES AND RELIEF REQUESTS

FOR -

STEAM GENERATOR BLOWDOWN

DWG. NO. 2165-S-551

z ''

,

÷

,

•

SYSTEM:	STEAM	GENERATOR	BLOWDOWN			
	٧		1		, 1	
,	NO.		NOTE			
	1.		Steam Generat Valves.	or Blowdown	Line	Block

ISI-203 Rev. 6

Page 117 of 244

ě

SYSTEM: STEAM GENERATOR BLOWDOWN

.

DWG. NO. 2165-S-551

1		· · · ·	1		· · · · · · · · · · · · · · · · · · ·		1	r	· · · · · · · · · · · · · · · · · · ·			
								1	c.s.	C.S.		
-	CLASS	VALVE	SIZE	ACTU.	NORM.	TEST	STROKE	CHECK	JUST.	OR	REMARKS	REV.
VALVE NUMBER	AND	(CAT.)	(IN.)	TYPE	POSIT.	. REQ.	DIRECT.	VALVE	OR	ALT.		
	DWG.		AND					TEST	RELIEF	TEST		NO.
	COOR.		TYPE					DIRECT.	REO.NO.	PERF.		
					-		· · · · · · · · · · · · · · · · · · ·					
- 180-1	2	С	2	AO	0	FS-1	С				NOTE 1	
	D-3		GL			TS-1						
1						FC-1						
						P1-5						
1BD-7	2	в	4	PO	0	FS-1	С				NOTE 1	
	C-3		GA		۲	TS-1	+					
1					٦	FC-1						
						PI_5						
						2						
1BD-11	2	в	4	P0	0	FS-1	ີ່ລ				NOTE 1	
	D7	-	GI		•	TS-1	Ŭ					
			•••			FC-1						
						DI.K						
	ĸ					11-2						•
18D-20	2	в	2	- AQ-	0	FS-1	C		n	•	NOTE 1	
	1-3	-	- 61		•	TS-1	Ŭ					
	•••			4		FC-1						
						PI_5	•	1				
						11-2						
18D-26	2	8	4	P0	0	FS-1	C				NOTE 1	
	H-3	•	GA	•••	-	TS-1	•					
			••••			FC-1					-	
	•					PI-5						
		,									•	
180-30	• 2	в	4	P0	0	FS-1	С				NOTE 1	•
	1-6		GL		-	TS-1	-					
						FC-1						
•						P1-5		•'				
1BD-39	2	8	2	AO	0	FS-1	٠c				NOTE 1	
	N-3		GL			TS-1	-					
						FC-1						
						P1-5	<u>;</u> ,					
							•					
1BD-45	2	8	4	P0	0	FS-1	c.				NOTE 1	
	L-3	-	GA		-	TS-1						
						FC-1	•	*				
						PI-5						¥
1BD-49	2	в	4	P0	0	FS-1	С	>			NOTE 1	
	N-7		GL			TS-1	2					
						FC-1					*	
						P1-5						

Ø

.

,

.

Page 118 of 244

FOR

SHEARON HARRIS NUCLEAR POWER PLANT

SECTION 5.6.13

VALVE TEST TABLES AND RELIEF REQUESTS

FOR

PROCESS SAMPLING

DWG. NO. 2165-S-551 2165-S-552



Page 119 of 244

SYSTEM: PROCESS SAMPLING

0S2

		NO.	NOTE
-	±	1.	Steam Generator Sample Block Valves.
		2.	Sampling System Containment Isolation Valves.
		3.	Position Indication will be verified during performance of Appendix J, LLRT Testing.

ISI-203 Rev. 6

.

`

•

x

۶

SYSTEM: PROCESS SAMPLING

DWG. NO. 2165-S-551

I	1	r					1	1		· · · ·		
	la						I		C.S.	c.s.		
	CLASS	VALVE	SIZE	ACTU.	NORM.	TEST	STROKE	CHECK	JUST.	OR	REMARKS	REV.
VALVE NUMBER	AND	(CAT.)	(11.)	TYPE	POSIT.	REQ.	DIRECT.	VALVE	OR	ALT.		
	DWG.	[AND					TEST	RELIEF	TEST		NO.
	COOR.		TYPE					DIRECT.	REQ.NO.	PERF.		
100 014	•	~	- / 4									
- ISP-214	2	8	3/4	SO	0/C	FS-1	C				NOTE 1	
	C-4		GL			TS-1						
						FC-1	•					
						PI-5		·				
1SP-216	2	в	3/4	SO	0/0	ES-1	C				NOTE 1	
	C-4	-	GL			TS-1	•					
	• •					FC-1						
×						PI-5						
,												
1SP-217	2	B	3/4	SO	0/C	FS-1	С				NOTE 1	
	C-6		GL		•	TS-1						
•						FC-1						
			•			P1-5						•
	_	_				_					-	
1SP-219	2	B	3/4	SO	0/C	FS-1	C				NOTE 1	
	G-4		GL			TS-1					•	
						FC-1						
						PI-5						
1SP-221	2	в	3/4	so	0/0	FS-1	C				NOTE 1	
	H-4	-	GL	•••	•, •	TS-1	Ŭ				MULE I	
			••			FC-1						
						P1-5						
ISP-222 -	2	B	3/4	SO	0/C	FS-1	C				NOTE 1	
	Н -б		GL			TS-1						
					,	FC-1						
						P1-5				*		
100-004	2	0	7/4	60	0.42	FO •	•				•	
138-224	2	5	<i>3/4</i>	50	0/0	FS-1	C				NOTE 1	
	L-4		66			15-1	•				•	
						FC-1	•					
						P1-5	•	:				-
isp-226	2	B	3/4	SO	0/C	FS-1	c.				NOTE 1	
	M-4		GL			TS-1						
						FC-1						
						PI-5			<i>.</i>			
		_			-		_					
15P-227	2	В	3/4	SO	0/C	FS-1	C				NOTE 1	
	L-0		GL			[S-1			•			
	-					FC-1						
						PI-5						



ISI-203 Rev. 6

Page 121 of 244

0S2

٠



SYSTEM: PROCESS SAMPLING

'n,

0S2

VALVE NUMBER		VALVE	SIZE	ACTU. TYPE	NORM.	TEST REQ.	STROKE	CHECK	U.S. JUST. OR	C.S. OR ALT.	REMARKS	RE
•	DWG. COOR.		AND TYPE					TEST DIRECT.	RELIEF REQ.NO.	TEST PERF.		N
1SP-40	2 C-4	A	3/8 GL	SO	0	FS-1 TS-1	C	5. 5.			NOTE 2, 3	
				n #		FC-1 P1-5	•					
1SP-41	2 C-5	A	3/8 GL	SO	0	FS-1 TS-1	C				NOTE 2, 3	
		÷.				FC-1 Pl-5						
1SP-59	2	٨	3/8	so	ο	LJ-3 FS-1	с				NOTE 2, 3	
	D-4		GL			TS-1 FC-1						
169-60	•		3 /9	50	0	P1-5 LJ-3	C				NOTE 2 3	
131-00	D-5	, ,	GL		v	TS-1 FC-1	. `				1012 2, 5	
						PI-5 LJ-3						
1SP-78	2 D-3	A	3/8 GL	SO	С	FS-1 TS-1 FC-1 P1-5	C				NOTE 2, 3	
1SP-81	2 E-3	۸	3/8 GL	SO	C	LJ-3 FS-1 TS-1	с _.	•			NOTE 2, 3	
						FC-1 P1-5						
1SP-84	2 F-3	۸	3/8 GL	50	С	CJ-5 FS-1 TS-1 FC-1	C				NOTE 2, 3	
1SP-85	2	 A	3/8	so	с	P1-5 LJ-3 FS-1	• C				NOTE 2, 3	
•	E-4		GL .			TS-1 FC-1 P1-5	•				*	
1SP-200	2 N-6	A	1 GL	SO	С	LJ-3 FS-1 TS-1	С				NOTE 2, 3	
`						FC-1 PI-5						

Page 122 of 244

0S2



SYSTEM: PROCESS SAMPLING

DWG. NO. 2165-	<u>S-552</u>											
VALVE NUMBER	CLASS AND DWG. COOR.	VALVE (CAT.)	SIZE (IN.) AND TYPE	ACTU. TYPE	NORM. POSIT.	TEST REQ.	STROKE DIRECT.	CHECK VALVE TEST DIRECT.	C.S. JUST. OR RELIEF REQ.NO.	C.S. OR ALT. TEST PERF.	REMARKS	REV NO
-1SP-201	. 2 N-5	Α	1 GL	SO	C	FS-1 TS-1 FC-1 P1-5 LJ-3	C	<u> </u> .	<u> </u>		NOTE 2, 3	<u> </u>
1SP-208	2 N-6	A	3/4 GL	SO	C	FS-1 TS-1 FC-1 P1-5 LJ-3	C				NOTE 2, 3	
15P-209	2 N-5		* 3/4 GL	SO	С	FS-1 TS-1 FC-1 PI-5 LJ-3	C				NOTE 2, 3	•
1SP-948	2 8-4	A	3/8 GL	SO	0	FS-1 TS-1 FC-1 P1-5 LJ-3	C				NOTE 2, 3	
15P -949	2 B -5	۸	3/8 GL	SO _	0	FS-1 TS-1 FC-1 P1-5 - LJ-3	С				NOTE 2, 3	

۰.

FOR

SHEARON HARRIS NUCLEAR POWER PLANT

SECTION 5.6.14

VALVE TEST TABLES AND RELIEF REQUESTS

FOR

.

.

DIESEL GENERATOR FUEL OIL TRANSFER

DWG. NO. 2165-S-563

Page 124 of 244

ISI-203 Rev. 6

(

SYSTEM: DIESEL GENERATOR FUEL OIL TRANSFER

NO.	NOTE
1.	D.G. Fuel Oil Transfer Pump Discharge Check Valves. Failure of the check valves to close on reverse flow will not siphon the tank or degrade system operation, so, verification of reverse flow closure is not required.
2.	Relief valve which protects safety-

Relief valve which protects safetyrelated equipment.

SYSTEM: D. G. FUEL OIL TRANSFER

DWG. NO. 2165-S-563

2101 1101 2103												
VALVE NUMBER	CLASS AND DWG. COOR.	VALVE (CAT.)	SIZE (IN.) AND TYPE	ACTU. TYPE	NORM. POSIT.	TEST REQ.	STROKE DIRECT.	CHECK VALVE TEST DIRECT.	C.S. JUST. OR RELIEF REQ.NO.	C.S. OR ALT. TEST PERF.	REMARKS	REV. NO.
·10F0-168	3 G-2	C	2 CK	SA	C	FS-1		FF			NOTE 1	·······
1DF0-170	3 G-1	C	3/4X1 RL	SA	C	RL-4					NOTE 2	
1DF0-186	3 G-7	C	2 CK	SA	Ċ	FS-1		FF		٠	NOTE 1	
1DF0-188	3 G-5	C	3/4X1, RL	, SA ,	C "	RL-4					NOTE.2	
1DF0-176	3 F-10	C	1 <u>1</u> X 1 RL	± sa	С	RL-4					NOTE 2	•
1DF0-194	3 F-15	С	1 <u>1</u> X 1 RL	‡ SA	С	RL-4					NOTE 2	

0S2



,

FOR

SHEARON HARRIS NUCLEAR POWER PLANT

SECTION 5.6.15

VALVE TEST TABLES AND RELIEF REQUESTS

FOR

RADIATION MONITOR AND HYDROGEN ANALIZER

DWG. NO. 2165-S-605

0S2

h

SYSTEM: RADIATION MONITOR AND HYDROGEN ANALIZER

NO.	NOTE
1.	Containment Isolation Valves.
2.	Position Indication will be verified during performance of Appendix J, LLRT Testing.



SYSTEM: RAD. MON. & H2 ANALIZER

DWG. NO. 2165-	<u>S-605</u>						1	r			·	
VALVE NUMBER	CLASS AND DWG	VALVE (CAT.)	SIZE (IN.) AND	ACTU. TYPE	NORM. POSIT.	TEST REQ.	STROKE DIRECT.	CHECK VALVE TEST	UST. JUST. OR RELIEF	OR ALT. TEST	REMARKS	REV.
	COOR.		TYPE					DIRECT.	REQ.NO.	PERF.		
1SP-12	2	A	1	so	0	FS-1	C				NOTE 1, 2	1
	C-12		GL			TS-1				-		
						FC-1						•
•						PI-5					•	
						LJ-3						
1SP-16	2	B	1	so	0	FS-1	С				NOTE 1, 2	
	C-13		GL			TS-1					*	
				,	`	FC-1						
•						P1-5			e			
1SP-42	2	A	1	so	С	FS-1	С				NOTE 1, 2	
	G-12		GL			TS-1	વ					
						FC-1						
						P1-5			•			
			-			LJ→3						-
1SP-62	2	A Ì	1	so	. C	FS-1	C				NOTE 1, 2	
	1-12		GL.			TS-1						
						FC-1						
•						PI-5						
						LJ-3						
1SP-915	2	A	1	so	0	FS-1	C		•		NOTE 1, 2	
	C-12		GL		•	TS-1						
						FC-1						
						P1-5						
						LJ-3						



.



SYSTEM: RAD. MON. & H2 ANALIZER

DWG. NO. 2165-	<u>s-605</u>		·				·	r=			• 	
VALVE NUMBER	CLÁSS AND DWG. COOR.	VALVE (CAT.)	SIZE (IN.) AND TYPE	ACTU. TYPE	NORM. POSIT.	TEST REQ.	STROKE DIRECT.	CHECK VALVE TEST DIRECT.	C.S. JUST. OR RELIEF REQ.NO.	C.S. OR ALT. TEST PERF.	REMARKS	REV.
-1SP-916	2 C-13	8	1 GL	SO	0	FS-1 TS-1 FC-1 PI-5 LJ-3	C			.,1	NOTE 1, 2	-
1SP-917	2 D-12	A	1 GL	SO	0	FS-1 TS-1 FC-1 P1-5 LJ-3	С				NOTE 1, 2	
15P-918	2 0-13	В	1 GL ,	SO	0	FS-1 TS-1 FC-1 P1-5 LJ-3	С				NOTE 1, 2	•
1SP-919	2 G-12		1 GL	so	Ċ	FS-1 TS-1 FC-1 PI-5 LJ-3	C	1			NOTE 1, 2	
1SP-939	2 D-13	В	1 GL	SO .	0	FS-1 TS-1 FC-1 P1-5 LJ-3	C			2	NOTE 1, 2	
1SP-941	2 D-12	•	1 GL	SO	0	FS-1 TS-1 FC-1 P1-5 LJ-3	C :				NOTE 1, 2	
1SP-943	2 I-12	A .	1 GL	SO	C	FS-1 TS-1 FC-1 P1-5 LJ-3	c			·	NOTE 1, 2	

ISI-203 Rev. 6

• •

Page 130 of 244

0S2

FOR

SHEARON HARRIS NUCLEAR POWER PLANT

SECTION 5.6.16

VALVE TEST TABLES AND RELIEF REQUESTS

FOR

DIESEL GENERATOR AIR START

DWG. NO. 2165-S-633



ISI-203 Rev. 6

SYSTEM: DIESEL GENERATOR AIR START

<u>NÖ.</u> 1.

2.

NOTE

D.G. Air Compressor to Air Receiver Check Valves. Valves are exercised by normal operation of the Compressors in the forward direction. Air Receivers are alarmed to indicate drop in pressure. Reverse flow verification is required to maintain sufficient Receiver inventory for D. G. Starting.

Relief Valve which protects safetyrelated equipment.

SYSTEM: D. G. AIR START

DWG. NO. 2165-S-633

1	1		1				_					
,VALVE NUMBER	CLASS AND DWG. COOR.	VALVE (CAT.)	SIZE (IN.) AND TYPE	ACTU. TYPE	NORM. POSIT.	TEST REQ.	STROKE DIRECT.	CHECK VALVE TEST DIRECT.	C.S. JUST. OR RELIEF REQ.NO.	C.S. OR ALT. TEST PERF.	REMARKS	REV. NO.
1EA-4	3 C-2	С	1 <u>1</u> СК	SA	0/C	FS-1		BS			NOTE 1	
1EA-6	3 8-3	C	1 <u>‡</u> RL	SA	C	RL-4					NOTE 2 .	
1EA-19	3 D-2	C	1 1 CK	SA	0/C	FS-İ		BS			NOTE 1	
1EA-21	3 C-3	C	וֿ± RL	SA	С	RL-4					NOTE 2	·
1EA-35	3 •C-12		1 1 CK	SA	0/C	FS-1		85	ı		NOTE 1	•
1EA-37	3 B-13		1 <u>1</u> RL	SA	С	RL-4					NOTE 2	
1EA-50	3 D-12	C	1 1 CK	SA	0/C	FS-1		BS			NOTE 1	
1EA-52	3 C-13	с	1 1 RL	SA	С	RL-4					NOTE 2	



.

Page 133 of 244



FOR

.

SHEARON HARRIS NUCLEAR POWER PLANT

SECTION 5.6.17

VALVE TEST TABLES AND RELIEF REQUESTS

FOR

.

DEMINERALIZED WATER

DWG. NO. 2165-5-799



ISI-203 Rev. 6

SYSTEM:	DEMINERALIZER WATER								
	NO.	NOTE							
•	1.	Containment	Isolation	Valves.					

ISI-203 Rev. 6

۰.

Page 135 of 244

.

•

VALVE

RELIEF REQUEST

<u>RV-1</u>

Demineralized Water

System:	
---------	--

Valve: 1Dh	-65
------------	-----

Category:

2.

AC

Function:

Class:

Test

Containment Isolation Simple Check Valve (reverse flow closure for containment isolation only).

Requirements: Verify reverse flow closure.

Basis for Relief: The only method available to verify reverse flow closure is by valve leak testing during Appendix J, Type C, testing at refueling.

 Alternate Testing: Reverse flow closure will be verified during Appendix J, Type C, testing at refueling.

ISI-203 Rev. 6

SYSTEM: DEMINERALIZED WATER

DWG. NO. 2165-5-799

VALVE NUMBER	CLASS AND DWG. COOR.	VALVE (CAT.)	SIZE (IN.) AND TYPE	ACTU. TYPE	NORM. POSIT.	TEST REQ.	STROKE DIRECT.	CHECK VALVE TEST DIRECT.	C.S. JUST. OR RELIEF REQ.NO.	C.S. OR ALT. TEST PERF.	REMARKS	REV'. NO.
1DW-63	2 , H-5	۸	3 GA	MA ,	LC LJ-3	· PV					NOTE 1	
1 DW-65	2 H-6	AC	`3 СК	SA .	FS-1 LJ-3			BS	RV-1	SP-3	NOTE 1	•



•

•

٩

÷

P

FOR

,

a.

SHEARON HARRIS NUCLEAR POWER PLANT

SECTION 5.6.18

VALVE TEST TABLES AND RELIEF REQUESTS

FOR

•

CONTAINMENT SUMP DRAINS

DWG. NO. 2165-S-685

0S2



ISI-203 Rev. 6

× •

N ٠

A , 8

и**н**

4

• • •

.,

	SYSTEM:	CONTAINMENT SUMP DR	AINS		
ъ		NO.	NOTE	•	
	ى	1.	Containment	Isolation	Valves.
	۰ ۱	•			•



Page 139 of 244

0S2

SYSTEM: CONTAINMENT SUMP DRAINS

DWG. NO. 2165-5-685

VALVE NUMBER	CLASS AND DWG. COOR.	VALVE (CAT.)	SIZE (IN.) AND TYPE	ACTU. TYPE	NORM. POSIT.	TEST REQ.	STROKE DIRECT.	CHECK VALVE TEST DIRECT.	C.S. JUST. OR RELIEF REQ.NO.	C.S. OR ALT. TEST PERF.	REMARKS	REV. NO.
1ED-94	2 M-7	A	3 •GA	мо	0	FS-1 TS-1 P1-5 LJ-3	C	• .			NOTE 1	
1ED-95	2 H-7 [,]	A	3 GA	мо	0	FS-1 TS-1 PI-5 LJ-3	С		•	×	NOTE 1	1

0S2

. .

. • **,**

. **"**

• "

•

FOR

SHEARON HARRIS NUCLEAR POWER PLANT

SECTION 5.6.19

VALVE TEST TABLES AND RELIEF REQUESTS

FOR

SERVICE AIR

DWG. NO. 2165-S-800

ISI-203 Rev. 6

Page 141 of 244

0S2

SYSTEM:	SERVICE AIR										
	<u>NO.</u>	NOTE									
4	1.	Containment Isolation Valves.									

ISI-203 Rev. 6

Page 142 of 244
VALVE

RELIEF REQUEST

<u>RV-1</u>

Service Air

1SA-82

Valve:

System:

Category:

Class:

Function:

Containment Isolation Simple Check Valve . (reverse flow closure for containment isolation only).

Test Requirement:

Basis for Relief:

Alternate Testing:

Verify reverse flow closure.

The only method available to verify reverse flow closure is by valve leak testing during Appendix J, Type C, testing at refueling.

Reverse flow closure will be verified during Appendix J, Type C, testing at refueling.



.

SYSTEM: SERVICE AIR

DWG. NO. 2165-5-800

VALVE NUMBER	CLASS AND DWG. COOR.	VALVE (CAT.)	SIZE (1N.) AND TYPE	ACTU. TYPE	NORM. POSIT.	TEST REQ.	STROKE DIRECT.	CHECK VALVE TEST DIRECT.	C.S. JUST. OR RELIEF REQ.NO.	C.S. OR ALT. TEST PERF.	REMARKS	REV. NO.
1SA-80	2 C-2	A	2 GL	МА	LC	PV LJ-3		f I			NOTE 1	
1SA-82	2 C-3	AC	2 CK	SA	C	FS-1 LJ-3		BS	RV-1	SP-3	NOTE 1	

PUMP AND VALVE INSERVICE TESTING PROGRAM PLAN

FOR

.

SHEARON HARRIS NUCLEAR POWER PLANT

SECTION 5.6.20

VALVE TEST TABLES AND. RELIEF REQUESTS

FOR

INSTRUMENT AIR

DWG. NO. 2165-S-801 2165-S-1017





.

SYSTEM:	INSTRUMENT AIR	
·	NO.	NOTE
	1.	Containment Isolation Valves.
	2.	Accumulator fill line check valves. Accumulators are maintained charged and are alarmed during normal operations.
,	3.	Valve numbers have been revised. Valves formally numbered as: 1CB- VO1A. VO1B. VO2A. VO2B AND 1CV-1.2.





COLD SHUTDOWN TEST JUSTIFICATION

CS-1

System:

Valve:

Instrument Air

IIA-819

Α

2

Category:

Class:

ASME Section XI Quarterly Test Requirements:

Cold Shutdown Test Justification:

Quarterly Part Stroke Testing:

Cold Shutdown Testing: Exercise, Time and Fail.

Instrument Air supplies a number of components inside Containment which are necessary for normal operation. Testing during normal operation would deprive these components of their normal air supply and, since the system has no reserve air storage capacity, could result in operating transients and a possible forced plant shutdown.

Valves are equipped with full stroke only operators and can not be partial stroke exercised.

Exercise, Time and Fail at cold shutdown when the normal Instrument Air can be isolated without causing loss of instruments and components necessary for normal plant operations.



ISI-203 Rev. 6

Page 147 of 244

OS2

RELIEF REQUEST

<u>RV-1</u>

Instrument Air

System:

1IA-220

Valve:

Class:

AC

2

Function:

Category:

Containment Isolation Simple Check Valve (reverse flow closure for Containment isolation only).

Test Requirements:

Basis for Relief:

Alternate Testing:

Verify reverse flow closure.

The only method available to verify reverse flow closure is by valve leak testing during Appendix J, Type C, testing at refueling.

Reverse flow closure will be verified during Appendix J, Type C, testing at refueling.



VALVE

RELIEF REQUEST

<u>RV-2</u>

Instrument Air

C

2

Valve:

System:

Category:

Class:

Function:

Test Requirements:

Basis for Relief:

Alternate Testing:

Verify reverse flow closure.

Instrument Air To Air Operated

Containment Isolation Valve Accumulators.

1IA-784, 785, 786, 787, 788, 789

Each fill line to the accumulators contains two simple check valves in series and there are no system provisions for individual valve closure verification. Only one automatic actuating valve is required to isolate the non-classed instrument air system from the accumulators. The two valves function as a single unit and if either of them close proper operation of the accumulators is assured. To verify reverse flow closure of the unit requires isolating and depressurization of a large segment of the Instrument Air System for an extended length of time. Loss of instrument air during operation would cause loss of instrumentation needed for normal operations. Because of the time required to perform testing, performing verification at cold shutdown could cause delays in returning the plant to normal operations.

One value on the accumulator side and one value on the instrument air side will be disassembled and inspected at each refueling. Failure of the tested value will initiate testing of the other two corresponding values.



Page 149 of 244

SYSTEM: INSTRUMENT AIR

DWG. NO. 2165-S-801

VALVE NUMBER	CLASS AND DWG. COOR.	VALVE (CAT.)	SIZE (IN.) AND TYPE	ACTU. TYPE	NORM. POSIT.	TEST REQ.	STROKE DIRECT.	CHECK VALVE TEST DIRECT.	C.S. JUST. OR RELIEF REQ.NO.	C.S. OR ALT. TEST PERF.	REMARKS	REV.
11A-220	2 (C-3	A	3 CK	SA	0	FS-1 LJ-3	,	BS	RV-1	SP-3	NOTE 1	
11 A-819	2 C-3	A	3 GA	PO	0	FS-1 TS-1 FC-1 P1-5	. C		CS-1 CS-1 CS-1	FS-2 FS-2 FS-2	NOTE 1	n

ISI-203 Rev. 6

Page 150 of 244

1

. .

90⁻¹ • 0 -

,

,

.

.

and a start of the

SYSTEM: INSTRUMENT AIR

DWG. NO. 2165-S-801

VALVE NUMBER	CLASS AND DWG. COOR.	VALVE (CAT.)	SIZE (IN.) AND TYPE	ACTU. TYPE	NORM. POSIT.	TEST REQ.	STROKE DIRECT.	CHECK VALVE TEST DIRECT.	C.S. JUST. OR RELIEF REQ.NO.	C.S. OR ALT. TEST PERF.	REMARKS	REV. NO.
118-784	2 B-7	С	3/4 CK	SA	0/C	FS-1		BS	RV-2	DS-3	NOTE 2,3	- t
11A-785	2 8-8	C	374 CK	SA	0/C	FS-1		BS	RV-2	DS-3	NOTE 2,3	
118-786	2 G-2	C	3/4 CK	SA .	0/C	FS-1		BS	RV-2	DS-3	NOTE 2,3	
11A-787	2 G-3	C	3/4 CK	SA	0/C	FS-1		BS	RV-2	DS-3	NOTE 2,3	
1 I A-788	2 H-2	C	3/4 CK	SA	0/C	FS-1		BS ·	RV-2	DS-3	NOTE 2,3	•
11A-789	2 H-3	Ċ	3/4 CK	SA	0/C	FS-1		BS	RV-2	DS-3	NOTE 2,3	



PUMP AND VALVE INSERVICE TESTING PROGRAM PLAN

FOR

SHEARON HARRIS NUCLEAR POWER PLANT

SECTION 5.6.21

VALVE TEST TABLES AND RELIEF REQUESTS

FOR

FUEL POOL COOLING

DWG. NO. 2165-S-561 2165-2-805

Page 152 of 244

4	
	~

<u>NO.</u>

1.

2[.].

NOTE

Containment Isolation Valves.

Fuel Pool Cooling Pump Discharge Check Valves. In normal operation only one pump is in service and the Discharge Header is isolated between the pumps by normally closed valves. Since recirculation flow back across the idle pump is not possible verification of reverse flow closure is not required.

Thermal Relief Valve added to the program to comply with North Carolina State Requirements.

3.

SYSTEM: FUEL POOL COOLING

["] DWG, NO, 2165-S-561

01101 1101 2105	<u> </u>						_					
VALVE NUMBER	CLASS AND DWG. COOR.	VALVE (CAT.)	SIZE (IN.) AND TYPE	ACTU. TYPE	NORM. POSIT.	TEST REQ.	STROKE DIRECT.	CHECK VALVE TEST DIRECT.	C.S. JUST. OR RELIEF REQ.NO.	C.S. OR ALT. TEST PERF.	REMARKS	REV. NO.
1SF-118	2 E-2	A	4 GA	ма	LC	PV LJ-3					NOTE 1	
1SF-119	2 E-3	A	4 GA	MA	LC	PV LJ-3			1		NOTE .1	
1SF-144	2 A-3	A	4 GA	ма	LC	PV LJ-3			•		NOTE 1	
1SF-145	2 A-2	A	4 GA	MA	LC	PV LJ-3					NOTE 1	

ISI-203 Rev. 6

٩,

SYSTEM: FUEL POOL COOLING

DWG. NO. 2165-S-805

VALVE NUMBER	CLASS AND DWG. COOR.	VALVE (CAT.)	SIZE (IN.) AND TYPE	ACTU. TYPE	NORM. POSIT.	TEST REQ.	STROKE DIRECT.	CHECK VALVE TEST DIRECT.	C.S. JUST. OR RELIEF REQ.NO.	C.S. OR ALT. TEST PERF.	REMARKS	REV. NO.
- 1SF-3	3 G-9	C	12 CK	SA	0/C	FS-1	•	FF	•	•	NOTE 2	
ISF-13	3 J-9	C	12 CK	' SA	0/C	FS-1		FF			NOTE 2	
1SF-45	3 H-3	C	3/4 X 1 RL	SA	С	RL-4					NOTE 3	
1SF-66	.3 К-3	C	3/4 X 1 RL	SA	C.	RL-4					NOTE 3	



PUMP AND VALVE INSERVICE TESTING PROGRAM PLAN

FOR

SHEARON HARRIS NUCLEAR POWER PLANT

SECTION 5.6.22

VALVE TEST TABLES AND RELIEF REQUESTS

' FOR

EMERGENCY SCREEN WASH

DWG. NO. 2165-S-808





10

" •

•

, • - NO.

1.

2.

NOTE

Emergency Screen Wash Pump Discharge to Screen Line Block Valves. Valves are used for system alignment and fail closed.

Emergency Screen Wash Pump Discharge . Check Valves. Failure of the valve to close on reverse flow will not degrade system operation, so, verification of reverse flow closure is not required.

0S2

Page 157 of 244

SYSTEM: EMERGENCY SCREEN WASH

DWG. NO. 2165-S-808

VALVE NUMBER	CLASS AND DWG. COOR.	VALVE (CAT.)	SIZE (IN.) AND TYPE	ACTU. TYPE	NORM. POSIT.	TEST REQ.	STROKE DIRECT.	CHECK VALVE TEST DIRECT.	C.S. JUST. OR RELIEF REQ.NO.	C.S. OR ALT. TEST PERF.	REMARKS	REV. NO.
1SC-20	3 D-16	B	3 GL	EH	0/C	FS-1 TM-1 FC-1 P1-5	C O				NOTE 1	±
1SC-24	3 C-15	C	3 CK	SA	0/C	FS-1		FF		DS-3	NOTE 2	
1SC-30	3 D-13	B	3 GL	EH	0/C	FS-1 TM-1 FC-1 P1 -5	С 0				NOTE 1	
1SC-34	3 C-12	C	3 CK	SA	0/C	FS-1		FF		DS-3	NOTE 2	•
1SC-37	3 8-13	8	3 GL	EH	0/C	FS-1 TM-1 FC-1 P1-5	C O				NOTE 1	`
1SC-40	3 B-16	B	3 GL	EH	0/C	FS-1 - TM-1 FC-1 PI-5	с о				NOTE 1	
3SC-41	3 B-16	8	3 GL	EH	0/C	FS-1 TM-1 FC-1 P1-5	C				NOTE 1	

Page 158 of 244

0S2

PUMP AND VALVE INSERVICE TESTING PROGRAM PLAN

.

FOR

SHEARON HARRIS NUCLEAR POWER PLANT

SECTION 5.6.23

VALVE TEST TABLES AND RELIEF REQUESTS

FOR

FIRE PROTECTION

DWG. NO. 2165-S-888



SYSTEM: FIRE PROTECTION NO.

1.

NOTE

Containment Isolation Valves.

Page 160 of 244

VALVE

RELIEF REQUEST

<u>RV-1</u>

Fire Protection

System:

Valve:

Class:

1FP-349,357

Category:

2

AC

Function:

Containment Isolation Simple Check Valve (reverse flow closure for containment isolation).

Test Requirements:

Basis for Relief:

Alternate Testing:

Verify reverse flow closure.

The only method available to verify reverse flow closure is by valve leak testing during Appendix J, Type C, testing at refueling.

Reverse flow closure will be verified during Appendix J, Type C, testing at refueling.



SYSTEM: FIRE PROTECTION

DWG. NO. 2165-5-888

VALVE NUMBER	CLASS AND DWG. COOR.	VALVE (CAT.)	SIZE (IN.) AND TYPE	ACTU. TYPE	NORM. POSIT.	TEST REQ.	STROKE DIRECT.	CHECK VALVE TEST DIRECT.	C.S. JUST. OR RELIEF REQ.NO.	C.S. OR ALT. TEST PERF.	REMARKS	REV. NO.
1FP347	2 L-2	A	6 GL	AO	0	FS-1 TS-1 FC-1 P1-5 LJ-3	с ,				NOTE 1	
1FP-349	2 L-3	AC	6 CK	SA	0	FS-1 LJ-3	-	BS	RV-1	SP-3	NOTE 1	
1FP-357	2 L-3	AC	4 CK	SA	C	FS-1 LJ-3		BS	RV-1	SP-3	NOTE 1	
1FP-355	2 L-2	A	4 GA	MA	C	LJ-3	•				NOTE 1	•

.

Page 162 of 244

•

· .

. . .

PUMP AND VALVE INSERVICE TESTING PROGRAM PLAN

FOR

SHEARON HARRIS NUCLEAR POWER PLANT

SECTION 5.6.24

VALVE TEST TABLES AND RELIEF REQUESTS

FOR

ESSENTIAL CHILLED WATER

DWG. NO. 2165-S-998 2165-2-998 SO2 2165-2-999 2165-S-999 SO2



Γ.

.

*

1

•



.

NO.	NOTE
1.	Valves Isolate Non-Safety-Related from Safety-Related portions of system and close on system initiation.
2.	Relief Valve which protects Safety- Related Equipment.
3.	Valve is a normally throttled pressure control valve. Valve automatically responds to changes in system pressure and as such is exempt from Section XI testing. Valve fails open on loss of power. Test fail open function only.
4.	Thermal Relief Valve added to the program to comply with North Carolina State Requirements.
5.	Recirculation Pump Discharge Check Valve. Reverse flow closure is required to prevent flow by-passing the Condenser.
6 .	Safety-Related Make-up to the Chillers Line Check Valve. Normally closed in-line block valve is only open when water is being added. Thus, Verification of reverse flow closure is not required.
7	Safety-Related Make-up to the Chillers, which is only used after an S Signal.

Page 164 of 244

SYSTEM: ESSENTIAL CHILLED WATER

DWG. NO. 2165-5-998

VALVE NUMBER	CLASS AND DWG. COOR.	VALVE (CAT.)	SIZE (IN.) AND TYPE	ACTU. TYPE	NORM. POSIT.	TEST REQ.	STROKE DIRECT.	CHECK VALVE TEST DIRECT.	C.S. JUST. OR RELIEF REQ.NO.	C.S. OR ALT. TEST PERF.	REMARKS	REV. NO.
1CH-115	3 H-14	B	4 BF	AO	0	FS-1 TM-1 FC-1 PI-5	C				NOTE 1	
1CH-116	3 H-14	B	4 BF	AO	0	FS-1 TH-1 FC-1 P1-5	С.				NOTE 1	
1CH-125	3 L-10	8	4 BF	AO	0	FS-1 TH-1 FC-1 P1-5	C				NOTE 1	•
1CH-126	3 L-10	в.	4 BF	AO	0	FS-1 'TM-1 FC-1 PI-5	C		-		NOTE 1	

SYSTEM: ' ESSENTIAL CHILLED WATER

DWG. NO. 2165-S-998 SO2

· · · · · · · · · · · · · · · · · · ·	· · · · · · · · · · · · · · · · · · ·	1						1	<u>,</u>			<u>``</u>	
VALVE	NUMBER		VALVE (CAT.)	SIZE (IN.)	ACTU. TYPE	NORM. POSIT.	TEST REQ.	STROKE DIRECT.	CHECK VALVE	C.S. JUST. OR	C.S. OR ALT.	REMARKS.	REV.
		COOR.		TYPE					DIRECT.	REQ.NO.	PERF.		NO.
- 1CH-	6	3 F-4	С	1X1 RL	SA	C	RL-4					NOTE 2	
jCH-	10	3 1-4	C	1X1 RL	SA	C	RL-4					NOTE 2	
104-	19	3 H-6	C :	3/4 X 1 RL	SA	С	RL-4					NOTE 2	
1FP-	1014	3 J-4	B	1 GL	SO	0	FS-1 TM-1 FC-1	C				NOTE 1	
ÎFP-	1015	3 J-4	B	1 GL	SO	0	FS-1 TM-1 FC-1 P1-5	C		κ		NOTE 1	•
' 1SA-	494	3 E-3	B	1 GA	SO	0	FS-1 TM-1 FC-1 PI-5	C				NOTE 1	
_1SA	495 •	3 E-3	В [*]	1 GA	SO	0	FS-1 TM-1 FC-1 P1-5	C		,		NOTE 1	•
1SW-	1055	3 E-6	B	10 . BF	EH	тн	F0-1 P1-5	ο				NOTE 3	×
15W-	1063	3 E-9	C 3	6/4 X 1 RL	SA	C	RL-4	:				NOTE 4	



SYSTEN: ESSENTIAL CHILLED WATER

DWG. NO. 2165-5-998 502

	VALVE NUMBER	CLASS AND DWG. COOR.	VALVE (CAT.)	SIZE (IN•) AND TYPE	ACTU. TYPE	NORM. POSIT.	TEST REQ.	STROKE DIRECT.	CHECX VALVE TEST DIRECT.	C.S. JUST. OR RELIEF REQ.NO.	C.S. OR ALT. TEST PERF.	REMARKS	REV.
-	,1SW-1078	3 C-8	С	3/4 X 1 RL	I SA '	C	RL-4					NOTE 2	•
	15W-1079	3. C-8	C	8 CK	SA	0/C	FS-1 BS-1		BS	-		NOTE 5	•
	15W-1170	3 F-3	C	1. СК	SA	C	FS-1		FF		,	NOTE 6	
	ISW-1171	3 G-5	B	1 GL	S0	C	FS-1 TM-1 FC-1 P1-5	0				NOTE 7	
	1CH-34	·3 F-11	C	3/4 X 1 RL	SA	C	RL-4					. NOTE 4	•

3.

SYSTEM: ESSENTIAL CHILLED WATER

DWG. NO. 2165-S-999 c.s. c.s. CLASS VALVE SIZE ACTU. NORM. TEST STROKE CHECK JUST. OR . REMARKS REV. VALVE NUMBER AND (CAT.) (IN.) TYPE POSIT. REQ. DIRECT. VALVE OR ALT. . DWG. AND TEST RELIEF TEST NO. COOR. TYPE DIRECT. REQ.NO. PERF. 1CH-148 3 B AO 4 0 FS-1 С NOTE 1 BF A-16 TH-1 FC-1 PI-5 1CH-149 3 4 ₿ AO 0 FS-1 С NOTE 1 A-16 8F TM-1 FC-1 P1-5 1CH-196 3 8 4 AO 0 FS-1 С NOTE 1 L-16 8F TM-1 FC-1 P1-5 1CH-197 3 4 AO в 0 FS-1 С NOTE 1 L-16 8F TM-1 FC-1 PI-5



, ,

, , ,

ч

.

v

· ·

SYSTEM: ESSENTIAL CHILLED WATER

DWG. NO. 2165-5-999 502

01101 1101 2105							T					
VALVE NUMBER	CLASS AND DWG. COOR.	VALVE (CAT.)	SIZE (IN.) AND TYPE	ACTU. TYPE	NORM. POSIT.	TEST REQ.	STROKE DIRECT.	CHECK VALVE TEST DIRECT.	C.S. JUST. OR RELIEF REQ.NO.	C.S. OR ALT. TEST PERF.	REMARKS	REV. NO.
104-50	3 G-3	C	1X1 RL	SA	Ċ	RL-4					NOTE 2	
1CH-54	3'. (-3	C	1X1 RL	SA	C_	RL-4					NOTE 2	
1CH-63	3 H-7	C	3/4 X 1 "RL	SA	C	RL-4					NOTE 2	
1FP-1025	3 J-4	B	1 GL	SO	0	FS-1 TM-1 FC-1 P1-5	C				NOTE 1	
1FP-1026	3 _J-4	B	1 GL	SO	0	FS-1 TM-1 FC-1 P1-5	c´ 、				NOTE 1	
1SA-502	3 E-3	B	1 GL	SO	0	FS-1 TM-1 FC-1 P1-5	С	·			NOTE 1	
15W-1203	3 G-3	C	1 CK	SA	C	FS-1		FF			NOTE 6	
15W-1204	3 H-5	B	* 1 GL	SO	C ·	FS-1 TM-1 FC-1 P1-5	0				NOTE 7	
1SA-503	3 E-3	B	1 GL	so	0	FS-1 TM-1 FC-1 P1-5	ċ	21			NOTE 1	



. *

. I.

'n

1

`

SYSTEM: ESSENTIAL CHILLED WATER

DWG. NO. 2165-5-999 502

VALVE NUMBER	CLASS AND .DWG. COOR.	VALVE (CAT.)	SIZE (IN•) AND TYPE	ACTU. TYPE	NORM. POSIT.	TEST REQ.	STROKE DIRECT.	CHECK VALVE TEST DIRECT.	C.S. JUST. OR RELIEF REQ.NO.	C.S. OR ALT. TEST PERF.	REMARKS	REV.
_1SW-1208	3 F-6	B	10 8F	EH	тн	F0-1 PI-5	0				NOTE 3	
1SW-1216	3 E-9	C	3/4 X 1 RL	I SA	С.	RL-4					NOTE 4	
1SW-1231	3 C-8	C	3/4 X 1 RL	I SA	С	RL-4		·		-	NOTE 2	
15W-1232	3 D-8	C	8 CK (SA	0/C	FS-1 BS-1			BS		NOTE 5	
1CH-78	3 F-10	C	3/4 X RL	1 SA	С	RL-4					NOTE 4	

0S2



Page 170 of 244

PUMP AND VALVE INSERVICE TESTING PROGRAM PLAN

FOR

SHEARON HARRIS NUCLEAR POWER PLANT

SECTION 5.6.25

VALVE TEST TABLES AND RELIEF REQUESTS

FOR

REACTOR COOLANT SYSTEM

DWG. NO. 2165-S-1301



ISI-203 Rev. 6

Page 171 of 244

SYSTEM: REACTOR COOLANT

1.

2.

3.

4.

5.

6.

.7.

8.

NO.

NOTE

Pressurizer Power. Operated Relief Line Block Valves.

Pressurizer Power Operated Relief Valves. Valves are controlled by the Pressureizer over Pressure Protection System, which automatically opens two of the valves at a preset pressure. These valves are tested/timed in open direction as a Augmented Test. Timing to open position will not be considered Section XI Commitment.

Pressurizer Relief Valves.

Containment Isolation Valve.

Reactor Pressure Vessel and Pressurizer Vent Path Block Valves. Tech. Spec. 3.4.11 requires that only one path be operable and the other valves be electrically disabled during normal operation.

Reactor Pressure Vessel and Pressurizer Vent Path Block Valves downstream of normally closed vent valves.

Reactor Pressure Vessel and Pressurizer Vent Path Check Valve.

Position Indication will be verified during performance of G.P.1.

ISI-203 Rev. 6

Page 172 of 244
CS-1

System:

Valve:

Reactor Coolant

1RC-114, 116, 118

B, C

Class:

Category:

Test Requirements:

ASME Section XI Quarterly Test Requirements:

Quarterly Part Stroke Testing:

Cold Shutdown Testing:

ISI-203 Rev. 6

1 .

Exercise, Time and Fail

These power operated relief (PORV) valves are controlled by the Pressurizer Overpressure Protection System, which automatically opens two of the valves at a preset pressure. Set pressures are established to limit undesirable opening of the spring-loaded Safety Valves. These valves have shown a high probability of sticking open and are not essential for overpressure protection during power operation. The PORV's are relied upon during reactor startup and shutdown to protect the RCS from low temperature overpressurization conditions. Therefore, testing these valves at cold shutdown will adequately demonstrate operability at the time the systems safety-related function is being performed.

Valve operators are full-stroke on initiation and can not be partial-stroke exercised.

Exercise, time and fail.

Page 173 of 244

<u>CS-2</u>

Reactor Coolant

System:

Valve:	1RC-900, 901, 902, 903, 904, 905
Category:	B: 1RC-900, 901, 902, 903, 904, 905
Class:	2
Function:	RCS Vent Valves
Test Requirements:	1RC-900, 901, 902, 903, 904, 905:

Cold Shutdown Justification:

Quarterly Part Stroke Testing:

Cold Shutdown Testing:



ISI-203 Rev. 6

Valves are RCS high point vent valves, which were installed subsequent to TMI accident, and are intended only to provide venting capabilities during a natural circulation cool-down evolution. Valves are only routinely used during cold shutdown to provide a path for RCS venting. 1RC-993 prevents normal PRT pressure from pressurizing 1RC-905.

Exercise valve for operability, observe proper operation of fail-safe actuators.

and measure stroke time quarterly.

Technical Specification 3.4.11 required that one vent path from the Reactor pressure vessel head and one vent path from the pressurizer be operable and closed during operation. Technical Specifications require testing of these valves every 18 months. Testing of these valves during power operation could result in an uncontrolled blowdown should the downstream block valves inadvertently open or experience excessive leakage resulting in a loss of RCS inventory to the pressurizer relief tank or containment atmosphere.

None. These valves are not equipped with part stroke exercisers.

1RC-900, 901, 902, 903, 904, 905: Exercise valve for operability, observe proper operation of fail-safe actuators, and measure stroke time at Cold Shutdown.

Page 174 of 244

VALVE

RELIEF REQUEST

<u>RV-1</u>

Reactor Coolant

System:

Valve:

Class:

1RC-164

Category:

AC

2

Function:

Containment Isolation Simple Check Valves (reverse flow closure for containment isolation only).

Test Requirements:

Basis for Relief:

Alternate Testing:

Verify reverse flow closure.

The only method available to verify reverse flow closure is by valve leak testing during Appendix J, Type C, testing at refueling.

Reverse flow closure will be verified during Appendix J, Type C, Testing at Refueling.

Page 175 of 244



SYSTEM: REACTOR COOLANT

0S2

DWG.	NO.	2165-S-1301

	VALVE NUMBER	CLASS AND DWG. COOR.	VALVE (CAT.)	SIZE (IN.) AND TYPE	ACTU. Type	NORM. POSIT.	test Req.	STROKE DIRECT.	CHECK VALVE TEST DIRECT.	C.S. JUST. OR RELIEF REQ.NO.	C.S. OR ALT. TEST PERF.	REMARKS	REV.
	1RC-113	1 H-2	8	3 GA	ы МО	0	FS-1 TH-1 PI-5	C				NOTE 1	
•	1RC-114	1 H-1	BC	3 GL	۸O	C	FS-1 TM-1 FC-1 P1-5	C 0	•	CS-1 CS-1 CS-1	FS-2 TM-2 FC-2	NOTE 2	
	1RC-115	1 F-2	8	3 GA	МО	0	FS-1 TM-1 P1-5	C				NOTE 1	
	1RC -116	1 F-1	BC	3 GL	AO	C 、	FS-1 TH-1 FC-1 P1-5	С 0	-	CS-1 CS-1 CS-1	FS-2 TM-2 FC-2	NOTE 2	-
	IRS-117	1 E-2	8	3 GA	мо	0	FS-1 TN-1 PI-5	C		<i>.</i> .		NOTE 1	
	, 1RC-118	1 E-1	BC	3 GL	AO	C	, FS-1 TM-1 FC-1 P1-5	C O		CS-1 CS-1 CS-1	FS-2 TM-2 FC-2	NOTE 2	-
	1RC-123	1 F-4	С	6 X 6 RL	5 · SA	, C	ŔL-4					NOTE 3	
	1RC-125	1 F-6	C	6 X (RL	5 SA	Ċ ,	RL-4	x				NOTE 3	
	1RC-127	1 F-8	Ç	6 X 6 RL	5 SA	С	RL-4	:			P	NOTE 3	

,

١,

0S2

P

SYSTEM: REACTOR COOLANT

DWG. NO. 2165-5-1301

							1		c.s.	C.S.		
	CLASS	VALVE	SIZE	ACTU.	NORM.	TEST	STROKE	CHECK	JUST.	OR	REMARKS	REV.
VALVE NUMBER	AND	(CAT.)	(11.)	TYPE	POSIT.	REQ.	DIRECT.	VALVE	OR	ALT.		1
	DWG.		AND					TEST	RELIEF	TEST		NO.
	COOR.	Į	TYPE					DIRECT.	REQ.NO.	PERF.		{
1RC-141	2	A	1	AO	0	FS-1	c	•			NOTE 4	
•	C-16		DA			TS-1						
•		-				FC-1	'					
						P1-5					*	¥
						LJ-3						
								•				
1RC-144	2	Α	1	AO	0	FS-1	С				NOTE 4	
	C-17		DA			TS-1						
						FC-1						
						PI-5						
						LJ-3						
1RC-161	2	A	3	AO	C	FS-1	C				NOTE 4	
	D-17		DA			TS-1						
						FC-1						
			•		· ·	P!-5						•
						LJ-3						
	-		-	••	•			~~				
1RC-164	2	AC	3	SA	C	FS-1		85	RV-1	SP-3	NOTE 4	
	U-10		UK			L]→3						
100-000	2	0	1	50	c	DI_5	c		<u> </u>	F6-2	NOTE 5 9	
110-300	A_7	5	CI	30	v	FC-1	v		~ <u>-</u> 2	TU-2	Noie 3, 0	
	<u>n-</u> 1		96			TM-1				FC-2		
						FC-1						
												•
180-901	2	в	1	so	С	P1-5	С		CS-2	FS-2	NOTE 5, 8	
	A-7	-	GL		-	FS-1	-			TM-2		
						TH-1				FC-2		
						FC-1						
				•						•		
1RC-902	2 '	в	1	SO	С	P1-5	C		CS-2	FS-2	NOTE 5, 8	
	B7		ĠL			FS-1				TM-2		
					•	TM-1				FC-2		
-		••	•		•	FC-1						
							•					
1RC-903	2	B	1	SO	С	P1-5	ç		CS-2	FS-2	NOTE 5, 8	
	- 8-7		GL.			FS-1	1			TM-2		
				•		TM-1				FC-2		
						FC-1						
100 004	•	•	•	60	~	01 F	~		06. 0	FC A		
1105-904	2	5		20	L,	F1-3	Li .		₩ -2	гэ-2 Ти-2	NULE 0, 8	
	6-5		GL			53-1 71-1				1M-2		
						1M-1				FU=2	•	
						ru=1						



Page 177 of 244

.

SYSTEM: REACTOR COOLANT

DWG. NO. 2165-S-1301

	VALVE.NUMBER	CLASS AND DWG. COOR.	VALVE (CAT.)	SIZE (IN.) AND TYPE	ACTU. TYPE	NORM. POSIT.	TEST REQ.	STROKE DIRECT.	CHECK VALVE TEST DIRECT.	C.S. JUST. OR RELIEF REQ.NO.	C.S. OR ALT. TEST PERF.	REMARKS	REV. NO.
•	1RC-905	2 A-8	B	1 GL	S0	C	PI-5 FS-1 TM-1 FC-1	C	<u> </u>	CS-2	FS-2 TM-2 FC-2	NOTE 6, 8	1 <u>-</u>

Page 178 of 244

0S2

PUMP AND VALVE INSERVICE TESTING PROGRAM PLAN

FOR

SHEARON HARRIS NUCLEAR POWER PLANT

.

SECTION 5.6.26

VALVE TEST TABLES AND RELIEF REQUESTS

FOR

.

CHEMICAL AND VOLUME CONTROL

DWG. NO. 2165-S-1303 2165-S-1303 S01 2165-S-1303 S02 2165-S-1304 2165-S-1305 2165-S-1306 2165-S-1306



SYSTEM:	CHEMICAL AND VOLUME	CONTROL
	NO.	NOTE
•	1.	RCS Normal Letdown to the CVCS Containment Isolation Valves. Valves are in parallel and can be exercised quarterly without terminating normal RCS Letdown Flow.
	2.	Relief Valve which protects Safety- Related Equipment.
	3.	RCS Normal Letdown to CVCS Containment Isolation Valves. Failure in the closed position would cause loss of Pressurizer Level Control.
	4.	CVCS Charging Flwo to RCS Containment Isolation Valves.
	5	CVCS to and from the RCS Pump Seals Containment Isolation Valves.
	6. .	A check value which functions as a thermal relief value when both containment isolation values are closed. The only Safety-Related function is containment isolation.
	7.	RCS Alternate Charging Line from the CVCS Block Valve. Provides redundant flow path to the RCS.
	8.	RCS Alternate Charging Line Check Valves.
	9.	RCS Normal Charging Line Check Valves.
,	10.	Alternate Charging Pump Minimum Flow Path Block Valves. Valves open in a S signal to prevent dead heading the pumps.
	11.	Thermal Relief Valve added to the program to comply with North Carolina State Requirements.
	12.	Volume Control Tank Valves are interlocked with the RWST Block Valves such that the VCT Block Valves can not be closed until the RWST Block Valves are fully open.

0S2

ISI-203 Rev. 6

Page 180 of 244

.

•



SYSTEM: CHEMICAL AND VOLUME CONTROL

NO.	NOTE
. 13.	VCT Outlet Check Valve. VCT provides head to the charging pumps until the RWST Block Valves are fully open. Reverse flow closure is not required since inline block valves close on system initiation.
14.	Charging Header Pump Inlet Header Block Valves.
15.	Charging Pump Discharge Check Valves. Charging Pump C is an installed spare and will not be connected unless Pump A or B isout of service. Only those valves associated with Charging Pumps in service will be tested.
16.	Charging Pump Minimum Flow Line Check Valves. Inline Motor operated valves close on a S signal. Since one pump is an installed spare a manual valve between headers is maintained closed and the two operating pumps are isolated from each other and reverse closure is not required for system operation.
17.	Charging Pump Minimum Flow line Block Valves. Valves close on an S signal.
18.	Charging Pump Discharge Header Isolation Valves. Valves used for system alignment for Post-LOCA System operation.
19.	Charging Pump Discharge Header Line to the RCS. Provides flow control during normal operation and fails open to guarantee full flow.
20.	Charging Pump Discharge Header Line to the RCS Block Valve. Valve receives an S signal to close on system initiation.



ISI-203 Rev. 6

Page 181 of 244

U. . .

۴ , .

.

.

.

SYSTEM: CHEMICAL AND VOLUME CONTROL

NO.

21.

22.

23.

24.

25.

NOTE Valves used for Emergency Boron Addition. Check valve is down stream of a normally closed flow control valve which will only be open during Boron addition. Reverse flow closure is not required for system operation. RWST Line to Charging Pump Inlet Header Check Valve. To verify full forward flow testing requires full flow through the Charging Pumps. Reverse flow closure is not required since in-line block valves will be closed except when forward flow is needed. Boron Transfer Pump Discharge Check Valves. Reverse flow closure required to prevent recirculation flow through idle pump.

> Valves open for Boric Acid Transfer for guaranteed cold shutdown.

Containment Isolation Valve

ISI-203 Rev. 6

Page 182 of 244

COLD SHUTDOWN TEST JUSTIFICATION

CS-1

1CS-11,231,235,238

System:

CVCS

2

Valve:

Category:

Class:

ASME Section XI Quarterly Test Requirements:

Cold Shutdown Test Justification:

Quarterly Part Stroke Testing:

Cold Shutdown Testing: Exercise and Time (1CS-235,238) Exercise, Time and Fail (1CS-11,231).

A(1CS-11,238) : B(1CS-231,235)

These values are in the normal letdown and charging lines to the RCS. Exercising during normal operation would disrupt normal RCS charging flow which could decrease significantly the capability of the CVCS to provide proper boration ratio. Failure of each value in the closed position coincident with normal charging flow could result in a high RCS water level trip. Because of these reasons and a potential for thermal shock to the Regenative Heat Exchanger, value testing will be delayed to cold shutdown.

Valves are equipped with full stroke only operators and can not be partial stroke exercised.

Exercise and time (1CS-235,238) Exercise, time and fail(1CS-11,231).



COLD SHUTDOWN TEST JUSTIFICATION

CS-2

CVCS

Α

2.

System:

Valve:

1CS-341,382,423,470,472

Category:

Class:

Function:

Valves.

CVCS Seal Water Flow to the Reactor Coolant Pumps Containment Isolation

Test Requirements:

Basis for Relief:

Exercise and Time.

Exercising these values during normal operation or at cold shutdown results in a loss of normal seal water to the RCS Pump Seals. If seal water is terminated, Reactor Coolant is forced from the high pressure RCS into the seals. Reactor Coolant normally contains a high particulate matter concentration which is carried with RCS inleakage and contaminates the seals.

Alternate Testing:

The values 1CS-341,382,423, and 472 will be tested at cold shutdown when the RCS is open, vented, and drained to the top of the vessel flange.

<u>CS-3</u>

1CS-165,166,291,292

System:

Valve:

CVCS

THE TOT

.

В

2

Category:

Class:

Function:

Volume Control Tank Discharge Block Valves (1CS-165,166) and BWST to CVCS Charging Pump Line Block Valves (1CS-291,292).

Test Requirement:

Basis for Relief:

Alternate Testing:

Exercise and Time

The Volume Control Tank Discharge Valves and RSWT to CVCS Charging Pump Inlet Header Block Valves are interlocked such that both sets of valves cannot be open at the same time. To exercise the valves would result in BWST water being injected into the RCS and RCS Pump Seals by the Charging Pumps. RCS Pump Seal flow is required at normal operation. Exercising at this time would affect RCS Boron Concentration and inlet high Boron concentrations into the RCS Pump Seals, which could cause seal damage and shorten service life.

Exercise and Time at cold shutdown when seal injection can be terminated.

Page 185 of 244



0S2



CS-4

System: CVCS Valve: 1CS-279,536,546 Category: C Class: 1CS-279: 2 1CS-536,546: 3 Function: 1CS-279: Check valve in the line from the CVCS BA Filter to the Charging Pump Header. 1CS-536,546: B.A. Transfer pump discharge check valve. Test Requirement: Verify forward flow operability. Basis for Relief: The only possible way to verify forward flow operability is by passing concentrated Boric Acid Fluid through the valve to the Charging Pump Inlet Header. Alternate Testing: Verify forward flow operability when borating to go to cold shutdown.

1.





۰. ۲

.

.

COLD SHUTDOWN TEST JUSTIFICATION

<u>CS-5</u>

CVCS

С

2

System:

Valve: 1CS-294

Category:

Class:

Function:

Test Requirement:

Basis for Relief:

Alternate Testing:

RWST line to CVCS Charging Pump Inlet Header Check Valve.

Verify forward flow operability.

To verify forward flow operability would require opening the downstream block valves(1CS-291,292) to the Charging Pump Inlet Header. Exercising the block valves results in injecting RWST water into the RCS and RCS Pump Seals. Exercising at normal operation when RCS Pump Seal flow is required, would inject high boron concentrations into the RCS Pump Seals. High Boron concentrations in the seal flow could cause seal damage and shorten service life.

Verify forward flow operability at cold shutdown when seal injection can be terminated.



ISI-203 Rev. 6

VALVE

RELIEF REQUEST

<u>RV-1</u>

System:

Valve:

CVCS

AC

2

1CS-344,385,426,471,477

Category:

Class:

.Function:

Containment Isolation Simple Check Valve (reverse flow closure for containment isolation only).

Test Requirement:

Basis for Relief:

Alternate Testing:

Verify reverse flow closure.

The only method available to verify reverse flow closure is by valve leak testing during Appendix J, Type C, testing at refueling.

Reverse flow closure will be verified during Appendix J, Type C, testing at refueling.



VALVE

RELIEF REQUEST

RV-2

1CS-178,192,206

CVCS

С

2

System:

Valve:

~

Category:

Class:

Function:

Charging Pump Discharge Line Check Valves.

Test Requirements:

Basis for Relief:

Alternate Testing:

Verify forward flow operability.

These Charging Pump discharge check valves can not be verified for full flow operability quarterly. Normal operating charging flow is automatically controlled by downstream flow control valve (1CS-231) in responce to RCS operating conditions. To inject full flow into the RCS during normal operation would result in undesirable RCS boron concentrations and system pressure, temperature and level transients. Full stroke exercising these valves at cold shutdown would result in RCS pressure and level transients due to limitations on letdown capability.

Valves will be partial stroke exercised quarterly and verification of full forward flow operability performed at refueling.



ISI-203 Rev. 6

SYSTEM: CVCS

DWG. NO. 2165-	<u>s-1303</u>						-					
VALVE NUMBER	CLASS AND DWG. COOR.	VALVE (CAT.)	SIZE (IN.) AND TYPE	ACTU. TYPE	' NORM. POSIT.	TEST REQ.	STROKE DIRECT.	CHECK VALVE TEST DIRECT.	C.S. JUST. OR RELIEF REQ.NO.	C.S. OR ALT. TEST PERF.	REMARKS	REV.
1CS-7	2 B-10	A	2 GL	AO	0	FS-1 TS-1 FC-1 P1-5 LJ-3	c		F		NOTE 1	— I —
1 CS-8	⊳ 2 B-11	A	2 GL	AO	0	FS-1 TS-1 FC-1 PI-5 LJ-3	С	A.			NOTE 1	
ICS-9	2 [`] B-12	A	2 GL	AO ¢	0	FS-1 TS-1 FC-1 P1-5 LJ-3	С				NOTE 1	. •
1CS-10 [']	2 A-10	С	2X3 RL	SA	С	RL-4 LJ-3	٠.				NOTE 2	
1CS-11	2 A-17	A	[°] 3 GL	AO	0 .	FS-1 TS-1 FC-1 PI-5 LJ-3	C	•	CS-1 CS-1 CS-1	FS-2 TS-2 FC-2	NOTE 3	
1CS-238	2 B-17	A	3 GA	ю	0	FS-1 TS-1 PI-5 LJ-3	C	·	CS-1 CS-1	FS-2 TS-2	NOTE 4	r
1CS-341	2 K-3	A	1 1/2 GL	мо	0	FS-1 TS-1 P1-5 LJ-3	, C		CS-2	FS-3 TS-3	NOTE 5	
1CS-344	2 К-3	AC	1 1/2 CK	SA	0	FS-1 LJ-3		BS	RV-1	SP-3	NOTE 5	-
1CS-467	2 D-16	С	2X3 RL	SA	C	RL-4				e.	NOTE 2	

0S2

.

•

.

.

Page 190 of 244

.

.

.

ø . . ι,

11

•

.

0S2

.

SHEARON HARRIS NUCLEAR POWER PLANT VALVE TEST TABLE

SYSTEM: CVCS

DWG. NO. 2165-5-1303

VALVE NUMBER	CLASS AND DWG. COOR.	VALVE (CAT.)	SIZE (IN.) AND TYPE	ACTU. TYPE	NORM. POSIT.	TEST REQ.	STROKE DIRECT.	CHECK VALVE TEST DIRECT.	C.S. JUST. OR RELIEF REQ.NO.	C.S. OR ALT. TEST PERF.	REMARKS	REV. NO.
1CS-470	2 D-16	A	2 GL	МО	0	FS-1 TS-1 PI-5 LJ-3	C.		CS-2	FS-3 TS-3	NOTE 5	
1CS-471	2 E-16	AC	3/4 CK	SA	C	FS-1 LJ-3		BS	RV-1	SP-3	NOTE 6	
1CS-472	2 D-17	A	2 GL	мо	0	FS-1 TS-1 PI-5 LJ-3	С		CS-2	FS-3 TS-3	NOTE 5	
1CS-477	2 B-16	AC	3 CK	SA	0	FS-1 LJ-3	,	FF 7 8S	RV-1	SP-3	NOTE 4	•
1CS-480	2 8-4	B	3 GL	AO	C	FS-1 TM-1 F0-1 P1-5	0				NOTE 7	
1CS-483	1 8-3	C	3 CK	SA	С	FS-1		FF			NOTE 8	
1CS-486	1 8-3	C	3 CK	SA	С	FS-1		۶F ۴			NOTE 8	
1CS-492	2 C-4	B	3 GL	AO	0	FS-1 TM-1 F0-1 P1-5	0				NOTE 7	
1CS-497	1 C-3	C	. CK	SA	0	FS-1		FF .	·		NOTE .9	v



Page 191 of 244



.

SYSTEM: CVCS

DWG. NO. 2165-S-1303

1CS-500	1	С	3	SA	0	FS-1	,	FF	-		NOTE 9 ·	
VALVE NUMBER	CLASS AND DWG. COOR.	VALVE (CAT.)	SIZE (IN.) AND TYPE	ACTU. TYPE	NORM. POSIT.	TEST REQ.	STROKE DIRECT.	CHECK • VALVE TEST DIRECT.	C.S. JUST. OR RELIEF REQ.NO.	C.S. OR ALT. TEST PERF.	REMARKS	REV.

.

÷

0S2

To

SYSTEM: CVCS

SHEARON HARRIS NUCLEAR POWER PLANT VALVE TEST TABLE

.

٠

۰.

DWG. NO. 2165-	<u>S-1303</u>	S01				••					- 1	
VALVE NUMBER	CLASS AND DWG. COOR.	VALVE (CAT.)	SIZE (IN.) AND TYPE	ACTU. TYPE	NORM. POSIT.	TEST REQ.	STROKE DIRECT.	CHECK VALVE TEST DIRECT.	C.S. JUST. OR RELIEF REQ.NO.	C.S. OR ALT. TEST PERF.	REMARKS	REV. NO.
1CS-382	2 L - 3	Α	1 1/2 GL	мо	0	FS-1 TS-1 PI-5 LJ-3	C	h	CS-2	FS-3 TS-3	NOTE 5	· _
1CS-385	2 K-3	AC	1_1/2 CK	SA	0	FS-1 LJ-3		BS	RV-1	SP-3	NOTE 5	

.



11 • • •

•

1

. • .

.

.

•



SYSTEM: CVCS

DWG. NO. 2165-5-1303 502

0S2

VALVE NUMBER	CLASS AND DWG. COOR.	VALVE (CAT.)	SIZE (IN.) AND TYPE	ACTU. TYPE	NORM. POSIT.	TEST REQ.	STROKE DIRECT.	CHECK VALVE TEST DIRECT.	C.S. JUST. OR RELIEF REQ.NO.	C.S. OR ALT. TEST PERF.	REMARKS	REV. NO.
1CS-423	2 K-3	A '	1 1/2 GL	но ,	0	FS-1 TS-1 PI-5 LJ-3	С` ,. ,	•	CS-2	FS-3 TS-3	NOTE 5	<u></u> 1
1CS-426	2 K-3	AC	1 1/2 CK	SA	0	FS-1 LJ-3		BS	RV-1	SP-3	NOTE 5	





SYSTEM: CVCS

DWG. NO. 2165-S-1304 ...

											1	
VALVE NUMBER	CLASS AND DWG. COOR.	VALVE (CAT.)	SIZE (IN.) AND TYPE	ACTU. TYPE	NORM. POSIT.	TEST REQ.	STROKE DIRECT.	CHECK VALVE TEST DIRECT.	C.S. JUST. OR RELIEF REQ.NO.	C.S. OR ALT. TEST PERF.	REMARKS	REV. NO.
1CS-47	2 E-12	с	2 RL	SA	С	RL-4					NOTE 2	
1CS-744	2 H-16	С	1.5X2.5 RL	SA	С	RL-4					NOTE 2	
1CS-746	2 H-18	B	2 GL	мо	Ċ	FS-1 TM-1 P1-5	0				NOTE 10	
103-752	2 I-18	B	2 GL	мо	С ,	FS-1 TM-1 P1-5	0				NOTE 10	
1CS-755	2 I-16	c	1.5X2.5 RL	SA	с <u>.</u>	RL-4					NOTE 2	

ISI-203 Rev. 6



•



.

SYSTEM: CVCS

DWG. NO. 2165-S-1305

VALVEINUMBER	CLASS AND DWG. COOR.	VALVE (CAT.)	SIZE (IN.) AND TYPE	ACTU. TYPE	NORM. POSIT.	TEST REQ.	STROKE DIRECT.	CHECK VALVE TEST DIRECT.	C.S. JUST. OR RELIEF REQ.NO.	C.S. OR ALT. TEST PERF.	REMARKS	REV. NO.
1CS-127	2 C-10	. C	3/4X1 ⁻ RL	SA .	С	RL-4		, ,			NOTE 11	- 4
1CS-165	2 G-11	, В	, 4 GA	мо	0	FS-1 TM-1 P1-5	С		CS-3 CS-3	FS-2 TM-2	NOTE 12	
1CS-166	2 G-11	В	4 GA	мо	0	FS-1 TM-1 PI-5	С		CS-3	FS-2 TM-2	NOTE 12	
1CS-167	2 G-11	C ⁻	4 CK	SA	0	FS-1		FF	,	•	NOTE 13	•
1CS-168 [*]	2 I-11	B	8 GT	мо	0	FS-1 TM-1 P1-5	С				NOTE 14	
1CS-169	2 J-11	B	8 GT	мо	0	FS-1 TM-1 P1-5	С				NOTE 14	,
1CS-170	2 1-11	8	8 GT	"MO	· 0	FS-1 TM-1 PI-5	С				NOTE 14	
1CS-171	2 K-11	8	8 GT	мо	0	FS-1 TM-1 P1-5	C	•			NOTE 14	
1CS-178	2 H-7	C	3 CK	SA	0/C	FS-1 85-1		FF BS	RV-2	FS-3 PE-1	NOTE 15	



pi

ISI-203 Rev. 6

Page 196 of 244

.

0S2

., 8



•

. .

•

.

η. .

SYSTEM: CVCS

DWG NO 2165-5-1305

010. 10. 2103-									-			
VALVE NUMBER	CLASS AND	VALVE (CAT.)	S1ZE (1N.)	ACTU. TYPE	NORM. POSIT.	TEST REQ.	STROKE	CHECK	C.S. JUST. OR	C.S. OR ALT.	REMARKS	REV.
,	DWG. COOR.		AND TYPE					TEST DIRECT.	RELIEF REQ.NO.	TEST PERF		NO.
- 1CS-179	2 H-8	C	2 CK	SA	0/C	FS-1	> •	FF			NOTE 16	
1CS-182 _,	2 G-7	8	2 GL	мо	0	FS-1 TM-1 PI-5	C	,			NOTE 17	
1CS-192	2 K-7	C	3 CK ₂	SA	0/C	FS-1 BS-1		FF BS	RV-2	FS-3 PE-1	NÓTE, 15	
1CS-193	2 K-8	C	2 CK	SA ·	0/C	FS-1		FF	υ -		NOTE 16	•
1CS-196	2 J-7	В	2 GL	мо	0	FS-1 TM-1 PI-5	C	a			NOTE 17	
1CS-206	2 J-7	C	3 CK	SA	0/C	FS-1 BS-1		FF BS	RV-2	FS-3 PE-1	NOTE 15	
1CS-207	2 1-8	С	2 CK	SA	0/C	FS-1		FF			NOTE 16	
1CS-210	2 1-7	B	2 GL	мо	0	FS-1 TM-1 P1-5	C.		· ·		NOTE 17	
1CS-214	2 G-4 [.]	8	3 GA	мо	0	FS-1 TM-1 P1-5	C				NOTE 17	`
			,									

.



Page 197 of 244

0S2

SYSTEM: CVCS

DWG. NO. 2165-5-1305

VALVE NUMBER	CLASS AND DWG. COOR.	VALVE (CAT.)	SIZE (IN.) AND TYPE	ACTU. TYPE	NORM. POSIT.	TEST REQ.	STROKE DIRECT.	CHECK VALVE TEST DIRECT.	C.S. JUST. OR RELIEF REQ.NO.	C.S. OR ALT. TEST PERF.	REMARKS	REV. NO.
105-217	2 1-6	В	4 GA	мо	0	FS-1 TM-1 P1-5	C ,				NOTE 18	
1CS-218	2 J-6	В	4 GA	МО	0	FS-1 TM-1 P1-5	С	· ,			NOTE 18	
1CS-219	2 I-6	B 	4 GA	мо	0	FS-1 TM-1 P1-5	С				NOTE 18	
1CS-220	2 K-6	B	4 GA	мо	0 [°] .	FS-1 TM-1 P1-5	С				NOTE 18	•
105-231	2 H-4	В	3 GL	AO	ТН	FS-1 TM-1 F0-1 P1-5	0		CS-1 CS-1 CS-1	FS-2 TM-2 F0-2	NOTE 19	
1CS-235 ·	2 H-2	8	3 GA	мо	0	FS-1 TM-1 P1-5	`c -		CS-1 CS-1	FS-2 TM-2	NOTE 20	
1CS-278	2 J-16	B	2 GL	мо	C	FS-1 TM-1 P1-5	0				NOTE 21	
1CS-279	2 J-13	С	2 CX	SA	C	FS-1		FF	CS-4	FS-2	NOTE 21	
1CS-290	2 J-13	С	3/4 X RL	1 SA	С	RL-4	•	•			NOTE 2	



Page 198 of 244

0S2



,

, ,

1 a

•

SYSTEM: CVCS

DWG. NO. 2165-S-1305

VALVE NUMBER	CLASS AND DWG. COOR.	VALVE (CAT.)	SIZE (IN.) AND TYPE	ACTU. TYPE	NORM. POSIT.	TEST REQ.	STROKE DIRECT.	CHECK VALVE TEST DIRECT.	C.S. JUST. OR RELIEF REQ.NO.	C.S. OR ALT. TEST PERF.	REMARKS	RĘV. NO.
105-291	2 I-12	8	8 GA	Mỹ	С	FS-1 TM-1 PI-5	C O		CS-3	FS-3 TM-3	NOTE 12	
105-292	2 K-12	B	8 GA	МО ,	C	FS-1 TM-1 P1-5	C O		CS-3	FS-3 TM-3	NOTE 12	
1CS-293	2 K-13	C	3/4 X 1 RL	SA	C	RL-4			¥		NOTE 2	
1CS-294	2 K-14	С	8 CK	SA	C	FS-1	-	FF	CS-5	FF-2	NOTE 22	•
1CS-310	2 E-4	C	3/4 X 1 RL	SA	С	RL-4	•				NOTE 11	<i>be</i>

•

• -,

ð

.

. .

۱.

× 4 .

٠



SYSTEM: CVCS

DWG. NO. 2165-S-1306

0S2

1CS-601	2008.	C	3/4 X	1 SA	с с	RL-4		DIRECT.	REQ.NO.	PERF.	NOTE 11	
VALVE NUMBER	CLASS AND DWG.	VALVE (CAT.)	SIZE (IN.) AND	ACTU. TYPE	NORM. POSIT.	TEST REQ.	STROKE DIRECT.	CHECK VALVE TEST	C.S. JUST. OR RELIEF	C.S. OR ALT. TEST	REMARKS	REV.



Page 200 of 244
SHEARON HARRIS NUCLEAR POWER PLANT ' VALVE TEST TABLE

•.

SYSTEM: CVCS

DWG. NO. 2165-S-1307 c.s. C.S. CLASS VALVE SIZE ACTU. NORH. TEST STROKE CHECK JUST. OR REMARKS REV. VALVE NUMBER AND (CAT.) (IN.) TYPE POSIT. REQ. DIRECT. VALVE ·OR ALT. DWG. AND TEST RELIEF TEST NO. COOR. TYPE DIRECT. REQ.NO. PERF. ۲ C FS-1 NOTE 23 105-536 3 C 2 SA FF CS-4 FS-2 85**-**2 E-7 CX **BS-1** 8S 2, 1CS-546 3 C SA C FS-1 FF CS-4 FS-2 NOTE 23 СХ BS-1 BS BS-2 G-7 3 Β. 2 PO 0 FS-1 0 NOTE 24 1CS-559 PG TH-1 E-3 F0-1 PI-5 1CS-563 3 PO FS-1 0 NOTE 24 B 2 ٥ E--2 PG TH-1 F0-1 PI-5

ISI-203 Rev. 6

Page 201 of 244

052

PUMP AND VALVE INSERVICE TESTING PROGRAM PLAN

FOR

•

SHEARON HARRIS NUCLEAR POWER PLANT

SECTION 5.6.27

VALVE TEST TABLES AND RELIEF REQUESTS

,

FOR

SAFETY INJECTION

DWG. NO. 2165-S-1308 2165-S-1309 2165-S-1310



ISI-203 Rev. 6

SYSTEM:	SAFETY INJECTION	
	<u>NO.</u>	NOTE
•	1.	BIT Inlet Block Valves. Valves open on a S signal for BIT injection.
-	2.	BIT Discharge to RCS at CTMT Penetration M-17. Valves open on a S signal and close for CTMT Isolation by operator action.
	3.	Safety Injection injection into the RCS Line Check Valves.
	4.	CVCS Charging Pump Discharge to CTMT Penetration Isolation Valves. At cold shutdown only one Charging Pump is in operation due to potential for cold overpressurization. Pump Discharge Header cannot be isolated without loss of seal injection flow.
	5.	RHR Heat Exchanger Outlet to RCS Line Check Valves.
	6.	Containment Isolation Valves.
	7.	Accumulator Safety Relief Valves.
	8.	Accumulator Discharge to RCS Line Check Valves. Valves are pressure isolation valves.
-	9.	Accumulator Drain to RWST Containment Isolation Valves.
	10.	Recirculation Sump Line Block Valves. Because of inline block valves it should be possible to exercise these valves without injecting water into the CTMT. RECIRC. Sumps. If it is found that valve exercising does drain water back into the sumps a relief request

ISI-203 Rev. 6

Page 203 of 244

.

will be prepared to delay testing to refueling when water can be removed from the sumps after exercising. ¢

æ

•



SYSTEM: SAFETY INJECTION

NO. NOTE 11. Forward flow of these 14 inch check valves is verified by flow through the RHR Pump 8 inch test line to the ' RWST. The test line flow is adequate to verify that the valves will pass full design operating flow. Reverse flow closure is not required since inline block valves can be closed to prevent back flow from the sumps. 12. RWST Line Block Valves. Valves close for recirculation mode of system operation. 13. Cross-tie Header Block Valves. Valves are used for Post-LOCA system alignment. 14. Relief Valves which protect Safety-Related Equipment. 15. RHR Heat Exchanger Line to RCS Block Valves. 16.

Low Head Safety Injection Line Check Valves. Valves are high pressure isolation valves between the RCS and the RHR systems.

A pressure isolation valve with a single downstream check valve. To preclude opening during operation the valve is electrically disabled.

0S2

17.

Page 204 of 244

COLD SHUTDOWN TEST JUSTIFICATION

<u>CS-1</u>

SAFETY INJECTION

System:

Valve:

Category:

347, 356, 357, 358 AC(1SI-134, 135, 136, 137, 346, 347, 356, 357, 358) C (1SI-81, 82, 83)

1SI-81, 82, 83, 134, 135, 136, 137, 346,

Class:

1(1SI-81, 81, 83, 134, 135, 136, 137, 356, 357, 358) 2(1SI-346,347)

ASME Section XI Quarterly Test Requirements:

Cold Shutdown Test Justification:

Quarterly Part Stroke Testing:

Cold Shutdown Testing: Verify forward flow operability.

. Verification of forward flow operability of these normally closed check valves can only be performed by injecting RHR water into the RCS. During normal operation the Low Pressure RHR Pumps cannot overcome the higher RCS operating pressure. Testing these valves with high head safety injection will cause pressurizer level control problems along with borating the RCS possibly leading to a reactor scram. The isolation valve test subsystem provides the capacity for determination of the integrity of these pressure isolation valves. It is used to verify that each of the series check valves are closed and can sustain operational differential pressure. This is a required periodic procedure performed at each refueling after RCS has been pressurized.

N/A

Verify forward flow operability during RHR System operation.





• • • •

1.

,







ISI-203 Rev. 6

Page 206 of 244

VALVE

RELIEF REQUEST

<u>RV-1</u>

Safety Injection

Verify forward flow.

C

1

System:

Valve:

1SI-8, 9, 10, 72, 73, 74, 104, 105, 106, 127, 128, 129, 138

Category:

Class:

Function:

Test Requirements:

Basis for Relief:

Alternate Testing:

Safety Injection to the RCS Check Valves.

Verification of forward flow operability can only be performed by injecting charging water into the RCS. The charging pumps have insufficient head to overcome normal RCS operating pressure for a full flow test. Partial testing using the charging pumps would inject CVCS water which has bypassed the Regenarative Heat Exchanger and could result in thermal shocking to the RCS piping. Forward flow verification at cold shutdown could result in a cold overpressurization of the RCS.

Verify forward flow operability at refueling when the Reactor Vessel Head is removed and full charging pump flow can be injected into the RCS.

0S2



ISI-203 Rev. 6

VALVE

RELIEF REQUEST

RV-2

Safety Injection

System:

Valve:

lSI-52,86,107

Α

2

Category:

Class:

Function:

Test

Requirement:

Basis for Relief:

Alternate Testing:

Safety Injection to the RCS Hot Legs Containment Isolation Valves.

Exercise and Time.

Exercising these valves during normal operation would result in injecting charging water flow directly into the RCS. This diverted charging water bypasses the Regenative Heat Exchanger which could cause thermal shocking to RCS piping and could also cause an overtemperature condition in the normal CVCS Letdown Line. At cold shutdown one Charging Pump is running (Tech. Spec. 3.5.3, A maximum of one Charging Pump shall be operating when RCS temperature is < 335 degrees F). This pump is supplying both RCP Pump Seals and required charging water. Seal Water flow is maintined during cold shutdown to preclude damage to the pump seals, thus if these valves were exercised at cold shutdown charging water would be injected into the RCS and a cold overpressurization of the RCS could result.

Valves will be exercised and timed at refueling.

ISI-203 Rev. 6

· · · ·

.

-

VALVE

RELIEF REQUEST

<u>RV-3</u>

System:

Valve:

Safety Injection

1SI-182,290

AC

2

Category:

Class:

Function:

Containment Isolation Simple Check Valve (reverse flow closure for containment isolation only).

Test Requirement:

Basis for Relief:

Alternate Testing:

Verify reverse flow closure.

The only method available to verify reverse flow closure is by valve leak testing during Appendix J, Type C, testing at refueling.

Reverse flow closure will be verified during Appendix J, Type C, testing at refueling.



VALVE

RELIEF REQUEST

<u>RV-4</u>

Safety Injection

AC

2

Valves.

1SI-249,250,251,252,253,254

System:

Valve:

Category:

Class:

Function:

Test Requirement:

Basis for Relief:

Alternate Testing:

Verify forward flow operability. The Accumuator Tanks are isolated from

Accumulator Discharge to RCS Check

the RCS by these normally closed check valves. Each Accumulator is charged with a Nitrogen blanket at approximately 650 psig, which is insufficient to inject into the RCS during normal operation. To exercise these valves to their full open position at cold shutdown would inject approximately 925 Cubic Ft. of high Boron Content water into the RCS, which could cause a cold overpressurization of the RCS. Dumping the full Accumulator inventory into the RCS at refueling could flush large amounts of crud into the RCS and Cleanup Systems. High particulates in the RCS at refueling reduces visibality for refueling operations and generates large amounts of contaminated wastes, which could lengthen the outage and increase personel exposures.

Partial forward flow operability will be verified at cold shutdown by performing an accumulator partial dump test. In addition one valve will be disassembled and visually inspected at refueling. Valve inspections will alternate with subsequent refuelings. Failure of a valve to pass inspection will either initiate inspection of the remaining valves or initiate verification of the remaining valves by Accumulator injection into the RCS.



SHEARON HARRIS NUCLEAR POWER PLANT VALVE TEST TABLE

SYSTEM: SAFETY INJECTION

DWG. NO. 2165-S-1308

						_	The second second second second second second second second second second second second second second second s					
VALVE NUMBER	CLASS AND DWG. COOR.	VALVE (CAT.)	SIZE (IN.) AND TYPE	ACTU. TYPE	NORM. POSIT.	TEST REQ.	STROKE DIRECT.	CHECK VALVE TEST DIRECT.	C.S. JUST. OR RELIEF REQ.NO.	C.S. OR ALT. TEST PERF.	REMARKS	REV. NO.
151-1	2 H-6	B	3 GA	МО	С -	FS-1 TS-1 P1-5	0 C	L	L	L, -,	NOTE 1	
151-2 ,	2 N-6	B	3 GA	мо	C	FS-1 TS-1 PI-5	o c				NOTE 1	
151-3	2 G-2	A	3 GA [/]	MO	C	FS-1 TS-1 PI-5	0 C		• •		NOTES 2,6	
151-4	2 F-11	. A	3 GA	Ю	C	FS-1 TS-1 P(-5	0 C				NOTES 2,6	
151-8	1 D-3	Ċ	2 CK	SA	C	FS-1	•	FF	RV-1	FF-3	NOTES 3,6	
151-9	1 D-4	C	2 CK	SA	C	FS-1		FF	RV-1	FF-3	NOTES 3,6	
1 51-10	1 0-5	C	2 CK	SA	C	FS-1		, FF	RV-1	FF-3	NOTES 3,6	
151-52	2 F-11	A	3 GA	мо	C	FS-1 TS-1 P1-5	0 . C		RV-2 RV-2	FS-3 TS-3	NOTES 4,6	
151-72	1 D-6	C	2 CK	SA	С	FS-1	, ,	FF ,	RV-1	FF-3	NOTES 3,6	

•



Page 211 of 244



SYSTEM: SYSTEM INJECTION

0S2

SHEARON HARRIS NUCLEAR POWER PLANT VALVE TEST TABLE

-

DWG. NO. 2165-5-1308

VALVE NUMBER	CLASS AND DWG. COOR.	VALVE (CAT.)	SIZE (IN.) AND TYPE	ACTU. TYPE	NORM. POSIT.	TEST REQ.	STROKE DIRECT.	CHECK VALVE TEST DIRECT.	C.S. JUST. OR RELIEF REQ.NO.	C.S. OR ALT. TEST PERF.	REMARKS	REV. NO.
151-73	1 D-7	C	2 CK	SA .	с	FS-1	٤*	FF	RV-1	FF-3	NOTES 3,6	
151–74	1 D-8	C	2 CK	SA	С	FS-1		FF	RV-1	FF-3	NOTES 3,6	
151-81	1 8-3	C	6 CK	SA	C	FS-1	•	FF	CS-1	FF-2	NOTE 3	
151-82	1 C-3	C	6 CK	SA	. с	FS-1		FF	CS-1	FF-2	NOTE 3	
151-83	1 D-3	C	6 CK	SA	С	FS-1		FF	CS-1	FF-2	NOTE 3	•
151-86	2 F-12	A	3 GA	МО	С	FS-1 TS-1 P1-5	o C		RV-2 .RV-2	FS-3 TS-3	NOTES 4,6	
151-104	1 D-12	C	2 СК	SA	C	FS-1		FF	RV-1	FF-3	NOTE 3,6	
151-105	1 D-13	C	2 · CK	SA	. C .	FS-1		FF	RV-1	FF-3	NOTE 3,6	
151-106	1 D-4	C	2 CK	SA	<mark>с</mark> .	FS-1		FF	RV-1	FF-3	NOTE 3,6	



Page 212 of 244



SHEARON HARRIS NUCLEAR POWER PLANT VALVE TEST TABLE

SYSTEM: SAFETY INJECTION

0S2 `

DWG. NO. 2165-S-1308

VALVE NUMBER	CLASS AND DWG. COOR.	VALVE (CAT.)	SIZE (IN.) AND TYPE	ACTU. TYPE	NORM. POSIT.	TEST REQ.	STROKE DIRECT.	CHECK VALVE TEST DIRECT.	C.S. JUST. OR RELIEF REQ.NO.	C.S. OR ALT. TEST PERF.	REMARKS	REV. NO.
151-107	2 F-15	A	3 GA	мо	C	FS-1 TS-1 P1-5	o C	_	RV-2 RV-2	FS-3. TS-3	NOTES 4,6	
151-127	1 D15	C	2 СК	SA	, c	FS-1	• ,	FF	RV-1	FF-3	NOTES 3,6	
151-128	1 D-15	C	2 CK	SA	C	FS-1		FF	RV-1	FF-3	NOTES 3,6	
151-129	1 D-16	C	2 CK	SA	C ,	FS-1		FF	RV-1	FF-3	NOTES 3,6	
151-134	1 8-11	AC	6 CK	SA	C	FS-1 LK-3		FF	CS-1	FF-2	NOTES 5,6	•
151-135	1 Ċ-11	AC	6 CK	SA	С	FS-1 LK-3		FF	CS-1	FF-2	NOTES 5,6	
151-136	1 B-17 [.]	C	6 CK	SA	C	FS-1		FF	CS-1	FF-2	NOTE 3	
151-137	1 C-17	C	6 CK	SA	C	'FS-1	ÿ	FF	CS-1	FF-2	NOTE 3	
151-138	1 D - 17	C	6 CK	SA	C	FS-1		FF	RV-1	FF-3	NOTE 3	

ISI-203 Rev. 6

,

Υ.

,

.

• .



SHEARON HARRIS NUCLEAR POWER PLANT VALVE TEST TABLE



SYSTEM: SAFETY INJECTION

DNG. NO. 2165-S-1309

VALVE NUMBER	CLASS AND DWG. COOR.	VALVE (CAT.)	SIZE (IN.) AND TYPE	ACTU. TYPE	NORM. POSIT.	TEST REQ.	STROKE DIRECT.	CHECK VALVE TEST DIRECT.	C.S. JUST. OR RELIEF REQ.NO.	C.S. OR ALT. TEST PERF.	REMARKS	REV.
- 15I-179	2 K-17	A	1 GL	A0 .	С	FS-1 TS-1 FC-1	C				NOTE 6	
						1-5 LJ-3						
151-182	2 K-16	AC	1 CK	SA ,	C	FS-1 LJ-3		85	RV-3	SP-3	NOTE 6	Į
151-225	2 B-12	C	1X2 RL	SA	C	RL-4					NOTE 7	
151-226	2 E-12	C	1X2 RL	SA	C	RL-4					NOTE 7	•
151-227	2 H-12	C	1X2 RL	. SA	Ċ	RL-4					NOTE 7	•
151-249	2 D-6	AC	12 CK	SA	С	FS-1 LK -3		FF	RV-4	PE-2 DS-3	NOTE 8	Ŀ
151-250	2 D-3	AC	12 CK	SA	C	FS-1 LK-3		FF	RV-4	PE-2 DS-3	NOTE 8 -	
151-251	2 G-6	AC	12 CK	SA	C	FS-1 LK-3		FF	RV-4	PE-2 DS-3	NOTE 8	
1SI-252	2 G-3	AC	12 CK	SA	C	FS-1 LK-3		FF	RV-4	PE-2 DS-3	NOTE 8	



ISI-203 Rev. 6

•••

Page 214 of 244 .

0S2



,

۰.

• .

SHEARON HARRIS NUCLEAR POWER PLANT VALVE TEST TABLE

SYSTEM: SAFETY INJECTION

DWG. NO. 2165-S-1309

1								· · · · · · · · · · · · · · · · · · ·		· · · · · · · · · · · · · · · · · · ·			
		CLASS	VALVE	SIZE	ACTU.	NORM.	TEST	STROKE	СНЕСК	C.S. JUST.	C.S. OR	REMARKS	REV.
	VALVE NUMBER	AND	(CAT.)	(IN.)	TYPE	POSIT.	REQ.	DIRECT.	VALVE	OR	ALT.		
		DWG.		· AND			-		TEST	RELIEF	TEST		NO.
		COOR.		TYPE					DIRECT.	REQ.NO.	PERF.		
	-	2	40	12	64	•	CO 1						
	131-233	<u>م</u> ار		12 CY	эл	* L	r3-1		FF	KV-4	PE-2	NOTE 8	
		U -U		un		•	LN-J		3		D2-2		
	151-254	2	AC	12	SA	С	FS-1		FF	RV-4	PE-2	NOTE 8	-
		J-3 ×		CK		I	LK-3				DS-3		
		_					-				_		
	151-263	2	A	3/4	AO	C	FS-1	C	•			NOTE 9	
	÷	D-4		GL			TS-1						
							FC-1						
					-		PI-5		-				
							LJ-3						
	151-264	2	۵	3/1	· 40	C	FC-1	` o					
	101-204	D-4	л	61 61	ΛV	, L	г3-1 те_1	L.				NOTE 9	
		0-4		GL			FC-1	I					
					1		PL-5	*					
							1.1-3						
	151-287	2	A	1	AO	C [.]	FS-1	С				NOTE 6	
		C-17		GL			TS-1						
						Ē	FC-1						
	•		•				P1-5						
			•				LJ-3		-				
	151-290	2	AC	· ·	SA	C	ES-1		BC	9V_7 ·	CD_7	NOTE C	
		C-16		cx	U 11	U	1.1=3		03	~~ <i>></i>	ر اد	NULE O	



SHEARON HARRIS NUCLEAR POWER PLANT VALVE TEST TABLE

-

SYSTEM: SAFETY INJECTION

DWG. NO. 2165-5-1310

0S2 .

1SI-300 2 B 14 HO C FS-1 0 NOTES 10,6 1SI-301 2 B 14 HO C FS-1 0 NOTES 10,6 1SI-301 2 B 14 HO C FS-1 0 NOTES 10,6 1SI-301 2 B 14 HO C FS-1 0 NOTE 10 1SI-310 2 B 14 HO C FS-1 0 NOTE 10 1SI-311 2 B 14 HO C FS-1 0 NOTE 10 1SI-320 2 C 14 SA C FS-1 PI-5 NOTE 11 1SI-321 2 C 14 SA C FS-1 FF NOTE 11 1SI-322 2 B 14 MO 0 FS-1 C NOTE 12 1SI-322 2 B 14 MO 0 FS-1 C NOTE 12 1SI-323 2 B 14 MO		VALVE NUMBER	CLASS AND DWG. COOR.	VALVE (CAT.)	SIZE (IN.) AND TYPE	ACTU. TYPE	NORM. POSIT.	TEST REQ.	STROKE DIRECT.	CHECK VALVE TEST DIRECT.	C.S. JUST. OR RELIEF REQ.NO.	C.S. OR ALT. TEST PERF.	REMARKS	REV. NO.
1S1-301 2. B 14 MO C $FS-1$ P1-5 0 C NOTES 10,6 1S1-310 2 B 14 MO C $FS-1$ P1-5 0 NOTE 10 1S1-310 2 B 14 MO C $FS-1P1-5$ 0 NOTE 10 1S1-311 2 B 14 MO C $FS-1P1-5$ 0 NOTE 10 1S1-320 2 C 14 SA C $FS-1P1-5$ 0 NOTE 11 1S1-321 2 C 14 SA C $FS-1P1-5 FF NOTE 11 1S1-322 2 C 14 SA C FS-1P1-5 C NOTE 11 1S1-323 2 B 14 MO 0 FS-1P1-5 C NOTE 12 1S1-326 2 B 14 MO 0 FS-1P1-5 C NOTE 13 1S1-326 2 B 10 MO 0 FS-1P1-5 C NOTE 13 1S1-326 2 $	-	1\$1-300	2 N-6	В.	14 GA	мо	С	FS-1 TS-1 PI-5	o C				NOTES 10,6	
1SI-310 2 B 14 MO C $FS-1$ PI-5 0 NOTE 10 1SI-311 2 B 14 MO C $FS-1PI-5 0 NOTE 10 1SI-311 2 B 14 MO C FS-1PI-5 0 NOTE 10 1SI-320 2 C 14 SA C FS-1 FF NOTE 11 1SI-320 2 C 14 SA C FS-1 FF NOTE 11 1SI-321 2 C 14 SA C FS-1 FF NOTE 11 1SI-322 2 B 14 MO 0 FS-1 C NOTE 12 1SI-323 2 B 14 MO 0 FS-1 C NOTE 12 1SI-323 2 B 14 MO 0 FS-1 C NOTE 12 1SI-326 2 B 10 MO 0 FS-1 C NOTE 13 1SI-326 2 B 10 MO$		151-301	2. M-6	B	14 GA	мо	C	FS-1 TS-1 PI-5	O C				NOTES 10,6	
1S1-311 2 B 14 MO C $FS-1$ 0 NOTE 10 1S1-320 2 C 14 SA C $FS-1$ FF NOTE 11 1S1-320 2 C 14 SA C $FS-1$ FF NOTE 11 1S1-321 2 C 14 SA C $FS-1$ FF NOTE 11 1S1-321 2 C 14 SA C $FS-1$ FF NOTE 11 1S1-322 2 B 14 MO 0 $FS-1$ C NOTE 12 1S1-322 2 B 14 MO 0 $FS-1$ C NOTE 12 1S1-323 2 B 14 MO 0 $FS-1$ C NOTE 12 1S1-326 2 B 10 MO 0 $FS-1$ C NOTE 13 1S1-326 2 B 10 MO 0 $FS-1$ C <td< td=""><th></th><td>151-310</td><td>2 N-7</td><td>B</td><td>14 GA</td><td>мо</td><td>С</td><td>FS-1 TS-1 PI-5</td><td>0</td><td></td><td></td><td></td><td>NOTE 10</td><td></td></td<>		151-310	2 N-7	B	14 GA	мо	С	FS-1 TS-1 PI-5	0				NOTE 10	
1S1-320 2 C 14 SA C FS-1 FF NOTE 11 1S1-321 2 C 14 SA C FS-1 FF NOTE 11 1S1-321 2 C 14 SA C FS-1 FF NOTE 11 1S1-322 2 B 14 MO 0 FS-1 C NOTE 12 1S1-322 2 A B 14 MO 0 FS-1 C NOTE 12 1S1-323 2 B 14 MO 0 FS-1 C NOTE 12 1S1-323 2 B 14 MO 0 FS-1 C NOTE 12 1S1-326 2 B 10 MO 0 FS-1 C NOTE 13 1S1-326 2 B 10 MO 0 FS-1 C NOTE 13 - 0-6 GA 10 MO 0 FS-1 C NOTE 13		151-311 ,	2 H-7	8	14 GA	мо	С	FS-1 TS-1 P1-5	0	1			NOTĘ 10	•
$1SI-321$ $2 \\ M-12$ C $14 \\ CK$ SA C $FS-1$ FF NOTE 11 $1SI-322$ $2 \\ N-10$ B $14 \\ GA$ MO 0 $FS-1 \\ PI-5$ C NOTE 12 $1SI-323$ $2 \\ M-10$ B $14 \\ GA$ MO 0 $FS-1 \\ PI-5$ C NOTE 12 $1SI-323$ $2 \\ M-10$ B $14 \\ GA$ MO 0 $FS-1 \\ PI-5$ C NOTE 12 $1SI-326$ $2 \\ D-6$ B $10 \\ GA$ MO 0 $FS-1 \\ PI-5$ C NOTE 13		151-320	2 N-12	С	14 СК	SA	C	FS-1		FF			NOTE 11	
1SI-322 2 B 14 MO 0 $FS-1$ C NOTE 12 $1SI-323$ 2 B 14 MO 0 $FS-1$ C NOTE 12 $1SI-323$ 2 B 14 MO 0 $FS-1$ C NOTE 12 $1SI-326$ 2 B 10 MO 0 $FS-1$ C NOTE 13 $1SI-326$ 2 B 10 MO 0 $FS-1$ C NOTE 13 $1SI-326$ 2 B 10 MO 0 $FS-1$ C NOTE 13 $D-6$ GA MO 0 $FS-1$ C $NOTE 13$		151-321	2 M-12	C	14 CK	SA	C	FS-1		FF	ų		NOTE 11	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$		151-322	2 N-10	B	14 GA	мо	0	FS-1 TM-1 PI-5	۲ C				NOTE 12	
151-326 2 B 10 MO O FS-1 C NOTE 13 D-6 GA TM-1 PI-5 .		151-323	2 M-10	B	14 GA	МО	0	FS-1 TM-1 P1-5	c ·				NOTE 12	
		151-326	2 D-6	B	10 GA	- MO ,	0	FS-1 TM-1 PI-5	с :		_		NOTE 13	



Page 216 of 244



,

• •

E

.



SHEARON HARRIS NUCLEAR POWER PLANT VALVE TEST TABLE



SYSTEM: SAFETY INJECTION

DWG. NO. 2165-	<u>s-1310</u>			·			<u> </u>		• •			
VALVE NUMBER	- CLASS AND	VALVE (CAT.)	SIZE	ACTU. TYPE	NORM. POSIT.	TEST REO.	STROKE	CHECK	C.S. JUST. OR	C.S. OR ALT.	REMARKS	REV.
	DWG. COOR.		AND TYPE					TEST DIRECT.	RELIEF REQ.NO.	TEST PERF.		NO.
Í ÍSI-327	2 E-6	В	10 GA	Ю	0	FS-1 TH-1 , PI-5	C				NOTE 13	
151-328	2 B-4	С	3/4X1 RL	SA	C	RL-4			-		NOTE 14	
151-329	2 E-4	C	3/4X1 RL	SA	С	RL-4					NOTE 14	
151 -330	2 • B-5	С	3/4X1 RL	SA .	C	RL-4	•				NOTE 14	
151-340	2 C-4	8	10 GA	HO	0	FS-1 TS-1 PI-5	C 0 /				NOTE 15	•
151-341	2 E-4	8	10 GA	МО	0	FS-1 TS-1 PI -5	C O			¢	NOTE 15	
15 1-346	2 C-3	AC	10 CK	SA	С	FS-1 LK-3		FF	CS-1	FF-2	NOTES 16,6	
151-347	2 E-3	AC	10 CK	SA	С	FS-1 LK-3		FF	CS-1	FF-2	NOTES 16,6	
151-356	1 C-2	AC [*]	6 CK	SA	۰C	FS-1 LK-3		FF	CS-1	· FF-2	NOTE 16	

Page 217 of 244

0S2

SHEARON HARRIS NUCLEAR POWER PLANT VALVE TEST TABLE

SYSTEM: SAFETY INJECTION

DWG. NO. 2165-5-1310

VALVE NUMBER	CLASS AND DWG. COOR.	VALVE (CAT.)	SIZE (IN.) AND TYPE	ACTU. TYPE	NORM. POSIT.	TEST REQ.	STROKE DIRECT.	CHECK VALVE TEST DIRECT.	C.S. JUST. OR RELIEF REQ.NO.	C.S. OR ALT. TEST PERF.	REMARKS	REV. NO.
151-357	1 E-2	AC	6 CX	SA	C	FS-1 LK-3	ş	FF	CS-1	FF-2	NOTE 16	,
151-358	1 E-2	AC	6 CX	SA	C	FS-1 LK-3		∠ FF	CS-1	FF-2	NOTE 16	
151-359	2 B-4	٨	10 GA	но	C Í	FS-1 TS-1 PI-5 LK-3	O C				NOTES 17,6	1
						•					1	

,

Page 218 of 244

PUMP AND VALVE INSERVICE TESTING PROGRAM PLAN

FOR

SHEARON HARRIS NUCLEAR POWER PLANT

SECTION 5.6.28

VALVE TEST TABLES AND RELIEF REQUESTS

FOR

CONTAINMENT WASTE PROCESSING

DWG. NO. 2165-5-1313

052



Page 219 of 244

, , ,

v

1.	\sim

14

SYSTEM: <u>CONTAINMENT WASTE PROCESSING</u>

NO. NOTE 1. Containment Isolation Valves.



ISI-203 Rev. 6

Page 220 of 244



SHEARON HARRIS NUCLEAR POWER PLANT VALVE TEST TABLE

SYSTEM: CTMT. WASTE PROCESSING

DWG. NO. 2165-S-1313

0S2

VALVE NUMBER	CLASS AND DWG. COOR.	VALVE (CAT.)	SIZE (IN.) AND TYPE	ACTU. TYPE	NORM. POSIT.	TEST REQ.	STROKE DIRECT.	CHECK VALVE TEST DIRECT.	C.S. JUST. OR RELIEF REQ.NO.	C.S. OR ALT. TEST PERF.	REMARKS	REV. NO.
1ED-119 .	2 E-17	A	3 DA	MA	LC	PV LJ-3					NOTE 1	_,,
1ED-121	2 E-16	A	3 GL	AO	0	FS-1 TS-1 FC-1 P1-5 LJ-3	C		•		NOTE 1	·
1ED-125	2 D-16	A	3 DA	AO	0	FS-1 TS-1 FC-1 P1-5 LJ-3	С				NOTE 1	•
1ED-161	2 C-7	A	3/4 DA	AO	0	FS-1 TS-1 FC-1 P1-5 LJ-3	C				NOTE 1	
1ED-164 .	2 E-6	A	3/4 DA	AO	0	FS-1 TS-1 FC-1 P1-5 LJ-3	C .	-		-	NOTE 1	



ISI-203 Rev. 6

PUMP AND VALVE INSERVICE TESTING PROGRAM PLAN

FOR

SHEARON HARRIS NUCLEAR POWER PLANT

SECTION 5.6.29

VALVE TEST TABLES AND RELIEF REQUESTS

FOR

COMPONENT COOLING WATER

DWG. NO. 2165-S-1319 2165-S-1320 2165-S-1321 2165-S-1322 2165-S-1322 S01

.

•

,

×

``

NO.

1.

2.

3.

4.

5.

6.

7.

8.

9.

NOTE

One of the three pumps is an installed spare. During normal operation one pump is running, a second pump aligned to automatically start if the running pump fails and the third is electrically disabled. Only those valves associated with the operating and reserve pumps will be tested. When, one of these is removed from service and the installed spare put into service, valve operability will be verified and section XI testing initiated.

Pump Discharge Check Valves. Reverse flow closure required to prevent recirculation flow back across the idle reserve pump.

Header Cross-tie Block Valves. Valves used to isolate Trains for Post-LOCA system alignment.

Sample System Block Valves. Valves close on a S signal.

Sample System Return Check Valve. Valve is relatively large and reverse flow closure is required to prevent excessive leakage from the system.

Thermal relief valves added to the program to comply with North Carolina State Requirements.

CCW to RHR Heat Exchanger Block Valves. Valves open when RHR is in operation.

Excess Letdown and Reactor Coolant Drain Tank Line Block Valves.

CCW to Reactor Coolant Pump Thermal Barriers. Cooling water must be provide at all times when RCS temperature is above 200 Degrees F.

ISI-203 Rev. 6

Page 223 of 244



SYSTEM: COMPONENT COOLING WATER

	NO.	NOTE
•	10.	CCW Inlet to Reactor Coolant Pump Thermal Barriers. Reverse flow closure required to prevent damage to CCW low pressure piping from excessive high pressure thermal barrier leakage.
	11.	Relief Valve which protects Safety- Related Equipment.
	12.	Containment Penetration Isolation Valve By-Pass Check Valve. Valve functions as a thermal relief when both CTMT. Pen. Isolation Valves are closed. Only Safety-Related function is to provide containment isolation.
	i3. ·	CCW to Gross Failed Fuel Detector Block Valves. Valves close on a S

signal.

14.

Containment Isolation Valve



.

.

•

•

.

, •

1,

·

'n

.

COLD SHUTDOWN TEST JUSTIFICATION

CS-1

System:

Component Cooling Water

Valve:

Category:

A(1CC-208,249,251,252,297,299)

1CC-207,208,249,251,252,297,299

Class:

2

B(1CC-207)

Function:

Test Requirements:

Basis for Relief:

Alternate Testing:

Component Cooling Water to the Reactor Coolant Pump Thermal Barriers and Bearing Oil Coolers.

Exercise and Time.

These are the Containment Isolation and Block valves in the RCP thermal barrier and bearing oil coolers lines. A loss of cooling water for more than a few minutes could result in extensive damage to the Reactor Coolant Pumps. Westinghouse Document 1B5710-100-07A states that . cooling water must be provided to the pumps at all times when the RCS temperature is above 200 degrees F. Because of local temperature variations in the RCS at RCS temperature near 200 degrees F, at least one RCP may be kept in operation during short duration cold shutdowns where the RCS temperature is maintained near 200 degrees F. It is felt that under these conditions stopping cooling water to the operating pump could contribute to pump degradation and result in unneccessary pump repairs.

Exercise and time at cold shutdown, when the RCS temperature is less than or equal to 200 degrees. It is our intent to perform this test when the corresponding RCP can be stopped.

ISI-203 Rev. 6

• · · · ·

. .

7 , . .



VALVE

RELIEF REQUEST

<u>RV-1</u>

Component Cooling Water

System:

Valve:

1CC-211,250,298

AC

Category:

Class:

Function:

Requirement:

Test

2 Containment Isolation Simple Check Valve (reverse flow closure for containment isolation only).

Verify reverse flow closure.

Basis for Relief: The only method available to verify reverse flow closure is by valve leak testing during Appendix J, Type C, testing at refueling.

Alternate Testing: Reverse flow closure will be verified during Appendix J, Type C, testing at refueling.



ISI-203 Rev. 6


t

, .

,

N N `

VALVE

RELIEF REQUEST

<u>RV-2</u>

System:

Valve:

Component Cooling Water

1CC-216,227,238

С

3

Category:

Class:

Function:

Test Requirement:

Basis for Relief:

Alternate Testing:

These Check Valves will close to protect the low pressure CCW piping from RCP Thermal Barrier Leakage.

Verify Reverse flow Closure.

The Westinghouse RCS Pumps must have cooling water to the bearing oil coolers and thermal barriers at all times when the RCS temperature is above 200 degrees F. and there are no installed taps or position indicators that could be used to verify reverse flow closure. Any possible test involves verification of these and associated upstream non-safetyrelated check valves as a single unit. To verify reverse flow closure at cold shutdown would involve draining large segments of the system and providing an alternate source of pressurized water inside the containment which may not be accessible during cold shutdown. Also, this test would involve waste processing of the water removed for testing and of the water used for testing. This type of testing would involve an excessive amount of time and personnel and could cause delays in plant startup.

One valve will be disassembled and visually inspected at refueling and alternate valves will be done during subsequent refuelings. Only one valve will be inspected at a refueling unless it fails to pass inspection. Failure to pass inspection will initiate disassembly and inspection of the other two valves.

ISI-203 Rev. 6

Page 227 of 244

~

SYSTEM: COMPONENT COOLING WATER

. DWG. NO. 2165-S-1319

VALVE NUMBER	CLASS AND DWG. COOR.	VALVE (CAT.)	SIZE (IN.) AND TYPE	ACTU. TYPE	NORM. POSIT.	TEST REQ.	STROKE DIRECT.	CHECK VALVE TEST DIRECT.	C.S. JUST. OR RELIEF REQ.NO.	C.S. OR ALT. TEST PERF.	REMARKS	REV.
100-33	3 E-8	C	18 CK	SA	0/C	FS-1 85-1		FF 8S			NOTES 182	_ _
1CC-50	3 K-8	с	18 CK	SA	0/C	FS-1 BS-1		FF BS			NOTES 182	
100-64	3 H-8	C	18 CK	SA	0/C	FS-1 BS-1		FF BS			NOTES 182	
1CC-99	3 F-17	В	18 BF	мо	0	FS-1 TM-1 PI-5	С				NOTE 3	
100-113	3 G-17	8	18 BF	Ю	0	FS-1 TM-1 P1-5	C				NOTE 3	•
ICC-114	3 F-18	В	4 DA	AO	0	FS-1 TM-1 FC-1 PI-5	C ,			÷	NOTE 4	
100-115	3 F-18	В	4 DA	AO	0	FS-1 TM-1 FC-1 P1-5	C				NOTE 4	
1CC-118	3 H-2	C	4. CK	SA	0/C	FS-1	•	BŞ			NOTE 5	
1CC-119	3 1-2	С	4 CK	SA	0/C	FS-1	•	BS			NOTE 5	



Page 228 of 244

· • • .

• • • ι. .

• • • •

-

· ·





SYSTEM: COMPONENT COOLING WATER

DWG. NO. 2165-S-1319

VALVE NUMBER	CLASS AND DWG. COOR.	VALVE (CAT.)	SIZE (IN.) AND TYPE	ACTU. TYPE	NORM. POSIT.	TEST REQ.	STROKE DIRECT.	CHECK VALVE TEST DIRECT.	C.S. JUST. OR RELIEF REQ.NO.	C.S. OR ALT. TEST PERF.	REMARKS	REV. NO.
1CC-127	3 H-3	В	18 8F	HO	0	FS-1 TM-1 P1-5	C				NOTE 3	
100-128	3 G-3	B	18 BF	мо	0	FS-1 TM-1 P1-5	C				NOTE 3	
100-129	3 G-4	С 3	74 X 1 RL	SA	C F	RL-4					NOTE 6	



SYSTEM: COMPONENT COOLING WATER

DWG. NO. 2165-S-1320

VALVE NUMBER	CLASS AND DWG. COOR.	VALVE (CAT.)	SIZE (IN.) AND TYPE	ACTU. TYPE	NORM. POSIT.	TEST REQ.	STROKE DIRECT.	CHECK VALVE TEST DIRECT.	C.S. JUST. OR RELIEF REQ.NO.	C.S. OR ALT. TEST PERF.	REMARKS	REV.
1CC-145	3 8-8	C	1 X 2 RL	SA	C	RL-4	L	L			NOTE 6	1
100-147	3 A-7	Β.	12 GA	мо	с	FS-1 TH-1 P1-5	0				NOTE 7	
100-165	3 L-8	C .	IX2 RL	SA	C	RL-4					NOTE 6	
100-167	- 3 L-7	B	12 GA	MO	C	FS-1 TH-1 P1-5	0				NOTE 7	



0S2

Page 230 of 244

r **`**

•

ı.

•

•

SYSTEM: COMPONENT COOLING WATER

DWG. NO. 2165-S-1321

	T				1							
VALVE NUMBER	CLASS AND DWG. COOR.	VALVE (CAT.)	SIZE (1N.) AND. TYPE	ACTÙ. TYPE	NORM. POSIT.	TEST REQ.	STROKE DIRECT.	CHECK VALVE TEST DIRECT.	C.S: JUST. OR RELIEF REQ.NO.	C.S. OR, ALT. TEST PERF.	REMARKS	REV. NO.
	I						<u> </u>					
1CC-176	· 2 D-3	B	6 GA	МО	0	FS-1 TS-1 P1-5	C				NOTES 8,14	
1CC-186	2 D-8	C	3/4 X 1 RL	I SA	C	RL-4	•		ŀ	r	NOTES 6,14	
1CC-194	2 E-8	С	3/4 X 1 RL	SA SA	C	RL-4				<i>p</i>	NOTES.6,14	
100-202	2 8-10	A	6 GA	мо	°.	FS-1 TS-1 P1 -5	C			-	NOTES 8,14	
100-207	2 E-1	`В	6 GA	мо	0	FS-1 TM-1 P1- <u>5</u>	C	4	CS-1 CS-1	FS-2 TM-2	NOTE 9	•
1CC-208	2 F-1	•	6 GA	МО	0	FS-1 TH-1 P1-5 LJ-3	С	v	CS-1 CS-1	FS-2 TM-2	NOTĘS 9,14	
1CC-211	2 [:] F-1	AC	6 CK -	SA	0	FS-1 LJ-3		BS	RV-1	SP-3	NOTE 9,14	
1CC-216	3 [.] N-2	C	2 CK	SA	0	FS-1		BS	RV-2	DS	NOTE 10	
100-219	3 N-4	с : `	3/4 X 1 RL	SA	C	RL-4	I				NOTE 11	



• . .

.

.

ų

e

n • · · ·

y

SYSTEM: COMPONENT COOLING WATER

DWG. NO. 2165-S-1321

1 T			T I				1		<u> </u>			
	01.400	VALVE	0.75	40771	1000				C.S.	c.s.		
VALVE MUNDED	ULASS	VALVE	SIZE	AU(U.	NORM.	TEST	STROKE	CHECK	JUST.	OR	REMARKS	REV.
VALVE NUMBER		(CAI.)	(14.)	ITPE	POSTI.	REQ.	DIRECT.	VALVE	OR	ALT.		
l I	Und.		AND					TEST	RELIEF	TEST		NO.
	шж.		ITPE	-				DIRECT.	REQ.NO.	PERF.		
-							1	,	*	I		L
1CC-227	3	C	2	SA	0	FS-1		BS	RV-2	- DS	NOTE 10	
	N-5		CK				1					
1CC-230	3	C :	3/4 X 1	SA	С	RL-4					NOTE 11	
	N-8		RL		-							•
100-238	3	C	2	SA	0	FS-1		BS	RV-2	DS	NOTE 10	
e.	N-9		CK									
100-241	3	c :	3/4 X 1	SA	С	RL-4					NOTE 11	
	N-11		RL	•							1012 11	
100-240	2	i		100	•	FC 1	•				`	
100-249	2 C_15	~	4	MU	U	FS-1	C		CS-I	FS-2	NOTES 9,14	•
	r-13		бл			13-1 DI-5			US-1	1 S- 2		۳
		•				1.1=3						
						LU-J						
100-250	2	AC	3/4	SA	С	FS-1		BS	RV-1	SP-3	NOTES 12.14	
-	F-15	4	СК			LJ-3						
100-251	2	A	4	мо	0	FS-1	c		1-20	55-3	NOTES O 14	•
	E-15		GA		•	TS-1	Ŭ		CS-1	TS-2	MU125 9,14	
				,		P1-5			···· ,	10 2		
						LJ-3			_			
					•				-			
1CC-252	2	A	4	MO	0	FS-1	C		CS-1	FS-2	NOTE 9	
	D-14		GA			TS-1			CS-1	TS-2		
						PI-5						
1CC-294	2	C 3	5 X 4	SA	Ċ	RL-4		,			NOTE 11	
۲.	F-12		RL									
100-297	2	A	6	мо	0	FS-1	'n	h	CS-1	56-2		
	- F-12		GA		~	TS-1	.0	•	03-1 CS-1	r3=2 TS_2	NU125 9,14	
						PI-5	•		-1	13-2		
						LJ-3						



a.

SYSTEM: COMPONENT COOLING WATER

DWG. NO. 2165-5-1321

VALVE NUMBER	CLASS AND DWG. COOR.	VALVE (CAT.)	SIZE (IN.) AND TYPE	ACTU. TYPE	NORM. POSIT.	TEST REQ.	STROKE DIRECT.	CHECK VALVE TEST DIRECT.	C.S. JUST. OR RELIEF REQ.NO.	C.S. OR ALT. TEST PERF.	REMARKS	REV. NO.
. 100-298	2 F-13	AC	3/4 CK	SA ·	C .	FS-1 LJ-3	×	BS	R¥→1	SP-3	NOTE 12	
100-299	2 E-12	۸	6 GA	МО	ο	FS-1 TS-1 P1-5 LJ-3	C	•	ເຊ-າ ເຊິ່	FS-2 TS-2	NOTES 9,14	



SYSTEM: COMPONENT COOLING WATER

DWG. NO. 2165-S-1322

0101 1101 2103	0 1244											
	CLASS	VALVE	SIZE	ACTU.	, NORM.	TEST	STROKE	СНЕСК	C.S. JUST.	C.S. OR	REMARKS	REV.
VALVE NUMBER	AND	(CAT.)	(IN.)	TYPE	POSIT.	REQ.	DIRECT.	VALVE	OR 3	ALT.		, ,
	UWG.		AND					TEST	RELIEF	TEST		NO.
	шж.							DIRECT.	REQ.NO.	PERF.		
- 1CC-304	3	в	3/4	AO	0	FS-1	C				NOTE 13	
	A-6		GA		•	TH-1	•					
						FC-1						
					•	P1-5						
100-305	3	в	3/4	AO	0	FS-1	С			•	NOTE 13	
	A-6		GA			TM-1						
1						FC-1		•		*		
						PI-5						
100-322	3 J-2	C :	3/4 X 1 RL	SA	ເ່	RL-4					NOTE 6	
100-335	3 J-5	C :	3/4 X 1 RL	SA	С	RL-4			-		NOTE 6	•
1CC-352	3 J-7	C	3/4 X 1 RL	SA	C	RL-4		•	•		NOTE 6	
100-355	3 J-10	C	3/4.X 1 RL	SA	С	RL-4					NOTE 6	
100-362	3 J-12	C 3	3/4 X 1 RL	SA	ເໍ	RL-4					NOTE 6	-
100-313	3 E-5	C 3	3/4 X 1 RL	SA .	C	RL-4					NOTE 6	





COMPONENT COOLING WATER

DWG. NO. 2165-S-1322 SOI

VALVE NUMBER	CLASS AND DWG. COOR.	VALVE (CAT.)	SIZE (IN.) AND TYPE	ACTU. TYPE	NORM. POSIT.	TEST REQ.	STROKE DIRECT.	CHECK VALVE TEST DIRECT.	C.S. JUST. OR RELIEF REQ.NO.	C.S. OR ALT. TEST PERF.	REMARKS	REV. NO.
1CC-381	3 H-3	C :	3/4 X 1 RL	I SA	C	RL-4	, ,				NOTE 6	
100-397	3 E-6	C	3/4 X 1 RL	I SA	C	RL-4					NOTE 6	
1CC-520	3 E-14	C	3/4 X 1 RL	I, SA	C	RL-4					NOTE 6	
100-534	3 H-10	C	3/4 X 1 RL	SA SA	С	RL-4					NOTE 6	



SYSTEM:

PUMP AND VALVE INSERVICE TESTING PROGRAM PLAN

FOR

SHEARON HARRIS NUCLEAR POWER PLANT

.

SECTION 5.6.30

VALVE TEST TABLES AND RELIEF REQUESTS

FOR

RESIDUAL HEAT REMOVAL

DWG. NO. 2165-5-1324



SYSTEM: RESIDUAL HEAT REMOVAL

NO.

1.

2.

3.

Boundary values between high pressure RCS and the low pressure RHR. Values are maintained closed during normal operation and are Pressure Isolation Values.

NOTE

Relief Valve which protects Safety-Related Equipment.

RHR Cross-tie to the CVCS opens for Safety-Related modes of operation.

RHR Heat Exchanger Outlet Flow Control Valves. Valves are used to control flow during RHR System operation. Valves are normally open, fail open and are maintained open with the controller for LPCI mode of operation. Test only the fail open feature for Section XI testing.

RHR Pump Min. Flow Line Block Valves. Valves close to prevent recirculation flow and to prevent flow diversion during system operation.

RHR System LHSI Line Check Valves. Reverse flow is required to prevent flow recirculation through the idle pump. Forward flow is verified using the 8 inch test line which is adequate to verify full flow operability of these 10 inch Valves.



5.

6.

ISI-203 Rev. 6

COLD SHUTDOWN TEST JUSTIFICATION

<u>CS-1</u>

System:

RESIDUAL HEAT REMOVAL

Valve:

1RH-1,2,39,40

Α

1

Category:

Class:

ASME Section XI Quarterly Test Requirements:

Cold Shutdown Test Justification:

Quarterly Part Stroke Testing:

Cold Shutdown Testing: Exercise and Time.

These are boundary valves between the high pressure Reactor coolant System and the low pressure Residual Heat Removal System piping. The valves are interlocked to RCS pressure and can not be opened with RCS pressure greater than 425 psig. Defeating the interlocks to perform testing is not desirable since they are pressure isolation valves. If the inline valves were inadvertently opened during testing an Inter-System-LOCA could occur.

Partial valve exercising is precluded for the same reasons as full stroke exercising.

Exercise and Time.





. . .

¥

•

٤

.

-

-

*

SYSTEM: RESIDUAL HEAT REMOVAL

DWG. NO. 2165-S-1324

VALVE NUMBER	CLASS AND DWG. COOR.	VALVE (CAT.)	SIZE (IN.) AND TYPE	ACTU. TYPE	NORM. POSIT.	TEST REQ.	STROKE DIRECT.	CHECK VALVE TEST DIRECT.	C.S. JUST. OR RELIEF REQ.NO.	C.S. OR ALT. TEST PERF.	REMARKS	REV. NO.
18H-1	1	Α	12	мо	С	FS-1	0	I	, CS-1	FS-2	NOTE 1	
	L-3	,	GA 、			TS-1 P1-5 LK-3	C		CS-1	TS-2		,
1RH-2	1	A	12	MO	С	FS-1	0		CS-1	FS-2	NOTE 1	
	L-4		GA			TS-1	С		CS-1	TS-2		
						P1-5						
	h					LK-3						
1 RH- 7	2 H-6	C :	3 X 3 RL	SA	• C	RL-4		×		1	NOTE 2	
1RH-25	2	8	8 [′]	мо	C	FS-1	0				NOTE 3	•
	C-12		GA		,	TH-1						
						P1-5						
184-30	2	8	10	AO	0	F0-1	0 .			-	NOTE A	*
-	C-11	-	BF		•	TM-1	•				1012 4	
			۳			P1-5				я		
104 71	•	•	-		' •							
16-11	2 H-7	в	С GA	MU	0	FS-I TV-1	С.				NOTE 5	
•			0.1			PI-5	٩					-
		,						•				•
1RH-34	2	C	10	SA	C	FS-1	•	FF	1		NOTE 6	
	C-7		CK			8S-1		BS				
1RH-39	1	A	12	мо	С	FS-1	0		CS-1	FS-2	NOTE 1	
	1-3		GA		•	TS-1	c		CS-1	TS-2		
	ŗ			•		PI-5					*	
						LK-3						
184-40	t	A	12	що	c	EC1				50.0	NOTE	
	1-4	~	GA		U	rs=1 TS=1	с. С.		i-دی 1=دی	r3-2 TS-2	NULE I	
						PI-5	~		φ υ Ι	13-2		
						LK-3					,	

.

SYSTEM: RESIDUAL HEAT REMOVAL

DWG. NO. 2165-S-1324

1	1					_	T	T	7			
	CLASS	VALVE	SIZE	ACTU.	NORM.	TEST	STROKE	CHECK	C.S. JUST.	C.S. OR	REMARKS	REV.
VALVE NUMBER	ANU	(CA1.)	(IN.)	ITPE	PUSIT.	REQ.	DIRECT.	VALVE	OR	ALT.		
	DWG.		AND					TEST	RELIEF	TEST		NO.
	COOR.		TYPE					DIRECT.	REQ.NO.	PERF.		
l	· ·						<u>l. </u>					
104-45	2	C	3 7 3	CA	c	DI						
1141-42	2 V_6	U U	2 2 2	SN	C	ru=4					NULE 2	
	<u> </u>		RL,		h							
184-63	. 2	в	8	МО	C	ES-1	0				· NOTE 3	
	- F-12	0	GA		•	TM-1	Ŭ					
	• • • •					PI-5						
									•			
1RH-66	2	в	10	AO	0	F0-1	0				NOTE 4	
	E-11		BF		-	TM-1	-					
						P1-5						
1RH-69	2	в	3	ŇO	0	FS-1	С				· NOTE 5	
	H-8		GA			TH-1						
						P1-5						-
1RH-70	2	C	10	SA	C	FS-1		FF			NOTE 6	
al.	E-8		CK			BS-1		8S				
									•			
1RH-120	2	C :	3/4 X 1	SA	C	RL-4					NOTE 2	
	L-4		RL				•					
					•							
1RH-121	2	С :	3/4 X 1	SA	С	RL-4					NOTE 2	
	1-4		RL.									



PUMP AND VALVE INSERVICE TESTING PROGRAM PLAN

FOR

SHEARON HARRIS NUCLEAR POWER PLANT

SECTION 5.6.31

VALVE TEST TABLES AND RELIEF REQUESTS

FOR

CONTAINMENT INTEGRATED LEAKAGE DETECTION

DWG. NO. 2166-S-916



ISI-203 Rev. 6

,	SYSTEM:	CTMT	LEAK	DETECTION		
	,	NO.	•	1. a	NOTE	*
	- -	1.		t	Locked Closed Manual Isolation Valves.	Containment
	•					
				-		

ISI-203 Rev. 6

Page 242 of 244



, · · ·

·

a

,

k.

SYSTEM: CTMT. LEAK DETECTION

DWG. NO. 2166-S-916

VALVE NUMBER	CLASS AND DWG. COOR:	VALVE (CAT.)	SIZE (IN.) AND TYPE	ACTU. TYPE	NORM. POSIT.	TEST REQ.	STROKE DIRECT.	CHECK VALVE TEST DIRECT.	C.S. JUST. OR RELIEF REQ.NO.	C.S. OR ALT. TEST PERF.	REMARKS	REV. NO.
1LT-V1 .	2 F-3	A	8 GA	НА	LC	PV LJ-3					NOTE 1	
1LT-V2	2. F-7	A	1 GL	МА	LC	PV LJ-3	•				NOTE 1	
1LT-V4	2 G-7	A	1 GL	MA	. LC	PV LJ-3	μ,				NOTE 1	

Page 243 of 244

. 052



6.0 DIAGRAMS/ATTACHMENTS

0S2



ISI-203 Rev. 6

Page 244 of 244 '



3

U

ŝ