REACTOR CONTAINMENT BUILDING INTEGRATED LEAK RATE TEST REPORT

1991 Turkey Point Unit #4 ILRT Date of Test Completion: October 20, 1991

Prepared by the Turkey Point Nuclear Plant Test And Performance Group. Florida Power And Light Co.

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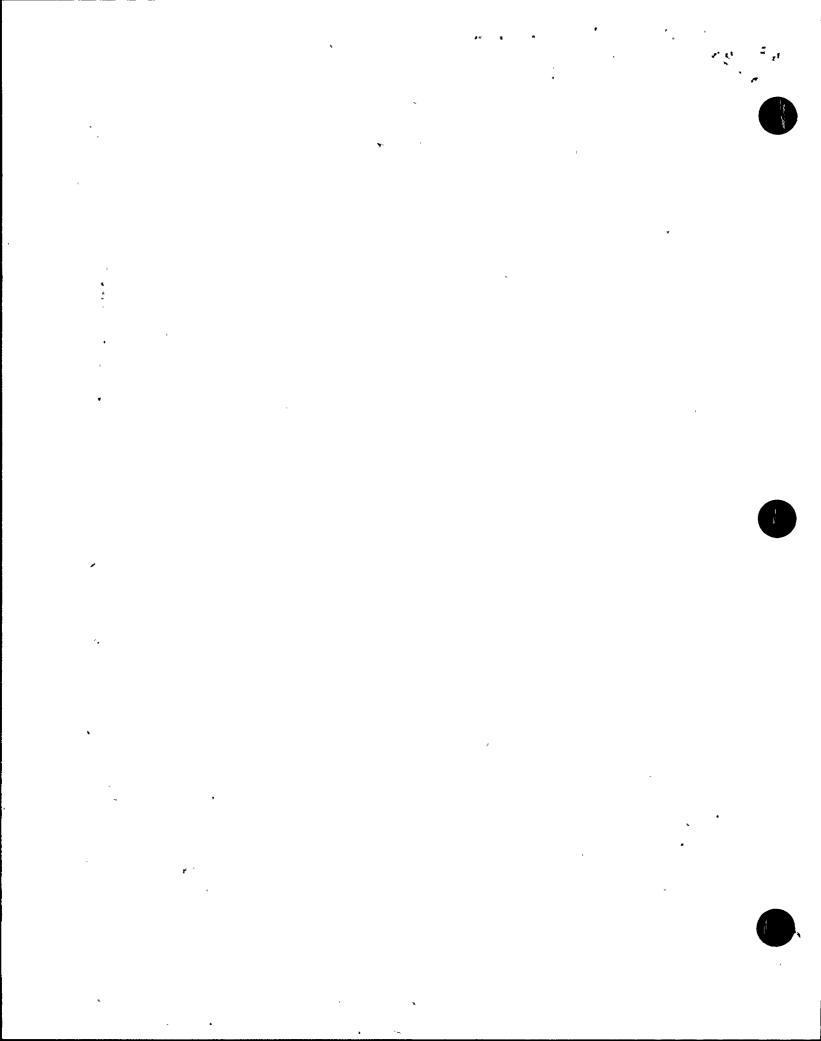


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I. INTRODUCTION AND PURPOSE

A periodic Type "A" Integrated Leakage Rate Test (ILRT) was successfully conducted on the primary containment structure of the Florida Power and Light's Turkey Point Nuclear Power Plant Unit No. 4 Pressurized Water Reactor. This test was performed in accordance with the Plant's Technical Specifications, and the Code of Federal Regulations, Title 10, Part 50, Appendix J, titled: "Primary Reactor Containment Leakage Testing for Water Cooled Power Reactors".

This report describes the test method used, and presents the results of the test, including the Supplemental Test (also known as the Controlled Leakage Rate Test, or CLRT), used for verification. Summaries of the types "B" and "C" Local Leakage Rate Tests (LLRT) performed since the last ILRT are also included.

Turkey Point Nuclear Plant Operating Procedures OP 13100.1, 13100.4 and 13404.1 provided necessary guidance during the performance of these Tests.

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II. TEST DISCUSSION

A. Description of the Containment

The containment structure completely encloses the reactor and reactor coolant system. It is the last barrier between fission materials and the environment.

Containment pressure retention is achieved by concrete walls that are post tensioned by a steel tendon system. Leakage prevention is achieved by a 0.25 inch steel liner on the inside of the containment wall.

Under accident conditions, leakage out of containment is not expected to exceed a predetermined amount. A periodic Leak Testing Program of the containment penetrations and structural inspections help assure containment leakage will not exceed the expected amount.

Applicable Containment Specifications:

Inside diameter = 116 ft. Inside height = 169 ft.

Approximate free volume = 1,550,000 cubic feet

Calculated peak accident pressure = 49.9 psig

Analyzed Leakage = La = 0.25 % Per day of air mass inside Containment at 49.9 psi.

Acceptance Criteria
for the ILRT = 0.75 * La
= 0.1875 % Per day of air mass inside
Containment at 49.9 psi.

During the performance of the ILRT, the containment penetrations and isolation valves were aligned per OP-13100.4 to simulate as closely as possible the post Accident Containment Configuration. Adjustments to the test's results were made for any valve lineups not representative of post LOCA configuration, and for any level increases noted during the test for vessels located inside Containment.

B. Description of the ILRT Instrumentation

The Containment Building was instrumented to permit leakage rate determination in accordance with the Code of Federal Regulations, Title 10, Part 50, Appendix J, "Primary Reactor Containment Leakage Testing for Water Cooled Power Reactors".

The ILRT instrumentation provided a sufficient quantity of sensors of each type to accommodate instrument failures during the test without jeopardizing acceptability of the test's results.

The instrumentation allowed leakage rate determination by the Mass Point Analysis. This method calculates the actual mass

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of dry air within the Containment. The leakage rate becomes the time rate of change of the calculated air mass. (M) is calculated according to the Ideal Gas Law as follows:

$M = 144 * ((P-P_V)*V)/R*T$

M = Containment Air Mass (Lbs)

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P = Containment Total Absolute Pressure, Psia T = Containment Absolute Temperature, Deg R

P_V= Containment Vapor Pressure, Psia, at Temp. T. V = Containment Net Free Volume, Ft³

R = Universal Gas Constant (Ft*Lbf/Lbm*Deg R)

(P., and T are weighted average values.)

The primary measurement variables required for the calculation of Containment air mass are absolute pressure, relative humidity and temperature as a function of time. During the Supplemental Test, a controlled Containment bleed off flow is also a measured variable.

The average Containment absolute temperature is determined by measuring specific local temperatures throughout the Containment and applying a mass and volume weighted averaging technique. The volume fraction for each temperature sensor is determined based upon geometrical calculations.

Average Containment water vapor pressure is determined by measuring specific local relative humidities throughout the Containment. This is converted to local vapor pressure using local group temperatures, a steam table, and a mass and volume weighted averaging technique. The volume fractions for the relative humidity sensors are determined in the same manner as for the temperature sensors. Wherever possible, Temperature and Relative Humidity Sensors were placed adjacent to each other.

1. Temperature Instrumentation

Twenty One (21) Platinum Resistance Temperature Detectors (RTDs) located throughout the Containment allowed measurement of the weighted average air temperature. Figure 1A through 1E depict the location of the RTDs in the Containment. Each RTD sensor has a calibrated resistance versus temperature curve accurate to less than ± 0.5 °F. The sensitivity and repeatability of each RTD sensor is less than ± 0.054 °F.

2. Humidity Instrumentation

Ten (10) Phys-Chem Relative Humidity Detectors (RHDs) located throughout the Containment allow measurement of the weighted average Containment vapor pressure. Figure 1A through 1E depicts the location of the RHDs in the Containment. RHDs connect to two, five channel Humeter amplifiers located outside the Containment. The calibrated accuracy of the RHDs is ± 2.0 % °F, the repeatability of the RHDs is ± 0.25 % RH and the sensitivity of the RHDs is ± 0.5 % °F. , t

3. Pressure Instrumentation

Two direct read out, Texas Instruments precision pressure monitors measured Containment absolute pressure. Figure 2 depicts the arrangement of the tubing connections between the monitors and the Containment. Only one pressure monitor was used for leakage rate calculations, with the second monitor as back-up in the event of failure. The monitors had a repeatability of ± 0.002 Psia.

4. Flow Instrumentation

A variable area float-type rotometer is used to superimpose a leakage during the Supplemental Test. Figure 5 depicts the piping configuration between the rotometer and the Containment. The rotometer has a $\pm 1.0\%$ accuracy, and a $\pm 0.5\%$ repeatability.

Two other instruments were used during the Supplemental Test. A local pressure gauge, and a PRTD were installed in the Containment vent piping, to allow for compensation in the event of substantial pressure or temperature deviation from the Rotometer's calibration point. The PRTD was connected to a Fluke 8520A/PRTD located in the same area as the test computer.

5. Atmospheric conditions

Ambient atmospheric conditions were monitored during the course of the test. Barometric pressure, temperature, wind speed and direction were obtained from Homestead Air Force Base Meteorological Facility. A summary of the information is contained in Appendix C.

6. Instrument Selection Guide (ISG) Calculation

The Instrument Selection Guide (ISG) compiled the instrument sensitivity and resolution for each process variable and evaluates the total instrumentation system's ability to detect leakage in the range required. The ISG for this test was calculated by the Computer Program used to compute the ILRT results. The calculated ISG for the instrumentation operable during this test (21 temperature sensors, 9 relative humidity sensors, and 1 pressure sensor) was 0.0054 % per day, which was verified to be less than .25 La as specified in ANSI 56.8.

C. Description of the Computer Program

Florida Power and Light utilized software developed by Ebasco Plant Services Inc. for leakage rate calculations during the course of the test. The Program is an interactive program written specifically for fast, easy utilization during all phases of the ILRT and Supplemental Test. The program is written in a high level, compiled, structured language and operates on a MS-DOS personal microcomputer. Besides providing extensive data verification routines, the program offers the flexibility of calculating leakage rates and the

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95 % Upper Confidence Levels utilizing Total Time or Mass Point Methods.

A given instrument may be deleted from the calculations if a sensor malfunctions. The deletion of a given instrument is performed on all samples in the data base. Volume fractions for the remaining instruments of that type are then recalculated based upon the placement and the amount of Containment volume sensed by these instruments.

Data evaluations are enhanced by the flexible display of either sensor variables or various computed values in tabular or graphical form on the computer screen or printer. Data is recorded on magnetic media to prevent loss during the test. In addition, two hard copies of the data are also made throughout the test by a printer attached to the test computer, and by the Datalogger's built in printer. All data is stored on the computer system in use, with retrieval capability to any desired data base throughout the testing.

Ancillary portions of the computer program assist the user in determination of temperature stabilization, determining the ILRT termination criteria, performing ISG calculations, and determination of acceptable Supplemental Test leakage verifications. It also allows the user to monitor instrument repeatability error, to aid in the identification of any malfunctioning sensors.

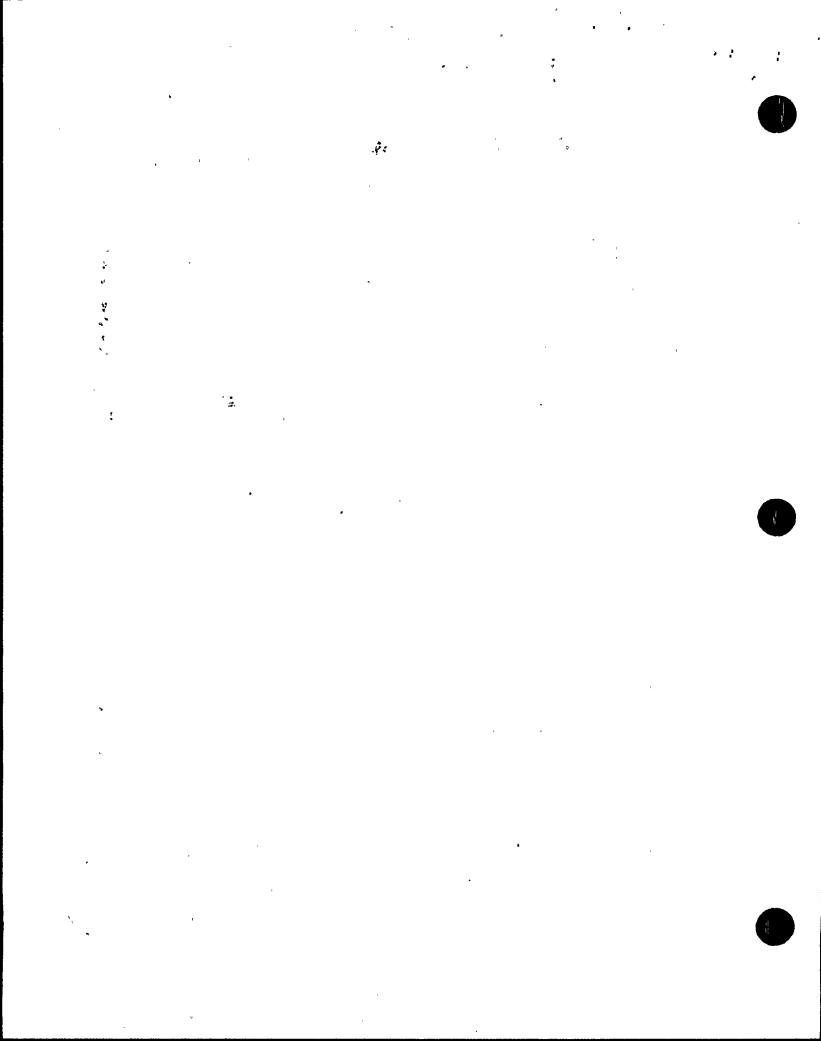
During the test, temperature, pressure and humidity data was automatically transmitted from the ILRT instrumentation system to the computer at approximately 20 minute intervals. Figure 3 illustrates the connection between the ILRT instrumentation system and the computer analysis system.

D. Containment Pressurization equipment.

The equipment used to pressurize the Containment is shown in Figure 4. The eight oil-free industrial diesel driven air compressors had a total nominal capacity of 11,100 SCFM. The compressed air was processed by a water cooled after-cooler, a moisture separator and a refrigerant air dryer.

E. Description of the Testing Sequence.

Preparations to pressurize the Containment for the conduct of the ILRT included internal and external inspections of the Containment structure; installation and checkout of the temporary ILRT instrumentation system; Types "B" and "C" Local Leakage Rate Testing of the Containment penetrations; alignment of the necessary valves and breakers for test conditions; the installation and checkout of the temporary Containment pressurization facilities; removal of plant instrumentation that could be damaged by the test pressure; venting of any permanently installed tanks that could be damaged by the test pressure; and the removal or depressurization of any pressurized gas sources inside Containment.



Containment pressurization started at 17:40 Hrs, 10-17-91, and was secured at 05:03 Hrs on 10-18-91 at a peak Containment pressure of 67.583 psia. The average pressurization rate throughout this time period was approximately 4.4 psi per hour. Appendix A1 illustrates the testing sequence.

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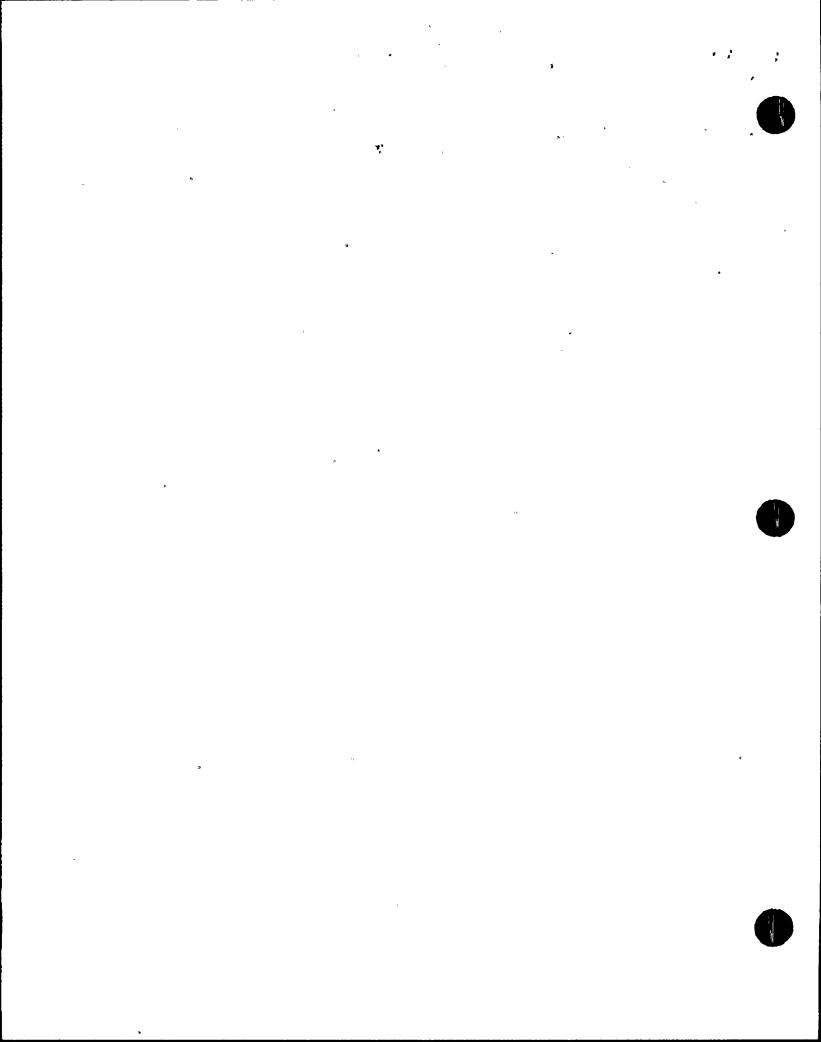
The temperature stabilization phase began at 05:04 Hrs on 10-18-91. External leakage surveys were initiated with no significant leakage found. The Mass Point temperature stabilization criteria was met at 10:04 Hrs on 10-18-91, and ILRT measurements were initiated. Appendix A2 contains the temperature stabilization results.

During the test, Containment vapor pressure and relative humidity were found to be higher than expected. This was attributed to a leak discovered, after the test, in a valve associated with the water cooled after-cooler. This higher than expected humidity caused fluctuations in containment pressure which in turn caused substantial deviations in calculated containment air mass. These deviations statistically would not support a short duration test as described in Bechtel Corporation's Topical Report BN-TOP-1, Revision 1, "Testing Criteria for Integrated Leakage Rate Testing of Primary Containment Structures for Nuclear Power Plants." At 10:04 Hrs, 10-19-91, all acceptance criteria for a 24 hour test was met, with Mass Point Upper Confidence Limit of 0.0540 %. The fitted Mass Point leakage rate was 0.0480 % per day. These values are well below the test acceptance criteria of 0.1875% per day. Appendix A3 contains the ILRT data and test results.

At 10:08 Hrs on 10-19-91, the Supplemental Test was started, and subsequently stopped due to condensation noted in the rotometer. The rotometer was disassembled for cleaning / drying, and the vent piping was insulated to allow the piping and Containment temperatures to equalize.

At 13:30 Hrs, 10-19-91, with the vent piping temperature stabilized, the Supplemental Test was re-started with an imposed leakage rate of 14 scfm. The fitted Supplemental Test leakage rate was 0.336 % per day. Appendix A4 contains the Supplemental Test data, results and acceptance criteria.

The Supplemental Test was completed at 17:35 Hrs on 10-19-91 with all acceptance criteria satisfied. Data analyses showed that RH Sensor #10 exceeded 100% relative humidity during the Supplemental Test. RH Sensor #10 was deleted, the remaining volume fractions recalculated, and all of the data for the ILRT and Supplemental Test re-analyzed. The other relative Humidity or temperature sensors in this group did not exhibit any unusual behavior and followed the expected process trend. The Data and the test results remained satisfactory for the recalculated values.



Containment de-pressurization was initiated at 18:04 Hrs on 10-19-91, and was completed at 02:45 Hrs on 10-20-91. Average de-pressurization rate was 6.75 psi per hour. Figure 6 illustrates the de-pressurization piping configuration.

Containment entry for post-test inspection was at 03:30 Hrs, 10-20-91. The post-test inspection detected no major anomalies or damage to the equipment or structures of the Containment.

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III. TEST RESULTS

A. Temperature Stabilization Phase Summary.

Temperature Stabilization was met in approximately five hours. The results and acceptance criteria of the Temperature Stabilization phase are presented in Appendix A2.

B. Integrated Leakage Rate Test Summary.
At the start of the testing sequence, the intent was to use the short duration method contained in Bechtel's Topical Report BN-TOP-1. However, due to the humidity problem mentioned in Section II, the test was converted to a 24 hour Mass Point Test. Appendix A3 contains detailed ILRT data.

Correction of ILRT Results.

Corrections were made to the ILRT results to account for any penetrations that could not be aligned to simulate the post Accident Containment Configuration and for any level increases noted during the test for the vessels located inside Containment. The following is a summary of these corrections and the final ILRT results.

Penetrations in service during ILRT

The following penetration leakage is required to be added to the results of the ILRT since the penetrations were isolated or could not be vented or drained during the Type A Test. The leakage assigned is the recorded as left value using minimum pathway analysis.

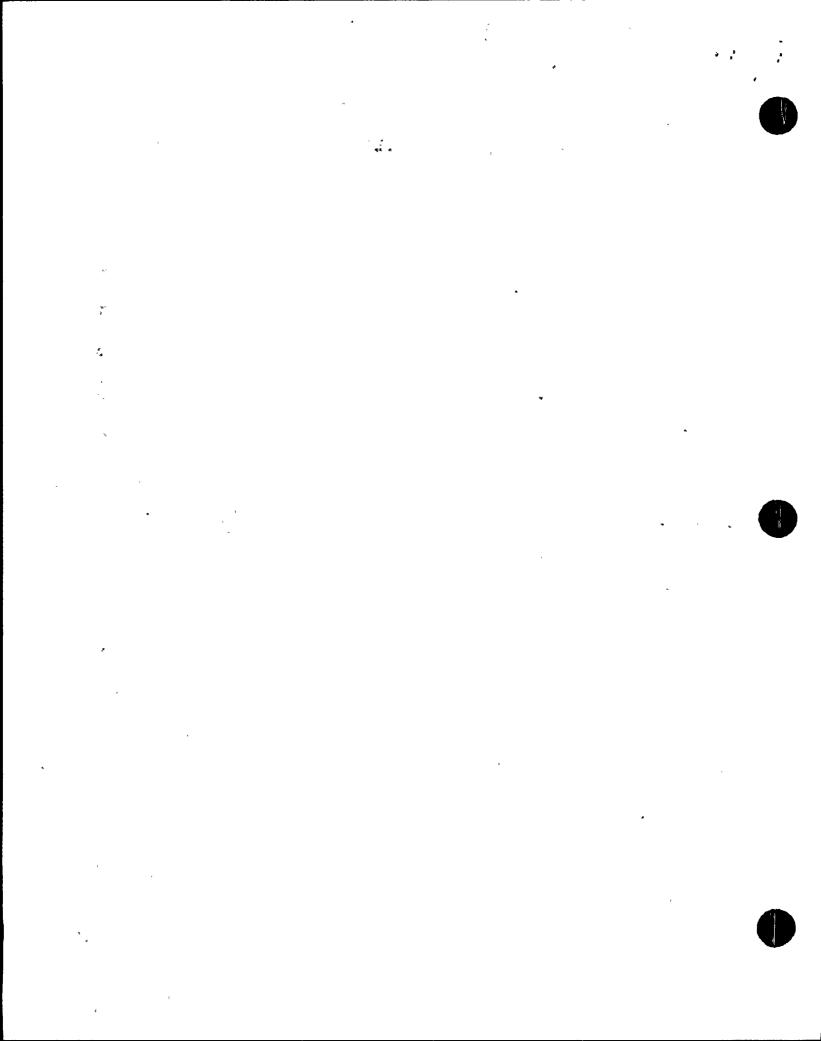
		Leakage (CCM):
11	ALT RHR	40
15	Charging	. 18
16	PACVÍS	18
24A	RCP Seal Inj.	160
24B	RCP Seal Inj.	, 620
24C	RCP Seal Inj.	35
51	PACV's	18
		

Correction to ILRT results = 909 CC/MIN

Summary of Containment levels

The following is a tabulation of various levels throughout Containment for which any unexplained increase must be accounted for in the results of the ILRT.

DATE: TIME:	<u>START</u> 10/18 10:00	END 10/19 17:30	DELTA	CORRECTION
RCDT LEVEL (%)	32 76 91 9	31 76 85 9	-1 0 -6 0	-1 0 -6 0
decrease in levels)	TOTAL	CORRE	CTION	= 0 %



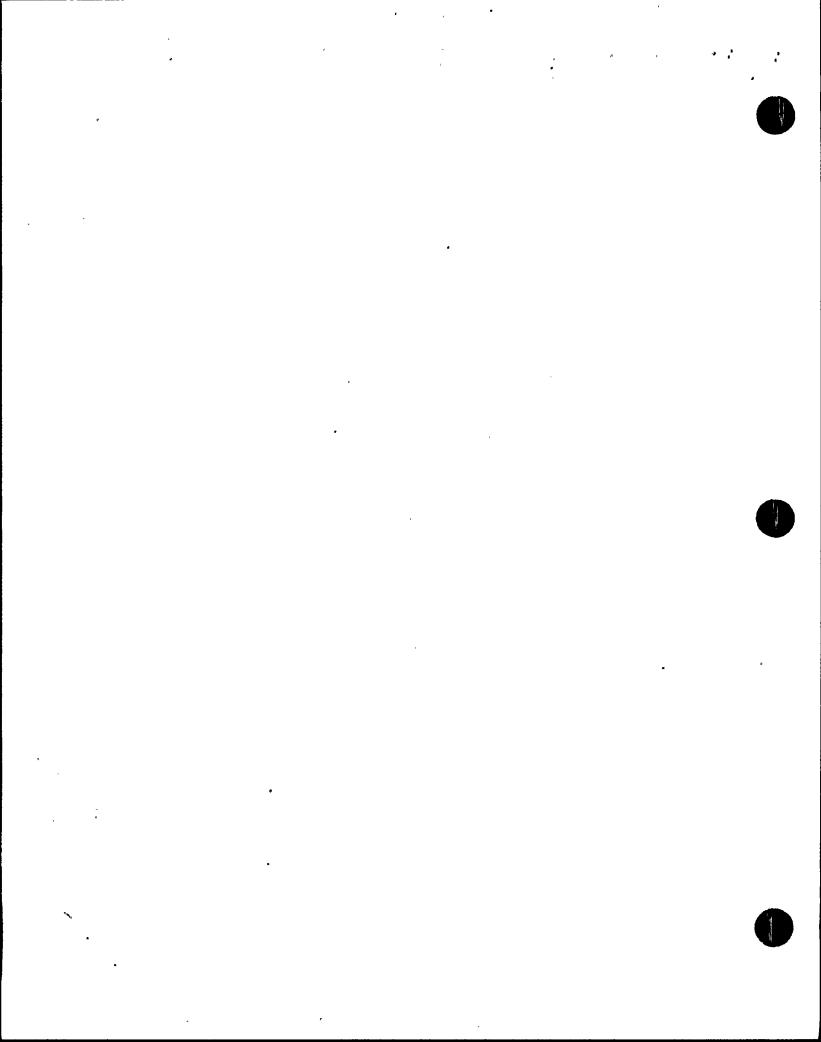
ILRT Results - Mass Point Analysis

- C. Supplemental Leakage Rate Test Summary.

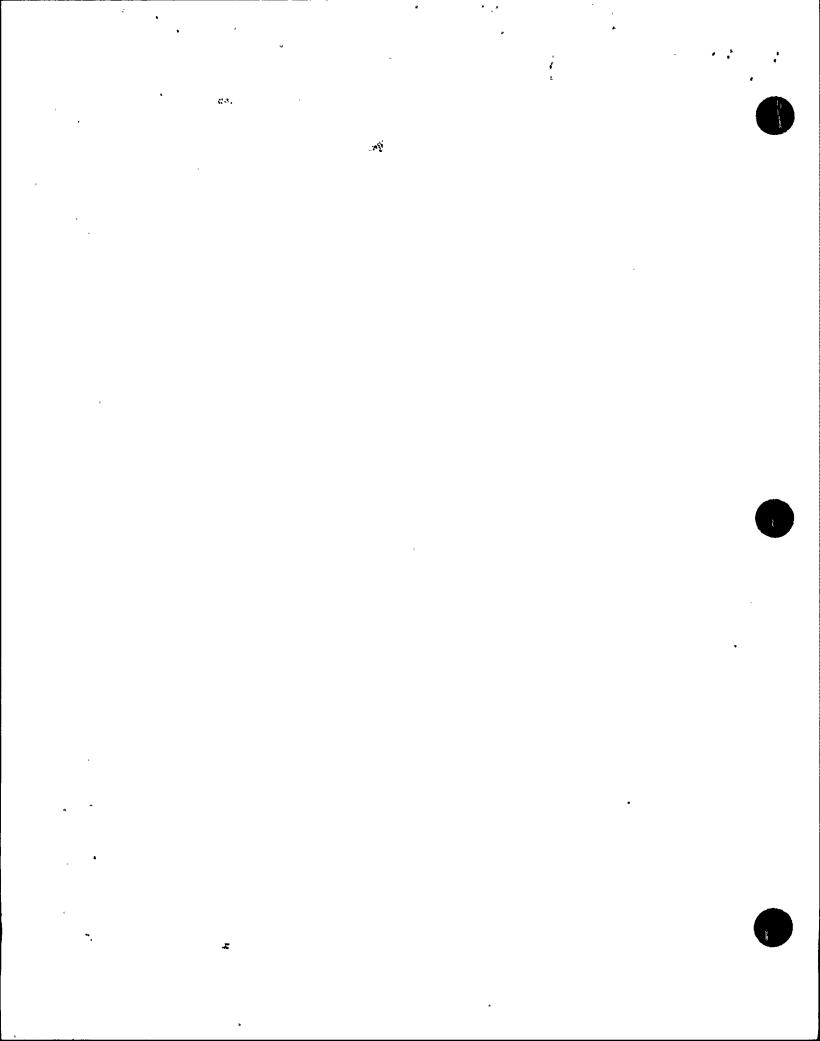
Following the acceptance of the ILRT results, a four hours Supplemental Test was added to the existing Containment leakage rate using the variable area rotometer.

Results are presented in Appendix A4. The test met the acceptance criteria for the verification phase. A summary follows:

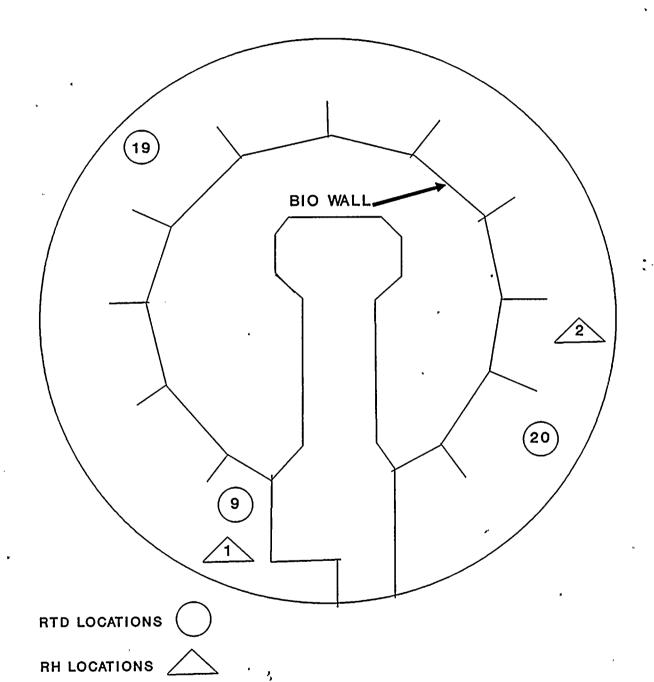
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SECTION IV. FIGURES



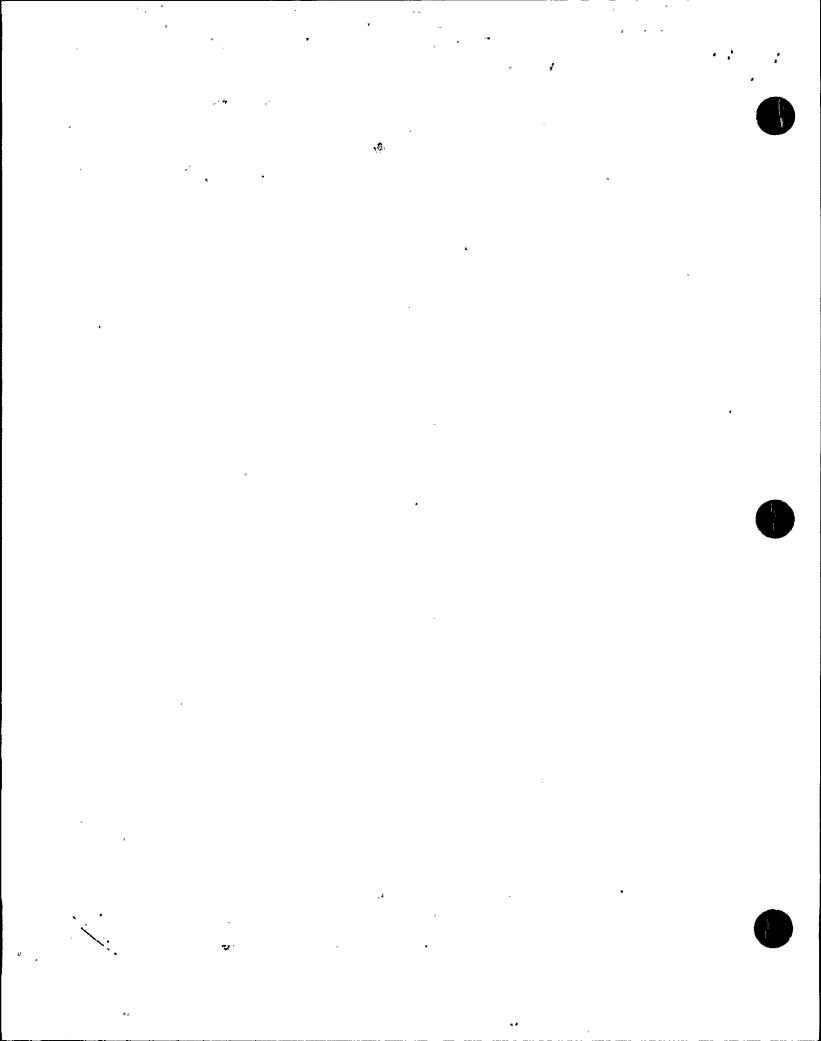
1991 TURKEY POINT UNIT 4 ILRT RTD/ RH SENSORS LOCATIONS INSIDE CONTAINMENT - TOP VIEW

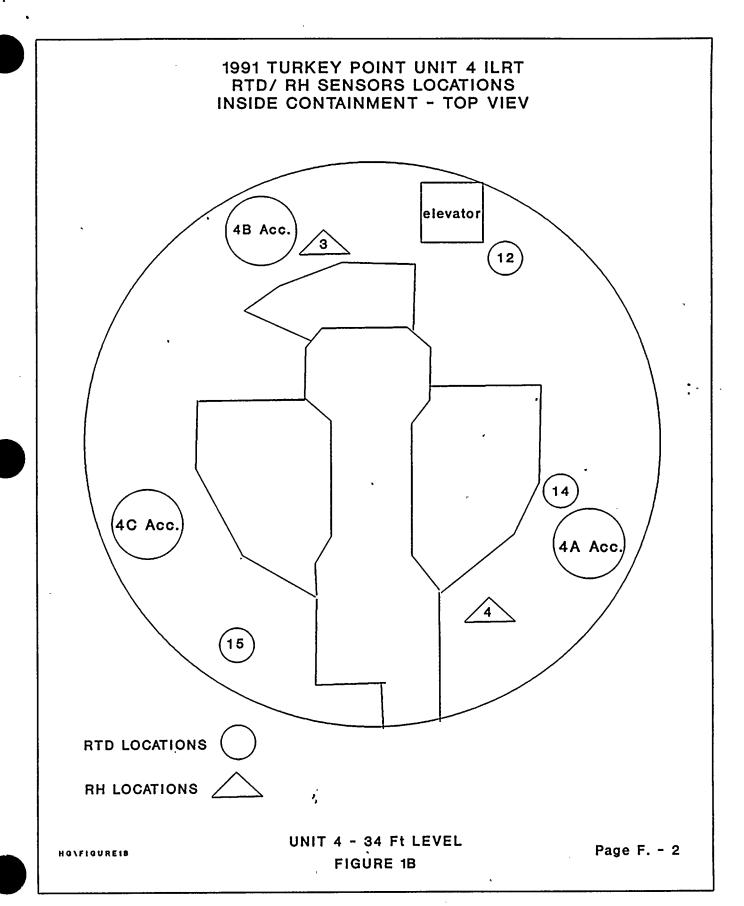


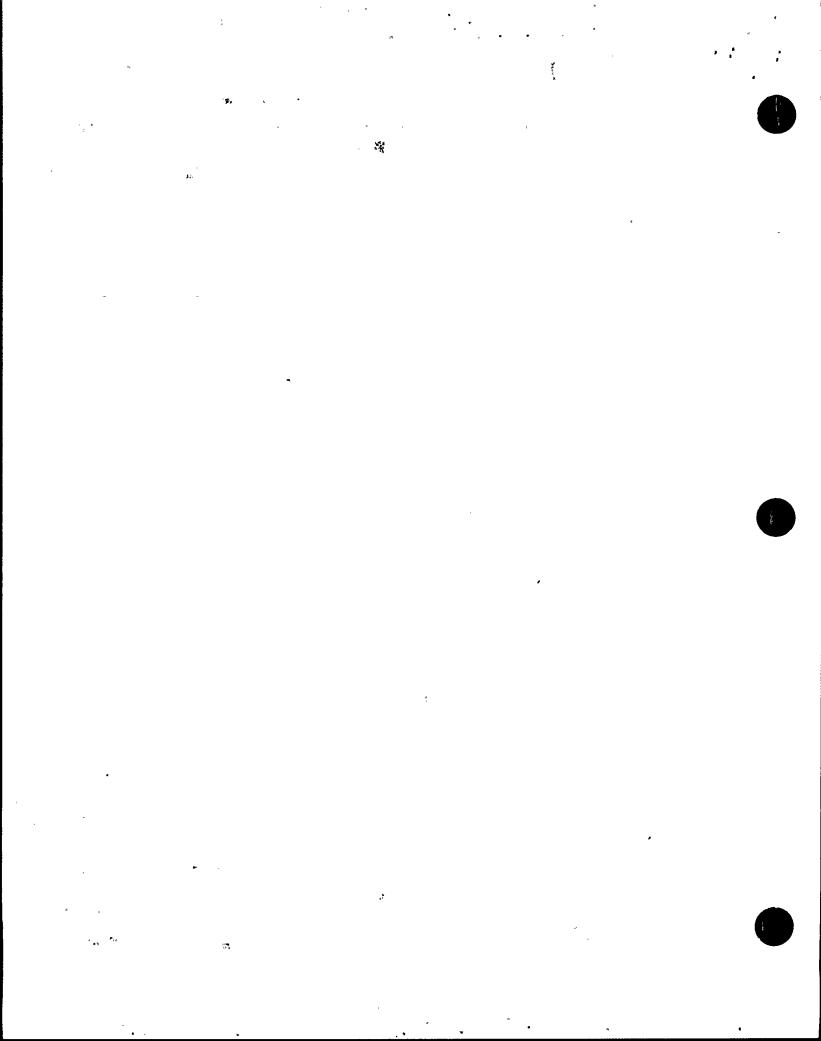
HQ\FIGURE1A

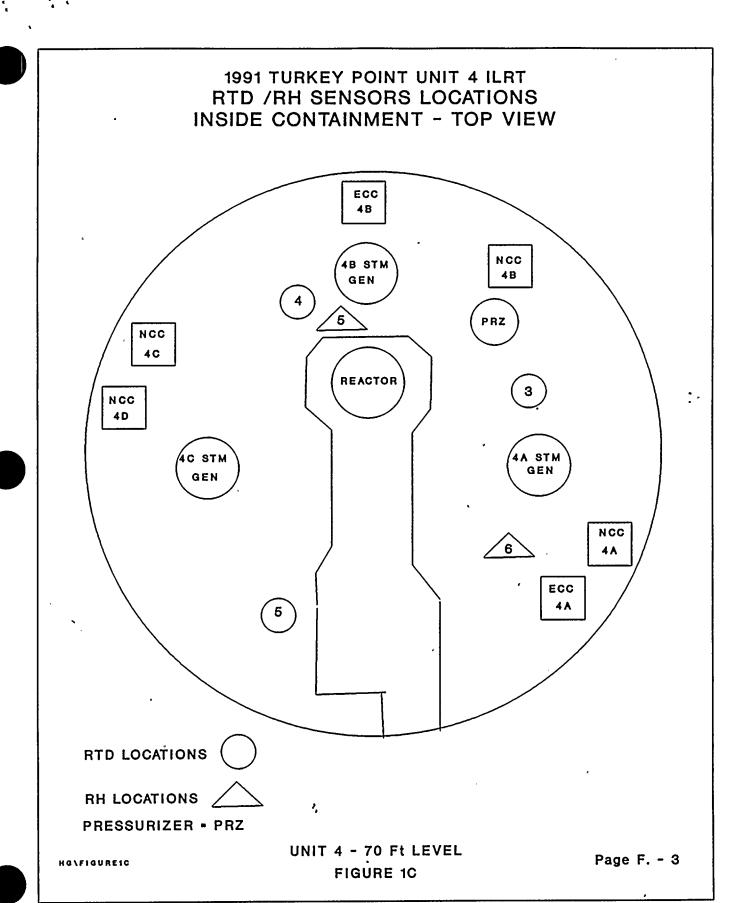
UNIT 4 - 19 Ft LEVEL FIGURE 1A

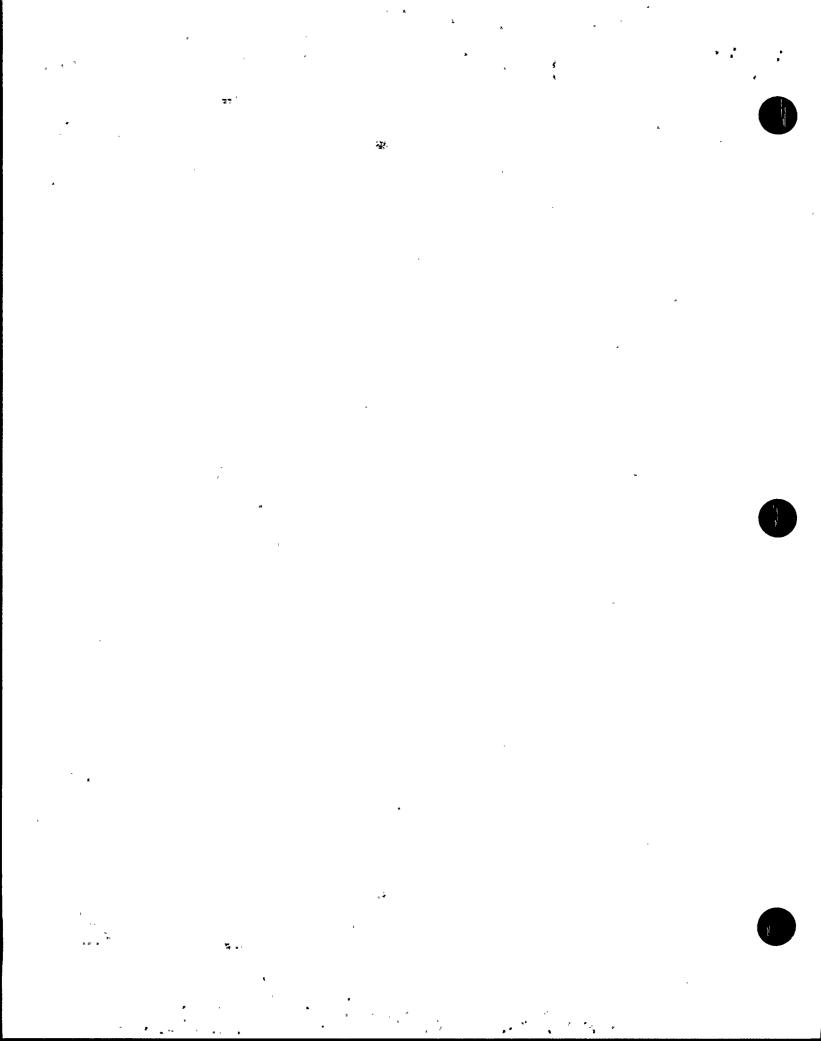
Page F. - 1



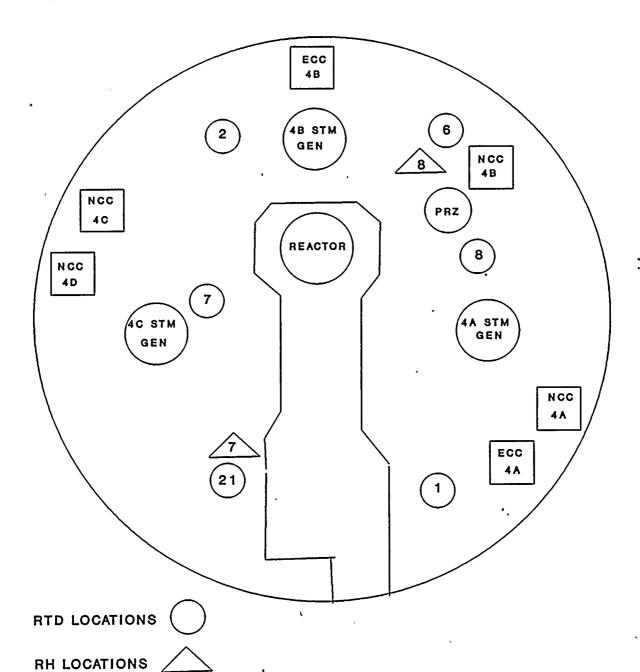












HG\FIGURE1D

PRESSURIZER - PRZ

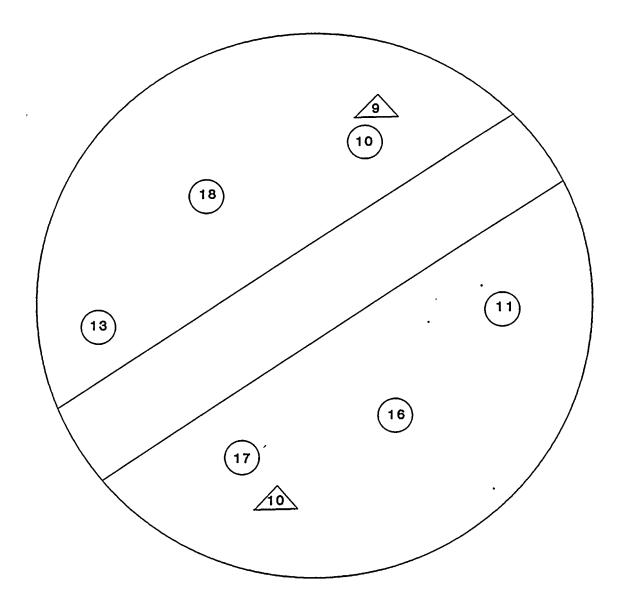
UNIT 4 - 94 Ft LEVĚL FIGÙRE 1D

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1991 TURKEY POINT UNIT 4 ILRT RTD /RH SENSORS LOCATIONS INSIDE CONTAINMENT - TOP VIEW

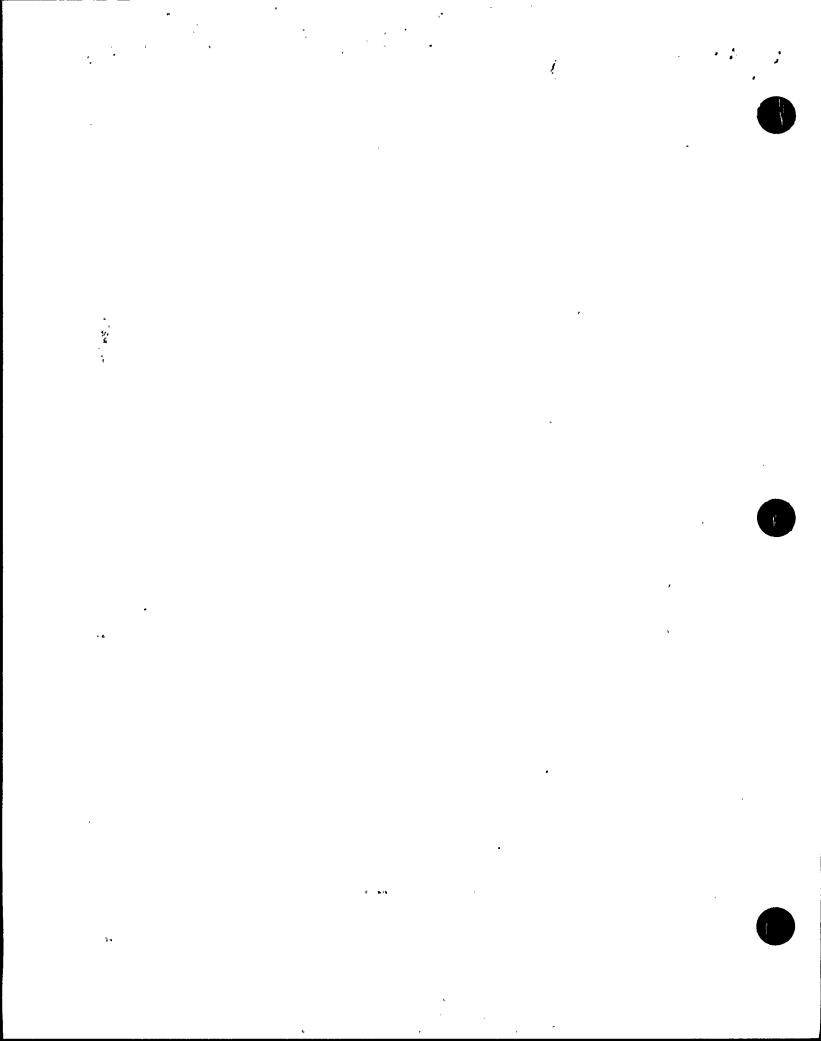


RTD LOCATIONS A

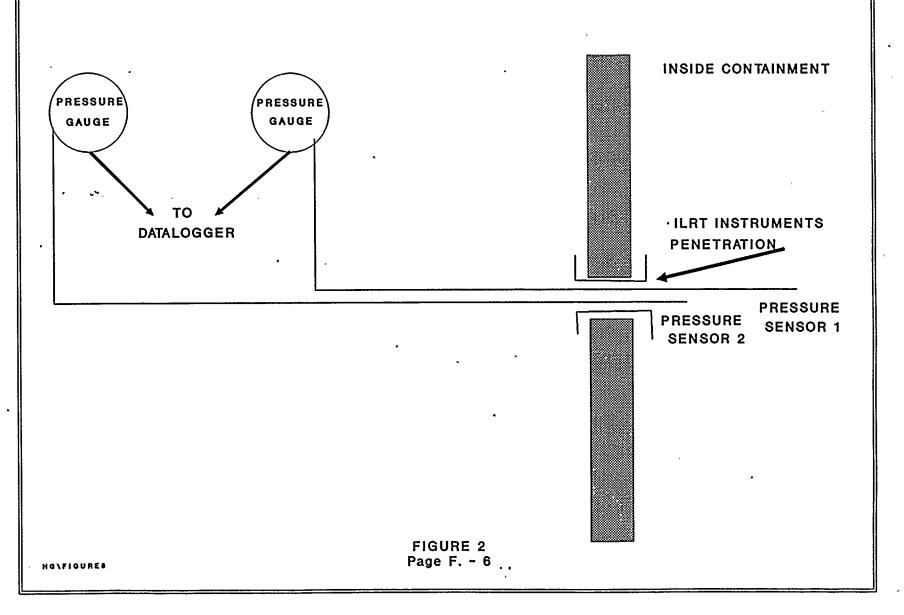
HG\FIGURE1E

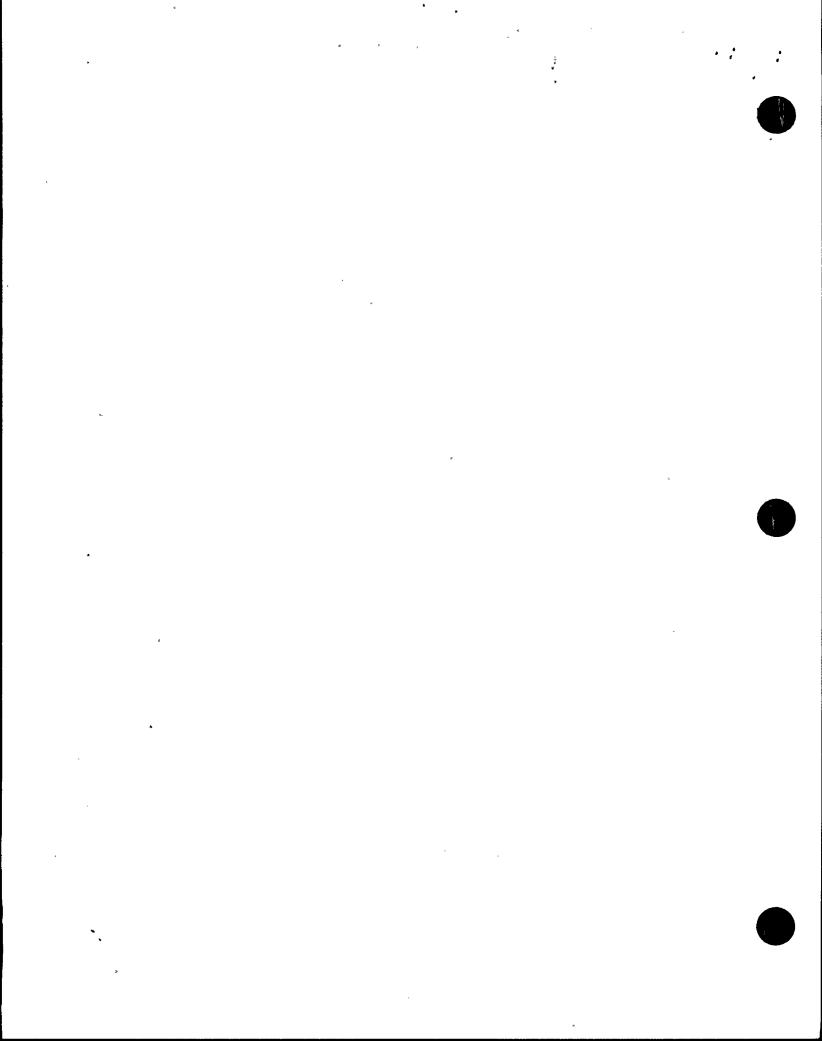
UNIT 4 - 143 Ft LEVEL FIGÜRE 1E

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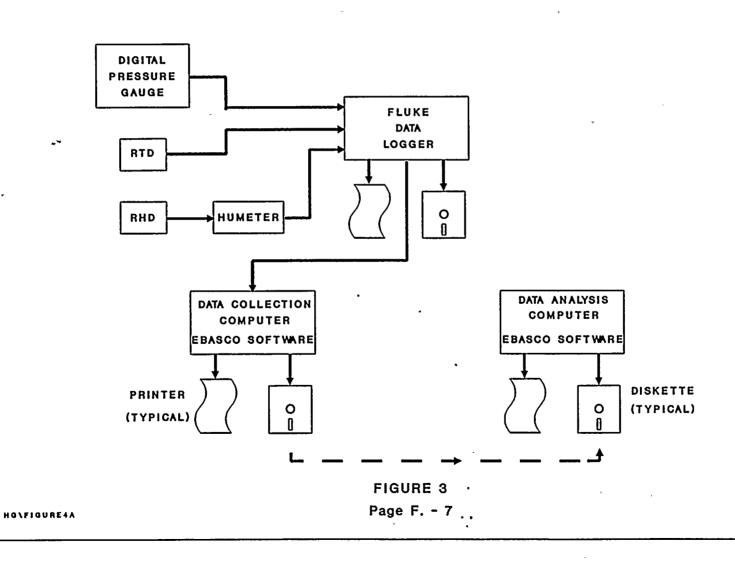


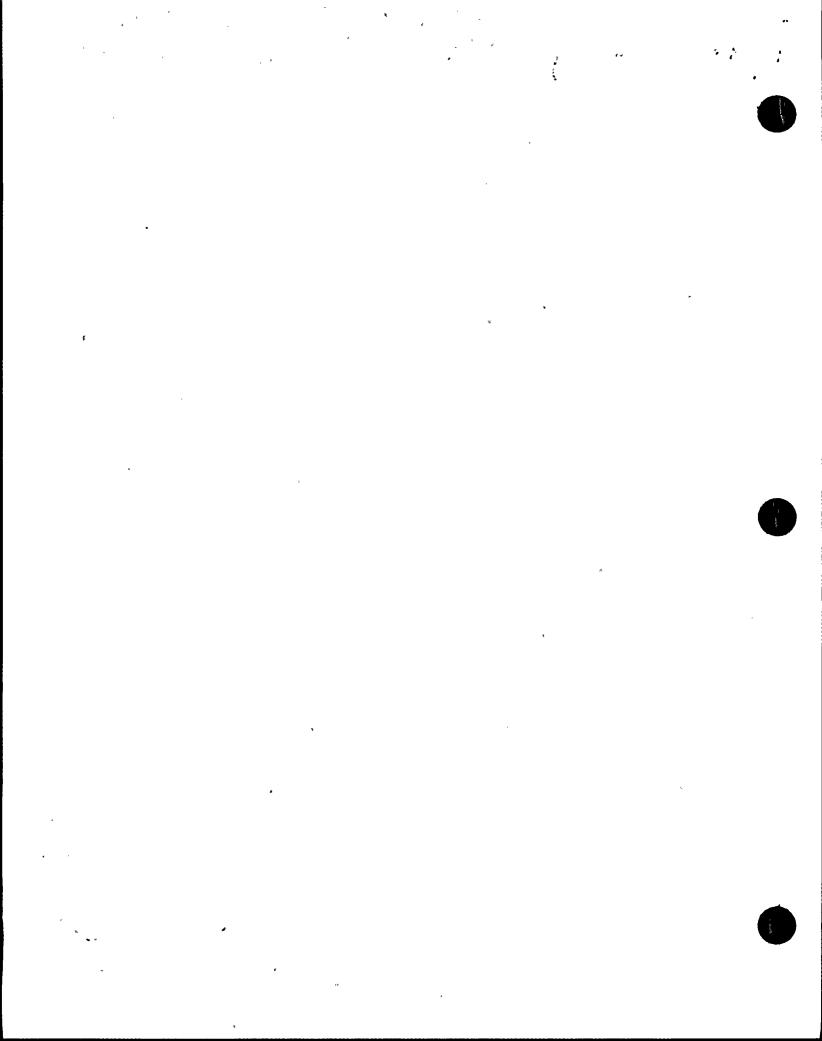
ILRT CONTAINMENT PRESSURE SENSOR PIPING¹¹ 1991 TURKEY POINT UNIT 4 ILRT



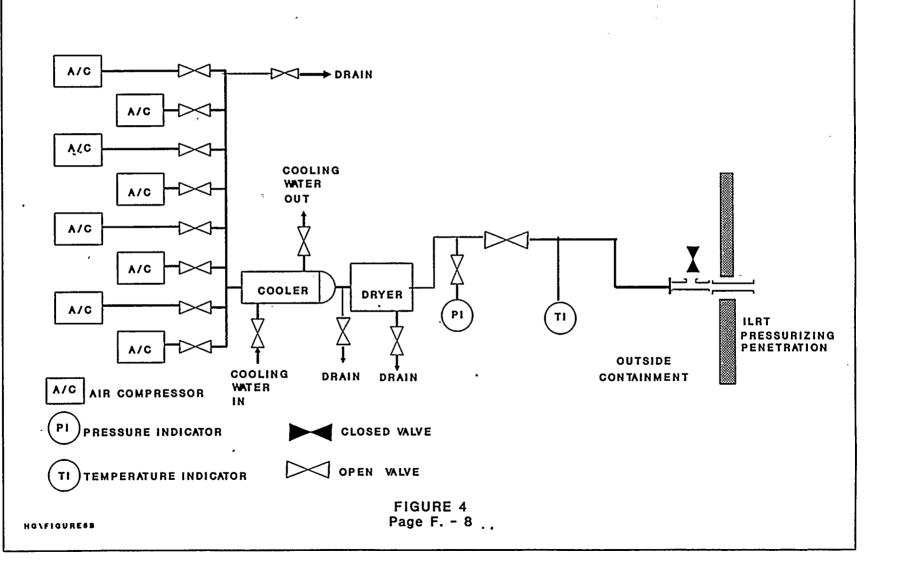


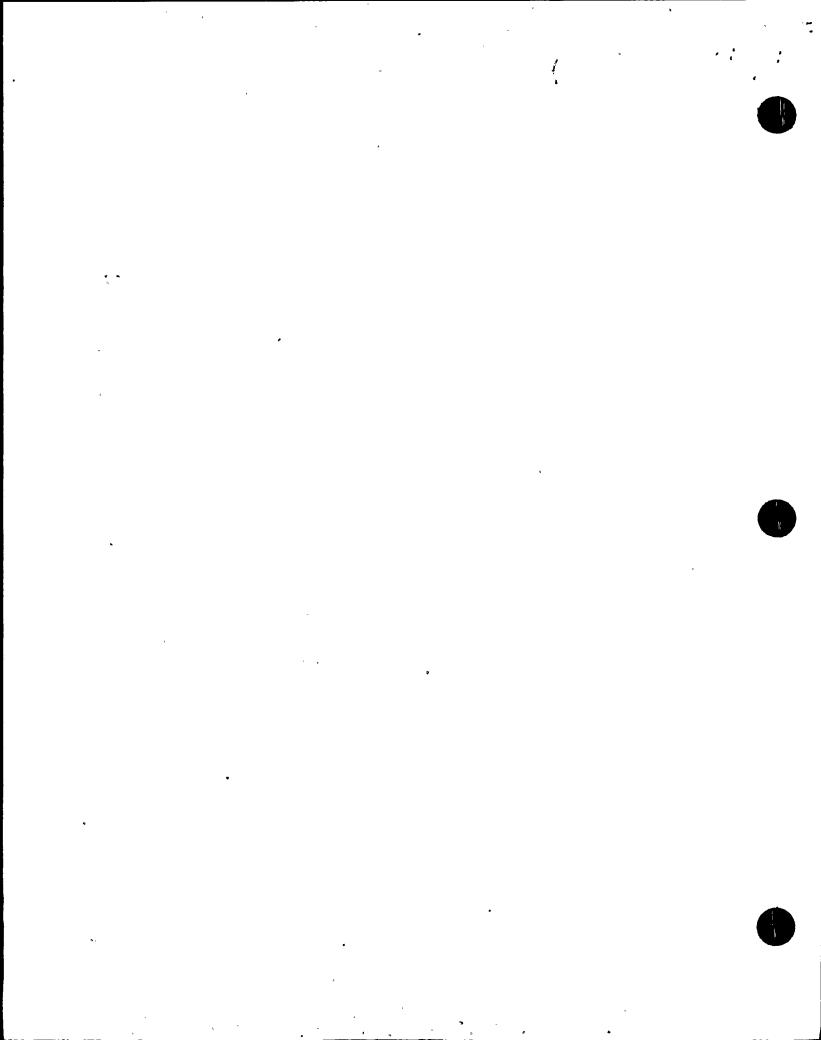
DATA COLLECTION, STORAGE AND ANALYSIS 1991 TURKEY POINT UNIT 4 ILRT



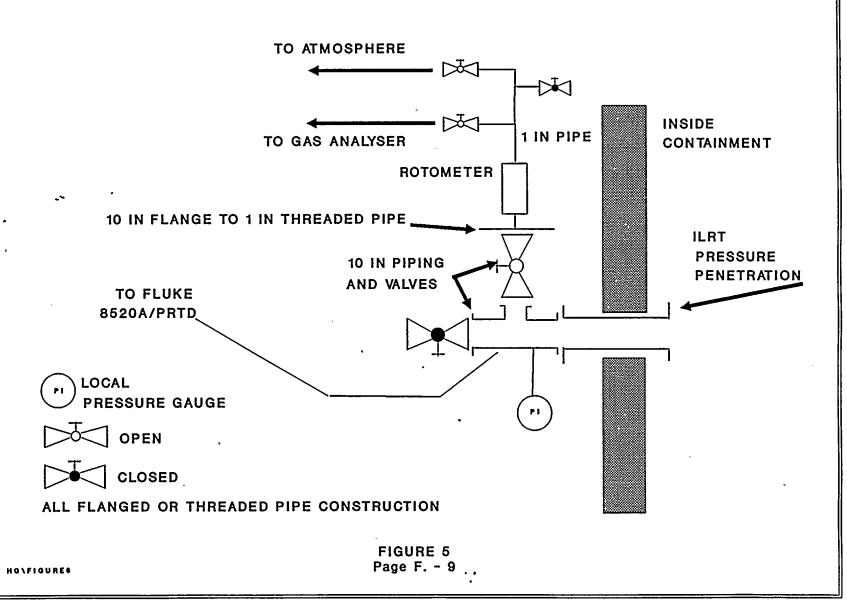


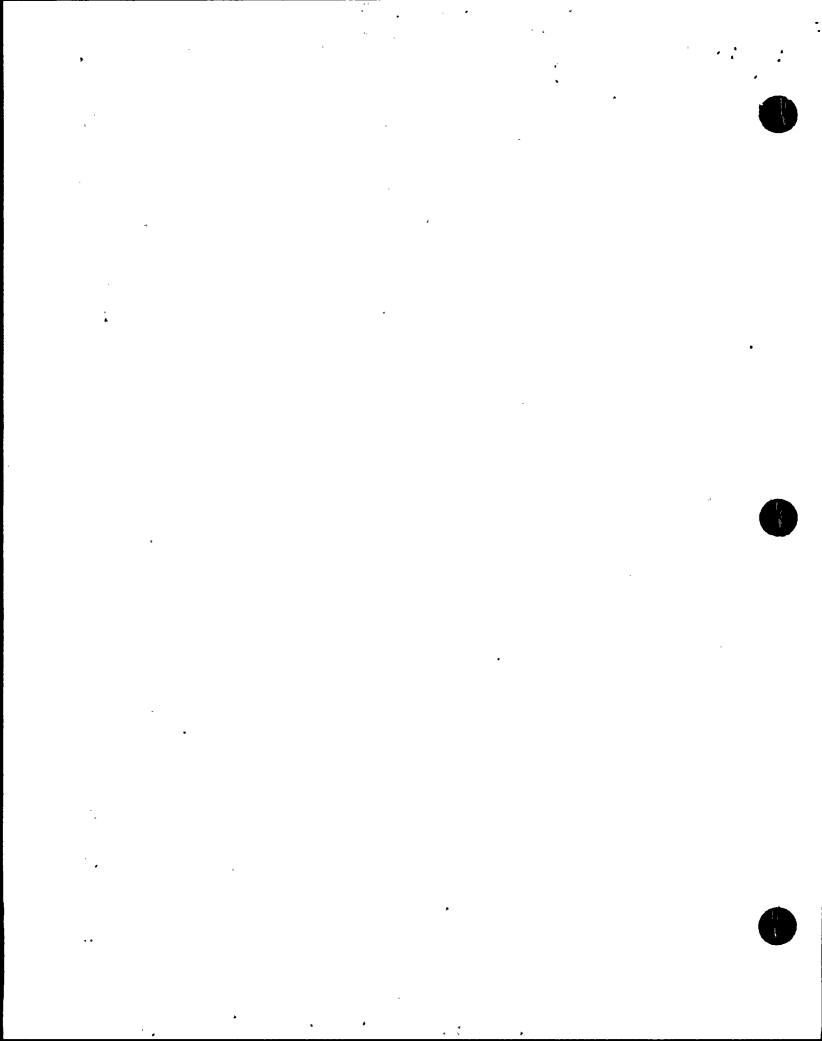
CONTAINMENT PRESSURIZATION SYSTEM 1991 TURKEY POINT UNIT 4 ILRT



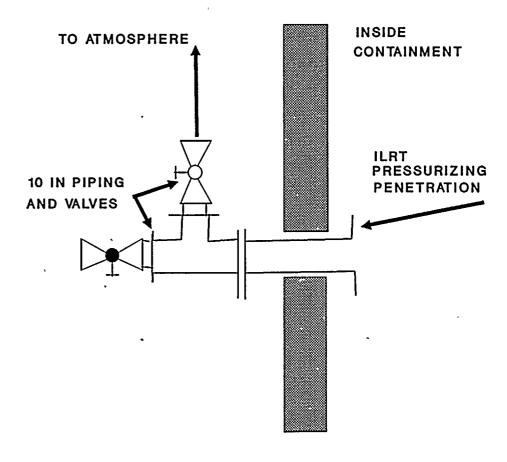


CONTROLLED LEAKAGE TEST PIPING 1991 TURKEY POINT UNIT 4 ILRT





ILRT VENT PIPING 1991 TURKEY POINT UNIT 4 ILRT



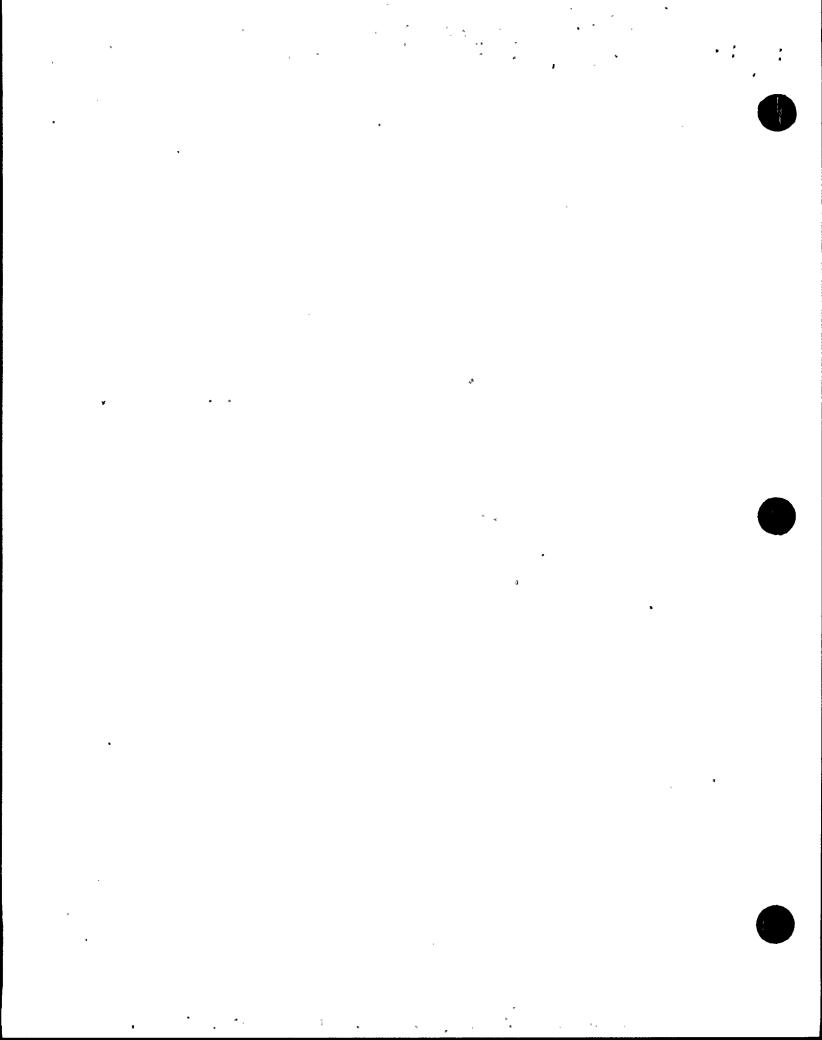
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HG\FIGURE7

FIGURE 6
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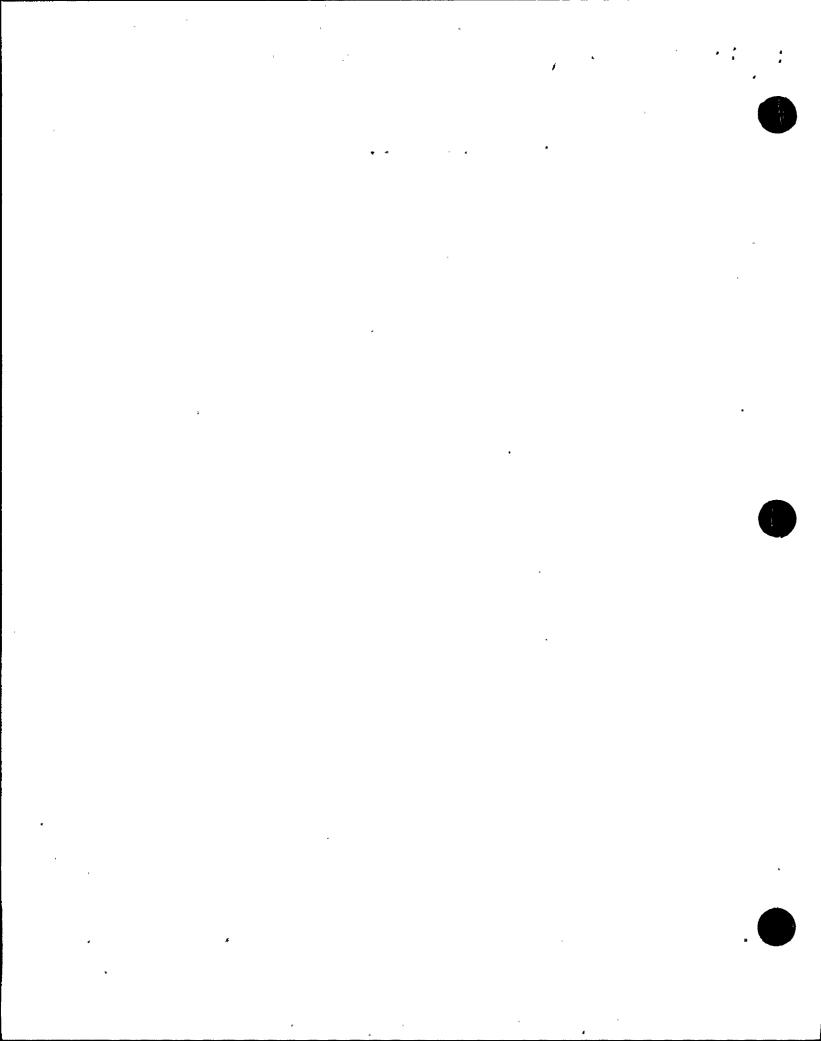
APPENDIX A1 TEST SEQUENCE



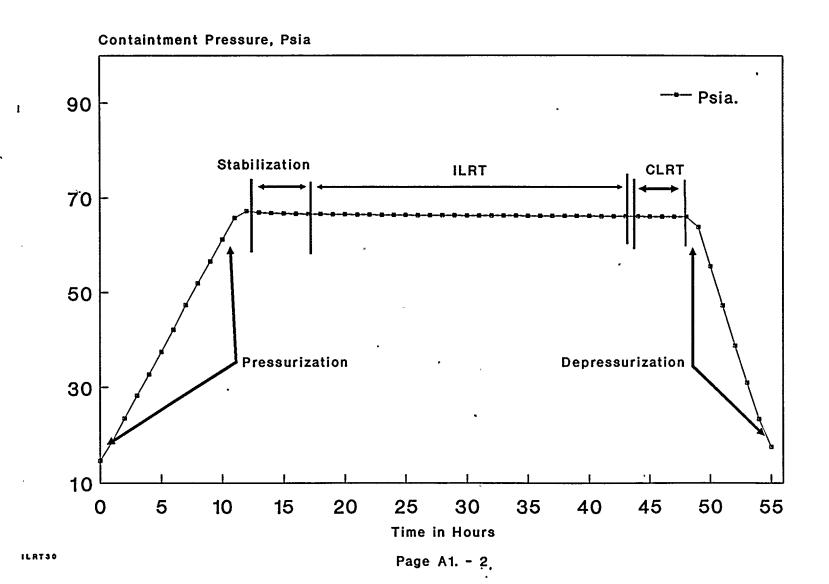
ILRT TEST SEQUENCE '

1991 Turkey Point Unit 4 ILRT

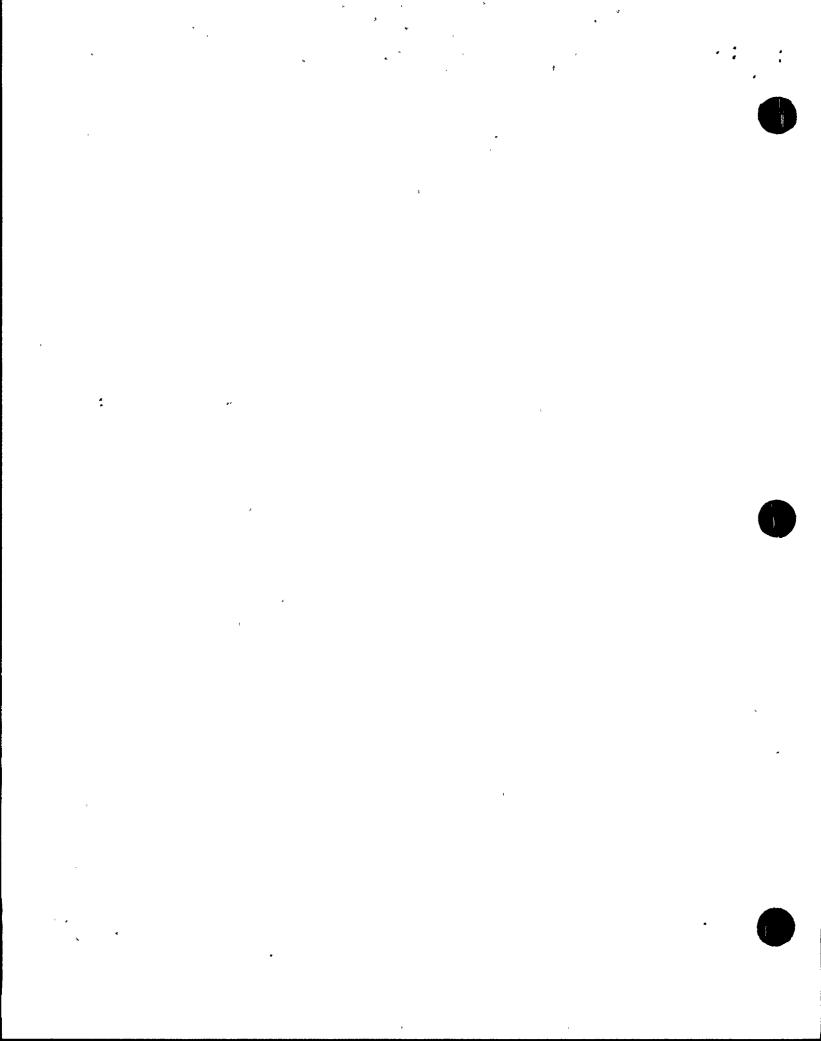
Sequence Started 17:33 10/17/91 Sequence Ended 00:35 10/20/91



ILRT TESTING SEQUENCE 1991 TURKEY POINT UNIT 4 ILRT



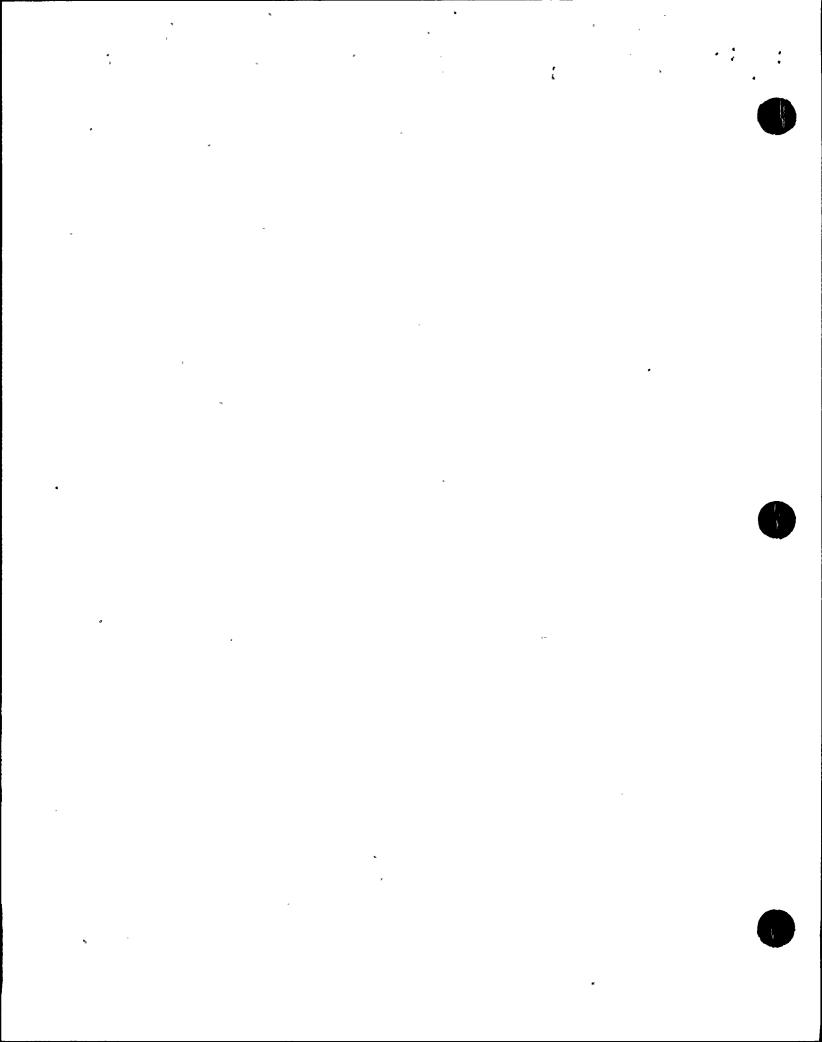
APPENDIX A2 .
TEMPERATURE STABILIZATION



TEMPERATURE STABILIZATION MODE

1991 Turkey Point Unit 4 ILRT

Sequence Started 05:04 10/18/91 Sequence Ended 10:04 10/18/91



1991 Turkey Point Unit 4 ILRT STABILIZATION PERIOD STARTED AT 05:04 ON 10/18/91

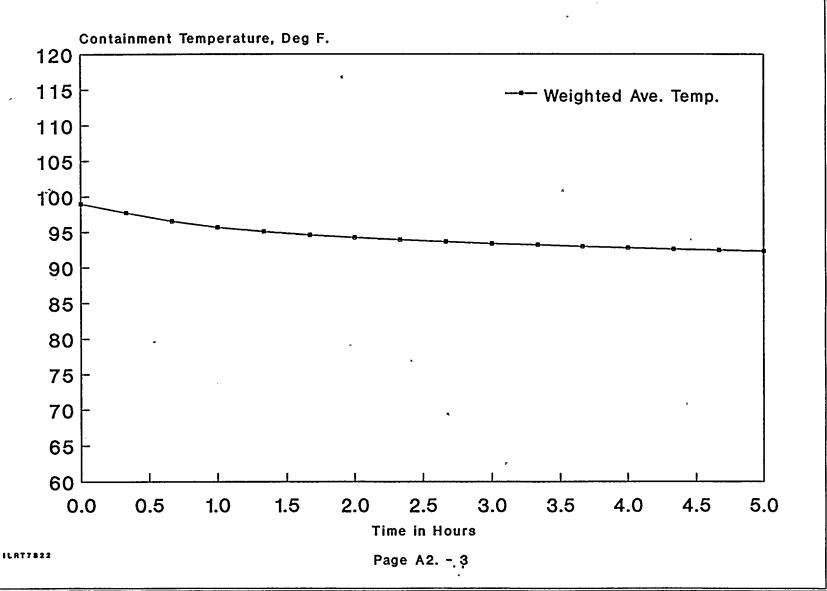
TEMPERATURE STABILIZATION

SAMPLE NUMBER	TIME HOURS	AVE TEMP DEG F	DELTA T/HR , LAST 1 HR	DELTA T/HR LAST 4 HR	
1 2 · 3	0.00 0.33 0.67	98.998 97.716 96.512	0.000 0.000 0.000	0.000 0.000 0.000	0.000 0.000 0.000
4 5 6 7	1.00 1.33 1.67	95.682 95.066 94.595		0.000 0.000 0.000	0.000 0.000 0.000
7 8 9 10	2.00 2.33 2.67	94.213 93.888	-1.469 -1.178	0.000 0.000 0.000	0.000 0.000 0.000
11	3.00 3.33	93.364 93.150	-0.849 -0.738	0.000 0.000	0.000 0.000 0.000
12 13 14	3.67 4.00 4.33	92.956 92.767 92.594	-0.598 -0.556	0.000 -1.558 -1.281	0.960 0.724 ;
15 16	4.67 5.00	92.454 92.311	-0.502 -0.456	-1.014 -0.843	0.512 0.387 *

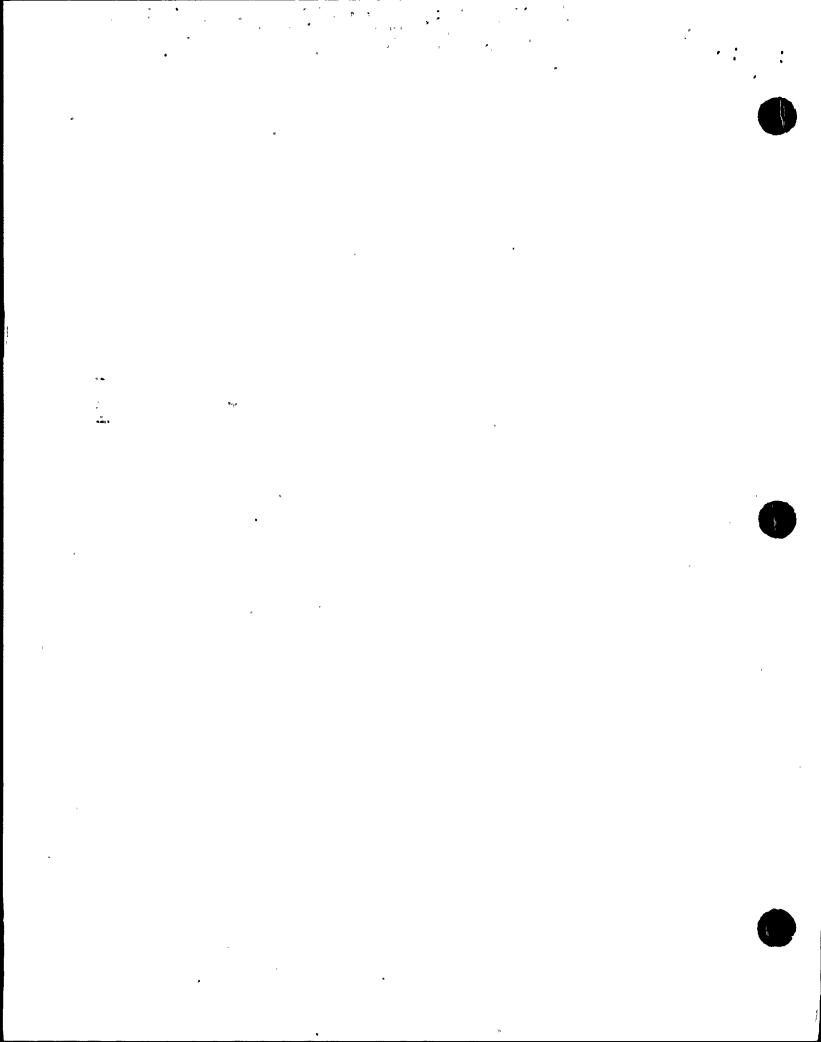
NOTES

- THE 1 HOUR AND 4 HOUR DELTA TEMPERATURE VALUES
 ARE NOT VALID UNTIL 1 HOUR AND 4 HOURS, RESPECTIVELY,
 HAVE PASSED IN THE TEST
- 2) THE STABILIZATION CRITERIA IS MET WHEN:
 - -THE HOURLY AVERAGE DELTA T FOR THE PRECEDING HOUR DIFFERS FROM THE HOURLY AVERAGE DELTA T FOR THE PRECEDING 4 HOURS BY LESS THAN 0.5 DEGREES F.
 - -THE STABILIZATION PERIOD IS A MINIMUM OF 4 HOURS
- 3) THE "*" INDICATES THAT THE STABILIZATION CRITERIA HAS BEEN MET.

TEMPERATURE STABILIZATION 1991 TURKEY POINT UNIT 4 ILRT



APPENDIX A3 . INTEGRATED LEAKAGE RATE TEST



ILRT TEST MODE

1991 Turkey Point Unit 4 ILRT

Sequence Started 10:04 10/18/91 Sequence Ended 10:20 10/19/91 And the second s

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1991 Turkey Point Unit 4 ILRT .

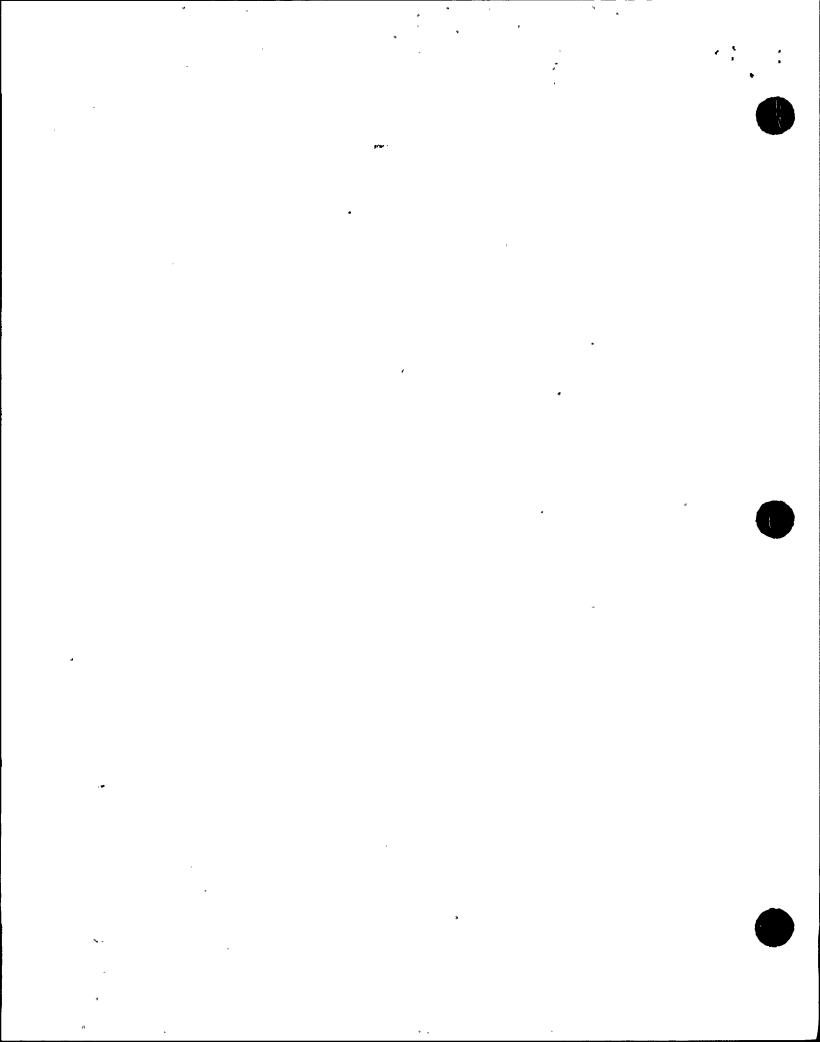
CONTAINMENT INTEGRATED LEAKAGE RATE TEST

LEAKAGE RATE IS MEASURED USING THE ABSOLUTE METHOD AND IS COMPUTED USING THE MASS POINT METHOD IN STRICT ACCORDANCE WITH AMERICAN NATIONAL STANDARD ANSI/ANS 56.8-1987

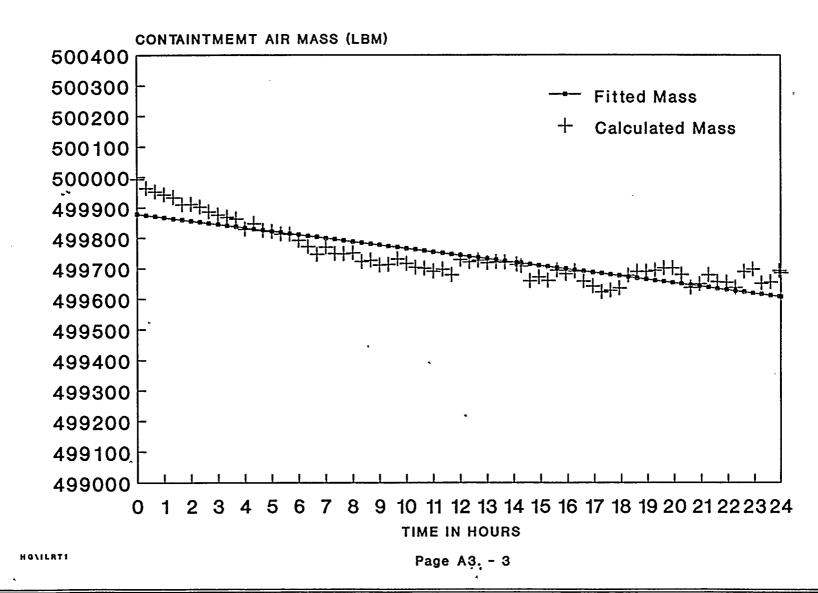
TEST PERIOD STARTED AT 10:04 HOURS ON 10/18/91 TEST CONDUCTED FOR 24.18 HOURS

FREESPACE VOLUME OF CONTAINMENT IS 1550000 CU FT CONTAINMENT WAS PRESSURIZED TO 66.63 PSIA

FITTED MASS POINT ILRT LEAKAGE RATE	Lam	=	= 0.048 %	/DAY
UPPER LIMIT OF 95% CONFIDENCE LEVEL	UCL	:	= 0.054 %	/DAY
CONTAINMENT DESIGN LEAKAGE RATE	La	=	= 0.250 %	/DAY
ILRT ACCEPTANCE CRITERIA	75% La	=	= 0.1875%	/DAY

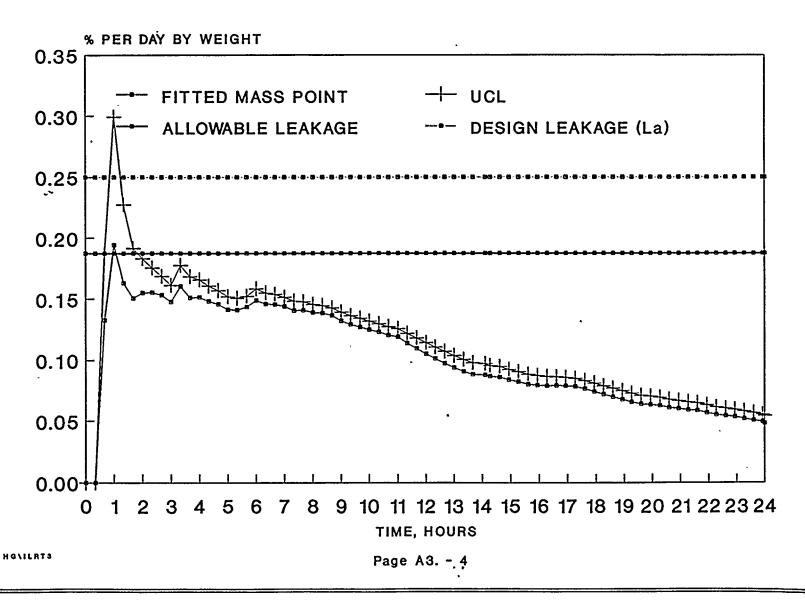


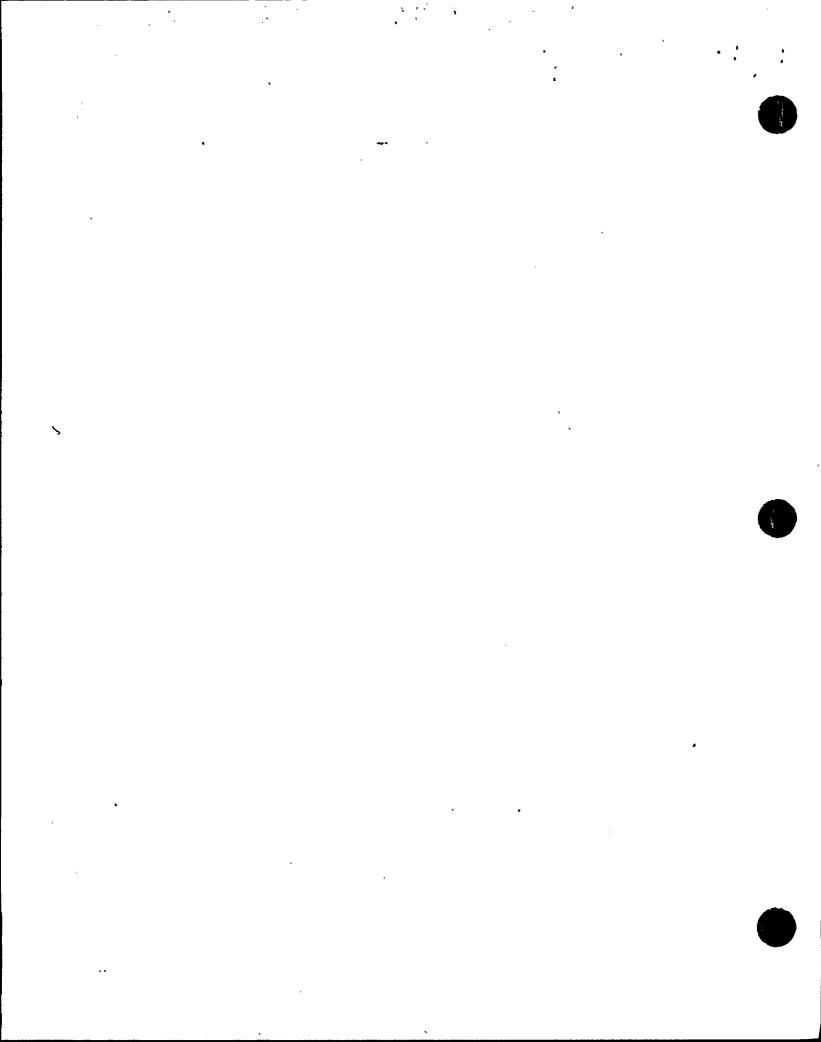
ILRT AIR MASS 1991 TURKEY POINT UNIT 4 ILRT



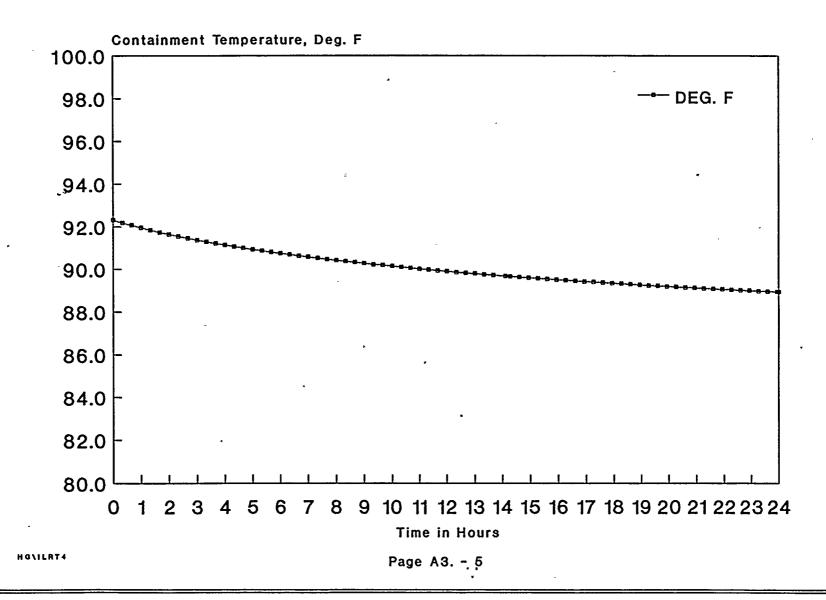
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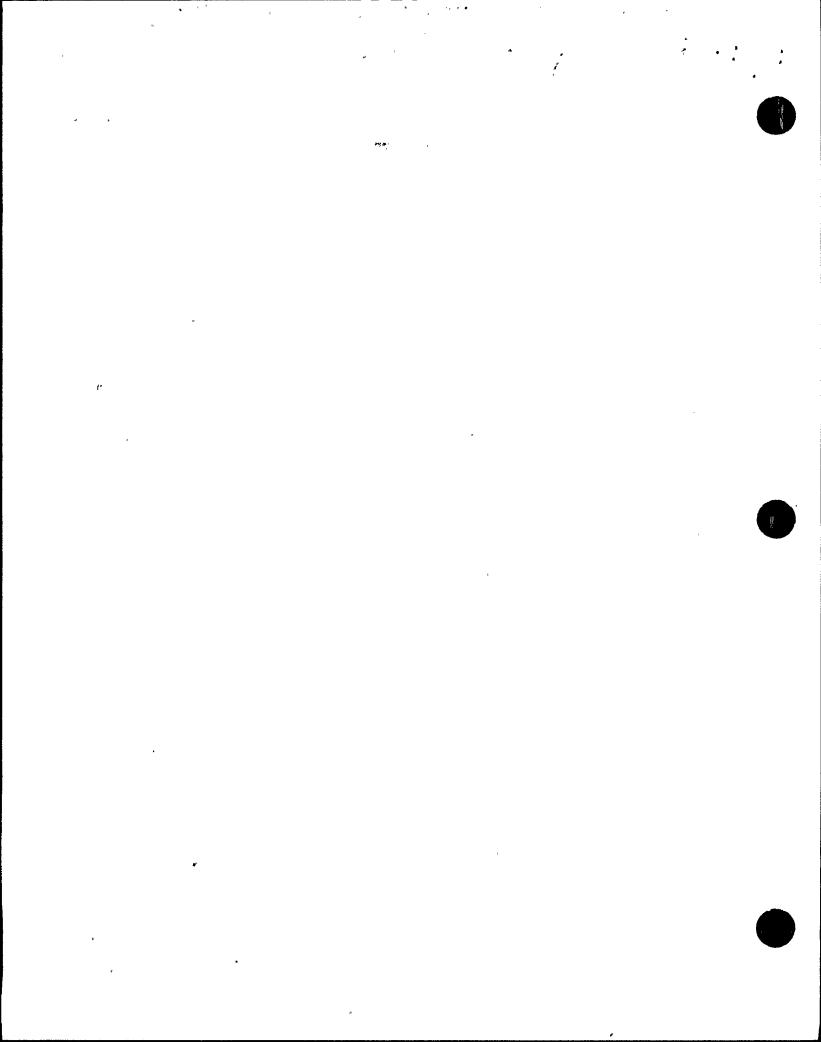
ILRT LEAKAGE RATES RELATIVE TO LIMITS 1991 TURKEY POINT UNIT 4 ILRT



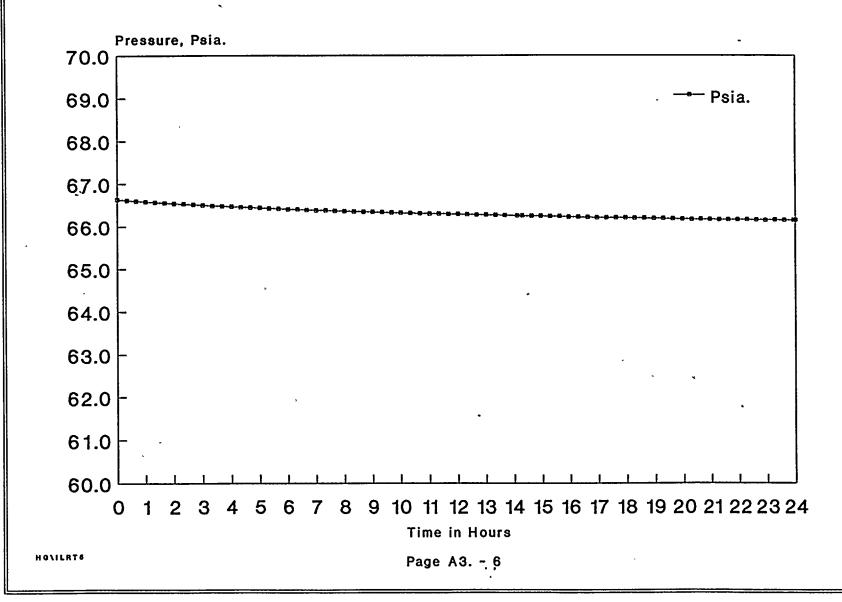


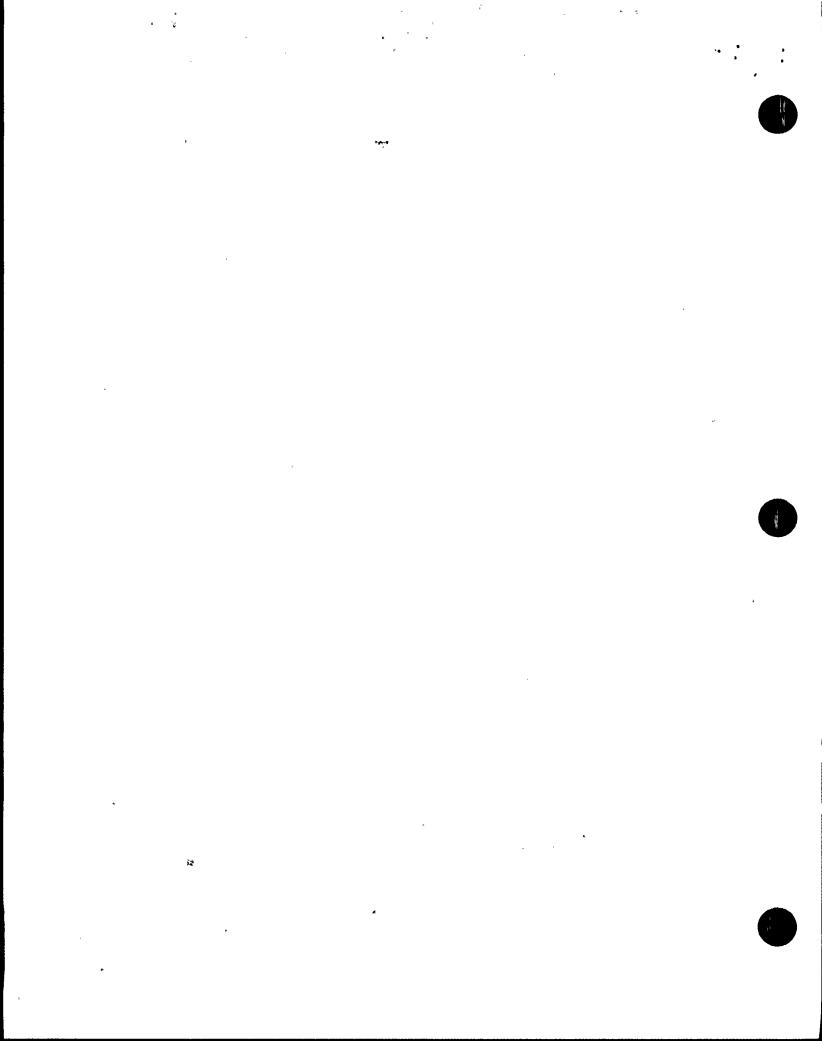
ILRT WEIGHTED AVERAGE TEMPERATURE 1991 TURKEY POINT UNIT 4 ILRT



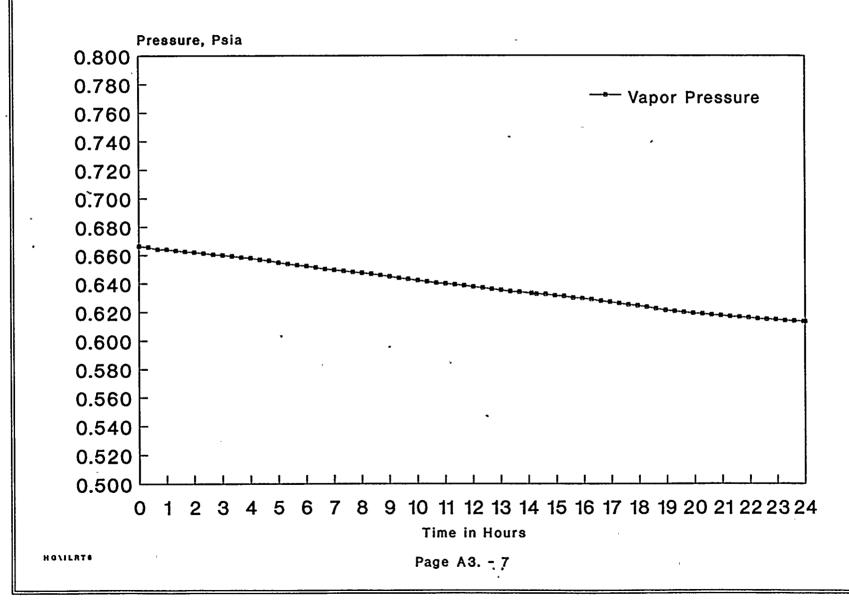


ILRT CONTAINMENT ABSOLUTE PRESSURE 1991 TURKEY POINT UNIT 4 ILRT





ILRT WEIGHTED AVERAGE VAPOR PRESSURE 1991 TURKEY POINT UNIT 4 ILRT



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DESCRIPTION OF VARIABLES

AVE TEMP - CONTAINMENT MEAN TEMPERATURE CALCULATED FROM VOLUMETRICALLY WEIGHTED RTD SENSOR INDICATIONS.

PRESSURE - PRIMARY CONTAINMENT PRESSURE INDICATION.

VAPOR PRES - CONTAINMENT VAPOR PRESSURE CALCULATED FROM VOLUMETRICALLY WEIGHTED HUMIDITY/DEWPOINT SENSOR INDICATIONS.

LEAK SIM - SIMPLE TOTAL TIME MEASURED LEAKAGE RATE.

LEAK FIT - LEAKAGE RATE CALCULATED FROM FIRST ORDER REGRESSION OF AIR MASS DATA.

95% UCL - UPPER LIMIT OF THE 95% CONFIDENCE LEVEL OF FITTED LEAKAGE RATE DATA.

AIR MASS - CONTAINMENT AIR MASS.

NOTES FOR TABULAR DATA -

- 1. TABLE VALUES OF ZERO SIGNIFY THE DATA IS NOT APPLICABLE TO THE CALCULATION.
- 2. "DELETED" SIGNIFIES THE SENSOR WAS DELETED.
- 3. "REJECTED" SIGNIFIES THE SAMPLE WAS REJECTED.

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ILRT VARIABLE TABLE SUMMARY

	SAM NO	TIME HOURS	AVE TEMP DEG F	PRESSURE PSIA	VAP PRES PSIA	LEAK SIM %/DAY	LEAK FIT %/DAY	UCL %/DAY	AIR MASS LBS
	1	0.00	92.311	66.632	0.6662	0.000	0.000	0.000	499952
	2	0.33	92.183	66.615	0.6656	0.122	0.000	0.000	499943
	3	0.67	92.064	66.598	0.6641	0.133	0.133	0.187	499933
	4	1.00	91.947	66.581	0.6641	0.200	0.194	0.299	499910
	4 5 6	1.33	91.836	66.567	0.6632	0.144	0.163	0.227	499911
		1.67	91.728	66.552	0.6624	0.143	0.150	0.192	499902
	7	2.00	91.633	66.538	0.6619	0.158	0.155	0.183	499886
	8	2.33	91.539	66.525	0.6613	0.155 0.151	0.155 0.153	0.175 0.169	499876 499868
	9	2.67	91.448	66.512 66.501	0.6604 0.6600	0.142	0.148	0.161	499863
	10 11	3.00 3.33	91.364 91.283	66.486	0.6592	0.177	0.160	0.178	499829
	12	3.67	91.202	66.478	0.6584	0.137	0.151	0.168	499847
	13	4.00	91.131	66.466	0.6578	0.152	0.151	0.166	499825
	14	4.33	91.060	66.456	0.6567	0.143	0.148	0.161	499822
	15	4.67	90.993	66.446	0.6560	0.143	0.146	0.157	499813
	16	5.00	90.920	66.436	0.6548	0.134	0.141	0.152	499812
	17	5.33	90.857	66.425	0.6539	0.144	0.141	0.150	499792
	18	5.67	90.794	66.414	0.6530	0.152	0.143	0.152	499772
	19	6.00	90.738	66.403	0.6522	0.165	0.149	0.158	499746
	20	6.33	90.678	66.398	0.6512	0.138	0.146	0.155	499770
	21	6.67	90.620	66.387	0.6501	0.147	0.146	0.154	499748
ſ	22	7.00	90.567	66.380	0.6494	0.140	0.144	0.151	
	3 24	7.33	90.511	66.373	0.6487	0.131	0.140	0.148	499751
		7.67	90.456	66.362	0.6481	0.144	0.141	0.148	499722
	25	8.00	90.406	66.356	0.6474	0.135	0.139	0.146 0.144	499726 499710
	26	8.33	90.355	66.347	0.6467	0.139° 0.133	0.138 0.136	0.144	499710
	27	8.67	90.309	66.341	0.6459 0.6449	0.133	0.130	0.142	499731
	28	9.00 9.33	90.263 90.214	66.337 66.328	0.6438	0.121	0.132	0.136	499716
	29 30	9.67	90.175	66.321	0.6431	0.124	0.127	0.134	499703
	31	10.00	90.175	66.314	0.6421	0.121	0.125	0.132	499700
	32	10.33	90.128	66.307	0.6414	0.121	0.123	0.130	499690
	33	10.67	90.044	66.302	0.6405	0.114	0.120	0.127	499697
	34	11.00	90.002	66.294	0.6399	0.119	0.119	0.125	499679
	35	11.33	89.963	66.295	0.6392	0.095	0.114	0.122	499728
	36	11.67	89.926	66.289	0.6385	0.095	0.109	0.118	499721
	37	12.00	89.885	66.284	0.6377	0.090	0.105	0.114	499726
	38		89.851	66.278	0.6369	0.091	0.101	0.111	499718
	39	12.67	89.812	66.273	0.6360	0.087	0.097	0.107	499721
	40	13.00	89.778	66.268	0.6353	0.086	0.094	0.104	499720
	41	13.33	89.742	66.262	0.6345	0.086	0.091	0.101	499712
	42	13.67	89.711	66.257	0.6340	0.086	0.088	0.098	499707
	43	14.10	89.664	66.244	0.6331	0.100	0.088	0.097	499658
	44	14.27	89.652	66.244	0.6327	0.094	0.087	0.096	499671
	45	14.60	89.618	66.238	0.6324	0.096	0.086	0.094	499659
	46	14.93	89.588		,0.6315	0.083	0.084	0.092	499693
	47	15.27	89.562	66.233	0.6311	0.085	0.082	0.090	499682
	48	15.60	89.529	66.229	0.6300	0.080	0.080	0.088	499690 499657
	49	15.93	89.495	66.220	0.6294	0.089	0.079	0.087	47700/
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ILRT VARIABLE TABLE SUMMARY

SAM NO	TIME HOURS	AVE TEMP DEG F	PRESSURE PSIA	VAP PRES PSIA	LEAK SIM %/DAY	LEAK FIT %/DAY	UCL %/DAY	AIR MASS LBS
50 51	16.27 16.60	89.468 89.438	66.214 66.207	0.6287 0.6277	0.092 0.095	0.079 0.079	0.086 0.086	499641 499622
52	16.93	89.412	66.204	0.6270	0.092	0.079	0.086	499628
53	17.27	89.388	66.201	0.6261	0.088	0.078	0.085	499635
54	17.60	89.359	66.202	0.6252	0.075	0.076	0.083	499676
55	17.93	89.335	66.200	0.6244	0.070	0.074	0.081	499689
56	18.27	89.308	66.196	0.6236	0.069	0.072	0.079	499689
57	18.60	89.279	66.192	0.6225	0.067	0.070	0.077	499693
58	18.93	89.254	66.189	0.6214	0.064	0.067	0.075	499701
59	19.27	89.226	66.185	0.6207	0.062	0.065	0.072	499701
60	19.60	89.204	66.179	0.6200	0.066	0.064	0.071	499680
61	19.93	89.183	66.170	0.6193	0.076	0.063	0.070	499637
62	20.27	89.158	66.168	0.6187	0.072	0.062	0.069	499649
63	20.60	89.137	66.169	0.6182	0.063	0.061	0.068	499679
64	20.93	89.116	66.163	0.6177	0.068	0.060	0.066	499656
65	21.27	89.092	66.159	0.6170	0.067	0.059	0.065	499654
66	21.60	89.072	66.154	0.6165	0.070	0.058	0.065	499637
67	21.93	89.053	66.158	0.6160	0.057	0.057	0.063	499689
68	22.27	89.031	66.156	0.6155	0.055	0.055	0.061	499698
69	22.60	89.011	66.147	0.6149	0.064	0.054	0.060	499651
70	22.93	88.993	66.145	0.6146	0.062	0.053	0.059	499655
71	23.27	88.973	66.147	0.6141	0.054	0.052	0.058	499692
2	23.60	88.956	66.144	0.6139	0.054	0.051	0.057	499686
73	23.93	88.936	66.141	0.6134	0.053	0.049	0.055	499685
74	24.00	88.933	66.140	0.6133	0.054	0.048	0.054	499681
75	24.27	88.920	66.128	0.6131	0.069	0.048	0.054	499604

SENSOR VOLUME FRACTIONS

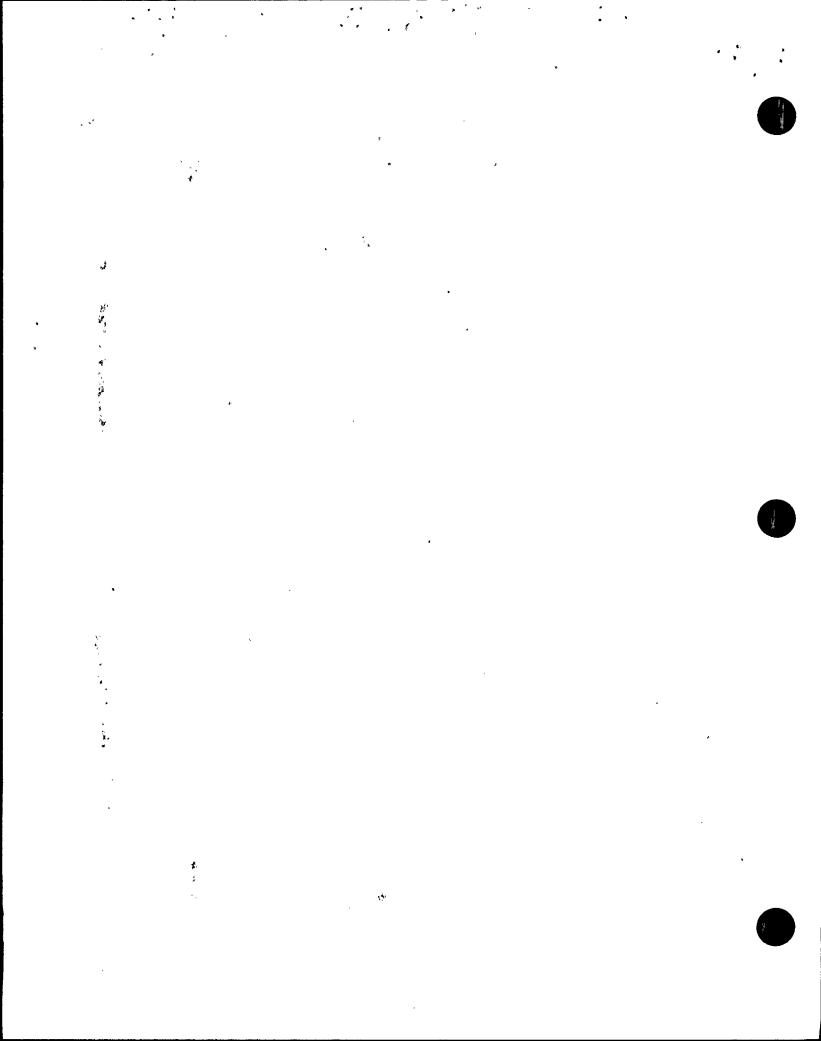
TEMPERATURE SENSORS

1 to 5	0.060333	0.060333	0.040000	0.040000	0.040000
6 to 10	0.060333	0.060333	0.060333	0.033000	0.053333
11 to 15	0.053333	0.033000	0.053333	0.033000	0.033000
16 to 20	0.053333	0.053333	0.053333	0.033000	0.033000
21 to 21	0.060333				

HUMIDITY/DP SENSORS

1 to 5	0.049500	0.049500	0.049500	0.049500	0.060000
6 to 10	0.060000	0.181000	0.181000	0.320000	0.000000

NOTE: VALUE OF ZERO INDICATES A DELETED SENSOR.



SAMPLE NUMBER	DELTA HOURS	TEMP 1 DEG F	TEMP 2 DEG F	TEMP 3 DEG F	TEMP 4 DEG F	TEMP 5 DEG F	TEMP 6 DEG F
NUMBER 1234567891011213145167189201122324256272893013233453673894041	HOURS 0.03 0.33 0.03 1.03 1.03 1.03 1.03 1.0	DEG F 93.1644331192.6501 92.6501 92.6501 92.352 92.140 92.8996 92.140 91.707 91.635 91.3805 91.3805 91.381 90.911.033 90.911.033 90.911.033 90.911.033 90.911.033 90.911.033 90.911.033 90.911.033 90.911.033 90.911.033 90.911.033 90.911.033 90.911.033 90.911.033 90.911.033 90.911.033	DEG F 92.7846 92.7846 92.3999 92.3992.1428 91.7562 92.1428 91.7562 91.8450 91.8450 91.8450 91.976 91	DEG F 91.360 91.25664 91.0928	DEG F 91.518 91.464 91.409 91.335 91.251 91.110 91.063 90.954 90.954 90.964 90.818 90.607 90.564 90.637 90.564 90.564 90.455 90.455 90.455 90.217 90.337 90.2260 90.217 90.134 90.109		
42 43 44 45 46 47 48 49	13.67 14.10 14.27 14.60 14.93 15.27 15.60 15.93	89.992 89.938 89.926 89.895 89.852 89.797 89.752	90.006 89.963 89.951 89.908 89.886 89.856 89.820 89.800	89.696 89.673 89.662 89.630 89.599 89.569 89.533	89.785 89.751 89.751 89.708 89.696 89.667 89.653	89.738 89.726 89.704 89.672 89.654 89.629	90.076 90.024 90.013 89.970 89.947 89.81 89.881

ILRT VARIABLE TABLE SUMMARY

SAMPLE	DELTA	TEMP 1	TEMP 2	TEMP 3	TEMP 4	TEMP 5	TEMP 6
NUMBER	HOURS	DEG F					
50	16.27	89.731	89.768	89.490	89.590	89.574	89.806
51	16.60	89.700	89.734	89.456	89.567	89.542	89.763
52	16.93	89.677	89.714	89.447	89.556	89.520	89.741
53	17.27	89.645	89.680	89.424	89.535	89.497	89.709
54	17.60	89.611	89.648	89.402	89.513	89.476	89.686
55	17.93	89.579	89.626	89.370	89.490	89.454	89.666
56	18.27	89.548	89.605	89.350	89.458	89.433	89.632
57	18.60	89.514	89.571	89.339	89.447	89.411	89.612
58	18.93	89.493	89.551	89.316	89.427	89.390	89.569
59	19.27	89.471	89.528	89.296	89.404	89.367	89.546
60	19.60	89.439	89.497	89.273	89.383	89.356	89.526
61	19.93	89.450	89.474	89.250	89.361	89.336	89.492
62	20.27	89.416	89.454	89.230	89.340	89.313	89.471
63	20.60	89.384	89.431	89.219	89.329	89.302	89.449
64	20.93	89.373	89.400	89.198	89.295	89.281	89.426
65	21.27		89.377	89.176	89.286	89.258	89.417
66	21.60	89.319	89.368	89.164	89.252	89.238	89.383
67	21.93	89.298		89.144	89.241	89.227	89.363
68	22.27	89.276	89.323	89.133	89.232	89.204	89.340
69	22.60	89.264	89.302	89.110	89.220	89.183	89.329
70	22.93	89.244	89.291	89.099	89,198	89.172	89.286
71	23.27	89.221	89.268	89.078	89.177	89.149	89.286
72	23.60	89.198	89.248	89.067	89.155	89.140	89.265
73	23.93	89.167	89.237	89.047	89.143	89.118	89.254
74	24.00	89.167	89.225	89.047	89.143	89.118	89.243
75	24.27	89.146	89.216	89.035	89.134	89.106	89.231

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SAMPLE NUMBER	DELTA HOURS	TEMP 7 DEG F	TEMP 8 DEG F	TEMP 9 DEG F	TEMP 10 DEG F	TEMP 11 DEG F	TEMP 12 DEG F
NUMBER 1 2 3 4 5 6 7 8 9 10 112 13 14 15 16 17 18 19 20 21 22 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41	HOURS 0.03 0.67 1.33 1.600 2.33 7.600 3.67 2.03 3.67 6.03 7.67 7.37 8.37 8.37 10.33 11.67 11.00 11.33 12.03 13.37			DEG F 87.434 87.435 87.445 87.445 87.436 87.436 87.434 87.434 87.434 87.436 87.437 87.427 87.427 87.427 87.421 87.411 87.416			
42 43 44 45 46 47 48 49	13.67 14.10 14.27 14.60 14.93 15.27 15.60 15.93	89.853 89.798 89.778 89.744 89.712 89.694 89.658	90.089 90.035 90.035 90.001 89.980 89.940 89.892 89.849	87.368 87.357 87.357 87.348 87.348 87.350 87.348	90.555 90.489 90.469 90.426 90.372 90.342 90.295 90.240	90.692 90.626 90.595 90.540 90.497 90.467 90.411 90.365	88.020 88.009 88.009 88.000 88.002 87.989 87.977

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ILRT VARIABLE TABLE SUMMARY

SAMPLE	DELTA	TEMP 7	TEMP 8	TEMP 9	TEMP 10	TEMP 11	TEMP 12
NUMBER	HOURS	DEG F	DEG F	DEG F	DEG F	DEG F	DEG F
50	16.27	89.592	89.828	87.337	90.209	90.322	87.977
51	16.60	89.560	89.806	87.337	90.154	90.279	87.966
52	16.93	89.539	89.794	87.325	90.123	90.225	87.957
53	17.27	89.517	89.785	87.325	90.080	90.182	87.957
54	17.60	89.485	89.762	87.314	90.046	90.139	87.957
55	17.93	89.451	89.751	87.314	90.003	90.107	87.946
56	18.27	89.430	89.708	87.314	89.971	90.052	87.946
57	18.60	89.396	89.676	87.305	89.928	90.009	87.946
58	18.93	89.376	89.633	87.305	89.894	89.975	87.934
59	19.27	89.353	89.588	87.305	89.862	89.921	87.923
60	19.60	89.333	89.579	87.294	89.831	89.889	87.923
61	19.93	89.310	89.544	87.294	89.797	89.857	87.923
62	20.27	89.290	89.524	87.294	89.765	89.814	87.912
63	20.60	89.267	89.501	87.294	89.742	89.780	87.903
64	20.93	89.244	89.490	87.282	89.699	89.737	87.903
65	21.27	89.212	89.470	87.282	89.667	89.705	87.903
66	21.60	89.201	89.458	87.271	89.645	89.662	87.891
67	21.93	89.180	89.438	87.271	89.613	89.628	87.891
68	22.27	89.158	89.415	87.271	89.579	· 89.597	87.880
69	22.60	89.137	89.404	87.271	89.547	89.553	87.880
_ 70	22.93	89.126	89.383	87.260	89.527	89.519	87.880
71	23.27	89.103	89.349	87.260	89.493	89.488	87.869
72	23.60	89.092	89.338	87.260	89.473	89.456	87.869
73	23.93	89.060	89.338	87.260	89.439	89.422	87.869
74	24.00	89.060	89.329	87.251	89.430	89.422	87.869
75	24.27	89.049	89.317	87.251	89.430	89.402	87.859

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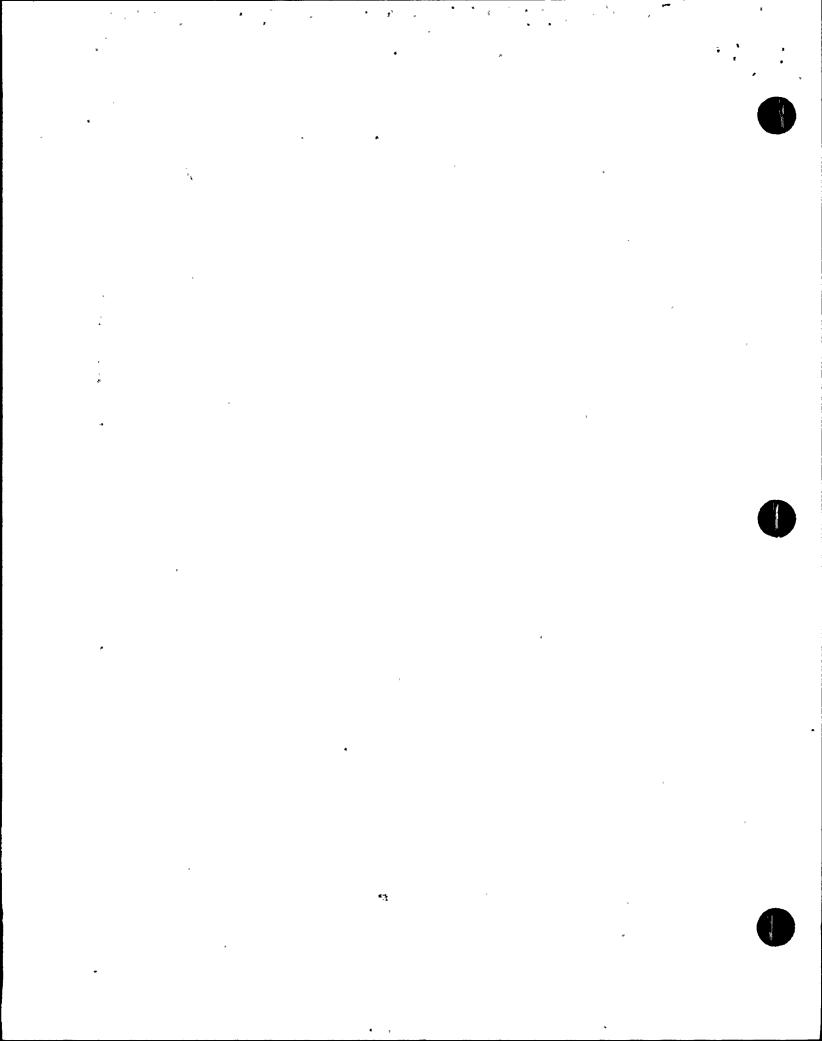
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SAMPLE NUMBER	DELTA HOURS	TEMP 13 DEG F	TEMP 14 DEG F	TEMP 15 DEG F	TEMP 16 DEG F	TEMP 17 DEG F	TEMP 18 DEG F
NUMBER 1234567890112134567890112222324567890112334567890412233456789041223	HOURS 0.03 0.33 0.67 1.33 1.60 2.33 1.60 2.33 1.60 3.67 2.03 3.67 3.67 3.67 3.67 3.67 3.67 3.67 3.6	DEG F 94.532 84.144 97.845 94.147 993.93.93.93.93.93.93.93.93.93.93.93.93.	DEG F 87.888 87.866 87.866 87.8559 87.8559 87.8559 87.8559 87.8559 87.8559 87.8559 87.8587 87.834 87.834 87.834 87.834 87.834 87.834 87.834 87.834 87.834 87.834 87.834 87.834 87.834 87.836 87.837 87.837 87.837 87.837 87.837	DEG F 88.237 88.237 88.227 88.2219 88.2219 88.2219 88.2219 88.317 88.303 88.317 88.303 88.317 88.303 88.227 88.217 88.129 88.227 88.1294 88.1294 88.1294 88.1294 88.1294 88.1297 88.1294 88.1297 88.1294 88.1298 88.1297 88.1298 88.1297 88.1298 88.1297 88.1298 88.1298 88.1298 88.1298 88.1298	DEG F 94.764 94.569 94.569 94.769 94.769 94.769 94.7869 94.786 94.00 93.718 93.442 93.442 93.174 93.93.93.93.93.93.93.93.93.93.93.93.93.9	DEG F 94.893	
44 45 46 47 48 49	14.27 14.60 14.93 15.27 15.60 15.93	90.428 90.394 90.331 90.322 90.254 90.199	87.780 87.780 87.769 87.771 87.769 87.757	87.946 87.934 87.934 87.928 87.923 87.914	90.605 90.539 90.507 90.446 90.399 90.367	90.893 90.839 90.794 90.744 90.687 90.633	90.530 90.476 90.447 90.401 90.347

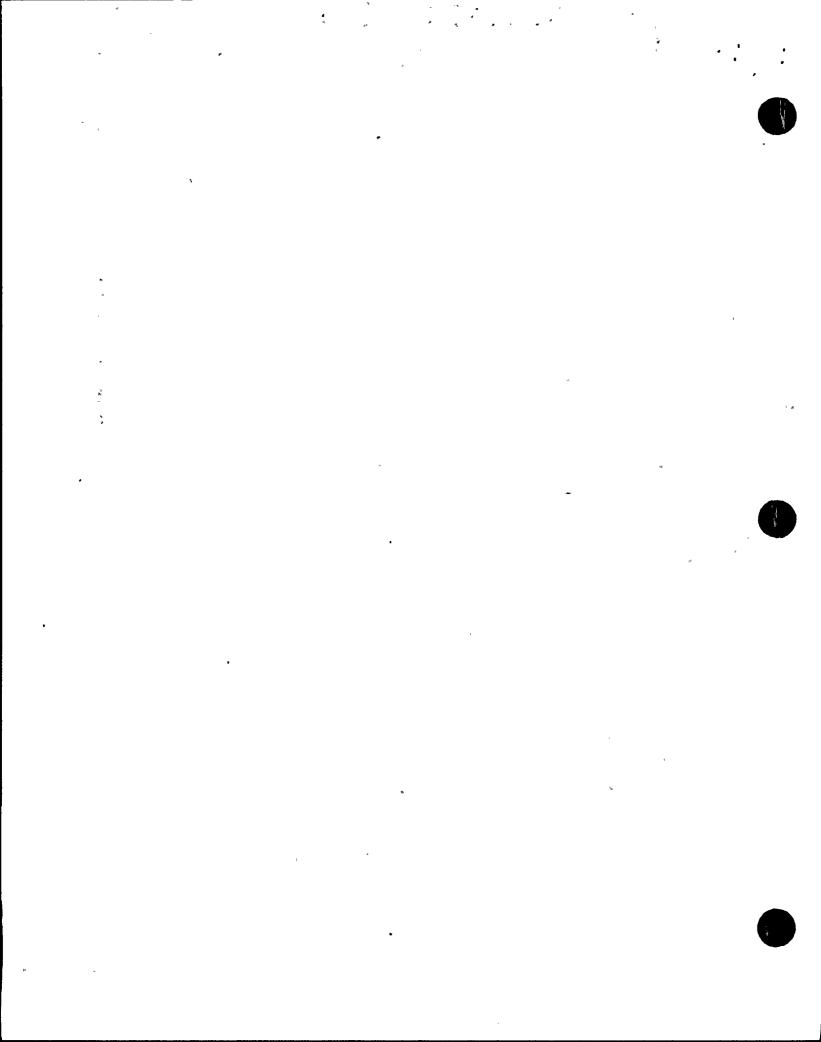
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ILRT VARIABLE TABLE SUMMARY

NUMBER HOURS DEG F 50 16.27 90.156 87.757 87.891 90.270 90.556 90.270 52 16.93 90.038 87.746 87.891 90.227 90.553 90.227 53 17.27 90.016 87.746 87.891 90.182 90.470 90.196 54 17.60 89.984 87.737 87.860 90.139 90.427 90.141 55 17.93 89.950 87.737 87.860 90.139 90.427 90.141 55 17.93 89.950 87.737 87.861 90.096 90.384 90.098 56 18.27 89.896 87.737 87.861 90.064 90.350 90.076 57 18.60 89.853 87.726 87.848 90.010 90.296 90.021 58 18.93 89.821 87.726 87.848 89.967 90.264 89.990 19.27 89.744 87.714 87.848 89.967 90.264 89.990 19.27 89.744 87.714 87.837 89.890 90.190 89.913 61 19.93 89.712 87.714 87.837 89.847 90.144 89.892 62 20.27 89.669 87.703 87.826 89.815 90.113 89.838 63 20.60 89.626 87.703 87.826 89.815 90.113 89.838 63 20.60 89.626 87.703 87.826 89.783 90.081 89.795 64 20.93 89.626 87.703 87.826 89.783 90.081 89.795 64 20.93 89.626 87.703 87.826 89.783 90.081 89.795 64 20.93 89.626 87.692 87.805 89.695 90.004 89.741 67 21.93 89.408 87.662 87.805 89.684 89.972 89.741 67 21.93 89.408 87.662 87.794 89.598 89.907 89.686 69 22.26 89.408 87.683 87.794 89.598 89.907 89.686 69 22.27 89.440 87.682 87.805 89.684 89.972 89.741 87.683 87.794 89.598 89.907 89.686 69 22.20 89.408 87.683 87.794 89.598 89.907 89.686 69.22 87.805 89.684 89.972 89.741 87.683 87.794 89.598 89.907 89.686 70.22 89.300 87.683 87.794 89.598 89.809 89.621 23.29 89.377 87.683 87.794 89.598 89.809 89.621 23.29 89.377 87.683 87.794 89.598 89.907 89.686 70.22 89.300 87.671 87.794 89.500 89.809 89.621 23.29 89.334 87.683 87.794 89.550 89.809 89.621 23.29 89.334 87.661 87.794 89.590 89.809 89.621 23.29 89.334 87.661 87.794 89.500 89.809 89.621 23.29 89.334 87.661 87.783 89.426 89.735 89.566									
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51 16.60 90.102 87.757 87.891 90.270 90.556 90.270 52 16.93 90.038 87.746 87.891 90.227 90.513 90.227 53 17.27 90.016 87.746 87.880 90.182 90.470 90.196 54 17.60 89.984 87.737 87.860 90.139 90.427 90.141 55 17.93 89.950 87.737 87.871 90.096 90.384 90.098 56 18.27 89.896 87.737 87.860 90.064 90.350 90.076 57 18.60 89.853 87.736 87.848 90.010 90.296 90.021 58 18.93 89.821 87.726 87.848 89.967 90.264 89.990 59 19.27 89.744 87.714 87.837 89.890 90.190 89.913 60 19.60 89.744 87.714 87.837 89.847 90.144 89.893 61 19.93 89.712 87.703 87.826 89.815 <th></th> <th>NUMBER</th> <th>HOURS</th> <th>DEG F</th> <th>DEG F</th> <th>DEG F</th> <th>DEG F</th> <th>DEG F</th> <th>DEG F</th>		NUMBER	HOURS	DEG F					
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52 16.93 90.038 87.746 87.891 90.227 90.513 90.227 53 17.27 90.016 87.746 87.880 90.182 90.470 90.196 54 17.60 89.984 87.737 87.860 90.139 90.427 90.141 55 17.93 89.950 87.737 87.860 90.064 90.384 90.098 56 18.27 89.896 87.737 87.860 90.064 90.350 90.076 57 18.60 89.853 87.726 87.848 90.010 90.296 90.021 58 18.93 89.821 87.726 87.848 89.967 90.264 89.999 59 19.27 89.744 87.714 87.848 89.933 90.221 89.967 60 19.60 89.744 87.714 87.837 89.890 90.190 89.913 61 19.93 89.712 87.714 87.837 89.847 90.144 89.892 62 20.27 89.669 87.703 87.826 89.783 <th></th> <th></th> <th></th> <th>-</th> <th>87.757</th> <th></th> <th></th> <th></th> <th>90.270</th>				-	87.757				90.270
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72 23.60 89.334 87.671 87.794 89.469 89.778 89.589 73 23.93 89.300 87.671 87.783 89.435 89.744 89.566 74 24.00 89.300 87.660 87.783 89.426 89.735 89.566	_								89.621
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7.4 2.400 00.000 0.4000 0.4000 0.4000									
		75	24.27	89.288	87.660	87.772	89.403	89.701	89.546



SAMPLE NUMBER	DELTA HOURS	TEMP 19 DEG F	TEMP 20 DEG F	TEMP 21 DEG F
TUMBER 12345678901234567890123222222333333567890123444444444444444444444444444444444444	HOURS 0.03 1.03 1.03 1.67 1.33 1.67 2.36 3.67	DEG F 333335 F 37.265	DEG 5.531 87.529 87.529 87.529 87.5529 87.5528 87.5500 87.5508 87.5508 87.5508 87.485 87.485	DEG 92.7447 92.7447792.3061 92.758792.3061 92.584792.3061 92.91.6388391.63891.63891.63891.63891.63891.90.91.91.91.91.91.91.91.91.91.91.91.91.91.
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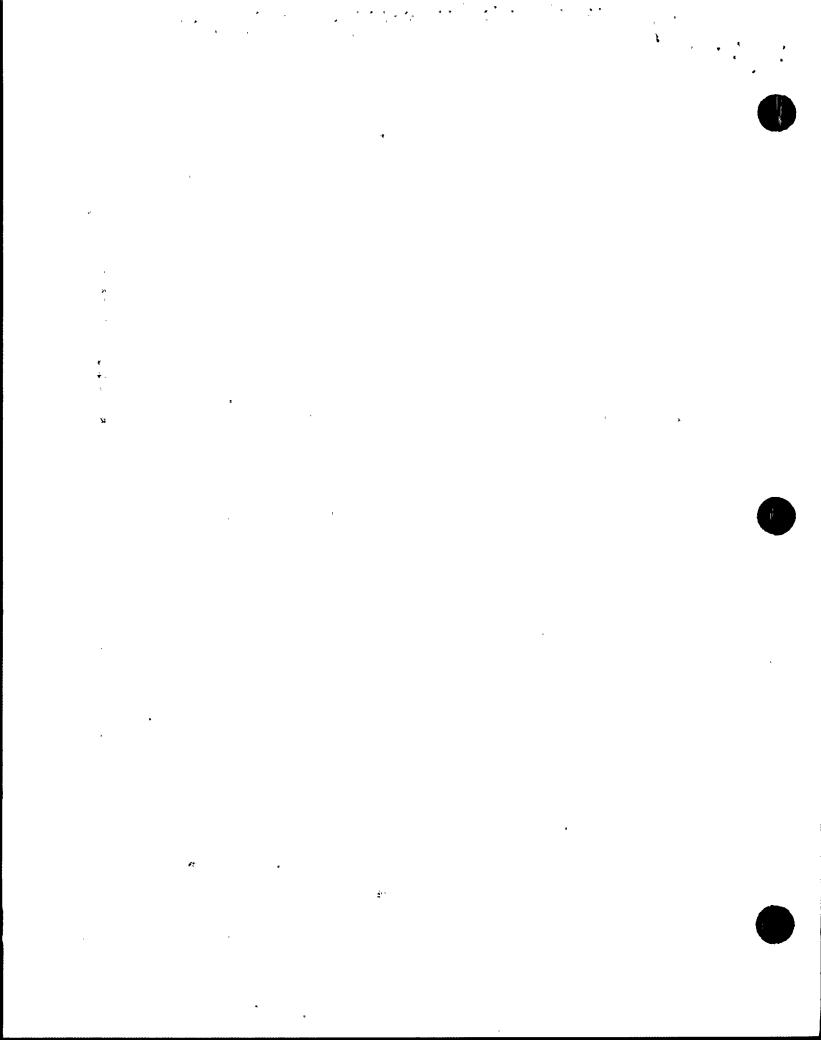
SAMPLE NUMBER	DELTA HOURS	TEMP 19 DEG F	TEMP 20 DEG F	TEMP 21 DEG F
50 51	16.27 16.60	87.175 87.175	87.402 87.409	89.593 89.577
52	16.93	87.175	87.402	89.539
53	17.27	87.166	87.398	89.514
54	17.60	87.154	87.398	89.480
55	17.93	87.154	87.386	89.459
56	18.27	87.154	87.382	89.421
57	18.60	87.143	87.377	89.405
58	18.93	87.143	87.377	89.373
59	19.27	87.143	87.359	89.344
60	19.60	87.132	87.359	89.323
61	19.93	87.132	87.359	89.301
62	20.27	87.132	87.355	89.276
63	20.60	87.132	87.348	89.258
64	20.93	87.123	87.337	89.235
65	21.27	87.123	87.337	89.215
66	21.60	87.111	87.328	89.192
67	21.93	87.111	87.328	89.181
68	22.27	87.100	87.328	89.160
69	22.60	87.100	87.335	89.145
70	22.93	87.100	87.316	89.129
71	23.27	87.089	87.305	89.106
72	23.60	87.089	87.305	89.095
73	23.93	87.077	87.305	89.074
74	24.00	87.089	87.305	89.074
75	24.27	87.089	87.305	89.052

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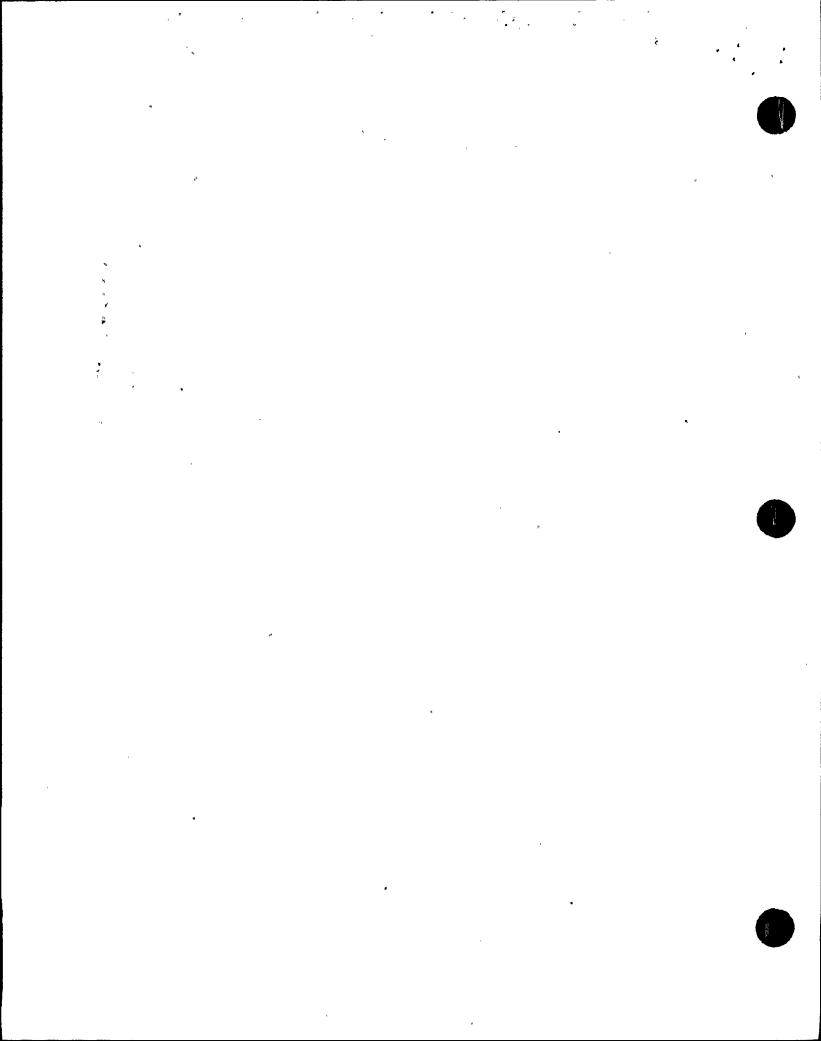
2 0.33 66.609 66.615 91.628 86.757 89.678 87 3 0.67 66.593 66.598 91.844 87.275 90.121 87 4 1.00 66.577 66.581 92.075 87.650 90.409 87 5 1.33 66.563 66.567 92.330 88.046 90.710 88 6 1.67 66.549 66.552 92.529 88.499 90.897 88 8 2.33 66.522 66.538 92.695 88.864 91.006 88 8 2.33 66.551 66.552 92.936 89.185 91.182 89 9 2.67 66.511 66.512 93.085 89.346 91.238 89 10 3.00 66.500 66.501 93.271 89.543 91.523 89 11 3.33 66.489 66.486 93.434 89.625 91.675 90 12 3.67 66.478 66.478 93.591 89.857 91.843 90 14 4.33 66.455 66.466 93.760 90.009 92.064 90 14 4.33 66.455 66.466 93.905 90.112 92.180 90 14 4.33 66.456 66.446 94.061 90.253 92.407 91 16 5.00 66.436 66.436 94.194 90.472 92.488 91 17 5.33 66.422 66.425 94.288 90.676 92.604 91 18 5.67 66.413 66.414 94.973 90.831 92.747 91 19 6.00 66.399 66.403 94.480 91.106 92.900 91 20 6.33 66.396 66.387 94.630 91.285 93.109 92 21 6.67 66.355 66.362 94.839 91.639 93.452 92 22 7.00 66.375 66.380 94.694 91.431 93.219 92 23 7.33 66.368 66.373 94.757 91.512 93.347 92 24 7.67 66.355 66.362 94.839 91.639 93.452 92 25 8.00 66.352 66.362 94.839 91.639 93.452 92 26 8.33 66.304 66.337 94.933 91.862 93.591 92 27 8.67 66.355 66.362 94.888 91.721 93.539 92 29 9.33 66.324 66.328 95.013 92.197 93.653 92 29 9.33 66.324 66.327 94.933 91.862 93.591 92 29 9.33 66.324 66.328 95.013 92.197 93.6673 92 29 9.33 66.324 66.327 95.134 92.955 93.389 92 30 9.67 66.315 66.321 95.072 92.220 93.777 92 31 10.00 66.288 66.294 95.153 92.338 93.783 92 33 10.67 66.297 66.302 65.307 95.103 92.339 93.895 92 34 11.00 66.288 66.294 95.153 92.587 94.067 92 35 11.33 66.291 66.295 95.165 92.581 94.171 92 36 11.67 66.285 66.284 95.154 92.666 94.275 93 39 12.67 66.269 66.273 95.134 92.666 94.275 93 39 12.67 66.266 66.269 66.273 95.134 92.666 94.275 93 30 12.67 66.264 66.268 95.134 92.666 94.275 93 31 10.00 66.244 66.244 95.062 92.755 94.215 92	SAMPLE NUMBER	DELTA HOURS	PRES 1 PSIA	PRES 2 PSIA	HUM 1 % RH	HUM 2 % RH	HUM 3 % RH	HUM 4 % RH
	NUMBER 1 2 3 4 5 6 7 8 9 10 11 2 13 14 5 16 7 18 9 20 1 22 2 24 2 5 6 2 7 2 8 9 30 1 3 2 3 3 4 5 3 6 7 3 8 9 40 41 42	HOURS 0.03 0.67 1.00 1.33 1.60 2.03 3.67 2.03 3.67 3.67 3.67 5.67 7.33 7.67 7.33 7.67 10.03 7.67 11.00 11.37 12.67 13.67 13.67 13.67	PSIA 66.6937739655549 66.59377398815839666.331027815866.3315 66.2666.443666.331524566.3315 66.2666.2666.3315 66.2666.3315 66.2666.3315 66.2666.3315 66.2666.3315 66.2666.3315 66.2666.3315 66.2666.3315 66.2666.3315 66.2666.3315	PSIA 235817 285 2818 66.618 66.55817 285 66.5532 21168 866.66.5532 21168 866.4413 870 3872 66.3314 728 887 887 887 887 887 887 887 887 887	RH 91.628445099565141051415891.88399565985141051488399999999999999999999999999999999999	RH 86.755506994566557902399592.6665551896.755069945665551	RH 89.678 90.1409 90.1409 90.1828 90.1407 91.1846 91.5275 91.8467 92.1847 92.1848 92.1849 92.1849 92.1847 93.1859	RH 86.128 87.5600 87.5600 87.5600 87.5600 87.5600 87.5600 87.6291 89.3848 90.3849 90.6872 91.405 91.5510 91.5550 91.629 91.7360 91
45 14.60 66.237 66.238 95.037 92.766 94.177 92 46 14.93 66.237 66.238 95.020 92.760 94.148 92 47 15.27 66.233 66.233 95.004 92.762 94.110 92 48 15.60 66.228 66.229 94.961 92.766 94.102 92	44 45 46 47 48	14.27 14.60 14.93 15.27 15.60	66.243 66.237 66.237 66.233 66.228	66.238 66.233 66.229	95.020 95.004 94.961	92.760 92.762 92.766	94.148 94.110 94.102	92.990 92.981 92.964 92.965 92.928 92.936

• 5 * 46 10 mg/m **₩** •

SAMPLE NUMBER	DELTA HOURS	PRES 1 PSIA	PRES 2 PSIA	HUM 1 % RH	HUM 2 % RH	HUM 3 % RH	HUM 4 % RH
NONDER	1100110			•		·	•
50	16.27	66.214	66.214	94.915	92.726	94.125	92.917
51	16.60	66.207	66.207	94.886	92.715	94.086	92.894
52	16.93	66.202	66.204	94.855	92.706	94.071	92.887
53	17.27	66.200	66.201	94.828	92.703	94.055	92.877
54	17.60	66.200	66.202	94.805	92.673	94.061	92.871
55	17.93	66.199	66.200	94.764	92.675	94.015	92.854
56	18.27	66.195	66.196	94.718	92.656	94.004	92.831
57	18.60	66.191	66.192	94.683	92.656	93.981	92.814
58	18.93	66.187	66.189	94.640	92.631	93.943	92.776
59	19.27	66.184	66.185	94.590	92.645	93.934	92.772
60	19.60	66.180	66.179	94.561	92.610	93.922	92.755
61	19.93	66.171	66.170	94.515	92.605	93.876	92.726
62	20.27	66.167	66.168	94.478	92.590	93.845	92.706
63	20.60	66.169	66.169	94.437	92.607	93.862	92.695
64	20.93	66.162	66.163	94.404	92.593	93.840	92.679
65	21.27	66.158	66.159	94.386	92.563	93.811	92.667
66	21.60	66.153	66.154	94.343	92.549	93.796	92.629
67	21.93	66.158	66.158	94.326	92.567	93.774	92. 6 14
68	22.27	66.156	66.156	94.290		93.744	92.589
69	22.60	66.146	66.147	94.279	92.520	93.716	92.572
70	22.93	66.144	66.145	94.240	92.544	93.711	92.561
71	23.27	66.146	66.147	94.246	92.567	93.671	92.544
72	23.60	66.143	66.144	94.224	92.563	93.661	92.528
73	23.93	66.140	66.141	94.193	92.584	93.641	92.515
74	24.00	66.139	66.140	94.199	92.550	93.654	92.527
75	24.27	66.124	66.128	94.193	92.532	93.647	92.504



SAMPLE NUMBER	DELTA HOURS	HUM 5 % RH	HUM 6 % RH	HUM 7 % RH	HUM 8 % RH	HUM 9 % RH	HUM 10 % RH
NUMBER 1 2 3 4 5 6 7 8 9 0 11 12 13 14 5 16 7 18 9 20 1 22 23 24 25 6 27 28 9 30 1 32 3 34 5 36 7 38 9 40 142	HOURS 0.033 0.67 1.33 1.600 2.337 2.600 3.670 3	* RH 71.5272 74.156.752.773.414.155.7756.755.7756.752.866.775.266.775.	* RH 72.76 73.586 74.476 75.985 77.054 78796 78796 78796 78796 78796 78796 78796 78796 78796 78796 79597 79597 80327 82582 82994 83690 83950 84614 84895 85764 85914 85914 86390 86390 86390 87230 887230 887230 887230 887230	* RH 88.698 89.050 89.401 89.758 89.758 89.927 90.326 90.746 90.748 90.798 90.955 91.036 91.086 91.100 91.106 91.106 91.106 91.106 91.060	RH 91.6359 91.6359 91.4963 91.4863 91.428 91.428 91.428 91.425 91.425 91.1003 91.01	RH 92.443 92.6623 92.975 92.975 93.177 93.217 93.217 93.313 93.224 93.313 93.224 93.325 93.224 93.325	
43 44 45 46 47 48 49	14.10 14.27 14.60 14.93 15.27 15.60 15.93	87.736 87.770 88.151 88.406 88.582 88.650 88.784	87.863 87.921 88.022 88.104 88.204 88.237 88.313	90.598 90.546 90.583 90.479 90.515 90.386 90.415	90.499 90.447 90.479 90.438 90.387 90.356	92.949 92.937 92.975 92.871 92.872 92.766 92.749	DELETED DELETED DELETED DELETED DELETED DELETED DELETED



SAMPLE	DELTA	HUM 5	HUM 6	HUM 7	HUM 8	HUM 9	HUM 10
NUMBER	HOURS	% RH					
50	16.27	88.870	88.370	90.327	90.304	92.755	DELETED
51	16.60	88.947	88.418	90.316	90.328	92.540	DELETED
52	16.93	88.961	88.456	90.332	90.337	92.468	DELETED
53	17.27	89.038	88.458	90.374	90.333	92.220	DELETED
54	17.60	89.080	88.505	90.374	90.287	92.087	DELETED
55	17.93	89.086	88.511	90.381	90.299	91.948	DELETED
56	18.27	89.097	88.505	90.421	90.288	91.826	DELETED
57	18.60	89.097	88.494	90.409	90.282	91.617	DELETED
58	18.93	89.066	88.479	90.372	90.267	91.417	DELETED
59	19.27	89.045	88.481	90.398	90.276	91.350	DELETED
60	19.60	89.050	88.469	90.374	90.264	91.274	DELETED
61	19.93	89.039	88.475	90.392	90.270	91.129	DELETED
62	20.27	89.054	88.479	90.385	90.286	91.075	DELETED
63	20.60	89.020	88.474	90.396	90.262	91.063	DELETED
64	20.93	89.044	88.469	90.409	90.293	91.024	DELETED
65	21.27	89.073	88.475	90.403	90.304	90.914	DELETED
66	21.60	89.076	88.478	90.400	90.284	90.894	DELETED
67	21.93	89.089	88.474	90.408	90.286	90.825	DELETED
68	22.27	89.076	88.478	90.399	90.289	90.812	DELETED
69	22.60	89.071	88.490	90.371	90.284	90.742	DELETED
70	22.93	89.077	88.497	90.389	90.297	90.739	DELETED
71	23.27	89.083	88.521	90.402	90.332	90.703	DELETED
72	23.60	89.084	88.522	90.472	90.350	90.699	DELETED
73	23.93	89.119	88.544	90.408	90.355	90.686	DELETED
74	24.00	89.124	88.549	90.425	90.349	90.669	DELETED
75	24.27	89.124	88.567	90.431	90.332	90.686	DELETED

APPENDIX A4 SUPPLEMENTAL LEAKAGE RATE TEST

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CLRT TEST MODE

1991 Turkey Point Unit 4 ILRT

Sequence Started 13:28 10/19/91 Sequence Ended 17:28 10/19/91 Ž. 4.4

1991 Turkey Point Unit 4 ILRT

CONTAINMENT INTEGRATED LEAKAGE RATE TEST SUPPLEMENTAL VERIFICATION TEST

LEAKAGE RATE IS MEASURED USING THE ABSOLUTE METHOD AND IS COMPUTED USING THE MASS POINT METHOD IN STRICT ACCORDANCE WITH AMERICAN NATIONAL STANDARD ANSI/ANS 56.8-1987

TEST PERIOD STARTED AT 13:28 HOURS ON 10/19/91 TEST CONDUCTED FOR 4.00 HOURS

FREESPACE VOLUME OF CONTAINMENT IS 1550000 CU FT CONTAINMENT WAS PRESSURIZED TO 66.08 PSIA

FITTED MASS POINT ILRT LEAKAGE RATE Lam = 0.048 % /DAY CONTAINMENT DESIGN LEAKAGE RATE La = 0.250 % /DAY SUPERIMPOSED CLRT LEAKAGE RATE Lo = 0.289 % /DAY FITTED CLRT TOTAL TIME LEAKAGE RATE Lc = 0.336 % /DAY

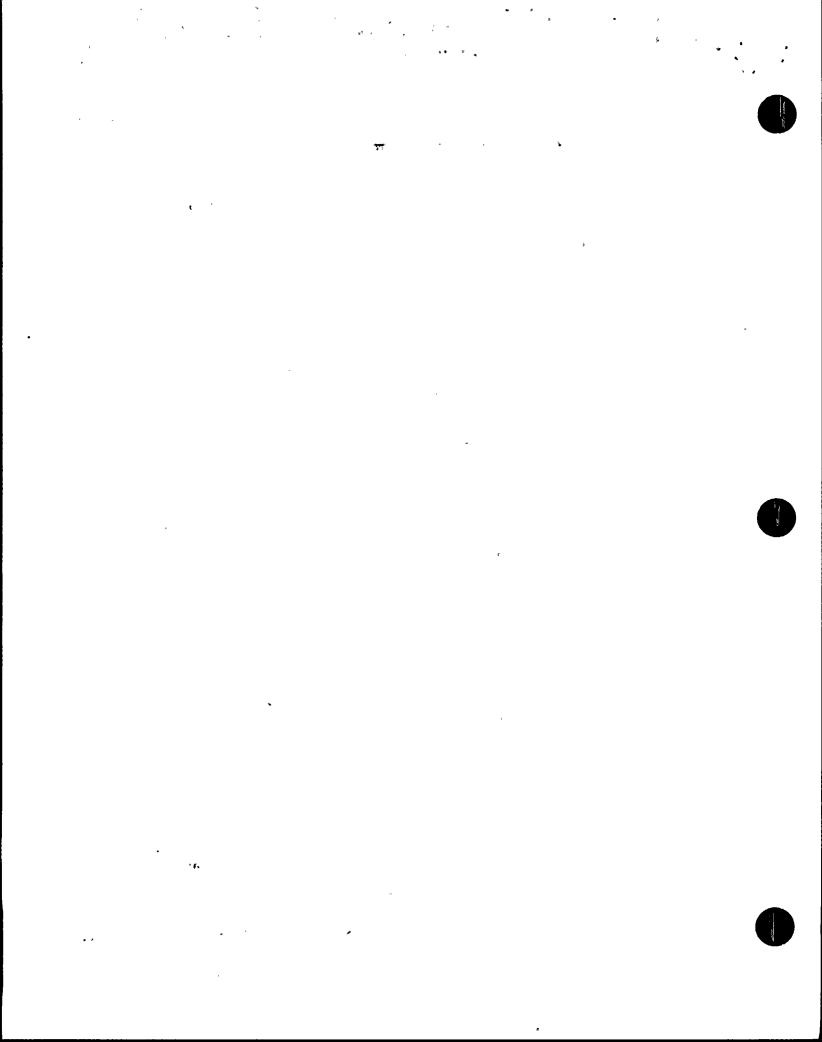
Lo + Lam - La/4 <= Lc <= Lo + Lam + La/4

0.289 + 0.048 - 0.063 <= 0.336 <= 0.289 + 0.048 + 0.063

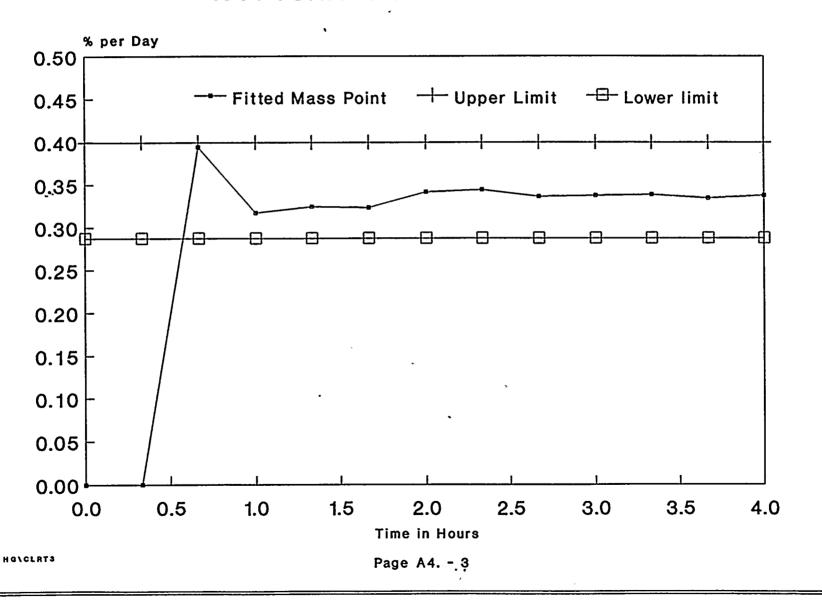
0.275 <= 0.336 <= 0.400

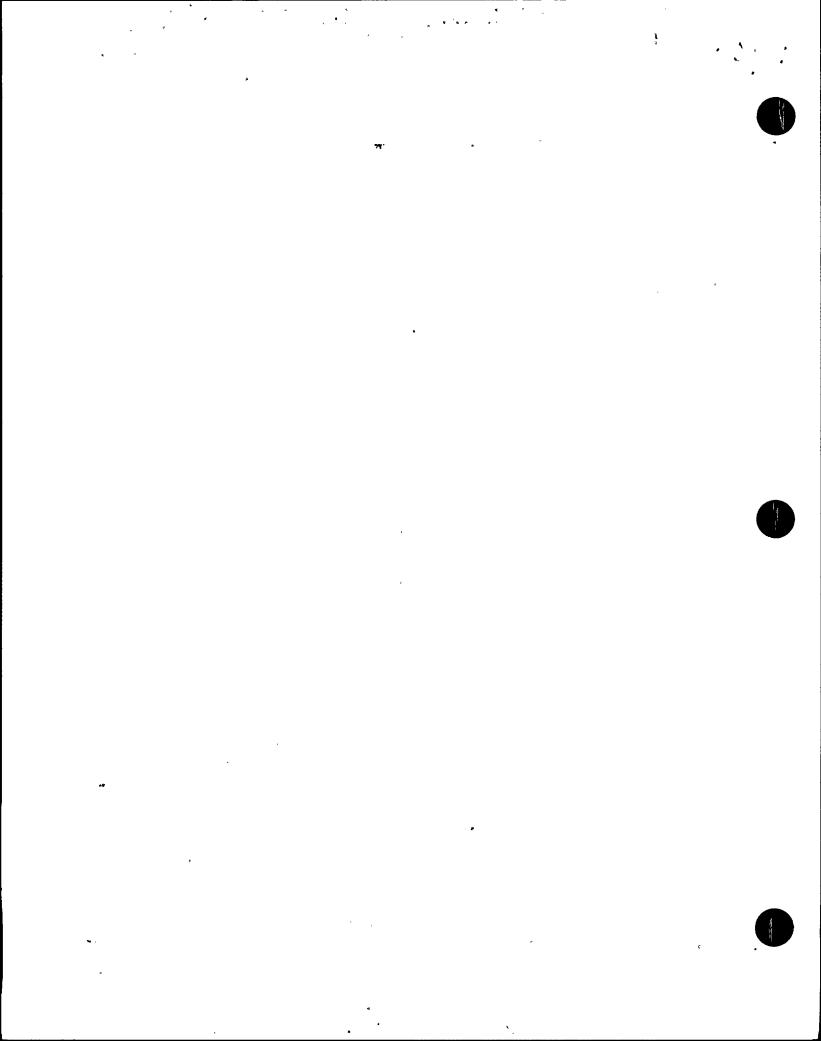
THE ACCEPTANCE CRITERIA FOR THIS TEST IS LEAKAGE BETWEEN 0.2745 % (0.275 %) PER DAY AND 0.3995 % (0.400 %) PER DAY.

THE SUPPLEMENTAL VERIFICATION TEST MET THE ACCEPTANCE CRITERIA AS SHOWN ABOVE AND AS GRAPHICALLY DEPICTED ON THE FOLLOWING PAGE.

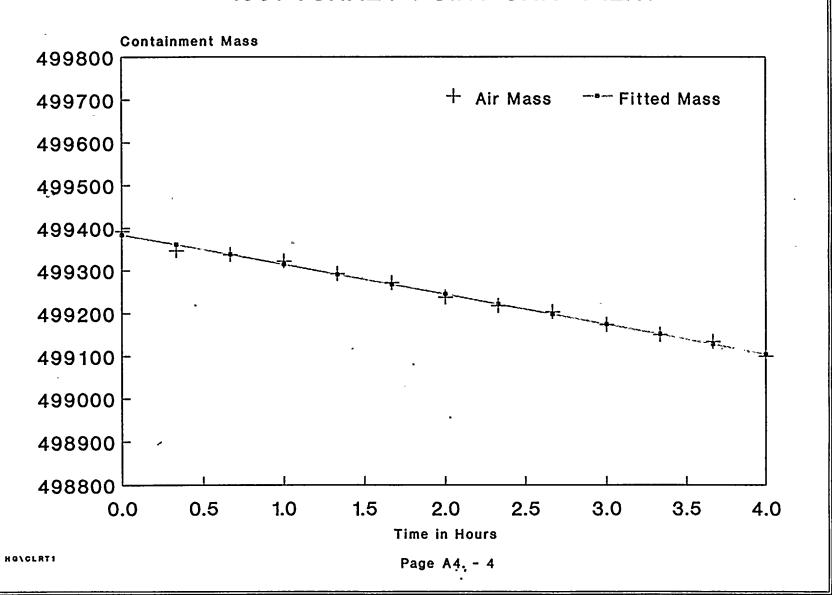


CLRT LEAKAGE RATES RELATIVE TO LIMITS 1991 TURKEY POINT UNIT 4 ILRT









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DESCRIPTION OF VARIABLES

AVE TEMP - CONTAINMENT MEAN TEMPERATURE CALCULATED FROM VOLUMETRICALLY WEIGHTED RTD SENSOR INDICATIONS.

PRESSURE - PRIMARY CONTAINMENT PRESSURE INDICATION.

VAPOR PRES - CONTAINMENT VAPOR PRESSURE CALCULATED FROM VOLUMETRICALLY WEIGHTED HUMIDITY/DEWPOINT SENSOR INDICATIONS.

LEAK SIM - SIMPLE TOTAL TIME MEASURED LEAKAGE RATE.

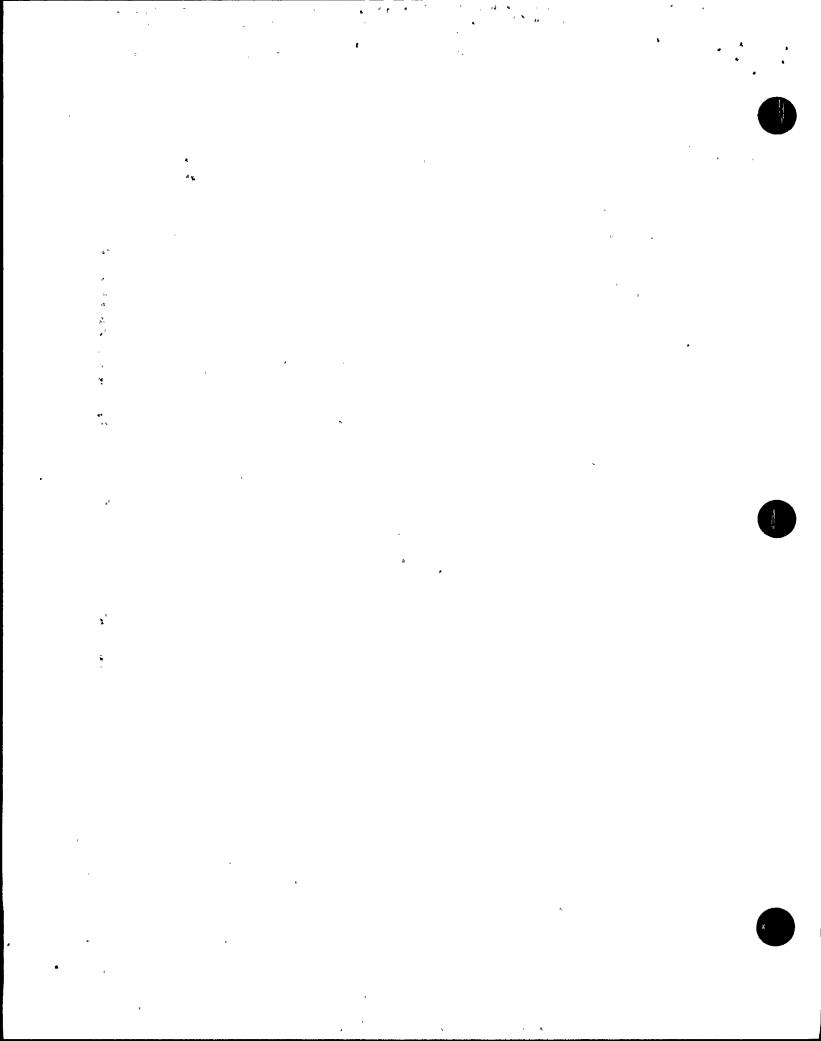
LEAK FIT - LEAKAGE RATE CALCULATED FROM FIRST ORDER REGRESSION OF AIR MASS DATA.

95% UCL - UPPER LIMIT OF THE 95% CONFIDENCE LEVEL OF FITTED LEAKAGE RATE DATA.

AIR MASS - CONTAINMENT AIR MASS.

NOTES FOR TABULAR DATA -

- 1. TABLE VALUES OF ZERO SIGNIFY THE DATA IS NOT APPLICABLE TO THE CALCULATION.
- 2. "DELETED" SIGNIFIES THE SENSOR WAS DELETED.
- 3. "REJECTED" SIGNIFIES THE SAMPLE WAS REJECTED.



CLRT VARIABLE TABLE SUMMARY

SAM NO	TIME HOURS	AVE TEMP DEG F	PRESSURE PSIA	VAP PRES PSIA	LEAK SIM %/DAY	LEAK FIT %/DAY	UCL %/DAY	AIR MASS LBS
1	0.00	88.756	66.078	0.6103	0.000	0.000	0.000	499392
2	0.33	88.741	66.070	0.6101	0.656	0.000	0.000	499347
· 3	0.67	88.727	66.067	0.6099	0.394	0.394	1.690	499337
4	1.00	88.712	66.063	0.6098	0.338	0.317	0.556	499322
5	1.33	88.696	66.057	0.6096	0.361	0.324	0.435	499292
6	1.67	88.679	66.052	0.6094	0.349	0.323	0.389	499271
7	2:00	88.667	66.046	0.6093	0.373	0.341	0.389	499237
8	2.33	88.649	66.041	0.6091	0.362	0.344	0.379	499217
9	2.67	88.632	66.037	0.6089	0.341	0.336	0.364	499203
10	3.00	88.616	66.031	0.6088	0.352	0.337	0.359	499173
11	3.33	88.600	66.026	0.6087	0.349	0.338	0.355	499150
12	3.67	88.585	66.022	0.6085	0.338	0.334	0.349	499134
13	4.00	88.573	66.016	0.6085	0.351	0.336	0.349	499100

SENSOR VOLUME FRACTIONS

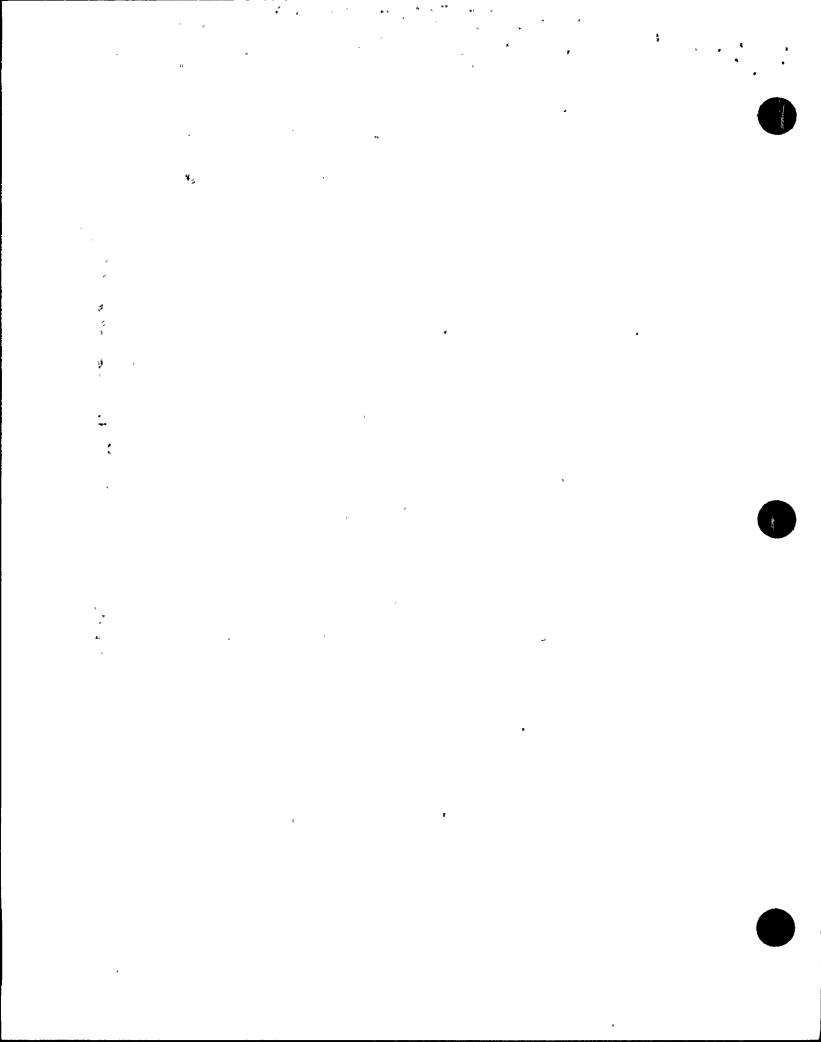
TEMPERATURE SENSORS

1 44 5	0 060222	0.060333	0.040000	0.040000	0.040000
1 to 5	0.060333	0.000333	0.04000	0.040000	0.04000
6 to 10	0.060333	0.060333	0.060333	0.033000	0.053333
11 to 15	0.053333	0.033000	0.053333	0.033000	0.033000
6 to 20	0.053333	0.053333	0.053333	0.033000	0.033000
1 40 21	0.060222				

HUMIDITY/DP SENSORS

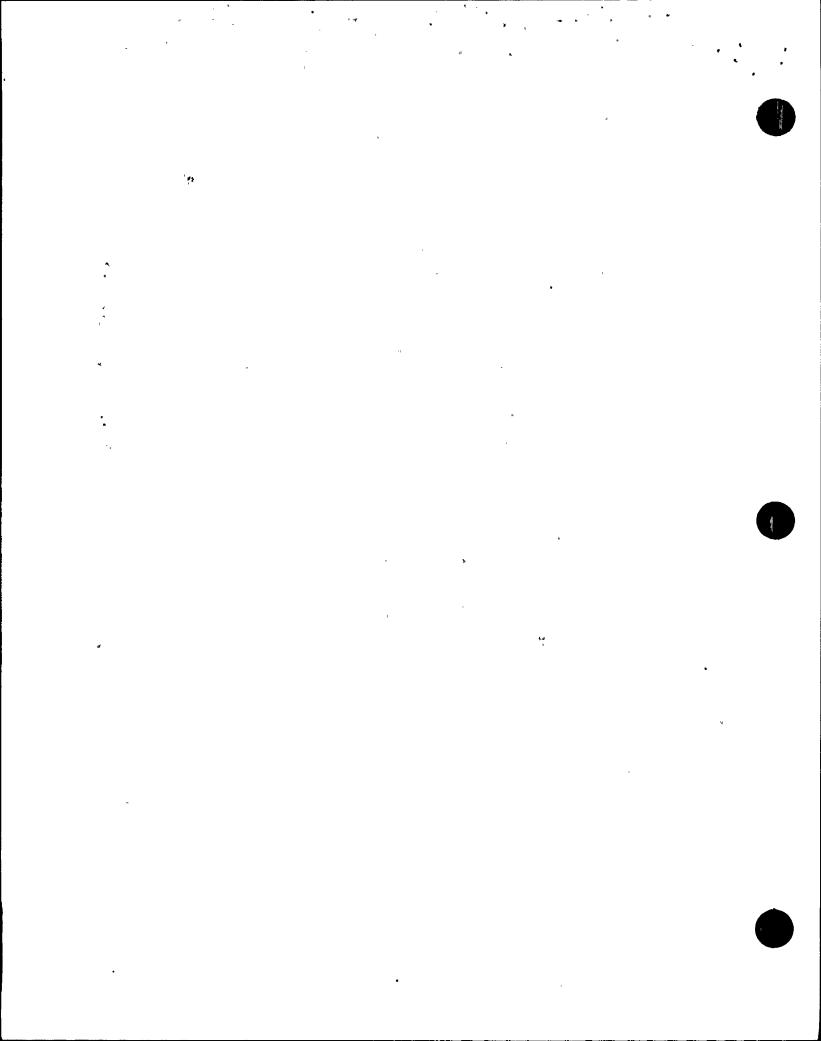
1 to 5	0.049500	0.049500	0.049500	0.049500	0.060000
6 to 10	0.060000	0.181000	0.181000	0.320000	0.000000

NOTE: VALUE OF ZERO INDICATES A DELETED SENSOR.



CLRT VARIABLE SUMMARY

SAMPLE NUMBER	DELTA HOURS	TEMP 1 DEG F	TEMP 2 DEG F	TEMP 3 DEG F	TEMP 4 DEG F	TEMP 5 DEG F	TEMP 6 DEG F
1 2 3 4 5 6 7 8 9 10 11 12 13	0.00 0.33 0.67 1.00 1.33 1.67 2.00 2.33 2.67 3.00 3.33 3.67 4.00	88.994 88.972 88.972 88.949 88.940 88.929 88.906 88.897 88.886 88.874 88.851 88.831	89.042 89.020 89.011 88.999 88.977 88.968 88.956 88.945 88.934 88.922 88.913 88.902 88.879	88.873 88.861 88.850 88.830 88.819 88.807 88.798 88.776 88.764 88.753 88.733 88.721 88.710	88.982 88.971 88.960 88.948 88.928 88.917 88.905 88.894 88.885 88.874 88.862 88.840 88.831	88.943 88.934 88.922 88.911 88.899 88.879 88.868 88.845 88.824 88.824 88.824	89.091 89.071 89.059 89.048 89.025 89.016 89.005 88.982 88.973 88.962 88.939 88.919
			CLRT VA	RIABLE SUMM	MARY		
SAMPLE NUMBER	DELTA HOURS	TEMP 7 DEG F	TEMP 8 DEG F	TEMP 9 DEG F	TEMP 10 DEG F	TEMP 11 DEG F	TEMP 12 DEG F
1 2 3 4 5 6 7 8 9 10 11 12. 13	0.00 0.33 0.67 1.00 1.33 1.67 2.00 2.33 2.67 3.00 3.33 3.67 4.00	88.876 88.853 88.842 88.821 88.810 88.799 88.787 88.778 88.735 88.735 88.735 88.735	89.165 89.154 89.143 89.134 89.111 89.088 89.079 89.045 89.045 89.045 89.025	87.260 87.271 87.260 87.260 87.260 87.260 87.251 87.251 87.251 87.251	89.178 89.169 89.158 89.135 89.115 89.092 89.072 89.049 89.038 89.018 88.995 88.984 88.963	89.086 89.055 89.021 89.000 88.966 88.934 88.903 88.860 88.826 88.771 88.771 88.728 88.708	87.837 87.837 87.826 87.826 87.826 87.826 87.826 87.826 87.826 87.826 87.826

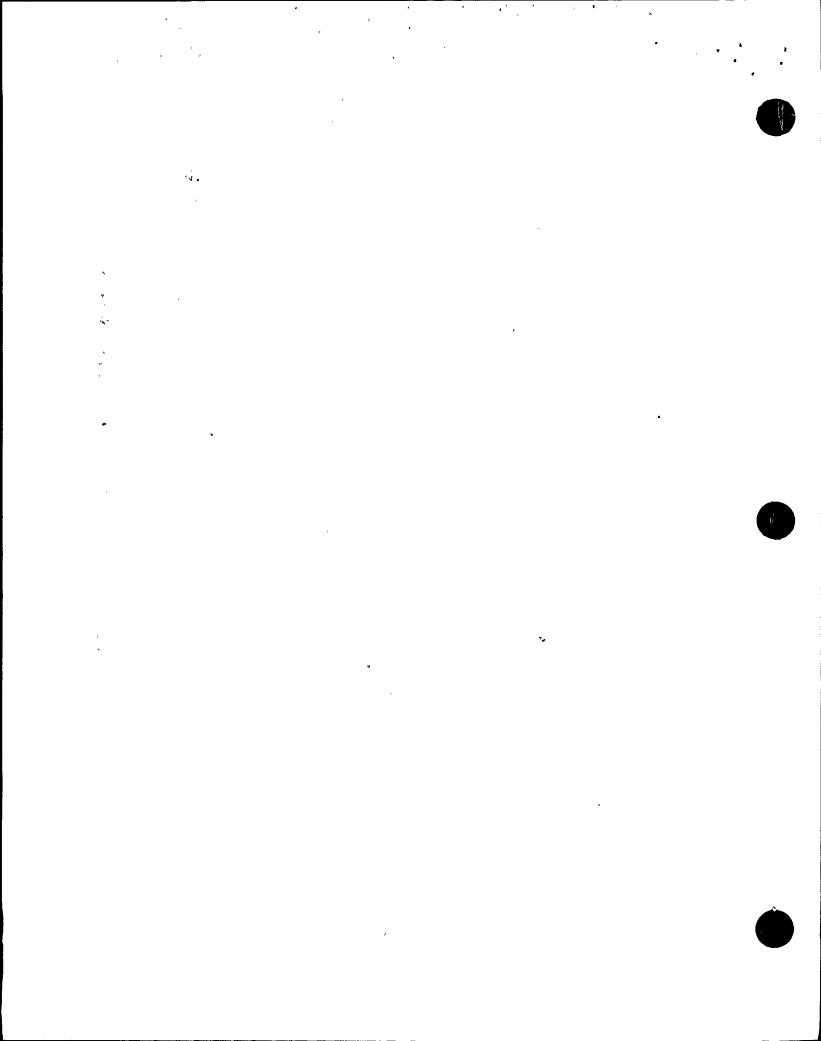


CLRT VARIABLE SUMMARY

SAMPLE NUMBER	DELTA HOURS	TEMP 13 DEG F	TEMP 14 DEG F	TEMP 15 DEG F	TEMP 16 DEG F	TEMP 17 DEG F	TEMP 18 DEG F
1	0.00	89.062	87.649	87.826	89.089	89.420	89.317
2	0.33	89.050	87.649	87.848	89.057	89.377	89.297
3	0.67	89.030	87649	87.837	89.025	89.344	89.274
4	1.00	89.007	87.649	87.848	89.002	89.312	89.252
5	1.33	88.987	87.649	87.860	88.982	89.269	89.231
6	1.67	88.964	87.649	87.871	88.948	89.194	89.209
7	2.00	88.942	87.649	87.880	88.917	89.194	89.188
8	2.33	88.921	87.649	87.880	88.883	89.129	89.166
9	2.67	88.899	87.649	87.880	88.851	89.086	89.146
10	3.00	88.887	87.649	87.891	88.754	89.074	89.123
îĭ	3.33	88.856	87.649	87.880	88.699	89.020	89.100
12	3.67	88.844	87.649	87.871	88.688	88.997	89.080
13	4.00	88.824	87.649	87.871	88.731	88.900	89.069

CLRT VARIABLE SUMMARY

SAMPLE	DELTA	TEMP 19	TEMP 20	TEMP 21
NUMBER	HOURS	DEG F	DEG F	DEG F
•	0.00	07 060	87.285	88.880
1	0.00	87.068	• • • • • •	
2	0.33	87.068	87.285	88.857
3	0.67	87.068	87.273	88.857
4	1.00	87.068	87.285	88.834
5	1.33	87.068	87.273	88.814
6	1.67	87.068	87.273	88.803
7	2.00	87.068	87.285	88.791
8	2.33	87.068	87.273	88.782
9	2.67	87.068	87.273	88.748
10	3.00	87.068	87.273	88.748
11	3.33	87.068	87.285	88.728
12.	3.67	87.077	87.285	88.717
12	4 00	87 068	87 285	88.694



CLRT VARIABLE SUMMARY

SAMPLE NUMBER	DELTA HOURS	PRES 1 PSIA	PRES 2 PSIA	HUM 1 % RH	HUM 2 % RH	HUM 3 % RH	HUM 4 % RH
1 2 3 4 5 6 7 8 9 10 11 12 13	0.00 0.33 0.67 1.00 1.33 1.67 2.00 2.33 2.67 3.00 3.33 3.67 4.00	66.076 66.070 66.069 66.059 66.054 66.050 66.046 66.041 66.037 66.031 66.024	66.078 66.070 66.067 66.063 66.057 66.052 66.041 66.037 66.031 66.026 66.022	94.108 94.100 94.126 94.125 94.117 94.131 94.137 94.166 94.177 94.181 94.207	92.482 92.494 92.484 92.477 92.488 92.462 92.482 92.476 92.458 92.471 92.485 92.471	93.545 93.539 93.535 93.551 93.550 93.549 93.573 93.579 93.602 93.608 93.618 93.627	92.505 92.494 92.489 92.500 92.494 92.491 92.499 92.505 92.517 92.522 92.544 92.540
			CLRT VAR	IABLE SUMM	ARY		
SAMPLE NUMBER	DELTA HOURS	HUM 5 % RH	HUM 6 % RH	HUM 7 % RH	HUM 8 % RH	HUM 9 % RH	HUM ·10 % RH
1 2 3 4 5 6 7 8 9 10 11 12 13	0.00 0.33 0.67 1.00 1.33 1.67 2.00 2.33 2.67 3.00 3.33 3.67 4.00	89.352 89.393 89.401 89.429 89.5513 89.550 89.602 89.625 89.625 89.724 89.757 89.823	88.882 88.916 88.936 88.987 89.080 89.106 89.166 89.225 89.288 89.335 89.393 89.449 89.526	90.583 90.624 90.614 90.642 90.657 90.657 90.717 90.752 90.798 90.809 90.842 90.874	90.461 90.472 90.480 90.503 90.531 90.564 90.635 90.659 90.717 90.710 90.767 90.792	90.653 90.653 90.667 90.676 90.723 90.715 90.740 90.746 90.769 90.809 90.802 90.868	DELETED

APPENDIX B LOCAL LEAKAGE RATE TESTING CONDUCTED SINCE THE LAST ILRT THE RESIDENCE OF THE PARTY OF T 3 844

			Appendix J 7	Type 'B' and 'C' I	.eakage Su	mmary		
PEN		TEST	EQUIPMENT/	AS FOUND		AS LEFT		
NUM	FUNCTION	TYPE	VALVES	LEAKAGE(CCM)	DATE	LEAKAGE(CCM)	DATE	REMARKS
5	PRT TO GAS	С	CV-516	18	07/23/90	18	807/23/90	
	ANALYZER			18	12/20/90	75	§ 06/19/91	
			SV-6385	18	07/23/90	18	07/23/90	-
ļ				18	12/20/90	18	8 806/19/918	
		_	01/0540		1:8:0:40(40)00	I managaman 4 o kalabanan m	*1207/00/04	1
6	NITROGEN	С	CK-518	380	12/19/90	18	07/20/91	NOTE 4
ł	TO PRT		CK-519	2000	12/19/90	225	07/20/91	INOIE
7	PRIMARY	С	CV-519A	18	01/15/91	18	07/11/91	1
'	WATER	U	CV-519B	COMBINATION TES	0 1 275200000000000000000000000000000000000		0,,,,,,	
	TO RCP/PRT		CV-522A	00				
	10 1101 /1 111		CV-522B					
			CV-522C					
ł								
8	PZR STEAM	С	CV-951	220	01/15/91	215	07/13/91	
	SAMPLE		CV-956A	18	01/18/90	18	01/18/90	
				18	01/16/91	100	8 (07/13/91)	
ŀ					F			1
9	PZR LIQUID	С	CV-953	1300	01/15/91		09/08/91	NOTE 2
	SAMPLE		CV-956B	18 +	01/16/91	18	07/19/91	
10	DODT AND	С	OV*4050A	00. Pro 00000000000 4 0 00000000000000		18	10/08/9 1	NOTE
10	RCDT AND PRT VENT	C	CV-4658A CV-4658B	18 18	01/15/91 12/26/90	18	© 07/07/91	INOTES
	PRI VENI		PCV-1014	1500	12/26/90	· · · · · · · · · · · · · · · · · · ·	10/13/918	NOTE 4
ļ			V-4656	80	01/14/91		10/08/91	1
	•		V		: :::::::O.17.174(O.12	. j energe en man (301281-010-013-15	jitores
11	ALT RHR	С	MOV-872	170	01/08/91	40	09/25/91	NOTE 6
''	,	•			1			1
14	LETDOWN	С	CV-200A	100	12/28/90	60	07/14/91	NOTE 7
			CV-200B	COMBINATION TES	Ϊ			
			CV-200C					
			CV-204	18	2 12/27/90	18	207/08/91]
	Page B. – 1							

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			Appendix J	Type 'B' and 'C' I	eakage Su	mmary		
PEN		TEST	EQUIPMENT/	AS FOUND		AS LEFT		
NUM	FUNCTION	TYPE	VALVES	LEAKAGE(CCM)	DATE	LEAKAGE(CCM)	DATE	REMARKS
15	CHARGING	C	HCV-121	18	12/27/90	18	07/31/91	NOTE 8
Ì			V-333	COMBINATION TES				
			CK-312C	60	12/27/90	130	07/02/91	
40	DAOV/DALIM	•	T. 10 (2.1.2.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1		1:00 OF 104 104		1207/00/04	7
16	PACV/PAHM	С	HV-4-1 HV-4-2	75 COMBINATION TES	05/01/91	18	07/09/91	
			PAHM-002A	COMBINATION 1ES				
			ENLINEO054		.		2 6 8 8 8 8 5 7 8 8 8	i
17	ACCUM TEST	С	V-895V	18	01/09/91	18	07/10/91	
								_
19A	CONT SPRAY	C	CK-890A	18	12/28/90		07/07/91	
			MOV-880A	18	12/28/90	18	07/08/91	NOTE 10
		_		XX.1		· Follows a victory————— contactory	3120-2222	l
19B	CONT SPRAY	С	CK-890B	10000	12/28/90	700		NOTE 11
			MOV-880B	18	12/28/90	35	<u>:[0///14/9]</u>	NOTE 12
20	RCS SAMPLE	С	SV-6427A	4100	04/19/91	18	07/05/91	NOTE 13
-			SV-6427B	25	04/23/91	18	07/05/91	-1
			SV-6428	400	07/31/90		07/31/90	
				85	04/23/91	55	07/05/91	
				·				
23	CONT SUMP	С	CV-2821	625	10/09/91	625	\$10/09/91	
	DISCHARGE		CV-2822	30000	10/09/91	25	18/10/15/91	NOTE 14
24	RCP SEAL	С	CK-298A	70	01/03/91	160	18001261018	NOTE 15
24	INJECTION	C	CK-298B	900	01/03/91	620		NOTE 16
	HOLOHON		CK-298C	18	01/04/91	35	08/27/91	
						× • • • • • • • • • • • • • • • • • • •		
25	RCP SEAL	С	MOV-6386	1220	07/22/90	50	07/26/90	NOTE 17
	RETURN			330	01/07/91	50	07/12/91	NOTE 17
			MOV-381	30	01/07/91	25	07/13/91	NOTE 18
	Page B. – 2				• •	··········		

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			Appendix J	Type 'B' and 'C' L	æakage Sur	nmary	
PEN		TEST	EQUIPMENT/	AS FOUND	_	AS LEFT	
NUM	FUNCTION	TYPE	VALVES .	LEAKAGE(CCM)	DATE	LEAKAGE(CCM)	DATE REMARKS
29	INSTRUMENT	C	CK-40-340A	950	02/04/91	330	£07/11/91
	AIR		CK-40-336	8025	02/04/91	910	07/01/91 NOTE 19
ŀ						-	
30	BREATHING	С	BA-201	18	11/28/90	18	07/04/91
	AIR		CV-6165	75	11/28/90	55	07/04/91
1	:						
31	RCDT TO GAS	С	CV-4659A	18	07/23/90	18	07/23/90
	ANALYZER		CV-4659B	18	02/04/91	18	06/19/91
1				COMBINATIONITES	I		
	CONTAINMENT	С	CK=11=003	500	07/22/90	500	07/22/90
32	CONTAINMENT AIR SAMPLE	C	CN-1:1-003	810	12/15/90	500	07/16/91
	AIR SAMPLE		SV-2912	900	07/22/90	900	07/22/90
			PAHM-001A	300	12/14/90	18	07/16/91
7			PAHM-001B	COMBINATION TES	. 🕷 / 👀 (00000000000000000000000000000000000		
			7.7 17 17 17 17 17 17 17 17 17 17 17 17 17	*** • • • • • • • • • • • • • • • • •	*******************	127000000000000000000000000000000000000	
33	CONTAINMENT	С	SV-2911	110	07/22/90	110	07/22/90
1	AIR SAMPLE			80	12/14/90	725	07/16/91
			SV-2913	280	07/22/90	280	07/22/90
				200	12/14/90	450	08/18/91
		~		· ·			
34	SERVICE	С	CK-40-205	980	12/17/90	425	08/15/91 NOTE 20
	AIR		V-40-204	1000	12/17/90	90	07/11/91 NOTE 21
			HV-17	COMBINATION TES	Т		
		_	(managed and a section	·	(1880) o a a a a a a a a	In.,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	
35	CONT PURGE	С	POV-2600	2200	07/22/90	2200	07/22/90 NOTE 22
ĺ	SUPPLY		POV-2601	11700	12/15/90	780	10/06/91
				COMBINATIONITES	1557		
36	CONT PURGE	С	POV-2602	530	07/22/90	530	07/22/90 NOTE 23
30	EXHAUST	U	POV-2603	10500	12/15/90	500 500	10/15/91
	LAHAOOI	-	7.51=2000	COMBINATION TES	8. ♥ 6860,8 28 00 00 00000000000000000000000000000000		
	Page B 3		***************************************	A	# 11 1 (\$ 10 190 Brid 1000000000000000000000000000000000000	Franco and an accordance in a polymery	V 1 - Construction (1990)
<u> </u>							

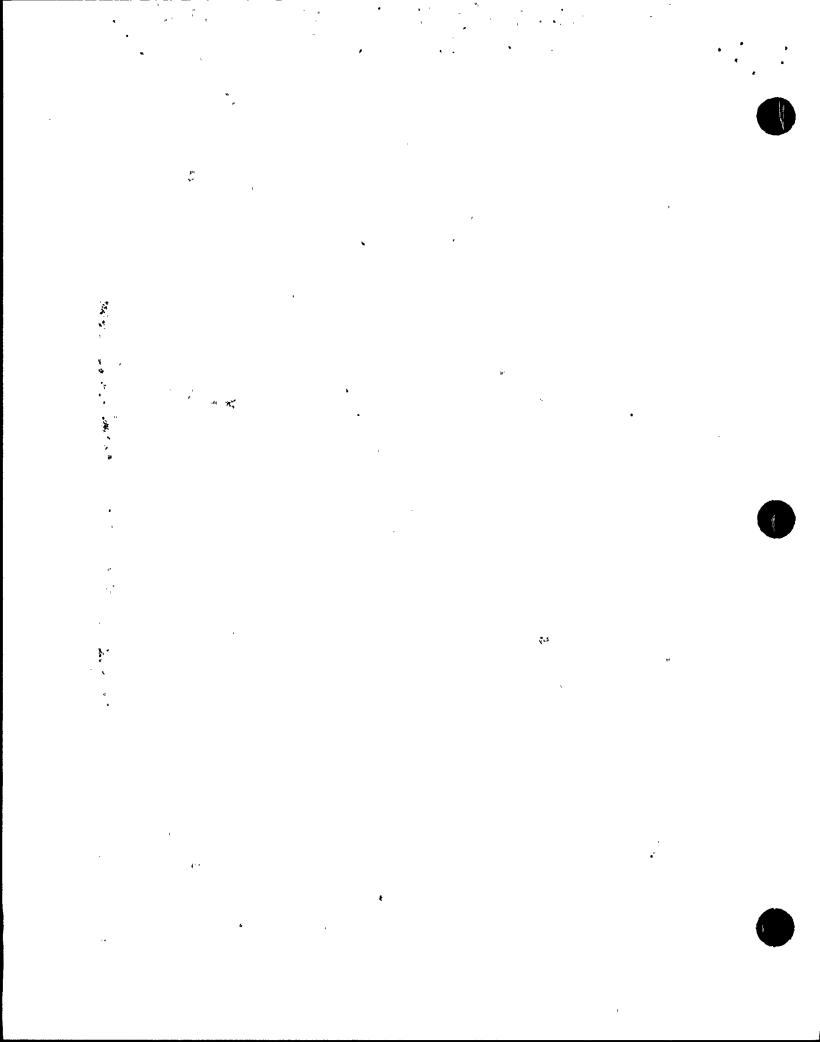
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PEN				Appendix J 7	Type 'B' and 'C'	Leakage Sur	nmary		
SPARE C V=10-879 18 07/23/90 18 07/23/90 18 10/07/91 18 10/07/91 18 10/07/91 18 10/07/91 18 10/07/91 18 10/07/91 18 10/07/91 18 10/07/91 18 10/07/91 18 10/08/91 18	PEN		TEST				AS LEFT		
18	NUM	FUNCTION							REMARKS
CAP	37	SPARE	С	V-10-879	***				
18									NOTE 24
38 ELECTRICAL B CANISTERS 185 07/21/90 185 07/21/90 39 FUEL X-FER B O-FINGS 18 11/27/90 70 10/11/91 40 EQUIP HATCH B O-FINGS 18 08/01/90 18 04/12/90 41 PERS HATCH B ANNULUS 460 08/15/90 460 09/15/90 NOTE 25 180 08/01/90 250 06/20/91 42 NITROGEN TO ACCUMULATOR C C CK-945E 85000 09/26/89 1400 09/27/89 OCCUMULATOR CV-955 310 09/27/89 310 09/27/89 00/27/99 00/27/89 00/27/99 00/2				CAP	000			72	
108 06/21/91 108 06/21/91 108 06/21/91 108 06/21/91 108 06/21/91 108 06/21/91 109 106/21/91 109 109/21/91					18.	02/07/91	18	\$10/08/91°	
39 FUEL X-FER B	38	ELECTRICAL	В	CANISTERS	185	07/21/90	185	07/21/90	
40 EQUIP HATCH B O-RINGS 18 04/12/90 18 04/12/90 18 04/12/90 18 04/12/90 18 04/12/90 18 04/12/90 18 04/12/90 18 04/12/90 18 04/12/90 18 04/12/90 18 04/12/90 18 04/12/90 18 04/12/90 18 04/12/90 18 04/12/90 18 05/15/90 NOTE 25 05/17/91 05/17					108	06/21/91	108	£06/21/91]
18	39	FUEL X-FER	В	O-RINGS	18	11/27/90	70	§10/11/91]
18			_			**!**** 0.440100°	[:::::::::::::::::::::::::::::::::::::	×0.44.0400	1
41 PERS HATCH B ANNULUS 460 08/15/90 460 08/15/90 NOTE 25 42 NITROGEN TO ACCUMULATOR C CK-945E 85000 09/26/89 1400 09/27/89 NOTE 26 740 12/19/90 250 06/20/91 CV-855 310 09/27/89 310 09/27/89 46A CONT PRESS SWITCHES B PS-2008 18 07/22/90 18 07/22/90 COMBINATION TEST 46B CONT PRESS B PS-2058 18 02/21/91 18 07/23/90 COMBINATION TEST 46C CONT PRESS SWITCHES B PS-2007 25 07/23/90 25 07/23/90 COMBINATION TEST 46C CONT PRESS SWITCHES B PS-2007 25 07/23/90 25 07/23/90 COMBINATION TEST COMBINATION TEST	40	EQUIP HATCH	В	O-RINGS	MARCH 1997			 	
1000 02/17/91 400 09/29/91 422 NITROGEN TO ACCUMULATOR C 85000 09/26/89 1400 09/27/89 06/20/91 CV-855 310 09/27/89 310 09/27/89 310 09/27/89 400 12/19/90 145 06/20/91					<u> </u>	<u> </u>	<u> </u>	EIOLIDIAI®]
1000 02/17/91 400 09/29/91 422 NITROGEN TO ACCUMULATOR C 85000 09/26/89 1400 09/27/89 06/20/91 CV-855 310 09/27/89 310 09/27/89 310 09/27/89 400 12/19/90 145 06/20/91 400 12/19/90 145 06/20/91 400 12/19/90 145 06/20/91 400 12/19/90 18 07/22/90 18 07/23/90 18	1	DEDC HATCH	D	ANNUILLIS	460		1	÷08/15/90\$	NOTE 25
ACCUMULATOR 740	4,1	PERSTATOR	5	ANTOCOO	- COO L.				4
ACCUMULATOR 740	12	NITROGEN TO	C	CK_945E	85000	09/26/89	1400	809/27/89	NOTE 26
CV-855 310 09/27/89 310 09/27/89	42		J	OK-546E	WV L	<u></u>		 	
46A CONT PRESS B PS-2008 18 07/22/90 18 07/22/90 SWITCHES B PS-2057 18 02/20/91 18 07/22/90 18 10/07/91 18 07/07/		,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,		CV-855					1
SWITCHES PS-2057 18					(27)		I	A]
SWITCHES PS-2057 18	46A	CONT PRESS	В	PS-2008	18	07/22/90	18	(07/22/90)	1
46B CONT PRESS B PS=2009 18 07/23/90 18 07/23/90 18 00/23/90 18 00/23/90 18 00/23/90 18 00/23/91 18 00/23/91 18 00/23/91 18 00/23/91 18 00/23/91 18 00/23/91 18 00/23/91 18 00/23/91 18 00/23/91 18 00/23/91 18 00/23/91 18 00/23/91 18 00/23/91 18 00/23/91 18 00/23/91 18 00/23/91				- Paga, 2000ki, Alike na 2000000000000000	XXXX.¥ XXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX	b GB 00000000000000000000000000000000000	18	10/07/91	
SWITCHES PS=2058 18 02/21/91 18 10/06/91 COMBINATION TEST 46C CONT PRESS B PS=2007 SWITCHES PS=2056 18 07/23/90 09/27/91 COMBINATION TEST COMBINATION TEST					COMBINATION TE	ST			
SWITCHES PS=2058 18 02/21/91 18 10/06/91 COMBINATION TEST 46C CONT PRESS SWITCHES B PS=2007 PS=2056 18 07/23/90 09/27/91 COMBINATION TEST COMBINATION TEST	46B	CONT PRESS	В	PS-2009	18	07/23/90	18	07/23/90	1
46C CONT PRESS B PS=2007 25 07/23/90 25 07/23/90 SWITCHES PS=2056 18 02/21/91 18 09/27/91 COMBINATION TEST		- ·		- 10% ar 60% a castar a chaill (1000) (1000)	18	0000 0 10010011100000000000000000000000	18	/10/06/91	
SWITCHES PS-2056 18 09/27/91 18 09/27/91 COMBINATION TEST					COMBINATION TE	ST			J
COMBINATION TEST	46C	CONT PRESS	В	- 100 - 4000 - Conductor 2000000000000000000000000000000000000	9608 B 0006000x 9 .662042944 AA 4046968 2000000	888 & 79965598000000000000000000000000000000000		 Bibliochiologic, processors and 	
		SWITCHES		PS-2056	200700 8	v65° 8 - 46000000 (brown gydd ywd y 6006)	18	09/27/91	
I 4308 B 4		Page B. – 4			## COMBINATION TE	> 1		Transmin	<u> </u>

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		-	Appendix J	Type 'B' and 'C' I	eakage Sur	mmary		
PEN		TEST	EQUIPMENT/	AS FOUND		AS LEFT		
NUM	FUNCTION	TYPE	VALVES	LEAKAGE(CCM)	DATE	LEAKAGE(CCM)	DATE	REMARK
47	PRIMARY WATER	С	V-10-582 CK-567	3800 COMBINATION TES	# 5000000000000000000000000000000000000	25	08/06/91	NOTE 27
48	RCP ELECT	В	CANISTERS	36 48	07/23/90 12/05/90		07/23/90	
40	EMEDO HATOH	Б	ANNULUS	900	07/18/90	900	07/18/90	<u>-</u> ገ
49	EMERG HATCH	В	MINIOCOS	900	03/16/91			2
51	PÀCV/PAHM	С	HV-4-3 HV-4-4	80 18	07/24/90 01/09/91	, 8	07/24/90 07/13/91	
	•		PAHM-002B	COMBINATION TES	T			
52	RCDT PUMP DISCHARGE	С	CV-4668A CV-4668B	18 COMBINATION TES	12/03/90 T	18	06/20/91	
54A	RECIRC SUMP SUCTION	С	MOV-860A MOV-861A	1100 COMBINATION TES	: * 2002:3000000000000000000000000000000000	120	07/11/91	NOTE 2
54B	RECIRC SUMP SUCTION	С	MOV-860B MOV-861B	360 COMBINATION TES	01/09/91 T	105	07/11/91	NOTE 2
55	ACCUMULATOR	С	CV-955C	80	04/23/91		© 08/01/91	-4
	SAMPLE		CV-955D CV-955E	100 65	04/19/91 04/19/91		08/01/91 08/01/91	₩
İ			CV-956D	750	04/24/91	18	08/01/91	NOTE 3

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			Appendix 11	Tyme 'R' and 'C' Le	eakage Sur	nmary		
PEN		TEST	Appendix J Type 'B' and 'C' Leakage Sur EQUIPMENT/ AS FOUND			AS LEFT		
NUM	FUNCTION	TYPE	VALVES	LEAKAGE(CCM)	DATE	LEAKAGE(CCM)	DATE	REMARKS
61A	SPARE	С	CAP	18 18	07/23/90 11/28/90	18 18	07/23/90 07/15/91	
61B	DEAD WEIGHT	С	V-2024	18	07/22/90	18	07/22/90	
	TESTER		CAP	18 COMBINATION TEST	12/29/90	18	09/03/91	
63	INST AIR	С	CV-2819	67.	07/21/90 01/02/91	67 95	06/29/91	
	BLEED		CV-2826	90	07/21/90	800	00/23/31	
	. ≈.		0 / 2020	420	01/02/91	400	06/29/91]
65A	ILRT TEST LINE	В	FLANGES	45	11/27/90	18	10/20/91	
65B	ILRT TEST LINE	B/C	V-2025 FLANGE	18 COMBINATION TEST	01/28/91	18	10/20/91	
65C	ILRT TEST LINE Page B. – 6	B/C	V-2026 FLANGE	18 COMBINATION TEST	01/28/91	18	10/20/91	

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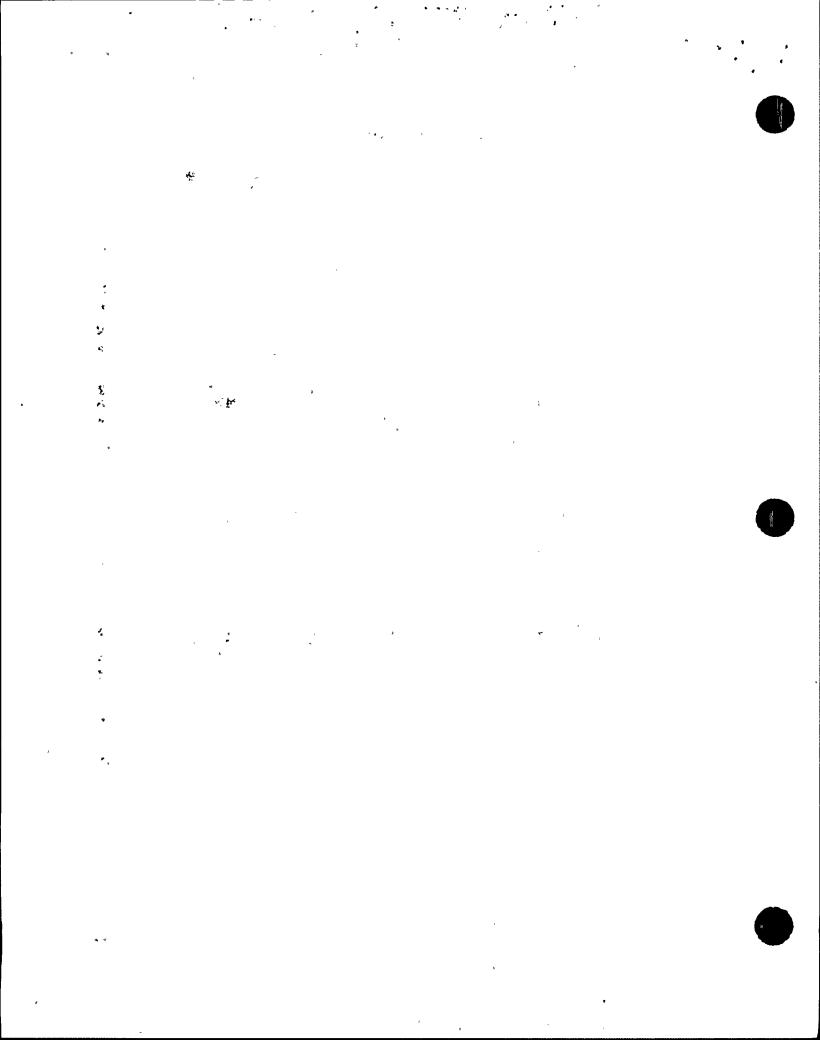
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Appendix J Type 'B' and 'C' Leakage Summary

NOTES:

- 1. CHECK VALVE 519 REPLACED
- 2. REPLACED VALVE BODY AND LAPPED SEAT FOR CV-953
- 3. REPLACED DIAPHRAGM FOR CV-4658A
- 4. PCV-1014 OVERHAULED
- 5. REPLACED DIAPHRAGM AND ADJUSTED VALVE STROKE FOR V-4656
- 6. MOV-872 DISASSEMBLED AND DISK DRILLED TO PREVENT THERMAL BINDING
- 7. CV-200A PACKING ADJUSTED
- 8. HCV-121 OVERHAULED TO REPAIR BONNET LEAK
- 9. CK-890A DISASSEMBLED, INSPECTED AND REASSEMBLED
- 10. MOTOR OPERATOR FOR MOV-880A OVERHAULED
- 11. CK-890B DISASSEMBLED, INSPECTED AND REASSEMBLED
- 12. MOTOR OPERATOR FOR MOV-880B OVERHAULED
- 13. SV-6427A REPLACED
- 14. CV-2822 OVERHAULED
- .15. CK-298A REPLACED
- 16. CK-298B REPLACED
- 17. MOTOR OPERATOR FOR MOV-6386 OVERHAULED
- 18. MOTOR OPERATOR FOR MOV-381 OVERHAULED
- 19. CK-40-336 REPLACED
- 20. CK-40-205 REPLACED
- 21. V-40-204 SEAT LAPPED AND PACKING FOR HV-17 REPLACED
- 22. REPLACED PACKING ON POV-2601; CLEANED SEATS FOR BOTH POV-2600,2601
- 23. REPLACED PACKING ON POV-2603; CLEANED AND ADJUSTED SEATS FOR BOTH POV-2602, 2603
- 24. V-10-879 REPLACED
- 25. PERSONNEL HATCH OVERHAULED
- 26. CLEANED AND LAPPED VALVE INTERNALS FOR CK-945E
- 27. SEATS FOR V-10-582 AND CK-567 LAPPED
- 28. MOTOR OPERATORS FOR MOV-860A, 861A OVERHAULED
- 29. MOTOR OPERATORS FOR MOV-860B, 861B OVERHAULED
- 30. CV-956D OVERHAULED

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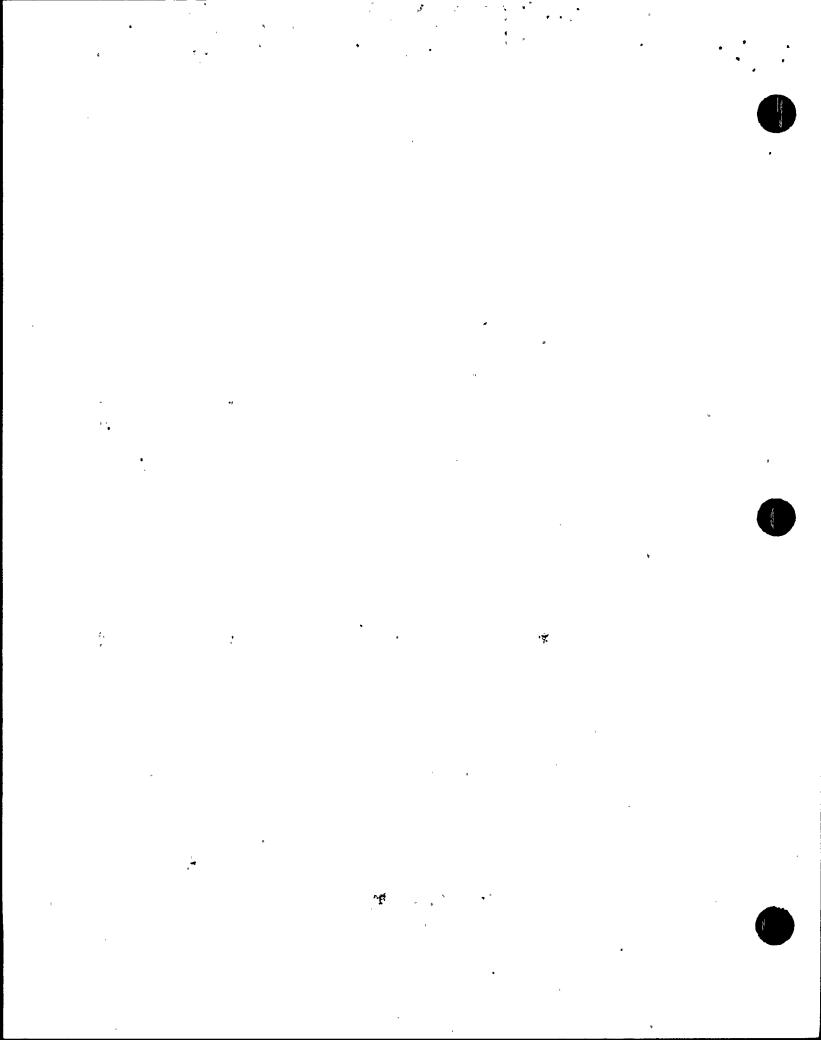


1990-1991 LOCAL LEAKAGE RATE SUMMARY ANALYSIS

The as found ILRT, by analysis, is used to show what the results of performing an ILRT at the beginning of the outage would have been, before any repairs or adjustments were made to the penetrations. The as found minimum pathway leakage, the repairs performed and the as left minimum pathway leakage for each boundary or penetration were reviewed. The net leakage contribution for each penetration was determined utilizing the following criteria:

- 1. A leakage rate add-on equivalent to the repair improvement is assigned to each penetration.
- 2. The net equivalent leakage assigned to the penetration is the lowest leakage of the valve grouping (e.g. simulates minimum pathway leakage).
- 3. If a repair was not performed on a containment isolation valve, and a reduction in leakage is noted between the as found and as left test, no penalty is required to be assessed.
- 4. No leakage credit is taken if the as left leakage rate is higher than the as found leakage rate. Only those penetrations where repairs were made to the isolation valves are included in this attachment.
- 5. For series isolation valves tested together (i.e. combination tests), the penetration net equivalent leakage is half the difference between the as found and the as left leakage rates when both valves are repaired at the same time. If only one valve is repaired or both valves are repaired at different times, subsequent analysis of test results may be performed to determine the penalty to be assessed.
- 6. When the summation of the leakage equivalent and the leakage measured during a successful Type A test is greater than L_a , the penetration(s) with excessive leakage(s) will be analyzed to determine the cause of the failure and/or corrective action taken to prevent recurrence.
 - 7. All measured leakage rate values are in units of cubic centimeters per minute (CCM) at 50 psig.

Based on the above criteria and the values tabulated on the next page, the net equivalent leakage of 0.036 percent/day, when added to the results of this ILRT (0.057 percent/day mass point UCL plus corrections), indicates that the as found ILRT test result, determined by analysis (0.093 percent/day) is below the plant's maximum allowable leakage rate of 0.25 percent/day.



1990-1991 LOCAL LEAKAGE RATE SUMMARY ANALYSIS

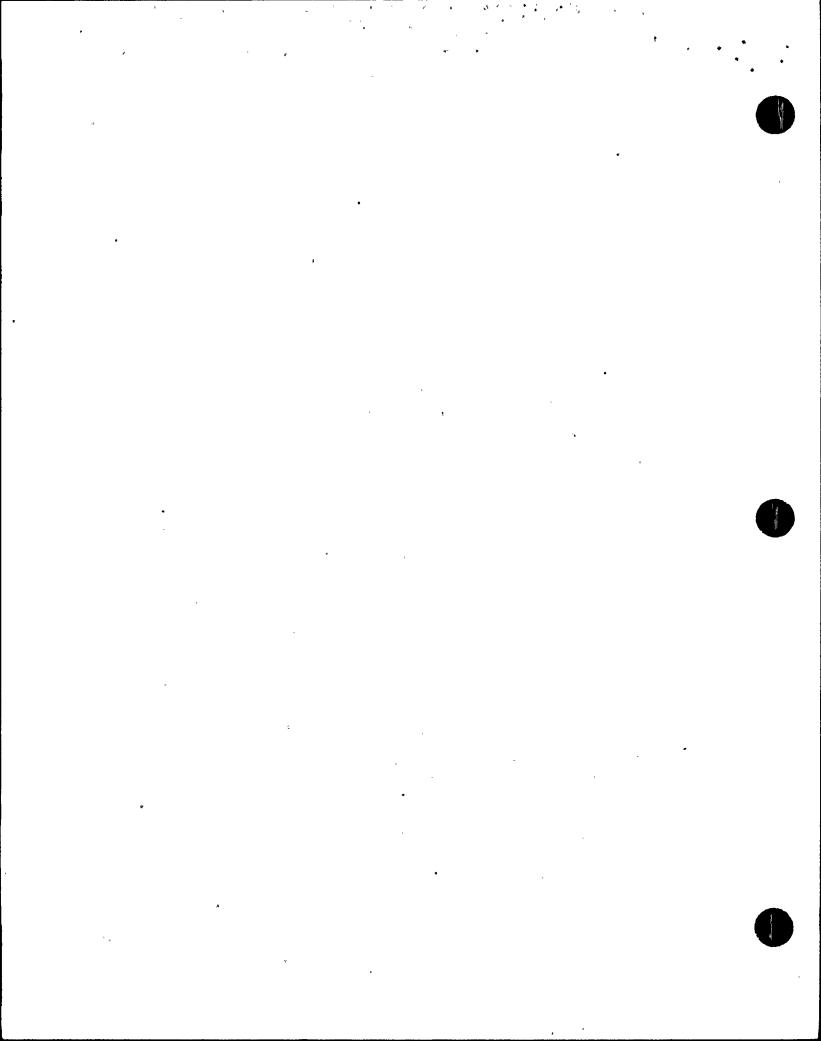
PEN.		AS FOUND	AS LEFT	PENALTY	•
NUM.	SYSTEM	LEAKRATE	LEAKRATE	<u>ASSESSED</u>	REMARKS (NOTE 1)
6	PRT TO GAS ANAL.	380	18	0	CRITERIA 3
10	NITROGEN TO PRT/RCDT	98	36	62	-
11	ALTERNATE LHSI	170	40	130	
19B	CONT SPRAY DISCH	18	35	0	CRITERIA 4
20	RCS SAMPLE	85	18	67	=
23	CONT SUMP DISCHARGE	625	25	600	•
24A	RCP SEAL INJECTION	70	160	0	CRITERIA 4
24B	RCP SEAL INJECTION.	900	620	280	
25	RCP SEAL RETURN	30	25	5	
29	INSTRUMENT AIR	950	330	620	
33	CONT AIR SAMPLE	80	450	0	CRITERIA 4
34	SERVICE AIR	980	180	.800	
35	CONT PURGE SUPPLY	11700	780	360	CRITERIA 5, NOTE 2
36	CONT PURGE EXHAUST	10500	500	5000	CRITERIA 5
41	PERSONNEL HATCH	1000	400	300	CRITERIA 5
42	NITROGEN TO ACCUM	400	145	255	
47	PRIMARY WATER	3800	25	1888	CRITERIA 5
54A	CONT RECIRC SUMP	1100	120	490	CRITERIA 5
54B	CONT RECIRC SUMP	360	105	128	CRITERIA 5
· 55	ACCUMULATOR SAMPLE	245	18	227	
65A	ILRT PRESSURIZATION	45	18	14	CRITERIA 5

TOTAL 11226 CCM

NOTE 1: CRITERIA REFERED TO IN THE REMARKS COLUMN ARE THOSE SHOWN ON THE PREVIOUS PAGE.

NOTE 2: PENETRATION 35 WAS RETESTED FOLLOWING REPACK OF POV-2601 WITH A RECORDED LEAKAGE OF 1500 CCM, NO WORK WAS PERFORMED ON POV-2600.

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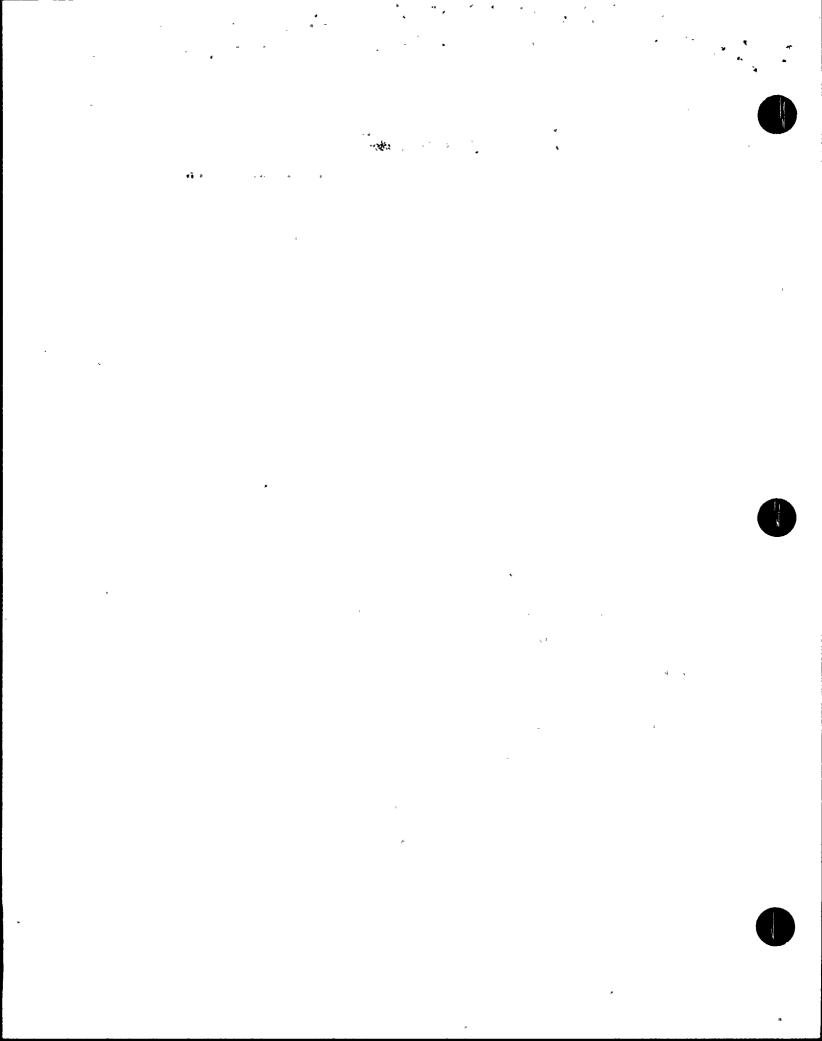


APPENDIX C METEOROLOGICAL DATA

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1991 TURKEY POINT UNIT 4 ILRT METEOROLOGICAL DATA

DATE 1991	TIME	PRESSURE IN. HG	TEMP	WIND DIRECTION	WIND SPEED KNOTS
10/15	1900	, 29.826	73	110	4
10/15	2007	29.831	73	170	3
10/15	2101	29.836	74	120	2
10/15	2211	29.840	74 .	calm	· calm
10/15	2310	29.845	74	90	2
10/16	0011	29.830	74	calm	calm
10/16	0108	29.820	74	calm	calm
10/16	0206	29.805	74	calm	calm
10/16	0311	29.785	73	060	2
10/16	0404	29.770	73	030	4
10/16	0515	29.770	74	080	2
10/16	0600	29.770	74	020 '	20
10/16	0807	28.785	74	340	6
10/16	1210	29.870	82	360	13
10/16	1600	29.845	82	360	13
10/16	2000	29.885	77	350	3
10/17	0002	29.950	70	360	4.
10/17	0400	29.950	64	330	2
10/17	0805	30.030	66	360	5
10/17	1240	30.065	82	058	10
10/17	1542	30.015	80	060	10
10/17	1658	30.010	80	070	11
10/17	1759	30.025	78	060	8
10/17	1924	30.050	75	060	6
10/17	2000	30.065	75	060	6



1991 TURKEY POINT UNIT 4 ILRT METEOROLOGICAL DATA

DATE 1991	TIME	PRESSURE IN. HG	TEMP OF	WIND DIRECTION	WIND SPEED KNOTS
10/17	2120	30.085	76	060	5
10/17	2155	30.095	73	050	3
10/17	2304	30.100	73	360	2
10/17	2358	30.100	73	360	4
10/18	0101	30.085	72	calm	calm
10/18	0201	30.075	74	360	4 ·
10/18	0258	30.065	74	360	2
10/18	0405	30.060	74	010	3
10/18	0501	30.060	75	030	6
10/18	0550	30.074	74	020 ،	3
10/18	0702	30.080	74	010	3
10/18	0801	30.115	75 `	010 '	3
10/18	0859	30.124	79	020	5
10/18	0955	30.145	81	040 ·	12
10/18	1058	30.151	82	050	12
10/18	1200	30.130	84	050	15
10/18	1305	30.100	84	060	14
10/18	1405	30.082	84	050	14
10/18	1500	30.055	85	050	15
10/18	1600	30.035	85	050	13
10/18	1728	30.035	82	050	13
10/18	1800	30.045	81	060	12
10/18	1915	30.060	78	040	12
10/18	2010	30.075 ,	78	040	8
10/18	2106	30.090	78	080	5

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1991 TURKEY POINT UNIT 4 ILRT METEOROLOGICAL DATA

DATE 1991	TIME	PRESSURE IN. HG	TEMP	WIND DIRECTION	WÎND SPEED KNOTS
10/18	2204	30.085	79	040	8
10/18	2310	30.075	78	080	4
10/18	2358	30.075	78	050	8
10/19	0158	30.045	78	030	2
10/19	0307	30.015	75	020	4
10/19	0402	30.005	74	360	4
10/19	0500	30.010	76	050	6
10/19	0558	30.000	74	calm	calm
10/19	0900	30.040	76	350	6
10/19	1011	30.070	77	040	6
10/19	1111	30.075	77	090	5
10/19	1215	30.020	85	calm '	calm
10/19	1330	30.000	86	120	3
10/19	1430	29.997	83	. 070	3
10/19	1530	29.950	85	090	5
10/19	1630	29.95	84	090	4
10/19	1726	29.955	82	080	5

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