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 ALEXICH, M. P. Indiana & Michigan Electric Co.
 RECIP. NAME RECIPIENT AFFILIATION
 DENTON, H. R. Office of Nuclear Reactor Regulation, Director (post 851125)

SUBJECT: Forwards response to BJ Youngblood 860402 request for addl info re NUREG-0737, TMI Action Item II.D.1 on relief & safety valve testing. Responses to Questions 3 & 4d postponed until addl info provided by NRC.

see RPTS

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INDIANA & MICHIGAN ELECTRIC COMPANY

P.O. BOX 16631
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July 30, 1986
AEP:NRC:0585I

Donald C. Cook Nuclear Plant Unit Nos. 1 and 2
Docket Nos. 50-315 and 50-316
License Nos. DPR-58 and DPR-74
RESPONSE TO NRC, REQUEST FOR ADDITIONAL INFORMATION
REGARDING TMI ACTION ITEM II.D.1 ON RELIEF AND SAFETY
VALVE TESTING

Mr. Harold R. Denton, Director
Office of Nuclear Reactor Regulation
U.S. Nuclear Regulatory Commission
Washington, D.C. 20555

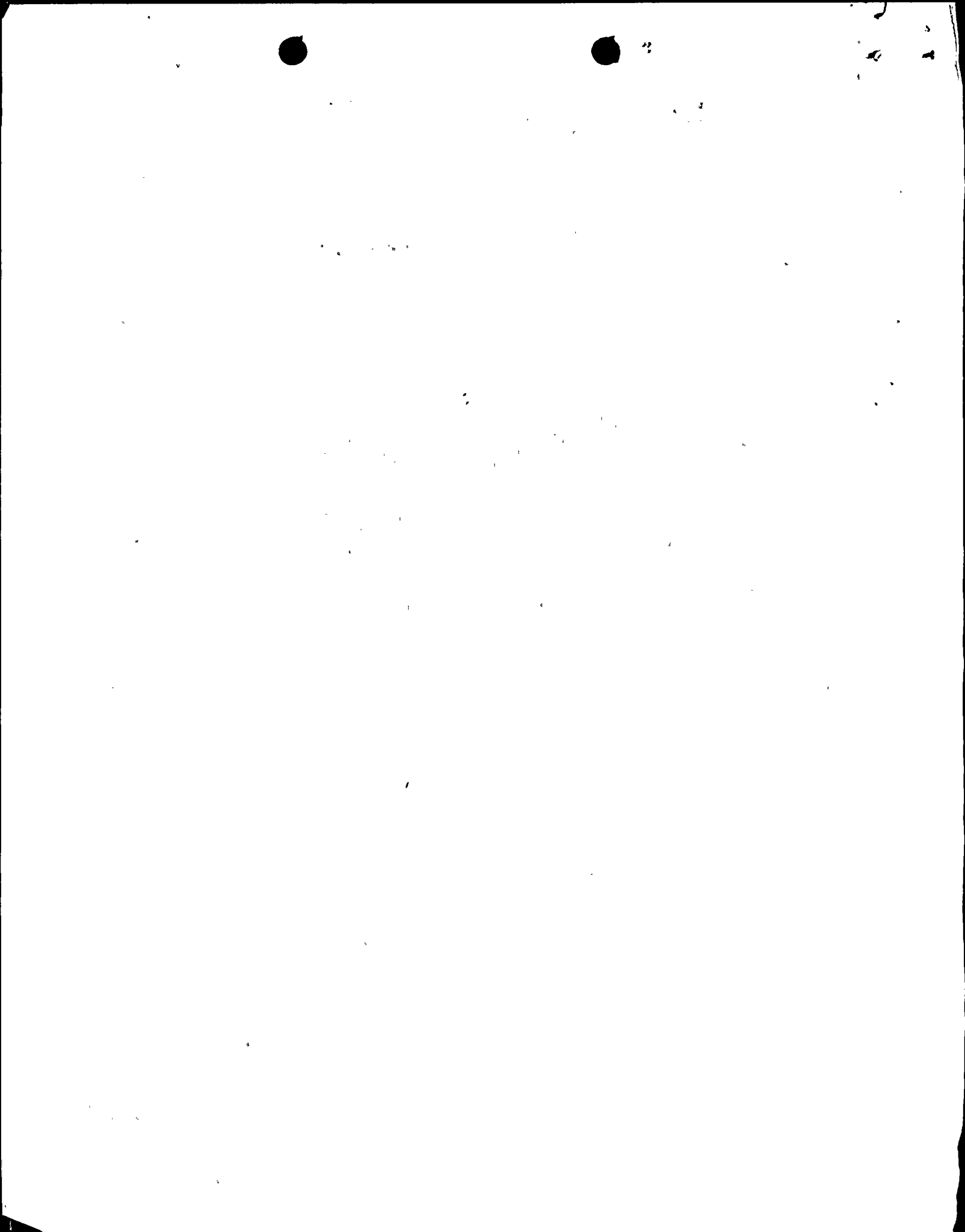
- References:
1. EPRI PWR Safety and Relief Valve Test Program Guide for Application of Valve Test Program Results to Plant-Specific Evaluations, Revision 2, Interim Report, July, 1982.
 2. EPRI PWR Safety and Relief Valve Test Program Safety and Relief Valve Test Report, EPRI NP-2628-SR, Dec., 1982.
 3. M. P. Alexich, Indiana & Michigan Electric Co., letter to H. R. Denton, NRC, "Donald C. Cook Nuclear Plant Units 1 and 2, NUREG-0737, Item II.D.1, PWR Relief and Safety Valve Test Program," AEP:NRC:0585D, December 15, 1983.
 4. M. P. Alexich, Indiana & Michigan Electric Co., letter to H. R. Denton, NRC, "Response to NRC, Request for Additional Information Regarding Testing of the Pressurizer Safety and Relief Valves, Donald C. Cook Nuclear Plant, Units 1 and 2," AEP:NRC:0585H, July 15, 1985.

Dear Mr. Denton:

This letter and its attachments respond to B. J. Youngblood's letter of April 2, 1986, which requested additional information regarding TMI Action Item II.D.1 on relief and safety valve testing. Six questions were to be addressed, but in discussions with your staff, it was agreed that response to Questions 3 and 4d would be postponed until after additional information is provided to us by your staff. This letter and its attachments respond to the remaining questions in Mr. Youngblood's letter, as applicable to the Donald C. Cook Nuclear Plant, Units 1 and 2.

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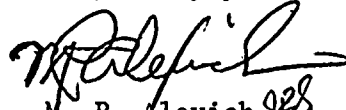


The attachments to this letter contain the following information:

- Attachment 1: Response to the questions in Mr. Youngblood's letter.
- Attachment 2: Teledyne input on Question 4a.
- Attachment 3: Teledyne input on Questions 4b and 4c.
- Attachment 4: Stress analysis results for Question 5c.
- Attachment 5: Westinghouse Report V-EC-108 related to Question 6.

This document has been prepared following Corporate procedures which incorporate a reasonable set of controls to ensure its accuracy and completeness prior to signature by the undersigned.

Very truly yours,


M. P. Alexich *9/28*
Vice President *7/20/86*

cm

Attachments

cc: (w/o attachments)
John E. Dolan
W. G. Smith, Jr. - Bridgman
R. C. Callen
G. Bruchmann
G. Charnoff
NRC Resident Inspector - Bridgman



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ATTACHMENT 1 TO AEP:NRC:0585I
RESPONSE TO NRC REGARDING
REQUEST FOR ADDITIONAL INFORMATION
ON RELIEF AND SAFETY VALVE TESTING

Question 1: Safety Valve Inlet Pressure Drop

"The licensee gave the pressure drop values through the inlet piping as 14.4 psi for the plant specific safety valve and 15.8 psi for applicable EPRI test valve. These pressure drop values appear to be extremely low, when compared with the pressure drop values listed in Table B-3 of Reference 1 for various EPRI valve inlet configurations. Please verify the pressure drop values given previously. Present a recalculation of the total pressure drops through the inlet piping of D. C. Cook Units 1 and 2 safety valves and the applicable EPRI inlet piping arrangement. The total pressure drop should include both the frictional and acoustic [sic] wave components evaluated under steam conditions."

Response 1:

The previous calculation considered only the frictional component of inlet piping pressure drop. The pressure drop was recalculated using the method given in Reference 1, Appendix B. This method includes both frictional and acoustic wave components evaluated during both valve opening and closing. The results of the calculations are shown in the following table. The ΔP values for the EPRI test were taken from Table B-3 of Appendix B in Reference 1.

INLET PIPING PRESSURE DROP (psi)

	Cook Plant			EPRI Test
	Frictional Component	Acoustic Wave Component	Total ΔP	
Valve Opening	12.1	216.1	228.2	263
Valve Closing	5.8	146.8	152.6	181

The above results are based on the transient ΔP which is the controlling ΔP . Steady-state ΔP is the same as the frictional component given in the above table.

It is observed by comparison of the Cook Plant and EPRI test inlet piping pressure drop that the Cook Plant ΔP is lower than the EPRI inlet piping ΔP . Since the Cook Plant pressurizer safety valves (PSVs) do not utilize loop seals, steam discharge conditions noted in Appendix B of Reference 1 are applicable to the Cook Plant. Therefore, the performance of the Cook Plant pressurizer safety valves can be evaluated based on the performance of the EPRI tested valve, Crosby 6M6.



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Question 2: Safety Valve Backpressure

"EPRI Test No. 1411, which was selected as a representative test of the D. C. Cook safety valve, showed that the maximum backpressure developed at the outlet of the test valve was 245 psia. The backpressure for the D. C. Cook safety valve was not given in the submittal. Please provide the predicted value of the maximum backpressure developed at the outlet of the D. C. Cook Units 1 and 2 safety valves in order to verify whether the plant specific pressure drop is bounded by the EPRI test."

Response 2:

Safety valve backpressure was calculated based on the procedure given in Reference 1, Appendix A. The approach assumes simultaneous discharge of all safety valves or all PORVs. Since Cook Plant PSVs do not utilize loop seals, the calculation was done only for steam conditions. Maximum pressurizer relief tank pressure (100 psig) was assumed. The backpressures were calculated using the actual discharge piping geometry and a two-phase homogeneous flow model. The Unit 2 piping geometry was used since it is slightly longer than that in Unit 1.

The homogeneous flow model considers the two phases to flow as a single phase possessing mean fluid properties. It provides more accurate pressure drop estimates for dispersed flow in the higher mass velocity ranges (2000 - 2500 Kg/M²sec). The following assumptions are implicit in the model:

- a) Entropy remains constant as fluid flows along the line.
- b) Steam and water velocities are equal.
- c) Steam and water are in thermodynamic equilibrium.
- d) There is no dissipation of mechanical energy at the steam and water interface.
- e) Suitably defined single-phase friction factor for two-phase flow was used.

The results of the calculations are shown in the following table:

Flow per Safety Valve (lb/hr)	Flow per PORV (lb/hr)	Total Flowrate (lb/hr)	Predicted Safety Valve Backpressure (psia)		
			SV-45A	SV-45B	SV-45C
458,000*	0	1,374,000	438.2	431.9	430.0
0	179,000	537,000	192.6	192.6	192.6

* This value is specified in Table B-1 of Reference 1.

Two EPRI "steam" tests (903 and 1411) were conducted on the Crosby 6M6 valve as shown in Table 3.5.1.b, Reference 2. Test 903 was conducted at high backpressure (665 psia) and Test 1411 at low backpressure (245 psia). Since the Cook valves maximum predicted backpressure (438 psia) is above that of Test 1411, this test is not applicable for demonstrating valve operability. Test 903, while conducted at sufficiently high backpressure, is also not applicable, since the valve ring settings were not representative of the ring settings on the Cook valves.

However, another test (929), which was a "loop seal" test, can be used as a basis for demonstrating satisfactory valve performance on steam at high backpressure. Test 929 was conducted on a valve with ring settings representative of the Cook valves and at high backpressure (710 psia). Although the valve chattered during this test as the water in the loop seal was expelled, the valve "stabilized on steam," (Note (4), Table 3.5.1.c in Reference 2). Therefore, it is concluded that the Crosby 6M6 valve operability on steam at high backpressure (710 psia) was demonstrated by Test 929. Since the Cook Plant PSV predicted maximum backpressure (438 psia) is enveloped by EPRI Test 929, Cook Plant PSV valve operability was demonstrated.

Question 3: (Awaiting further NRC clarification)

Question 4: Safety Valve and PORV Piping Stress Analysis

- a. "Reference 4 indicates that details of the piping stress analysis for PORV discharge cases are contained in the Teledyne Reports TR-5364-1 and TR-5364-2. Our record shows that the above reports have not been submitted for review by the licensee. Please provide copies of the above reports so that the piping analysis pertinent to PORV discharge can be reviewed.
- b. In the thermal hydraulic analysis of the piping discharge conditions, the computer codes REPIPE/SAP2SAP were used to calculate the fluid force time histories from RELAP5 analysis results. Provide verification of the REPIPE/SAP2SAP codes by showing that these codes produce accurate results for similar problems.
- c. The licensee presented a verification of the structural analysis code, TMRSAP, using assumed force time histories in the form of ramp functions to represent the fluid forces exerted on the piping model (Question 16, Reference 4). In order to demonstrate that the computer code produces accurate results for the valve discharge problem analyzed, similar piping model and fluid forces must be used. The ramp shape force histories used in the verification problem does not realistically represent the type of fluid forces in a safety valve/PORV discharge event. Therefore, present a verification of the TMRSAP code using fluid forces representative of the valve discharge conditions."

Response 4a:

Included as Attachment 2 to this submittal are the Teledyne Reports requested by Question 4a.

Response 4b and 4c:

Included as Attachment 3 to this submittal is the response from Teledyne Engineering Services regarding the REPIPE/SAP2SAP codes and the TMRSAP code discussed in Questions 4b and 4c.

Question 4d: (Awaiting further NRC clarification)

Question 5: Piping Support Stresses

"The Teledyne stress report indicates that a number of pipe supports (8 in Unit 1 and 24 in Unit 2) exceeded their design loads. Subsequent reanalysis performed by the licensee concluded that, with the exception of a few supports which required modifications, the rest of the supports were found to be adequate to resist the revised loads. Since the licensee did not provide any detail concerning the reanalysis, a review of the support adequacy cannot be performed. Therefore provide the following information required for the evaluation.

- a. Identify the governing code and standards used for support design.
- b. List the load combination equations used including all the operation conditions as suggested in the EPRI Guide for Plant Specific Evaluations (Reference 2). Also specify the allowable stress limit applicable to each condition.
- c. Provide a comparison of the worst case support stresses (or loads) with the applicable allowable stress limits (or allowable loads) and identify the load combinations associated with the worst stresses. These data should be presented for the questionable supports indicated in the Teledyne stress report."

Response 5a:

The governing codes and standards used for support design are as follows:

1. American Institute for Steel Construction (AISC) Code for auxiliary steel
2. Manufacturers Standardization Society (M.S.S.)-SP-58 for commercial pipe hanger attachments
3. Power Piping USAS B.31.1-1967 - for pipe integral attachments

Response 5b:

The load combination equations for normal and upset conditions are:

$$D_1 = \begin{array}{l} \text{Normal} \\ \text{(Weight Load)} \end{array} + \begin{array}{l} \text{Normal} \\ \text{(Thermal Range Load)} \end{array} \pm \text{OBE Load}$$

$$D_2 = \begin{array}{l} \text{PORV Transient} \\ \text{(Weight Load)} \end{array} + \begin{array}{l} \text{PORV Transient} \\ \text{(Thermal Range Load)} \end{array} \pm \sqrt{\begin{array}{l} (\text{OBE})^2 \\ \text{Load} \end{array} + \begin{array}{l} (\text{PORV Trans.})^2 \\ \text{Shock Load} \end{array}}$$

The load summation shall not provide support component stress greater than 100% of that permitted by 5a.

The load combination equations for emergency conditions are:

$$E_1 = \begin{array}{l} \text{Normal} \\ \text{(Weight Load)} \end{array} + \begin{array}{l} \text{Normal} \\ \text{(Thermal Range Load)} \end{array} \pm \text{DBE Load}$$

$$E_2 = \begin{array}{l} \text{SV Transient} \\ \text{(Weight Load)} \end{array} + \begin{array}{l} \text{SV Transient} \\ \text{(Thermal Range Load)} \end{array} \pm \begin{array}{l} \text{SV Transient} \\ \text{(Shock Load)} \end{array}$$

The load summation shall not produce support component stress greater than 133% of that permitted by 5a.

Additionally, 90% of yield stress shall not be exceeded.

Response 5c:

A tabulated summary for comparing the worst-case support stresses with the applicable stress limits for the supports identified in the Teledyne Stress Report is provided in Attachment 4. For three items noted in Attachment 4, stress comparisons will be made after as-built information is obtained from the plant.

Question 6: Valve Accelerations

"The licensee stated in Reference 3 that the Teledyne analysis showed that the maximum vertical acceleration of the D. C. Cook safety valve resulting from a piping discharge transient exceeded the design allowable of 2 g by less than 1 g. The licensee contended that these valves were successfully tested in the Westinghouse seismic test to 4 g in the vertical direction. Therefore, the predicted acceleration for the D. C. Cook valves, although exceeding the design allowable, would still be acceptable. However, the licensee did not provide any details of the test and its findings. Since NUREG-0737, Item II.D.I requires that the valve operability must be demonstrated for operating and transient conditions, the operability of the valves under the predicted g loadings must be assured. Therefore, provide a discussion of the seismic test performed by Westinghouse to demonstrate that the operability of the safety valve will not be impaired under the predicted acceleration level."

Response 6:

In the December 15, 1983, submittal, Reference 3, it was stated that "we were informed by Westinghouse... that the valves have been successfully seismically test for 4 g - vertical and 6 g - horizontal accelerations." That statement was based on a September 1, 1983, letter from Westinghouse, which stated: "The specified seismic accelerations under which the valve successfully completed seismic testing were 4 g - vertical and 6 g - horizontal."

In response to Question 6, Westinghouse informed us that upon further investigation, they learned from Crosby that the valve seismically tested was a forged valve design and not the cast version. Since Westinghouse supplied Cook Plant with cast valves, the seismic tests referred to above may not be directly applicable to the Cook PSVs.

However, a seismic analysis was performed for the cast version of the valve based on 4 g - vertical and 6 g - horizontal seismic accelerations. The analysis and results are contained in Crosby Valve and Gage Company Report No. EC-310, dated March, 1977, which is a proprietary report. Westinghouse did prepare and submit to us a summary of the report, V-EC-108, attached for reference (Attachment 5). The results of the seismic analysis showed a maximum stress in the valve body of 5058 psi (allowable = 18,700 psi) and a maximum stress in the valve bonnet of 5720 psi (allowable = 17,400 psi). The evaluation showed that the "valve remains structurally sound and maintains full operational capabilities" for the 4 g - vertical and 6 g - horizontal seismic conditions. Since the predicted maximum vertical acceleration of the Cook PSVs in the Teledyne analysis was less than 3 g, and the Crosby seismic analysis concludes that the valve maintains full operational capability under 4 g - vertical acceleration, it is concluded that the operability of the Cook PSV will not be impaired by the predicted acceleration level. It should be noted that the predicted maximum horizontal acceleration of the Cook PSVs in the Teledyne analysis was within the design allowable of 3 g, and hence within the tested value of 6 g, and is therefore acceptable.

ATTACHMENT 2

TO

AEP:NRC:0585I

TELEDYNE INPUT (QUESTION 4a)

ATTACHMENT 3

TO

AEP:NRC:0585I

TELEDYNE INPUT (QUESTIONS 4b AND 4c)

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ENGINEERING SERVICES**

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WALTHAM, MASSACHUSETTS 02254-9195

(617) 890-3350 TWX (710) 324-7508

July 9, 1986
5364-73

American Electric Power Service Corp.
1 Riverside Plaza
Columbus, OH, 43216-6631

Attention: Mr. Osman Yasin

Subject: REPIPE Verification

Dear Gentlemen,

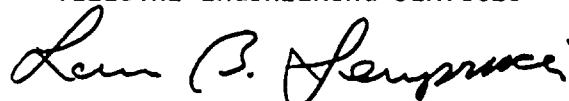
The REPIPE computer program is a Control Data Corporation (CDC) proprietary program. It is made available to the public on a fee basis. CDC is a Teledyne Engineering Services (TES) Approved Vendor. This means that TES quality assurance engineers have audited the CDC quality assurance program and have found it to meet our standards.

TES used the REPIPE version 3.10 computer program in the execution of Technical Reports TR-5364-1, 2, 3 and 4.

This program was used with the understanding that CDC had tested the program under their QA procedures. CDC QA records have been reviewed in the safety-related library for REPIPE version 3.10 as installed on KHE in April, 1983. Quality assurance testing was performed per the CDC SRQA program at that time. Test results are on file as lifetime records.

Very truly yours,

TELEDYNE ENGINEERING SERVICES



Lenin B. Semprucci
Principal Engineer

LBS:mld

cc: D. Messinger (TES)
R. Berks (TES)

 **TELEDYNE
ENGINEERING SERVICES**

130 SECOND AVENUE

WALTHAM, MASSACHUSETTS 02254-9195

(617) 890-3350 TWX (710) 324-7508

June 5, 1986
5364-17

American Electric Power Service Corp.
1 Riverside Plaza
Columbus, OH, 43216-6631

Attn: Mr. J. L. Williams
Section Manager

Subject: D. C. Cook Nuclear Plant
NRC Questions Related to TMI Action Item II.D.1 on Relief and
Safety Valve Testing, File No. DC-D-0353.36M

Ref: AEPSC letter dated 5/29/86 from Osman Yasin to L. B. Semprucci

Dear Sirs,

Enclosed you will find our response to NRC Questions 4b and 4c. Copies of Technical Reports TR-5364-1 and TR-5364-2 books 1, 2 and 3 are also enclosed as requested in Question 4a.

If there are any questions please call me at (617) 890-3350.

Very truly yours,

TELEDYNE ENGINEERING SERVICES


Lenin B. Semprucci
Principal Engineer

LBS:mld

cc: J.A. DiBello (AEPSC)
M.J. Noronha (AEPSC)
O. Yasin (AEPSC)
R. Wray (TES)
R.H. Berks (TES)
D.F. Landers (TES)

5364
June 5, 1986
Page 1

In response to question 4b which states:

In the thermal hydraulic analysis of the piping discharge conditions, the computer codes REPIPE/SAP2SAP were used to calculate the fluid force time histories from RELAP5 analysis results. Provide verification of the REPIPE/SAP2SAP codes by showing that these codes produce accurate results for similar problems.

The REPIPE computer code is maintained and serviced by Control Data Corporation. Verification of REPIPE's capacity to develop a force time history from RELAP5 mod 1 is provided by Control Data Corporation.

SAP2SAP is a TES generated program which reformats SAP force time history files. SAP2SAP was used on the D.C. Cook force time history files generated by REPIPE for the following reasons.

The REPIPE program generates force time histories from RELAP output in SAP format. For each straight pipe segment in which a force time history occurs REPIPE assigns the positive force to the structural node at one end of the pipe segment and the negative force to the structural node at the other end. This requires two structural nodes associated with two force time history tables for every straight pipe segment. The D.C. Cook structural model was so big that the number of structural nodes with force time histories exceeded the capacity of the program. Therefore the SAP2SAP program was used to reduce the number of structural nodes being loaded by adding the force time histories of the nodes at each end of a pipe segment and replace the two force time histories with a single force time history applied to one structural node on the pipe segment.

The SAP2SAP program is simply an "arithmetic" program providing the user with several options. The program is independent of the valve discharge problem.

5364
June 7, 1986
Page 2

NRC question 4C states:

The licensee presented a verification of the structural analysis code, TMRSAP, using assumed force time histories in the form of ramp functions to represent the fluid forces exerted on the piping model (Question 16, Reference 1). In order to demonstrate that the computer code produces accurate results for the valve discharge problem analyzed, similar piping model and fluid forces must be used. The ramp shape force time histories used in the verification problem does not realistically represent the type of fluid forces found in a safety valve PORV discharge event. Therefore, present a verification of the TMRSAP code using fluid forces representative of the valve discharge conditions.

In response to question 4C, TES provides the following:

The verification problem used by TES realistically represents the fluid forces found in a safety valve/PORV discharge event. This is evident by a comparison of the TES verification fluid loads with those used in the EPRI/CE Test Program (Ref. 2) shown in the following figures.

Figures 4-8, 4-10 and 4-12, from Ref. 2, illustrate the fluid loads (shown as solid lines) and the structural response (shown in dashed lines) corresponding to test #1411 of the EPRI/CE safety valve tests performed in response to NUREG 0737. We call your attention to the fluid loads (the structural response is not in question). It can be seen that these fluid loads are a ramp up to a peak value followed by a ramp down to the no load position.

Figures 3, 4, 5 and 6 present the fluid forces used in the TES verification problem. It can be seen that TES's verification fluid forces ramp up to a peak value and then ramp down to the no load position as do those in the EPRI/CE program. The TES verification problem geometry is not identical to the EPRI/CE test geometry (see figures 1 and 2), therefore one would not expect the magnitude and duration of the forces to be identical. The point is that the forces are similar in general configuration and therefore representative of the valve discharge problem.

The NRC reviewer's concern may be due to a misunderstanding of the TES forcing function.

The TES fluid forcing function as presented in the verification problem is a total elbow load. The forcing function presented in the EPRI/CE problem are net segment loads (known as unbalanced forces, or wave forces). The net segment load is the difference in the elbow loads at either end of the pipe segment. In order to compare the TES forcing function with the EPRI/CE forcing function, one must take the difference in the total elbow loads bounding each segment. This has been done in figures 3, 4, 5 and 6. Now it can be seen that the TES forcing function is indeed representative of the EPRI/CE forcing function.

S364
June 5, 1986
Page 3

It must be further pointed out that the method by which TMRSAP (or any dynamic program) solves a force time history problem is independent of the form of the forcing function. The analyst inputs the forcing function as a table of load versus time. Whether the function is a ramp, series of ramps or any arbitrary function doesn't matter to the program. The same equations are being solved with each time step. What is important is that the analyst chose the time steps properly.

As additional information on January 7-11, 1985, NRC personnel conducted an inspection at our facility in Waltham, Massachusetts (NRC Inspection Report and Docket No. 99900513/85-01 dated July 11, 1985). The purpose of this inspection was to review our Quality Assurance Program in the areas of computer code verification, computer code error handling procedures, and pipe support design calculations.

Regarding computer program verification, the following is an excerpt from the Report:

"The development and verification of the computer program TMRSAP, which is used by TES in the design of safety-related items was reviewed during this inspection. Technical Engineering Procedures TEP-1-005, Application Computer Program Development, was reviewed and utilized throughout the inspection of TMRSAP.

The computer code TMRSAP, which was developed internally by TES, is used for static and dynamic analysis of linear piping systems. It employs a finite element solution technique with a library consisting of curved and straight pipe elements, and a boundary element for simulation of pipe restraints. TMRSAP provides capability for analysis of such static loading as deadweight, thermal, and pressure elongation loadings. Capabilities for dynamic analysis include response spectrum and time history (both modal and direct) analysis. Solution methods include Gaussian elimination for static solutions, and determinant search for subspace iteration for the modal dynamic solutions. Direct integration is performed with the Wilson- θ -method.

TES verified TMRSAP by a comparison of the output of 22 verification problem solutions with either the results of hand calculations or the output of other computer codes (STARDYNE, EPIPE, ANSYS, and ADLPIPE). During this inspection all verification problems were reviewed. Although the verification of this code was done according to a general design control procedure (Section 3.0 of the TES Quality Assurance Manual), it was found to meet the requirements of the latest TES procedure controlling computer code verification (TES-1-005), with one exception. The exception was that the source code listing and computation outputs were not included in the verification

5364
June 5, 1986
Page 4

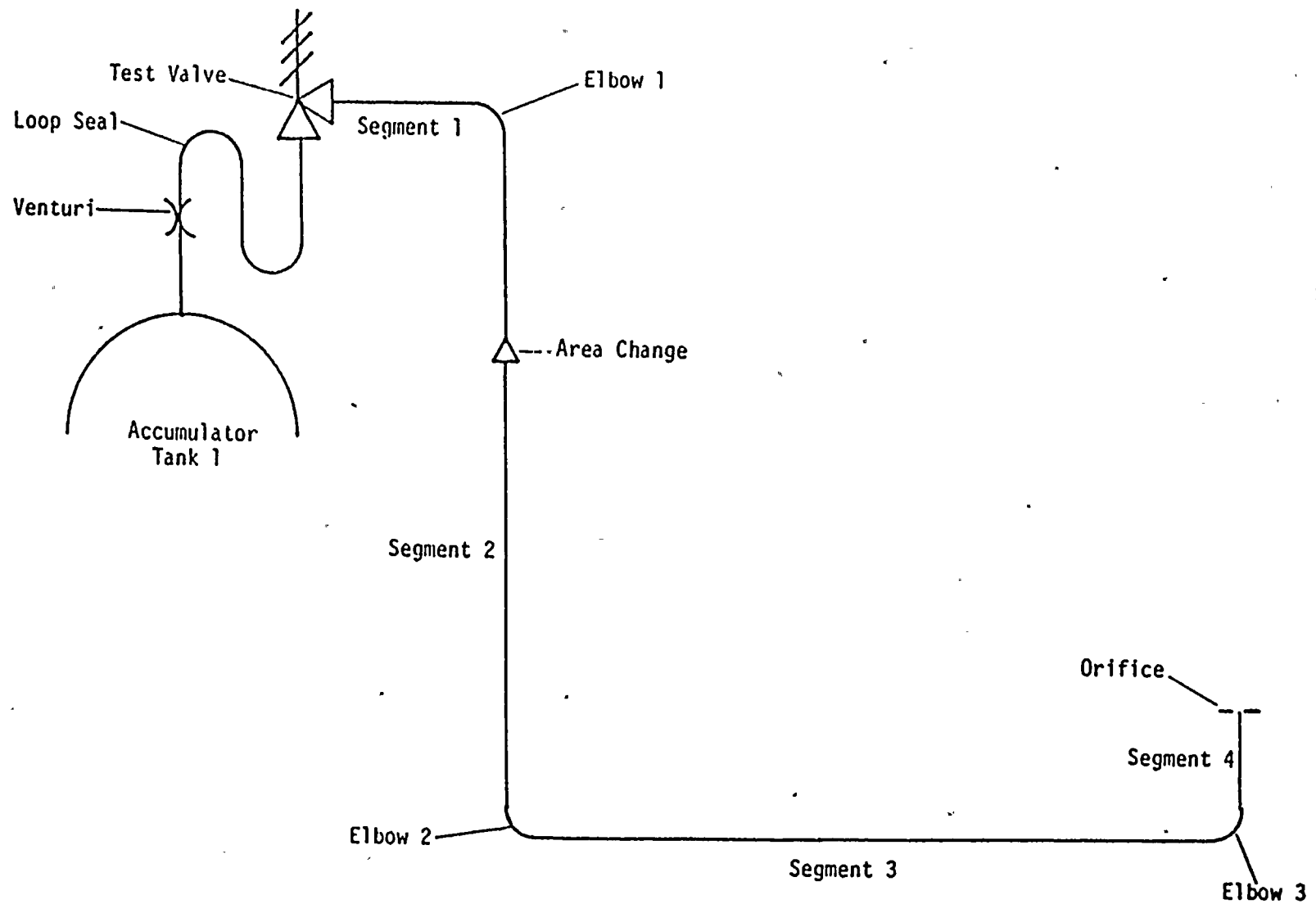
 **TELEDYNE**
ENGINEERING SERVICES

manual. However, the computation output includes a source code listing that was clearly identified in the verification manual and was readily available at the TES office. No violations or nonconformances were identified during this part of the inspection."

BY LBS DATE 6-5-86
CHKD. BY NA DATE NA

RESPONSE TO NEC QUESTIONS

SHEET NO. _____ OF _____
PROJ. NO. 5164



EPRI/CE SAFETY VALVE TEST GEOMETRY
FIG 1

TELEDYNE ENGINEERING SERVICES

BY LBS DATE 6-5-86

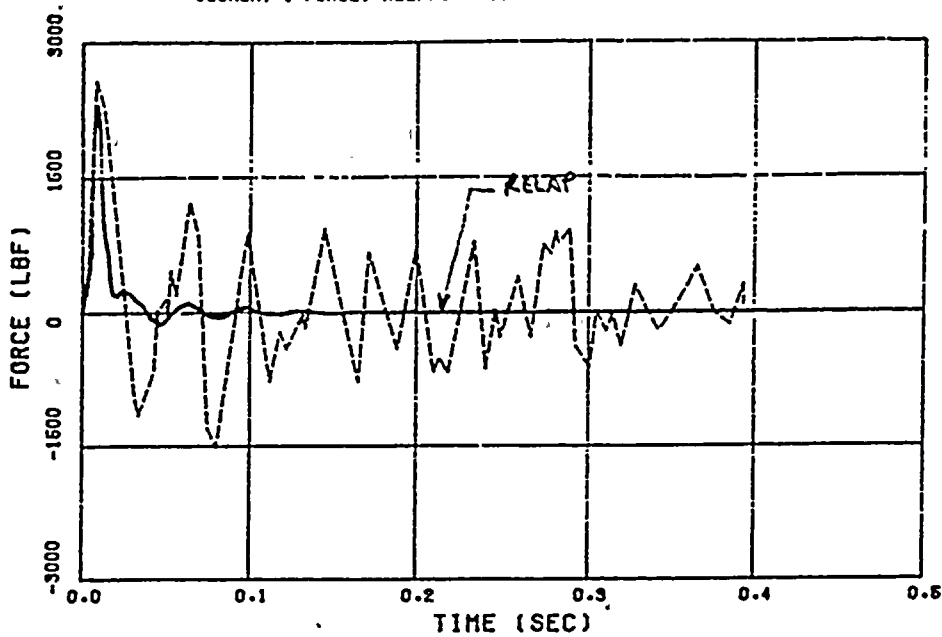
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RESPONSE TO NRC QUESTIONS

SHEET NO. _____ OF _____

PROJ. NO. 5364

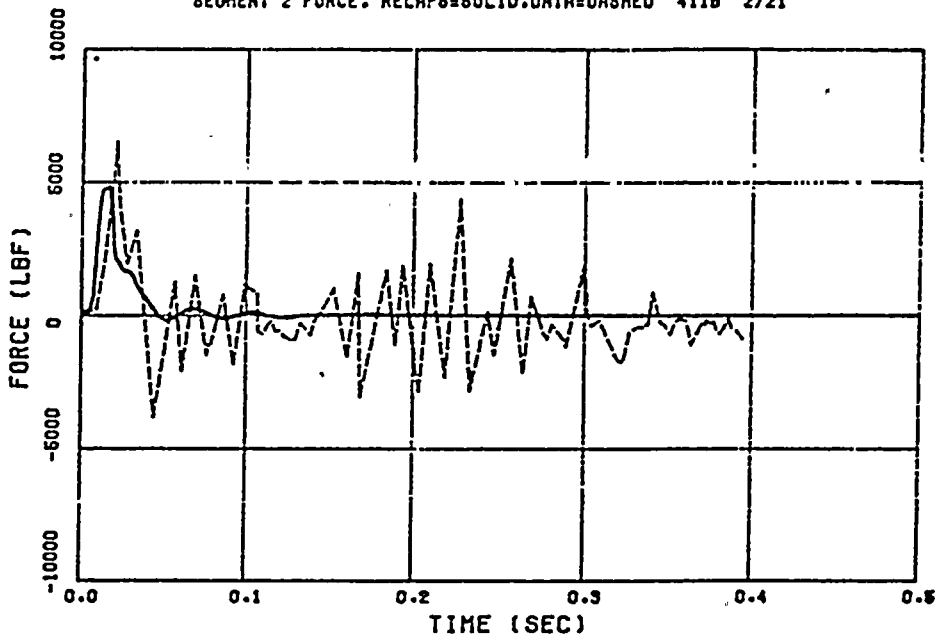
CE TEST NO. 1411
SEGMENT 1 FORCE. RELAP5=SOLID, DATA=DASHED 411B 2/21



(REF 2)

Figure 4-8. Comparison Plot of RELAP5/MOD1-Calculated Segment 1 Force with Experimental Data, Test 1411.

CE TEST NO. 1411
SEGMENT 2 FORCE. RELAP5=SOLID, DATA=DASHED 411B 2/21



(REF 2)

Figure 4-10. Comparison Plot of RELAP5/MOD1-Calculated Segment 2 Force with Experimental Data, Test 1411.

TELEDYNE ENGINEERING SERVICES

BY LBS DATE 6-5-86

CHKD. BY _____ DATE _____

RESPONSE TO NRC QUESTIONS

SHEET NO. _____ OF _____

PROJ. NO. 5364

CE TEST NO. 1411

SEGMENT 3 FORCE. RELAPS=SOLID. DATA=DASHED 4118 2/21

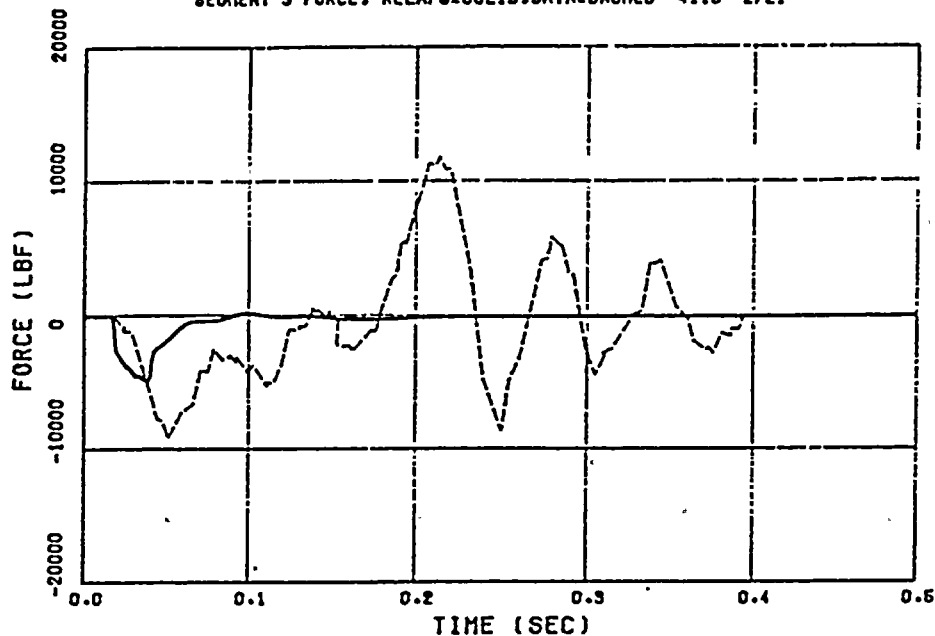


Figure 4-12. Comparison Plot of RELAP5/MOD1-Calculated Segment 3 Force with Experimental Data, Test 1411.

:(REF 2)

TELEDYNE ENGINEERING SERVICES

BY LRS DATE 6-5-86
CHKD. BY _____ DATE _____

RESPONSE TO NRC QUESTIONS

SHEET NO. _____ OF _____
PROJ. NO. 5634

TES VERIFICATION MODEL

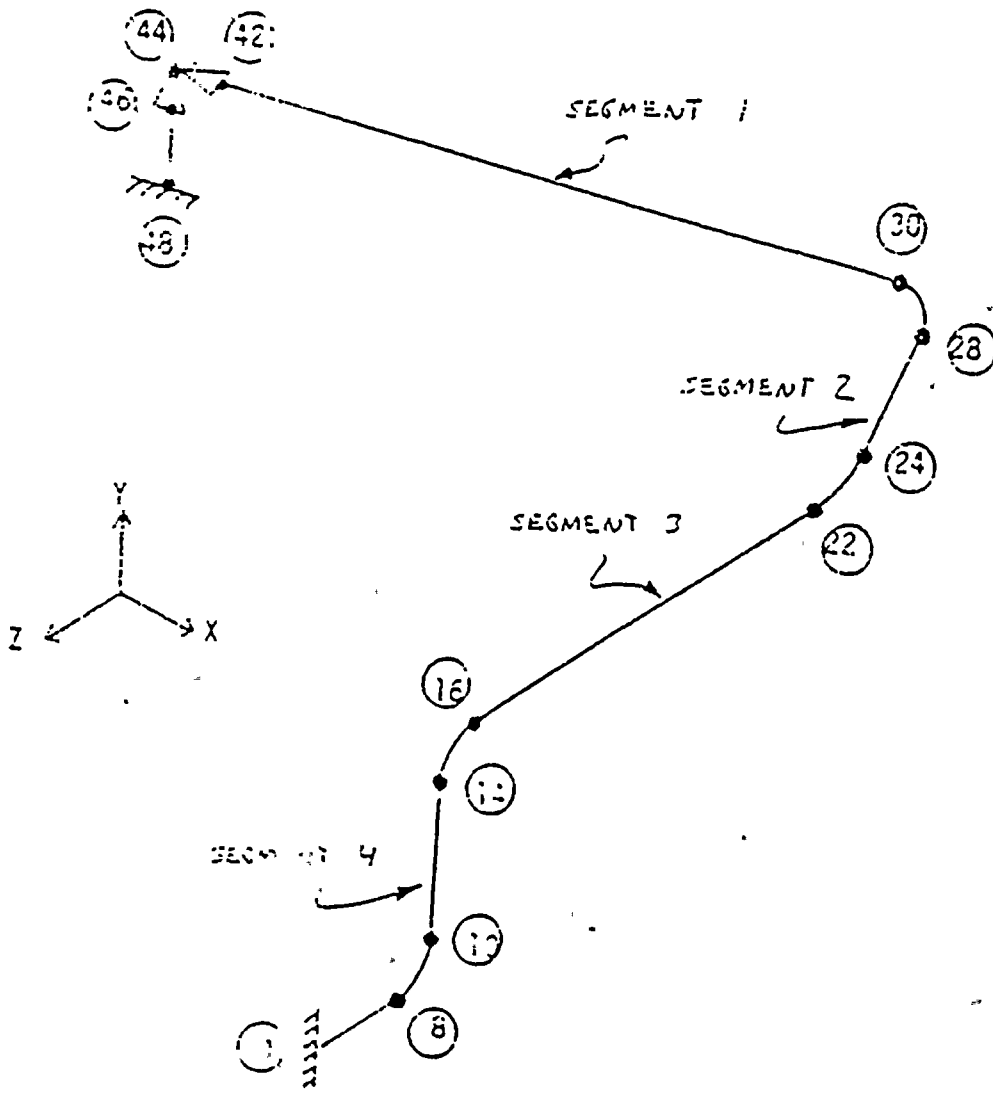


FIG 2.0

TELETYPE ENGINEERING SERVICES

BY LBS DATE 6-3-86
CHKD. BY _____ DATE _____

RESPONSE TO NRC QUESTIONS

SHEET NO. _____ OF _____
PROJ. NO. 5164

NET SEGMENT LOAD

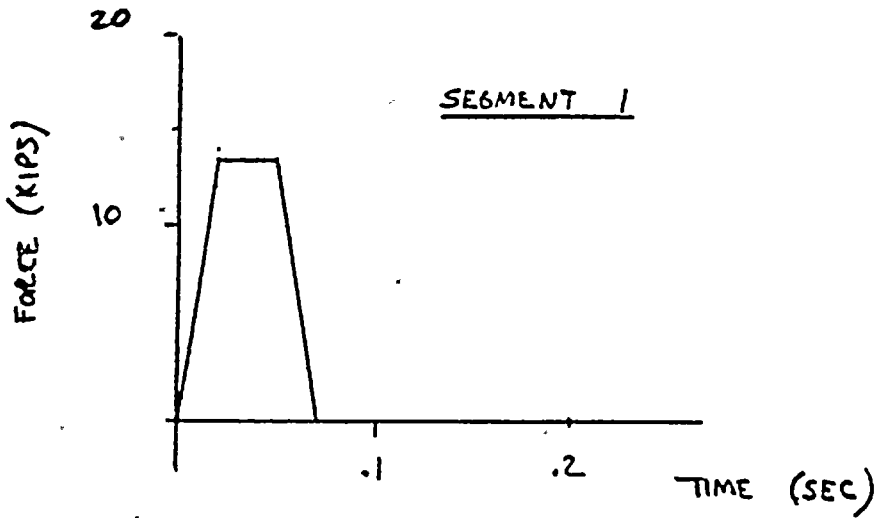


FIG 3.0

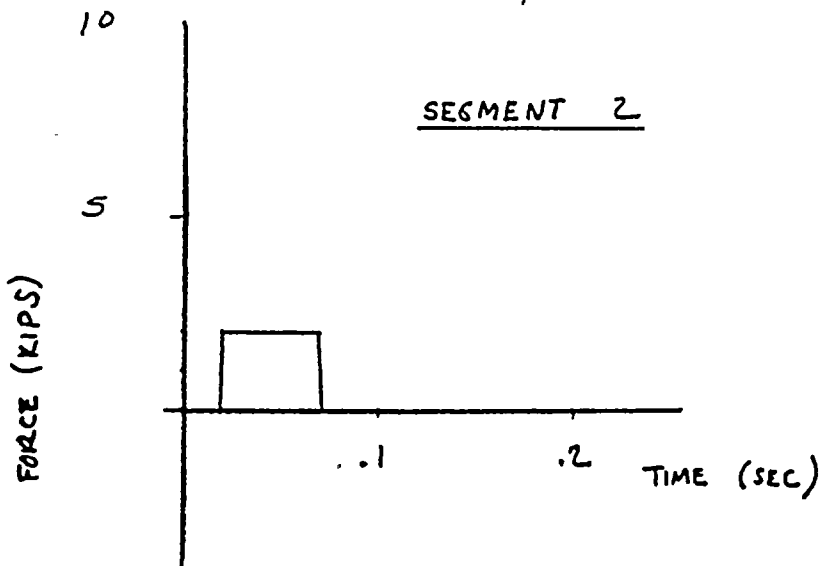


FIG. 4.0

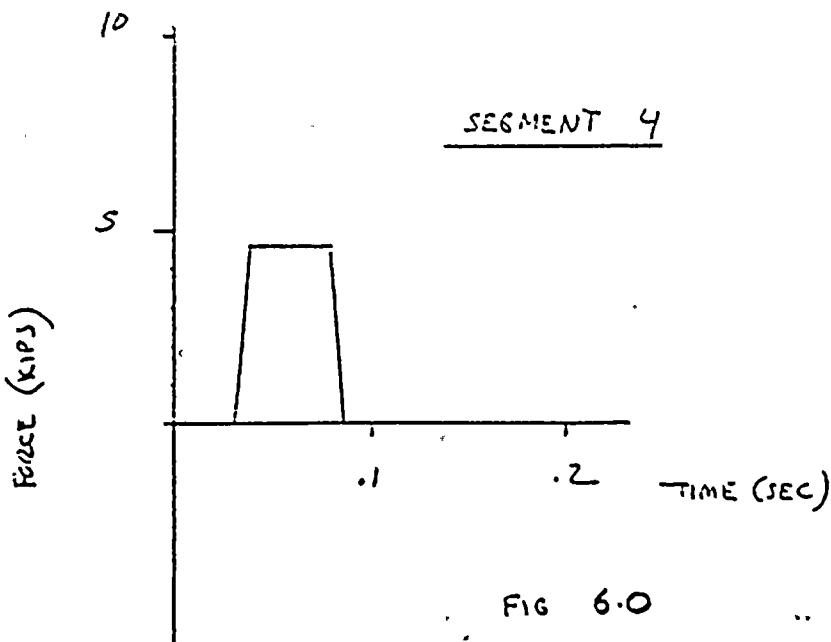
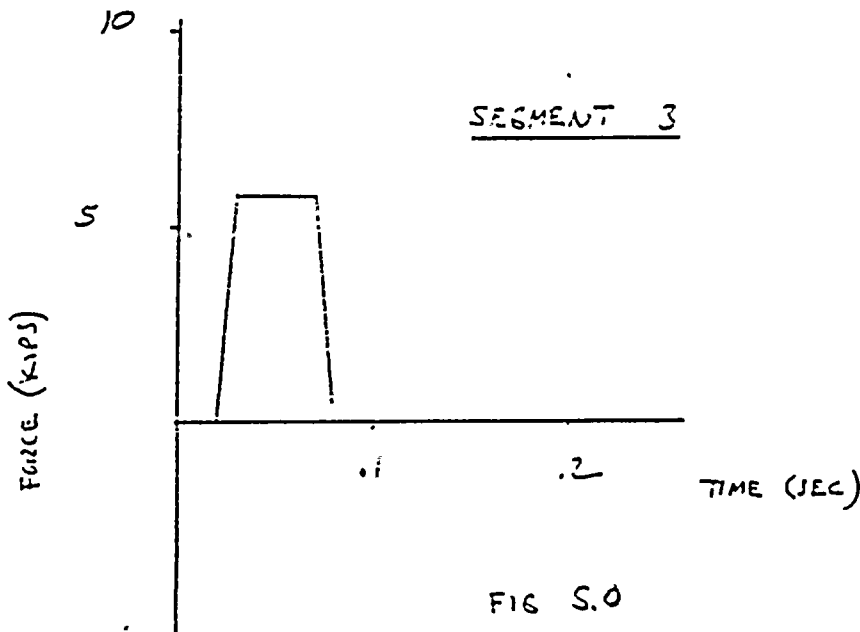
TELEDYNE ENGINEERING SERVICES

BY LRS DATE 6-5-86
CHKD. BY _____ DATE _____

RESPONSE TO NRC QUESTIONS

SHEET NO. _____ OF _____
PROJ. NO: ST64

NET SEGMENT LOAD



5364
June 5, 1986
Page 11

REFERENCES

1. M.P. Alexich, Indiana & Michigan Electric Co., letter to M.R. Denton, NRC, "Response to NRC Request for Additional Information Regarding Testing of the Pressurizer Safety and Relief Valves, Donald C. Cook Nuclear Plant, Units 1 and 2," AEP:NRC:0585H, July 15, 1985.
2. Application of RELAP5/MOD1 for calculation of Safety and Relief Valve Discharge Piping Hydrodynamic Loads, EPRI NP-2479, Project V102-28, Final Report, December 1982.

ATTACHMENT 4

TO

AEP:NRC:0585I

PIPING SUPPORT STRESS ANALYSIS

RESPONSE TO NRC QUESTION 5c
PORV/SV DISCHARGE ANALYSIS

UNIT NO. 1

Hanger Mark Number	Catalog Items <u>Actual Load</u> Allow Load	Structural Steel Members <u>Actual Stress/Allow Stress</u>				Remarks
		Axial +Bending	Shear	Weld	Expansion Bolts	
1-GRC-R585	0.94	NA	NA	0.32	1.43*	Before Modification
	0.94	.98	0.18	0.32	0.45	After Modification
1-GRC-R589	NA	0.57	0.32	0.74	0.68*	No Modification
1-GRC-R591	0.72	0.60	0.33	0.40	NA	No Modification
1-GRC-R601	0.72	0.22	0.14	0.18	NA	No Modification
1-GRC-R608	0.42	NA	NA	0.22	NA	No Modification
1-GRC-R613	NA	0.27	0.08	0.39	NA	No Modification
1-GRC-S614	0.73	NA	NA	0.26	NA	No Modification
1-GRC-R616	NA	1.09	0.41	1.67	NA	Before Modification
	NA	0.98	0.41	0.76	NA	After Modification

* Based on "Teledyne Engineering Services" allowable expansion anchor loads.

RESPONSE TO NRC QUESTION 5c
PORV/SV DISCHARGE ANALYSIS

UNIT NO. 2

Hanger Mark Number	Catalog Items <u>Actual Load</u> <u>Allow Load</u>	Structural Steel Members <u>Actual Stress/Allow Stress</u>				Expansion Bolts	Remarks
		Axial +Bending	Shear	Weld			
2-GRC-R585	NA	0.72	0.71	0.12	4.58*	Before Modification	
	NA	0.72	0.71	0.08	0.99	After Modification	
2-GRC-R586	SEE NOTE					Before Modification	
	0.56	0.39	0.37	0.48	NA	After Modification	
2-GRC-R587	3.12	1.07	0.56	0.96	NA	Before Modification	
	0.53	0.44	0.40	0.19	NA	After Modification	
2-GRC-R591	0.98	0.42	0.31	0.36	NA	Before Modification	
	0.35	0.83	0.25	0.36	NA	After Modification	
2-GRC-R600	1.07	0.87	0.06	0.72	NA	Before Modification	
	NA	0.65	0.10	0.39	NA	After Modification	

Note: Hanger 2-GRC-R586 was analyzed by Structural Design because it had to be relocated due to a field interference. Therefore, no calculations were performed for the "Before Modification" condition.

RESPONSE TO NRC QUESTION 5c
PORV/SV DISCHARGE ANALYSIS

UNIT NO. 2

Hanger Mark Number	Catalog Items <u>Actual Load</u> Allow Load	Structural Steel Members <u>Actual Stress/Allow Stress</u>				Remarks
		Axial +Bending	Shear	Weld	Expansion Bolts	
2-GRC-R601	3.83	0.95	0.85	0.81	NA	Before Modification
	0.79	0.95	0.85	0.83	NA	After Modification
2-GRC-R624	5.66	NA	NA	1.11	NA	Before Modification
	0.62	NA	NA	0.57	NA	After Modification
2-GRC-S629	0.58	0.37	0.35	0.35	NA	No Modification
2-GRC-S631	0.93	NA	NA	0.11	0.91*	No Modification
2-GRC-S632	0.57	0.90	NA	0.19	1.85*	Before Modification
	0.57	0.95	NA	0.10	0.98	After Modification

* Based on "Teledyne Engineering Services" allowable loads on expansion anchors.

RESPONSE TO NRC QUESTION 5c
PORV/SV DISCHARGE ANALYSIS

UNIT NO. 2

Hanger Mark Number	Catalog Items <u>Actual Load</u> Allowable Load	Structural Steel Members <u>Actual Stress/Allowable Stress</u>				Remarks
		Axial +Bending	Shear	Weld	Expansion Bolts	
2-GRC-S-594	0.33	0.37	0.23	0.45	NA	No Modification
2-GRC-S-596	0.35	0.074	0.11	*	0.58	No Modification
2-GRC-S-598	0.54	NA	NA	0.05	NA	No Modification
2-GRC-S-599	0.657	NA	NA	0.27	NA	No Modification
2-GRC-R-605	NA	0.156	NA	NA	NA	No Modification
2-GRC-R-607	NA	0.38	0.11	0.13	NA	No Modification
2-GRC-R-609	0.29	0.11	0.045	0.13	NA	No Modification

* Comparison of actual stress and allowable stress will be made after as-built information from the plant is obtained.

RESPONSE TO NRC QUESTION 5c
PORV/SV DISCHARGE ANALYSIS

UNIT NO. 2

Hanger Mark Number	Catalog Items <u>Actual Load</u> <u>Allowable Load</u>	Structural Steel Members <u>Actual Stress/Allowable Stress</u>				Remarks
		Axial	Shear	Weld	Expansion	
		+Bending			Bolts	
2-GRC-R589	NA	.38	.18	.56	.45	No Modification
2-GRC-S611	.41	NA	NA	.11	NA	No Modification
2-GRC-R612	NA	.243	.357	.32	*	No Modification
2-GRC-R614	NA	.44	.3	*	NA	No Modification
2-GRC-S626	.48	.07	NA	.12	NA	No Modification
2-GRC-S630	.64	.04	NA	.07	NA	No Modification
2-GRC-R633	NA	.73	.26	.24	.94	No Modification

* Comparison of actual stress and allowable stress will be made after as-built information from the plant is obtained.

ATTACHMENT 5

TO

AEP:NRC:0585I

WESTINGHOUSE REPORT V-EC-108 (QUESTION 6)



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JUN 9 1986

Westinghouse
Electric Corporation

Power Systems

Energy Systems
Service Division

P. & V

Box 355
Pittsburgh Pennsylvania 15230-0355

AEP-86-592

June 5, 1986

Mr. J. D. Hoffman
Piping & Valves Section
American Electric Power Service Corporation
One Riverside Plaza
Columbus, Ohio 43216

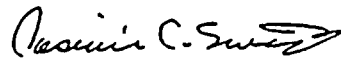
American Electric Power Service Corporation
D. C. Cook Units 1 and 2
Summary of Pressurizer Safety Valve Seismic Evaluation

Dear Mr. Hoffman:

Enclosed please find a copy of the subject seismic evaluation as per your request. This summary was previously telecopied to you to give you an advance copy.

This mailing completes your request. Please call me if I can be of further service.

Very truly yours,


H. C. Walls, Manager
Mid-America Area
Projects Department

CAS/lee

7138f

cc: M. Marrocco

Calculation: V-EC-108 Rev. 0
File: 70502/220/5

SUMMARY OF SEISMIC EVALUATION
- PRESSURIZER SAFETY VALVE -
6RV58MSB
DONALD C. COOK UNITS 1 AND 2

- Reference: 1. Westinghouse Equipment Specification No.
676279 Rev. 2, Spec. Sheet 1
2. Crosby Report No. EC-310 Rev. 0
(File: 70502/220/5)

Summary Prepared By: E. M. Petrosky Date 5/8/86
E. M. Petrosky

Summary Reviewed By: T. J. Matty Date 5/8/86
T. J. Matty

Westinghouse Electric Corporation
Power Systems Division
P.O. Box 355
Pittsburgh, PA 15230

1.0 INTRODUCTION AND EQUIPMENT DESCRIPTION

The object of the evaluation was to demonstrate the structural integrity and operability of the 6RV58MSB under loading due to 6g horizontal and 4g vertical seismic accelerations.

Both the valve body and bonnet were analyzed as pressurized thick-walled cylinders.

The 6RV58MSB is a 6 inch safety valve per Crosby Drawing H-51688. The valve has design conditions of 2500 psia at 650°F and is designed per ANSI-B-16.5. Its location numbers are 8010 A, B, and C.

2.0 METHODS OF QUALIFICATION

The valve body and bonnet of the 6RV58MSB were modeled as thick walled pressurized cylinders. Forces due to the seismic accelerations were applied to the center of gravity of the valve. Using conventional analyses, stresses were determined for the minimum cross section areas.

Although the 6RV58MSB was designed and built to ANSI-B-16.5, the stress criteria of the ASME Boiler and Pressure Vessel Code, Section III, were used as the basis for establishing allowable stress levels. Allowable stresses were set at or below yield to preclude any permanent deformations to the valve while simultaneously subjected to seismic and normal operating loads.

The valve body and bonnet were modeled as thick walled pressurized cylinders subjected to pressure, seismic and operational loading. Stresses were calculated using classical formulae. The maximum stresses in body and bonnet were less than the allowable stresses.

The valve satisfies the requirements that the minimum section modulus and minimum cross sectional metal area are greater than those of the connected piping. This assures that stresses in the valve body will be less than those in the connected piping at the piping-to-valve interface. By then limiting stresses in the piping due to pressure plus dead weight plus thermal plus seismic to less than yielded it is assured that the state of stress in the valve body will be elastic therefore precluding any permanent deformations in the valves for this conservative loading combination. These requirements assure that the structural integrity and operability of the valve will not be compromised by externally applied piping loads.

3.0 NATURAL FREQUENCY

The natural frequency of the 6RV58MSB was determined using a single-degree-of-freedom model with a single lumped mass at the center of gravity of the valve. The model conservatively assumes that the equivalent body and bonnet cylinders have dimensions equal to their minimum cross sections. The minimum natural frequency was found to be 216 Hz.

4.0 SUMMARY OF RESULTS

A. Valve Body: Maximum Stress - 5058 psi
Allowable Stress - 18,7000 psi

Bonnet: Maximum Stress - 5720 psi
Allowable Stress - 17,400 psi

B. The natural frequency of the valve assembly is greater than 33 Hz.

C. There are no appurtenances on the 6RV58MSB requiring qualification in order to demonstrate structural integrity and operability.

5.0 CONCLUSION

This evaluation shows that the 6RV58MSB valve remains structurally sound and maintains full operational capabilities for the conditions subjected.

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TECHNICAL REPORT TR-5364-2
REVISION 0

BOOK 2 OF 10

DONALD C. COOK NUCLEAR GENERATING PLANT

ANALYSIS OF PRESSURIZER SAFETY/RELIEF VALVES
DISCHARGE PIPING SYSTEM PER NUREG 0737, I.D.1,
UNIT 2

860 8060048

JUNE 10, 1983

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AMERICAN ELECTRIC POWER SERVICE CORPORATION
2 BROADWAY
NEW YORK, NEW YORK 10004

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DONALD C. COOK NUCLEAR GENERATING STATION

ANALYSIS OF PRESSURIZER SAFETY/RELIEF VALVES
DISCHARGE PIPING SYSTEM PER NUREG 0737, II. D.1,
UNIT 2

JUNE 10, 1983

 TELEDYNE ENGINEERING SERVICES
130 SECOND AVENUE
WALTHAM, MASSACHUSETTS 02254
617-890-3350

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230/1000



1000
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4.9 RELAP Input

The RELAP5 MOD1 input listings are included for each of the transient conditions.

Input Listing

Transient Case

4.9.1	PORV Solid 400° Liquid 0-400 msec
4.9.2	PORV Solid 400° Liquid Restart 400-600 msec
4.9.3	SV Cold Loop Seal (Quarter Model)

The PORV model has:

- 411 volumes
- 412 junctions
- 7 tee branches

The SRV model has:

- 190 volumes
- 191 junctions

Heat structures were not included in the RELAP model because of the program capacity. Including heat structures would have further reduced the number of available control volumes. This is a conservative assumption, ITI (Reference 18) showed higher loads were computed without heat structures.

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TR-5364-2
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4.9.1 PORV Solid 400° Liquid

SAI0ES

00	0000000000	0000000000
01	0000000000	0000000000
02	0000000000	0000000000
03	0000000000	0000000000
04	0000000000	0000000000
05	0000000000	0000000000
06	0000000000	0000000000
07	0000000000	0000000000
08	0000000000	0000000000
09	0000000000	0000000000
10	0000000000	0000000000
11	0000000000	0000000000
12	0000000000	0000000000
13	0000000000	0000000000
14	0000000000	0000000000
15	0000000000	0000000000
16	0000000000	0000000000
17	0000000000	0000000000
18	0000000000	0000000000
19	0000000000	0000000000
20	0000000000	0000000000
21	0000000000	0000000000
22	0000000000	0000000000
23	0000000000	0000000000
24	0000000000	0000000000
25	0000000000	0000000000

LISTING OF INPUT DATA FOR CASE 1

```

1  =AEP UNIT2 1 LINE RELAPS
2  *
3  *
4  *
5  *
6  *
7  *
8  *
9  *
10 *
11 *
12 *
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20 *
21 *
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56 *

```

```

*****
*****
**                               **
**      UNIT 2 PORV MODEL,  SOLID CASE      **
**                               **
*****
*****

```

```

20 * AEP D.C. COOK UNIT2
21 * DISCHARGE PIPING
22 * THIS IS THE NUMBERING SYSTEM FOR UNIT2S' RELAP MODEL
23 * WHERE COMPONENTS NUMBERED IN THE:
24 *   100'S ARE VALVE SV-45C AND ARC 1 LEVEL 669'-2"
25 *   200'S ARE VALVE SV-45B AND ARC 2 LEVEL 670'-10"
26 *   300'S ARE VALVE SV-45A AND ARC 3 LEVEL 672'-6"
27 *   400'S ARE PORV NRV-151 AND ARC "A"
28 *   500'S ARE PORV NRV-153 AND ARC "B"
29 *   600'S ARE PORV NRV-152 AND ARC "C"
30 *   700'S ARE 6" DISCHARGE PIPING
31 *   800'S ARE 12" DISCH.
32 *   900'S QUENCH TANK PORTION
33 *   999 ATMOSPHERE

```

```

34 100 NEW TRANSNT
35 101 RUN
36 102 BRITISH BRITISH
37 104 NOACTION

```

```

39 *****
40 * TIME STEP CONTROL *
41 *****
42 *
43 201 0.400 1.0-7 2.0-4 11001 5 50 250
44 *

```

```

46 * MINOR EDITS *
47 *****
48 *
49 301 MFLOWJ 415000000
50 302 MFLOWJ 490000000
51 303 MFLOWJ 493000000
52 304 MFLOWJ 388000000
53 305 MFLOWJ 811140000
54 306 MFLOWJ 811790000
55 307 MFLOWJ 307000000
56 308 MFLOWJ 207000000

```

BY KJG DATE 5-17-83
 CHKD. BY CMM DATE 6-2-83

1002

1002

1002
1003
1004
1005
1006

```

57 309 MFLOWJ 107000000
58 *
59 310 QUALS 400010000
60 311 QUALS 500010000
61 312 QUALS 600010000
62 313 QUALS 410210000
63 314 QUALS 485270000
64 315 QUALS 492110000
65 316 QUALS 389010000
66 317 QUALS 811140000
67 318 QUALS 811790000
68 319 QUALS 106010000
69 320 QUALS 106390000
70 321 QUALS 206010000
71 322 QUALS 206330000
72 323 QUALS 306010000
73 324 QUALS 306250000
74 *
75 325 P 400010000
76 326 P 500010000
77 327 P 600010000
78 328 P 410210000
79 329 P 485270000
80 330 P 492110000
81 331 P 389010000
82 332 P 811140000
83 333 P 811790000
84 334 P 106010000
85 335 P 106390000
86 336 P 206010000
87 337 P 206330000
88 338 P 306010000
89 339 P 306250000
90 *
91 *
92 *
93 *
94 *
95 *****
96 ** **
97 ** FORCE CARDS FOR REPIPE **
98 ** **
99 *****
100 *
101 * ***** ARC 2, ELEVATION 670' 10", SV-45B *****
102 *
103 2001 5, 151
104 2002 206010000, 206020000, 206030000, 206040000, 206050000
105 2003 206060000, 206070000, 206080000, 206090000, 206100000
106 2004 206110000, 206120000, 206130000, 206140000, 206150000
107 2005 206160000, 206170000, 206180000, 206190000, 206200000
108 2006 206210000, 206220000, 206230000, 206240000, 206250000
109 2007 206260000, 206270000, 206280000, 206290000, 206300000
110 2008 206310000, 206320000, 206330000
111 *
112 *
113 *
114 *

```


VOICES



115
111
110
108
107

```

115 * **** FIRST C.V. DOWNSTREAM OF THE ARC ****
116 *
117 *
118 * 2010 805010000
119 *
120 *
121 *
122 *
123 * ***** 12 INCH DISCHARGE DOWN TO THE QUENCH TANK *****
124 *
125 *
126 * 2020 811190000,811200000,811210000,811220000,811230000
127 * 2021 811240000,811250000,811260000,811270000,811280000
128 * 2022 811290000,811300000,811310000,811320000,811330000
129 * 2023 811340000,811350000,811360000,811370000,811380000
130 * 2024 811390000,811400000,811410000,811420000,811430000
131 * 2025 811440000,811450000,811460000,811470000,811480000
132 * 2026 811490000,811500000,811510000,811520000,811530000
133 * 2027 811540000,811550000,811560000,811570000,811580000
134 * 2028 811590000,811600000,811610000,811620000,811630000
135 * 2029 811640000,811650000,811660000,811670000,811680000
136 * 2030 811690000,811700000,811710000,811720000,811730000
137 * 2031 811740000,811750000,811760000,811770000,811780000
138 * 2032 811790000,811800000,811810000,811820000,811830000
139 * 2033 811840000,811850000,811860000,811870000,811880000
140 * 2034 811890000,811900000,811910000,811920000,811930000
141 * 2035 811940000,811950000,811960000,811970000,811980000
142 * 2036 811990000,811180000
143 *
144 * 2040 813010000,813020000,813030000,813040000,813050000
145 * 2041 813060000,813070000,813080000,813090000,813100000
146 * 2042 813110000,813120000,813130000,813140000,813150000
147 * 2043 813160000,813170000,813180000,813190000,813200000
148 * 2044 813210000,813220000,813230000,813240000,813250000
149 * 2045 813260000,813270000,813280000,813290000,813300000
150 *
151 *
152 *
153 * ***** PIPE DOWN INTO THE QUENCH TANK *****
154 *
155 *
156 * 2050 901010000,901020000,903010000,903020000
157 * 2051 903030000
158 *
159 *
160 *
161 *
162 *
163 *
164 *
165 *
166 *
167 * ***** PIPING UPSTREAM OF PORV NRV - 153 *****
168 *
169 *
170 *
171 *
172 *

```



```

173 *
174 *
175 *
176 *
177 *
178 *****
179 *          TRIPS
180 *****
181 *
182 501 P 907010000 GT NULL 0 114.7 L *QUENCH TANK BLOW OUT PATCH
183 502 TIME 0 GT NULL 0 1.5 L * JOB TERMINATION TRIP
184 503 TIME 0 GE NULL 0 0.0 L * VALVE OPEN
185 504 TIME 0 GE NULL 0 5.0 L * VALVE CLOSED
186 600 502
187 *
188 *****
189 *          * HYDRODYNAMIC COMPONENTS *
190 *          *
191 *          *****
192 *****
193 *
194 3850000 "PRESS4" TMDPVOL
195 3850101 0.0 20.0 500.0 0.0 0.0 0.0 0.00005 0.0 11
196 3850200 3
197 3850201 0.0 2349.7 400.0 0.8 2420.0 400.0 1.2 2498.7 400.0
198 *
199 *          *****
200 *          * PORV UPSTREAM PIPING *
201 *          *****
202 *
203 *
204 3860000 "NOZ" SNGLJUN
205 3860101 385000000 387000000 0.0 0.0 0.0 1100
206 3860201 1 0.0 0.0 0.0
207 *
208 *          6 INCH SCH. 160 PIPE
209 *
210 3870000 "PORVU" PIPE
211 3870001 12
212 3870101 0.14653 12
213 3870301 0.328 1
214 3870302 0.5227 12
215 3870401 0.0 12
216 3870601 42.733 1
217 3870602 90.0 12
218 3870801 0.000151 0.0 12
219 3870901 0.0964 0.0964 1
220 3870902 0.0 0.0 11
221 3871001 00 12
222 3871101 1000 11
223 3871201 3 2349.7 400.0 0.0 0.0 12
224 3871300 1
225 3871301 0.0 0.0 0.0 11
226 *
227 3880000 "PORVU" SNGLJUN
228 3880101 387010000 389000000 0.0 0.0 0.0 1000
229 3880201 1 0.0 0.0 0.0
230 *

```

```

231 * 6 X 6 X 3 INCH REDUCING TEE
232 *
233 3890000 "PORV" BRANCH
234 3890001 0
235 3890101 0.14653 0.25 0.0 0.0 90.0 0.25 0.000151 0.0 00
236 3890200 3 2349.7 400.0 0.0 0.0 0.0
237 *
238 4980000 "PORV" SNGLJUN
239 4980101 389010000 410000000 0.0 0.1836 0.1836 1000
240 4980201 1 0.0 0.0 0.0
241 *
242 * 3 INCH SCH. 160 PIPING
243 *
244 4100000 "PORV" PIPE
245 4100001 21
246 4100101 0.03757 17
247 4100102 0.03387 18
248 4100103 0.0265 19
249 4100104 0.01912 20
250 4100105 0.01175 21
251 4100301 0.5 5
252 4100302 0.5278 11
253 4100303 0.5313 17
254 4100304 0.2657 21
255 4100401 0.0 21
256 4100601 0.0 5
257 4100602 90.0 11
258 4100603 0.0 21
259 4100801 0.000153 0.0 21
260 4100901 0.0 0.0 4
261 4100902 0.2172 0.2172 5
262 4100903 0.0 0.0 10
263 4100904 0.2172 0.2172 11
264 4100905 0.0 0.0 20
265 4101001 00 21
266 4101101 1000 20
267 4101201 3 2349.7 400.0 0.0 0.0 21
268 4101300 1
269 4101301 0.0 0.0 0.0 20
270 *
271 * PORV VALVE NRV - 153
272 *
273 4150000 "PORV153" VALVE
274 4150101 410010000 500000000 0.00806 0.0 0.0 0100
275 4150201 1 0.0 0.0 0.0
276 4150300 MTRVLV
277 4150301 503 504 1.0 0.0
278 *
279 4200000 "PORV" SNGLJUN
280 4200101 389010000 425000000 0.0 0.0 0.0 1000
281 4200201 1 0.0 0.0 0.0
282 *
283 * 6 INCH SCH. 160 PIPING
284 *
285 4250000 "PORV" PIPE
286 4250001 5
287 4250101 0.1465 5
288 4250301 0.3889 3

```



289	4250302	0.375	5						
290	4250401	0.0	5						
291	4250601	90.0	3						
292	4250602	0.0	5						
293	4250801	0.000151	0.0	5					
294	4250901	0.0	0.0	2					
295	4250902	0.1836	0.1836	3					
296	4250903	0.0	0.0	4					
297	4251001	00	5						
298	4251101	1000	4						
299	4251201	3	2349.7	400.0	0.0	0.0	5		
300	4251300	1							
301	4251301	0.0	0.0	0.0,	4				
302	*								
303	4300000	"PORV"	SINGLJUN						
304	4300101	425010000	435000000	0.0	0.0	0.0	1000		
305	4300201	1	0.0	0.0	0.0				
306	†								
307	*	6 INCH	X 4 INCH	REDUCER					
308	†								
309	4350000	"PORV"	PIPE						
310	4350001	2							
311	4350101	0.1465	1						
312	4350102	0.0716	2						
313	4350301	0.2292	2						
314	4350401	0.0	2						
315	4350601	0.0	2						
316	4350801	0.000151	0.0	1					
317	4350802	0.000133	0.0	2					
318	4350901	0.0577	0.0961	1					
319	4351001	00	2						
320	4351101	1000	1						
321	4351201	3	2349.7	400.0	0.0	0.0	2		
322	4351300	1							
323	4351301	0.0	0.0	0.0	1				
324	†								
325	*								
326	4400000	"PORV"	SINGLJUN						
327	4400101	435010000	445000000	0.0	0.0	0.0	1000		
328	4400201	1	0.0	0.0	0.0				
329	*								
330	*	4 INCH	SCH. 120	PIPING					
331	†								
332	4450000	"PORV"	PIPE						
333	4450001	10							
334	4450101	0.0716	10						
335	4450301	0.35833	5						
336	4450302	0.5	10						
337	4450401	0.0	10						
338	4450601	0.0	5						
339	4450602	90.0	9						
340	4450603	0.0	10						
341	4450801	0.000133	0.0	10					
342	4450901	0.0	0.0	4					
343	4450902	0.1944	0.1944	5					
344	4450903	0.0	0.0	8					
345	4450904	0.1944	0.1944	9					
346	4451001	00	10						

```

347 4451101 1000 9
348 4451201 3 2349.7 400.0 0.0 0.0 10
349 4451300 1
350 4451301 0.0 0.0 0.0 9
351 *
352 4500000 "PORV" SNGLJUN
353 4500101 445010000 455000000 0.0 0.0 0.0 1000
354 4500201 1 0.0 0.0 0.0
355 *
356 * 4 X 4 X 3 INCH REDUCING BRANCH
357 *
358 4550000 "PORV" BRANCH
359 4550001 0
360 4550101 0.0716 0.5 0.0 0.0 0.0 0.0 0.000133 0.0 00
361 4550200 3 2349.7 400.0 0.0 0.0 0.0
362 *
363 4600000 "PORV" SNGLJUN
364 4600101 455010000 465000000 0.0 0.0 0.0 1000
365 4600201 1 0.0 0.0 0.0
366 *
367 * 4 INCH SCH. 120 PIPING
368 *
369 4650000 "PORV" PIPE
370 4650001 3
371 4650101 0.0716 3
372 4650301 0.25 3
373 4650401 0.0 3
374 4650601 0.0 3
375 4650801 0.000133 0.0 3
376 4650901 0.0 0.0 2
377 4651001 00 3
378 4651101 1000 2
379 4651201 3 2349.7 400.0 0.0 0.0 3
380 4651300 1
381 4651301 0.0 0.0 0.0 2
382 *
383 4700000 "PORV" SNGLJUN
384 4700101 465010000 475000000 0.0 0.0 0.0 1000
385 4700201 1 0.0 0.0 0.0
386 *
387 * 4 INCH X 3 INCH REDUCER
388 *
389 4750000 "PORV" PIPE
390 4750001 2
391 4750101 0.0716 1
392 4750102 0.0376 2
393 4750301 0.1667 2
394 4750401 0.0 2
395 4750601 0.0 2
396 4750801 0.000133 0.0 1
397 4750802 0.000153 0.0 2
398 4750901 0.0472 0.0730 1
399 4751001 00 2
400 4751101 1000 1
401 4751201 3 2349.7 400.0 0.0 0.0 2
402 4751301 0.0 0.0 0.0 1
403 *
404 4800000 "PORV" SNGLJUN

```




```

405 4800101 475010000 485000000 0.0 0.0 0.0 1000
406 4800201 1 0.0 0.0 0.0
407 *
408 * 3 INCH SCH. 160 PIPING
409 *
410 4850000 "PORV" PIPE
411 4850001 27
412 4850101 0.0376 23
413 4850102 0.0339 24
414 4850103 0.0266 25
415 4850104 0.0192 26
416 4850105 0.0118 27
417 4850301 0.4375 4
418 4850302 0.4690 12
419 4850303 0.500 15
420 4850304 0.368 16
421 4850305 0.367 17
422 4850306 0.5405 23
423 4850307 0.41937 27
424 4850401 0.0 27
425 4850601 0.0 27
426 4850801 0.000153 0.0 27
427 4850901 0.0 0.0 26
428 4851001 00 27
429 4851101 1000 26
430 4851201 3 2349.7 400.0 0.0 0.0 27
431 4851300 1
432 4851301 0.0 0.0 0.0 26
433 *
434 * PORV VALVE NRV - 151
435 *
436 4900000 "PORV" VALVE
437 4900101 485010000 400000000 0.00806 0.0 0.0 0100
438 4900201 1 0.0 0.0 0.0
439 4900300 MTRVLV
440 4900301 503 504 1.0 0.0
441 *
442 4910000 "PORV" SNGLJUN
443 4910101 455010000 492000000 0.0 0.095 0.095 1000
444 4910201 1 0.0 0.0 0.0
445 *
446 * 3 INCH SCH. 160 PIPING
447 *
448 4920000 "PORV" PIPE
449 4920001 11
450 4920101 0.0376 7
451 4920102 0.0339 8
452 4920103 0.0266 9
453 4920104 0.0192 10
454 4920105 0.0118 11
455 4920301 0.4881 7
456 4920302 0.4792 11
457 4920401 0.0 11
458 4920601 0.0 11
459 4920801 0.000153 0.0 11
460 4920901 0.0 0.0 10
461 4921001 00 11
462 4921101 1000 10

```

1000 1000 1000 1000 1000 1000 1000 1000 1000 1000



```

463 4921201 3 2349.7 400.0 0.0 0.0 ii
464 4921300 1
465 4921301 0.0 0.0 0.0 10
466 *
467 *   PORV VALVE NRV - 152
468 *
469 4930000 "PORV" VALVE
470 4930101 492010000 600000000 0.00806 0.0 0.0 0100
471 4930201 1 0.0 0.0 0.0
472 4930300 MTRVLV
473 4930301 503 504 1.0 0.0
474 *
475 *
476 *****
477 *   SAFETY VALVES DISCHARGE SECTION
478 *****
479 *
480 *
481 *
482 *****
483 *   SAFETY VALVE-45C DISCHARGING AT ELEV. 669'-2" ARC 1 *
484 *****
485 *
486 *
487 **
488 *   DISCHARGE PIPING
489 *
490 *   6 INCH SCH. 40 PIPING
491 **
492 1060000 "DISCHA1" PIPE
493 1060001 39
494 1060101 0.20069 39
495 1060301 0 526 4
496 1060302 1.094 14
497 *   ARC STARTS HERE LEVEL 669-2"
498 1060303 1.000 20
499 1060304 0.8994 29
500 1060305 0.7436 35
501 *   ARC ENDS
502 1060306 0.7980 39
503 1060401 0.0 39
504 1060601 0.0 4
505 1060602 -90.0 14
506 1060603 0.0 39
507 1060801 0.000152 0.0 39
508 1060901 0.0 0.0 3
509 1060902 0.1800 0.1800 4
510 1060903 0.0 0.0 13
511 1060904 0.1800 0.1800 14
512 1060905 0.0 0.0 38
513 1061001 00 39
514 1061101 1000 38
515 1061201 4 17.7 120.0 0.9284 0.0 39
516 1061300 1
517 1061301 0.0 0.0 0.0 38
518 *
519 1070000 "DISCHA1" SNGLJUN
520 1070101 106010000 809000000 0.0 0.1560 0.1560 1000 *LOSSES FOR A 12 IN ELBOW

```

```

521 1070201 1 0.0 0.0 0.0
522 *
523 *
524 *
525 *****
526 *      MAIN DISCHARGE 12" HEADER TO QUENCH TANK      *
527 *****
528 *
529 *
530 *      12 X 12 X 6 INCH REDUCING TEE
531 *
532 *      CONNECTS SRV PIPING TO MAIN DISCHARGE
533 *
534 *
535 8090000 "DISCHA1" BRANCH
536 8090001 0
537 8090101 0.77708 0.5 0.0 0.0 -90.0 -0.5 0.000169 0.0 00
538 8090200 4 17.7 120.0 0.9284
539 *
540 8100000 "DISCHA1" SNGLJUN
541 8100101 809010000 811000000 0.0 0.0 0.0 1000
542 8100201 1 0.0 0.0 0.0
543 *
544 *      12 INCH SCH. 40 DISCHARGE PIPING
545 *
546 8110000 "DISCHA1" PIPE
547 8110001 99
548 8110101 0.7771 99
549 8110301 1.039 14
550 8110302 0.53025 18
551 8110303 0.5 22
552 8110304 0.53025 26
553 8110305 0.9875 56
554 8110306 0.475 66
555 8110307 0.49359 79
556 8110308 0.46875 87
557 8110309 0.50 95
558 8110310 0.875 99
559 8110401 0.0 99
560 8110601 -90.0 14
561 8110602 -45.0 18
562 8110603 -90.0 22
563 8110604 -45.0 26
564 8110605 -90.0 56
565 8110606 0.0 87
566 8110607 -90.0 95
567 8110608 0.0 99
568 8110801 0.000169 0.0 99
569 8110901 0.0 0.0 13
570 8110902 0.078 0.078 14
571 8110903 0.0 0.0 17
572 8110904 0.078 0.078 18
573 8110905 0.0 0.0 21
574 8110906 0.078 0.078 22
575 8110907 0.0 0.0 25
576 8110908 0.078 0.078 26
577 8110909 0.0 0.0 55
578 8110910 0.158 0.158 56

```

```

579 8110911 0.0 0.0 65
580 8110912 0.026 0.026 66
581 8110913 0.0 0.0 78
582 8110914 0.13 0.13 79
583 8110915 0.0 0.0 88
584 8110916 0.156 0.156 87
585 8110917 0.0 0.0 94
586 8110918 0.156 0.156 95
587 8110919 0.0 0.0 88
588 8111001 00 99
589 8111101 1000 98
590 8111201 4 17.7 120.0 0.9284 0.0 99
591 8111300 1
592 8111301 0.0 0.0 0.0 98
593 *
594 8120000 "DISCHA1" SNGLJUN
595 8120101 811010000 813000000 0.0 0.0 0.0 1000
596 8120201 1 0.0 0.0 0.0
597 *
598 † 12 INCH SCH. 40 DISCHARGE PIPING
599 †
600 8130000 "DISCHA1" PIPE
601 8130001 30
602 8130101 0.7771 30
603 8130301 0.875 6
604 8130302 1.0 20
605 8130303 0.5 30
606 8130401 0.0 30
607 8130601 0.0 30
608 8130801 0.000169 0.0 30
609 8130901 0.0 0.0 5
610 8130902 0.156 0.156 6
611 8130903 0.0 0.0 19
612 8130904 0.156 0.156 20
613 8130905 0.0 0.0 29
614 8131001 00 30
615 8131101 1000 29
616 8131201 4 17.7 120.0 0.9284 0.0 30
617 8131300 1
618 8131301 0.0 0.0 0.0 29
619 †
620 †
621 †
622 *****
623 † SAFETY VALVE 45B AT ELEV. 670'-10" ARC 2 *
624 *****
625 †
626 †
627 †
628 **
629 † DISCHARGE PIPING
630 †
631 * 6 INCH SCH. 40 PIPING
632 **
633 2060000 "DISCHA2" PIPE
634 2060001 33
635 2060101 0.20069 33
636 2060301 0.4635 4

```

```

637 2060302 0.927 14
638 *ARC STARTS LEVEL 670'-10"
639 2060303 0.955 23
640 2060304 0.727 29
641 2060308 0.7980 33
642 2060401 0.0 33
643 2060601 0.0 4
644 2060602 -90. 14
645 2060603 0.0 33
646 2060801 0.000152 0.0 33
647 2060901 0.0 0.0 3
648 2060902 0.1800 0.1800 4
649 2060903 0.0 0.0 13
650 2060904 0.1800 0.1800 14
651 2060905 0.0 0.0 32
652 2061001 00 33
653 2061101 1000 32
654 2061201 4 17.7 120.0 0.9284 0.0 33
655 2061300 1
656 2061301 0.0 0.0 0.0 32
657 *
658 *****
659 * SAFETY VALVE 45A AT ELEV. 672'-6" ARC 3 *
660 *****
661 *
662 *
663 *
664 **
665 * DISCHARGE PIPING
666 *
667 * 6 INCH SCH. 40 PIPING
668 **
669 3060000 "DISCHA3" PIPE
670 3060001 25
671 3060101 0.20069 25
672 3060301 0.526 4
673 3060302 0.969 12
674 * ARC STARTS LEVEL 672'-6"
675 3060303 0.635 15
676 3060304 0.991 18
677 3060305 0.991 21
678 3060306 0.799 25
679 * ARC ENDS
680 3060401 0.0 25
681 3060601 0.0 4
682 3060602 -90.0 12
683 3060603 0.0 25
684 3060801 0.000152 0.0 25
685 3060901 0.0 0.0 3
686 3060902 0.1800 0.1800 4
687 3060903 0.0 0.0 11
688 3060904 0.1800 0.1800 12
689 3060905 0.0 0.0 24
690 3061001 00 25
691 3061101 1000 24
692 3061201 4 17.7 120.0 0.9284 0.0 25
693 3061300 1
694 3061301 0.0 0.0 0.0 24

```

```

695 *
696 *
697 *
698 *
699 *****
700 *      PORV PIPING
701 *****
702 *
703 *
704 *      PIPING DOWNSTREAM OF VALVE NRV - 153
705 *
706 *      3 INCH SCH. 40 PIPING
707 *
708 *
709 5000000 "PORVB" PIPE
710 5000001 16
711 5000101 0.05132 16 " * 3 IN SCH40S
712 5000301 0.497 3
713 5000302 0.556 6
714 *      ARC STARTS LEVEL 684'-9"
715 5000303 0.365 7 *
716 5000304 0.6448 13
717 5000305 0.5892 16
718 5000401 0.0 16
719 5000601 0.0 3
720 5000602 -90.0 6
721 5000603 0.0 16
722 5000801 0.000153 0.0 16
723 5000901 0.0 0.0 2
724 5000902 0.2088 0.2088 3
725 5000903 0.0 0.0 5
726 5000904 0.2088 0.2088 6
727 5000905 0.0 0.0 15
728 5001001 00 16
729 5001101 1000 15
730 5001201 4 17.7 120.0 0.9284 0.0 16
731 5001300 1
732 5001301 0.0 0.0 0.0 15
733 *
734 5010000 "PORVB" SNGLJUN * THIS JUNCTION IS ON ARC B
735 5010101 500010000 502000000 0.0 0.0 0.0 1000
736 5010201 1 0.0 0.0 0.0
737 *
738 *      4 INCH X 3 INCH DIFFUSER
739 *
740 5020000 "PORVB" PIPE * REDUCER ON ARC B 3IN X4IN
741 5020001 2
742 5020101 0.05132 1 * 3IN SCH40S
743 5020102 0.08840 2 * 4IN SCH40S
744 5020301 0.3385 2
745 5020401 0.0 2
746 5020601 0.0 2
747 5020801 0.000153 0.0 1
748 5020802 0.000134 0.0 2
749 5020901 0.0399 0.0544 1
750 5021001 00 2
751 5021101 1000 1
752 5021201 4 17.7 120.0 0.9284 0.0 2

```




```

753 5021300 1
754 5021301 0.0 0.0 0.0 1
755 *
756 *
757 5030000 "PORVB" SNGLJUN * ON ARC B
758 5030101 502010000 504000000 0.0 0.0 0.0 1000
759 5030201 1 0.0 0.0 0.0
760 *
761 * 4 X 4 X 3 INCH BRANCH
762 *
763 5040000 "PORVB" BRANCH * ON ARC B @ 242
764 5040001 0
765 5040101 0.0884 0.361 0.0 0.0 0.0 0.0 0.000134 0.0 00
766 5040200 4 17.7 120.0 0.9284 0.0 0.0
767 *
768 5050000 "PORVB" SNGLJUN * ON ARC B
769 5050101 504010000 506000000 0.0 0.0 0.0 1000
770 5050201 1 0.0 0.0 0.0
771 *
772 * 4 INCH SCH. 40 PIPING
773 *
774 5060000 "PORVB" PIPE * ON ARC B
775 5060001 9
776 5060101 0.0884 9
777 5060301 0.6211 8
778 5060302 0.7607 9
779 5060401 0.0 9
780 5060601 0.0 9
781 5060801 0.000134 0.0 9
782 5060901 0.0 0.0 8
783 5061001 00 9
784 5061101 1000 8
785 5061201 4 17.7 120.0 0.9284 0.0 9
786 5061300 1
787 5061301 0.0 0.0 0.0 8
788 *
789 5070000 "PORVB" SNGLJUN
790 5070101 506010000 508000000 0.0 0.0 0.0 1000
791 5070201 1 0.0 0.0 0.0
792 *
793 * 4 INCH X 6 INCH DIFFUSER
794 *
795 5080000 "PORVB" PIPE
796 5080001 2
797 5080101 0.0884 1
798 5080102 0.20069 2
799 5080301 0.5792 2
800 5080401 0.0 2
801 5080601 0.0 2
802 5080801 0.000134 0.0 1
803 5080802 0.000152 0.0 2
804 5080901 0.1483 0.0815 1
805 5081001 00 2
806 5081101 1000 1
807 5081201 4 17.7 120.0 0.9284 0.0 2
808 5081300 1
809 5081301 0.0 0.0 0.0 1
810 *

```

```

811 5090000 "PORVB" SNGLJUN * ON ARC B
812 5090101 508010000 510000000 0.0 0.0 0.0 1000
813 5090201 1 0.0 0.0 0.0
814 *
815 * 6 X 6 X 3 INCH REDUCING TEE
816 *
817 5100000 "PORVB" BRANCH * ON ARC B @ 232
818 5100001 0
819 5100101 0.20069 0.25 0.0 0.0 0.0 0.0 0.000152 0.0 00
820 5100200 4 17.7 120.0 0.9284 0.0 0.0
821 *
822 5110000 "PORVB" SNGLJUN * ON ARC B
823 5110101 510010000 700000000 0.0 0.0 0.0 1000
824 5110201 1 0.0 0.0 0.0
825 *
826 * PIPING DOWNSTREAM OF VALVE NRV - 151
827 *
828 * 3 INCH SCH. 40 PIPING
829 *
830 4000000 "PORVA" PIPE
831 4000001 8
832 4000101 0.05132 8
833 4000301 0.4141 4
834 4000302 0.4375 8
835 4000401 0.0 8
836 4000601 0.0 4
837 4000602 -90.0 8
838 4000801 0.000153 0.0 8
839 4000901 0.0 0.0 3
840 4000902 0.2088 0.2088 4
841 4000903 0.0 0.0 7
842 4001001 00 8
843 4001101 1000 7
844 4001201 4 17.7 120.0 0.9284 0.0 8
845 4001300 1
846 4001301 0.0 0.0 0.0 7
847 *
848 4010000 "PORVAB" SNGLJUN
849 4010101 400010000 510000000 0.0 0.1800 0.1800 1000
850 4010201 1 0.0 0.0 0.0
851 *
852 * DOWNSTREAM PIPING FROM VALVE NRV - 152
853 *
854 * 3 INCH SCH. 40 PIPING
855 *
856 6000000 "PORVC" PIPE
857 6000001 7
858 6000101 0.05132 7
859 6000301 0.4722 3
860 6000302 0.4375 7
861 6000401 0.0 7
862 6000601 0.0 3
863 6000602 -90.0 7
864 6000801 0.000153 0.0 7
865 6000901 0.0 0.0 2
866 6000902 0.2088 0.2088 3
867 6000903 0.0 0.0 8
868 6001001 00 7

```

```

869 6001101 1000 6
870 6001201 4 17.7 120.0 0.9284 0.0 7
871 6001300 1
872 6001301 0.0 0.0 0.0 8
873 *
874 6010000 "PORVBC" SNGLJUN
875 6010101 600010000 504000000 0.0 0.1932 0.1932 1000
876 6010201 1 0.0 0.0 0.0
877 *
878 * MAIN HEADER DOWNSTREAM OF PORV PIPING
879 *
880 7000000 "PORVBD" PIPE
881 7000001 12
882 7000101 0.20069 12
883 7000301 0.75 2
884 7000302 1.075 12
885 7000401 0.0 12
886 7000601 0.0 2
887 7000602 -90. 12
888 7000801 0.000152 0.0 12
889 7000901 0.0 0.0 1
890 7000902 0.1800 0.1800 2
891 7000903 0.0 0.0 11
892 7001001 00 12
893 7001101 1000 11
894 7001201 4 17.7 120.0 0.9284 0.0 12
895 7001300 1
896 7001301 0.0 0.0 0.0 11
897 *
898 7010000 "PORVD" SNGLJUN
899 7010101 700010000 702000000 0.0 0.0 0.0 1000
900 7010201 1 0.0 0.0 0.0
901 *
902 *
903 *
904 *
905 *
906 *****
907 **
908 ** MAIN ARC CONNECTIONS **
909 **
910 *****
911 *
912 *
913 *
914 * 12 INCH X 6 INCH DIFFUSER ABOVE SRV ARCS ON MAIN DISCHARGE
915 *
916 *
917 *
918 7020000 "PORVD" PIPE
919 7020001 3
920 7020101 0.20069 1
921 7020102 .77708 3
922 7020301 0.75 1
923 7020302 0.375 3
924 7020401 0.0 3
925 7020601 -90.0 3
926 7020801 0.000152 0.0 1

```

927	7020802	0.000169	0.0	3						
928	7020901	0.4930	0.2045	1						
929	7020902	0.0	0.0	2						
930	7021001	00		3						
931	7021101	1000		2						
932	7021201	4	17.7	120.0	0.9284	0.0	3			
933	7021300	1								
934	7021301	0.0	0.0	0.0	2					
935	*									
936	8000000	"PORVD"	SNGLJUN							
937	8000101	702010000	801000000	0.0	0.0	0.0	1000			
938	8000201	1	0.0	0.0	0.0					
939	*									
940	3070000	"PORVD3"	SNGLJUN							
941	3070101	306010000	801000000	0.0	0.156	0.156	1000	*	12 IN ELBOW LOSSES	
942	3070201	1	0.0	0.0	0.0					
943	†									
944	†	12 X	12 X	6	INCH REDUCING TEE CONNECTS ARC WITH DISCHARGE					
945	†									
946	8010000	"PORVD"	BRANCH							
947	8010001	0								
948	8010101	0.77708	0.5	0.0	0.0	-90.	-0.5	0.000169	0.0	00
949	8010200	4	17.7	120.0	0.9284	0.0	0.0			
950	†									
951	8020000	"PORVD"	SNGLJUN							
952	8020101	801010000	803000000	0.0	0.0	0.0	1000			
953	8020201	1	0.0	0.0	0.0					
954	*									
955	8030000	"PORVD"	SNGLVOL							
956	8030101	0.77708	1.1667	0.0	0.0	-90.	-1.1667	0.000169	0.0	00
957	8030200	4	17.7	120.0	0.9284	0.0	0.0			
958	†									
959	8040000	"PORVD"	SNGLJUN							
960	8040101	803010000	805000000	0.0	0.0	0.0	1000			
961	8040201	1	0.0	0.0	0.0					
962	*									
963	2070000	"PORVD"	SNGLJUN							
964	2070101	206010000	805000000	0.0	0.156	0.156	1000	*	12 IN ELBOW LOSSES	
965	2070201	1	0.0	0.0	0.0					
966	†									
967	†	12 X12 X	6	INCH REDUCING TEE. CONNECTS SRV ARC WITH DISCHARGE PIPING.						
968	†									
969	8050000	"PORVD"	BRANCH							
970	8050001	0								
971	8050101	0.77708	0.5	0.0	0.0	-90.	-0.5	0.000169	0.0	00
972	8050200	4	17.7	120.0	0.9284	0.0	0.0			
973	†									
974	8060000	"PORVD"	SNGLJUN							
975	8060101	805010000	807000000	0.0	0.0	0.0	1000			
976	8060201	1	0.0	0.0	0.0					
977	†									
978	8070000	"PORVD"	SNGLVOL							
979	8070101	0.77708	1.1667	0.0	0.0	-90.	-1.1667	0.000169	0.0	00
980	8070200	4	17.7	120.0	0.9284	0.0	0.0			
981	*									
982	8080000	"PORVD"	SNGLJUN							
983	8080101	807010000	809000000	0.0	0.0	0.0	1000			
984	8080201	1	0.0	0.0	0.0					

```

985 *
986 9000000 "QTANKD"  SNGLJUN
987 9000101 813010000 901000000 0.0 0.1560 0.1560 1000
988 9000201 1 0.0 0.0 0.0
989 *
990 9010000 "QTANKD"  PIPE
991 9010001 2
992 9010101 0.77708 2
993 9010301 1.0833 2
994 9010401 0.0 2
995 9010601 -90.0 2
996 9010801 0.000169 0.0 2
997 9010901 0.0 0.0 1
998 9011001 00 2
999 9011101 1000 1
1000 9011201 4 17.7 120.0 0.9284 0.0 2
1001 9011300 1
1002 9011301 0.0 0.0 0.0 1
1003 *
1004 *****
1005 ** **
1006 ** QUENCH TANK **
1007 ** **
1008 *****
1009 *
1010 9020000 "QTANK-IN" SNGLJUN
1011 9020101 901010000 903000000 0.0 0.0 0.0 1000
1012 9020201 1 0.0 0.0
1013 **
1014 * SPARGER 12 IN SCH40 PIPE
1015 **
1016 9030000 "SPARGER" PIPE
1017 * NO OF VOLUMES
1018 9030001 18
1019 * FLOW AREA
1020 9030101 0.7773 18
1021 * VOL. LENGTHS
1022 9030301 1.125 2
1023 9030302 1.1333 7
1024 9030303 1.0 18
1025 * VOL. VOLS.
1026 9030401 0.0 18
1027 *
1028 * VERTICAL ANGLES
1029 9030601 -90. 7
1030 9030602 0.0 18
1031 * PIPE ROUGHNESS
1032 9030801 1.69-4 0.0 18
1033 * JUNCTION LOSS COEFF.
1034 9030901 0.0 0.0 6
1035 9030902 0.156 0.156 7
1036 9030903 0.0 0.0 17
1037 * VOL. CONTROL FLAG
1038 9031001 00 18
1039 * JUN. CONTROL FLAG
1040 9031101 1000 17
1041 * INITIAL COND.
1042 9031201 4 17.7 120. 0.9284 0.0 2

```

```

1043 9031202 3 17.7 120. 0.0 0. 18.
1044 * JUN. INITIAL COND.
1045 9031300 1
1046 9031301 0.0 0.0 0.0 17
1047 **
1048 * SPARGER EXIT
1049 **
1050 9040000 "EXIT" SNGLJUN
1051 9040101 903010000 905000000 0.0 1.0 1.0 0100
1052 9040201 1 0. 0. 0.
1053 **
1054 * WATER VOL.
1055 **
1056 9050000 "QT. WATER" SNGLVOL
1057 9050101 260.4706 5.6667 0.0 0.0 90. 5.6667 0.003 0.0 01
1058 9050200 3 17.7 120.
1059 **
1060 * INTERFACE
1061 **
1062 9060000 "INTERFACE" SNGLJUN
1063 9060101 905010000 907000000 0.0 0.0 0.0 1000
1064 9060201 1 0.0 0.0 0.0
1065 **
1066 * AIR VOLUME
1067 **
1068 9070000 "QT. AIR" SNGLVOL
1069 9070101 260.4706 1.2439 0.0 0.0 90. 1.2439 0.003 0.0 01
1070 9070200 4 17.7 120. 0.9284
1071 **
1072 * RUPTURE DISC
1073 **
1074 9080000 "RUP. DISC" VALVE
1075 9080101 907010000 999000000 1.77 0. 0. 1100
1076 9080201 1 0. 0. 0.
1077 9080300 TRPVLV
1078 9080301 501 * VALVE OPENING TRIP
1079 **
1080 * PIPE OUTSIDE ENVIRONMENT
1081 **
1082 9990000 "ATMOSPHERE" TMDPVOL
1083 9990101 10000. 10000. 0.0 0.0 0.0 0.0 .00001 0.0 11
1084 9990200 4
1085 9990201 0.0 17.7 120. 0.9284
1086 .END OF CASE

```

Technical Report
TR-5364-2
Revision 0

4.9.2 PORV Solid 400^o Liquid Restart

LISTING OF INPUT DATA FOR CASE 1

Technical Report
- TR-5364-2
Revision 0

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TELEDYNE
ENGINEERING SERVICES

```

1 =THIS RESTARTS RELAP 3 PORVS OPENING ON SOLID WATER UNIT2 RED
2 *
3 100 RESTART TRANSNT
4 101 RUN
5 *
6 103 2000
7 104 NOACTION
8 201 0.600 1.-7 2.-4 11001.5 50 250
9 *
10 *
11 * MINOR EDITS
12 *
13 301 MFLOWJ 41500000
14 302 MFLOWJ 490000000
15 303 MFLOWJ 493000000
16 304 MFLOWJ 388000000
17 305 MFLOWJ 811140000
18 306 MFLOWJ 811790000
19 307 MFLOWJ 307000000
20 308 MFLOWJ 207000000
21 309 MFLOWJ 107000000
22 *
23 310 QUALS 400010000
24 311 QUALS 500010000
25 312 QUALS 600010000
26 313 QUALS 410210000
27 314 QUALS 485270000
28 315 QUALS 492110000
29 316 QUALS 389010000
30 317 QUALS 811140000
31 318 QUALS 811790000
32 319 QUALS 106010000
33 320 QUALS 106390000
34 321 QUALS 206010000
35 322 QUALS 206330000
36 323 QUALS 306010000
37 324 QUALS 306250000
38 *
39 325 P 400010000
40 326 P 500010000
41 327 P 600010000
42 328 P 410210000
43 329 P 485270000
44 330 P 492110000
45 331 P 389010000
46 332 P 811140000
47 333 P 811790000
48 334 P 106010000
49 335 P 106390000
50 336 P 206010000
51 337 P 206330000
52 338 P 306010000
53 339 P 306250000
54 *
55 2001 5,151
56 2002 206010000,206020000,206030000,206040000,206050000

```

BY KJG DATE 5-20-83
 CHKD. BY CMM DATE 6-2-83

57 2003 206060000,206070000,206080000,206090000,206100000
 58 2004 206110000,206120000,206130000,206140000,206150000
 59 2005 206160000,206170000,206180000,206190000,206200000
 60 2006 206210000,206220000,206230000,206240000,206250000
 61 2007 206260000,206270000,206280000,206290000,206300000
 62 2008 206310000,206320000,206330000

63 *
 64 *
 65 *
 66 *

67 * **** FIRST C.V. DOWNSTREAM OF THE ARC **** *

68 *
 69 *

70 2010 805010000

71 *
 72 *
 73 *
 74 *

75 * ***** 12 INCH DISCHARGE DOWN TO THE QUENCH TANK ***** *

76 *
 77 *

78 2020 811190000,811200000,811210000,811220000,811230000
 79 2021 811240000,811250000,811260000,811270000,811280000
 80 2022 811290000,811300000,811310000,811320000,811330000
 81 2023 811340000,811350000,811360000,811370000,811380000
 82 2024 811390000,811400000,811410000,811420000,811430000
 83 2025 811440000,811450000,811460000,811470000,811480000
 84 2026 811490000,811500000,811510000,811520000,811530000
 85 2027 811540000,811550000,811560000,811570000,811580000
 86 2028 811590000,811600000,811610000,811620000,811630000
 87 2029 811640000,811650000,811660000,811670000,811680000
 88 2030 811690000,811700000,811710000,811720000,811730000
 89 2031 811740000,811750000,811760000,811770000,811780000
 90 2032 811790000,811800000,811810000,811820000,811830000
 91 2033 811840000,811850000,811860000,811870000,811880000
 92 2034 811890000,811900000,811910000,811920000,811930000
 93 2035 811940000,811950000,811960000,811970000,811980000
 94 2036 811990000,811180000

95 *
 96 2040 813010000,813020000,813030000,813040000,813050000
 97 2041 813060000,813070000,813080000,813090000,813100000
 98 2042 813110000,813120000,813130000,813140000,813150000
 99 2043 813160000,813170000,813180000,813190000,813200000
 100 2044 813210000,813220000,813230000,813240000,813250000
 101 2045 813260000,813270000,813280000,813290000,813300000

102 *
 103 *
 104 *

105 * ***** PIPE DOWN INTO THE QUENCH TANK ***** *

106 *
 107 *

108 2050 901010000,901020000,903010000,903020000

109 2051 903030000

110 *
 111 *

112 *
 113 3880000 "PORVU" SNGLJUN

114 3880101 387010000 389000000 0.0 0.0 0.0 1000

115	3880201	1	0.0	0.0	0.0
116	20300100	MFLOWJ	415000000		
117	20300200	MFLOWJ	493000000		
118	20300300	MFLOWJ	490000000		
119	20300400	MFLOWJ	388000000		
120	20300500	MFLOWJ	811140000		
121	20300600	MFLOWJ	811790000		
122	20300700	MFLOWJ	307000000		
123	20300800	MFLOWJ	207000000		
124	20300900	MFLOWJ	107000000		
125	*				
126	20301000	QUALS	400010000		
127	20301100	QUALS	500010000		
128	20301200	QUALS	600010000		
129	20301300	QUALS	410210000		
130	20301400	QUALS	485270000		
131	20301500	QUALS	492110000		
132	20301600	QUALS	389010000		
133	20301700	QUALS	811140000		
134	20301800	QUALS	811790000		
135	20301900	QUALS	106010000		
136	20302000	QUALS	106390000		
137	20302100	QUALS	206010000		
138	20302200	QUALS	206330000		
139	20302300	QUALS	306010000		
140	20302400	QUALS	306250000		
141	*				
142	20302500	P	400010000		
143	20302600	P	500010000		
144	20302700	P	600010000		
145	20302800	P	410210000		
146	20302900	P	485270000		
147	20303000	P	492110000		
148	20303100	P	389010000		
149	20303200	P	811140000		
150	20303300	P	811790000		
151	20303400	P	106010000		
152	20303500	P	106390000		
153	20303600	P	206010000		
154	20303700	P	206330000		
155	20303800	P	306010000		
156	20303900	P	306250000		
157	*				
158	.END				

Technical Report
TR-5364-2
Revision 0

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 **TELEDYNE
ENGINEERING SERVICES**

4.9.3 SV Cold Loop Seal (Quarter Model)

LISTING OF INPUT DATA FOR CASE 1

```

1  =AEP UNIT2 1 LINE RELAP5
2  100 NEW TRANSNT
3  101 RUN
4  102 BRITISH BRITISH
5  104 NOACTION
6  * TIME STEP CONTROL
7  *
8  201 0.6000 1.0-7 2.0-4 11001 5 25 250
9  * MINOR EDITS
10 *
11 301 QUALS 007010000
12 302 QUALS 005200000
13 303 QUALS 013200000
14 304 P 005200000
15 305 P 007010000
16 308 P 007380000
17 307 MFLOWJ 006000000
18 308 MFLOWJ 005070000
19 309 MFLOWJ 014000000
20 310 P 007140000
21 311 P 011560000
22 312 P 013300000
23 313 MFLOWJ 007140000
24 314 MFLOWJ 007380000
25 315 MFLOWJ 011560000
26 *
27 *
28 2001 5,192,001010000,003010000,005010000
29 2002 005020000,005030000,005040000,005050000,005080000
30 2003 005070000,005080000,005090000,005100000,005110000
31 2004 005120000,005130000,005140000,005150000,005180000
32 2005 005170000,005180000,005190000,005200000,007010000
33 2006 007020000,007030000,007040000,007050000,007080000,007070000
34 2007 007080000,007090000,007100000,007110000,007120000
35 2008 007130000,007140000,007150000,007160000,007170000
36 2009 007180000,007190000,007200000,007210000,007220000
37 2010 007230000,007240000,007250000,007260000,007270000
38 2011 007280000,007290000,007300000,007310000,007320000
39 2012 007330000,007340000,007350000,007360000,007370000
40 2013 007380000,007390000,009010000,011010000,011020000
41 2014 011030000,011040000,011050000,011060000,011070000
42 2015 011080000,011090000,011100000,011110000,011120000
43 2016 011130000,011140000,011150000,011160000,011170000
44 2017 011180000,011190000,011200000,011210000,011220000
45 2018 011230000,011240000,011250000,011260000,011270000
46 2019 011280000,011290000,011300000,011310000,011320000
47 2020 011330000,011340000,011350000,011360000,011370000
48 2021 011380000,011390000,011400000,011410000,011420000
49 2022 011430000,011440000,011450000,011460000,011470000
50 2023 011480000,011490000,011500000,011510000,011520000
51 2024 011530000,011540000,011550000,011560000,011570000
52 2025 011580000,011590000,011600000,011610000,011620000
53 2026 011630000,011640000,011650000,011660000,011670000
54 2027 011680000,011690000,011700000,011710000,011720000
55 2028 011730000,011740000,011750000,011760000,011770000
56 2029 011780000,011790000,011800000,011810000,011820000

```

BY CLM DATE 2-9-83
 CHKD. BY LBS DATE 2-9-83

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```

57 2030 011830000,011840000,011850000,011860000,011870000
58 2031 011880000,011890000,011900000,011910000,011920000
59 2032 011930000,011940000,011950000,011960000,011970000
60 2033 011980000,011990000,013010000,013020000,013030000
61 2034 013040000,013050000,013060000,013070000,013080000
62 2035 013090000,013100000,013110000,013120000,013130000
63 2036 013140000,013150000,013160000,013170000,013180000
64 2037 013190000,013200000,013210000,013220000,013230000
65 2038 013240000,013250000,013260000,013270000,013280000
66 2039 013290000,013300000,015010000

```

```

87 *
88 *TRIPS
89 *
90 502 TIME 0 GT NULL 0 1.500 L * JOB TERMINATION TRIP
91 503 TIME 0 GE NULL 0 0.0 L * VALVE OPEN
92 504 TIME 0 GE NULL 0 5.0 L * VALVE CLOSED
93 600 502
94 *

```

75 * HYDRODYNAMIC COMPONENTS

77 * PRESSURIZER

```

80 0010000 "PRESS1" TMDPVOL
81 0010101 0.0 20.0 500.0 0.0 0.0 0.0 0.00005 0.0 11
82 0010200 2
83 0010201 0.0 2500.0 1.0 0.1 2514.0 1.0 0.3 2555.0 1.0 0.5 2600.0 1.0
84 0010202 0.7 2687.0 1.0 0.9 2700.0 1.0 1.1 2740.0 1.0 1.3 2745.0 1.0
85 0010203 1.5 2747.0 1.0 1.7 2748.0 1.0 1.9 2750.0 1.0 2.0 2750.0 1.0
86 0010204 2.5 2750.0 1.0

```

88 * LOOP SEAL GEOMETRY

```

90 0020000 "LPSL" SNGLJUN
91 0020101 001000000 003000000 0.0 0.0 0.0 1000 * THIS IS A SHORT RADIUS ELBOW LEAVING
92 0020201 1 0.0 0.0 0.0

```

```

94 0030000 "LPSL" SNGLVOL
95 0030101 0.1465 1.0 0.0 90.0 0.0 0.0 0.000151 0.0 00
96 0030200 2 2500.0 1.0

```

```

98 0040000 "LPSL" SNGLJUN
99 0040101 003010000 005000000 0.0 0.1838 0.1838 1000
100 0040201 1 0.0 0.0 0.0

```

```

102 0050000 "LPSL" PIPE
103 0050001 20
104 0050101 0.1485 20
105 0050301 0.50 10
106 0050302 0.574 20
107 0050401 0.0 20
108 0050601 -90.0 7
109 0050602 0.0 10
110 0050603 90.0 20
111 0050801 0.000151 0.0 20
112 0050901 0.0 0.0 8
113 0050902 0.1838 0.1838 7
114 0050903 0.0 0.0 8

```

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```

115 0050904 0.1838 0.1838 10
116 0050905 0 0 0.0 19
117 0051001 00 20
118 0051101 1000 19
119 0051201 3 2500.0 584.4 0.0 0.0 1
120 0051202 3 2500.0 451.1 0.0 0.0 2
121 0051203 3 2500.0 352.1 0.0 0.0 3
122 0051204 3 2500.0 278.8 0.0 0.0 4
123 0051205 3 2500.0 218.1 0.0 0.0 5
124 0051206 3 2500.0 169.3 0.0 0.0 6
125 0051207 3 2500.0 141.1 0.0 0.0 20
126 0051300 1
127 0051301 0.0 0.0 0.0 19
128 *
129 *****
130 * VALVE 6M8 CROSBY SAFETY
131 *****
132 0060000 "SRV" VALVE
133 0080101 005010000 007000000 0.022 0.0 0.0 0100
134 0060201 1 0.0 0.0 0.0
135 0060300 MTRVLV
136 0060301 503 504 100.0 0.0 * CROSBY 6M8 OPENING IN 10 MSEC
137 *
138 * DISCHARGE PIPING
139 0070000 "DISCHA1" PIPE
140 0070001 39
141 0070101 0.20069 39
142 0070301 0.526 4
143 0070302 1.094 14
144 * ARC STARTS HERE LEVEL 669-2"
145 0070303 0.94187 17
146 0070304 0.942 20
147 0070305 0.8425 23
148 0070306 0.844 26
149 0070307 0.8433 29
150 0070308 0.8333 32
151 0070309 0.8333 35
152 * ARC ENDS
153 0070310 0.91750 39
154 0070401 0.0 39
155 0070601 0.0 4
156 0070602 -90.0 14
157 0070603 0.0 39
158 0070801 0.000152 0.0 39
159 0070901 0.0 0.0 3
160 0070902 0.1800 0.1800 4
161 0070903 0.0 0.0 13
162 0070904 0.1800 0.1800 14
163 0070905 0 0 0.0 38
164 0071001 00 39
165 0071101 1000 38
166 0071201 4 14.7 120.0 0.9284 0.0 39
167 0071300 1
168 0071301 0.0 0.0 0.0 38
169 *
170 0080000 "DISCHA1" SNGLJUN
171 0080101 007010000 009000000 0.0 0.1560 0.1560 1000 *LOSSES FOR A 12 IN ELBOW
172 0080201 1 0.0 0.0 0.0

```

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```

173 *
174 * INPUT A BRANCH HERE FOR A COMPLETE MODEL
175 *
176 0090000 "DISCHA1" SNGLVOL
177 0090101 0.7771 0.5 0.0 0.0 -90.0 -0.5 0.000169 0.0 00
178 0090200 4 14.7 120.0 0.9284
179 *
180 0100000 "DISCHA1" SNGLJUN
181 0100101 00901000 011000000 0.0 0.0 0.0 1000
182 0100201 1 0.0 0.0 0.0
183 *
184 0110000 "DISCHA1" PIPE
185 0110001 99
186 0110101 0.7771 99
187 0110301 1.039 14
188 0110302 0.53025 18
189 0110303 0.5 22
190 0110304 0.53025 28
191 0110305 0.9875 58
192 0110308 0.475 68
193 0110307 0.49359 79
194 0110308 0.46875 87
195 0110309 0.51172 95
196 0110310 0.85 99
197 0110401 0.0 99
198 0110601 -90.0 14
199 0110602 -45.0 18
200 0110603 -90.0 22
201 0110604 -45.0 28
202 0110605 -90.0 58
203 0110606 0.0 87
204 0110607 -90.0 95
205 0110608 0.0 99
206 0110801 0.000169 0.0 99
207 0110901 0.0 0.0 13
208 0110902 0.078 0.078 14
209 0110903 0.0 0.0 17
210 0110904 0.078 0.078 18
211 0110905 0.0 0.0 21
212 0110908 0.078 0.078 22
213 0110907 0.0 0.0 25
214 0110908 0.078 0.078 26
215 0110909 0.0 0.0 55
216 0110910 0.158 0.158 58
217 0110911 0.0 0.0 65
218 0110912 0.158 0.158 68
219 0110913 0.0 0.0 78
220 0110914 0.158 0.158 79
221 0110915 0.0 0.0 88
222 0110918 0.158 0.158 87
223 0110917 0.0 0.0 94
224 0110918 0.158 0.158 95
225 0110919 0.0 0.0 98
226 0111001 00 99
227 0111101 1000 98
228 0111201 4 14.7 120.0 0.9284 0.0 99
229 0111300 1
230 0111301 0.0 0.0 0.0 98

```



```

231 *
232 0120000 "DISCHA1" SNGLJUN
233 0120101 011010000 013000000 0.0 0.0 0.0 1000
234 0120201 1 0.0 0.0 0.0
235 *
236 0130000 "DISCHA1" PIPE
237 0130001 30
238 0130101 0.7771 30
239 0130301 0.95 8
240 0130302 1.0 20
241 0130303 0.5 30
242 0130401 0.0 30
243 0130601 0.0 30
244 0130801 0.000169 0.0 30
245 0130901 0.0 0.0 5
246 0130902 0.156 0.156 8
247 0130903 0.0 0.0 19
248 0130904 0.156 0.156 20
249 0130905 0.0 0.0 29
250 0131001 00 30
251 0131101 1000 29
252 0131201 4 14.7 120.0 0.9284 0.0 30
253 0131300 1
254 0131301 0.0 0.0 0.0 29
255 *
256 0140000 "DISCHA1" SNGLJUN
257 0140101 013010000 015000000 0.0 0.0 0.0 0100
258 0140201 1 0.0 0.0 0.0
259 *
260 0150000 "ATMOS" TMDPVOL
261 0150101 10000.0 10000.0 0.0 0.0 0.0 0.00001 0.0 11
262 0150200 4
263 0150201 0.0 14.7 120.0 0.9284
264 *
265 * PLOT CARDS
266 *
267 20300100 QUALS 007010000
268 20300200 QUALS 005200000
269 20300300 QUALS 013200000
270 20300400 P 005200000
271 20300500 P 007010000
272 20300600 P 007380000
273 20300700 MFLOWJ 006000000
274 20300800 MFLOWJ 005070000
275 20300900 MFLOWJ 014000000
276 20301000 P 007140000
277 20301100 P 011560000
278 20301200 P 013300000
279 20301300 MFLOWJ 007140000
280 20301400 MFLOWJ 007380000
281 20301500 MFLOWJ 011560000
282 .END OF CASE

```

4.10 REPIPE Input.

These are input listings of Control Data Corporation's RELAP post-processor, REPIPE. Each set represents direction cosines of the RELAP model as well as structural node assignments. On the Unit 2 PORV model, it was necessary to break up the model in two sections because of REPIPE's size limitations.

<u>Input Set</u>	<u>Model Section</u>
4.10.1	A
4.10.2	B
4.10.3	Quarter Model

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 **TELEDYNE
ENGINEERING SERVICES**

4.10.1 Model Section A PORV Unit 2

\$PIPES
 INLINE=3,KBLOCK=200,KPIPE=10,KPLOT(1)=1,KWAVE=1,
 KPRINT=-1,KPNV=1,KSTEP=3,
 NDROPV=385010000,206330000,811190000\$

342	386000000	-0.3710	0.6786	0.6340/
340	-387010000	-0.3710	0.6786	0.6340/
339	387010000	0.0	1.0	0.0/
339	387020000	0.0	1.0	0.0/
339	387030000	0.0	1.0	0.0/
339	387040000	0.0	1.0	0.0/
339	387050000	0.0	1.0	0.0/
339	387060000	0.0	1.0	0.0/
339	387070000	0.0	1.0	0.0/
339	387080000	0.0	1.0	0.0/
339	387090000	0.0	1.0	0.0/
339	387100000	0.0	1.0	0.0/
339	387110000	0.0	1.0	0.0/
339	388000000	0.0	1.0	0.0/
339	420000000	0.0	1.0	0.0/
339	425010000	0.0	1.0	0.0/
339	425020000	0.0	1.0	0.0/
336	-387020000	0.0	1.0	0.0/
336	-387030000	0.0	1.0	0.0/
336	-387040000	0.0	1.0	0.0/
336	-387050000	0.0	1.0	0.0/
336	-387060000	0.0	1.0	0.0/
336	-387070000	0.0	1.0	0.0/
336	-387080000	0.0	1.0	0.0/
336	-387090000	0.0	1.0	0.0/
336	-387100000	0.0	1.0	0.0/
336	-387110000	0.0	1.0	0.0/
336	-388000000	0.0	1.0	0.0/
336	-420000000	0.0	1.0	0.0/
336	-498000000	0.0	1.0	0.0/
338	-425010000	0.0	1.0	0.0/
336	-425020000	0.0	1.0	0.0/
336	-425030000	0.0	1.0	0.0/
334	425030000	0.7844	0.0	0.6202/
334	425040000	0.7844	0.0	0.6202/
334	430000000	0.7844	0.0	0.6202/
330	-425040000	0.7844	0.0	0.6202/
330	-430000000	0.7844	0.0	0.6202/
330	-435010000	0.7844	0.0	0.6202/
334	435010000	0.7844	0.0	0.6202/
334	440000000	0.7844	0.0	0.6202/
334	445010000	0.7844	0.0	0.6202/
334	445020000	0.7844	0.0	0.6202/
334	445030000	0.7844	0.0	0.6202/
334	445040000	0.7844	0.0	0.6202/
330	-440000000	0.7844	0.0	0.6202/
330	-445010000	0.7844	0.0	0.6202/
330	-445020000	0.7844	0.0	0.6202/
330	-445030000	0.7844	0.0	0.6202/
330	-445040000	0.7844	0.0	0.6202/
330	-445050000	0.7844	0.0	0.6202/
328	445050000	0.0	1.0	0.0/
328	445060000	0.0	1.0	0.0/
328	445070000	0.0	1.0	0.0/
328	445080000	0.0	1.0	0.0/

BY KJG DATE 5-21-83
 CHKD. BY MR DATE 5/22/83

324	-445060000	0.0	1.0	0.0/
324	-445070000	0.0	1.0	0.0/
324	-445080000	0.0	1.0	0.0/
324	-445090000	0.0	1.0	0.0/
322	445090000	0.9138	0.0	-0.4062/
322	450000000	0.9138	0.0	-0.4062/
322	460000000	0.9138	0.0	-0.4062/
322	465010000	0.9138	0.0	-0.4062/
322	465020000	0.9138	0.0	-0.4062/
322	470000000	0.9138	0.0	-0.4062/
318	-450000000	0.9138	0.0	-0.4062/
318	-460000000	0.9138	0.0	-0.4062/
318	-491000000	0.9138	0.0	-0.4062/
318	-465010000	0.9138	0.0	-0.4062/
318	-465020000	0.9138	0.0	-0.4062/
318	-470000000	0.9138	0.0	-0.4062/
318	-475010000	0.9138	0.0	-0.4062/
318i	475010000	0.8212	0.0	-0.5707/
318i	480000000	0.8212	0.0	-0.5707/
318i	485010000	0.8212	0.0	-0.5707/
318i	485020000	0.8212	0.0	-0.5707/
318i	485030000	0.8212	0.0	-0.5707/
316	-480000000	0.8212	0.0	-0.5707/
316	-485010000	0.8212	0.0	-0.5707/
316	-485020000	0.8212	0.0	-0.5707/
316	-485030000	0.8212	0.0	-0.5707/
316	-485040000	0.8212	0.0	-0.5707/
316i	485040000	0.5557	0.0	-0.8314/
316i	485050000	0.5557	0.0	-0.8314/
316i	485060000	0.5557	0.0	-0.8314/
316i	485070000	0.5557	0.0	-0.8314/
314	-485050000	0.5557	0.0	-0.8314/
314	-485060000	0.5557	0.0	-0.8314/
314	-485070000	0.5557	0.0	-0.8314/
314	-485080000	0.5557	0.0	-0.8314/
314i	485080000	0.2178	0.0	-0.9760/
314i	485090000	0.2178	0.0	-0.9760/
314i	485100000	0.2178	0.0	-0.9760/
314i	485110000	0.2178	0.0	-0.9760/
312	-485090000	0.2178	0.0	-0.9760/
312	-485100000	0.2178	0.0	-0.9760/
312	-485110000	0.2178	0.0	-0.9760/
312	-485120000	0.2178	0.0	-0.9760/
312i	485120000	-0.1543	0.0	-0.9880/
312i	485130000	-0.1543	0.0	-0.9880/
312i	485140000	-0.1543	0.0	-0.9880/
312i	485150000	-0.1543	0.0	-0.9880/
310	-485130000	-0.1543	0.0	-0.9880/
310	-485140000	-0.1543	0.0	-0.9880/
310	-485150000	-0.1543	0.0	-0.9880/
310	-485160000	-0.1543	0.0	-0.9880/
310i	485160000	-0.9272	-0.0262	-0.3745/
308	485170000	-0.9272	-0.0262	-0.3745/
308	485180000	-0.9272	-0.0262	-0.3745/
308	485190000	-0.9272	-0.0262	-0.3745/
308	485200000	-0.9272	-0.0262	-0.3745/
308	485210000	-0.9272	-0.0262	-0.3745/
308	485220000	-0.9272	-0.0262	-0.3745/
308	485230000	-0.9272	-0.0262	-0.3745/
308	485240000	-0.9272	-0.0262	-0.3745/



308	485250000	-0.9272	-0.0262	-0.3745/
308	485260000	-0.9272	-0.0262	-0.3745/
308 1	-485170000	-0.9272	-0.0262	-0.3745/
294	-485180000	-0.9272	-0.0262	-0.3745/
294	-485190000	-0.9272	-0.0262	-0.3745/
294	-485200000	-0.9272	-0.0262	-0.3745/
294	-485210000	-0.9272	-0.0262	-0.3745/
294	-485220000	-0.9272	-0.0262	-0.3745/
294	-485230000	-0.9272	-0.0262	-0.3745/
294	-485240000	-0.9272	-0.0262	-0.3745/
294	-485250000	-0.9272	-0.0262	-0.3745/
294	-485260000	-0.9272	-0.0262	-0.3745/
294	-490000000	-0.9272	-0.0262	-0.3745/
292	490000000	-0.9272	-0.0262	-0.3745/
292	400010000	-0.9272	-0.0262	-0.3745/
292	400020000	-0.9272	-0.0262	-0.3745/
292	400030000	-0.9272	-0.0262	-0.3745/
288	-400010000	-0.9272	-0.0262	-0.3745/
288	-400020000	-0.9272	-0.0262	-0.3745/
288	-400030000	-0.9272	-0.0262	-0.3745/
288	-400040000	-0.9272	-0.0262	-0.3745/
286	400040000	0.0	-1.0	0.0/
286	400050000	0.0	-1.0	0.0/
286	400060000	0.0	-1.0	0.0/
286	400070000	0.0	-1.0	0.0/
230	-400050000	0.0	-1.0	0.0/
230	-400060000	0.0	-1.0	0.0/
230	-400070000	0.0	-1.0	0.0/
230	-401000000	0.0	-1.0	0.0/
320	491000000	0.3746	0.0185	-0.9272/
320	492010000	0.3746	0.0185	-0.9272/
320	492020000	0.3746	0.0185	-0.9272/
320	492030000	0.3746	0.0185	-0.9272/
320	492040000	0.3746	0.0185	-0.9272/
320	492050000	0.3746	0.0185	-0.9272/
320	492060000	0.3746	0.0185	-0.9272/
320	492070000	0.3746	0.0185	-0.9272/
320	492080000	0.3746	0.0185	-0.9272/
320	492090000	0.3746	0.0185	-0.9272/
320	492100000	0.3746	0.0185	-0.9272/
348	-492010000	0.3746	0.0185	-0.9272/
348	-492020000	0.3746	0.0185	-0.9272/
348	-492030000	0.3746	0.0185	-0.9272/
348	-492040000	0.3746	0.0185	-0.9272/
348	-492050000	0.3746	0.0185	-0.9272/
348	-492060000	0.3746	0.0185	-0.9272/
348	-492070000	0.3746	0.0185	-0.9272/
348	-492080000	0.3746	0.0185	-0.9272/
348	-492090000	0.3746	0.0185	-0.9272/
348	-492100000	0.3746	0.0185	-0.9272/
348	-493000000	0.3746	0.0185	-0.9272/
346	493000000	0.3746	0.0185	-0.9272/
346	600010000	0.3746	0.0185	-0.9272/
346	600020000	0.3746	0.0185	-0.9272/
344	-600010000	0.3746	0.0185	-0.9272/
344	-600020000	0.3746	0.0185	-0.9272/
344	-600030000	0.3746	0.0185	-0.9272/
404	600030000	0.0	-1.0	0.0/
404	600040000	0.0	-1.0	0.0/
404	600050000	0.0	-1.0	0.0/



404	600060000	0.0	-1.0	0.0/
240	-600040000	0.0	-1.0	0.0/
2402	-600050000	0.0	-1.0	0.0/
2402	-600060000	0.0	-1.0	0.0/
2402	-601000000	0.0	-1.0	0.0/
284	498000000	-0.9272	0.0	-0.3746/
284	410010000	-0.9272	0.0	-0.3746/
284	410020000	-0.9272	0.0	-0.3746/
284	410030000	-0.9272	0.0	-0.3746/
284	410040000	-0.9272	0.0	-0.3746/
282	-410010000	-0.9272	0.0	-0.3746/
282	-410020000	-0.9272	0.0	-0.3746/
282	-410030000	-0.9272	0.0	-0.3746/
282	-410040000	-0.9272	0.0	-0.3746/
282	-410050000	-0.9272	0.0	-0.3746/
280	410050000	0.0	1.0	0.0/
280	410060000	0.0	1.0	0.0/
280	410070000	0.0	1.0	0.0/
280	410080000	0.0	1.0	0.0/
280	410090000	0.0	1.0	0.0/
280	410100000	0.0	1.0	0.0/
278	-410060000	0.0	1.0	0.0/
278	-410070000	0.0	1.0	0.0/
278	-410080000	0.0	1.0	0.0/
278	-410090000	0.0	1.0	0.0/
278	-410100000	0.0	1.0	0.0/
278	-410110000	0.0	1.0	0.0/
276	410110000	0.9270	-0.0218	0.3745/
276	410120000	0.9270	-0.0218	0.3745/
276	410130000	0.9270	-0.0218	0.3745/
276	410140000	0.9270	-0.0218	0.3745/
276	410150000	0.9270	-0.0218	0.3745/
276	410160000	0.9270	-0.0218	0.3745/
276	410170000	0.9270	-0.0218	0.3745/
276	410180000	0.9270	-0.0218	0.3745/
276	410190000	0.9270	-0.0218	0.3745/
276	410200000	0.9270	-0.0218	0.3745/
264	-410120000	0.9270	-0.0218	0.3745/
264	-410130000	0.9270	-0.0218	0.3745/
264	-410140000	0.9270	-0.0218	0.3745/
264	-410150000	0.9270	-0.0218	0.3745/
264	-410160000	0.9270	-0.0218	0.3745/
264	-410170000	0.9270	-0.0218	0.3745/
264	-410180000	0.9270	-0.0218	0.3745/
264	-410190000	0.9270	-0.0218	0.3745/
264	-410200000	0.9270	-0.0218	0.3745/
264	-415000000	0.9270	-0.0218	0.3745/
262	415000000	0.9270	-0.0218	0.3745/
262	500010000	0.9270	-0.0218	0.3745/
262	500020000	0.9270	-0.0218	0.3745/
260	-500010000	0.9270	-0.0218	0.3745/
260	-500020000	0.9270	-0.0218	0.3745/
260	-500030000	0.9270	-0.0218	0.3745/
257	500030000	0.0	-1.0	0.0/
257	500040000	0.0	-1.0	0.0/
257	500050000	0.0	-1.0	0.0/
252	-500040000	0.0	-1.0	0.0/
252	-500050000	0.0	-1.0	0.0/
252	-500060000	0.0	-1.0	0.0/
250	500060000	0.7559	0.0	-0.6547/

248	-500070000	0.7559	0.0	-0.6547/
248 i	500070000	0.7170	0.0	-0.6971/
248 i	500080000	0.7170	0.0	-0.6971/
248 i	500090000	0.7170	0.0	-0.6971/
246	-500080000	0.7170	0.0	-0.6971/
246	-500090000	0.7170	0.0	-0.6971/
246	-500100000	0.7170	0.0	-0.6971/
246 i	500100000	0.3736	0.0	-0.9276/
246 i	500110000	0.3736	0.0	-0.9276/
246 i	500120000	0.3736	0.0	-0.9276/
244	-500110000	0.3736	0.0	-0.9276/
244	-500120000	0.3736	0.0	-0.9276/
244	-500130000	0.3736	0.0	-0.9276/
244 i	500130000	0.0282	0.0	-0.9996/
244 i	500140000	0.0282	0.0	-0.9996/
244 i	500150000	0.0282	0.0	-0.9996/
244 i	501000000	0.0282	0.0	-0.9996/
242	-500140000	0.0282	0.0	-0.9996/
242	-500150000	0.0282	0.0	-0.9996/
242	-501000000	0.0282	0.0	-0.9996/
242	-502010000	0.0282	0.0	-0.9996/
242 i	502010000	-0.2531	0.0	-0.9674/
240	-503000000	-0.2531	0.0	-0.9674/
240 i	503000000	-0.3508	0.0	-0.9364/
240 i	601000000	-0.3508	0.0	-0.9364/
238	-505000000	-0.3508	0.0	-0.9364/
238 i	505000000	-0.6395	0.0	-0.7688/
238 i	505010000	-0.6395	0.0	-0.7688/
238 i	505020000	-0.6395	0.0	-0.7688/
238 i	505030000	-0.6395	0.0	-0.7688/
236	-506010000	-0.6395	0.0	-0.7688/
236	-506020000	-0.6395	0.0	-0.7688/
236	-506030000	-0.6395	0.0	-0.7688/
236	-506040000	-0.6395	0.0	-0.7688/
236 i	506040000	-0.9576	0.0	-0.2882/
236 i	506050000	-0.9576	0.0	-0.2882/
236 i	506060000	-0.9576	0.0	-0.2882/
236 i	506070000	-0.9576	0.0	-0.2882/
234	-506050000	-0.9576	0.0	-0.2882/
234	-506060000	-0.9576	0.0	-0.2882/
234	-506070000	-0.9576	0.0	-0.2882/
234	-506080000	-0.9576	0.0	-0.2882/
234 i	506080000	-0.9998	0.0	-0.0175/
234 i	507000000	-0.9998	0.0	-0.0175/
234 i	508010000	-0.9998	0.0	-0.0175/
234 i	509000000	-0.9998	0.0	-0.0175/
234 i	511000000	-0.9998	0.0	-0.0175/
226	-507000000	-0.9998	0.0	-0.0175/
226	-508010000	-0.9998	0.0	-0.0175/
226	-509010000	-0.9998	0.0	-0.0175/
226	-511000000	-0.9998	0.0	-0.0175/
226	-700010000	-0.9998	0.0	-0.0175/
224	700010000	0.0	-1.0	0.0/
224	700020000	0.0	-1.0	0.0/
224	700030000	0.0	-1.0	0.0/
224	700040000	0.0	-1.0	0.0/
224	700050000	0.0	-1.0	0.0/
224	700060000	0.0	-1.0	0.0/
224	700070000	0.0	-1.0	0.0/
224	700080000	0.0	-1.0	0.0/

224	700090000	0.0	-1.0	0.0/
224	700100000	0.0	-1.0	0.0/
224	700110000	0.0	-1.0	0.0/
224	701000000	0.0	-1.0	0.0/
68	-700030000	0.0	-1.0	0.0/
68	-700040000	0.0	-1.0	0.0/
68	-700050000	0.0	-1.0	0.0/
68	-700060000	0.0	-1.0	0.0/
68	-700070000	0.0	-1.0	0.0/
68	-700080000	0.0	-1.0	0.0/
68	-700090000	0.0	-1.0	0.0/
68	-700100000	0.0	-1.0	0.0/
68	-700110000	0.0	-1.0	0.0/
68	-701000000	0.0	-1.0	0.0/
68	-702010000	0.0	-1.0	0.0/
224	702010000	0.0	-1.0	0.0/
224	702020000	0.0	-1.0	0.0/
224	800000000	0.0	-1.0	0.0/
224	307000000	0.0	-1.0	0.0/
224	802000000	0.0	-1.0	0.0/
224	804000000	0.0	-1.0	0.0/
224	207000000	0.0	-1.0	0.0/
224	806000000	0.0	-1.0	0.0/
224	808000000	0.0	-1.0	0.0/
224	107000000	0.0	-1.0	0.0/
224	810000000	0.0	-1.0	0.0/
224	811010000	0.0	-1.0	0.0/
224	811020000	0.0	-1.0	0.0/
224	811030000	0.0	-1.0	0.0/
224	811040000	0.0	-1.0	0.0/
224	811050000	0.0	-1.0	0.0/
224	811060000	0.0	-1.0	0.0/
224	811070000	0.0	-1.0	0.0/
224	811080000	0.0	-1.0	0.0/
224	811090000	0.0	-1.0	0.0/
224	811100000	0.0	-1.0	0.0/
224	811110000	0.0	-1.0	0.0/
224	811120000	0.0	-1.0	0.0/
224	811130000	0.0	-1.0	0.0/
68	-700020000	0.0	-1.0	0.0/
68	-800000000	0.0	-1.0	0.0/
68	-802000000	0.0	-1.0	0.0/
68	-804000000	0.0	-1.0	0.0/
68	-806000000	0.0	-1.0	0.0/
68	-808000000	0.0	-1.0	0.0/
68	-810000000	0.0	-1.0	0.0/
68	-811010000	0.0	-1.0	0.0/
68	-811020000	0.0	-1.0	0.0/
68	-811030000	0.0	-1.0	0.0/
68	-811040000	0.0	-1.0	0.0/
68	-811050000	0.0	-1.0	0.0/
68	-811060000	0.0	-1.0	0.0/
68	-811070000	0.0	-1.0	0.0/
68	-811080000	0.0	-1.0	0.0/
68	-811090000	0.0	-1.0	0.0/
68	-811100000	0.0	-1.0	0.0/
68	-811110000	0.0	-1.0	0.0/
68	-811120000	0.0	-1.0	0.0/
68	-811130000	0.0	-1.0	0.0/
68	-811140000	0.0	-1.0	0.0/



68	811140000	-0.2356	-0.7071	0.6667/
68	811150000	-0.2356	-0.7071	0.6667/
66	811160000	-0.2356	-0.7071	0.6667/
66	811170000	-0.2356	-0.7071	0.6667/
64	-811150000	-0.2356	-0.7071	0.6667/
64	-811160000	-0.2356	-0.7071	0.6667/
64	-811170000	-0.2356	-0.7071	0.6667/
64	-811180000	-0.2356	-0.7071	0.6667/
198	305000000	-0.9975	0.0	0.0709/
198	306010000	-0.9975	0.0	0.0709/
198	306020000	-0.9975	0.0	0.0709/
198	306030000	-0.9975	0.0	0.0709/
195	-306010000	-0.9975	0.0	0.0709/
195	-306020000	-0.9975	0.0	0.0709/
195	-306030000	-0.9975	0.0	0.0709/
195	-306040000	-0.9975	0.0	0.0709/
190	306040000	0.0	-1.0	0.0/
190	306050000	0.0	-1.0	0.0/
190	306060000	0.0	-1.0	0.0/
190	306070000	0.0	-1.0	0.0/
190	306080000	0.0	-1.0	0.0/
190	306090000	0.0	-1.0	0.0/
190	306100000	0.0	-1.0	0.0/
190	306110000	0.0	-1.0	0.0/
186	-306050000	0.0	-1.0	0.0/
186	-306060000	0.0	-1.0	0.0/
186	-306070000	0.0	-1.0	0.0/
186	-306080000	0.0	-1.0	0.0/
186	-306090000	0.0	-1.0	0.0/
186	-306100000	0.0	-1.0	0.0/
186	-306110000	0.0	-1.0	0.0/
186	-306120000	0.0	-1.0	0.0/
184	306120000	-0.9359	0.0	-0.3523/
184	306130000	-0.9359	0.0	-0.3523/
184	306140000	-0.9359	0.0	-0.3523/
182	-306130000	-0.9359	0.0	-0.3523/
182	-306140000	-0.9359	0.0	-0.3523/
182	-306150000	-0.9359	0.0	-0.3523/
182 i	306150000	-0.6354	0.0	-0.7722/
182 i	306160000	-0.6354	0.0	-0.7722/
182 i	306170000	-0.6354	0.0	-0.7722/
180	-306160000	-0.6354	0.0	-0.7722/
180	-306170000	-0.6354	0.0	-0.7722/
180	-306180000	-0.6354	0.0	-0.7722/
180 i	306180000	-0.0516	0.0	-0.9987/
180 i	306190000	-0.0516	0.0	-0.9987/
180 i	306200000	-0.0516	0.0	-0.9987/
178	-306190000	-0.0516	0.0	-0.9987/
178	-306200000	-0.0516	0.0	-0.9987/
178	-306210000	-0.0516	0.0	-0.9987/
178 i	306210000	0.2639	0.0	-0.9645/
178 i	306220000	0.2639	0.0	-0.9645/
178 i	306230000	0.2639	0.0	-0.9645/
178 i	306240000	0.2639	0.0	-0.9645/
176	-306220000	0.2639	0.0	-0.9645/
176	-306230000	0.2639	0.0	-0.9645/
176	-306240000	0.2639	0.0	-0.9645/
176	-307000000	0.2639	0.0	-0.9645/
104	105000000	0.7169	0.0	0.6972/
104	106010000	0.7169	0.0	0.6972/

104	106020000	0.7169	0.0	0.6972/
104	106030000	0.7169	0.0	0.6972/
98	-106010000	0.7169	0.0	0.6972/
98	-106020000	0.7169	0.0	0.6972/
98	-106030000	0.7169	0.0	0.6972/
98	-106040000	0.7169	0.0	0.6972/
96	106040000	0.0	-1.0	0.0/
96	106050000	0.0	-1.0	0.0/
96	106060000	0.0	-1.0	0.0/
96	106070000	0.0	-1.0	0.0/
96	106080000	0.0	-1.0	0.0/
96	106090000	0.0	-1.0	0.0/
96	106100000	0.0	-1.0	0.0/
96	106110000	0.0	-1.0	0.0/
96	106120000	0.0	-1.0	0.0/
96	106130000	0.0	-1.0	0.0/
90	-106050000	0.0	-1.0	0.0/
90	-106060000	0.0	-1.0	0.0/
90	-106070000	0.0	-1.0	0.0/
90	-106080000	0.0	-1.0	0.0/
90	-106090000	0.0	-1.0	0.0/
90	-106100000	0.0	-1.0	0.0/
90	-106110000	0.0	-1.0	0.0/
90	-106120000	0.0	-1.0	0.0/
90	-106130000	0.0	-1.0	0.0/
90	-106140000	0.0	-1.0	0.0/
88	106140000	0.2657	0.0	0.9641/
88	106150000	0.2657	0.0	0.9641/
88	106160000	0.2657	0.0	0.9641/
86	-106150000	0.2657	0.0	0.9641/
86	-106160000	0.2657	0.0	0.9641/
86	-106170000	0.2657	0.0	0.9641/
861	106170000	-0.3889	0.0	0.9213/
861	106180000	-0.3889	0.0	0.9213/
861	106190000	-0.3889	0.0	0.9213/
84	-106180000	-0.3889	0.0	0.9213/
84	-106190000	-0.3889	0.0	0.9213/
84	-106200000	-0.3889	0.0	0.9213/
841	106200000	-0.8464	0.0	0.5326/
841	106210000	-0.8464	0.0	0.5326/
841	106220000	-0.8464	0.0	0.5326/
82	-106210000	-0.8464	0.0	0.5326/
82	-106220000	-0.8464	0.0	0.5326/
82	-106230000	-0.8464	0.0	0.5326/
821	106230000	-0.9999	0.0	0.0162/
821	106240000	-0.9999	0.0	0.0162/
821	106250000	-0.9999	0.0	0.0162/
80	-106240000	-0.9999	0.0	0.0162/
80	-106250000	-0.9999	0.0	0.0162/
80	-106260000	-0.9999	0.0	0.0162/
801	106260000	-0.8289	0.0	-0.5595/
801	106270000	-0.8289	0.0	-0.5595/
801	106280000	-0.8289	0.0	-0.5595/
78	-106270000	-0.8289	0.0	-0.5595/
78	-106280000	-0.8289	0.0	-0.5595/
78	-106290000	-0.8289	0.0	-0.5595/
781	106290000	-0.4813	0.0	-0.8766/
781	106300000	-0.4813	0.0	-0.8766/
781	106310000	-0.4813	0.0	-0.8766/
78	-106300000	-0.4813	0.0	-0.8766/

76	-106310000	-0.4813	0.0	-0.8766/
76	-106320000	-0.4813	0.0	-0.8766/
761	106320000	-0.2356	-0.7071	0.6667/
781	106330000	-0.2356	-0.7071	0.6667/
761	106340000	-0.2356	-0.7071	0.6667/
74	-106330000	-0.2356	-0.7071	0.6667/
74	-106340000	-0.2356	-0.7071	0.6667/
74	-106350000	-0.2356	-0.7071	0.6667/
741	106350000	0.2639	0.0	-0.9645/
741	106360000	0.2639	0.0	-0.9645/
741	106370000	0.2639	0.0	-0.9645/
741	106380000	0.2639	0.0	-0.9645/
72	-106360000	0.2639	0.0	-0.9645/
72	-106370000	0.2639	0.0	-0.9645/
72	-106380000	0.2639	0.0	-0.9645/
72	-107000000	0.2639	0.0	-0.9645/

99999/

\$STEPS TSTEP(1)=0.001,0.200,-1,-1\$

Technical Report
TR-5364-2
Revision 0

4-271

 **TELEDYNE
ENGINEERING SERVICES**

4.10.2 Model Section B PORV Unit 2

\$PIPES
 INLINE=3,KBLOCK=200,KPIPE=10,KPLOT(1)=1,KWAVE=1,
 KPRINT=-1,KPNV=1,KSTEP=3,
 NDR0PV=206010000,903030000,805010000,811180000\$

154	206010000	-0.4181	0.0	0.9084/
154	206020000	-0.4181	0.0	0.9084/
154	206030000	-0.4181	0.0	0.9084/
148	-206020000	-0.4181	0.0	0.9084/
148	-206030000	-0.4181	0.0	0.9084/
148	-206040000	-0.4181	0.0	0.9084/
146	206040000	0.0	-1.0	0.0/
146	206050000	0.0	-1.0	0.0/
146	206060000	0.0	-1.0	0.0/
146	206070000	0.0	-1.0	0.0/
146	206080000	0.0	-1.0	0.0/
146	206090000	0.0	-1.0	0.0/
146	206100000	0.0	-1.0	0.0/
148	206110000	0.0	-1.0	0.0/
148	206120000	0.0	-1.0	0.0/
148	206130000	0.0	-1.0	0.0/
140	-206050000	0.0	-1.0	0.0/
140	-206060000	0.0	-1.0	0.0/
140	-206070000	0.0	-1.0	0.0/
140	-206080000	0.0	-1.0	0.0/
140	-206090000	0.0	-1.0	0.0/
140	-206100000	0.0	-1.0	0.0/
140	-206110000	0.0	-1.0	0.0/
140	-206120000	0.0	-1.0	0.0/
140	-206130000	0.0	-1.0	0.0/
140	-206140000	0.0	-1.0	0.0/
138	206140000	-0.8064	0.0	0.5913/
138	206150000	-0.8064	0.0	0.5913/
138	206160000	-0.8064	0.0	0.5913/
138	-206150000	-0.8064	0.0	0.5913/
136	-206160000	-0.8064	0.0	0.5913/
136	-206170000	-0.8064	0.0	0.5913/
136.1	206170000	-0.9998	0.0	0.0191/
136.1	206180000	-0.9998	0.0	0.0191/
136.1	206190000	-0.9998	0.0	0.0191/
134	-206180000	-0.9998	0.0	0.0191/
134	-206190000	-0.9998	0.0	0.0191/
134	-206200000	-0.9998	0.0	0.0191/
134.1	206200000	-0.8285	0.0	-0.5599/
134.1	206210000	-0.8285	0.0	-0.5599/
134.1	206220000	-0.8285	0.0	-0.5599/
132	-206210000	-0.8285	0.0	-0.5599/
132	-206220000	-0.8285	0.0	-0.5599/
132	-206230000	-0.8285	0.0	-0.5599/
132.1	206230000	-0.4217	0.0	-0.9067/
132.1	206240000	-0.4217	0.0	-0.9067/
132.1	206250000	-0.4217	0.0	-0.9067/
130	-206240000	-0.4217	0.0	-0.9067/
130	-206250000	-0.4217	0.0	-0.9067/
130	-206260000	-0.4217	0.0	-0.9067/
130.1	206260000	0.0323	0.0	-0.9995/
130.1	206270000	0.0323	0.0	-0.9995/
130.1	206280000	0.0323	0.0	-0.9995/
128	-206270000	0.0323	0.0	-0.9995/
128	-206280000	0.0323	0.0	-0.9995/

BY KJG DATE 5-21-83
 CHKD. BY MIL DATE 5-26-83

128	-206290000	0.0323	0.0	-0.9995/
1281	206290000	0.2639	0.0	-0.9645/
1281	206300000	0.2639	0.0	-0.9645/
1281	206310000	0.2639	0.0	-0.9645/
1231	206320000	0.2639	0.0	-0.9645/
126	-206300000	0.2639	0.0	-0.9645/
126	-206310000	0.2639	0.0	-0.9645/
126	-206320000	0.2639	0.0	-0.9645/
126	-207000000	0.2639	0.0	-0.9645/
62	811180000	0.0	-1.0	0.0/
62	811190000	0.0	-1.0	0.0/
62	811200000	0.0	-1.0	0.0/
62	811210000	0.0	-1.0	0.0/
58	-811190000	0.0	-1.0	0.0/
58	-811200000	0.0	-1.0	0.0/
58	-811210000	0.0	-1.0	0.0/
58	-811220000	0.0	-1.0	0.0/
58	811220000	0.2356	-0.7071	-0.6667/
56	811230000	0.2356	-0.7071	-0.6667/
56	811240000	0.2356	-0.7071	-0.6667/
56	811250000	0.2356	-0.7071	-0.6667/
54	-811230000	0.2356	-0.7071	-0.6667/
54	-811240000	0.2356	-0.7071	-0.6667/
54	-811250000	0.2356	-0.7071	-0.6667/
54	-811260000	0.2356	-0.7071	-0.6667/
52	811260000	0.0	-1.0	0.0/
52	811270000	0.0	-1.0	0.0/
52	811280000	0.0	-1.0	0.0/
52	811290000	0.0	-1.0	0.0/
52	811300000	0.0	-1.0	0.0/
52	811310000	0.0	-1.0	0.0/
52	811320000	0.0	-1.0	0.0/
52	811330000	0.0	-1.0	0.0/
52	811340000	0.0	-1.0	0.0/
52	811350000	0.0	-1.0	0.0/
52	811360000	0.0	-1.0	0.0/
52	811370000	0.0	-1.0	0.0/
52	811380000	0.0	-1.0	0.0/
52	811390000	0.0	-1.0	0.0/
52	811400000	0.0	-1.0	0.0/
52	811410000	0.0	-1.0	0.0/
52	811420000	0.0	-1.0	0.0/
52	811430000	0.0	-1.0	0.0/
52	811440000	0.0	-1.0	0.0/
52	811450000	0.0	-1.0	0.0/
52	811460000	0.0	-1.0	0.0/
52	811470000	0.0	-1.0	0.0/
52	811480000	0.0	-1.0	0.0/
52	811490000	0.0	-1.0	0.0/
52	811500000	0.0	-1.0	0.0/
52	811510000	0.0	-1.0	0.0/
52	811520000	0.0	-1.0	0.0/
52	811530000	0.0	-1.0	0.0/
52	811540000	0.0	-1.0	0.0/
52	811550000	0.0	-1.0	0.0/
46	-811270000	0.0	-1.0	0.0/
46	-811280000	0.0	-1.0	0.0/
46	-811290000	0.0	-1.0	0.0/
46	-811300000	0.0	-1.0	0.0/
46	-811310000	0.0	-1.0	0.0/



48	-811320000	0.0	-1.0	0.0/
46	-811330000	0.0	-1.0	0.0/
46	-811340000	0.0	-1.0	0.0/
46	-811350000	0.0	-1.0	0.0/
46	-811360000	0.0	-1.0	0.0/
46	-811370000	0.0	-1.0	0.0/
46	-811380000	0.0	-1.0	0.0/
46	-811390000	0.0	-1.0	0.0/
46	-811400000	0.0	-1.0	0.0/
46	-811410000	0.0	-1.0	0.0/
46	-811420000	0.0	-1.0	0.0/
46	-811430000	0.0	-1.0	0.0/
46	-811440000	0.0	-1.0	0.0/
46	-811450000	0.0	-1.0	0.0/
46	-811460000	0.0	-1.0	0.0/
46	-811470000	0.0	-1.0	0.0/
46	-811480000	0.0	-1.0	0.0/
46	-811490000	0.0	-1.0	0.0/
46	-811500000	0.0	-1.0	0.0/
46	-811510000	0.0	-1.0	0.0/
46	-811520000	0.0	-1.0	0.0/
46	-811530000	0.0	-1.0	0.0/
46	-811540000	0.0	-1.0	0.0/
46	-811550000	0.0	-1.0	0.0/
46	-811560000	0.0	-1.0	0.0/
44	811560000	0.0	0.0	-1.0/
44	811570000	0.0	0.0	-1.0/
44	811580000	0.0	0.0	-1.0/
44	811590000	0.0	0.0	-1.0/
44	811600000	0.0	0.0	-1.0/
44	811610000	0.0	0.0	-1.0/
44	811620000	0.0	0.0	-1.0/
44	811630000	0.0	0.0	-1.0/
44	811640000	0.0	0.0	-1.0/
44	811650000	0.0	0.0	-1.0/
42	-811570000	0.0	0.0	-1.0/
42	-811580000	0.0	0.0	-1.0/
42	-811590000	0.0	0.0	-1.0/
42	-811600000	0.0	0.0	-1.0/
42	-811610000	0.0	0.0	-1.0/
42	-811620000	0.0	0.0	-1.0/
42	-811630000	0.0	0.0	-1.0/
42	-811640000	0.0	0.0	-1.0/
42	-811650000	0.0	0.0	-1.0/
42	-811660000	0.0	0.0	-1.0/
40	811660000	0.2588	0.0	-0.9659/
40	811670000	0.2588	0.0	-0.9659/
40	811680000	0.2588	0.0	-0.9659/
40	811690000	0.2588	0.0	-0.9659/
40	811700000	0.2588	0.0	-0.9659/
40	811710000	0.2588	0.0	-0.9659/
40	811720000	0.2588	0.0	-0.9659/
40	811730000	0.2588	0.0	-0.9659/
40	811740000	0.2588	0.0	-0.9659/
40	811750000	0.2588	0.0	-0.9659/
40	811760000	0.2588	0.0	-0.9659/
40	811770000	0.2588	0.0	-0.9659/
40	811780000	0.2588	0.0	-0.9659/
38	-811670000	0.2588	0.0	-0.9659/
38	-811680000	0.2588	0.0	-0.9659/

38	-811690000	0.2588	0.0	-0.9659/
38	-811700000	0.2588	0.0	-0.9659/
38	-811710000	0.2588	0.0	-0.9659/
38	-811720000	0.2588	0.0	-0.9659/
38	-811730000	0.2588	0.0	-0.9659/
38	-811740000	0.2588	0.0	-0.9659/
38	-811750000	0.2588	0.0	-0.9659/
38	-811760000	0.2588	0.0	-0.9659/
38	-811770000	0.2588	0.0	-0.9659/
38	-811780000	0.2588	0.0	-0.9659/
38	-811790000	0.2588	0.0	-0.9659/
38	811790000	1.0	0.0	0.0/
36	811800000	1.0	0.0	0.0/
36	811810000	1.0	0.0	0.0/
36	811820000	1.0	0.0	0.0/
38	811830000	1.0	0.0	0.0/
36	811840000	1.0	0.0	0.0/
36	811850000	1.0	0.0	0.0/
36	811860000	1.0	0.0	0.0/
34	-811800000	1.0	0.0	0.0/
34	-811810000	1.0	0.0	0.0/
34	-811820000	1.0	0.0	0.0/
34	-811830000	1.0	0.0	0.0/
34	-811840000	1.0	0.0	0.0/
34	-811850000	1.0	0.0	0.0/
34	-811860000	1.0	0.0	0.0/
34	-811870000	1.0	0.0	0.0/
33	811870000	0.0	-1.0	0.0/
33	811880000	0.0	-1.0	0.0/
33	811890000	0.0	-1.0	0.0/
33	811900000	0.0	-1.0	0.0/
33	811910000	0.0	-1.0	0.0/
33	811920000	0.0	-1.0	0.0/
33	811930000	0.0	-1.0	0.0/
33	811940000	0.0	-1.0	0.0/
28	-811880000	0.0	-1.0	0.0/
28	-811890000	0.0	-1.0	0.0/
28	-811900000	0.0	-1.0	0.0/
28	-811910000	0.0	-1.0	0.0/
28	-811920000	0.0	-1.0	0.0/
28	-811930000	0.0	-1.0	0.0/
28	-811940000	0.0	-1.0	0.0/
28	-811950000	0.0	-1.0	0.0/
26	811950000	1.0	0.0	0.0/
26	811960000	1.0	0.0	0.0/
26	811970000	1.0	0.0	0.0/
26	811980000	1.0	0.0	0.0/
26	812000000	1.0	0.0	0.0/
26	813010000	1.0	0.0	0.0/
26	813020000	1.0	0.0	0.0/
26	813030000	1.0	0.0	0.0/
26	813040000	1.0	0.0	0.0/
26	813050000	1.0	0.0	0.0/
20	-811960000	1.0	0.0	0.0/
20	-811970000	1.0	0.0	0.0/
20	-811980000	1.0	0.0	0.0/
20	-812000000	1.0	0.0	0.0/
20	-813010000	1.0	0.0	0.0/
20	-813020000	1.0	0.0	0.0/
20	-813030000	1.0	0.0	0.0/

20	-813040000	1.0	0.0	0.0/
20	-813050000	1.0	0.0	0.0/
20	-813060000	1.0	0.0	0.0/
18	813060000	0.0	0.0	1.0/
18	813070000	0.0	0.0	1.0/
18	813080000	0.0	0.0	1.0/
18	813090000	0.0	0.0	1.0/
18	813100000	0.0	0.0	1.0/
18	813110000	0.0	0.0	1.0/
18	813120000	0.0	0.0	1.0/
18	813130000	0.0	0.0	1.0/
18	813140000	0.0	0.0	1.0/
18	813150000	0.0	0.0	1.0/
18	813160000	0.0	0.0	1.0/
18	813170000	0.0	0.0	1.0/
18	813180000	0.0	0.0	1.0/
18	813190000	0.0	0.0	1.0/
12	-813070000	0.0	0.0	1.0/
12	-813080000	0.0	0.0	1.0/
12	-813090000	0.0	0.0	1.0/
12	-813100000	0.0	0.0	1.0/
12	-813110000	0.0	0.0	1.0/
12	-813120000	0.0	0.0	1.0/
12	-813130000	0.0	0.0	1.0/
12	-813140000	0.0	0.0	1.0/
12	-813150000	0.0	0.0	1.0/
12	-813160000	0.0	0.0	1.0/
12	-813170000	0.0	0.0	1.0/
12	-813180000	0.0	0.0	1.0/
12	-813190000	0.0	0.0	1.0/
12	-813200000	0.0	0.0	1.0/
10	813200000	-1.0	0.0	0.0/
10	813210000	-1.0	0.0	0.0/
10	813220000	-1.0	0.0	0.0/
10	813230000	-1.0	0.0	0.0/
10	813240000	-1.0	0.0	0.0/
10	813250000	-1.0	0.0	0.0/
10	813260000	-1.0	0.0	0.0/
10	813270000	-1.0	0.0	0.0/
10	813280000	-1.0	0.0	0.0/
10	813290000	-1.0	0.0	0.0/
8	-813210000	-1.0	0.0	0.0/
8	-813220000	-1.0	0.0	0.0/
8	-813230000	-1.0	0.0	0.0/
8	-813240000	-1.0	0.0	0.0/
8	-813250000	-1.0	0.0	0.0/
8	-813260000	-1.0	0.0	0.0/
8	-813270000	-1.0	0.0	0.0/
8	-813280000	-1.0	0.0	0.0/
8	-813290000	-1.0	0.0	0.0/
6	-813300000	-1.0	0.0	0.0/
4	900000000	0.0	-1.0	0.0/
4	901010000	0.0	-1.0	0.0/
4	901020000	0.0	-1.0	0.0/
4	902000000	0.0	-1.0	0.0/
4	903010000	0.0	-1.0	0.0/
2	-901010000	0.0	-1.0	0.0/
2	-902000000	0.0	-1.0	0.0/
2	-903010000	0.0	-1.0	0.0/
2	-903020000	0.0	-1.0	0.0/

89989/
\$STEPS TSTEP(1)=0.001, 1.0, -1, -1\$

[The remainder of the page contains extremely faint and illegible text, likely a technical report or code listing.]

Technical Report
TR-5364-2
Revision 0

4.10.3 Quarter Model

\$PIPES
INLINE=3,KBLOCK=601,KPIPE=0,KPLOT(1)=1,KWAVE=1,
KPRINT=-1,KPNV=1,KSTEP=3,NDROPV=1010000,15010000\$

1	002000000	-1.0	0.0	0.0/
2	-004000000	-1.0	0.0	0.0/
3	004000000	0.0	-1.0	0.0/
3	005010000	0.0	-1.0	0.0/
3	005020000	0.0	-1.0	0.0/
3	005040000	0.0	-1.0	0.0/
3	005050000	0.0	-1.0	0.0/
3	005060000	0.0	-1.0	0.0/
4	-005010000	0.0	-1.0	0.0/
4	-005020000	0.0	-1.0	0.0/
4	-005030000	0.0	-1.0	0.0/
4	-005040000	0.0	-1.0	0.0/
4	-005050000	0.0	-1.0	0.0/
4	-005060000	0.0	-1.0	0.0/
4	-005070000	0.0	-1.0	0.0/
5	005070000	-1.0	0.0	0.0/
5	005080000	-1.0	0.0	0.0/
5	005090000	-1.0	0.0	0.0/
6	-005080000	-1.0	0.0	0.0/
6	-005090000	-1.0	0.0	0.0/
6	-005100000	-1.0	0.0	0.0/
7	005100000	0.0	1.0	0.0/
7	005110000	0.0	1.0	0.0/
7	005120000	0.0	1.0	0.0/
7	005130000	0.0	1.0	0.0/
7	005140000	0.0	1.0	0.0/
7	005150000	0.0	1.0	0.0/
7	005160000	0.0	1.0	0.0/
7	005170000	0.0	1.0	0.0/
7	005180000	0.0	1.0	0.0/
7	005190000	0.0	1.0	0.0/
8	-005110000	0.0	1.0	0.0/
8	-005120000	0.0	1.0	0.0/
8	-005130000	0.0	1.0	0.0/
8	-005140000	0.0	1.0	0.0/
8	-005150000	0.0	1.0	0.0/
8	-005160000	0.0	1.0	0.0/
8	-005170000	0.0	1.0	0.0/
8	-005180000	0.0	1.0	0.0/
8	-005190000	0.0	1.0	0.0/
8	-008000000	0.0	1.0	0.0/
9	008000000	-1.0	0.0	0.0/
9	007010000	-1.0	0.0	0.0/
9	007020000	-1.0	0.0	0.0/
9	007030000	-1.0	0.0	0.0/
10	-007010000	-1.0	0.0	0.0/
10	-007020000	-1.0	0.0	0.0/
10	-007030000	-1.0	0.0	0.0/
10	-007040000	-1.0	0.0	0.0/
11	007040000	0.0	-1.0	0.0/
11	007050000	0.0	-1.0	0.0/
11	007080000	0.0	-1.0	0.0/
11	007070000	0.0	-1.0	0.0/
11	007080000	0.0	-1.0	0.0/
11	007090000	0.0	-1.0	0.0/
11	007100000	0.0	-1.0	0.0/
11	007110000	0.0	-1.0	0.0/

BY CAIM DATE 2-9-83
CHKD. BY LOS DATE 2-9-83

11	007120000	0 0	-1.0	0.0/
11	007130000	0.0	-1.0	0.0/
12	-007050000	0.0	-1.0	0.0/
12	-007060000	0.0	-1.0	0.0/
12	-007070000	0.0	-1.0	0.0/
12	-007080000	0.0	-1.0	0.0/
12	-007090000	0.0	-1.0	0.0/
12	-007100000	0.0	-1.0	0.0/
12	-007110000	0.0	-1.0	0.0/
12	-007120000	0.0	-1.0	0.0/
12	-007130000	0.0	-1.0	0.0/
12	-007140000	0.0	-1.0	0.0/
14	007140000	-.258	0.0	-.966/
14	007150000	-.258	0.0	-.966/
14	007160000	-.258	0.0	-.968/
15	-007150000	-.258	0.0	-.966/
15	-007160000	-.258	0.0	-.966/
15	-007170000	-.258	0.0	-.968/
16	007170000	.337	0.0	-.942/
16	007180000	.337	0.0	-.942/
16	007190000	.337	0.0	-.942/
17	-007180000	.337	0.0	-.942/
17	-007190000	.337	0.0	-.942/
17	-007200000	.337	0.0	-.942/
18	007200000	.793	0.0	-.609/
18	007210000	.793	0.0	-.609/
18	007220000	.793	0.0	-.609/
19	-007210000	.793	0.0	-.609/
19	-007220000	.793	0.0	-.609/
19	-007230000	.793	0.0	-.609/
20	007230000	.994	0.0	-.1132/
20	007240000	.994	0.0	-.1132/
20	007250000	.994	0.0	-.1132/
21	-007240000	.994	0.0	-.1132/
21	-007250000	.994	0.0	-.1132/
21	-007260000	.994	0.0	-.1132/
22	007260000	.910	0.0	.415/
22	007270000	.910	0.0	.415/
22	007280000	.910	0.0	.415/
23	-007270000	.910	0.0	.415/
23	-007280000	.910	0.0	.415/
23	-007290000	.910	0.0	.415/
24	007290000	.555	0.0	.8321/
24	007300000	.555	0.0	.8321/
24	007310000	.555	0.0	.8321/
25	-007300000	.555	0.0	.8321/
25	-007310000	.555	0.0	.8321/
25	-007320000	.555	0.0	.8321/
26	007320000	.0183	0.0	.9998/
26	007330000	.0183	0.0	.9998/
26	007340000	.0183	0.0	.9998/
27	-007330000	.0183	0.0	.9998/
27	-007340000	.0183	0.0	.9998/
27	-007350000	.0183	0.0	.9998/
28	007350000	-.264	0.0	.965/
28	007360000	-.264	0.0	.965/
28	007370000	-.264	0.0	.965/
28	007380000	-.264	0.0	.965/
28	-007360000	-.264	0.0	.965/
28	-007370000	-.264	0.0	.965/

29	-007380000	-.264	0.0	.965/
29	-008000000	-.264	0.0	.965/
30	008000000	0.0	-1.0	0.0/
30	010000000	0.0	-1.0	0.0/
30	011010000	0.0	-1.0	0.0/
30	011020000	0.0	-1.0	0.0/
30	011030000	0.0	-1.0	0.0/
30	011040000	0.0	-1.0	0.0/
30	011050000	0.0	-1.0	0.0/
30	011060000	0.0	-1.0	0.0/
30	011070000	0.0	-1.0	0.0/
30	011080000	0.0	-1.0	0.0/
30	011090000	0.0	-1.0	0.0/
30	011100000	0.0	-1.0	0.0/
30	011110000	0.0	-1.0	0.0/
30	011120000	0.0	-1.0	0.0/
30	011130000	0.0	-1.0	0.0/
31	-010000000	0.0	-1.0	0.0/
31	-011010000	0.0	-1.0	0.0/
31	-011020000	0.0	-1.0	0.0/
31	-011030000	0.0	-1.0	0.0/
31	-011040000	0.0	-1.0	0.0/
31	-011050000	0.0	-1.0	0.0/
31	-011060000	0.0	-1.0	0.0/
31	-011070000	0.0	-1.0	0.0/
31	-011080000	0.0	-1.0	0.0/
31	-011090000	0.0	-1.0	0.0/
31	-011100000	0.0	-1.0	0.0/
31	-011110000	0.0	-1.0	0.0/
31	-011120000	0.0	-1.0	0.0/
31	-011130000	0.0	-1.0	0.0/
31	-011140000	0.0	-1.0	0.0/
32	011140000	.316	-.707	-.948/
32	011150000	.316	-.707	-.948/
32	011160000	.316	-.707	-.948/
32	011170000	.318	-.707	-.948/
33	-011150000	.318	-.707	-.948/
33	-011160000	.318	-.707	-.948/
33	-011170000	.318	-.707	-.948/
33	-011180000	.318	-.707	-.948/
34	011180000	0.0	-1.0	0.0/
34	011190000	0.0	-1.0	0.0/
34	011200000	0.0	-1.0	0.0/
34	011210000	0.0	-1.0	0.0/
35	-011200000	0.0	-1.0	0.0/
35	-011210000	0.0	-1.0	0.0/
35	-011220000	0.0	-1.0	0.0/
36	011220000	-.316	-.707	.948/
36	011230000	-.316	-.707	.948/
36	011240000	-.316	-.707	.948/
36	011250000	-.316	-.707	.948/
37	-011230000	-.316	-.707	.948/
37	-011240000	-.316	-.707	.948/
37	-011250000	-.318	-.707	.948/
37	-011260000	-.318	-.707	.948/
38	011260000	0.0	-1.0	0.0/
38	011270000	0.0	-1.0	0.0/
38	011280000	0.0	-1.0	0.0/
38	011290000	0.0	-1.0	0.0/
38	011300000	0.0	-1.0	0.0/



38	011310000	0.0	-1.0	0.0/
38	011320000	0.0	-1.0	0.0/
38	011330000	0.0	-1.0	0.0/
38	011340000	0.0	-1.0	0.0/
38	011350000	0.0	-1.0	0.0/
38	011360000	0.0	-1.0	0.0/
38	011370000	0.0	-1.0	0.0/
38	011380000	0.0	-1.0	0.0/
38	011390000	0.0	-1.0	0.0/
38	011400000	0.0	-1.0	0.0/
38	011410000	0.0	-1.0	0.0/
38	011420000	0.0	-1.0	0.0/
38	011430000	0.0	-1.0	0.0/
38	011440000	0.0	-1.0	0.0/
38	011450000	0.0	-1.0	0.0/
38	011460000	0.0	-1.0	0.0/
38	011470000	0.0	-1.0	0.0/
38	011480000	0.0	-1.0	0.0/
38	011490000	0.0	-1.0	0.0/
38	011500000	0.0	-1.0	0.0/
38	011510000	0.0	-1.0	0.0/
38	011520000	0.0	-1.0	0.0/
38	011530000	0.0	-1.0	0.0/
38	011540000	0.0	-1.0	0.0/
38	011550000	0.0	-1.0	0.0/
39	-011270000	0.0	-1.0	0.0/
39	-011280000	0.0	-1.0	0.0/
39	-011290000	0.0	-1.0	0.0/
39	-011300000	0.0	-1.0	0.0/
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39	-011330000	0.0	-1.0	0.0/
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39	-011370000	0.0	-1.0	0.0/
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40	011590000	0.0	0.0	-1.0/
40	011600000	0.0	0.0	-1.0/

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52	013250000	1.0	0.0	0.0/
52	013260000	1.0	0.0	0.0/
52	013270000	1.0	0.0	0.0/
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53	-014000000	1.0	0.0	0.0/

99999/
\$STEPS TSTEP(1)=0.001,0.600\$



Technical Report
TR-5364-2
Revision 0

4-286

 **TELEDYNE
ENGINEERING SERVICES**

4.11 APPENDIX A

TELEDYNE ENGINEERING SERVICES

BY SM DATE 8-24-82
 CHKD. BY JGC DATE 8-25-82
SM 6-1-83

AMERICAN ELECTRIC POWER
 D.C. COOK UNITS 1 & 2
 PIPE PROPERTIES

SHEET NO. 1 OF 1
 PROJ. NO. 5364

PIPE PROPERTIES

SIZE	SCHEDULE	I. D. (in.)	FLOW AREA (ft ²)	FRICITION FACTOR f	e/d	ROUGHNESS ε (ft)	* K _{90°} 125
1"	40	3.068	.05132	.0174	.0006	1.53 x 10 ⁻⁴	.2029
1 1/2"	160	2.624	.03757	.0181	.0007	1.53 x 10 ⁻⁴	.2172
2"	40	4.026	.08840	.0161	.0004	1.34 x 10 ⁻⁴	.1932
2 1/2"	120	3.624	.07160	.0162	.00044	1.33 x 10 ⁻⁴	.1944
3"	40	6.065	.20069	.015	.0003	1.52 x 10 ⁻⁴	.1800
3 1/2"	160	5.189	.14653	.0153	.00035	1.51 x 10 ⁻⁴	.1836
4"	40	11.938	.77708	.013	.00017	1.69 x 10 ⁻⁴	.1560

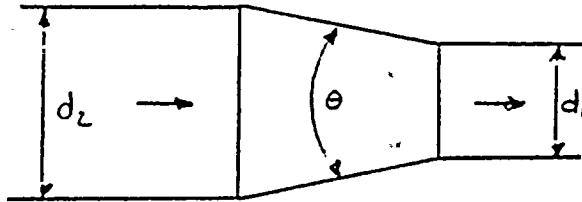
* RESISTANCE DUE TO BEND ONLY FOR 1.5d BENDS

REF: CRANE TECHNICAL PAPER No. 410

BY JBM DATE 12-8-82
 CHKD. BY J.E.Y. DATE 12-8-82
207 6.11.83

AMERICAN ELECTRIC POWER
 D.C. COOK UNITS 1 & 2
 LOSSES IN REDUCERS

SHEET NO. 1 OF 1
 PROJ. NO. 536A



$$\beta = \frac{d_1}{d_2}$$

IF: $\theta \leq 45^\circ$

FORWARD LOSS COEFFICIENTS

$$K = 0.8 \left(\sin \frac{\theta}{2} \right) (1 - \beta^2)$$

REVERSE LOSS COEFFICIENTS

$$K = 2.6 \left(\sin \frac{\theta}{2} \right) (1 - \beta^2)^2$$

SIZE	d_1	d_2	β	θ	$K, \text{ FORWARD}$	$K, \text{ REVERSE}$
17" SCH 40 x 6" SCH 40S	6.065"	11.938"	.5080	40.3°	.2045	.4930
6" SCH 40S x 4" SCH 40S	4.026"	6.065"	.6638	21°	.0815	.1483
4" SCH 40S x 3" SCH 40	3.068"	4.026"	.7620	13.66°	.0399	.0544
3" SCH 160 x 4" SCH 120	2.624"	3.624"	.7241	14.25°	.0472	.0730
4" SCH 120 x 6" SCH 160	3.624"	5.189"	.6984	16.19°	.0577	.0961
6" SCH 40S x 5" SCH 40	3.068"	6.065"	.5059	36.48°	.1565	.3784

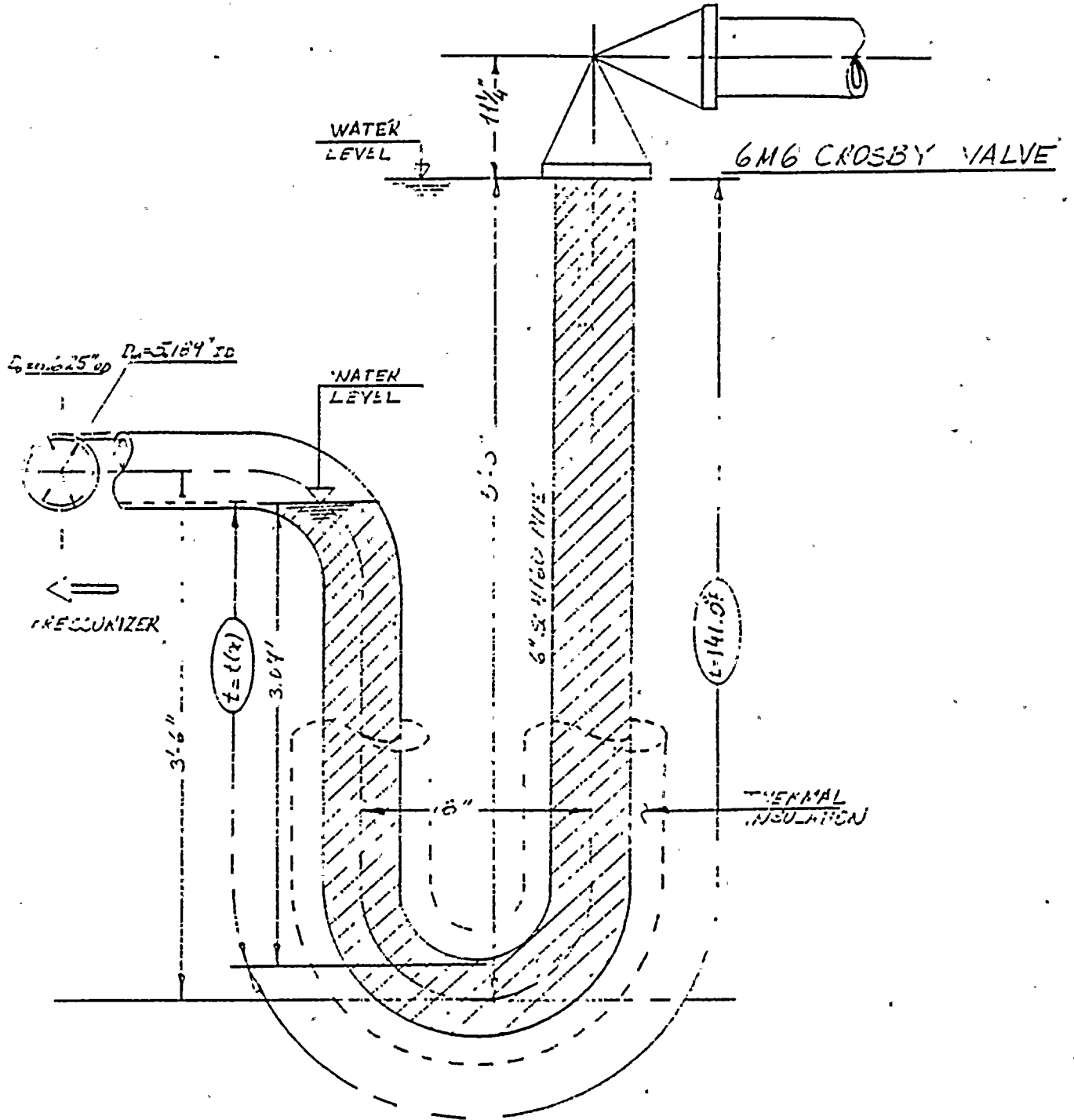
REFERENCE: CRANE TECHNICAL PAPER 410 p. A-26

K IS TAKEN WITH RESPECT TO THE SMALLER DIAMETER PIPE.

BY BAT DATE 12-17-62
CHKD. BY WJA DATE 1-5-63

AEP D.C. COOK UNIT 1
SV LINE LOOP SEAL TEMP DISTRIBUTION

SHEET NO. 1 OF 12
PROJ. NO. 5364



○ INDICATES TEMPERATURE VARIATIONS IN LOOP SEAL (REF. TEXT)

D.C. COOK UNIT 1
SAFETY VALVE LINE-LOOP SEAL
GEOMETRY



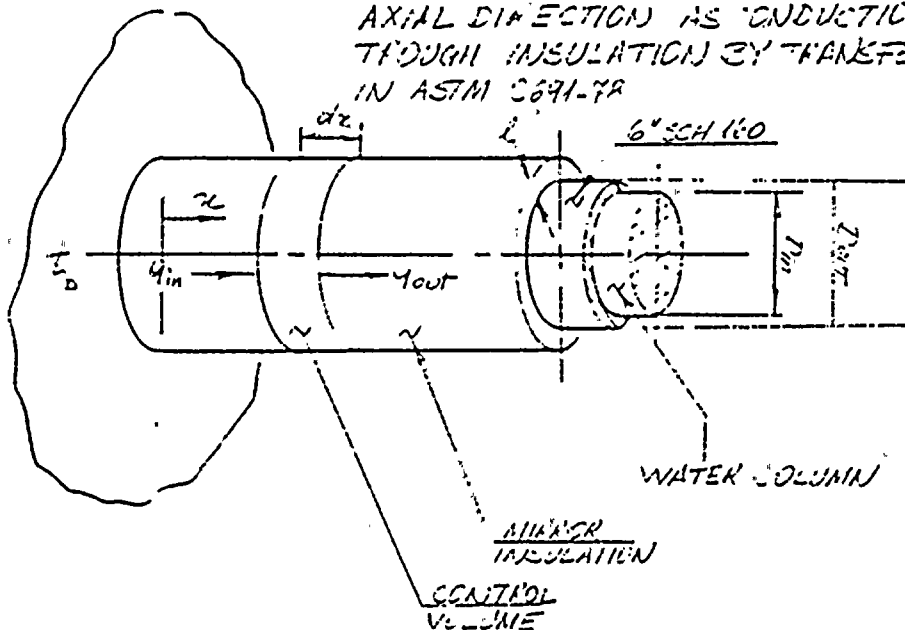
BY EAT DATE 12-19-82
 CHKD. BY UL DATE -3-83

AEP D.C. COOK UNIT 1
 SV LINE LOOP SEAL TEMP. DISTRIBUTION

SHEET NO. 2 OF 12
 PROJ. NO. 5364

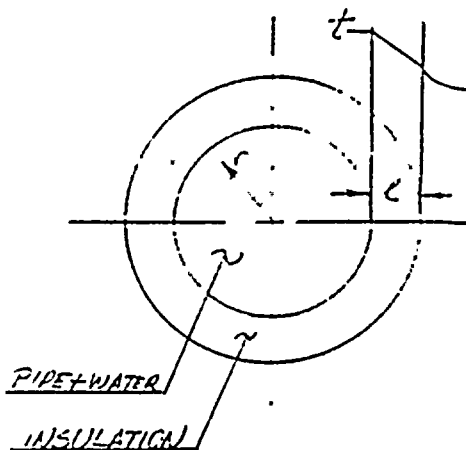
DERIVATION OF ENERGY EQUATION

ASSUMPTION 1: LOOP SEAL PIPE... IS MODELED AS STRAIGHT PIPE WITH FINITE LENGTH WITH BOUNDARY CONDITIONS DESCRIBED BELOW. HEAT IS TRANSFERRED BOTH IN AXIAL DIRECTION AS CONDUCTION AND IN RADIAL DIRECTION THROUGH INSULATION BY TRANSFERENCE EQUATION AS DESCRIBED IN ASTM C691-78



PIPE MODEL

ASSUMPTION 2: TEMPERATURE ACROSS CROSS-SECTION OF THE PIPE INCLUDING WATER AND WALL IS CONSTANT.



$$q_{in} \text{ (CONDUCTED INTO ELEMENT)} = [(KA)_{PIPE} + (KA)_{WATER}] \frac{dt}{dx}$$

$$q_{in} = -(KA)_{eff} \frac{dt}{dx} \quad \text{WHERE } (KA)_{eff} = (KA)_{PIPE} + (KA)_{WATER}$$

$$q_{out} \text{ (CONDUCTED OUT OF ELEMENT)} = q_{in} + \Delta q$$

$$q_{out} = \left[-(KA)_{eff} \frac{dt}{dx} + \frac{d}{dx} \left(-KA_{eff} \frac{dt}{dx} \right) dx \right]$$

TEMPERATURE DISTRIBUTION ACROSS THE CROSS-SECTION OF PIPE

BY EAT DATE 12-17-82
 CHKD. BY VIM DATE 1-2-83

AEP D.C. COOK UNIT 1
 SY LINE LOOP SEAL TEMP. DISTRIBUTION

SHEET NO. 3 OF 12
 PROJ. NO. 5364

$(KA)_{eff}$ = EQUIVALENT THERMAL CONDUCTANCE OF PIPE IN AXIAL DIRECTION

t = TEMPERATURE AS A FUNCTION OF x

$$q_s \text{ (TRANSFERRED OUT OF SURFACE OF THE PIPE)} = T_r A_s (t_{in} - t_{\infty})$$

(REF: ASTM C591-75)

WHERE: A_s = SURFACE AREA OF PIPE ($d^2 = \pi D_o dx$)

t_{in} = TEMPERATURE OF PIPE + WATER (ASSUMED EQUAL)

t_{∞} = PIPE ENVIRONMENT TEMPERATURE = 120 °F

T_r = THERMAL TRANSFERENCE $\frac{Btu}{hr-ft^2-F}$

ENERGY EQUATION FOR THE CONTROL VOLUME

$$q_{in} = q_{out} + q_s$$

$$-(KA)_{eff} \frac{dt}{dx} = \left\{ -(KA)_{eff} \frac{dt}{dx} + \frac{d}{dx} \left[-(KA)_{eff} \frac{dt}{dx} \right] dx \right\} + T_r \pi D_o dx (t - t_{\infty})$$

$$(KA)_{eff} \frac{d^2 t}{dx^2} = T_r \pi D_o (t - t_{\infty})$$

LET $\theta = t - t_{\infty}$ THEN $\frac{d\theta}{dx} = \frac{dt}{dx}$ AND $\frac{d^2 \theta}{dx^2} = \frac{d^2 t}{dx^2}$

LET $m^2 = \frac{T_r \pi D_o}{(KA)_{eff}}$

THEREFORE:

$$\frac{d^2 \theta}{dx^2} = m^2 \theta$$

$$\theta = C_1 e^{mx} + C_2 e^{-mx}$$

$$t = C_1 e^{mx} + C_2 e^{-mx} + 120$$

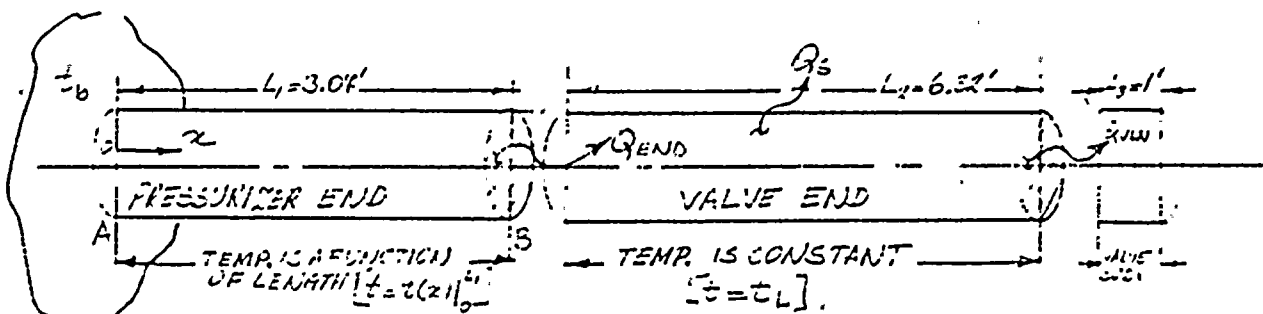
EQUATION - (1)
 GENERAL TEMPERATURE
 DISTRIBUTION EQN.

BY EAT DATE 11-20-81
 CHKD. BY VJM DATE 1-7-82

AEP D. C. COOK UNIT 1
 S.V. LINE LOOP SEAL TEMP. DISTRIBUTION

SHEET NO. 4 OF 12
 PROJ. NO. 5564

ASSUMPTIONS. TEMPERATURE VARIES ONLY IN THE PRESSURIZER END OF THE LOOP SEAL AND REMAINS CONSTANT AT THE VALVE END OF THE LOOP SEAL. THIS IS DUE TO THE CIRCULATION OF WATER IN THE VALVE END OF LOOP SEAL BECAUSE OF NATURAL CONVECTION (REF. PAGE 1 OF THIS ANALYSIS).



LOOP SEAL MODEL

BOUNDARY CONDITIONS FOR EQN 1

- 1- $x = 0 \quad t = t_0 = 660^\circ F$ (SAT. STEAM TEMP. @ 2500 psia)
- 2- $x = 3.04 \text{ ft} \quad -(kA)_{eff} \left. \frac{dt}{dx} \right|_{x=3.04} = Q_{END}$

$$-(kA)_{eff} [mC_1 e^{mx} - mC_2 e^{-mx}] = Q_{END} \quad \text{EQN. (2)}$$

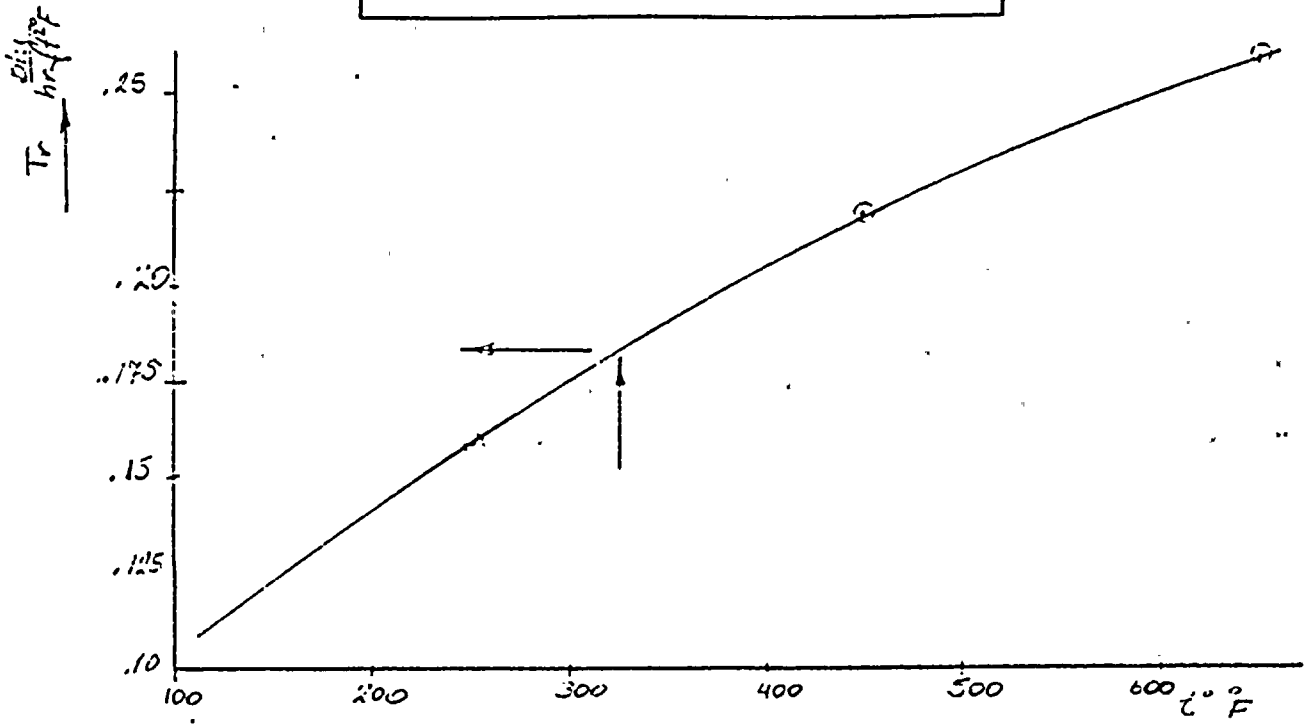
C₁ AND C₂ ARE FOUND FROM EQN. 1 AND EQN. 2
 T_r (TRANSMISSIVITY) IS A FUNCTION OF TEMPERATURE AND FROM THE TELECON BETWEEN "TES" AND "DIAMOND POWER" DATED (12-16-82)

$T_r \frac{BTU}{hr \text{ ft}^2 \text{ }^\circ F}$	TEMP °F
0.254	650
0.219	450
0.158	250

BY SAT DATE 12-20-82
 CHKD. BY MM DATE 1-3-83

AEP D.C. COOK UNIT 1
 S.V. LINE LOOP SEAL TEMP. DISTRIBUTION

SHEET NO. 5 OF 12
 PROJ. NO. 5364



PLOT OF TRANSMISSIVITY VS TEMPERATURE FROM DATA ON TELECON BETWEEN "TES" AND "DIAMOND FLUOR" DATED (12-16-82)

ASSUMED AVERAGE FLUID TEMPERATURE = 325 °F

FROM PLOT $T_r = 0.18 = \frac{3tu}{nr-ft^2}$ @ $t = 325 °F$

$$(KA)_{eff} = (KA)_{PIPE} + (KA)_{WATER}$$

$$A_{PIPE} = 13.22 \text{ in}^2$$

$$A_{WATER} = 21.1 \text{ in}^2$$

ESTIMATED AVERAGE VALUES

$$K_{PIPE} \approx 7.9 \frac{Btu}{hr-ft^2-F} \quad (\text{REF: PIPE MAT. SPECT OCCPM1040CS PROVIDED BY AEP AND ASME III COLLN PRESSURE WHEEL COIL})$$

$$K'_{WATER} = 0.38 \frac{Btu}{hr-ft^2-F} \quad (\text{REF: HEAT TRANSFER, J. P. HOLMAN Fig 1.5) FIRST EDITION})$$

$$(KA)_{eff} = 0.48 \frac{Btu-ft}{hr-ft^2-F}$$

(*NOTE: PIPE IS MADE OF ASTM A-376 GRADE TP316 SEAMLESS AUSTENITIC STEEL)

BY SAE DATE 12-21-62
 CHKD. BY WLL DATE 1-7-63

A E D S. C. COCK JNITI
 S.V. LINE LOOP SEAL TEMP. DISTRIBUTION

SHEET NO. 5 OF 12
 PROJ. NO. 5364

ASSUME $t = 145^{\circ}F$ AT VALVE END OF LOOP SEAL

$$Q_{END} = Q_s + Q_{VLV}$$

$Q_s =$ HEAT LOSS ACROSS INSULATION FROM VALVE END OF LOOP SEAL

$$Q_s = T_r A_s (t_L - t_{\infty})$$

WHERE $A_s = D_o \pi L_2$ SURFACE AREA OF VALVE END OF LOOP SEAL

$$T_r = 0.120 \frac{Btu}{ft^2 hr F} \quad \textcircled{1} \quad 145^{\circ}F \text{ (FROM PICT AT PAGES OF THIS ANALYSIS)}$$

(NOTE: DIFFERENT T_r IS USED IN EQN. 1 AND Q_s SINCE MEAN TEMPERATURES ARE DIFFERENT)

$$Q_s = (0.120)(0.55 \times \pi \times 6.32) [145 - 120]$$

$$Q_s = 32.76 \frac{Btu}{hr}$$

VALVE END HEAT LOSS IS ASSUMED AS HEAT FLOWING THROUGH A SOLID VALVE BODY WITH $L_3 = 1'$ EQUIVALENT LENGTH AND D_o DIAMETER.

$$Q_{VLV} = (kA)_{steel} \frac{t_L - t_{\infty}}{L_3}$$

$$Q_{VLV} = .79(0.24) \frac{145 - 120}{1.0}$$

$$Q_{VLV} = 47.28 \frac{Btu}{hr}$$

$$Q_{END} = Q_s + Q_{VLV}$$

$$\underline{Q_{END} = 80.04 \frac{Btu}{hr}}$$

BY SAT DATE 12-21-82
 CHKD. BY [Signature] DATE 1-7-83

AEP S.C. COOL UNIT 1
 S.V LINE LOOP SEAL TEMP. DISTRIBUTION

SHEET NO. 7 OF 12
 PROJ. NO. 5364

TEMPERATURE DISTRIBUTION EQUATION (2) $0 < x < L_1 = 3.07$

$$t = C_1 e^{mx} + C_2 e^{-mx} + 120$$

SOLVE FOR C_1 AND C_2 USING BOUNDARY CONDITIONS:

$x = 0 \quad t = t_b = 668 \text{ }^\circ\text{F}$ BOUNDARY CON. 1

$-kA \left. \frac{dt}{dx} \right|_{x=L_1} = Q_{END}$ BOUNDARY CON. 2

$$-m \cdot 0.78 \left[C_1 e^{mL_1} - C_2 e^{-mL_1} \right] = 80.04$$

$$m = \left[\frac{T_r \pi D_o}{kA_{eff}} \right]^{1/2}$$

$$m = \left[\frac{0.152 \pi \cdot 2.55}{0.78} \right]^{1/2}$$

$$m = 0.64$$

SUBSTITUTING BOUNDARY CONDITIONS:

FROM BC.1 $C_1 e^{0.64(0)} + C_2 e^{-0.64(0)} = 548$ EQN. (2)

FROM BC.2 $-C_1 e^{0.64L_1} + C_2 e^{-0.64L_1} = (k \dots [Q_s + Q_{vuv}])$ EQN. (3)

AFTER SUBSTITUTING

$$C_1 + C_2 = 548$$

$$-7.13 C_1 + 0.14 C_2 = 160.08$$

TWO EQUATIONS WITH TWO UNKNOWNS AFTER SOLVING

$$C_1 = -11.5 \quad \text{AND} \quad C_2 = 559.50$$

BY EAT DATE 12-21-82
 CHKD. BY W.A. DATE 1-2-83

AEP J. J. COOK UNIT 1
 S.V. LINE LOOP SEAL TEMP. DISTRIBUTION

SHEET NO. 3 OF 12
 PROJ. NO. 5300

TEMPERATURE DISTRIBUTION EQUATION BECOMES

$$t = -11.5 e^{0.64x} + 559.5 e^{-0.64x} + 120 \quad @ \quad 0 < x < 3.07$$

CHECKING ASSUMED $t = t_L = 145^\circ$ @ $x = 3.074$

PROCEDURE: FIND $A(t)$ BY SUBSTITUTING $x = 3.07$ AND COMPARE THIS (t) BY ASSUMED $t = 145^\circ F$

$$t = -11.5 e^{10.64(3.07)} + 559.5 e^{-10.64(3.07)} + 120$$

$$t_{1000} = 116.44^\circ F < t_{200} = 145^\circ F$$

ASSUME: $t = t_L = 135^\circ F$

EQUATIONS (2) AND (3) BECOMES:

$$\begin{cases} C_1 + C_2 = 548 & Q_{VIV} = 28.74 \text{ STU/HR} \\ -7.13 C_1 + 0.14 C_2 = 96.00 & Q_S = 19.56 \text{ STU/HR} \end{cases}$$

$Q_{END} = 40.0$

AFTER SOLVING

$$C_1 = -2.68$$

$C_2 = 550.68$ AND TEMP DISTRIBUTION:

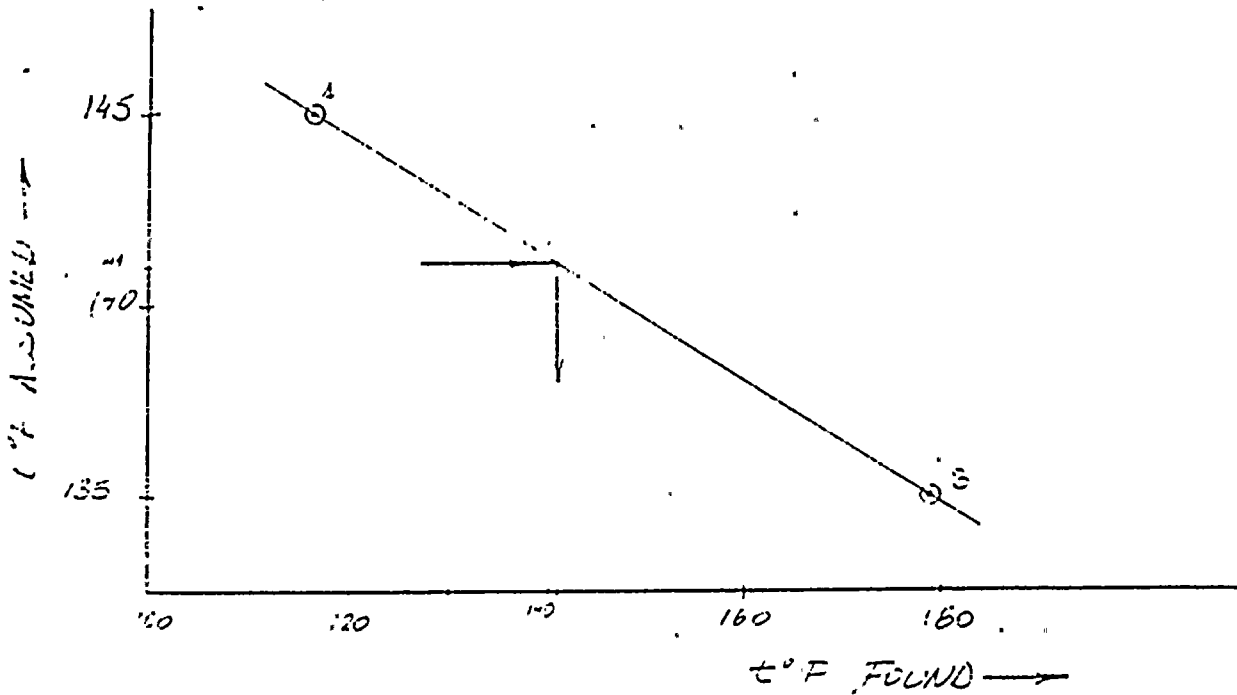
$$t = -2.68 e^{0.64x} + 550.68 e^{-0.64x} + 120$$

$$@ \quad x = 3.07 \quad t = 178.08^\circ F > t_{200} = 135^\circ F$$

BY SAT DATE 12-21-82
 CHKD. BY J. M. DATE 1-1-83

AEP D.C. COOK UNIT 1
 S.V. LINE LOOP SEAL TEMP. DISTRIBUTION

SHEET NO. 9 OF 12
 PROJ. NO. 5364



AFTER PLOTTING t_{ass} VS. t_{found} AND BY VISUAL INTERPOLATION
 (PROCEDURE: FIND $t_{ass} = t_{found}$ ON LINE A-S)
 THEN $t_{ass} = 141^{\circ}F$

SUBSTITUTING $t_{ass} = 141^{\circ}F$ INTO EQN (2) AND EQN (3)

$$Q_1 = 27.52 \frac{Btu}{hr}$$

$$Q_{VLV} = 39.32 \frac{Btu}{hr}$$

$$Q_{END} = 67.34 \frac{Btu}{hr}$$

$$\begin{cases} C_1 + C_2 = 548 \\ -7.13C_1 + 0.14C_2 = 134.67 \end{cases}$$

$$C_1 = -7.97$$

$$C_2 = 555.97$$

$$t = -7.97 e^{0.64x} + 555.97 e^{-0.64x} + 120$$

$$@ x = 3.07 ; t_{FOUND} = 141.08^{\circ}F \approx t_{ass} = 141.00$$

BY ZAT DATE 12-21-53
 CHKD. BY JULI DATE 1-7-54

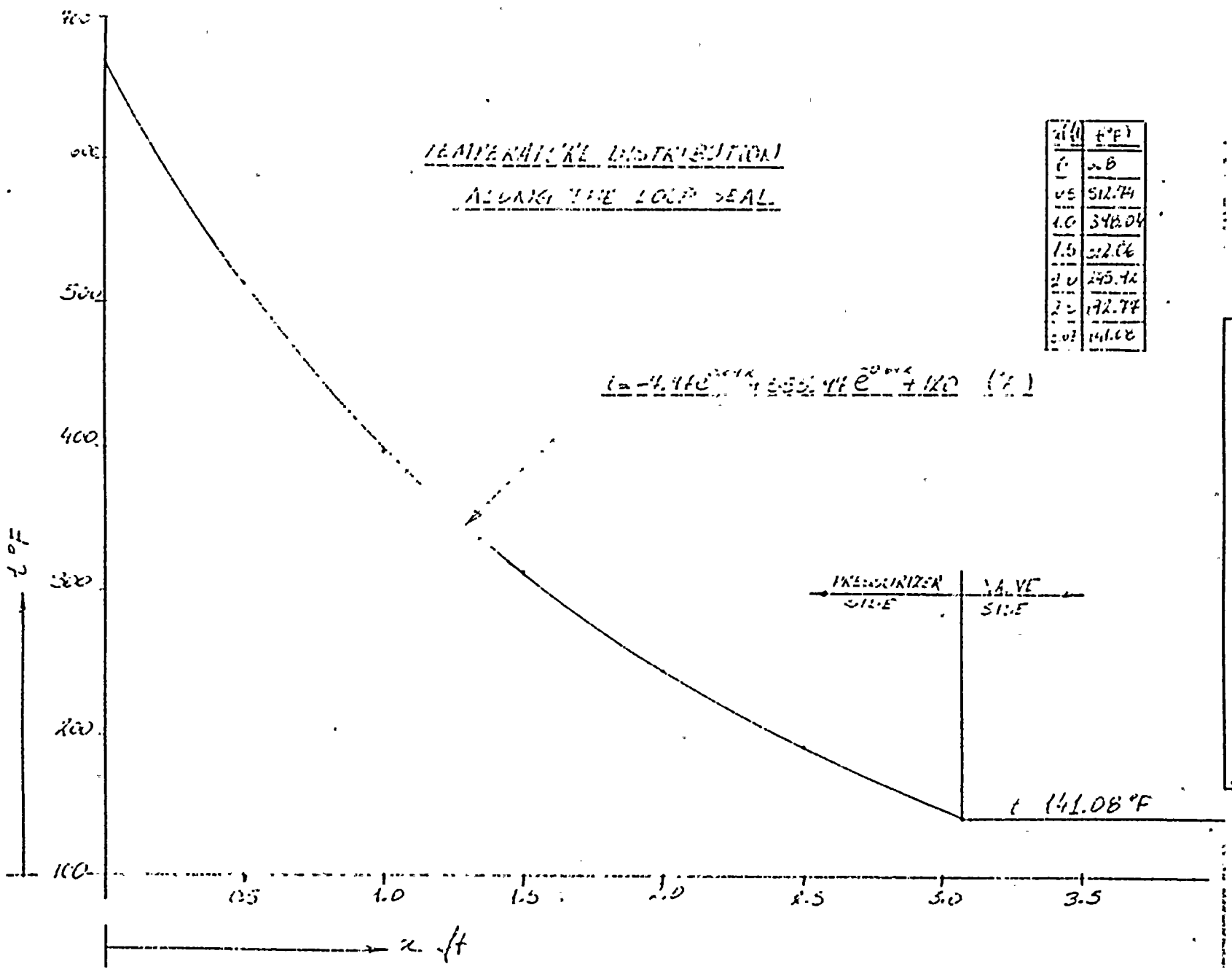
A E P S-C-L-COK
 S. V. LINE - TOP SEAL TEMP DISTRIBUTION

SHEET NO. 10 OF 12
 PROJ. NO. 5364

x (ft)	T (°F)
0	526
0.5	512.74
1.0	500.04
1.5	487.06
2.0	475.74
2.5	462.74
3.0	441.08

TEMPERATURE DISTRIBUTION
ALONG THE LOOP SEAL

$$T = 526 - 4.71x + 0.002x^2 + 110 \quad (1)$$



BY BAT DATE 12-21-62
 CHKD. BY ... DATE ...

AEP D.C. COOK UNIT 1
 S.V. LINE LOOP SEAL TEMP. DISTRIBUTION

SHEET NO. 11 OF 12
 PROJ. NO. 5364

CHECKING $T_r = 0.181 \frac{\text{Btu}}{\text{hr ft}^2 \text{F}}$ FOR $T_{\text{AVE}} = 325^\circ\text{F}$ (PAGE 5)

AREA UNDER $t = t(x)$ CURVE @ $0 < x < L, L = 3.07'$

$$\text{AREA} = \int_0^L t(x) dx$$

$$= \int_0^L [-11.47 e^{(0.64)x} + 555.47 e^{-(0.64)x} + 120] dx$$

$$= - \frac{11.47}{0.64} e^{0.64x} \Big|_0^{3.07} + \frac{555.47}{0.64} e^{-(0.64)x} \Big|_0^{3.07} + 120x \Big|_0^{3.07}$$

$$= (-38.83 + 12.45) - (121.75 - 868.70) + (368.4)$$

$$\text{AREA} = 1038.24 \text{ } \frac{\text{Btu}}{\text{hr ft}^2}$$

$$t_{\text{AVE}} = \frac{1038.24}{3.07}$$

$$t_{\text{AVE}} = 338.12^\circ\text{F}$$

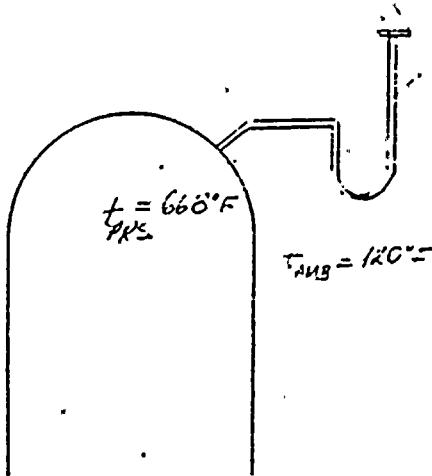
2% DIFFERENCE FROM THE ASSUMED $t_{\text{AVE}} = 325^\circ\text{F}$
WHICH IS ACCEPTABLE

BY SAJ DATE 12-22-82
 CHKD. BY 1/11/83 DATE 1-11-83

AEP D. C. COOK UNIT 1
 S.V. LINE LOOP SEAL TEMP. DISTRIBUTION

SHEET NO. 12 OF 12
 PROJ. NO. 5364

CHECKING THE RADIATION EFFECTS ON LOOP SEAL BY
TAKING CONSERVATIVE VALUES FOR THE WORST CASE



ASSUME THE LOOP SEAL AS LUMPED VOL.
 AVERAGE TEMPERATURE OF LOOP SEAL

$$T_{AVE} = \frac{C_1 P A L_1 (338.42) + C_2 P A L_2 (41.08)}{C_1 P A L_1 + C_2 P A L_2} = 205.6$$

$$T_{AVE} = 205.60^\circ F = 205.60^\circ K \quad L_1 = 3.07'$$

WHERE ρ = DENSITY $L_2 = 6.32'$
 A : CROSS-SECTIONAL AREA
 C_p : HEAT CAPACITY

FROM PAGE 5 $T_r = 122.41^\circ F$ @ $t = 2.12 \times 10^{-4}$

$$\frac{Q}{A} = (1.45)(205.6 - 120) = 12.41 \frac{Btu}{hr \cdot ft^2}$$

T_s - SURFACE TEMP. OF LOOP SEAL
 USING NEWTON'S LAW OF
 COOLING $h = 5 \frac{Btu}{hr \cdot ft^2 \cdot ^\circ F}$

$$12.41 = 5(T_s - 120)$$

$$T_s = 122.40^\circ F$$

PRESSURIZER :

MAX. HEAT LOSS FROM PRESSURIZER $\frac{Q}{A} = 30 \frac{Btu}{hr \cdot ft^2}$ (REF. METALLIC INSULATION
 AEP SPEC. NO. ECC001029CS

T_p SURFACE TEMP. OF PRESSURIZER $80 = 5(L_p - 120)$
 $T_p = 136^\circ$

ASSUMING : RADIATION SHAPE FACTORS = 0.5
 EMISSIVITY = 0.03 (SINCE SURFACES ARE MIRROR)
 (REF: MARKS MECH. ENG. HANDBOOK
 5TH EDITION)

STEFAN-BOLTZMANN CONST. $\sigma = 0.1714 \times 10^{-8} \frac{Btu}{hr \cdot ft^2 \cdot ^\circ R^4}$

$$\frac{Q}{A}_{RAD} = \sigma \epsilon F_{12} (T_p^4 - T_s^4) = (0.03)(0.5)(0.1714 \times 10^{-8}) [596^4 - 562^4]$$

$$\frac{Q}{A}_{RAD} = 0.294 \frac{Btu}{hr \cdot ft^2}$$

RADIATION HEAT TRANSFER HAS NEGLIGIBLE
EFFECT ON LOOP SEAL TEMP. DISTRIBUTION

BY CHM DATE 1-11-82
 CHKD. BY KG DATE 5-24-83

TEMPERATURE DISTRIBUTION
 DETERMINATION - UNIT 2

SHEET NO. 1 OF 1
 PROJ. NO. 5364

USING THE EQUATION:

$$t = -7.97e^{0.64n} + 555.97e^{-0.64n} + 120 \text{ (OF)}$$

WHERE n = AXIAL DISTANCE AWAY FROM
 PRESSURIZED ALONG ROOF SEAL

ACCURATE $0 \leq n \leq 3.07$ (FT)

FOR VALUES $n > 3.07$ $t = 141.08 \text{ °F}$

REF. SAS HAND CALC. 2-22-82

UNIT VOL VOLUME	n VALUE (FT)	t DETERMINED, (°F)
501	0.25	537.7
502	0.75	452.2
503	1.25	352.2
504	1.75	276.8
505	2.25	218.2
506	2.75	169.3
507	3.25	141.1
↓		↓
520	VALVE	Y

BY JHM DATE 5-4-69
 CHKD. BY KG DATE 5-24-83

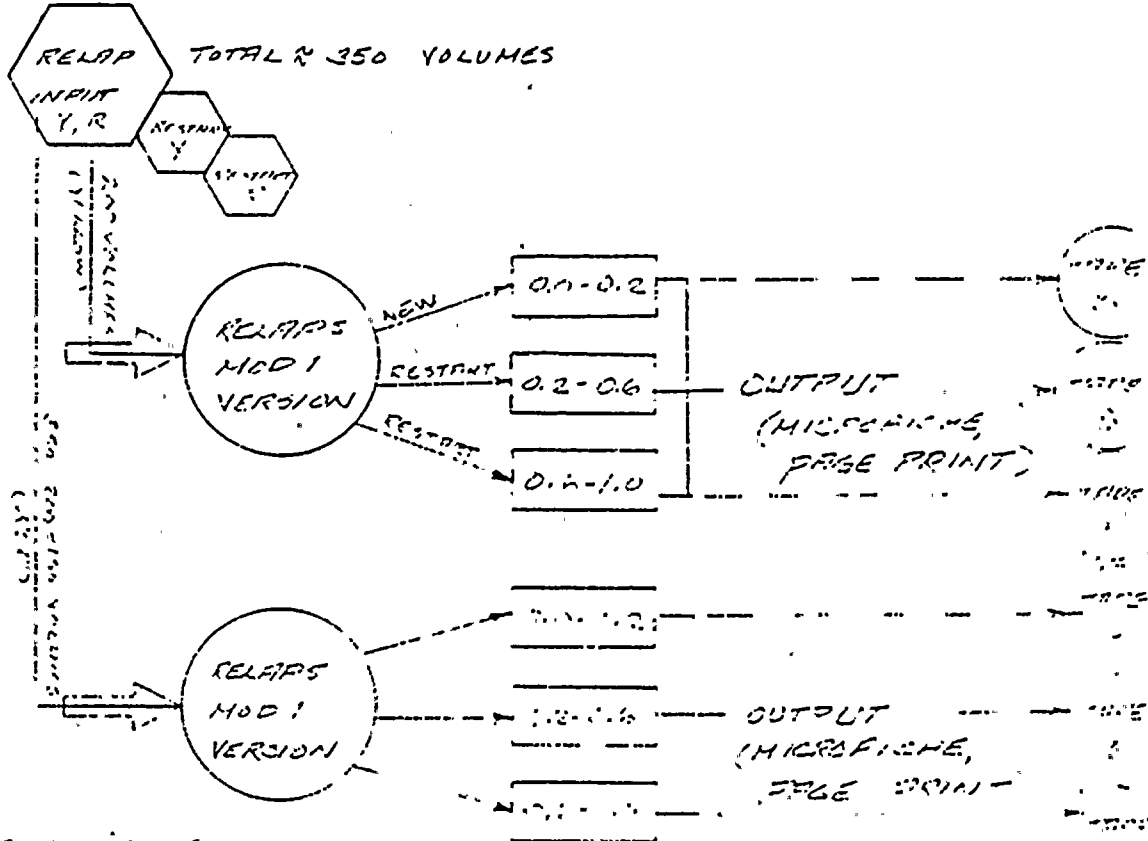
COMPUTER USAGE FOR
 THERMAL ANALYSIS

SHEET NO. 1 OF 2
 PROJ. NO. 5364

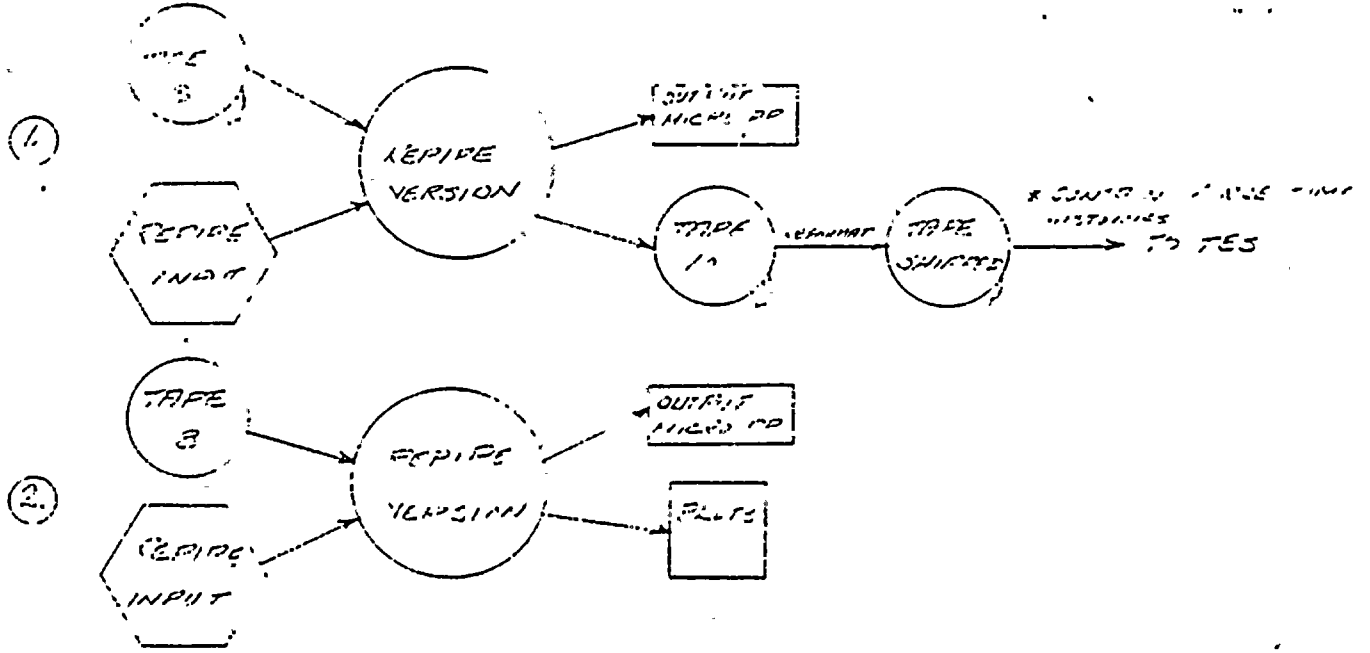
TRANSIENTS:

1. LOOPSEAL (SATURATED) STEAM CASE
2. SOLID 400° WATER CASE

© CDC



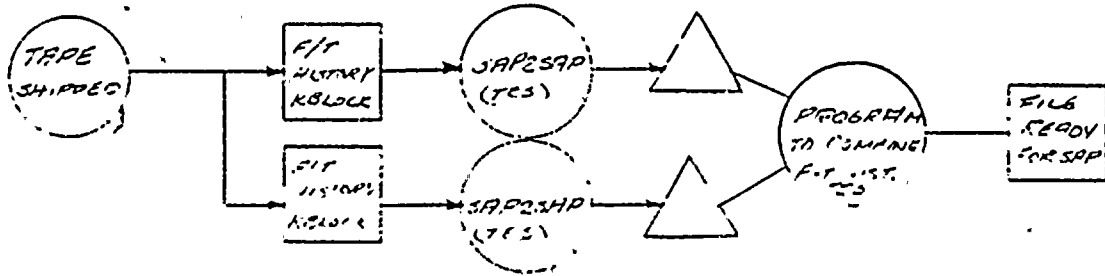
FOR EACH TAPE 6: FOLLOW 1 & 2.



BY JMM DATE 5-4-83
CHKD. BY KJG DATE 5-24-83

COMPUTER USAGE FOR
THERMAL ANALYSIS.

SHEET NO. 2 OF 2
PROJ. NO. 5364





10

BY QUM DATE 3-28-83
CHKD. BY KIT DATE 5-9-83

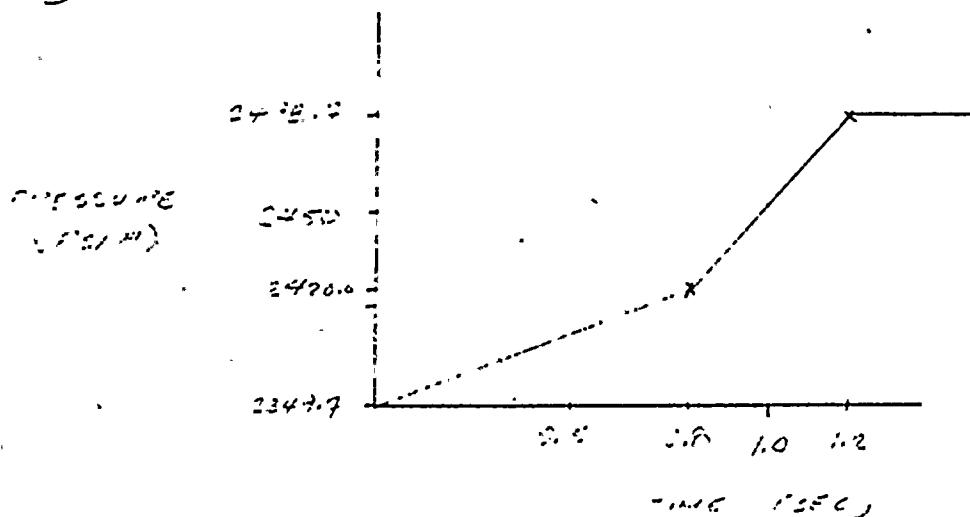
POPV UNIT / BOUNDARY
CONDITIONS

SHEET NO. 1 OF 1
PROJ. NO. 5364

① VALVE OPENING TIME, POPV : 1.0 SEC
MARSONEILAN : REF.

(TIME) REF: TABLE 4.5.2-1 PG 4-53 API SAFETY
RELIEF VALVE TEST REPORT (CP-4102)

② PRESSURIZED CONDITIONS:



REF: REP LETTER TO LOS 11-29-82 / CURVE #3 6 OF 7

③ VALVE FLOW AREA CALCULATED KNOWING TIME
FLOW RATE = 177,000 LBM/HR. REF: PG 4-53 API
SAFETY AND RELIEF VALVE TEST REPORT (CP-4102)
AND RUN BEICORD AREA = 0.00006 FT²

④ QUALITY USED IN UPSTREAM PIPING TO
SIMULATE CONDENSATE SEE KUG CALC

BY JMM DATE 5-21-83
CHKD. BY SK DATE 5-24-83

NON-CONDENSIBLE GAS QUALITY
CALCULATION FOR INITIAL COND.
IN. TS 152

SHEET NO. 1 OF 1
PROJ. NO. 5364

FOR INITIAL CONDITIONS OF:

$$P_T = 17.7 \text{ PSIA}$$

$$T = 120^\circ \text{ F} \quad P_g = 1.6724 \text{ PSIA}$$

SPECIFIC HUMIDITY

$$Y = \frac{M_w}{M_a} = \frac{\text{MASS OF WATER VAPOR}}{\text{MASS OF AIR}} = \frac{V_w}{V_a}$$

$$Y = \frac{P_w T / P_a}{R_{wT} / P_w} = 0.622 \frac{P_w}{P_a}$$

$$Y = 0.622 \frac{1.6724 \text{ PSIA}}{16.002 \text{ PSIA}}$$

$$Y = 0.06576$$

$$\text{NONCONDENSIBLE GAS (AIR) QUALITY} = 1 - Y = 0.93424$$

5.0 STRUCTURAL ANALYSIS

Deadweight, thermal, seismic and force/time history analyses were performed for the pressurizer safety and relief valve discharge piping using the TMRSAP computer program; a modified version of SAPIV. The computer model used was based on TES isometric drawing E-5761, Revision 2 included in Section 7.0. In general, the structural analysis was done in accordance with AEP letter dated November 29, 1982 from Mr. Sam Ulan of AEP to Mr. L. B. Semprucci of TES (Reference 2) and AEP letter dated March 15, 1983 from Mr. Sam Ulan of AEP to Mr. Pat Harrison of TES (Reference 3). Section 6.0 contains all of the results for the analyses performed.

Only the piping shown on drawing E-5761 was included in the analysis. Branch lines not in the scope of work were decoupled in accordance with the procedure outlined in TES letter 5364-21 dated February 2, 1983 (Reference 8); that is if the moment of inertia of the main run of pipe is greater than or equal to 40 times the moment of inertia of the branch, the branch line was decoupled.

Valve drawing 88405-1 listed the weight of valves NMO-151, 152 and 153 as being 352 pounds and this value was used by TES in the deadweight and seismic analyses. However, per Reference 7, TES was informed by AEP that the valve weight was actually 400 pounds. TES reran the deadweight and seismic analyses and determined that the net result of the valve weight change was negligible. Since pipe stresses and support loads had already been extracted and calculated based on the 352 pound valve weight, it was decided not to revise the deadweight and seismic analyses. The valve weight was changed to 400 pounds prior to executing the PORV transient shock analysis.

5.1 Deadweight Analysis

The effects of pipe weight, water weight and insulation weight were considered in the deadweight analysis. In addition, concentrated weights were located wherever branch lines were decoupled, at flanges, and at valve cg's. The weights used for decoupled branch lines were calculated in accordance with the procedure defined in TES letter 5364-25, dated February 14, 1983 (Reference 9). Per Reference 3, only the normal operating deadweight case was analyzed.

A summary of the weights and forces applied in the deadweight analysis are shown in Table 5-1.

5.2 Thermal Analysis

Three thermal cases were analyzed; normal operation, PORV operation, and SV operation. Temperature distributions for the PORV and SV cases were obtained from the RELAP5 output. Throughout this report, thermal case 1 refers to normal operation, thermal case 2 refers to PORV operation, and thermal case 3 refers to SV operation. Results of thermal case 3 are given only for the nodes, supports, and valves which are part of the quarter model, described in Section 2.

Boundary displacements were calculated for the quench tank nozzle, pressurizer nozzles and support 1-GRC-R-616, which connects to the pressurizer, for all thermal conditions analyzed. These calculations are shown in Section 6.6.

5.3 Seismic Analysis

Seismic analysis was performed for both the operating basis earthquake (OBE) and design basis earthquake (DBE). For each of these conditions, two analyses were made; one considering response spectra applied in the X and Y directions and one considering response spectra applied in the Y and Z directions. All seismic values reported in Section 6 are based (per node) on the analysis direction yielding the larger results.

For the OBE analysis, the horizontal spectra was obtained by enveloping Containment Crane Wall Figures for elevations 651'-3", 663'-4", 675'-4" and 687'-6". The figures used were based on .5% equipment damping and 2% structural damping. Prior to enveloping the figures, the peaks of each curve were broadened +/-15%, in accordance with NRC Regulatory Guide 1.122.

For the vertical direction Containment Base Slab, elevation 597'6" was used with .5% equipment damping and 2% structural damping. The peaks of this curve were also broadened +/-15% and two-thirds of the value obtained from the figure was used in the spectra.

For the DBE analysis, the spectra for the horizontal and vertical directions were obtained in the same manner as for the OBE analysis; except that 5% structural damping was used rather than 2%.

The procedures described above are in accordance with the November 29, 1982 letter from AEP (Reference 2) and TES letter 5364-33, dated April 8, 1983 (Reference 10).

The figures used and spectra obtained are detailed in Section 6.6.

5.4 Force/Time History Analysis

5.4.1 PORV Transient

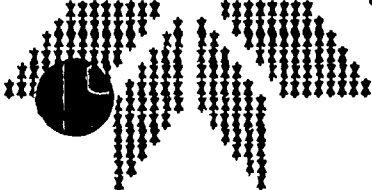
Two potential PORV transients exist, condensate and solid water. Based on a preliminary analysis, of Unit 1, it was determined that the solid water case was the dominating condition throughout the piping system, therefore, only the solid water case was analyzed for Unit 2.

The solid water analysis was performed at one millisecond intervals for a length of one second. All loads peaked previous to one second, indicating that the analysis was performed for a sufficient length of time.

5.4.2. SV Transient

A quarter model analysis was performed for the SV transient shock condition. This analysis, which considered the opening of valve SV-45C only, resulted in catastrophic failure of the piping system. For economic reasons, it was decided that no further evaluation of the SV transient shock condition would be considered until the system was modified.

TELEDYNE ENGINEERING SERVICES



PROJECT: 5364 8 JUNE 1983
 D. C. COOK UNIT 2
 DEADWEIGHT DATA TABLE 5-1

BY *DMB* DATE *6-8-83*
 CHKD *DMB* DATE *6/2/83*
 SHEET NO. _____ OF _____

MAIN RISER

NODES	PIPE SIZE	DIST. WEIGHT LBS/IN	CONTENTS PIPE/INSULATION/WATER
2	12" SCH. 40	34.748 *	(P) I W
4 THRU 176	12" SCH. 40	4.458	(P) I W
219 THRU 230	6" SCH. 40S	1.582	(P) I W

* FLANGE WEIGHT DISTRIBUTED OVER 2.042' ADDED TO PIPE WEIGHT.

APPLIED FORCES

NODE	FORCE LBS.
50	3281

CONCENTRATED WEIGHTS

NODE	WEIGHT LBS.
1000	122
1001	20
1005	12

NOTE: APPLIED FORCES REPRESENT THE SETTINGS OF CONSTANT FORCE SUPPORTS AT THE NODES INDICATED. ALL FORCES ARE APPLIED IN THE +Y GLOBAL DIRECTION.

SRV LOOP C (REFERS TO SRV LOOP CONTAINING VALVE SV-45C, THIS NOTATION IS TYPICAL OF LOOPS B AND A ALSO.)

NODES	PIPE SIZE	DIST. WEIGHT LBS/IN	CONTENTS PIPE/INSULATION/WATER
72 THRU 97	6" SCH. 40S	1.582	(P) I W
94 THRU 103	6" SCH. 40S	2.632	(P) (I) W
107 THRU 116	6" SCH. 160	5.575	(P) (I) (W)
118 THRU 124	6" SCH. 160	4.904	(P) (I) W

APPLIED FORCES

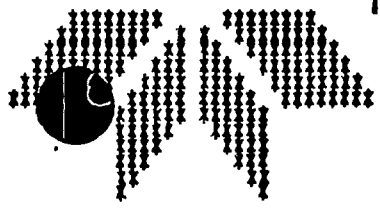
NODE	FORCE LBS.
99	1054

CONCENTRATED WEIGHTS

NODE	WEIGHT LBS.
102	81
105	685
1006	164



TELEDYNE ENGINEERING SERVICES



PROJECT: 5364
 D. C. COOK UNIT 2
 DEADWEIGHT DATA

8 JUNE 1983

TABLE 5-1 Cont.

BY AMB DATE 6-8-83
 CHKD dm DATE 6/8/83
 SHEET NO. _____ OF _____

SRV LOOP B

NODES	PIPE SIZE	DIST. WEIGHT LBS/IN	CONTENTS PIPE/INSULATION/WATER		
126 THRU 143	6" SCH. 40S	1.582	(F)	I	W
144 THRU 152	6" SCH. 40S	2.632	(F)	(I)	W
156 THRU 166	6" SCH. 160	5.575	(F)	(I)	(W)
168 THRU 174	6" SCH. 160	4.904	(F)	(I)	W

APPLIED FORCES		CONCENTRATED WEIGHTS	
NODE	FORCE LBS.	NODE	WEIGHT LBS.
147	1072	153	81
		1540	685
		155	164
		1007	14

SRV LOOP A

NODES	PIPE SIZE	DIST. WEIGHT LBS/IN	CONTENTS PIPE/INSULATION/WATER		
176 THRU 187	6" SCH. 40S	1.582	(F)	I	W
188 THRU 196	6" SCH. 40S	2.632	(F)	(I)	W
200 THRU 210	6" SCH. 160	5.575	(F)	(I)	(W)
212 THRU 218	6" SCH. 160	4.904	(F)	(I)	W

APPLIED FORCES		CONCENTRATED WEIGHTS	
NODE	FORCE LBS.	NODE	WEIGHT LBS.
189	983	197	81
		1980	685
		199	164
		1008	14

REV. NO. 0

TELEDYNE ENGINEERING SERVICES



PROJECT: 5364 8 JUNE 1983
 D. C. COOK UNIT 2
 DEADWEIGHT DATA TABLE 5-1 Cont.

BY DMB DATE 6-8-83
 CHKD DMB DATE 6/8/83
 SHEET NO. _____ OF _____

FORV LOOP 151 (REFERS TO FORV LOOP CONTAINING VALVES NMO-151 AND NRV-151, THIS NOTATION IS TYPICAL OF LOOPS 152 AND 153 ALSO.)

NODES	PIPE SIZE	DIST. WEIGHT LBS/IN	CONTENTS PIPE/INSULATION/WATER		
230	3" SCH. 40S	.632	(P)	I	W
286 THRU 292	3" SCH. 40S	1.190	(P)	(I)	W
296 THRU 308	3" SCH. 160	1.948	(P)	(I)	(W)
310 THRU 316	3" SCH. 160	1.753	(P)	(I)	W
318 THRU 330	4" SCH. 120	2.200	(P)	(I)	W
332 THRU 342	6" SCH. 160	4.825	(P)	(I)	W

APPLIED FORCES

NODE	FORCE LBS.
290	798
304	858
316	634

CONCENTRATED WEIGHTS

NODE	WEIGHT LBS.
295	480
301	400
1003	14
1002	14

TELEDYNE ENGINEERING SERVICES

PROJECT: 5364 8 JUNE 1983
 D. C. COOK UNIT 2
 DEADWEIGHT DATA TABLE 5-1 Cont.

BY DMB DATE 6-8-83
 CHKD Smb DATE 6/8/83
 SHEET NO. _____ OF _____

PORV LOOP 152

NODES	PIPE SIZE	DIST. WEIGHT LBS/IN	CONTENTS PIPE/INSULATION/WATER		
240 THRU 402	3" SCH. 40S	.632	(P)	I	W
404 THRU 346	3" SCH. 40S	1.190	(P)	(I)	W
350 THRU 320	3" SCH. 160	1.948	(P)	(I)	(W)

APPLIED FORCES

NODE	FORCE LBS.
400	732

CONCENTRATED WEIGHTS

NODE	WEIGHT LBS.
349	480
355	400

PORV LOOP 153

NODES	PIPE SIZE	DIST. WEIGHT LBS/IN	CONTENTS PIPE/INSULATION/WATER		
232 THRU 240	4" SCH. 40S	.899	(P)	I	W
242 THRU 259	3" SCH. 40S	.632	(P)	I	W
257 THRU 262	3" SCH. 40S	1.190	(P)	(I)	W
266 THRU 276	3" SCH. 160	1.948	(P)	(I)	(W)
278 THRU 284	3" SCH. 160	1.772	(P)	(I)	W

APPLIED FORCES

NODE	FORCE LBS.
261	720
274	637

CONCENTRATED WEIGHTS

NODE	WEIGHT LBS.
265	480
271	400
1004	14

6.0 ANALYTICAL RESULTS

6.1 Stress Summary

Stress calculations were based on the 1967 Edition of the ANSI B31.1 Code (Reference 11), the AEP letter dated November 29, 1982 (Reference 2), and the AEP letter dated March 15, 1983 (Reference 3). These stress combinations were performed:

- A1 normal pressure stress + deadweight stress $\leq S_h$
- A2 normal thermal stress range $\leq (1.25 S_c + .25 S_h)$
- B1 normal pressure stress + deadweight stress + OBE stress $\leq 1.2 S_h$
- B2 PORV transient pressure stress + deadweight stress + $\left[(\text{OBE stress})^2 + (\text{PORV transient shock stress})^2 \right]^{1/2} \leq 1.2 S_h$
- B3 PORV transient thermal stress range $\leq 1.25 S_c + .25 S_h$
- C1 normal pressure stress + deadweight stress + DBE stress $\leq 1.8 S_h$
- C2 SV transient pressure stress + deadweight stress + SV transient shock stress $\leq 1.8 S_h$
- C3 SV transient thermal stress range $\leq 1.25 S_c + .25 S_h$

Stresses were not calculated for equation A3 since all node points passed the equation A2 stress criteria with the exception of node 230B. For this node, equation A3 stress was calculated and was less than the allowable. Stresses for equations C2 and C3 are presented only for those nodes that are part of the quarter model.

The TMRPASS computer program was used, when possible, to aid in the stress calculations. The program; however, does not allow for intensification factors to be omitted in the torsional direction as does the B31.1 code, therefore, at any intensified nodes, the torsional moments are intensified.

Allowable stresses were obtained by using the maximum temperature experienced during any loading case to determine S_h . The value of S_c was based on 70°F per Reference 2. A summary of the allowable stresses is given in Table 6.1-1.

Section 119.6.1 of the B31.1 code indicates that the thermal range stress calculations shall be based on the range between the minimum and maximum temperature. The worst thermal moments due to all conditions considered were reviewed and found to be satisfactory.

Stresses were calculated as follows:

Pressure

$$\frac{Pd^2}{D^2-d^2}$$

Deadweight

$$\frac{.75i M_A}{Z}$$

Thermal

$$\frac{i M_C}{Z}$$

Seismic

$$\frac{.75i M_B}{Z}$$

Force/Time History

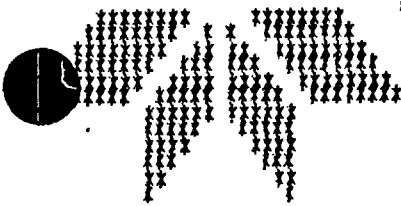
$$\frac{.75i M_D}{Z}$$

where:

- d = inside diameter of pipe
- D = outside diameter of pipe
- i = intensification factor
- M_A = resultant moment due to deadweight loadings
- M_B = resultant moment due to seismic loadings
- M_C = range of resultant moments due to thermal loadings
- M_D = resultant moment due to force/time history analysis



TELEDYNE ENGINEERING SERVICES



PROJECT: 5364 3 JUNE 1983
D. C. COOK UNIT 2
SUMMARY OF ALLOWABLES TABLE 6.1-1

BY *AMB* DATE *6-3-83*
CHKD *DMU* DATE *6/3/83*
SHEET NO. _____ OF _____

MAIN RISER

NODES	MATERIAL	TEMPERATURE (F)	Sh (PSI)
2 THRU 24	SA-358-316 CL 1	430	16210
26 THRU 36	'	326	16744
38 THRU 51	'	337	16678
52 THRU 71	'	354	16576
72 THRU 219	'	348	16612
222 THRU 226	SA-312-304	380	15070
228 THRU 230	'	413	14898

SRV LOOPS

NODES LOOP C	NODES LOOP B	NODES LOOP A	MATERIAL	TEMPERATURE (F)	Sh (PSI)
72 THRU 82	126 THRU 136	176 THRU 182	SA-312-304	348	15262
84 THRU 92	138 THRU 143	184 THRU 187	'	370	15130
97 THRU 96	144 THRU 146	188 THRU 190	'	430	14830
98	148	195	'	460	14710
103	152	196	'	460	11740 *
197	156	200	SA-376-316	653	11600 *
108 THRU 124	158 THRU 174	202 THRU 218	SA-376-316	653	16000

NOTE: LOOP C REFERS TO SRV LOOP CONTAINING VALVE SV-45C THIS IS TYPICAL OF LOOPS B AND A ALSO.
* ALLOWABLE AS PER NOTE (6), TABLE A-1 OF B 31.1.0, 1967 CODE.

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SUMMARY OF ALLOWABLES TABLE 6.1-1 Cont.

BY *AMB* DATE *6-3-83*
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PORV LOOP 151

NODES	MATERIAL	TEMPERATURE (F)	Sh (PSI)
230	SA-312-304	413	14898
286 THRU 290	.	480	14630
292 THRU 318	.	653	14300
320 THRU 342	SA-376-316	653	16000

PORV LOOP 152

NODES	MATERIAL	TEMPERATURE (F)	Sh (PSI)
340 THRU 344	SA-312-304	480	14630
346	SA-312-304	653	14300
350 THRU 356	SA-376-304	653	14300

PORV LOOP 153

NODES	MATERIAL	TEMPERATURE (F)	Sh (PSI)
232 THRU 236	SA-312-304	413	14898
238 THRU 260	SA-312-304	480	14630
262	SA-312-304	653	14300
266 THRU 284	SA-376-304	653	14300

NOTE: PORV LOOP 151 REFERS TO THE PORV LOOP CONTAINING VALVES NMO-151 AND NRV-151. THIS IS TYPICAL OF LOOPS 152 AND 153.

6.1.1 Equation A-1 Stresses

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STRESS SUMMARY - EQUATION A1

NODE #	PRESSURE STRESS (KSI)	DEADWEIGHT STRESS (KSI)	EQUATION A1 STRESS (KSI)	ALLOWABLE STRESS (KSI)
2	0	0	0	16.2
4		.3	.3	
6		.4	.4	
7		.2	.2	
8		.3	.3	
10		.7	.7	
12		1.0	1.0	
14		.5	.5	
16		.6	.6	
18		1.1	1.1	
20		1.5	1.5	
21		.8	.8	
24		.8	.8	↓
26		.8	.8	16.7
28		.9	.9	
32		.5	.5	
33		.9	.9	
34		1.0	1.0	
36		1.0	1.0	↓
38	↓	.9	.9	16.7

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STRESS SUMMARY - EQUATION A1

NODE #	PRESSURE STRESS (KSI)	DEADWEIGHT STRESS (KSI)	EQUATION A1 STRESS (KSI)	ALLOWABLE STRESS (KSI)
40	0	.4	.4	16.7
42		.3	.3	
44		.9	.9	
46		1.3	1.3	
48		.6	.6	
49		.6	.6	
50		.6	.6	
51		.4	.4	<u>1</u>
52		.4	.4	16.6
54		.2	.2	
56		.4	.4	
58		.6	.6	
60		.3	.3	
62		.6	.6	
64		.4	.4	
66		.3	.3	
68		.3	.3	
70		.2	.2	
71		.3	.3	<u>1</u>
72 R	<u>1</u>	.4	.4	16.6

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STRESS SUMMARY - EQUATION A1

NODE #	PRESSURE STRESS (KSI)	DEADWEIGHT STRESS (KSI)	EQUATION A1 STRESS (KSI)	ALLOWABLE STRESS (KSI)
72R	0	.6	.6	16.6
73		.4	.4	
126R		.6	.6	
126R		.6	.6	
127		.4	.4	
176R		.3	.3	
176R		.2	.2	
219		.4	.4	
222		1.5	1.5	15.1
224		2.9	2.9	
226		2.6	2.6	
228		1.3	1.3	14.9
230R		.9	.9	
230R		1.6	1.6	
232		3.0	3.0	
234		2.9	2.9	
236		2.0	2.0	
238		1.3	1.3	14.6
240R		1.1	1.1	
240R		1.3	1.3	

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STRESS SUMMARY - EQUATION A1

NODE #	PRESSURE STRESS (KSI)	DEADWEIGHT STRESS (KSI)	EQUATION A1 STRESS (KSI)	ALLOWABLE STRESS (KSI)
242	0	2.0	2.0	14.6
244		1.6	1.6	
246		1.2	1.2	
248		1.1	1.1	
250		1.5	1.5	
252		1.8	1.8	
258		1.7	1.7	
259		1.5	1.5	
257		2.6	2.6	
260		1.3	1.3	↓
262	↓	2.9	2.9	14.3
266	2.9	3.0	5.9	
268		3.6	6.5	
272		3.5	6.4	
274		2.7	5.6	
276		3.1	6.0	
278		3.4	6.3	
279		3.4	6.3	
280		2.2	5.1	
282	↓	1.6	4.5	↓

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STRESS SUMMARY - EQUATION A1

NODE #	PRESSURE STRESS (KSI)	DEADWEIGHT STRESS (KSI)	EQUATION A1 STRESS (KSI)	ALLOWABLE STRESS (KSI)
284B	2.9	.9	3.8	14.3
72B	0	2.0	2.0	15.3
74		1.0	1.0	
76		.6	.6	
78		.3	.3	
80		.3	.3	
82		.4	.4	
84		.4	.4	15.1
86		.3	.3	
88		1.2	1.2	
90		1.5	1.5	
92		.9	.9	
97		1.0	1.0	14.8
94		1.2	1.2	
100		.3	.3	
96		.5	.5	
98		.8	.8	14.7
103		.5	.5	11.7
107	3.5	.7	4.2	11.6
108	3.5	.8	4.3	16.0

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STRESS SUMMARY - EQUATION A1

NODE #	PRESSURE STRESS (KSI)	DEADWEIGHT STRESS (KSI)	EQUATION A1 STRESS (KSI)	ALLOWABLE STRESS (KSI)
110	3.5	.6	4.1	16.0
111		.6	4.1	
112		.6	4.1	
114		.3	3.8	
116		.3	3.8	
118		.6	4.1	
120		.7	4.2	
122		1.0	4.5	
124	↓	1.0	4.5	↓
126B	0	.7	.7	15.3
128		.4	.4	
130		.4	.4	
132		.4	.4	
134		.2	.2	
136		.2	.2	↓
138		1.0	1.0	15.1
140		1.4	1.4	
142		.8	.8	
143		.9	.9	↓
144	↓	1.1	1.1	14.8

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STRESS SUMMARY - EQUATION A1

NODE #	PRESSURE STRESS (KSI)	DEADWEIGHT STRESS (KSI)	EQUATION A1 STRESS (KSI)	ALLOWABLE STRESS (KSI)
145	0	.3	.3	14.8
146		.6	.6	14.8
148		1.0	1.0	14.7
152		.5	.5	11.7
156	3.5	.8	4.3	11.6
158		.9	4.4	16.0
160		.7	4.2	
161		.7	4.2	
162		.7	4.2	
164		.5	4.0	
166		.5	4.0	
168		.8	4.3	
170		.9	4.4	
172		1.2	4.7	
174	↓	1.2	4.7	↓
176 B	0	.7	.7	15.3
178		.6	.6	
180		.3	.3	
182		.3	.3	↓
184	↓	.9	.9	15.1

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STRESS SUMMARY - EQUATION A1

NODE #	PRESSURE STRESS (KSI)	DEADWEIGHT STRESS (KSI)	EQUATION A1 STRESS (KSI)	ALLOWABLE STRESS (KSI)
186	0	1.3	1.3	15.1
187		.9	.9	15.1
188		1.0	1.0	14.8
192		.3	.3	
190		.5	.5	↓
195		1.0	1.0	14.7
196	↓	.6	.6	11.7
200	3.5	.8	4.3	11.6
202		.9	4.4	16.0
204		.6	4.1	
205		.6	4.1	
206		.6	4.1	
208		.3	3.8	
210		.3	3.8	
212		.7	4.2	
214		.8	4.3	
216		1.1	4.6	
218	↓	1.1	4.6	↓
230B	0	3.2	3.2	14.9
286	0	6.4	6.4	14.6

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STRESS SUMMARY - EQUATION A1

NODE #	PRESSURE STRESS (KSI)	DEADWEIGHT STRESS (KSI)	EQUATION A1 STRESS (KSI)	ALLOWABLE STRESS (KSI)
288	0	6.7	6.7	14.6
290	↓	3.6	3.6	14.6
292	↓	3.9	3.9	14.3
296	2.9	2.1	5.0	
298	↓	1.4	4.3	
302	↓	1.8	4.7	
304	↓	2.5	5.4	
306	↓	2.0	4.9	
308	↓	1.7	4.6	
310	↓	1.3	4.2	
312	↓	3.2	6.1	
314	↓	..9	3.8	
316	↓	1.1	4.0	
318	4.1	5.6	9.7	↓
320R	↓	4.3	8.4	16.0
320R	↓	3.1	7.2	
322	↓	3.3	7.4	
324	↓	3.1	7.2	
325	↓	3.1	7.2	
326	↓	2.7	6.8	↓

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STRESS SUMMARY - EQUATION A1

NODE #	PRESSURE STRESS (KSI)	DEADWEIGHT STRESS (KSI)	EQUATION A1 STRESS (KSI)	ALLOWABLE STRESS (KSI)
328	4.1	2.5	6.6	16.0
330	↓	2.4	6.5	
332	↓	2.6	6.7	
334	3.5	.8	4.3	↓
336		.7	4.2	↓
284R		.7	4.2	16.0
284R		.6	4.1	↓
338		.4	3.9	↓
339		.6	4.1	↓
340	↓	.7	4.2	↓
342	↓	.8	4.3	↓
240B	0	1.3	1.3	14.6
241	↓	1.3	1.3	↓
402		3.5	3.5	↓
404		4.7	4.7	↓
344	↓	3.5	3.5	↓
346	↓	.9	.9	14.3
350	2.9	.7	3.6	↓
352	↓	.9	3.8	↓
356	↓	.4	3.3	↓



6.1.2 Equation A-2 Stresses



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STRESS SUMMARY - EQUATION A2

NODE #	NORMAL THERMAL STRESS (KSI)	ALLOWABLE STRESS (KSI)
2	.7	27.6
4	7.2	
6	6.7	
7	2.5	
8	2.6	
10	7.4	
12	8.2	
14	3.2	
16	3.7	
18	10.1	
20	8.8	
21	3.3	
24	3.3	
26	5.4	27.7
28	7.2	
32	2.7	
33	7.4	
34	9.2	
36	10.4	
38	10.7	

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STRESS SUMMARY - EQUATION A2

NODE #	NORMAL THERMAL STRESS (KSI)	ALLOWABLE STRESS (KSI)
40	9.8	27.7
42	9.9	
44	12.0	
46	11.9	
48	2.6	
49	2.5	
50	2.3	
51	1.4	
52	2.8	
54	2.8	
56	2.8	
58	2.9	
60	1.1	
62	2.9	
64	2.8	
66	2.9	
68	3.1	
70	1.1	
71	1.1	
72R	2.3	↓

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STRESS SUMMARY - EQUATION A2

NODE #	NORMAL THERMAL STRESS (KSI)	ALLOWABLE STRESS (KSI)
72 R	2.2	27.7
73	1.1	
126R	1.7	
126R	2.1	
127	.6	
176R	.9	
176R	2.8	
219	4.5	↓
222	10.3	27.2
224	12.2	
226	10.2	
228	4.5	
230R	7.5	
230R	2.5	
232	3.0	
234	2.9	
236	3.3	↓
238	7.2	27.1
240R	8.7	↓
240R	12.1	↓



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STRESS SUMMARY - EQUATION A2

NODE #	NORMAL THERMAL STRESS (KSI)	ALLOWABLE STRESS (KSI)
242	9.8	27.1
244	11.2	
246	16.7	
248	13.2	
250	23.5	
252	14.2	
258	9.5	
259	9.2	
257	16.4	
260	15.2	
262	8.1	27.0
266	4.2	
268	3.9	
272	3.8	
274	3.9	
276	4.0	
278	4.2	
279	4.1	
280	5.1	
282	5.3	

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STRESS SUMMARY - EQUATION A2

NODE #	NORMAL THERMAL STRESS (KSI)	ALLOWABLE STRESS (KSI)
284 B	6.4	27.0
72 B	4.3	27.3
74	2.5	
76	2.2	
78	1.9	
80	1.8	
82	2.1	
84	2.5	27.2
86	2.4	
88	5.0	
90	4.6	
92	1.9	
97	.6	27.1
94	.9	
100	1.0	
96	2.2	
98	2.8	
103	1.2	26.4
107	.5	26.4
108	.5	27.4

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STRESS SUMMARY - EQUATION A2

NODE #	NORMAL THERMAL STRESS (KSI)	ALLOWABLE STRESS (KSI)
110	.7	27.4
111	.6	
112	.7	
114	.8	
116	.8	
118	.8	
120	.8	
122	.8	
124	.7	↓
126 B	6.8	27.3
128	3.0	
130	2.5	
132	2.5	
134	2.8	
136	2.9	↓
138	6.7	27.2
140	6.3	
142	2.6	
143	.9	
144	1.0	↓

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STRESS SUMMARY - EQUATION A2

NODE #	NORMAL THERMAL STRESS (KSI)	ALLOWABLE STRESS (KSI)
145	1.5	27.1
146	4.7	27.1
148	5.4	27.1
152	1.8	26.4
156	1.7	26.4
158	.9	27.4
160	1.2	
161	1.1	
162	1.2	
164	1.4	
166	1.3	
168	1.2	
170	1.2	
172	1.2	
174	1.1	↓
176B	10.0	27.3
178	4.5	27.3
180	3.5	27.3
182	3.3	27.3
184	7.9	27.2

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STRESS SUMMARY - EQUATION A2

NODE #	NORMAL THERMAL STRESS (KSI)	ALLOWABLE STRESS (KSI)
186	7.4	27.2
187	.6	27.2
188	2.0	27.1
192	2.2	27.1
190	4.9	27.1
195	5.8	27.1
196	2.6	26.4
200	1.2	26.4
202	1.8	27.4
204	2.4	
205	2.2	
206	2.4	
208	2.7	
210	2.4	
212	2.2	
214	2.2	
216	2.2	
218	2.0	
230 B	29.6*	27.2
286	6.9	27.1

* EQUATION A3 STRESS IS $32.8 < 42.1 = 1.25 (S_C + S_H)$
 \therefore node. 230 B stress is acceptable

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STRESS SUMMARY - EQUATION A2

NODE #	NORMAL THERMAL STRESS (KSI)	ALLOWABLE STRESS (KSI)
288	10.3	27.1
290	5.3	27.1
292	5.0	27.0
296	2.8	
298	3.4	
302	4.3	
304	4.6	
306	5.6	
308	6.6	
310	5.4	
312	6.9	
314	1.7	
316	2.3	
318	1.7	↓
320 R	1.5	27.4
320 R	2.7	↓
322	2.3	
324	3.6	
325	3.0	
326	5.9	↓

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STRESS SUMMARY - EQUATION A2

NODE #	NORMAL THERMAL STRESS (KSI)	ALLOWABLE STRESS (KSI)
328	6.2	27.4
330	5.6	
332	6.3	
334	2.1	
336	2.6	
284 R	2.4	27.4
284 R	2.7	
338	3.9	
339	5.3	
340	5.6	
342	5.1	
240 B	15.3	27.1
241	5.7	
402	6.3	
404	11.2	
344	14.2	
346	7.2	27.0
350	3.5	
352	3.4	
356	3.9	

6.1.3 Equation B-1 Stresses

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STRESS SUMMARY - EQUATION B1

NODE #	PRESSURE STRESS (KSI)	DEADWEIGHT STRESS (KSI)	OBE STRESS (KSI)	EQUATION B1-STRESS (KSI)	ALLOWABLE STRESS (KSI)
2	0	0	0	0	19.5
4		.3	.2	.5 XY	
6		.4	0	.4 XY	
7		.2	0	.2 XY	
8		.3	0	.3 XY	
10		.7	.1	.8 XY	
12		1.0	0	1.0 XY	
14		.5	.1	.6 XY	
16		.6	0	.6 XY	
18		1.1	.1	1.2 XY	
20		1.5	.2	1.7 XY	
21		.8	0	.8 YZ	
24		.8	0	.8 YZ	↓
26		.8	.3	1.1 YZ	20.1
28		.9	.2	1.1 XY YZ	
32		.5	.1	.6 XY	
33		.9	.2	1.1 XY	
34		1.0	.1	1.1 XY	
36		1.0	.1	1.1 XY	↓
38	↓	.9	.2	1.1 XY	20.0

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CHECKED BY: SMB DATE: 5-4-83

STRESS SUMMARY - EQUATION B1

NODE #	PRESSURE STRESS (KSI)	DEADWEIGHT STRESS (KSI)	OBE STRESS (KSI)	EQUATION B1-STRESS (KSI)	ALLOWABLE STRESS (KSI)
40	0	.4	.2	.6 XY	20.0
42		.3	.3	.6 XY	
44		.9	.2	1.1 YZ	
46		1.3	.2	1.5 XY	
48		.6	.3	.9 YZ	
49		.6	.2	.8 YZ	
50		.6	.2	.8 XY	
51		.4	.3	.7 XY	↓
52		.4	.2	.6 XY YZ	19.9
54		.2	.1	.3 YZ	
56		.4	.1	.5 YZ	
58		.6	.2	.8 XY	
60		.3	.1	.4 XY	
62		.6	.2	.8 XY	
64		.4	.2	.6 XY	
66		.3	.2	.5 XY	
68		.3	.2	.5 XY	
70		.2	.3	.5 YZ	
71		.3	.4	.7 YZ	↓
72R	↓	.4	.8	1.2 YZ	19.9

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STRESS SUMMARY - EQUATION B1

NODE #	PRESSURE STRESS (KSI)	DEADWEIGHT STRESS (KSI)	OBE STRESS (KSI)	EQUATION B1-STRESS (KSI)	ALLOWABLE STRESS (KSI)
72R	0	.6	.8	1.4 YZ	19.9
73		.4	.6	1.0 YZ	
126 R		.6	.8	1.4 YZ	
126 R		.6	.9	1.5 YZ	
127		.4	.5	.9 YZ	
176 R		.3	.5	.8 YZ	
176 R		.2	.4	.6 YZ	
219		.4	1.1	1.5 YZ	↓
222		1.5	2.8	4.3 YZ	18.1
224		2.9	2.0	4.9 YZ	
226		2.6	2.5	5.1 YZ	↓
228		1.3	1.9	3.2 YZ	17.9
230 R		.9	2.4	3.3 YZ	
230 R		1.6	2.1	3.7 YZ	
232		3.0	2.3	5.3 YZ	
234		2.9	2.3	5.2 YZ	
236		2.0	2.2	4.2 YZ	↓
238		1.3	3.7	5.0 XY	17.6
240 R		1.1	4.0	5.1 XY	
240 R	↓	1.3	2.9	4.2 YZ	↓

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DONALD C. COOK
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STRESS SUMMARY - EQUATION B1

NODE #	PRESSURE STRESS (KSI)	DEADWEIGHT STRESS (KSI)	OBE STRESS (KSI)	EQUATION B1-STRESS (KSI)	ALLOWABLE STRESS (KSI)
242	0	2.0	3.5	5.5 YZ	17.6
244		1.6	2.6	4.2 YZ	
246		1.2	2.8	4.0 YZ	
248		1.1	4.0	5.1 YZ	
250		1.5	5.3	6.8 YZ	
252		1.8	7.7	9.5 YZ	
258		1.7	8.6	10.3 YZ	
259		1.5	7.6	9.1 YZ	
257		2.6	10.2	12.8 YZ	
260		1.3	7.8	9.1 YZ	
262		2.9	5.5	8.4 YZ	17.2
266	2.9	3.0	2.3	9.2 XY	
268		3.6	2.4	8.9 YZ	
272		3.5	3.1	9.5 YZ	
274		2.7	2.9	8.5 YZ	
276		3.1	2.8	8.8 YZ	
278		3.4	2.9	9.2 YZ	
279		3.4	2.9	9.2 YZ	
280		2.2	4.7	9.8 YZ	
282		1.6	5.1	9.6 YZ	

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DONALD C. COOK
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STRESS SUMMARY - EQUATION B1

NODE #	PRESSURE STRESS (KSI)	DEADWEIGHT STRESS (KSI)	OBE STRESS (KSI)	EQUATION B1-STRESS (KSI)	ALLOWABLE STRESS (KSI)
284B	2.9	.9	6.7	10.5 YZ	17.2
72B	0	2.0	1.1	3.1 XY	18.3
74		1.0	.7	1.7 XY	
76		.6	.5	1.1 XY	
78		.3	.4	.7 XY	
80		.3	.2	.5 XY	
82		.4	.3	.7 YZ	↓
84		.4	.6	1.0 YZ	18.2
86		.3	.7	1.0 YZ	
88		1.2	1.2	2.4 YZ	
90		1.5	1.4	2.9 YZ	
92		.9	.8	1.7 YZ	↓
97		1.0	.9	1.9 YZ	17.8
94		1.2	1.3	2.5 YZ	↑
100		.3	1.3	1.6 YZ	↓
96		.5	2.3	2.8 YZ	↓
98		.8	2.4	3.2 YZ	17.7
103	↓	.5	1.4	1.9 YZ	14.1
107	3.5	.7	.4	4.6 XY	13.9
108	3.5	.8	2.2	6.5 YZ	19.2

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STRESS SUMMARY - EQUATION B1

NODE #	PRESSURE STRESS (KSI)	DEADWEIGHT STRESS (KSI)	OBE STRESS (KSI)	EQUATION B1-STRESS (KSI)	ALLOWABLE STRESS (KSI)
110	3.5	.6	2.5	6.6 YZ	19.2
111		.6	2.5	6.6 YZ	
112		.6	2.5	6.6 YZ	
114		.3	2.2	6.0 YZ	
116		.3	1.4	5.2 YZ	
118		.6	1.2	5.3 YZ	
120		.7	1.2	5.4 YZ	
122		1.0	1.3	5.8 XY	
124	↓	1.0	1.3	5.8 XY	↓
126B	0	.7	1.0	1.7 XY	18.3
128		.4	.4	.8 XY	
130		.4	.3	.7 YZ	
132		.4	.4	.8 XY	
134		.2	.7	.9 XY	
136		.2	1.0	1.2 XY	↓
138		1.0	2.0	3.0 XY	18.2
140		1.4	2.1	3.5 XY	
142		.8	1.3	2.1 XY	
143		.9	1.3	2.2 XY	↓
144	↓	1.1	1.3	2.4 XY	17.8



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STRESS SUMMARY - EQUATION B1

NODE #	PRESSURE STRESS (KSI)	DEADWEIGHT STRESS (KSI)	OBE STRESS (KSI)	EQUATION B1-STRESS (KSI)	ALLOWABLE STRESS (KSI)
145	0	.3	1.4	1.7 XY	17.8
146		.6	3.2	3.8 XY	17.8
148		1.0	3.3	4.3 XY	17.7
152	↓	.5	1.5	2.0 XY	14.1
156	3.5	.8	.5	4.8 YZ	13.9
158		.9	2.5	6.9 XY	19.2
160		.7	2.9	7.1 XY	
161		.7	2.9	7.1 XY	
162		.7	2.9	7.1 XY	
164		.5	2.5	6.5 XY	
166		.5	1.5	5.5 XY	
168		.8	1.2	5.5 YZ	
170		.9	1.3	5.7 YZ	
172		1.2	1.5	6.2 YZ	
174	↓	1.2	1.5	6.2 YZ	↓
176B	0	.7	.7	1.4 YZ	18.3
178		.6	.4	1.0 YZ	
180		.3	.8	1.1 YZ	
182		.3	1.3	1.6 YZ	↓
184	↓	.9	2.5	3.4 YZ	18.2

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STRESS SUMMARY - EQUATION B1

NODE #	PRESSURE STRESS (KSI)	DEADWEIGHT STRESS (KSI)	OBE STRESS (KSI)	EQUATION B1-STRESS (KSI)	ALLOWABLE STRESS (KSI)
186	0	1.3	2.5	3.8 YZ	18.2
187		.9	1.2	2.1 YZ	18.2
188		1.0	1.1	2.1 YZ	17.8
192		.3	1.1	1.4 YZ	17.8
190		.5	1.9	2.4 YZ	17.8
195		1.0	1.9	2.9 YZ	17.7
196		.6	1.1	1.7 YZ	14.1
200	3.5	.8	.5	4.8 XY	13.9
202		.9	2.2	6.6 YZ	19.2
204		.6	2.6	6.7 YZ	
205		.6	2.6	6.7 YZ	
206		.6	2.6	6.7 YZ	
208		.3	2.3	6.1 YZ	
210		.3	1.4	5.2 YZ	
212		.7	1.1	5.3 XY	
214		.8	1.2	5.5 XY	
216		1.1	1.4	6.0 XY	
218		1.1	1.4	6.0 XY	
230B	0	3.2	9.5	12.7 YZ	17.9
286	0	6.4	6.3	12.7 YZ	17.6

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STRESS SUMMARY - EQUATION B1

NODE #	PRESSURE STRESS (KSI)	DEADWEIGHT STRESS (KSI)	OBE STRESS (KSI)	EQUATION B1-STRESS (KSI)	ALLOWABLE STRESS (KSI)
288	0	6.7	5.8	12.5 YZ	17.6
290	↓	3.6	4.7	8.3 YZ	17.6
292	↓	3.9	5.2	9.1 YZ	17.2
296	2.9	2.1	4.0	9.0 YZ	
298		1.4	3.5	7.8 YZ	
302		1.8	4.0	8.7 YZ	
304		2.5	3.8	9.2 YZ	
306		2.0	3.8	8.7 YZ	
308		1.7	4.0	8.6 YZ	
310		1.3	3.9	8.1 YZ	
312		3.2	3.4	9.5 YZ	
314		.9	2.6	6.4 YZ	
316	↓	1.1	2.6	6.6 YZ	
318	4.1	5.6	1.9	11.6 XY	↓
320 R		4.3	1.4	9.8 XY	19.2
320 R		3.1	1.5	8.7 YZ	
322		3.3	1.6	9.0 YZ	
324		3.1	1.6	8.8 YZ	
325		3.1	1.6	8.8 YZ	
326	↓	2.7	1.9	8.7 YZ	↓

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DONALD C. COOK
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STRESS SUMMARY - EQUATION B1

NODE #	PRESSURE STRESS (KSI)	DEADWEIGHT STRESS (KSI)	OBE STRESS (KSI)	EQUATION B1-STRESS (KSI)	ALLOWABLE STRESS (KSI)
328	4.1	2.5	1.7	8.3 YZ	17.2
330	↓	2.4	1.7	8.2 YZ	19.2
332	↓	2.6	2.1	8.8 YZ	↓
334	3.5	.8	.6	4.9 YZ	↓
336	↓	.7	.7	4.9 YZ	↓
284R	↓	.7	.6	4.8 YZ	19.2
284R	↓	.6	.8	4.9 YZ	↓
338	↓	.4	.9	4.8 YZ	↓
339	↓	.6	1.1	5.2 YZ	↓
340	↓	.7	1.2	5.4 YZ	↓
342	↓	.8	1.1	5.4 YZ	↓
240B	0	1.3	6.9	8.2 XY	17.6
241	↓	1.3	5.4	6.7 XY	↓
402	↓	3.5	4.0	7.5 XY	↓
404	↓	4.7	5.3	10.0 XY	↓
344	↓	3.5	4.7	8.2 XY	↓
346	↓	.9	4.0	4.9 XY	17.2
350	2.9	.7	3.1	6.7 XY	↓
352	↓	.9	2.7	6.5 XY	↓
356	↓	.4	3.1	6.4 XY	↓

6.1.4 Equation B-2 Stresses

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DONALD C. COOK
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STRESS SUMMARY - EQUATION B2

NODE #	PRESSURE STRESS (KSI)	DEADWEIGHT STRESS (KSI)	OBE STRESS (KSI)	PORV TRANSIENT SHOCK STRESS(KSI)	EQUATION B2 STRESS (KSI)	ALLOWABLE STRESS (KSI)
2	.6	0	0	0	.6	19.5
4		.3	.2	.1	1.1	
6		.4	0	0	1.0	
7		.2	0	0	.8	
8		.3	0	0	.9	
10		.7	.1	0	1.4	
12		1.0	0	0	1.6	
14		.5	.1	.1	1.2	
16		.6	0	.1	1.3	
18		1.1	.1	.1	1.8	
20		1.5	.2	.1	2.3	
21	.7	.8	0	.1	1.6	
24		.8	0	.1	1.6	
26		.8	.3	.2	1.9	20.1
28		.9	.2	.1	1.8	
32		.5	.1	.1	1.3	
33		.9	.2	.1	1.8	
34		1.0	.1	.1	1.8	
36		1.0	.1	.1	1.8	
38		.9	.2	.1	1.8	20.0

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DONALD C. COOK
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STRESS SUMMARY - EQUATION B2

NODE #	PRESSURE STRESS (KSI)	DEADWEIGHT STRESS (KSI)	OBE STRESS (KSI)	PORV TRANSIENT SHOCK STRESS (KSI)	EQUATION B2 STRESS (KSI)	ALLOWABLE STRESS (KSI)
40	.7	.4	.2	.2	1.4	20.0
42		.3	.3	.2	1.4	
44		.9	.2	.2	1.9	
46		1.3	.2	.1	2.2	
48		.6	.3	.4	1.8	
49		.6	.2	.4	1.7	
50		.6	.2	.4	1.7	
51		.4	.3	.5	1.7	↓
52		.4	.2	.2	1.4	19.9
54		.2	.1	.1	1.0	
56		.4	.1	.1	1.2	
58		.6	.2	.2	1.6	
60		.3	.1	.2	1.2	
62		.6	.2	.2	1.6	
64		.4	.2	.2	1.4	
66		.3	.2	.2	1.3	
68		.3	.2	.2	1.3	
70		.2	.3	.3	1.3	
71	↓	.3	.4	.2	1.4	
72R	.9	.4	.8	.2	2.1	↓



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STRESS SUMMARY - EQUATION B2

NODE #	PRESSURE STRESS (KSI)	DEADWEIGHT STRESS (KSI)	OBE STRESS (KSI)	PORV TRANSIENT SHOCK STRESS (KSI)	EQUATION B2 STRESS (KSI)	ALLOWABLE STRESS (KSI)
72R	.9	.6	.8	.2	2.3	19.9
73		.4	.6	.2	1.9	
126R		.6	.8	.2	2.3	
126R		.6	.9	.2	2.4	
127		.4	.5	.3	1.9	
176R		.3	.5	.2	1.7	
176R		.2	.4	.1	1.5	
219	<u>1</u>	.4	1.1	.6	2.6	<u>1</u>
222	1.0	1.5	2.8	.9	5.4	18.1
224	1.0	2.9	2.0	.6	6.0	<u>1</u>
226	1.0	2.6	2.5	.4	6.1	<u>1</u>
228	1.5	1.3	1.9	.5	4.8	17.9
230R	1.5	.9	2.4	.8	4.9	
230R	1.5	1.6	2.1	.5	5.3	
232	1.5	3.0	2.3	1.1	7.0	
234	1.1	2.9	2.3	1.0	6.5	
236	1.1	2.0	2.2	1.3	5.7	<u>1</u>
238	2.3	1.3	3.7	1.7	7.7	17.6
240R	2.3	1.1	4.0	1.2	7.6	<u>1</u>
240R	2.3	1.3	2.9	1.2	6.7	<u>1</u>

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STRESS SUMMARY - EQUATION B2

NODE #	PRESSURE STRESS (KSI)	DEADWEIGHT STRESS (KSI)	OBE STRESS (KSI)	PORV TRANSIENT SHOCK STRESS (KSI)	EQUATION B2 STRESS (KSI)	ALLOWABLE STRESS (KSI)
242	2.3	2.0	3.5	1.3	8.0	17.6
244		1.6	2.6	1.8	7.1	
246		1.2	2.8	2.2	7.1	
248		1.1	4.0	1.8	7.8	
250		1.5	5.3	1.8	9.4	
252		1.8	7.7	1.4	11.9	
258		1.7	8.6	2.4	12.9	
259		1.5	7.6	2.8	11.9	
257		2.6	10.2	2.8	15.5	
260	↓	1.3	7.8	2.5	11.8	↓
262	2.9	2.9	5.5	3.9	12.5	17.2
266		3.0	2.3	4.5	11.0	
268		3.6	2.4	3.7	10.9	
272		3.5	3.1	4.0	11.5	
274		2.7	2.9	1.3	8.8	
276		3.1	2.8	1.1	9.0	
278		3.4	2.9	1.3	9.5	
279		3.4	2.9	1.3	9.5	
280		2.2	4.7	1.7	10.1	
282	↓	1.6	5.1	1.3	9.8	↓

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DONALD C. COOK
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STRESS SUMMARY - EQUATION B2

NODE #	PRESSURE STRESS (KSI)	DEADWEIGHT STRESS (KSI)	OBE STRESS (KSI)	PORV TRANSIENT SHOCK STRESS (KSI)	EQUATION B2 STRESS (KSI)	ALLOWABLE STRESS (KSI)
284B	2.9	.9	6.7	4.4	11.9	17.2
72B	.7	2.0	1.1	.3	3.9	18.3
74		1.0	.7	.2	2.4	
76		.6	.5	.2	1.8	
78		.3	.4	.3	1.5	
80		.3	.2	.2	1.3	
82		.4	.3	.2	1.5	
84	.3	.4	.6	.2	1.3	18.2
86		.3	.7	.1	1.3	
88		1.2	1.2	.1	2.7	
90		1.5	1.4	.1	3.2	
92		.9	.9	.2	2.0	
97		1.0	.9	.2	2.2	17.8
94		1.2	1.3	.1	2.8	
100		.3	1.3	.1	1.9	
96		.5	2.3	.1	3.1	
98	.1	.8	2.4	.1	3.3	17.7
103	.1	.5	1.4	.1	2.0	14.1
107	3.5	.7	.4	0	4.6	13.9
108	3.5	.8	2.2	0	6.5	19.2

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DONALD C. COOK
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STRESS SUMMARY - EQUATION B2

NODE #	PRESSURE STRESS (KSI)	DEADWEIGHT STRESS (KSI)	OBE STRESS (KSI)	PORV TRANSIENT SHOCK STRESS(KSI)	EQUATION B2 STRESS (KSI)	ALLOWABLE STRESS (KSI)
110	3.5	.6	2.5	0	6.6	19.2
111		.6	2.5	0	6.6	
112		.6	2.5	0	6.6	
114		.3	2.2	0	6.0	
116		.3	1.4	0	5.2	
118		.6	1.2	.1	5.3	
120		.7	1.2	.1	5.4	
122		1.0	1.3	.1	5.8	
124	↓	1.0	1.3	.1	5.8	↓
126 B	.7	.7	1.0	.6	2.6	18.3
128		.4	.4	.4	1.7	
130		.4	.3	.2	1.5	
132		.4	.4	.2	1.5	
134		.2	.7	.2	1.6	
136	↓	.2	1.0	.2	1.9	↓
138	.3	1.0	2.0	.2	3.3	18.2
140		1.4	2.1	.3	3.8	
142		.8	1.3	.3	2.4	
143		.9	1.3	.2	2.5	↓
144	↓	1.1	1.3	.1	2.7	17.8

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STRESS SUMMARY - EQUATION B2

NODE #	PRESSURE STRESS (KSI)	DEADWEIGHT STRESS (KSI)	OBE STRESS (KSI)	PORV TRANSIENT SHOCK STRESS (KSI)	EQUATION B2 STRESS (KSI)	ALLOWABLE STRESS (KSI)
145	.3	.3	1.4	.1	2.0	17.8
146	.3	.6	3.2	.1	4.1	17.8
148	.1	1.0	3.3	.1	4.4	17.7
152	.1	.5	1.5	.1	2.1	14.1
156	3.5	.8	.5	.1	4.8	13.9
158		.9	2.5	.1	6.9	19.2
160		.7	2.9	0	7.1	
161		.7	2.9	.1	7.1	
162		.7	2.9	.1	7.1	
164		.5	2.5	0	6.5	
166		.5	1.5	.1	5.5	
168		.8	1.2	.1	5.5	
170		.9	1.3	.1	5.7	
172		1.2	1.5	.1	6.2	
174		1.2	1.5	.1	6.2	
176B	.7	.7	.7	.3	2.2	18.3
178		.6	.4	.2	1.7	
180		.3	.8	.5	1.9	
182		.3	1.3	.1	2.3	
184	.3	.9	2.5	.1	3.7	18.2

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STRESS SUMMARY - EQUATION B2

NODE #	PRESSURE STRESS (KSI)	DEADWEIGHT STRESS (KSI)	OBE STRESS (KSI)	PORV TRANSIENT SHOCK STRESS(KSI)	EQUATION B2 STRESS (KSI)	ALLOWABLE STRESS (KSI)
186	.3	1.3	2.5	.1	4.1	18.2
187		.9	1.2	.1	2.4	18.2
188		1.0	1.1	.1	2.4	17.8
192		.3	1.1	.1	1.7	17.8
190		.5	1.9	.1	2.7	17.8
195	.1	1.0	1.9	.1	3.0	17.7
196	.1	.6	1.1	.1	1.8	14.1
200	3.5	.8	.5	.1	4.8	13.9
202		.9	2.2	.1	6.6	19.2
204		.6	2.6	.1	6.7	
205		.6	2.6	.1	6.7	
206		.6	2.6	.1	6.7	
208		.3	2.3	.1	6.1	
210		.3	1.4	.1	5.2	
212		.7	1.1	.1	5.3	
214		.8	1.2	.1	5.5	
216		1.1	1.4	.1	6.0	
218		1.1	1.4	.1	6.0	
230B	1.9	3.2	9.5	3.1	15.1	17.9
286	1.9	6.4	6.3	1.3	14.7	17.6

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STRESS SUMMARY - EQUATION B2

NODE #	PRESSURE STRESS (KSI)	DEADWEIGHT STRESS (KSI)	OBE STRESS (KSI)	PORV TRANSIENT SHOCK STRESS (KSI)	EQUATION B2 STRESS (KSI)	ALLOWABLE STRESS (KSI)
288	1.9	6.7	5.8	1.2	14.5	17.6
290	1.9	3.6	4.7	2.8	11.0	17.6
292	1.9	3.9	5.2	4.6	12.7	17.2
296	2.9	2.1	4.0	4.2	10.8	
298		1.4	3.5	3.4	9.2	
302		1.8	4.0	2.9	9.6	
304		2.5	3.8	2.4	9.9	
306		2.0	3.8	2.4	9.4	
308		1.7	4.0	1.7	8.9	
310		1.3	3.9	1.3	8.3	
312		3.2	3.4	4.0	11.3	
314		.9	2.6	1.5	6.8	
316	↓	1.1	2.6	2.5	7.6	
318	4.1	5.6	1.9	2.3	12.7	↓
320R		4.3	1.4	1.9	10.8	19.2
320R		3.1	1.5	2.3	9.9	
322		3.3	1.6	2.0	10.0	
324		3.1	1.6	1.2	9.2	
325		3.1	1.6	1.2	9.2	
326	↓	2.7	1.9	2.5	9.9	↓

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STRESS SUMMARY - EQUATION B2

NODE #	PRESSURE STRESS (KSI)	DEADWEIGHT STRESS (KSI)	OBE STRESS (KSI)	PORV TRANSIENT SHOCK STRESS(KSI)	EQUATION B2 STRESS (KSI)	ALLOWABLE STRESS (KSI)
328	4.1	2.5	1.7	2.3	9.5	17.2
330	4.1	2.4	1.7	2.1	9.2	19.2
332	4.1	2.6	2.1	2.1	9.7	
334	3.5	.8	.6	.6	5.1	
336		.7	.7	.7	5.2	
284R		.7	.6	.9	5.3	
284R		.6	.8	.9	5.3	
338		.4	.9	.4	4.9	
339		.6	1.1	.7	5.4	
340		.7	1.2	1.2	5.9	
342	↓	.8	1.1	1.2	5.9	↓
240B	1.9	1.3	6.9	1.9	10.4	17.6
241		1.3	5.4	1.4	8.8	
402		3.5	4.0	1.5	9.7	
404		4.7	5.3	1.5	12.1	
344		3.5	4.7	1.8	10.4	↓
346	↓	.9	4.0	4.8	9.0	17.2
350	2.9	.7	3.1	2.8	7.8	
352	2.9	.9	2.7	3.6	8.3	
356	2.9	.4	3.1	4.7	8.9	↓

6.1.5 Equation B-3 Stresses

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STRESS SUMMARY - EQUATION B3

NODE #	PORV TRANSIENT THERMAL STRESS RANGE KSI	ALLOWABLE STRESS (KSI)
2	.2	27.6
4	2.1	
6	2.3	
7	.8	
8	.9	
10	2.4	
12	2.5	
14	.9	
16	1.0	
18	2.7	
20	2.7	
21	1.0	
24	1.0	
26	1.8	27.7
28	1.7	
32	.6	
33	1.7	
34	2.0	
36	2.2	
38	2.3	



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STRESS SUMMARY - EQUATION B3

NODE #	PORV TRANSIENT THERMAL STRESS RANGE KSI	ALLOWABLE STRESS (KSI)
40	2.3	27.7
42	2.3	
44	2.6	
46	3.2	
48	1.4	
49	1.4	
50	1.3	
51	.7	
52	.6	
54	.5	
56	.5	
58	.4	
60	.2	
62	.4	
64	.5	
66	.7	
68	1.0	
70	1.0	
71	1.6	
72 R	3.6	

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STRESS SUMMARY - EQUATION B3

NODE #	PORV TRANSIENT THERMAL STRESS RANGE KSI	ALLOWABLE STRESS (KSI)
72R	3.8	27.7
73	1.7	
126R	2.6	
126R	3.3	
127	1.1	
176R	1.3	
176R	2.4	
219	2.7	
222	18.3	27.2
224	5.0	
226	6.8	
228	2.8	
230R	4.0	
230R	6.1	
232	3.8	
234	8.7	
236	6.0	
238	7.3	27.1
240R	3.2	
240R	6.9	



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STRESS SUMMARY - EQUATION B3

NODE #	PORV TRANSIENT THERMAL STRESS RANGE KSI	ALLOWABLE STRESS (KSI)
242	8.0	27.1
244	5.9	
246	2.8	
248	2.4	
250	4.3	
252	4.9	
258	3.0	
259	2.8	
257	5.0	
260	4.4	
262	2.3	27.0
266	1.4	
268	2.0	
272	2.6	
274	3.1	
276	3.4	
278	3.3	
279	3.3	
280	1.9	
282	1.5	

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STRESS SUMMARY - EQUATION B3

NODE #	PORV TRANSIENT THERMAL STRESS RANGE KSI	ALLOWABLE STRESS (KSI)
284 B	1.2	27.0
72 B	4.1	27.3
74	2.6	
76	5.6	
78	6.8	
80	5.8	
82	2.6	↓
84	3.6	27.2
86	2.8	
88	5.0	
90	4.3	
92	1.8	↓
97	1.5	27.1
94	2.2	
100	2.3	
96	5.1	
98	5.8	↓
103	2.6	26.4
107	1.1	26.4
108	.7	27.4

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STRESS SUMMARY - EQUATION B3

NODE #	PORV TRANSIENT THERMAL STRESS RANGE KSI	ALLOWABLE STRESS (KSI)
110	.7	27.4
111	.6	
112	.7	
114	.8	
116	1.1	
118	1.2	
120	1.2	
122	1.2	
124	1.1	↓
126 B	4.3	27.3
128	2.4	
130	2.1	
132	1.7	
134	1.1	
136	.8	↓
138	1.9	27.2
140	2.2	
142	.9	
143	.7	
144	.5	↓

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STRESS SUMMARY - EQUATION B3

NODE #	PORV TRANSIENT THERMAL STRESS RANGE KSI	ALLOWABLE STRESS (KSI)
145	.5	27.1
146	1.4	↓
148	1.0	
152	.3	26.4
156	.3	26.4
158	.5	27.4
160	.6	↓
161	.5	
162	.6	↓
164	.6	
166	.5	↓
168	.4	
170	.4	↓
172	.4	
174	.3	↓
176B	6.3	
178	3.3	↓
180	2.4	
182	1.3	↓
184	2.3	

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STRESS SUMMARY - EQUATION B3

NODE #	PORV TRANSIENT THERMAL STRESS RANGE KSI	ALLOWABLE STRESS (KSI)
186	2.0	27.2
187	.6	27.2
188	.7	27.1
192	.7	
190	1.6	
195	2.5	↓
196	1.1	26.4
200	.7	26.4
202	.7	27.4
204	.8	
205	.7	
206	.8	
208	1.0	
210	1.1	
212	1.0	
214	1.0	
216	.9	
218	.8	↓
230 B	8.0	27.2
286	3.5	27.1



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STRESS SUMMARY - EQUATION B3

NODE #	PORV TRANSIENT THERMAL STRESS RANGE KSI	ALLOWABLE STRESS (KSI)
288	5.5	27.1
290	3.0	27.1
292	2.9	27.0
296	1.6	
298	1.7	
302	1.8	
304	1.9	
306	2.1	
308	2.4	
310	2.0	
312	2.3	
314	1.0	
316	1.9	
318	1.8	
320 R	1.8	27.4
320 R	2.7	
322	1.3	
324	3.9	
325	3.2	
326	6.1	

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STRESS SUMMARY - EQUATION B3

NODE #	PORV TRANSIENT THERMAL STRESS RANGE KSI	ALLOWABLE STRESS (KSI)
328	6.2	27.4
330	5.4	
332	6.0	
334	2.0	
336	2.4	
284 R	2.3	
284 R	2.3	
338	4.0	
339	5.5	
340	5.9	
342	5.4	↓
240 B	20.0	27.1
241	2.3	
402	5.8	
404	10.4	
344	18.9	↓
346	9.7	27.0
350	4.6	
352	3.6	
356	3.2	↓

6.1.6 Equation C-1 Stresses

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STRESS SUMMARY - EQUATION C1

NODE #	PRESSURE STRESS (KSI)	DEADWEIGHT STRESS (KSI)	DBE STRESS (KSI)	EQUATION C1 STRESS (KSI)	ALLOWABLE STRESS (KSI)
2	0	0	0	0	29.2
4		.3	.3	.6 XY	
6		.4	.1	.5 XY	
7		.2	.1	.3 XY	
8		.3	0	.3 XY	
10		.7	.1	.8 XY	
12		1.0	.1	1.1 XY	
14		.5	.1	.6 XY	
16		.6	.1	.7 XY	
18		1.1	.2	1.3 XY	
20		1.5	.3	1.8 YZ	
21		.8	.1	.9 YZ	
24		.8	.1	.9 YZ	↓
26		.8	.5	1.3 YZ	30.1
28		.9	.4	1.3 YZ	
32		.5	.1	.6 XY	
33		.9	.3	1.2 XY	
34		1.0	.3	1.3 XY	
36		1.0	.3	1.3 XY	↓
38	↓	.9	.3	1.2 XY	30.0

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STRESS SUMMARY - EQUATION C1

NODE #	PRESSURE STRESS (KSI)	DEADWEIGHT STRESS (KSI)	DBE STRESS (KSI)	EQUATION C1 STRESS (KSI)	ALLOWABLE STRESS (KSI)
40	0	.4	.4	.8 XY	30.0
42		.3	.5	.8 XY	
44		.9	.4	1.3 YZ	
46		1.3	.3	1.6 XY	
48		.6	.5	1.1 YZ	
49		.6	.4	1.0 YZ	
50		.6	.3	.9 XY	
51		.4	.5	.9 XY	↓
52		.4	.3	.7 XY	29.3
54		.2	.3	.5 YZ	
56		.4	.2	.6 YZ	
58		.6	.4	1.0 XY	
60		.3	.2	.5 XY	
62		.6	.4	1.0 XY	
64		.4	.4	.8 XY	
66		.3	.3	.6 XY	
68		.3	.4	.7 XY	
70		.2	.5	.7 YZ	
71		.3	.7	1.0 YZ	↓
72R	↓	.4	1.2	1.6 YZ	29.9

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STRESS SUMMARY - EQUATION C1

NODE #	PRESSURE STRESS (KSI)	DEADWEIGHT STRESS (KSI)	DBE STRESS (KSI)	EQUATION C1 STRESS (KSI)	ALLOWABLE STRESS (KSI)
72R	0	.6	1.3	1.9 YE	29.9
73		.4	.9	1.3 YE	
126R		.6	1.2	1.8 YE	
126R		.6	1.4	2.0 YE	
127		.4	.8	1.2 YE	
176R		.3	.8	1.1 YE	
176R		.2	.6	.8 YE	
219		.4	1.8	2.2 YE	↓
222		1.5	4.4	5.9 YE	27.1
224		2.9	3.2	6.1 YE	↓
226		2.6	3.9	6.5 YE	↓
228		1.3	3.0	4.3 YE	26.8
230R		.9	3.8	4.7 YE	
230R		1.6	1.8	3.4 YE	
232		3.0	3.6	6.6 YE	
234		2.9	3.6	6.5 YE	
236		2.0	3.4	5.4 YE	↓
238		1.3	6.3	7.6 XY	26.3
240R		1.1	6.9	8.0 XY	↓
240R	↓	1.3	4.4	5.7 YE	↓

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STRESS SUMMARY - EQUATION C1

NODE #	PRESSURE STRESS (KSI)	DEADWEIGHT STRESS (KSI)	DBE STRESS (KSI)	EQUATION C1 STRESS (KSI)	ALLOWABLE STRESS (KSI)
242	0	2.0	5.4	7.4 YZ	26.3
244		1.6	4.0	5.6 YZ	
246		1.2	4.1	5.3 YZ	
248		1.1	6.0	7.1 YZ	
250		1.5	7.9	9.4 YZ	
252		1.8	11.4	13.2 YZ	
258		1.7	12.7	14.4 YZ	
259		1.5	11.3	12.8 YZ	
257		2.6	15.1	17.7 YZ	
260		1.3	11.6	12.9 YZ	↓
262	↓	2.9	8.2	11.1 YZ	25.7
266	2.9	3.0	3.1	9.0 YZ	
268		3.6	3.7	10.2 YZ	
272		3.5	4.6	11.0 YZ	
274		2.7	4.2	9.8 YZ	
276		3.1	4.1	10.1 YZ	
278		3.4	4.3	10.6 YZ	
279		3.4	4.3	10.6 YZ	
280		2.2	6.9	12.0 YZ	
282	↓	1.6	7.5	12.0 YZ	↓

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STRESS SUMMARY - EQUATION C1

NODE #	PRESSURE STRESS (KSI)	DEADWEIGHT STRESS (KSI)	DBE STRESS (KSI)	EQUATION C1 STRESS (KSI)	ALLOWABLE STRESS (KSI)
284B	2.9	.9	10.0	13.8 YZ	25.7
72B	0	2.0	1.9	3.9 XY	27.5
74		1.0	1.2	2.2 XY	
76		.6	.8	1.4 XY	
78		.3	.7	1.0 XY	
80		.3	.4	.7 XY	
82		.4	.6	1.0 YZ	↓
84		.4	1.0	1.4 YZ	27.2
86		.3	1.1	1.4 YZ	
88		1.2	2.2	3.4 YZ	
90		1.5	2.4	3.9 YZ	
92		.9	1.5	2.4 YZ	↓
97		1.0	1.7	2.7 YZ	26.7
94		1.2	2.2	3.4 YZ	26.7
100		.3	2.3	2.6 YZ	26.7
96		.5	4.1	4.6 YZ	26.7
98		.8	4.2	5.0 YZ	26.5
103	↓	.5	2.5	3.0 YZ	21.1
107	3.5	.7	.7	4.9 XY	21.0
108	3.5	.8	3.8	8.1 YZ	28.8



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STRESS SUMMARY - EQUATION C1

NODE #	PRESSURE STRESS (KSI)	DEADWEIGHT STRESS (KSI)	DBE STRESS (KSI)	EQUATION C1 STRESS (KSI)	ALLOWABLE STRESS (KSI)
110	3.5	.6	4.4	8.5 YZ	28.8
111		.6	4.4	8.5 YZ	
112		.6	4.4	8.5 YZ	
114		.3	3.9	7.7 YZ	
116		.3	2.4	6.2 YZ	
118		.6	2.0	6.1 YZ	
120		.7	2.0	6.2 YZ	
122		1.0	2.2	6.7 XY	
124	↓	1.0	2.2	6.7 XY	↓
126B	0	.7	1.7	2.4 XY	27.5
128		.4	.7	1.1 XY	
130		.4	.5	.9 YZ	
132		.4	.7	1.1 XY	
134		.2	1.2	1.4 XY	
136		.2	1.8	2.0 XY	↓
138		1.0	3.4	4.4 XY	27.2
140		1.4	3.6	5.0 XY	
142		.8	2.2	3.0 XY	
143		.9	2.2	3.1 XY	↓
144	↓	1.1	2.3	3.4 XY	26.7

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STRESS SUMMARY - EQUATION C1

NODE #	PRESSURE STRESS (KSI)	DEADWEIGHT STRESS (KSI)	DBE STRESS (KSI)	EQUATION C1 STRESS (KSI)	ALLOWABLE STRESS (KSI)
145	0	.3	2.4	2.7 xy	26.7
146		.6	5.6	6.2 xy	26.7
148		1.0	5.7	6.7 xy	26.5
152	↓	.5	2.6	3.1 xy	21.1
156	3.5	.8	.8	5.1 yz	20.9
158		.9	4.2	8.6 xy	28.8
160		.7	5.0	9.2 xy	
161		.7	5.0	9.2 xy	
162		.7	5.0	9.2 xy	
164		.5	4.4	8.4 xy	
166		.5	2.7	6.7 xy	
168		.8	2.0	6.3 xy	
170		.9	2.1	6.5 yz	
172		1.2	2.5	7.2 yz	
174	↓	1.2	2.5	7.2 yz	↓
176B	0	.7	1.2	1.9 yz	27.5
178		.6	.7	1.3 yz	
180		.3	1.4	1.7 yz	
182		.3	2.2	2.5 yz	↓
184	↓	.9	4.2	5.1 yz	27.2

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DONALD C. COOK
UNIT #2
PROJECT 5364

BY: DMD DATE: 5/5/83

CHECKED BY: AWB DATE: 5-6-83

STRESS SUMMARY - EQUATION C1

NODE #	PRESSURE STRESS (KSI)	DEADWEIGHT STRESS (KSI)	DBE STRESS (KSI)	EQUATION C1 STRESS (KSI)	ALLOWABLE STRESS (KSI)
186	0	1.3	4.3	5.6 YZ	27.2
187		.9	2.1	3.0 YZ	27.2
188		1.0	1.9	2.9 YZ	26.7
192		.3	1.8	2.1 YZ	26.7
190		.5	3.2	3.7 YZ	26.7
195		1.0	3.1	4.1 YZ	26.5
196		.6	1.9	2.5 YZ	21.1
200	3.5	.8	.8	5.1 XY	20.9
202		.9	3.8	8.2 YZ	28.8
204		.6	4.4	8.5 YZ	
205		.6	4.4	8.5 YZ	
206		.6	4.4	8.5 YZ	
208		.3	3.9	7.7 YZ	
210		.3	2.4	6.2 YZ	
212		.7	1.9	6.1 YZ	
214		.8	2.0	6.3 XY	
216		1.1	2.3	6.9 XY	
218		1.1	2.3	6.9 XY	
230 B	0	3.2	15.0	18.2 YZ	26.8
286	0	6.4	10.1	16.5 YZ	26.3

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DONALD C. COOK
UNIT #2
PROJECT 5364

BY: DMD DATE: 5/5/83

CHECKED BY: AKB DATE: 5-6-83

STRESS SUMMARY - EQUATION C1

NODE #	PRESSURE STRESS (KSI)	DEADWEIGHT STRESS (KSI)	DBE STRESS (KSI)	EQUATION C1 STRESS (KSI)	ALLOWABLE STRESS (KSI)
288	0	6.7	9.2	15.9 YZ	26.3
290	0	3.6	7.5	11.1 YZ	26.3
292	0	3.9	8.3	12.2 YZ	25.7
296	2.9	2.1	6.3	11.3 YZ	
298		1.4	5.6	9.9 YZ	
302		1.8	6.3	11.0 YZ	
304		2.5	6.1	11.5 YZ	
306		2.0	6.1	11.0 YZ	
308		1.7	6.4	11.0 YZ	
310		1.3	6.2	10.4 YZ	
312		3.2	5.3	11.4 YZ	
314		.9	4.2	8.0 YZ	
316		1.1	4.1	8.1 YZ	
318	4.1	5.6	3.3	13.0 XY	↓
320R		4.3	2.4	10.8 XY	28.8
320R		3.1	2.4	9.6 YZ	
322		3.3	2.6	10.0 YZ	
324		3.1	2.5	9.7 YZ	
325		3.1	2.5	9.7 YZ	
326	↓	2.7	2.9	9.7 YZ	↓

Technical Report
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DONALD C. COOK
UNIT #2
PROJECT 5364

BY: SMD DATE: 5/5/83

CHECKED BY: AMB DATE: 5-6-83

STRESS SUMMARY - EQUATION C1

NODE #	PRESSURE STRESS (KSI)	DEADWEIGHT STRESS (KSI)	DBE STRESS (KSI)	EQUATION C1 STRESS (KSI)	ALLOWABLE STRESS (KSI)
328	4.1	2.5	2.7	9.3 YZ	28.8
330		2.4	2.5	9.1 YZ	
332	↓	2.6	3.3	10.0 YZ	
334	3.5	.8	1.0	5.3 YZ	
336		.7	1.1	5.3 YZ	↓
284R		.7	.9	5.1 YZ	28.8
284R		.6	1.3	5.4 YZ	
338		.4	1.3	5.2 YZ	
339		.6	1.7	5.8 YZ	
340		.7	1.8	6.0 YZ	
342	↓	.8	1.7	6.0 YZ	↓
240B	0	1.3	11.8	13.1 XY	26.3
241		1.3	9.1	10.4 XY	
402		3.5	7.0	10.5 XY	
404		4.7	9.2	13.9 XY	
344		3.5	8.1	11.6 XY	↓
346	↓	.9	6.9	7.8 XY	25.7
350	2.9	.7	5.4	9.0 XY	
352		.9	4.7	8.5 XY	
356	↓	.4	5.3	8.6 XY	↓

6.1.7 Equation C-2 Stresses

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DONALD C. COOK
UNIT #2
PROJECT 5364

BY: DWC DATE: 5-18-83

CHECKED BY: SMS DATE: 5/18/83

STRESS SUMMARY - EQUATION C2

NODE #	PRESSURE STRESS (KSI)	DEADWEIGHT STRESS (KSI)	SV TRANSIENT SHOCK STRESS (KSI)	EQUATION C2 STRESS (KSI)	ALLOWABLE STRESS (KSI)
2	.4	0	5.4	5.8	29.2
4		.3	39.7	40.4	
6		.4	20.3	21.1	
7		.2	10.0	10.6	
8		.3	6.9	7.6	
10		.7	16.7	17.8	
12		1.0	18.8	20.2	
14		.5	13.1	14.0	
16		.6	28.1	29.1	
18		1.1	56.8	58.3	
20		1.5	32.9	34.8	
21	↓	.8	16.2	17.4	↓
24	.7	.8	16.8	18.3	30.1
26		.8	77.5	79.0	
28		.9	55.9	57.5	
32		.5	19.8	21.0	
33		.9	40.	41.6	
34		1.0	40.4	42.1	
36	↓	1.0	41.1	42.8	↓
38	.8	.9	59.6	61.3	30.0



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DONALD C. COOK
UNIT #2
PROJECT 5364

BY: DHB DATE: 5-18-83

CHECKED BY: JMS DATE: May 18 '83

STRESS SUMMARY - EQUATION C2

NODE #	PRESSURE STRESS (KSI)	DEADWEIGHT STRESS (KSI)	SV TRANSIENT SHOCK STRESS (KSI)	EQUATION C2 STRESS (KSI)	ALLOWABLE STRESS (KSI)
40	.8	.4	56.3	57.5	30.0
42		.3	55.3	56.4	
44		.9	54.3	56.0	
46		1.3	48.7	50.8	
48		.6	59.2	60.6	
49		.6	51.2	52.6	
50		.6	44.4	45.8	
51	↓	.4	64.3	65.5	↓
52	1.0	.4	93.6	95.0	29.8
54		.2	59.1	60.3	
56		.4	24.2	25.6	
58		.6	51.2	52.8	
60		.3	28.2	29.5	
62		.6	54.0	55.6	
64		.4	40.6	42.0	
66		.3	27.8	29.1	
68		.3	37.5	38.8	
70		.2	32.9	34.1	
71	↓	.3	15.6	16.9	↓
72R	.9	.4	36.3	37.6	29.9

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DONALD C. COOK
UNIT #2
PROJECT 5364

BY: AMB DATE: 5-18-83

CHECKED BY: Sms DATE: 5/18/83

STRESS SUMMARY - EQUATION C2

NODE #	PRESSURE STRESS (KSI)	DEADWEIGHT STRESS (KSI)	SV TRANSIENT SHOCK STRESS (KSI)	EQUATION C2 STRESS (KSI)	ALLOWABLE STRESS (KSI)
72B	.7	2.0	74.	76.7	27.5
74		1.0	48.3	50.0	
76		.6	106.1	107.4	
78		.3	194.4	195.4	
80		.3	146.9	147.9	
82	↓	.4	201.3	202.4	↓
84	.9	.4	53.4	54.7	27.2
86		.3	49.0	50.2	
88		1.2	49.1	51.2	
90		1.5	97.3	99.7	
92	↓	.9	75.0	76.8	↓
97	1.8	1.0	69.0	71.8	26.7
94		1.2	59.5	62.5	
100		.3	62.5	64.6	
96	↓	.5	101.5	103.8	↓
98	2.4	.8	114.2	117.4	26.5
103	2.4	.5	67.2	70.1	21.1
107	3.5	.7	32.5	36.7	21.0
108	3.5	.8	23.5	27.8	28.8
110	3.5	.6	30.9	35.0	28.8

6.1.8 Equation C-3 Stresses

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DONALD C. COOK
UNIT #2
PROJECT 5364

BY: SMB DATE: 5/4/83

CHECKED BY: AMB DATE: 5-4-83

STRESS SUMMARY - EQUATION C3

NODE #	SV TRANSIENT THERMAL STRESS (KSI)	ALLOWABLE STRESS (KSI)
2	.2	27.6
4	1.9	
6	2.1	
7	.8	
8	.8	
10	2.1	
12	2.1	
14	.8	
16	.9	
18	2.5	
20	2.4	
21	.9	
24	.9	1
26	1.8	27.7
28	1.6	
32	.6	
33	1.6	
34	1.8	
36	2.1	
38	2.1	

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DONALD C. COOK
UNIT #2
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BY: DMD DATE: 5/4/83

CHECKED BY: JMB DATE: 5-4-83

STRESS SUMMARY - EQUATION C3

NODE #	SV TRANSIENT THERMAL STRESS (KSI)	ALLOWABLE STRESS (KSI)
40	1.9	27.7
42	1.9	
44	2.1	
46	2.7	
48	1.4	
49	1.3	
50	1.3	
51	.7	
52	.8	
54	.7	
56	.7	
58	.6	
60	.2	
62	.6	
64	.7	
66	.9	
68	1.1	
70	.9	
71	1.4	
72R	3.2	

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DONALD C. COOK
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STRESS SUMMARY - EQUATION C3

NODE #	SV TRANSIENT THERMAL STRESS) (KSI)	ALLOWABLE STRESS (KSI)
72B	4.1	27.3
74	2.1	
76	5.0	
78	6.1	
80	5.3	
82	2.3	
84	3.0	27.2
86	2.2	
88	3.9	
90	3.2	
92	1.4	
97	1.3	27.1
94	2.2	
100	2.2	
96	5.1	
98	5.6	
103	2.5	26.4
107	1.0	26.4
108	.6	27.4
110	.6	27.4

6.2 Support Loads

Support loads are given for each support on the pressurizer relief line piping. Support load combinations were calculated in accordance with Table II, Reference 2. Combination E2 was only considered for those supports that are part of the quarter model. Thermal-1 refers to the normal thermal operating case and thermal-2 refers to the PORV transient thermal loading and thermal-3 refers to SV transient thermal condition.

The support load combinations considered are as follows:

D1 = deadweight + normal thermal +/- OBE

D2 = deadweight + PORV transient thermal +/- $\left[\frac{(OBE)^2 + (PORV \text{ transient shock})^2}{2} \right]^{1/2}$

E1 = deadweight + normal thermal +/- DBE

E2 = deadweight + SV transient thermal +/- SV transient shock



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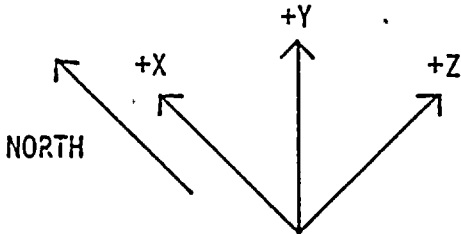
TELEDYNE
ENGINEERING SERVICES

SUPPORT LOAD SUMMARY SHEET

DONALD C. COOK
UNIT #2
PROJECT 5364

BY: SKB DATE: 6-9-83
CHECKED BY: SD DATE: 6/9/83

GLOBAL COORDINATE SYSTEM



MARK NUMBER 2-GRC-R-585
NODE NUMBER 16

DESIGN LOADINGS									
	DISPLACEMENTS			FORCES			MOMENTS		
	X	Y	Z	FX	FY	FZ	MX	MY	MZ
DEADWEIGHT-1		.019	.001	-20					
THERMAL-1		-.161	.027	-1860					
THERMAL-2		-.035	-.377	350					
THERMAL-3		-.029	-.377	493					
SEISMIC-OBE		±.001	±.001	±202					
SEISMIC-DBE		±.002	±.002	±351					
BLOWDOWN-SRV		+.266 -.264	+.292 -.464	±76790					
BLOWDOWN-PORV		±.001	±.002	±377					
TES COMBINED LOADS				SUPPORT DRAWING LOADS					
	FX	FY	FZ		FX	FY	FZ		
NORMAL/UPSET	+758 -2082			DESIGN (+)	4132				
EMERGENCY	+77263 -76317			DESIGN (-)	397				

UNITS: DISPLACEMENTS : INCHES
FORCES : POUNDS
MOMENTS : INCH-POUNDS

For normal/upset conditions TES combined loads are less for +FX and greater for -FX. For the emergency condition TES loads are greater.

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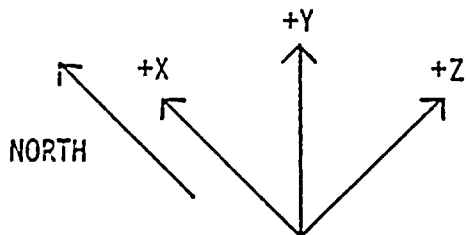
SUPPORT LOAD SUMMARY SHEET

DONALD C. COOK
 UNIT #2
 PROJECT 5364

BY: EWB DATE: 6-9-83

CHECKED BY: Dmd DATE: 6/9/83

GLOBAL COORDINATE SYSTEM



MARK NUMBER 2-GRC-R-586

NODE NUMBER 24

DESIGN LOADINGS

	DISPLACEMENTS			FORCES			MOMENTS		
	X	Y	Z	FX	FY	FZ	MX	MY	MZ
DEADWEIGHT-1	-0.003		.006		-1170				
THERMAL-1	-0.034		.067		1700				
THERMAL-2	-0.061		-.400		241				
THERMAL-3	-0.051		-.362		139				
SEISMIC-OBE	±.001		0		± 111				
SEISMIC-DBE	±.001		0		± 201				
BLOWDOWN-SRV	+ .261 - .373		+ .064 - .062		± 25780				
BLOWDOWN-PORV	±.002		± 0		± 110				

TES COMBINED LOADS

	FX	FY	FZ
NORMAL/UPSET		+ 641 - 1281	
EMERGENCY		+ 24749 - 26811	

SUPPORT DRAWING LOADS

	FX	FY	FZ
DESIGN (+)		3890	
DESIGN (-)		479	

UNITS: DISPLACEMENTS : INCHES
 FORCES : POUNDS
 MOMENTS : INCH-POUNDS

For normal/upset conditions TES combined loads are less for +FY and greater for -FY. For the emergency condition TES combined loads are greater.

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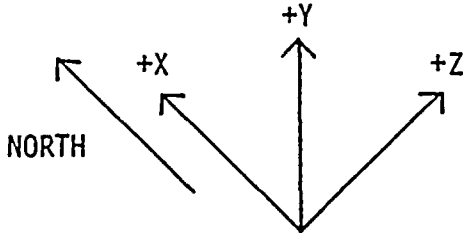
SUPPORT LOAD SUMMARY SHEET

DONALD C. COOK
UNIT #2
PROJECT 5364

BY: SWB DATE: 6-9-83

CHECKED BY: DMD DATE: 6/9/83

GLOBAL COORDINATE SYSTEM



MARK NUMBER 2-GRC-S-587

NODE NUMBER 32

DESIGN LOADINGS									
	DISPLACEMENTS			FORCES			MOMENTS		
	X	Y	Z	FX	FY	FZ	MX	MY	MZ
DEADWEIGHT-1	-0.036	-1.129	.028						
THERMAL-1	.226	1.01	.276						
THERMAL-2	-.203	.370	-.330						
THERMAL-3	-.186	.330	-.330						
SEISMIC-OBE	±.009	0	±.007		±134				
SEISMIC-DBE	±.007	0	±.011		±237				
BLOWDOWN-SRV	+1.307 -1.491	0	+1.522 -1.398		±51450				
BLOWDOWN-PORV	±.007 -.003	0	±.014 -.012		±257				
TES COMBINED LOADS				SUPPORT DRAWING LOADS					
	FX	FY	FZ		FX	FY	FZ		
NORMAL/UPSET		±290		DESIGN (+)		1037			
EMERGENCY		±51450		DESIGN (-)		1037			

UNITS: DISPLACEMENTS : INCHES
 FORCES : POUNDS
 MOMENTS : INCH-POUNDS

TES COMBINED LOADS ARE LESS THAN THE LOAD SHOWN ON THE SUPPORT DRAWING FOR THE NORMAL/UPSET CONDITIONS AND GREATER FOR THE EMERGENCY CONDITION.

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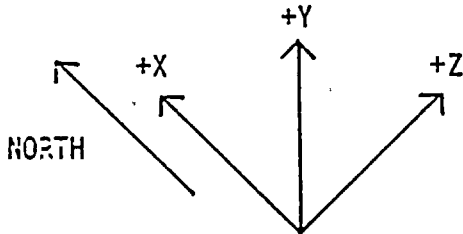
SUPPORT LOAD SUMMARY SHEET

DONALD C. COOK
UNIT #2
PROJECT 5364

BY: SD/13 DATE: 6-9-83

CHECKED BY: Sms DATE: 6/9/83

GLOBAL COORDINATE SYSTEM



MARK NUMBER 2-GRC-R-589

NODE NUMBER 48

DESIGN LOADINGS									
	DISPLACEMENTS			FORCES			MOMENTS		
	X	Y	Z	FX	FY	FZ	MX	MY	MZ
DEADWEIGHT-1		.004		-30		20			
THERMAL-1		2.27		1150		-770			
THERMAL-2		.985		-399		246			
THERMAL-3		.904		-501		333			
SEISMIC-OBE		±.007		±254		±380			
SEISMIC-DBE		±.011		±427		±662			
BLOWDOWN-SRV		+ .758 - .786		±45110		±75580			
BLOWDOWN-PORV		+ .006 - .005		±170		±537			
TES COMBINED LOADS				SUPPORT DRAWING LOADS					
	FX	FY	FZ		FX	FY	FZ		
NORMAL/UPSET	+1374 -735		+924 -1130		DESIGN (+)	615		5682	
EMERGENCY	+44579 -45641		+75933 -75227		DESIGN (-)	3236		4144	

UNITS: DISPLACEMENTS : INCHES
FORCES : POUNDS
MOMENTS : INCH-POUNDS

TES COMBINED LOADS ARE LESS THAN THE LOAD SHOWN ON THE SUPPORT DRAWING FOR THE NORMAL/UPSET CONDITIONS AND GREATER FOR THE EMERGENCY CONDITION.

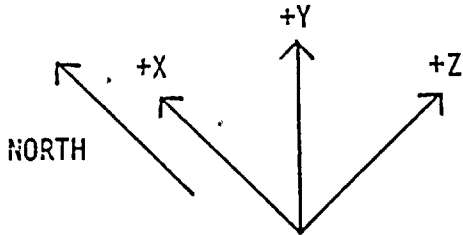
SUPPORT LOAD SUMMARY SHEET

DONALD C. COOK
 UNIT #2
 PROJECT 5364

BY: AKB DATE: 6-9-83

CHECKED BY: SMD DATE: 6/9/83

GLOBAL COORDINATE SYSTEM



MARK NUMBER 2-GRC-C-590

NODE NUMBER 50

DESIGN LOADINGS

	DISPLACEMENTS			FORCES			MOMENTS		
	X	Y	Z	FX	FY	FZ	MX	MY	MZ
DEADWEIGHT-1	-0.001	.004	-0.010		3281				
THERMAL-1	.024	2.27	-0.023						
THERMAL-2	.018	1.06	-0.017						
THERMAL-3	.019	.980	-0.017						
SEISMIC-OBE	+0.004	+0.011	+0.003						
SEISMIC-OBE	+0.007	+0.004	+0.005						
BLOWDOWN-SRV	+0.341 -0.314	+0.752 -0.784	+0.712 -0.573						
BLOWDOWN-PORV	+0.002 -0.002	+0.006 -0.005	+0.006 -0.007						

TES COMBINED LOADS

	FX	FY	FZ
NORMAL/UPSET		+3281	
EMERGENCY		+3281	

SUPPORT DRAWING LOADS

	FX	FY	FZ
DESIGN (+)		3281	
DESIGN (-)			

UNITS: DISPLACEMENTS : INCHES
 FORCES : POUNDS
 MOMENTS : INCH-POUNDS

TES COMBINED LOADS ARE _____
 THAN THE LOAD SHOWN
 ON THE SUPPORT DRAWING

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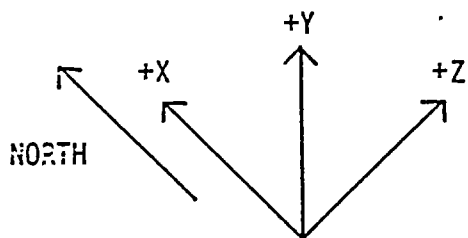
TELEDYNE
ENGINEERING SERVICES

SUPPORT LOAD SUMMARY SHEET

DONALD C. COOK
UNIT #2
PROJECT 5364

BY: DLB DATE: 6-9-83
CHECKED BY: DMD DATE: 6/9/83

GLOBAL COORDINATE SYSTEM



MARK NUMBER 2-GRC-R-591
NODE NUMBER 60

DESIGN LOADINGS									
	DISPLACEMENTS			FORCES			MOMENTS		
	X	Y	Z	FX	FY	FZ	MX	MY	MZ
DEADWEIGHT-1		-0.001		30		-70			
THERMAL-1		2.31		180		-500			
THERMAL-2		1.76		-219		-211			
THERMAL-3		1.72		-171		-238			
SEISMIC-OBE		± .007		± 272		± 247			
SEISMIC-DBE		± .011		± 447		± 417			
BLOWDOWN-SRV		+405 -526		±39540		±73540			
BLOWDOWN-PORV		+607 -1005		±392		±764			
TES COMBINED LOADS				SUPPORT DRAWING LOADS					
	FX	FY	FZ		FX	FY	FZ		
NORMAL/UPSET	+492 -666		+522 -1084		DESIGN (+)	972		657	
EMERGENCY	+39399 -39681		+73232 -73848		DESIGN (-)	1566		1044	

UNITS: DISPLACEMENTS : INCHES
FORCES : POUNDS
MOMENTS : INCH-POUNDS

TES COMBINED LOADS ARE LESS THAN THE LOAD SHOWN ON THE SUPPORT DRAWING FOR THE NORMAL/UPSET CONDITIONS AND GREATER FOR THE EMERGENCY CONDITION.

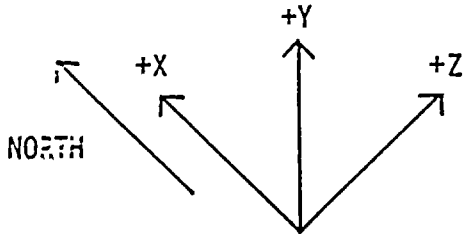
SUPPORT LOAD SUMMARY SHEET

DONALD C. COOK
 UNIT #2
 PROJECT 5364

BY: AKB DATE: 6-9-83

CHECKED BY: DMB DATE: 6/9/83

GLOBAL COORDINATE SYSTEM



MARK NUMBER 2-GRC-S-592

NODE NUMBER 101

DESIGN LOADINGS

	DISPLACEMENTS			FORCES			MOMENTS		
	X	Y	Z	FX	FY	FZ	MX	MY	MZ
DEADWEIGHT-1	-036	.024	-023						
THERMAL-1	.224	2.82	-.116						
THERMAL-2	.263	2.79	-.152						
THERMAL-3	.269	2.79	-.151						
SEISMIC-OBE	±.101	0	±.144		± 800				
SEISMIC-DBE	±.176	0	±.250		± 1324				
BLOWDOWN-SRV	+455 -369	0	+409 -461		± 55600				
BLOWDOWN-PORV	±.001	0	±.001		± 95				
TES COMBINED LOADS				SUPPORT DRAWING LOADS					
	FX	FY	FZ		FX	FY	FZ		
NORMAL/UPSET		± 806		DESIGN (+)		5301			
EMERGENCY		± 55600		DESIGN (-)		5301			

UNITS: DISPLACEMENTS : INCHES
 FORCES : POUNDS
 MOMENTS : INCH-POUNDS

TES COMBINED LOADS ARE LESS THAN THE LOAD SHOWN ON THE SUPPORT DRAWING FOR THE NORMAL/UPSET CONDITION AND GREATER FOR THE EMERGENCY CONDITION.

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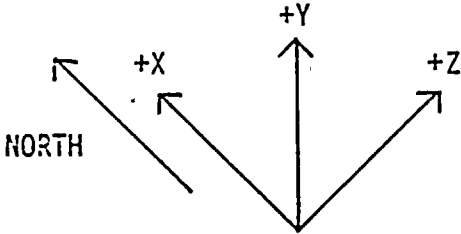
SUPPORT LOAD SUMMARY SHEET

DONALD C. COOK
 UNIT #2
 PROJECT 5364

BY: DLB DATE: 6-9-83

CHECKED BY: D.M.H. DATE: 6/9/83

GLOBAL COORDINATE SYSTEM



MARK NUMBER 2-GRC-C-593

NODE NUMBER 99

DESIGN LOADINGS									
	DISPLACEMENTS			FORCES			MOMENTS		
	X	Y	Z	FX	FY	FZ	MX	MY	MZ
DEADWEIGHT-1	-0.035	.038	-.019		1054				
THERMAL-1	.215	2.80	-.107						
THERMAL-2	.290	2.74	-.161						
THERMAL-3	.309	2.73	-.146						
SEISMIC-OBE	±.104	±.004	±.148						
SEISMIC-DBE	±.132	±.007	±.258						
BLOWDOWN-SRV	+ .760 - .617	+ .308 - .299	+ .499 - .728						
BLOWDOWN-PORV	±.001	±.001	±.002 - .001						
TES COMBINED LOADS				SUPPORT DRAWING LOADS					
	FX	FY	FZ		FX	FY	FZ		
NORMAL/UPSET		+1054				1054			
EMERGENCY		+1054							

UNITS: DISPLACEMENTS : INCHES
 FORCES : POUNDS
 MOMENTS : INCH-POUNDS

TES COMBINED LOADS ARE _____
 THAN THE LOAD SHOWN
 ON THE SUPPORT DRAWING

Technical Report
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TELEDYNE
ENGINEERING SERVICES

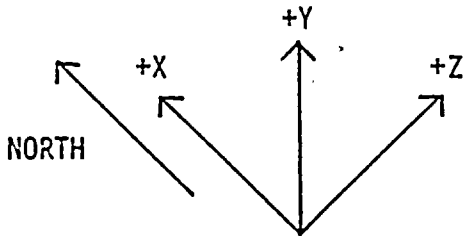
SUPPORT LOAD SUMMARY SHEET

DONALD C. COOK
 UNIT #2
 PROJECT 5364

BY: DLB DATE: 6-9-83

CHECKED BY: omb DATE: 6/9/83

GLOBAL COORDINATE SYSTEM



MARK NUMBER 2-GRC-S-594

NODE NUMBER 149

DESIGN LOADINGS									
	DISPLACEMENTS			FORCES			MOMENTS		
	X	Y	Z	FX	FY	FZ	MX	MY	MZ
DEADWEIGHT-1	.023	.027	-.047						
THERMAL-1	.160	2.81	.166						
THERMAL-2	.206	2.81	.154						
THERMAL-3	—	—	—						
SEISMIC-OBE	±.192	0	±.047		±1100				
SEISMIC-DBE	±.332	0	±.078		±1820				
BLOWDOWN-SRV	—	—	—		—				
BLOWDOWN-PORV	±.002	0	±.002		±142				
TES COMBINED LOADS				SUPPORT DRAWING LOADS					
	FX	FY	FZ		FX	FY	FZ		
NORMAL/UPSET		±1109				4479			
EMERGENCY		±1820				4479			

UNITS: DISPLACEMENTS : INCHES
 FORCES : POUNDS
 MOMENTS : INCH-POUNDS

TES COMBINED LOADS ARE LESS
 THAN THE LOAD SHOWN
 ON THE SUPPORT DRAWING



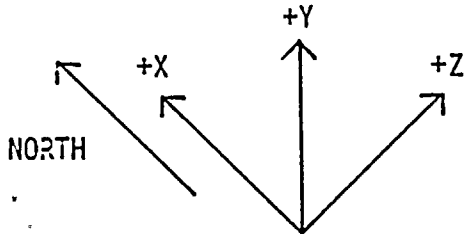
SUPPORT LOAD SUMMARY SHEET

DONALD C. COOK
UNIT #2
PROJECT 5364

BY: SKB DATE: 6-9-83

CHECKED BY: DMD DATE: 6/9/83

GLOBAL COORDINATE SYSTEM



MARK NUMBER 2-GRC-C-595

NODE NUMBER 147

DESIGN LOADINGS

	DISPLACEMENTS			FORCES			MOMENTS		
	X	Y	Z	FX	FY	FZ	MX	MY	MZ
DEADWEIGHT-1	.012	.045	-.035		1072				
THERMAL-1	.135	2.79	.142						
THERMAL-2	.206	2.79	.176						
THERMAL-3	—	—	—						
SEISMIC-OBE	±.173	±.007	±.040						
SEISMIC-OBE	±.299	±.012	±.068						
BLOWDOWN-SRV	—	—	—						
BLOWDOWN-PORV	±.002	±.001	±.002						

TES COMBINED LOADS

	FX	FY	FZ
NORMAL/UPSET		+1072	
EMERGENCY		+1072	

SUPPORT DRAWING LOADS

	FX	FY	FZ
DESIGN (+)		1072	
DESIGN (-)			

UNITS: DISPLACEMENTS : INCHES
FORCES : POUNDS
MOMENTS : INCH-POUNDS

TES COMBINED LOADS ARE _____
THAN THE LOAD SHOWN
ON THE SUPPORT DRAWING

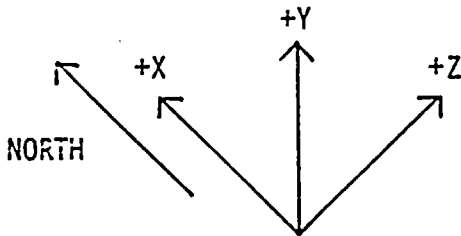
SUPPORT LOAD SUMMARY SHEET

DONALD C. COOK
UNIT #2
PROJECT 5364

BY: DLB DATE: 6-9-83

CHECKED BY: DMB DATE: 6/9/83

GLOBAL COORDINATE SYSTEM



MARK NUMBER 2-GRC-S-596

NODE NUMBER 193

DESIGN LOADINGS									
	DISPLACEMENTS			FORCES			MOMENTS		
	X	Y	Z	FX	FY	FZ	MX	MY	MZ
DEADWEIGHT-1	.045	.024	-.003						
THERMAL-1	-.177	2.76	.187						
THERMAL-2	-.081	2.80	.248						
THERMAL-3	—	—	—						
SEISMIC-OBE	±.045	0	±.167		± 997				
SEISMIC-OBE	±.075	0	±.286		± 1646				
BLOWDOWN-SRV	—	—	—		—				
BLOWDOWN-PORV	±.001	0	±.002 -.003		± 93				
TES COMBINED LOADS				SUPPORT DRAWING LOADS					
	FX	FY	FZ		FX	FY	FZ		
NORMAL/UPSET		±1001				4218			
EMERGENCY		± 1646				4218			

UNITS: DISPLACEMENTS : INCHES
FORCES : POUNDS
MOMENTS : INCH-POUNDS

TES COMBINED LOADS ARE LESS
THAN THE LOAD SHOWN
ON THE SUPPORT DRAWING

Technical Report
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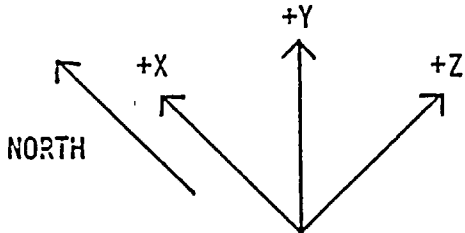
SUPPORT LOAD SUMMARY SHEET

DONALD C. COOK
UNIT #2
PROJECT 5364

BY: DLB DATE: 6-9-83

CHECKED BY: SmD DATE: 6/9/83

GLOBAL COORDINATE SYSTEM



MARK NUMBER 2-GRC-C-597

NODE NUMBER 189

DESIGN LOADINGS

	DISPLACEMENTS			FORCES			MOMENTS		
	X	Y	Z	FX	FY	FZ	MX	MY	MZ
DEADWEIGHT-1	.041	.044	-.005		983				
THERMAL-1	-.175	2.72	.145						
THERMAL-2	-.104	2.75	.247						
THERMAL-3	—	—	—						
SEISMIC-OBE	±.044	±.009	±.167						
SEISMIC-OBE	±.072	±.015	±.285						
BLOWDOWN-SRV	—	—	—						
BLOWDOWN-PORV	±.001	±.001	±.002 -.004						

TES COMBINED LOADS

	FX	FY	FZ
NORMAL/UPSET		+983	
EMERGENCY		+983	

SUPPORT DRAWING LOADS

	FX	FY	FZ
DESIGN (+)		983	
DESIGN (-)			

UNITS: DISPLACEMENTS : INCHES
FORCES : POUNDS
MOMENTS : INCH-POUNDS

TES COMBINED LOADS ARE —
THAN THE LOAD SHOWN
ON THE SUPPORT DRAWING

Technical Report
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TELEDYNE
ENGINEERING SERVICES

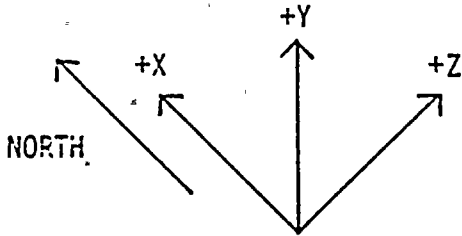
SUPPORT LOAD SUMMARY SHEET

DONALD C. COOK
UNIT #2
PROJECT 5364

BY: DLB DATE: 6-9-83

CHECKED BY: DMD DATE: 6/9/83

GLOBAL COORDINATE SYSTEM



MARK NUMBER 2-GRC-S-598

NODE NUMBER 95

DESIGN LOADINGS

	DISPLACEMENTS			FORCES			MOMENTS		
	X	Y	Z	FX	FY	FZ	MX	MY	MZ
DEADWEIGHT-1	.016	.030	.002						
THERMAL-1	.085	2.81	-1.31						
THERMAL-2	-1.03	2.59	-4.45						
THERMAL-3	-0.96	2.74	-4.35						
SEISMIC-OBE	±.007	±.003	±.006	±121	±131	±191			
SEISMIC-OBE	±.012	±.005	±.011	±209	±226	±330			
BLOWDOWN-SRV	+3.39 -3.28	+1.66 -1.173	+1.99 -1.48	±34425	±37195	±54455			
BLOWDOWN-PORV	±.004	±.001	±.003 -.002	±45	±49	±72			

TES COMBINED LOADS

	FX	FY	FZ
NORMAL/UPSET	±129	±140	±204
EMERGENCY	±34425	±37195	±54455

SUPPORT DRAWING LOADS

	FX	FY	FZ
DESIGN (+)	731	823	1223
DESIGN (-)	731	823	1223

UNITS: DISPLACEMENTS : INCHES
FORCES : POUNDS
MOMENTS : INCH-POUNDS

TES COMBINED LOADS ARE LESS THAN THE LOAD SHOWN ON THE SUPPORT DRAWING FOR THE NORMAL/UPSET CONDITIONS AND GREATER FOR THE EMERGENCY CONDITION.

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 TR-5364-2
 Revision 0

6-102

TELEDYNE
ENGINEERING SERVICES

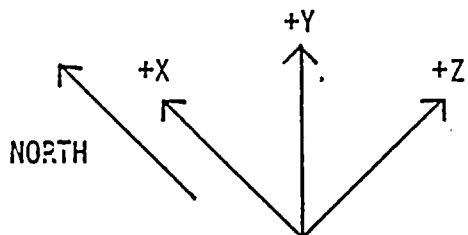
SUPPORT LOAD SUMMARY SHEET

DONALD C. COOK
 UNIT #2
 PROJECT 5364

BY: DLB DATE: 6-9-83

CHECKED BY: DMO DATE: 6/9/83

GLOBAL COORDINATE SYSTEM



MARK NUMBER 2-GRC-S-599

NODE NUMBER 141

DESIGN LOADINGS

	DISPLACEMENTS			FORCES			MOMENTS		
	X	Y	Z	FX	FY	FZ	MX	MY	MZ
DEADWEIGHT-1	-0.020	.028	.042						
THERMAL-1	.114	2.80	.039						
THERMAL-2	.301	2.64	.142						
THERMAL-3	—	—	—						
SEISMIC-OBE	±.010	±.006	±.004	±85	±42	±62			
SEISMIC-OBE	±.017	±.011	±.007	±145	±73	±106			
BLOWDOWN-SRV	—	—	—	—	—	—			
BLOWDOWN-PORV	±.002	±.001	±.001	±68	±34	±50			

TES COMBINED LOADS

	FX	FY	FZ
NORMAL/UPSET	±109	±54	±80
EMERGENCY	±145	±73	±106

SUPPORT DRAWING LOADS

	FX	FY	FZ
DESIGN (+)	422		573
DESIGN (-)	422		573

UNITS: DISPLACEMENTS : INCHES
 FORCES : POUNDS
 MOMENTS : INCH-POUNDS

TES COMBINED LOADS ARE LESS
 THAN THE LOAD SHOWN
 ON THE SUPPORT DRAWING

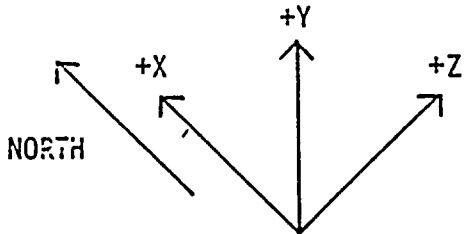
SUPPORT LOAD SUMMARY SHEET

DONALD C. COOK
 UNIT #2
 PROJECT 5364

BY: DLB DATE: 6-9-83

CHECKED BY: S.M.D. DATE: 6/9/83

GLOBAL COORDINATE SYSTEM



MARK NUMBER 2-GRC-R-600

NODE NUMBER 73

	DESIGN LOADINGS								
	DISPLACEMENTS			FORCES			MOMENTS		
	X	Y	Z	FX	FY	FZ	MX	MY	MZ
DEADWEIGHT-1		-0.002		-180		-170			
THERMAL-1		2.35		2060		2030			
THERMAL-2		2.32		1742		252			
THERMAL-3		—		—		—			
SEISMIC-OBE		±.005		±362		±517			
SEISMIC-OBE		±.008		±573		±872			
BLOWDOWN-SRV		—		—		—			
BLOWDOWN-PORV		+ .003 - .002		±327		±1006			
TES COMBINED LOADS				SUPPORT DRAWING LOADS					
	FX	FY	FZ		FX	FY	FZ		
NORMAL/UPSET	+2242 -542		+2377 -1049		DESIGN (+)	2395		1997	
EMERGENCY	+2453 -753		+2732 -1042		DESIGN (-)	981		3659	

UNITS: DISPLACEMENTS : INCHES
 FORCES : POUNDS
 MOMENTS : INCH-POUNDS

LESS (-FX, -FZ)
 TES COMBINED LOADS ARE GREATER (+FX, +FZ)
 THAN THE LOAD SHOWN
 ON THE SUPPORT DRAWING

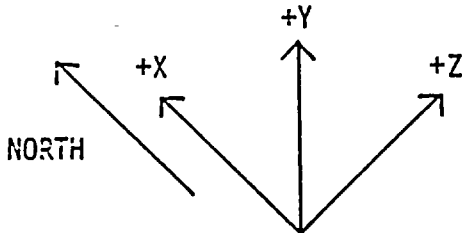
SUPPORT LOAD SUMMARY SHEET

DONALD C. COOK
 UNIT #2
 PROJECT 5364

BY: AKB DATE: 6-9-83

CHECKED BY: DMD DATE: 6/9/83

GLOBAL COORDINATE SYSTEM



MARK NUMBER 2-GRC-R-601

NODE NUMBER 222

DESIGN LOADINGS									
	DISPLACEMENTS			FORCES			MOMENTS		
	X	Y	Z	FX	FY	FZ	MX	MY	MZ
DEADWEIGHT-1		-0.002		530		370			
THERMAL-1		2.37		-1769		-2000			
THERMAL-2		2.62		-5054		-2181			
THERMAL-3		—		—		—			
SEISMIC-OBE		±.006		±701		±392			
SEISMIC-DBE		±.009		±1092		±632			
BLOWDOWN-SRV		—		—		—			
BLOWDOWN-PORV		+0.003 -0.002		±352		±254			
TES COMBINED LOADS				SUPPORT DRAWING LOADS					
	FX	FY	FZ		FX	FY	FZ		
NORMAL/UPSET	+1231 -5308		+762 -2278		DESIGN (+)	1223		1106	
EMERGENCY	+1622 -2331		+1002 -2262		DESIGN (-)	8757		2740	

UNITS: DISPLACEMENTS : INCHES
 FORCES : POUNDS
 MOMENTS : INCH-POUNDS

TES COMBINED LOADS ARE LESS *
 THAN THE LOAD SHOWN
 ON THE SUPPORT DRAWING

* EXCEPT IN + FX

Technical Report
 TR-5364-2
 Revision 0

TELEDYNE
ENGINEERING SERVICES

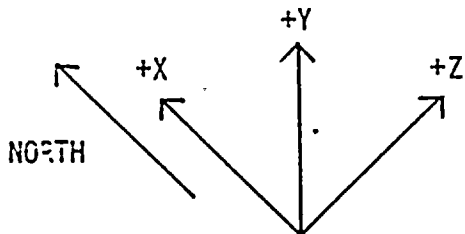
SUPPORT LOAD SUMMARY SHEET

DONALD C. COOK
 UNIT #2
 PROJECT 5364

BY: DIC DATE: 6-9-83

CHECKED BY: DMD DATE: 6/9/83

GLOBAL COORDINATE SYSTEM



MARK NUMBER 2-GRC-C-602

NODE NUMBER 290

DESIGN LOADINGS									
	DISPLACEMENTS			FORCES			MOMENTS		
	X	Y	Z	FX	FY	FZ	MX	MY	MZ
DEADWEIGHT-1	-0.030	.077	.056		798				
THERMAL-1	-.523	2.71	-.508						
THERMAL-2	-.574	3.15	-.502						
THERMAL-3	—	—	—						
SEISMIC-OBE	±.077	±.010	±.147						
SEISMIC-DBE	±.123	.016	.234						
BLOWDOWN-SRV	—	—	—						
BLOWDOWN-PORV	+0.017 -0.024	+0.011 -0.009	+0.025 -0.017						
TES COMBINED LOADS				SUPPORT DRAWING LOADS					
	FX	FY	FZ		FX	FY	FZ		
NORMAL/UPSET		+798	-			798			
EMERGENCY		+798							

UNITS: DISPLACEMENTS : INCHES
 FORCES : POUNDS
 MOMENTS : INCH-POUNDS

TES COMBINED LOADS ARE —
 THAN THE LOAD SHOWN
 ON THE SUPPORT DRAWING

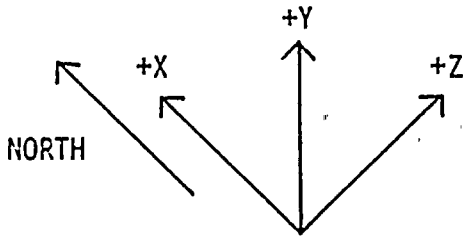
SUPPORT LOAD SUMMARY SHEET

DONALD C. COOK
 UNIT #2
 PROJECT 5364

BY: SKB DATE: 6-9-83

CHECKED BY: J.M.D DATE: 6/9/83

GLOBAL COORDINATE SYSTEM



MARK NUMBER 2-GRC-R-605

NODE NUMBER 326

DESIGN LOADINGS									
	DISPLACEMENTS			FORCES			MOMENTS		
	X	Y	Z	FX	FY	FZ	MX	MY	MZ
DEADWEIGHT-1		.120		170		-30			
THERMAL-1		3.36		-2220		3530			
THERMAL-2		3.36		-1381		3692			
THERMAL-3		—		—		—			
SEISMIC-OBE		±.013		±714		±1095			
SEISMIC-DBE		±.012		±1117		±1718			
BLOWDOWN-SRV		—		—		—			
BLOWDOWN-PORV		+ .014 - .012		+2305		+1683			
TES COMBINED LOADS				SUPPORT DRAWING LOADS					
	FX	FY	FZ		FX	FY	FZ		
NORMAL/UPSET	+1202 -3624		+5670 -1125		DESIGN (+)	1313		5851	
EMERGENCY	+1287 -3167		+5218 -1748		DESIGN (-)	2972		2412	

UNITS: DISPLACEMENTS : INCHES
 FORCES : POUNDS
 MOMENTS : INCH-POUNDS

TES COMBINED LOADS ARE LESS
 THAN THE LOAD SHOWN
 ON THE SUPPORT DRAWING

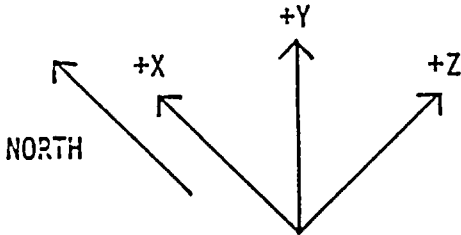
SUPPORT LOAD SUMMARY SHEET

DONALD C. COOK
 UNIT #2
 PROJECT 5364

BY: SAIB DATE: 6-9-83

CHECKED BY: hmi DATE: 6/9/83

GLOBAL COORDINATE SYSTEM



MARK NUMBER 2-GRC-C-606

NODE NUMBER 316

DESIGN LOADINGS									
	DISPLACEMENTS			FORCES			MOMENTS		
	X	Y	Z	FX	FY	FZ	MX	MY	MZ
DEADWEIGHT-1	-0.023	.235	.021		634				
THERMAL-1	.076	3.67	-2.82						
THERMAL-2	.093	3.66	-2.53						
THERMAL-3	—	—	—						
SEISMIC-OBE	±.032	±.064	±.051						
SEISMIC-OBE	±.050	±.102	±.080						
BLOWDOWN-SRV	—	—	—						
BLOWDOWN-PORV	+0.015 -0.018	+0.046 -0.031	+0.029 -0.035						
TES COMBINED LOADS				SUPPORT DRAWING LOADS					
	FX	FY	FZ		FX	FY	FZ		
NORMAL/UPSET		+634				634			
EMERGENCY		+634							

UNITS: DISPLACEMENTS : INCHES
 FORCES : POUNDS
 MOMENTS : INCH-POUNDS

TES COMBINED LOADS ARE _____
 THAN THE LOAD SHOWN
 ON THE SUPPORT DRAWING

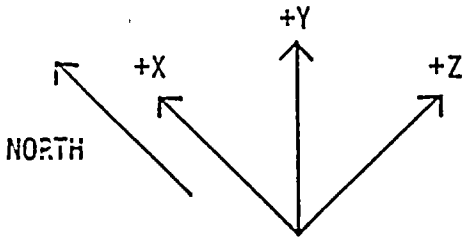
SUPPORT LOAD SUMMARY SHEET

DONALD C. COOK
 UNIT #2
 PROJECT 5364

BY: DHC DATE: 6-9-83

CHECKED BY: DMD DATE: 6/9/83

GLOBAL COORDINATE SYSTEM



MARK NUMBER 2-GRC-R-607

NODE NUMBER 312

DESIGN LOADINGS									
	DISPLACEMENTS			FORCES			MOMENTS		
	X	Y	Z	FX	FY	FZ	MX	MY	MZ
DEADWEIGHT-1	-0.002	.452	.031	-1069		-36			
THERMAL-1	.023	3.69	-5.82	3205		109			
THERMAL-2	.020	3.73	-5.59	1095		37			
THERMAL-3	—	—	—	—		—			
SEISMIC-OBE	±.001	±.049	±.041	±950		±32			
SEISMIC-OBE	±.001	±.077	±.064	±1470		±50			
BLOWDOWN-SRV	—	—	—	—		—			
BLOWDOWN-PORV	±.001	+0.047 -0.020	+0.026 -0.029	+1617		±55			
TES COMBINED LOADS				SUPPORT DRAWING LOADS					
	FX	FY	FZ		FX	FY	FZ		
NORMAL/UPSET	+3086 -2019		+105 -68		DESIGN (+)	5245		720	
EMERGENCY	+3606 -2539		+123 -86		DESIGN (-)	2146		340	

UNITS: DISPLACEMENTS : INCHES
 FORCES : POUNDS
 MOMENTS : INCH-POUNDS

TES COMBINED LOADS ARE LESS
 THAN THE LOAD SHOWN
 ON THE SUPPORT DRAWING

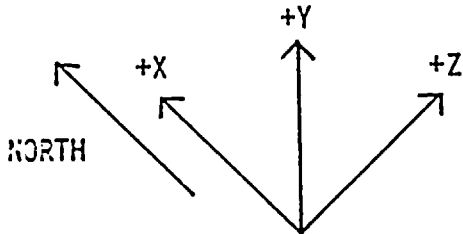
SUPPORT LOAD SUMMARY SHEET

DONALD C. COOK
 UNIT #2
 PROJECT 5364

BY: DJK DATE: 6-9-83

CHECKED BY: DMD DATE: 6/9/83

GLOBAL COORDINATE SYSTEM



MARK NUMBER 2-GRC-C-608

NODE NUMBER 304

DESIGN LOADINGS

	DISPLACEMENTS			FORCES			MOMENTS		
	X	Y	Z	FX	FY	FZ	MX	MY	MZ
DEADWEIGHT-1	-0.026	.361	.047		858				
THERMAL-1	-1.185	3.30	-1.669						
THERMAL-2	-2.242	3.50	-1.628						
THERMAL-3	—	—	—						
SEISMIC-OBE	±.051	±.004	±.082						
SEISMIC-DBE	±.081	±.006	±.130						
BLOWDOWN-SRV	—	—	—						
BLOWDOWN-PORV	+0.021 -0.022	+0.008 -0.010	+0.022 -0.018						

TES COMBINED LOADS

	FX	FY	FZ
NORMAL/UPSET		+858	
EMERGENCY		+353	

SUPPORT DRAWING LOADS

	FX	FY	FZ
DESIGN (+)		858	
DESIGN (-)			

UNITS: DISPLACEMENTS : INCHES
 FORCES : POUNDS
 MOMENTS : INCH-POUNDS

TES COMBINED LOADS ARE _____
 THAN THE LOAD SHOWN
 ON THE SUPPORT DRAWING

Technical Report
 TR-5364-2
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6-110

TELEDYNE
ENGINEERING SERVICES

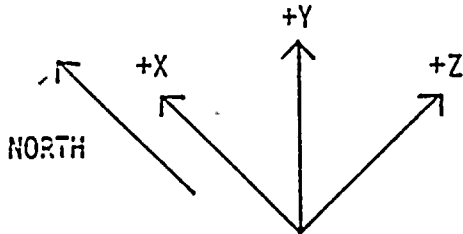
SUPPORT LOAD SUMMARY SHEET

DONALD C. COOK
 UNIT #2
 PROJECT 5364

BY: AKB DATE: 6-9-83

CHECKED BY: DMD DATE: 6/9/83

GLOBAL COORDINATE SYSTEM



MARK NUMBER 2-GRC-S-609

NODE NUMBER 306

DESIGN LOADINGS									
	DISPLACEMENTS			FORCES			MOMENTS		
	X	Y	Z	FX	FY	FZ	MX	MY	MZ
DEADWEIGHT-1	-0.024	4.20	.042						
THERMAL-1	-.114	3.42	-.693						
THERMAL-2	-.170	3.57	-.652						
THERMAL-3	—	—	—						
SEISMIC-OBE	±.043	0	±.064		±333				
SEISMIC-DBE	±.069	0	±.101		±516				
BLOWDOWN-SRV	—	—	—		—				
BLOWDOWN-PORV	±.021	0	±.024 -.021		±687				
TES COMBINED LOADS				SUPPORT DRAWING LOADS					
	FX	FY	FZ		FX	FY	FZ		
NORMAL/UPSET		±763				560			
EMERGENCY		±516				560			

UNITS: DISPLACEMENTS : INCHES
 FORCES : POUNDS
 MOMENTS : INCH-POUNDS

TES COMBINED LOADS ARE GREATER
 THAN THE LOAD SHOWN
 ON THE SUPPORT DRAWING

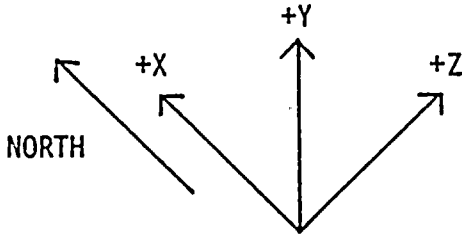
SUPPORT LOAD SUMMARY SHEET

DONALD C. COOK
 UNIT #2
 PROJECT 5364

BY: AKB DATE: 6-9-83

CHECKED BY: S.M.D. DATE: 6/9/83

GLOBAL COORDINATE SYSTEM



MARK NUMBER 2-GRC-C-610

NODE NUMBER 274

	DESIGN LOADINGS								
	DISPLACEMENTS			FORCES			MOMENTS		
	X	Y	Z	FX	FY	FZ	MX	MY	MZ
DEADWEIGHT-1	-0.031	.029	-0.041		637				
THERMAL-1	-0.430	3.23	.187						
THERMAL-2	-0.390	3.27	-0.078						
THERMAL-3	—	—	—						
SEISMIC-OBE	±.108	±.011	±.281						
SEISMIC-DBE	±.160	±.019	±.417						
BLOWDOWN-SRV	—	—	—						
BLOWDOWN-PORV	+0.026 -0.027	+0.021 -0.023	+0.046 -0.045						
TES COMBINED LOADS				SUPPORT DRAWING LOADS					
	FX	FY	FZ		FX	FY	FZ		
NORMAL/UPSET		+637				637			
EMERGENCY		+637							

UNITS: DISPLACEMENTS : INCHES
 FORCES : POUNDS
 MOMENTS : INCH-POUNDS

TES COMBINED LOADS ARE —
 THAN THE LOAD SHOWN
 ON THE SUPPORT DRAWING

Technical Report
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ENGINEERING SERVICES

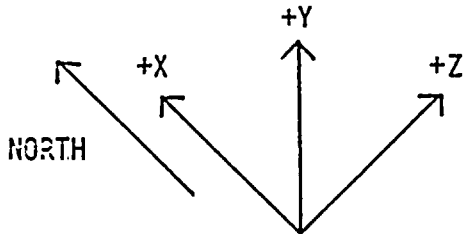
SUPPORT LOAD SUMMARY SHEET

DONALD C. COOK
 UNIT #2
 PROJECT 5364

BY: SKB DATE: 6-9-83

CHECKED BY: SMD DATE: 6/9/83

GLOBAL COORDINATE SYSTEM



MARK NUMBER 2-GRC-S-611

NODE NUMBER 248

DESIGN LOADINGS									
	DISPLACEMENTS			FORCES			MOMENTS		
	X	Y	Z	FX	FY	FZ	MX	MY	MZ
DEADWEIGHT-1	.045	.340	.050						
THERMAL-1	.093	3.36	-.193						
THERMAL-2	.070	3.61	.014						
THERMAL-3	—	—	—						
SEISMIC-OBE	±.010	±.016	±.049	± 26	± 184	± 62			
SEISMIC-OBE	±.016	±.023	±.073	± 41	± 286	± 96			
BLOWDOWN-SRV	—	—	—	—	—	—			
BLOWDOWN-PORV	+ .021 - .018	+ .008 - .009	+ .016 - .017	± 160	± 1124	± 376			
TES COMBINED LOADS				SUPPORT DRAWING LOADS					
	FX	FY	FZ		FX	FY	FZ		
NORMAL/UPSET	± 162	± 1139	± 381		DESIGN (+)	79	550	184	
EMERGENCY	± 41	± 286	± 96		DESIGN (-)	79	550	184	

UNITS: DISPLACEMENTS : INCHES
 FORCES : POUNDS
 MOMENTS : INCH-POUNDS

TES COMBINED LOADS ARE GREATER
 THAN THE LOAD SHOWN
 ON THE SUPPORT DRAWING

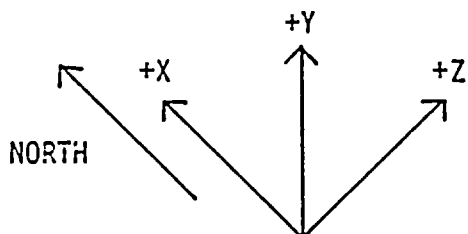
SUPPORT LOAD SUMMARY SHEET

DONALD C. COOK
 UNIT #2
 PROJECT 5364

BY: DLB DATE: 6-9-83

CHECKED BY: DMD DATE: 6/9/83

GLOBAL COORDINATE SYSTEM



MARK NUMBER 2-GRC-R-612

NODE NUMBER 258

DESIGN LOADINGS									
	DISPLACEMENTS			FORCES			MOMENTS		
	X	Y	Z	F _X	F _Y	F _Z	M _X	M _Y	M _Z
DEADWEIGHT-1		.341		-21		30			
THERMAL-1		3.30		162		-2820			
THERMAL-2		3.65		-32		-152			
THERMAL-3		—		—		—			
SEISMIC-OBE		±.023		±60		±1211			
SEISMIC-OBE		±.035		±910		±1792			
BLOWDOWN-SRV		—		—		—			
BLOWDOWN-PORV		+0.010 -0.009		±873		±669			
TES COMBINED LOADS				SUPPORT DRAWING LOADS					
	FX	FY	FZ		FX	FY	FZ		
NORMAL/UPSET	+2024 -1610		+1262 -4001		DESIGN (+)	1105		1768	
EMERGENCY	+2329 -1120		+1822 -4582		DESIGN (-)	3141		4894	

UNITS: DISPLACEMENTS : INCHES
 FORCES : POUNDS
 MOMENTS : INCH-POUNDS

TES COMBINED LOADS ARE LESS
 THAN THE LOAD SHOWN
 ON THE SUPPORT DRAWING

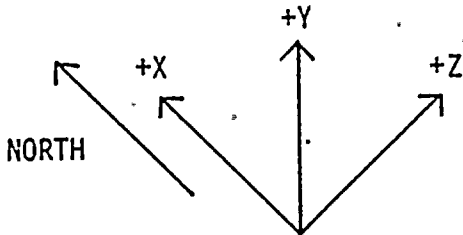
SUPPORT LOAD SUMMARY SHEET

DONALD C. COOK
UNIT #2
PROJECT 5364

BY: SHB DATE: 6-9-83

CHECKED BY: DMD DATE: 6/9/83

GLOBAL COORDINATE SYSTEM



MARK NUMBER 2-GRC-C-613

NODE NUMBER 261

DESIGN LOADINGS									
	DISPLACEMENTS			FORCES			MOMENTS		
	X	Y	Z	FX	FY	FZ	MX	MY	MZ
DEADWEIGHT-1	-0.014	.933	-0.015		720				
THERMAL-1	-0.037	3.29	.057						
THERMAL-2	-0.028	3.65	-0.011						
THERMAL-3	—	—	—						
SEISMIC-OBE	±.006	±.022	±.022						
SEISMIC-OBE	±.009	±.033	±.032						
BLOWDOWN-SRV	—	—	—						
BLOWDOWN-PORV	±.007 -.009	±.010 -.007	±.005						
TES COMBINED LOADS				SUPPORT DRAWING LOADS					
	FX	FY	FZ		FX	FY	FZ		
NORMAL/UPSET		+720				720			
EMERGENCY		+720							

UNITS: DISPLACEMENTS : INCHES
FORCES : POUNDS
MOMENTS : INCH-POUNDS

TES COMBINED LOADS ARE —
THAN THE LOAD SHOWN
ON THE SUPPORT DRAWING

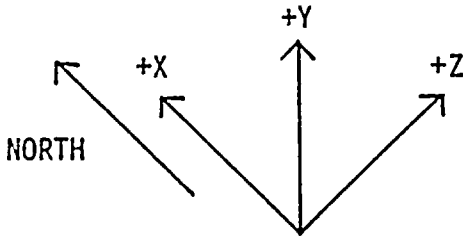
SUPPORT LOAD SUMMARY SHEET

DONALD C. COOK
UNIT #2
PROJECT 5364

BY: DLB DATE: 6-9-83

CHECKED BY: DMD DATE: 6/9/83

GLOBAL COORDINATE SYSTEM



MARK NUMBER 2-GRC-R-614

NODE NUMBER 238

	DESIGN LOADINGS								
	DISPLACEMENTS			FORCES			MOMENTS		
	X	Y	Z	FX	FY	FZ	MX	MY	MZ
DEADWEIGHT-1	.018	.198	.041	371.		-157			
THERMAL-1	-.118	3.34	-.437	-2147		912			
THERMAL-2	-.183	3.42	-.440	3293		-1393			
THERMAL-3	—	—	—	—		—			
SEISMIC-OBE	±.015	±.004	±.038	±720		±306			
SEISMIC-OBE	±.023	±.006	±.057	±1076		±457			
BLOWDOWN-SRV	—	—	—	—		—			
BLOWDOWN-PORV	+ .010 - .014	+ .002 - .031	+ .024 - .031	±670		±284			
TES COMBINED LOADS				SUPPORT DRAWING LOADS					
	FX	FY	FZ		FX	FY	FZ		
NORMAL/UPSET	+4648 -2496		±1061 -1972		DESIGN (+)	9331		538	
EMERGENCY	+1447 -2852		+1212 -614		DESIGN (-)	1264		3962	

UNITS: DISPLACEMENTS : INCHES
FORCES : POUNDS
MOMENTS : INCH-POUNDS

TES COMBINED LOADS ARE LESS
THAN THE LOAD SHOWN
ON THE SUPPORT DRAWING

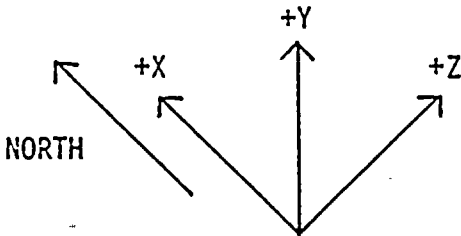
SUPPORT LOAD SUMMARY SHEET

DONALD C. COOK
 UNIT #2
 PROJECT 5364

BY: SAIB DATE: 6-9-83

CHECKED BY: DMD DATE: 6/9/83

GLOBAL COORDINATE SYSTEM



MARK NUMBER 2-GRC-R-616

NODE NUMBER 129

DESIGN LOADINGS									
	DISPLACEMENTS			FORCES			MOMENTS		
	X	Y	Z	FX	FY	FZ	MX	MY	MZ
DEADWEIGHT-1	-0.004	0	.001		-276				
THERMAL-1	.012	2.35	-.006		-558				
THERMAL-2	.063	2.35	.041		-8				
THERMAL-3	—	—	—		—				
SEISMIC-OBE	±.002		±.005		±1753				
SEISMIC-DBE	±.003		±.008		±2789				
BLOWDOWN-SRV	—		—		—				
BLOWDOWN-PORV	±.003		±.002		±754				
TES COMBINED LOADS				SUPPORT DRAWING LOADS					
	FX	FY	FZ		FX	FY	FZ		
NORMAL/UPSET		+1624 -2587				37502			
EMERGENCY		+2513 -3623				36947			

UNITS: DISPLACEMENTS : INCHES
 FORCES : POUNDS
 MOMENTS : INCH-POUNDS

TES COMBINED LOADS ARE LESS
 THAN THE LOAD SHOWN
 ON THE SUPPORT DRAWING

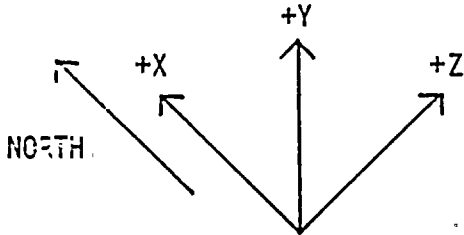
Technical Report
TR-5364-2
Revision 0

SUPPORT LOAD SUMMARY SHEET

DONALD C. COOK
UNIT #2
PROJECT 5364

BY: SAH DATE: 6-9-83
CHECKED BY: DMD DATE: 6/9/83

GLOBAL COORDINATE SYSTEM



MARK NUMBER 2-GRC-S-624

NODE NUMBER 22

DESIGN LOADINGS									
	DISPLACEMENTS			FORCES			MOMENTS		
	X	Y	Z	FX	FY	FZ	MX	MY	MZ
DEADWEIGHT-1	-0.008	-0.003	.006						
THERMAL-1	-0.069	-0.003	.065						
THERMAL-2	-0.074	-0.009	-.429						
THERMAL-3	-0.059	-0.009	-.387						
SEISMIC-OBE	+1.001	0	0	+7		+75			
SEISMIC-OBE	+1.002	+1.001	0	+11		+122			
BLOWDOWN-SRV	+1.437 -1.675	+0.088 -0.084	+0.065 -0.063	+40292		+3572			
BLOWDOWN-PORV	+1.003	0	+0	+18		+199			
TES COMBINED LOADS				SUPPORT DRAWING LOADS					
	FX	FY	FZ		FX	FY	FZ		
NORMAL/UPSET	+19		+213					1429	
EMERGENCY	+40292		+3572					1429	

UNITS: DISPLACEMENTS : INCHES
FORCES : POUNDS
MOMENTS : INCH-POUNDS

TES COMBINED LOADS ARE LESS THAN THE LOAD SHOWN ON THE SUPPORT DRAWING FOR THE NORMAL/UPSET CONDITIONS AND GREATER FOR THE EMERGENCY CONDITION.

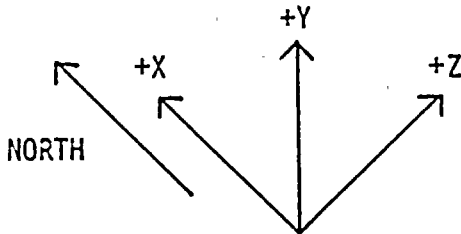
SUPPORT LOAD SUMMARY SHEET

DONALD C. COOK
 UNIT #2
 PROJECT 5364

BY: AKB DATE: 6-9-83

CHECKED BY: DMD DATE: 6/9/83

GLOBAL COORDINATE SYSTEM



MARK NUMBER 2-GRC-S-626

NODE NUMBER 402

DESIGN LOADINGS									
	DISPLACEMENTS			FORCES			MOMENTS		
	X	Y	Z	FX	FY	FZ	MX	MY	MZ
DEADWEIGHT-1	-0.017	.210	.013						
THERMAL-1	-0.270	3.39	-0.599						
THERMAL-2	-0.171	3.51	-0.575						
THERMAL-3	—	—	—						
SEISMIC-OBE	±0.048	0	±0.039		±291				
SEISMIC-DBE	±0.082	0	±0.060		±503				
BLOWDOWN-SRV	—	—	—		—				
BLOWDOWN-PORV	±0.016 -0.020	0	±0.018 -0.026		±1396				
TES COMBINED LOADS				SUPPORT DRAWING LOADS					
	FX	FY	FZ		FX	FY	FZ		
NORMAL/UPSET		±1426		DESIGN (+)		945			
EMERGENCY		±503		DESIGN (-)		945			

UNITS: DISPLACEMENTS : INCHES
 FORCES : POUNDS
 MOMENTS : INCH-POUNDS

TES COMBINED LOADS ARE GREATER
 THAN THE LOAD SHOWN
 ON THE SUPPORT DRAWING

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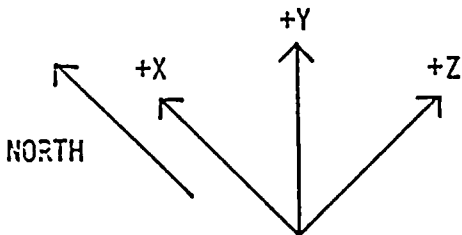
SUPPORT LOAD SUMMARY SHEET

DONALD C. COOK
UNIT #2
PROJECT 5364

BY: SAIB DATE: 6-9-83

CHECKED BY: DMD DATE: 6/9/83

GLOBAL COORDINATE SYSTEM



MARK NUMBER 2-GRC-C-627

NODE NUMBER 400

DESIGN LOADINGS									
	DISPLACEMENTS			FORCES			MOMENTS		
	X	Y	Z	FX	FY	FZ	MX	MY	MZ
DEADWEIGHT-1	-0.005	.202	.022		732				
THERMAL-1	-.238	3.38	-5.30						
THERMAL-2	-.133	3.51	-4.94						
THERMAL-3	—	—	—						
SEISMIC-OBE	±.032	±.014	±.037						
SEISMIC-DBE	±.053	±.024	±.057						
BLOWDOWN-SRV	—	—	—						
BLOWDOWN-PORV	+0.012 -0.018	+0.004	+0.022 -0.028						
TES COMBINED LOADS				SUPPORT DRAWING LOADS					
	FX	FY	FZ		FX	FY	FZ		
NORMAL/UPSET		+732			DESIGN (+)	732			
EMERGENCY		+732			DESIGN (-)				

UNITS: DISPLACEMENTS : INCHES
FORCES : POUNDS
MOMENTS : INCH-POUNDS

TES COMBINED LOADS ARE —
THAN THE LOAD SHOWN
ON THE SUPPORT DRAWING:

Technical Report
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ENGINEERING SERVICES

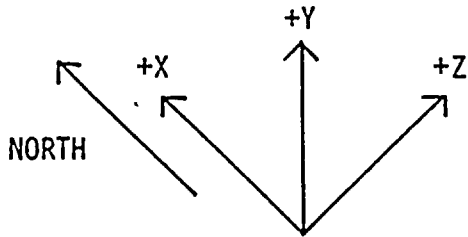
SUPPORT LOAD SUMMARY SHEET

DONALD C. COOK
 UNIT #2
 PROJECT 5364

BY: DLB DATE: 6-9-83

CHECKED BY: DMD DATE: 6/9/83

GLOBAL COORDINATE SYSTEM



MARK NUMBER 2-GRC-S-629

NODE NUMBER 228

DESIGN LOADINGS									
	DISPLACEMENTS			FORCES			MOMENTS		
	X	Y	Z	FX	FY	FZ	MX	MY	MZ
DEADWEIGHT-1	.018	.013	.036						
NORMAL-1	-.279	2.47	-.252						
THERMAL-2	-.500	2.91	-.309						
THERMAL-3	—	—	—						
SEISMIC-0BE	±.044		±.084		±1766				
SEISMIC-DBE	±.068		±.133		±2808				
BLOWDOWN-SRV	—		—		—				
BLOWDOWN-PORV	±.015 -.022		±.025 -.019		±1025				
TES COMBINED LOADS				SUPPORT DRAWING LOADS					
	FX	FY	FZ		FX	FY	FZ		
NORMAL/UPSET		±2042				5943			
EMERGENCY		±2808				5943			

UNITS: DISPLACEMENTS : INCHES
 FORCES : POUNDS
 MOMENTS : INCH-POUNDS

TES COMBINED LOADS ARE LESS
 THAN THE LOAD SHOWN
 ON THE SUPPORT DRAWING



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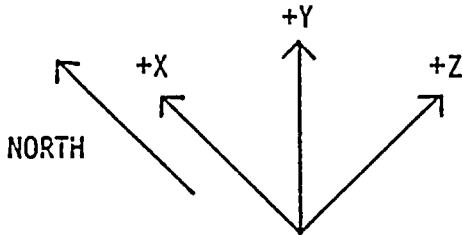
SUPPORT LOAD SUMMARY SHEET

DONALD C. COOK
UNIT #2
PROJECT 5364

BY: DLB DATE: 6-9-83

CHECKED BY: Dmd DATE: 6/9/83

GLOBAL COORDINATE SYSTEM



MARK NUMBER 2-GRC-9-630

NODE NUMBER 182

DESIGN LOADINGS

	DISPLACEMENTS			FORCES			MOMENTS		
	X	Y	Z	FX	FY	FZ	MX	MY	MZ
DEADWEIGHT-1	-0.028	.030	.005						
THERMAL-1	.003	2.65	.030						
THERMAL-2	.072	2.55	.280						
THERMAL-3	—	—	—						
SEISMIC-OBE	±.008	±.009	±.005	± 56		± 88			
SEISMIC-DBE	±.013	±.014	±.008	± 95		± 150			
BLOWDOWN-SRV	—	—	—	—		—			
BLOWDOWN-PORV	±.005 - .007	±.002	±.003 - .005	± 98		± 155			

TES COMBINED LOADS

	FX	FY	FZ
NORMAL/UPSET	± 113		± 178
EMERGENCY	± 95		± 150

SUPPORT DRAWING LOADS

	FX	FY	FZ
DESIGN (+)	339		404
DESIGN (-)	339		404

UNITS: DISPLACEMENTS : INCHES
FORCES : POUNDS
MOMENTS : INCH-POUNDS

TES COMBINED LOADS ARE LESS
THAN THE LOAD SHOWN
ON THE SUPPORT DRAWING

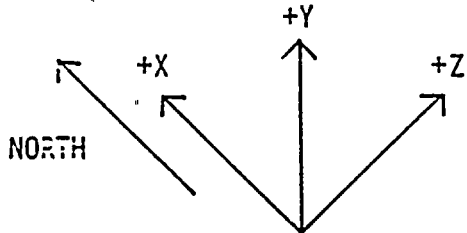
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TR-5364-2
Revision 0

SUPPORT LOAD SUMMARY SHEET

DONALD C. COOK
UNIT #2
PROJECT 5364

BY: DLB DATE: 6-9-83
CHECKED BY: DMD DATE: 6/9/83

GLOBAL COORDINATE SYSTEM



MARK NUMBER 2-GRC-S-631
NODE NUMBER 132

DESIGN LOADINGS									
	DISPLACEMENTS			FORCES			MOMENTS		
	X	Y	Z	FX	FY	FZ	MX	MY	MZ
DEADWEIGHT-1	-.023	-.005	.002						
THERMAL-1	.080	2.48	.009						
THERMAL-2	.080	2.40	.230						
THERMAL-3	—	—	—						
SEISMIC-OBE	±.002	±.025	±.002	±107		±84			
SEISMIC-DBE	±.003	±.043	±.003	±184		±146			
BLOWDOWN-SRV	—	—	—						
BLOWDOWN-PORV	±.001 -.002	±.021 -.020	±.001 -.002	±183		±145			
TES COMBINED LOADS				SUPPORT DRAWING LOADS					
	FX	FY	FZ		FX	FY	FZ		
NORMAL/UPSET	±212		±168		DESIGN (+)	681		811	
EMERGENCY	±184		±146		DESIGN (-)	681		811	

UNITS: DISPLACEMENTS : INCHES
FORCES : POUNDS
MOMENTS : INCH-POUNDS

TES COMBINED LOADS ARE LESS
THAN THE LOAD SHOWN
ON THE SUPPORT DRAWING

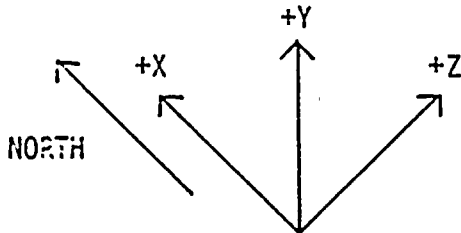
SUPPORT LOAD SUMMARY SHEET

DONALD C. COOK
 UNIT #2
 PROJECT 5364

BY: DMB DATE: 6-9-83

CHECKED BY: DMB DATE: 6/9/83

GLOBAL COORDINATE SYSTEM



MARK NUMBER 2-GRC-S-632

NODE NUMBER 78

DESIGN LOADINGS									
	DISPLACEMENTS			FORCES			MOMENTS		
	X	Y	Z	FX	FY	FZ	MX	MY	MZ
DEADWEIGHT-1	.001	-.058	-.001						
THERMAL-1	.084	2.43	.002						
THERMAL-2	.093	2.27	.197						
THERMAL-3	.035	2.25	.182						
SEISMIC-OBE	±.002	±.033	±.002	±224		±184			
SEISMIC-OBE	±.002	±.065	±.003	±384		±316			
BLOWDOWN-SRV	+ .268 - .312	+ 1.14 - 1.24	+ .384 - .441	±128356		±105579			
BLOWDOWN-PORV	±.002	±.009 - .006	±.002	±168		±138			
TES COMBINED LOADS				SUPPORT DRAWING LOADS					
	FX	FY	FZ		FX	FY	FZ		
NORMAL/UPSET	±280		±230		DESIGN (+)	2500		3167	
EMERGENCY	±128356		±105579		DESIGN (-)	2500		3167	

UNITS: DISPLACEMENTS : INCHES
 FORCES : POUNDS
 MOMENTS : INCH-POUNDS

TES COMBINED LOADS ARE LESS THAN THE LOAD SHOWN ON THE SUPPORT DRAWING FOR THE NORMAL/UPSET CONDITIONS AND GREATER FOR THE EMERGENCY CONDITION.

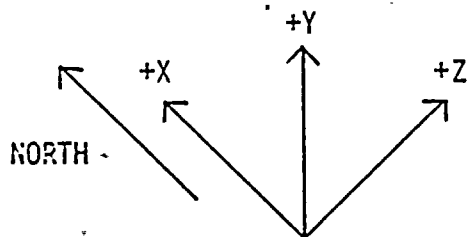
SUPPORT LOAD SUMMARY SHEET

DONALD C. COOK
UNIT #2
PROJECT 5364

BY: JMB DATE: 6-9-83

CHECKED BY: DMJ DATE: 6/9/83

GLOBAL COORDINATE SYSTEM



MARK NUMBER 2-GRC-R-633

NODE NUMBER 84

DESIGN LOADINGS

	DISPLACEMENTS			FORCES			MOMENTS		
	X	Y	Z	FX	FY	FZ	MX	MY	MZ
DEADWEIGHT-1	.003	-.051	-.003	46		40			
THERMAL-1	.106	2.68	-.120	73		64			
THERMAL-2	.276	3.32	-.312	1207		1060			
THERMAL-3	.213	2.20	-.240	1136		998			
SEISMIC-OBE	±.002	±.053	±.003	±284		±249			
SEISMIC-DBE	±.004	±.085	±.005	±488		±429			
SLOWDOWN-SRV	+1.43 -1.63	+ .890 - .883	+2.02 -1.82	±102123		±89665			
SLOWDOWN-PORV	±.002	±.003 -.006	±.003 -.002	±96		±84			

TES COMBINED LOADS

	FX	FY	FZ
NORMAL/UPSET	+1453 -238		+1363 -209
EMERGENCY	+103305 -100941		+90703 -88627

SUPPORT DRAWING LOADS

	FX	FY	FZ
DESIGN (+)	4210		3173
DESIGN (-)	1984		1495

UNITS: DISPLACEMENTS : INCHES
FORCES : POUNDS
MOMENTS : INCH-POUNDS

TES COMBINED LOADS ARE LESS THAN THE LOAD SHOWN ON THE SUPPORT DRAWING FOR THE NORMAL/UPSET CONDITIONS AND GREATER FOR THE EMERGENCY CONDITION.

6.3 Valve Accelerations

Valve accelerations were calculated for all valves due to the DBE seismic condition and the PORV transient shock condition. In addition, the acceleration of valve SV-45C was calculated for the SV transient shock condition since this valve is part of the quarter model. The horizontal allowable was taken as 3g and the vertical allowable as 2g based on the attachments to AEP letter dated September 16, 1982 from Mr. J. L. Williams of AEP to Mr. L. B. Semprucci of TES (Reference 12). For the seismic accelerations, the resultant horizontal acceleration was compared against the 3g allowable. Weights for valves NMO-151, 152 and 153 were taken as 352 pounds, in determining the seismic acceleration, since this is the value used in the seismic analysis, see Section 5.0.

For the PORV transient shock accelerations, the updated valve weight of 400 pounds was used in both the analysis and the acceleration calculations. It should be noted that valves NRV-151, NRV-152, NRV-153, NMO-151, NMO-152 and NMO-153 all fail the vertical acceleration criteria of 2g and valves NMO-151, 152 and 153 exceed the horizontal acceleration criteria of 3g. These values are considered acceptable per reference 7 (see Section 2.0).

The acceleration of valve SV-45C for the SV transient shock condition exceeds all criteria by a large margin, which further indicates the failure of the system during emergency conditions.

6.3.1 DBE Seismic Valve Accelerations

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CHECKED BY: J.H. DATE: 5-12-83

VALVE NO.		SV-45A			SV-45B			SV-45C		
NODE NO.		1980			1540			105		
		ACCELERATION			ACCELERATION			ACCELERATION		
		A _x	A _y	A _z	A _x	A _y	A _z	A _x	A _y	A _z
SHOCK DIRECTION	X	1.02	.16	.41	1.47	.19	.34	.82	.12	.80
	Y	.04	.02	.05	.06	.03	.05	.06	.03	.06
	Z	.42	.20	1.34	.34	.16	1.07	.81	.14	1.05
SRSS RESULTS	A _{xT}	1.10 g			1.51 g			1.15 g		
	A _{yT}	.26 g			.25 g			.19 g		
	A _{zT}	1.40 g			1.12 g			1.32 g		
		ACCEL.	ALLOWABLE		ACCEL.	ALLOWABLE		ACCEL.	ALLOWABLE	
VERTICAL A _{yT}		.26 g	2 g		.25 g	2 g		.19 g	2 g	
HORIZONTAL *		1.78 g	3 g		1.88 g	3 g		1.75 g	3 g	

$$* \text{ HORIZONTAL ACCELERATION} = \sqrt{(A_{xT})^2 + (A_{zT})^2}$$

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VALVE NO.		NMO-151			NMO-152			NMO-153		
NODE NO.		301			355			271		
		ACCELERATION			ACCELERATION			ACCELERATION		
		A _x	A _y	A _z	A _x	A _y	A _z	A _x	A _y	A _z
SHOCK DIRECTION	X	.35	.17	.39	.78	.35	.40	.54	.39	.90
	Y	.17	.09	.11	.16	.16	.08	.11	.12	.19
	Z	.50	.24	.91	.49	.26	.35	.51	.19	1.14
SRSS RESULTS	A _{xT}	.63 g			.93 g			.75 g		
	A _{yT}	.32 g			.46 g			.45 g		
	A _{zT}	1.00 g			.54 g			1.46 g		
		ACCEL.	ALLOWABLE		ACCEL.	ALLOWABLE		ACCEL.	ALLOWABLE	
VERTICAL A _{yT}		.32 g	2 g		.46 g	2 g		.45 g	2 g	
HORIZONTAL *		1.18 g	3 g		1.07 g	3 g		1.65 g	3 g	

* HORIZONTAL ACCELERATION = $\sqrt{(A_{xT})^2 + (A_{zT})^2}$

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VALVE NO.		NRV-151			NRV-152			NRV-153		
NODE NO.		295			347			365		
		ACCELERATION			ACCELERATION			ACCELERATION		
		A _x	A _y	A _z	A _x	A _y	A _z	A _x	A _y	A _z
SHOCK DIRECTION	X	.54	.18	.61	1.40	.19	.75	.62	.31	.91
	Y	.13	.33	.12	.12	.09	.19	.22	.10	.13
	Z	.86	.22	1.53	.72	.14	.53	.47	.18	1.26
SRSS RESULTS	A _{XT}	1.02 g			1.58 g			.82 g		
	A _{YT}	.30 g			.25 g			.37 g		
	A _{ZT}	1.67 g			.94 g			1.56 g		
		ACCEL.	ALLOWABLE	ACCEL.	ALLOWABLE	ACCEL.	ALLOWABLE	ACCEL.	ALLOWABLE	ACCEL.
VERTICAL A _{YT}		.30 g	2 g	.25 g	2 g	.37 g	2 g	.37 g	2 g	.37 g
HORIZONTAL *		1.97 g	3 g	1.84 g	3 g	1.76 g	3 g	1.76 g	3 g	1.76 g

* HORIZONTAL ACCELERATION = $\sqrt{(A_{XT})^2 + (A_{ZT})^2}$

6.3.2 PORV Transient Shock and SV Transient Shock Valve Accelerations

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CHECKED BY: AMB DATE: 8 June 83

VALVE ACCELERATIONS

VALVE	SV-45A			SV-45B		
NODE NUMBER	1980			1540		
VALVE WEIGHT	685 LBS			685 LBS		
DIRECTION	X	Y	Z	X	Y	Z
FORCE (LBS)	36	56	49	41	47	53
ACCELERATION	.05g	.08g	.07g	.06g	.07g	.08g
ALLOWABLE	3g	2g	3g	3g	2g	3g

VALVE	SV-45C			SV-45C *		
NODE NUMBER	105			105		
VALVE WEIGHT	685 LBS			685 LBS		
DIRECTION	X	Y	Z	X	Y	Z
FORCE (LBS)	27	34	21	19469	21145	8192
ACCELERATION	.04g	.05g	.03g	28.4g	30.9g	12.0g
ALLOWABLE	3g	2g	3g	3g	2g	3g

* ACCELERATIONS ARE THE RESULTS OF THE SV TRANSIENT SHOCK CONDITION FROM THE QUARTER MODEL ANALYSIS. ALL OTHER VALVE ACCELERATIONS IN THIS SECTION RESULT FROM THE PORV TRANSIENT SHOCK CONDITION.

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VALVE ACCELERATIONS

VALVE	NMO-151			NMO-152		
NODE NUMBER	301			355		
VALVE WEIGHT	400 LBS			400 LBS		
DIRECTION	X	Y	Z	X	Y	Z
FORCE (LBS)	1413	891	633	636	1248	1498
ACCELERATION	3.53g	2.23g	1.58g	1.59g	3.12g	3.75g
ALLOWABLE	3g	2g	3g	3g	2g	3g

VALVE	NMO-153					
NODE NUMBER	271					
VALVE WEIGHT	400 LBS					
DIRECTION	X	Y	Z	X	Y	Z
FORCE (LBS)	1554	1156	632			
ACCELERATION	3.89g	2.89g	1.58g			
ALLOWABLE	3g	2g	3g			

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VALVE ACCELERATIONS

VALVE	NRV-151			NRV-152		
NODE NUMBER	295			349		
VALVE WEIGHT	480 LBS			480 LBS		
DIRECTION	X	Y	Z	X	Y	Z
FORCE (LBS)	597	1003	234	346	1754	647
ACCELERATION	1.24g	2.09g	.49g	.72g	3.65g	1.35g
ALLOWABLE	3g	2g	3g	3g	2g	3g

VALVE	NRV-153					
NODE NUMBER	265					
VALVE WEIGHT	480 LBS					
DIRECTION	X	Y	Z	X	Y	Z
FORCE (LBS)	555	1123	222			
ACCELERATION	1.16g	2.34g	.46g			
ALLOWABLE	3g	2g	3g			

6.4 Nozzle Loads

Forces and Moments for the four pressurizer nozzles and the quench tank nozzles are given in this section for each loading condition analyzed.

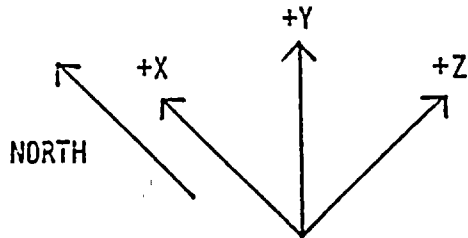
NOZZLE LOAD SUMMARY SHEET

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 UNIT #2
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CHECKED BY: AMB DATE: 6-8-83

GLOBAL COORDINATE SYSTEM



NODE NUMBER 2

	DESIGN LOADINGS								
	DISPLACEMENTS			FORCES			MOMENTS		
	X	Y	Z	FX	FY	FZ	MX	MY	MZ
DEADWEIGHT-1	—	—	—	70	-950	50	-2580	-3220	-6470
THERMAL-1	—	—	—	460	590	1150	53470	-41790	-117040
THERMAL-2	—	—	—	-120	180	-110	-310	23990	-27730
THERMAL-3	—	—	—	-160	170	-200	-2360	25980	-22200
SEISMIC-OBE	—	—	—	±36	±94	±50	±795	±1565	±4116
SEISMIC-DBE	—	—	—	±58	±166	±85	±1329	±2599	±7133
BLOWDOWN-SRV	—	—	—	±32019	±19725	±27766	±351784	±858752	±973166
BLOWDOWN-PORV	—	—	—	±351	±117	±104	±1569	±3272	±5446

UNITS: DISPLACEMENTS : INCHES
 FORCES : POUNDS
 MOMENTS : INCH-POUNDS

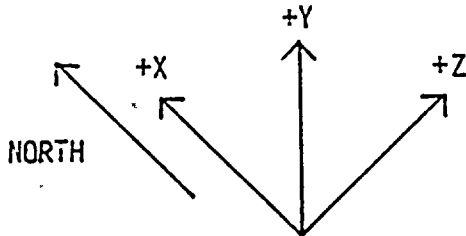
NOZZLE LOAD SUMMARY SHEET

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GLOBAL COORDINATE SYSTEM



NODE NUMBER 124

	DESIGN LOADINGS								
	DISPLACEMENTS			FORCES			MOMENTS		
	X	Y	Z	FX	FY	FZ	MX	MY	MZ
DEADWEIGHT-1	—	—	—	-60	-980	0	-19300	-1010	-2569
THERMAL-1	—	—	—	-180	-320	150	-160	-5150	-13550
THERMAL-2	—	—	—	-230	-200	-40	7220	11740	-16410
THERMAL-3	—	—	—	-200	-100	-80	6990	11450	-13570
SEISMIC-OBE	—	—	—	±591	±852	±701	±16243	±13095	±17376
SEISMIC-DBE	—	—	—	±1003	±1406	±1213	±28151	±21905	±28949
BLOWDOWN-SRV	—	—	—	±14971	±33525	±52119	±1674445	±559588	±419711
BLOWDOWN-PORV	—	—	—	±29	±55	±45	±1716	±823	±766

UNITS: DISPLACEMENTS : INCHES
 FORCES : POUNDS
 MOMENTS : INCH-POUNDS

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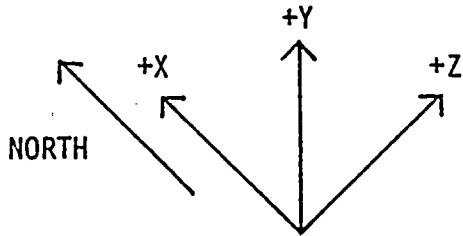
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GLOBAL COORDINATE SYSTEM



NODE NUMBER 174

	DESIGN LOADINGS								
	DISPLACEMENTS			FORCES			MOMENTS		
	X	Y	Z	FX	FY	FZ	MX	MY	MZ
DEADWEIGHT-1	—	—	—	0	-910	-40	-7530	-800	-20980
THERMAL-1	—	—	—	-380	-490	-110	16750	-10960	-7250
THERMAL-2	—	—	—	-70	-270	20	6460	-950	790
SEISMIC-OBE	—	—	—	±891	±1210	±790	±15309	±16045	±22664
SEISMIC-OBE	—	—	—	±1542	±1991	±1300	±25318	±26549	±39163
BLOWDOWN-SRV	—	—	—	—	—	—	—	—	—
BLOWDOWN-PORV	—	—	—	±57	±78	±56	±1212	±1081	±2519

UNITS: DISPLACEMENTS : INCHES
FORCES : POUNDS
MOMENTS : INCH-POUNDS



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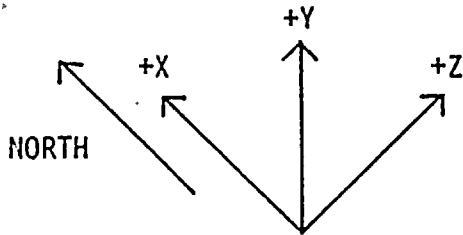
NOZZLE LOAD SUMMARY SHEET

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GLOBAL COORDINATE SYSTEM



NODE NUMBER 218

	DESIGN LOADINGS								
	DISPLACEMENTS			FORCES			MOMENTS		
	X	Y	Z	FX	FY	FZ	MX	MY	MZ
DEADWEIGHT-1	—	—	—	40	-989	-10	15160	-250	-13760
THERMAL-1	—	—	—	-276	-860	-579	21990	-21679	24070
THERMAL-2	—	—	—	90	-400	-60	4940	-970	15200
SEISMIC-OBE	—	—	—	±740	±1100	±780	±22610	±14193	±7406
SEISMIC-OBE	—	—	—	±1221	±1821	±1331	±37426	±23445	±12649
BLOWDOWN-SRV	—	—	—	—	—	—	—	—	—
BLOWDOWN-PORV	—	—	—	±57	±86	±56	±1725	±1000	±1503

UNITS: DISPLACEMENTS : INCHES
 FORCES : POUNDS
 MOMENTS : INCH-POUNDS

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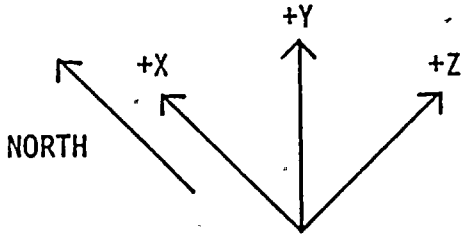
NOZZLE LOAD SUMMARY SHEET

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GLOBAL COORDINATE SYSTEM



NODE NUMBER 342

	DESIGN LOADINGS								
	DISPLACEMENTS			FORCES			MOMENTS		
	X	Y	Z	FX	FY	FZ	MX	MY	MZ
DEADWEIGHT-1	—	—	—	310	-170	10	1330	4320	-13070
THERMAL-1	—	—	—	70	-60	-1150	-87270	38800	29390
THERMAL-2	—	—	—	40	450	-1159	-97290	31640	26650
SEISMIC-OBE	—	—	—	±182	±284	±241	±15557	±12931	±10248
SEISMIC-DBE	—	—	—	±294	±477	±393	±23938	±19320	±15538
BLOWDOWN-SRV	—	—	—	—	—	—	—	—	—
BLOWDOWN-PORV	—	—	—	±650	±6248	±554	±19815	±5301	±17464

UNITS: DISPLACEMENTS : INCHES
 FORCES : POUNDS
 MOMENTS : INCH-POUNDS



6.5 Valve Loads

Section 6.5 gives the moments on each end of all valves in the piping system for each loading condition analyzed.

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VALVE END MOMENTS

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VALVE NUMBER SV-45A

NODE NUMBER	196			200		
	MX	MY	MZ	MX	MY	MZ
DEADWEIGHT	2532	998	4853	3242	1046	14021
THERMAL 1	-22224	2773	4017	-12742	12244	-14350
THERMAL 2	2172	1696	-9635	2836	2570	-14309
SEISMIC OBE	±8522	±3675	±1779	±2077	±1291	±8896
SEISMIC DBE	±14573	±6280	±2978	±3497	±2148	±14684
BLOWDOWN PORV	±882	±285	±597	±917	±730	±854

VALVE NUMBER _____

NODE NUMBER						
	MX	MY	MZ	MX	MY	MZ
DEADWEIGHT						
THERMAL 1						
THERMAL 2						
SEISMIC OBE						
SEISMIC DBE						
BLOWDOWN PORV						

UNITS: INCH-POUNDS

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VALVE END MOMENTS

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BY: JMB DATE: 6-8-83

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VALVE NUMBER SV-45B

NODE NUMBER	152			156		
	MX	MY	MZ	MX	MY	MZ
DEADWEIGHT	3963	1343	99	13948	1588	5144
THERMAL 1	-6572	1225	14663	-11581	7505	4517
THERMAL 2	2055	-1423	-1573	-2199	-544	-4628
THERMAL-3	—	—	—	—	—	—
SEISMIC OBE	±3762	±3713	±12031	±6927	±906	±6495
SEISMIC DBE	±6504	±6423	±20814	±11460	±1507	±10755
BLOWDOWN PORV	±375	±196	±419	±872	±685	±460

VALVE NUMBER SV-45C

NODE NUMBER	103			107		
	MX	MY	MZ	MX	MY	MZ
DEADWEIGHT	1798	819	-3676	7708	1492	-10836
THERMAL 1	5555	299	9505	-650	3946	9948
THERMAL 2	-8372	-10721	18035	-9908	-8612	16182
THERMAL-3	-9678	-9073	17487	-9336	-7745	14976
SEISMIC OBE	±9863	±2919	±7704	±7041	±746	±4154
SEISMIC DBE	±17131	±5077	±13374	±11679	±1244	±6881
BLOWDOWN PORV	±620	±130	±564	±750	±557	±706
BLOWDOWN SRV	±433358	±84761	±502148	±391070	±255572	±578093

UNITS: INCH-POUNDS

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VALVE END MOMENTS

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VALVE NUMBER NRV-151

NODE NUMBER	292			296		
	MX	MY	MZ	MX	MY	MZ
DEADWEIGHT	1305	1338	6933	1460	1690	6549
THERMAL 1	6579	1741	-6163	6375	-2570	-5656
THERMAL 2	4729	213	-2379	4594	-1096	-2044
SEISMIC OBE	±7008	±6142	±1983	±7941	±7814	±6151
SEISMIC DBE	±11146	±9772	±3029	±12646	±12433	±9834
BLOWDOWN PORV	±3576	±1129	±7671	±7647	±2661	±13478

VALVE NUMBER NMD-151

NODE NUMBER	298			302		
	MX	MY	MZ	MX	MY	MZ
DEADWEIGHT	2967	2084	2817	4660	2428	-2677
THERMAL 1	6141	-7434	-5077	5941	-11682	-4531
THERMAL 2	4439	-2581	-1662	4307	-3862	-1334
SEISMIC OBE	±8219	±6296	±4674	±11359	±3878	±4451
SEISMIC DBE	±13090	±10021	±7504	±18076	±6171	±7087
BLOWDOWN PORV	±8087	±5021	±10421	±4703	±5603	±8713

UNITS: INCH-POUNDS

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VALVE END MOMENTS

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UNIT #2
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BY: AMB DATE: 5.27.83

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VALVE NUMBER NRV-152

NODE NUMBER	346			350		
	MX	MY	MZ	MX	MY	MZ
DEADWEIGHT	809	-275	1382	-2492	-389	54
THERMAL 1	11080	5888	4243	10447	1662	3988
THERMAL 2	15352	1300	9007	12609	-1039	7899
SEISMIC OBE	±3106	±4196	±5116	±4329	±5260	±7278
SEISMIC DBE	±5275	±7312	±8915	±7257	±9160	±12551
BLOWDOWN PORV	±7740	±1096	±4492	±8822	±2339	±7346

VALVE NUMBER NMO-152

NODE NUMBER	352			356		
	MX	MY	MZ	MX	MY	MZ
DEADWEIGHT	-3004	-546	-157	-1051	-660	109
THERMAL 1	9575	-4166	3635	8954	-3322	3385
THERMAL 2	8824	-4264	6371	6133	-6576	5286
SEISMIC OBE	±3712	±3372	±7236	±3792	±1538	±9170
SEISMIC DBE	±6252	±5827	±12497	±6515	±2534	±15906
BLOWDOWN PORV	±10489	±5586	±5966	±14880	±6371	±6195

UNITS: INCH-POUNDS

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VALVE END MOMENTS

DONALD C. COOK
UNIT #2
PROJECT 5364

BY: AMB DATE: 5-27-83

CHECKED BY: SM DATE: 5/27/83

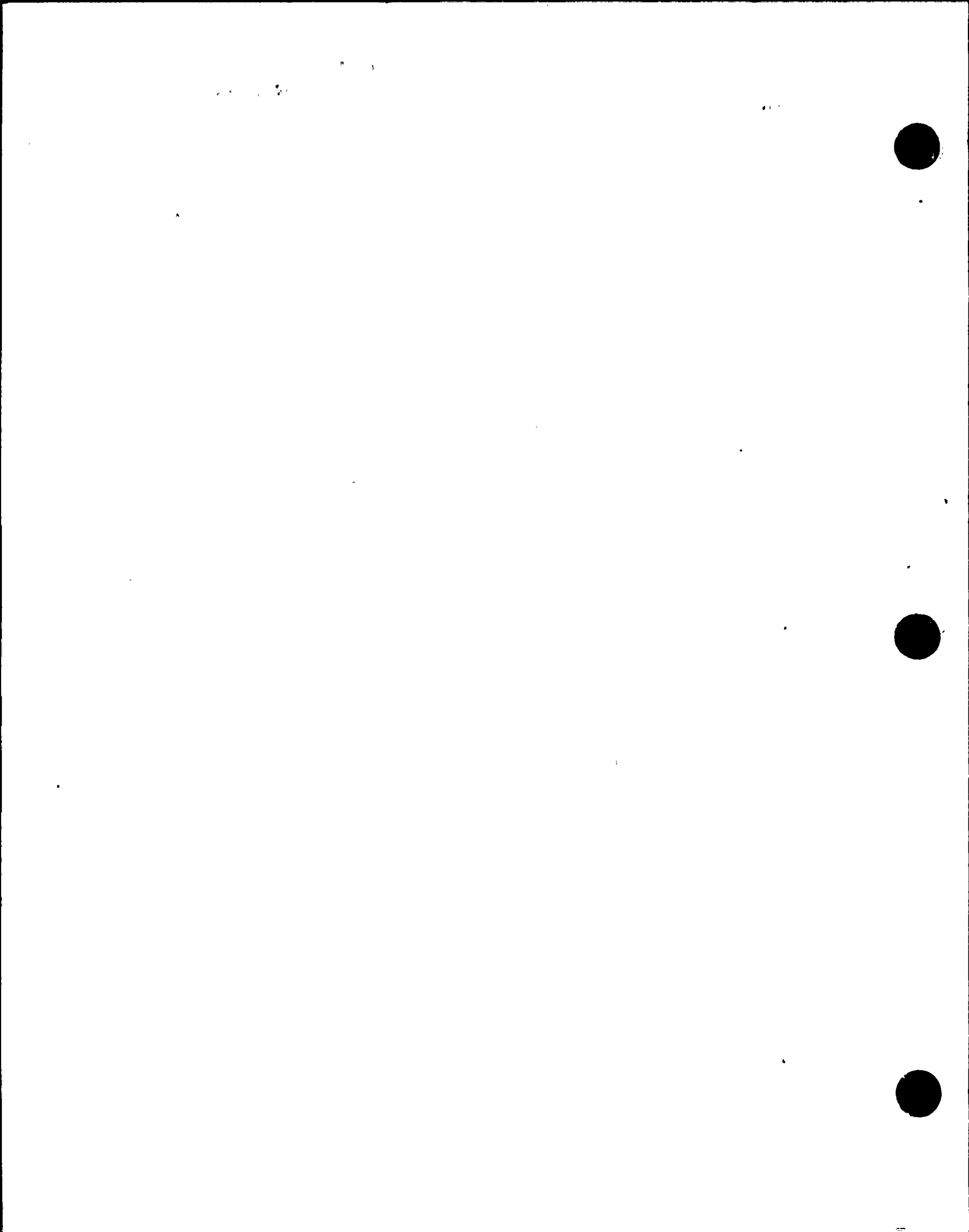
VALVE NUMBER NRV-153

NODE NUMBER	262			266		
	MX	MY	MZ	MX	MY	MZ
DEADWEIGHT	3490	-224	-3953	5265	-41	-8350
THERMAL 1	-9400	-7395	-8140	-10151	-6228	-6280
THERMAL 2	1198	-3818	-996	2002	-2637	-2988
SEISMIC OBE	± 9149	± 770	± 4255	± 4528	± 2963	± 4959
SEISMIC DBE	± 13560	± 1221	± 6318	± 7296	± 4435	± 8120
BLOWDOWN PORV	± 2573	± 1296	± 7121	± 6328	± 1946	± 13676

VALVE NUMBER NMO-153

NODE NUMBER	268			272		
	MX	MY	MZ	MX	MY	MZ
DEADWEIGHT	6007	180	-10184	6196	360	-9360
THERMAL 1	-11065	-4200	-4020	-11800	-2566	-2196
THERMAL 2	2981	-1202	-5409	3768	-42	-7363
SEISMIC OBE	± 3722	± 6476	± 2187	± 7515	± 6167	± 2910
SEISMIC DBE	± 5692	± 9605	± 3625	± 11152	± 9150	± 4402
BLOWDOWN PORV	± 5957	± 2541	± 11249	± 4781	± 2193	± 12104

UNITS: INCH-POUNDS



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 **TELEDYNE
ENGINEERING SERVICES**

6.6 Miscellaneous Calculations



6.6.1 Thermal Boundary Displacements

Revision Q



BY DMD DATE 4/8/83
CHKD. BY JLR DATE 4-12-83

THERMAL BOUNDARY DISPLACEMENTS
NORMAL THERMAL CONDITION

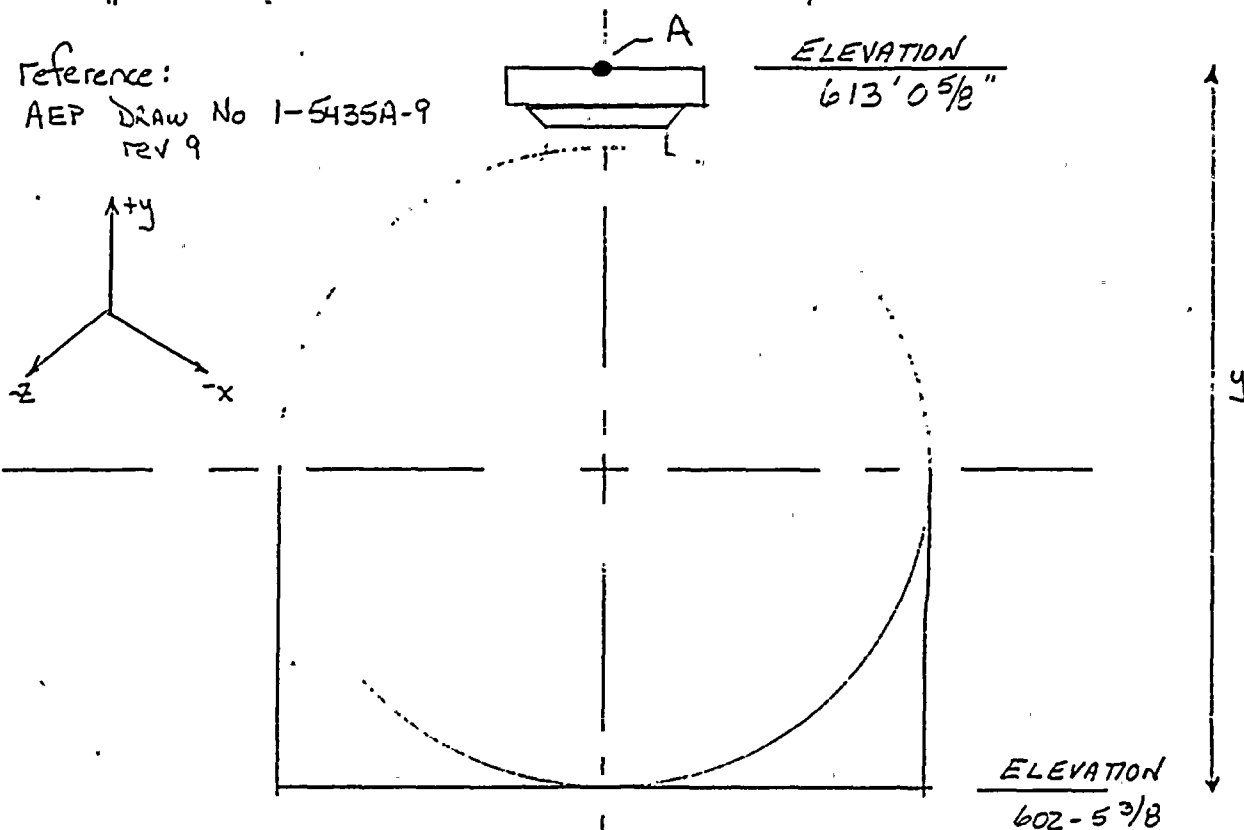
SHEET NO. 1 OF
PROJ. NO. 5364

UNITS 1/2

Temperature @ Quench Tank = 85°F (per AEP letter dated 11/29/82)

Reference:

AEP DRAW No 1-5435A-9
REV 9



Want displacements at point A

$$y = \frac{613' - 0 \frac{5}{8}'' - 602' - 5 \frac{3}{8}''}{10' - 7 \frac{1}{4}''} = 10.604'$$

x movement = z movement = 0 since nozzle is at ϕ of Q-tank

y movement = $\alpha \Delta t l$

$\alpha = 6.135 \times 10^{-6}$ in/in/°F (for ferritic carbon steel)

$\Delta t = 15^\circ\text{F}$ (85-70)

$l = 10.604' = 127.248''$

$\Delta y = 6.135 \times 10^{-6} \times 15 \times 127.248 = .0117''$

Summary $\Delta x = 0$ $\Delta y = +.0117''$ $\Delta z = 0$

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TELEDYNE ENGINEERING SERVICES



BY Dmb. DATE 4/12/83
CHKD. BY [Signature] DATE 4-12-83

$\alpha, \Delta T$ Values UNITS 1/2

SHEET NO. 1 OF
PROJ. NO. 5364

temperature $\Rightarrow 653^{\circ}F$

$$\Delta T = 653 - 70 = 583$$

for austentic stainless steel $\alpha_{650} = 9.87 \times 10^{-6}$

$$\alpha_{700} = 9.93 \times 10^{-6}$$

$$\alpha_{700} - \alpha_{650} = 9.93 - 9.87 = .06$$

$$\therefore \frac{.06}{50^{\circ}} = \frac{x}{3^{\circ}} \quad x = .0036$$

$$\alpha_{653} = 9.87 + .0036 = 9.8736 \times 10^{-6}$$

temperature = 85°

$$\Delta T = 85 - 70 = 15^{\circ}$$

for austentic stainless steel

$$\alpha_{70} = 9.11 \times 10^{-6}$$

$$\alpha_{100} = 9.16 \times 10^{-6}$$

$$\alpha_{100} - \alpha_{70} = 9.16 - 9.11 = .05$$

$$\frac{.05}{30} = \frac{x}{15} \Rightarrow x = .025$$

$$\alpha_{85} = 9.11 + .025 = 9.135 \times 10^{-6}$$



BY DMD DATE 4/12/83
 CHKD. BY [Signature] DATE 4-15-83

Thermal Boundary Displacements
 Normal Thermal Condition

SHEET NO. 2 OF
 PROJ. NO. 5364

Temperature of Pressurizer = 653°F (per AEP letter dated 11/29/82)

- References ① AEP DRAW No 1-5435-8 rev 8
 ② (W) DRAW No 1097 J56 sheet 1 of 2
 ③ AEP DRAW No 1-5436-8

per reference ② dimension from base of pressurizer to SRV & PORV nozzles is :

$$635.5 - (52.00 - 35.06) = 618.56''$$

Δy will be same for all four nozzles since the elevations are the same.

$$\alpha_{503^\circ} = 7.3366 \times 10^{-6} \text{ in./in./}^\circ\text{F for carbon steel @ } 653^\circ$$

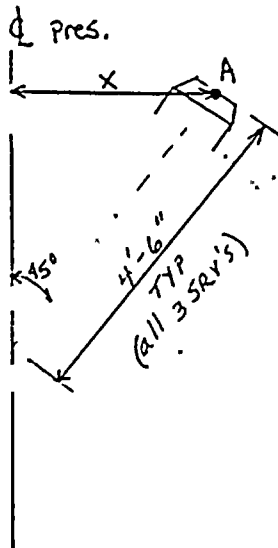
$$l = 618.56''$$

$$\Delta t = 653 - 70 = 583$$

$$\Delta y = + \alpha \Delta t l = 7.3366 \times 10^{-6} \times 618.56'' \times 583^\circ\text{F} = 2.6457''$$

radial growth

per section "G-7" of ref 3



$$\frac{\sin 90}{4.5} = \frac{\sin 45}{x}$$

$$x = 3.182' = 38.1838''$$

note: this page of calculations is the same for both units since the pressurizer & nozzle dimensions are essentially identical



BY: DMD DATE 4/13/83
 CHKD. BY: AMB DATE 4-13-83

Thermal Boundary Displacements
 NORMAL THERMAL CONDITION

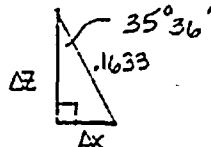
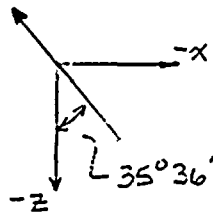
SHEET NO. 3 OF
 PROJ. NO. 5.364

UNIT 2

radial $\Delta = 7.3366 \times 10^{-6} \times 583 \times 38.1838 = .1633''$

determine X & Z Components for radial Δ for each SRV valve nozzle

Valve SV-45A



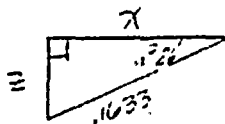
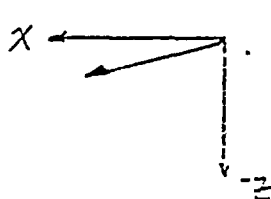
$$\frac{\sin 90}{.1633} = \frac{\sin 35^{\circ}36'}{\Delta X} = \frac{\cos 35^{\circ}36'}{\Delta Z}$$

$\Delta X = + .0951$

$\Delta Z = + .1328$



valve SV-45B

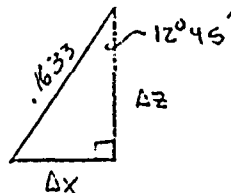
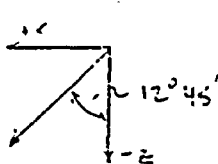


$$\frac{\sin 90}{.1633} = \frac{\sin 11^{\circ}26'}{-\Delta Z} = \frac{\cos 11^{\circ}26'}{\Delta X}$$

$\Delta X = + .1601$

$\Delta Z = - .0324$

valve SV-45C



$$\frac{\sin 90}{.1633} = \frac{\sin 12^{\circ}45'}{\Delta X} = \frac{\cos 12^{\circ}45'}{-\Delta Z}$$

$\Delta X = + .0360$

$\Delta Z = - .1593$

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TELEDYNE ENGINEERING SERVICES

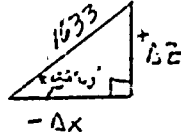
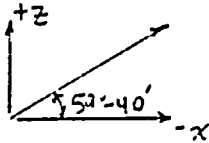
BY DMD DATE 4/13/83
CHKD. BY DWB DATE 4-13-83

Thermal Boundary Displacements
NORMAL THERMAL CONDITION

SHEET NO. 4 OF
PROJ. NO. 5364

UNIT 2

Porv Relief Line



$$\frac{\sin 90}{.1633} = \frac{\sin 59^{\circ}40'}{+\Delta z} = \frac{\cos 59^{\circ}40'}{-\Delta x}$$

$$\Delta x = -.0825$$

$$\Delta z = +.1409$$

for the 4 pressurizer nozzles the following displacements will be inserted.

node 218
(valve SV-45A)

$$\Delta x = +.0951''$$

$$\Delta y = +2.6457''$$

$$\Delta z = +.1328''$$

node 174
(SV-45B)

$$\Delta x = +.1601''$$

$$\Delta y = +2.6457''$$

$$\Delta z = -.0324''$$

node 124
(SV-45C)

$$\Delta x = +.0360''$$

$$\Delta y = +2.6457''$$

$$\Delta z = -.1593''$$

node 342
(Porv Relief)

$$\Delta x = -.0825''$$

$$\Delta y = +2.6457''$$

$$\Delta z = +.1409''$$

6.6.2 OBE Spectra

Technical Report
 TR-5364-2

Revision

BY SMB DATE 4/8/83CHKD. BY SMB DATE 4/8/83

Response Spectra

SHEET NO. 1 OF PROJ. NO. 5364

OBE Analysis

For both Units 1 & 2 the attached spectra curves indicate that Containment CRANE WALL elevation 687'-6" governs for all frequencies. Therefore the horizontal ($X \& Z$) response spectra for OBE analysis is

f	g
.5	.10
1.0	.30
1.2	.50
1.7	5.0
2.3	5.0
3.6	1.10
5.0	.90
10.0	.60
21.0	.42
50.0	.42

VERTICAL

The vertical, OBE response, per the attached spectra, is:

f	g
.5	.04
1.0	.13
1.22	.20
1.70	1.33
2.30	1.33
3.10	1.62
5.00	1.62
10.0	.23
22.0	.12
50.0	.12

Technical Report
TR-5364-2

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PROJECT 5364
D C Cook

by: SLD 4/8/83

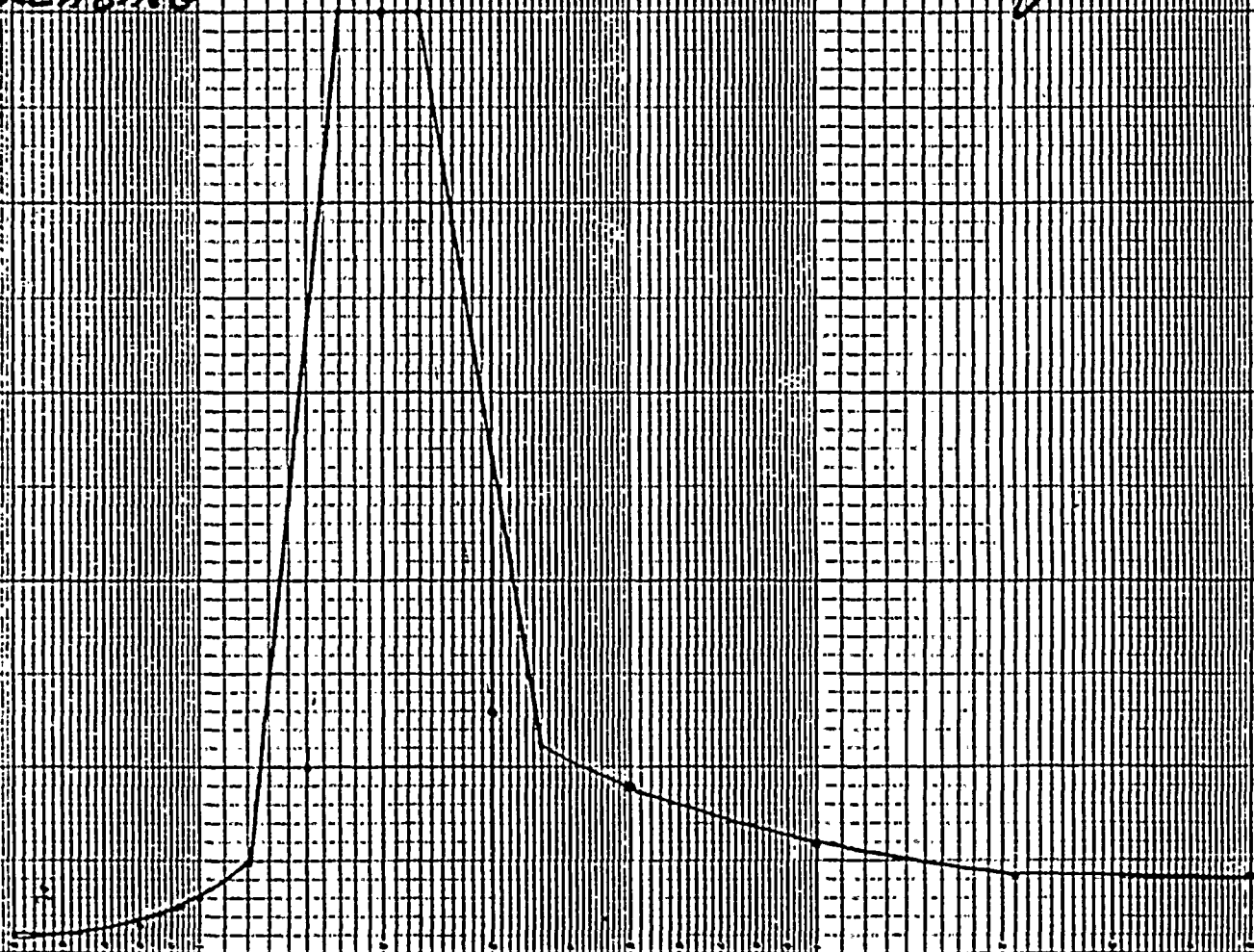
checked by: BMS 4/8/83

HORIZONTAL
5% EQUIPMENT DAMPING
2% STRUCTURAL DAMPING
CONTAINMENT CRANE WALL
ELEVATION 687'6"
OBE ANALYSIS
15% PEAK SPREADING

9
5
4
3
2
1

POINTS

5	9
5	11
1.0	3
1.2	5
1.7	5.0
2.3	5.0
3.6	1.2
5.0	9
10.0	6
21.0	42
50.0	42



6-155

10 10.0 frequency 100.0

0000
1
00000000



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Revision 0

HORIZONTAL

.5% EQUIPMENT DAMPING
2% STRUCTURAL DAMPING
CONTAINMENT CRANE WALL
ELEVATION 675' 4"
DBE ANALYSIS
±15% PEAK SPREADING

PROJECT 5364
DC Cook
by: DMB 4/8/83
Checked by: JME 4/8/83

9

5

4

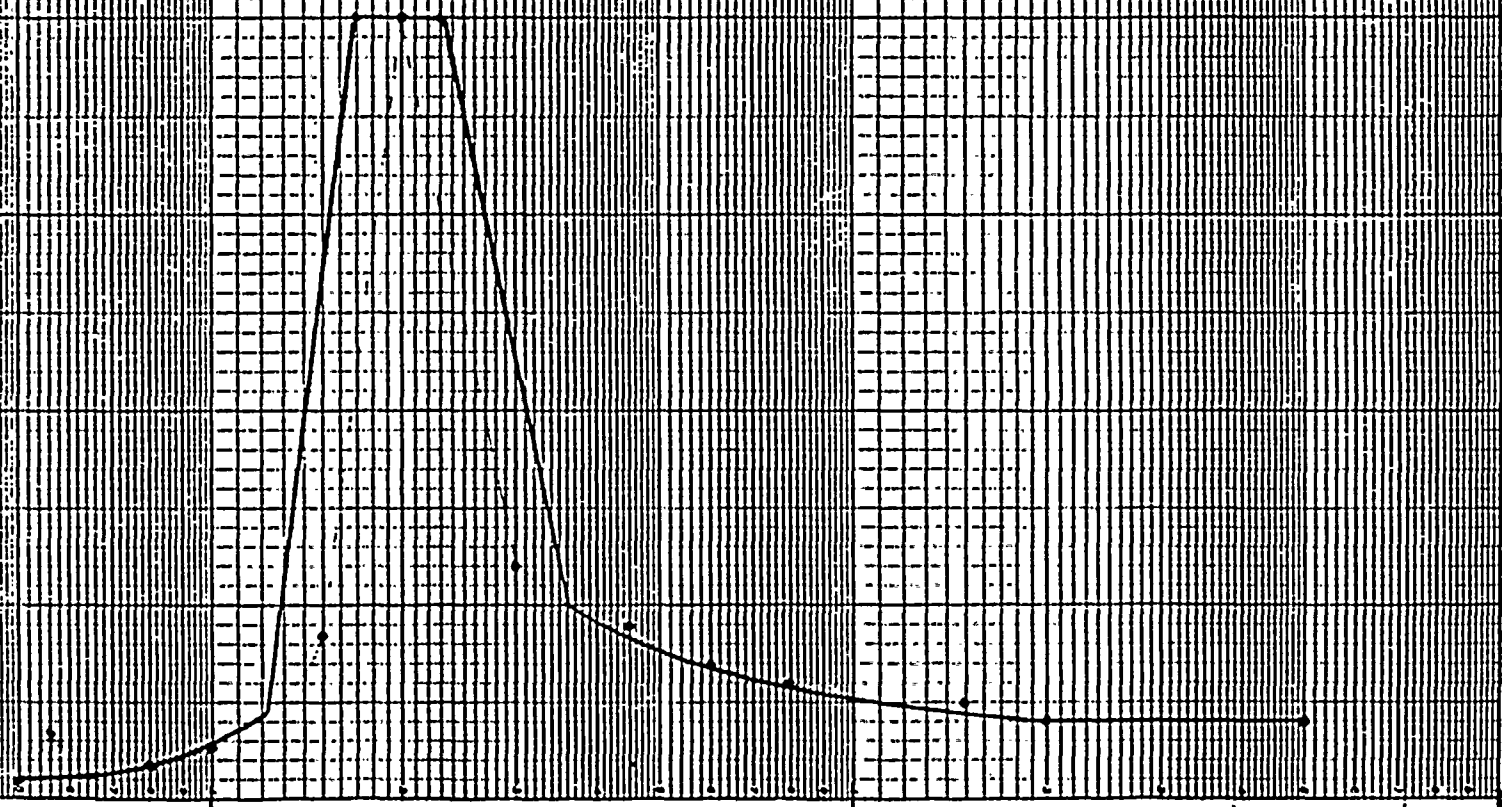
3

2

1

Points

f	g
.5	.10
1.0	.28
1.2	.42
1.7	1.0
2.3	4.0
3.6	1.0
6.0	.7
10.0	.5
20.0	.4
50.0	.4



6-156

HORIZONTAL
 5% EQUIPMENT DAMPING
 2% STRUCTURAL DAMPING
 CONTAINMENT CRANE WALL
 ELEVATION 663'4"
 OBE ANALYSIS
 ± 15% PEAK SPREADING

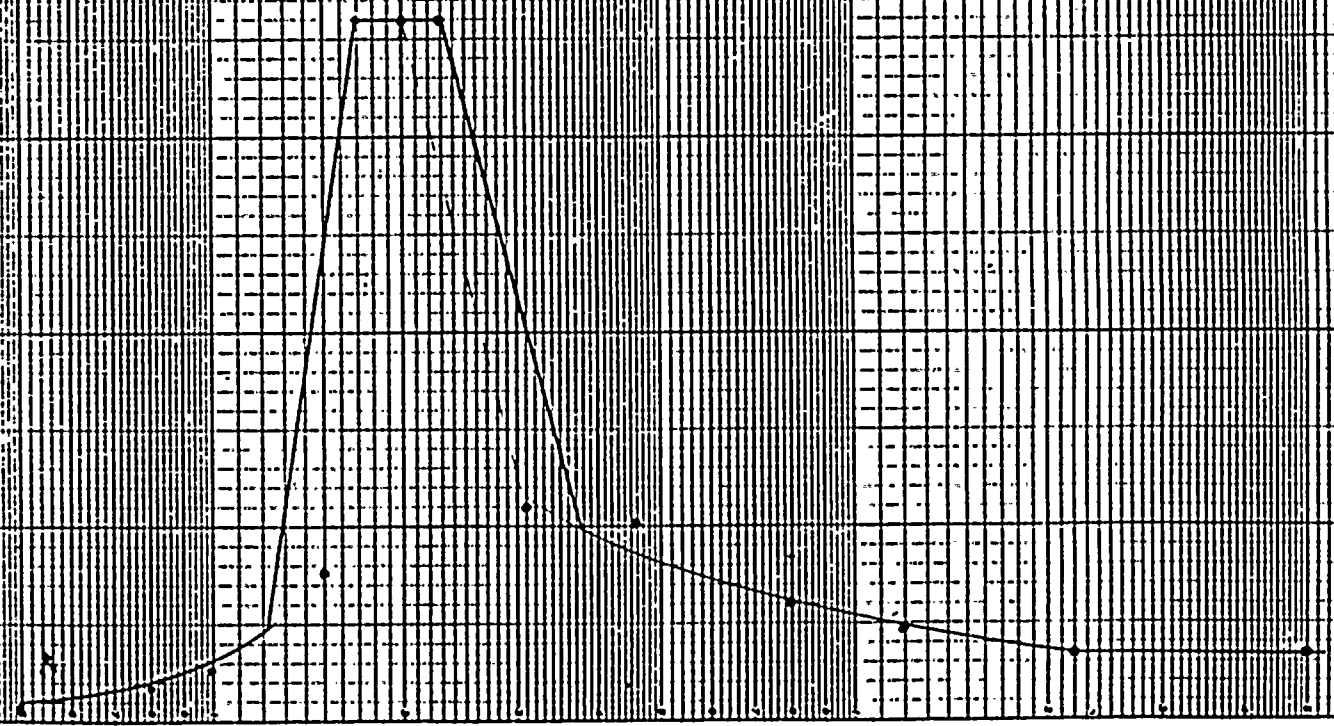
Project 5364
 D C Cook

by: D.H.D. 4/8/83

checked by: A.M.B. 4/8/83

Points

	<u>f</u>	<u>g</u>
4	.5	.10
	1.0	.30
3	1.21	.50
	1.70	3.60
	2.30	3.60
2	3.80	1.00
	8.0	.60
	12.0	.50
1	22.0	.35
	50.0	.35



6-157

1.0

10.0

100

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Handwritten text, possibly a signature or name, located in the bottom left corner.



HORIZONTAL

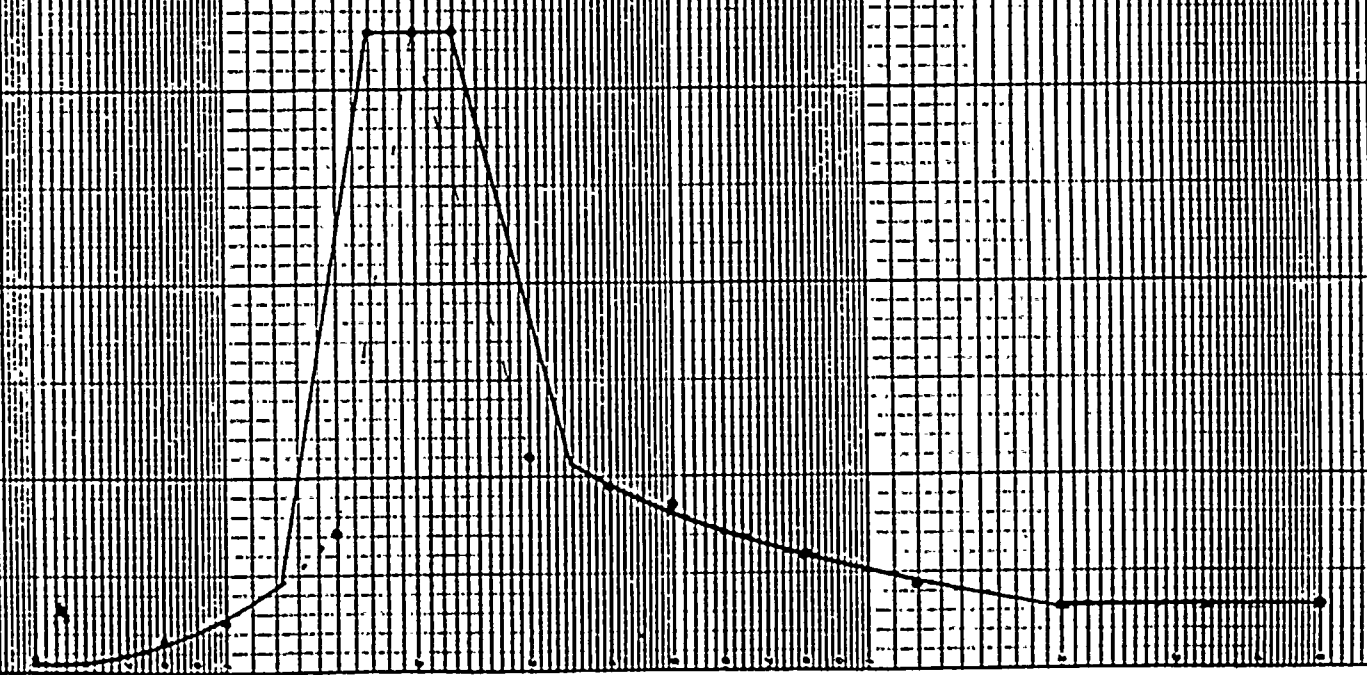
PROJECT 5364
 DC Book

.5% EQUIPMENT DAMPING
 2.9% STRUCTURAL DAMPING
 CONTAINMENT CRANE WALL
 ELEVATION 651'3"
 OBE ANALYSIS
 ± 15% PEAK SPREADING

by: DMD 1/8/83
 checked by: AMB 4/13/83

Points

f	g
.5	.09
1.0	.30
1.22	.45
1.7	.33
2.3	.33
3.45	1.05
5.0	.80
8.0	.60
15.0	.40
20.0	.32
50.0	.32



6-158

Frequency 100

8/1
The following information was obtained from the records of the
Department of the Interior, Bureau of Land Management, on
August 1, 1964.

100-100000



VERTICAL

5% EQUIPMENT DAMPING
 2% STRUCTURAL DAMPING
 CONTAINMENT BASE SLAB
 ELEVATION 597'6"
 OGE ANALYSIS
 ± 15% PEAK SPREADING

Project 5364
 DC Cook

by: SMD 1/18/83

checked by: JWB 2/18/83

Points

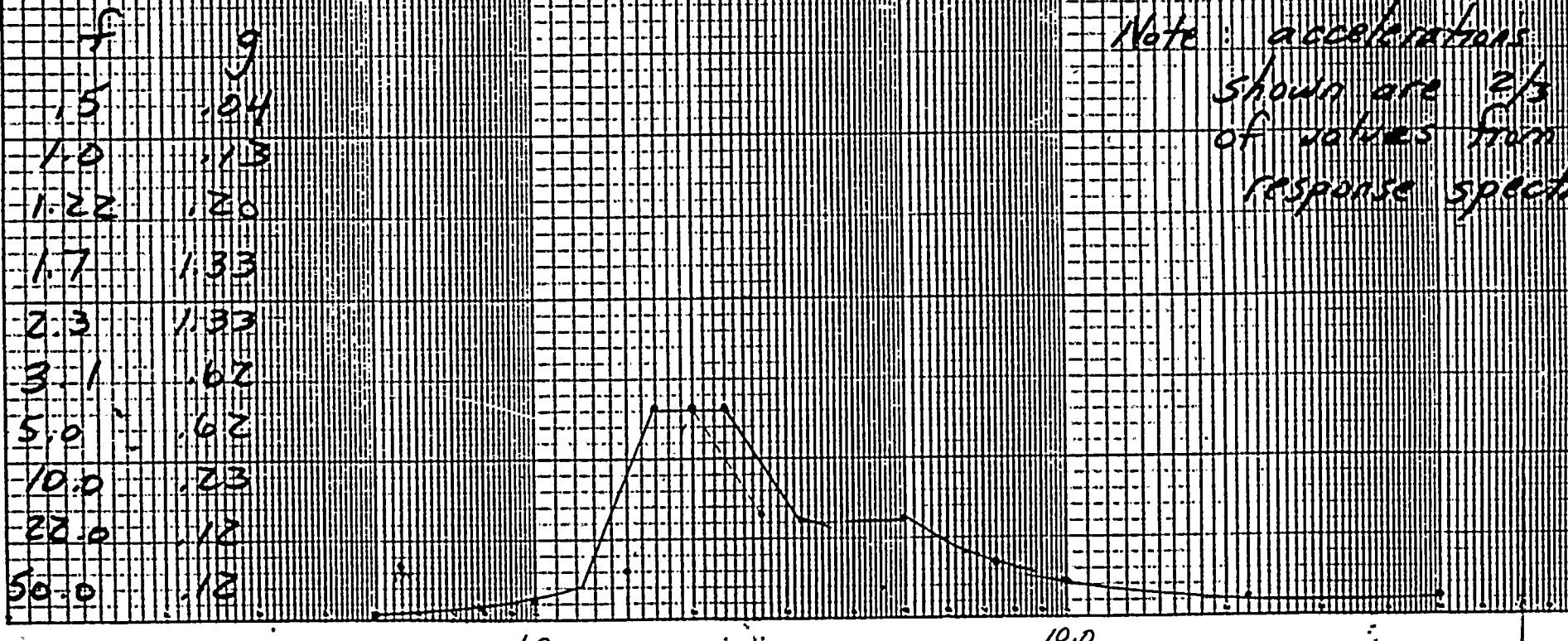
4

f	g
1.5	.04
1.0	.13
1.22	.20
1.7	.33
2.3	.33
3.1	.62
5.0	.62
10.0	.23
20.0	.12
50.0	.12

3

2

1



Note: accelerations shown are 2/3 of values from response spectra

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22



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 **TELEDYNE
ENGINEERING SERVICES**

6.6.3 DBE Spectra

BY SMD / DATE 4/11/83
CHKD. BY AME / DATE 4-12-83

RESPONSE SPECTRA

SHEET NO. 1 OF
PROJ. NO. 5364

DBE Analysis

per the attached figures, enveloping CONTAINMENT CRANE WALL ELEVATIONS 651.3, 663.3, 675.3 & 687.5 results in the following DBE horizontal spectra for both Units 1 & 2

<u>f</u>	<u>g</u>
.5	.19
1.0	.50
1.18	.70
1.7	5.2
2.3	5.2
3.15	2.6
3.65	1.46
6.0	1.40
7.0	1.15
10.0	1.0
17.0	.72
50.0	.72

VERTICAL

The vertical DBE response for Units 1 & 2, per the attached spectra, is:

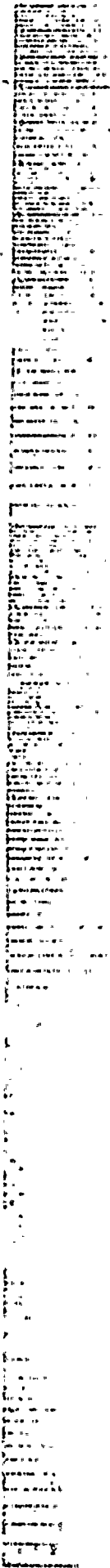
<u>f</u>	<u>g</u>
.5	.11
1.0	.25
1.18	.33
1.70	1.40
2.30	1.40
3.42	.80
6.00	.80
10.0	.43
15.0	.28
25.0	.20
50.0	.20

0.001

0.001

0.01

0.01



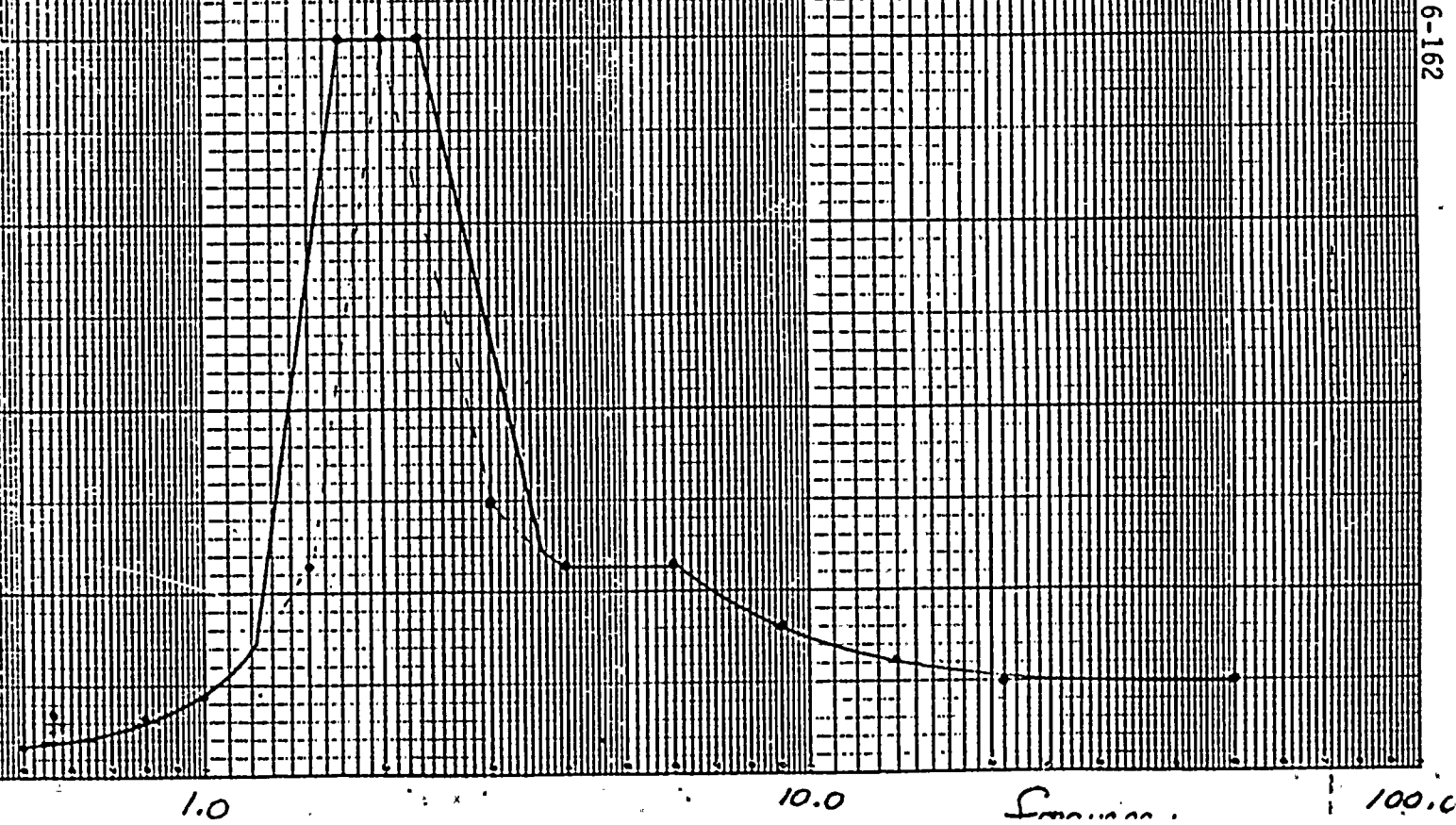
HORIZONTAL
 .5% EQUIPMENT DAMPING
 5% STRUCTURAL DAMPING
 CONTAINMENT CRANE WALL
 ELEVATION 651.3'
 NCE Analysis
 ±16% PEAK SPREADING

PROJECT 5364
 DC Cook

by: SWS #1/1/83
 checked by: SWS 4-13-83

Points

S	g
5	.17
1.0	.44
1.21	.72
1.70	4.0
2.30	4.0
3.60	1.22
4.00	1.75
6.0	1.15
9.0	.8
21.0	.5
50.0	.5



6-162

101

[Extremely faint and illegible text, possibly a list or index, spanning the left side of the page. The text is too light to transcribe accurately.]

5

2
2



HORIZONTAL
 5% EQUIPMENT DAMPING
 5% STRUCTURAL DAMPING
 CONTAINMENT CRANE WALL
 ELEVATION 663.3
 NBE Analysis
 ± 15% PEAK SPREADING

PROJECT 5364

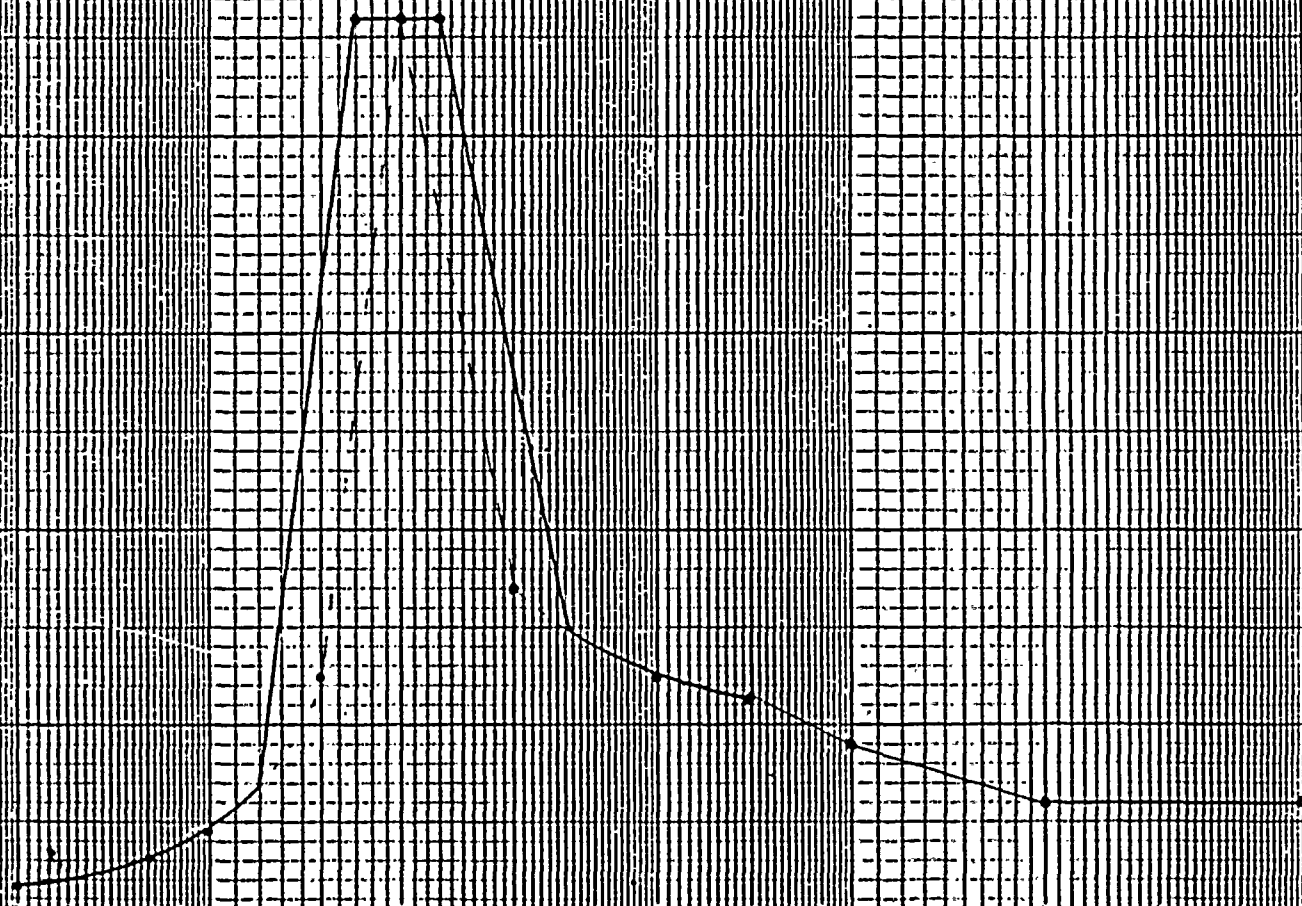
DC Cook

by: DMS 4/1/83

checked by: SWB 4-13-83

Points

F	Q
1.5	1.18
1.0	4.6
1.2	7.0
1.7	4.6
2.3	4.6
3.65	1.48
5.0	1.25
7.0	1.15
10.0	.90
20.0	.60
50.0	.60



1001

1001

1001

1001

Table with multiple columns and rows, containing dense text or data points. The table structure is highly repetitive and difficult to discern due to the quality of the scan. It appears to be a ledger or data record with several columns of varying widths and many rows of data.



HORIZONTAL
 5% EQUIPMENT DAMPING
 5% STRUCTURAL DAMPING
 CONTAINMENT CRANE WALL
 ELEVATION 675.3'

PROJECT 5364
 DC Cook

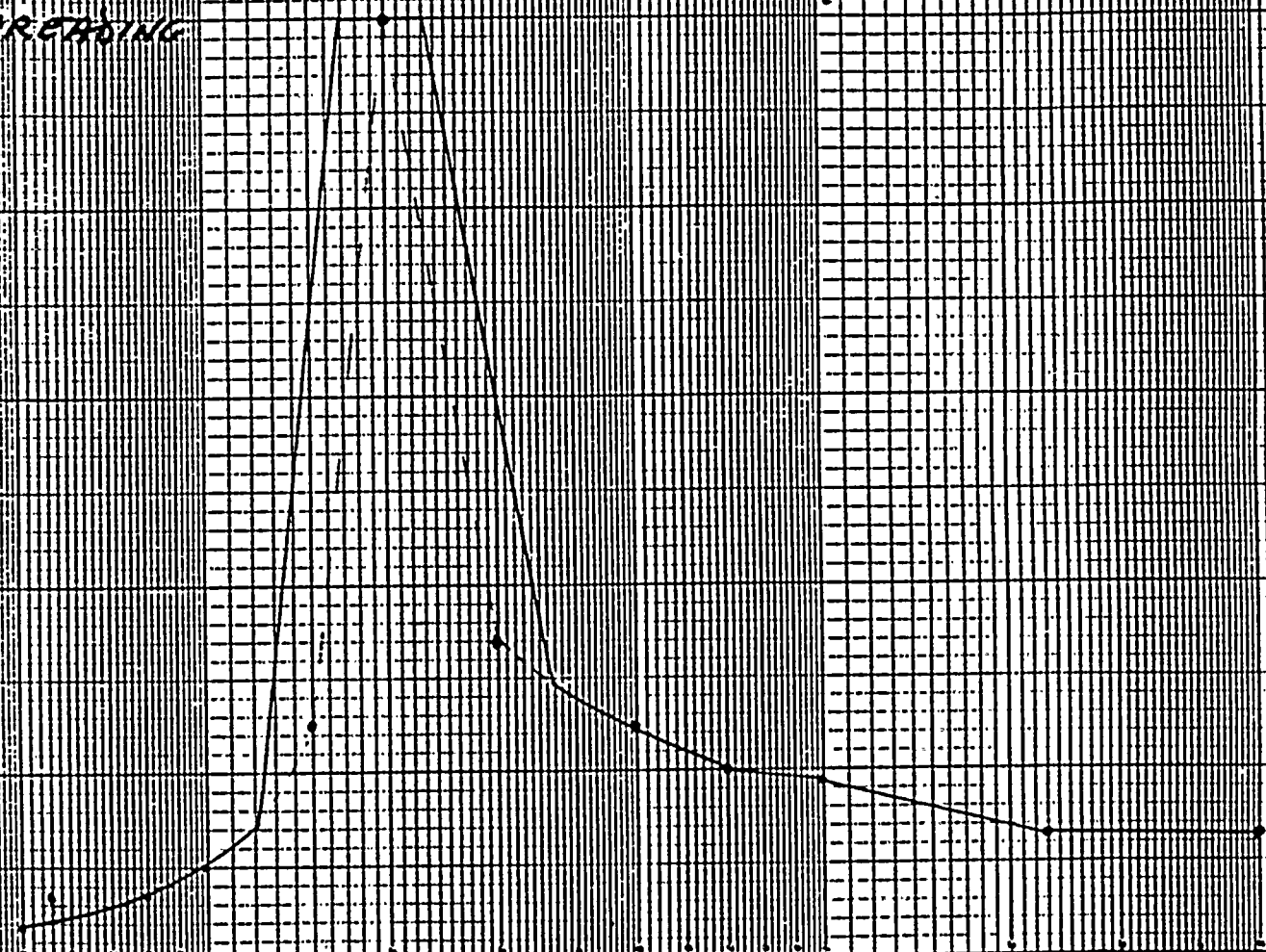
by: DMS 4/11/83

checked by: ~~DMS~~ 4-13-83

DBE ANALYSIS
 ± 15% PEAK SPREADING

Points

F	S
.5	.19
1.0	.50
1.21	.72
1.7	5.0
2.3	5.0
3.15	2.6
3.65	1.46
5.0	1.25
6.0	1.0
10.0	.95
23.0	.65
50.0	.65



6-164

1.0 10.0 Frequency 100.0

10001

3

1000

100

[The following text is extremely faint and largely illegible due to the quality of the scan. It appears to be a list or a series of entries, possibly containing names, dates, and other data points. The text is organized in a structured manner, likely a table or a list of records.]



HORIZONTAL
 .5% EQUIPMENT DAMPING
 .5% STRUCTURAL DAMPING
 CONTAINMENT CRANE WALL
 ELEVATION 687'-6"
 DBE ANALYSIS
 ± 15% PEAK SPREADING

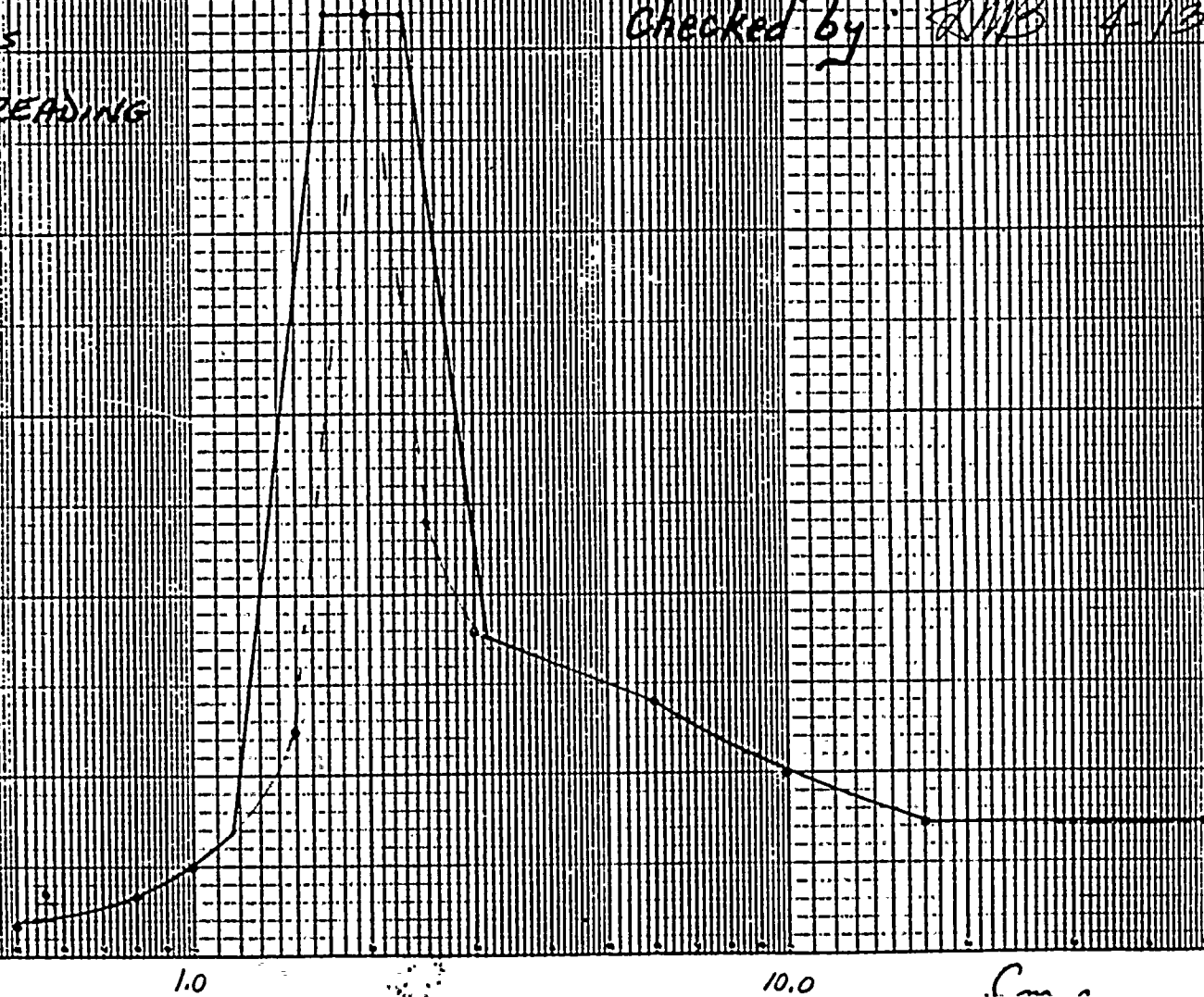
PROJECT 5364
 D C Cook

by DMD 4/11/83

checked by ~~DMD~~ 4-13-83

Points

freq	g
.5	.18
1.0	.50
1.18	.70
1.7	5.2
2.3	5.2
3.15	1.76
6.0	.74
10.0	1.0
17.0	.72
50.0	.72

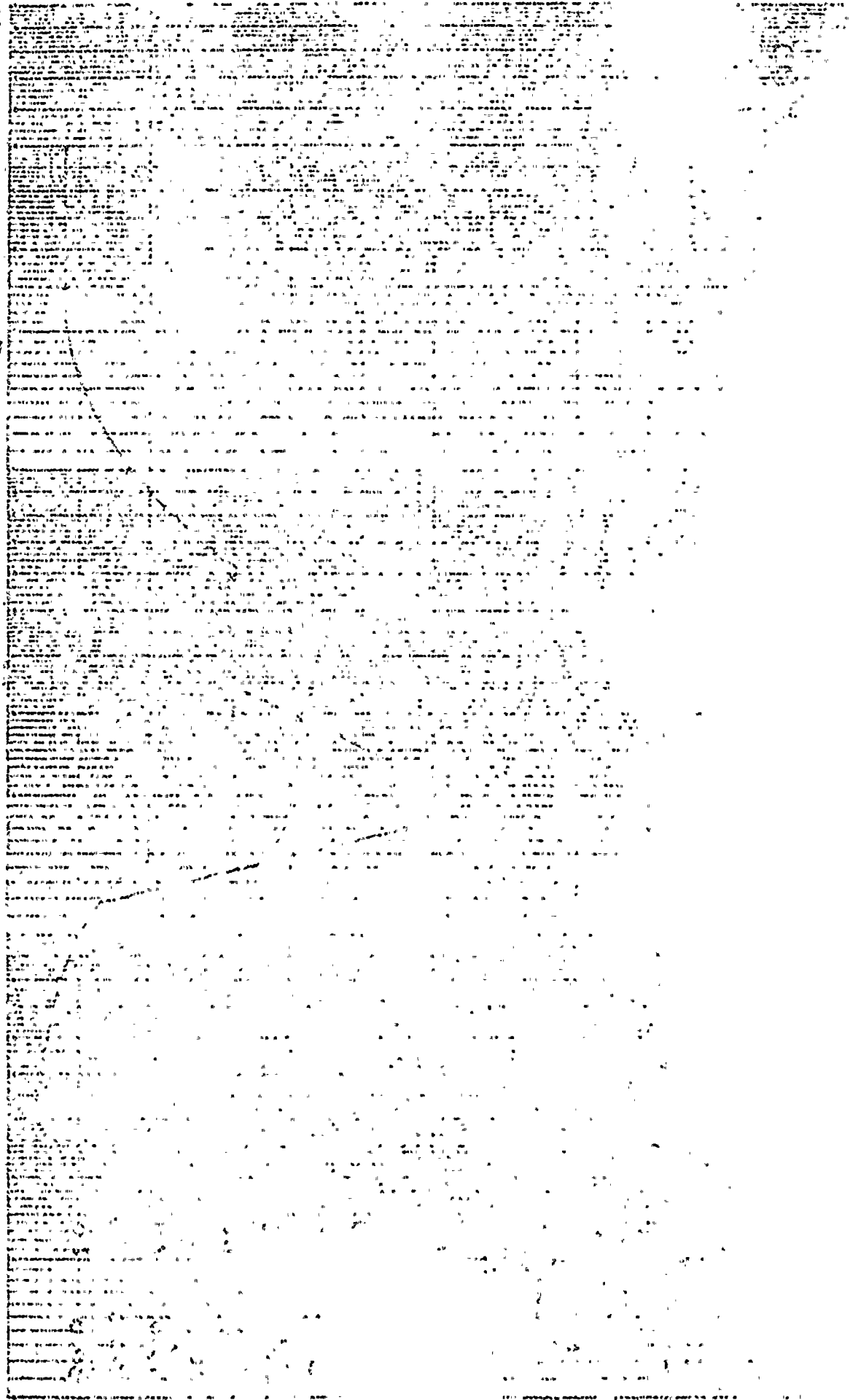


1001

2

0.0

1001



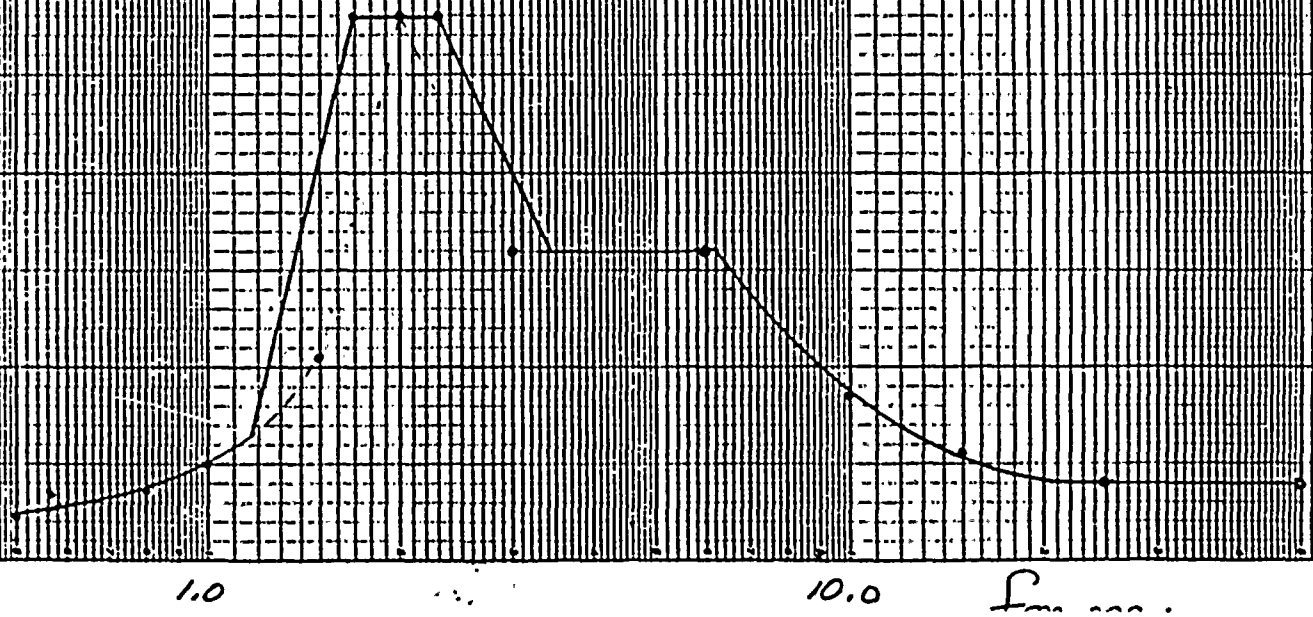
VERTICAL
 5% EQUIPMENT DAMPING
 5% STRUCTURAL DAMPING
 CONTAINMENT BASE SAG
 ELEVATION 597'-6"
 DBE Analysis
 ± 15% PEAK SPREADING

PROJECT 5364
 DC Cook

by DMB
 checked by: DMB 4-13-83

Points

f	g
.5	.11
1.0	.25
1.18	.33
1.70	.40
2.30	.40
3.42	.80
6.0	.80
10.0	.43
16.0	.28
25.0	.20
50.0	.20



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BAYCE ST.

2011

Technical Report
TR-5364-2
Revision 0

7-1

 **TELEDYNE
ENGINEERING SERVICES**

7.0 DRAWINGS

REPUBLICAN PARTY
STATE OF TEXAS

1. The first section of the constitution...

2. The second section of the constitution...

3. The third section of the constitution...

4. The fourth section of the constitution...

5. The fifth section of the constitution...

6. The sixth section of the constitution...

7. The seventh section of the constitution...

8. The eighth section of the constitution...

9. The ninth section of the constitution...

10. The tenth section of the constitution...

8.0 REFERENCES

1. Teledyne Engineering Services Technical Proposal PR-5653, dated May 14, 1981.
2. Letter from Mr. S. Ulan of AEP to Mr. L.B. Semprucci of TES, dated November 29, 1983.
3. Letter from Mr. S. Ulan of AEP to Mr. P. D. Harrison of TES, dated March 15, 1983.
4. RELAP5 MOD1 - Version 2.11 - A five equation Thermal-Hydrodynamic Analysis computer program including non-condensibles.
5. TMRPIPE - A system of Computer Programs for the Complete Analysis of Nuclear Piping.
6. TES Technical Report TR-5364-1, Donald C. Cook Nuclear Generating Station, "Analysis of Pressurizer Safety Valves/Relief Valves Discharge Piping Systems per NUREG 0737, II.D.1, Unit 1.
7. Letter from Mr. S. Ulan of AEP to Mr. P. D. Harrison of TES, dated May 26, 1983.
8. TES letter 5364-21, dated February 2, 1983 from Mr. P. D. Harrison of TES to Mr. Sam Ulan of AEP.
9. TES letter 5364-25, dated February 14, 1983 from Mr. P. D. Harrison of TES to Mr. Sam Ulan of AEP.
10. TES letter 5364-33, dated April 8, 1983 from Mr. P. D. Harrison of TES to Mr. Sam Ulan of AEP.

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8.0 REFERENCES (Continued)

11. 1967 Edition of USAS B31.1 Power Piping Code.
12. Letter from Mr. J. L. Williams of AEP to Mr. L. B. Semprucci of TES dated September 16, 1982.
13. Crosby Valve Drawing and Gage Company Drawing No. H-51688, Revision A.
14. Masoneilan International, Inc. Control Valve Model No. 38-20721, Drawing No. CP1-18-55, Revision H.
15. Westinghouse Electric Company, Drawing No. 110E272.
16. EPRI Safety and Relief Valve Test Report, Research Project V102 Interim Report, April 1982.
17. ASME Code NB7000, Section III.
18. ITI Report, "Evaluation of RELAP5/MOD1 for Calculation of Safety and Relief Valve Discharge Piping Hydrodynamic Loads," February 1982. Prepared by Intermountain Technologies.
19. Technical Paper #410 by Crane.

1007

1007 - 1007 831.1 Power Rating Table.

1008 - Mr. J. Williams of the U.S. Government, 1008
Number 1008.

1009 - Mr. J. Williams of the U.S. Government, 1009
Number 1009.

1010 - Mr. J. Williams of the U.S. Government, 1010
Number 1010.

1011 - Mr. J. Williams of the U.S. Government, 1011
Number 1011.

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DATE 6.13.86

TECHNICAL REPORT

TECHNICAL REPORT TR-5364-2
REVISION 0

BOOK 3 OF 10

DONALD C. COOK NUCLEAR GENERATING PLANT

ANALYSIS OF PRESSURIZER SAFETY/RELIEF VALVES
DISCHARGE PIPING SYSTEM PER NUREG 0737, I.L.D.1,
UNIT 2

8608060048

JUNE 10, 1983



12

AMERICAN ELECTRIC POWER SERVICE CORPORATION
2 BROADWAY
NEW YORK, NEW YORK 10004

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TECHNICAL REPORT TR-5364-2
REVISION 0

BOOK 3 OF 10

DONALD C. COOK NUCLEAR GENERATING STATION

ANALYSIS OF PRESSURIZER SAFETY/RELIEF VALVES
DISCHARGE PIPING SYSTEM PER NUREG 0737, II. D.1,
UNIT 2

JUNE 10, 1983

- Section 9.1.1 RELAP Input
 - 9.1.1.1 PORV Solid 400° Liquid
 - 9.1.1.2 PORV Solid 400° Liquid Restart
 - 9.1.1.3 SV Cold Loop Seal (Quarter Model)

- Section 9.1.2 REPIPE Input
 - 9.1.2.1 Unit 2 - Model Section A
 - 9.1.2.2 Unit 2 - Model Section B
 - 9.1.2.3 Unit 2 - Quarter Model

TELEDYNE ENGINEERING SERVICES

130 SECOND AVENUE
WALTHAM, MASSACHUSETTS 02254
617-890-3350

272



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GE-1
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23
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TELEDYNE ENGINEERING SERVICES

Section 9.1.1

RELAP Input

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9.1.1.1 PORV Solid 400 Liquid

28	308	HLGDW	303000000
22	303	HLGWN	303000000
24	306	HLGDW	811300000
23	302	HLGDW	811100000
25	304	HLGWT	300000000
21			



LISTING OF INPUT DATA FOR CASE 1

```

1  =AEP UNIT2 1 LINE RELAP5
2  *
3  *
4  *
5  *
6  *
7  *
8  *
9  *
10 *
11 *
12 *
13 *
14 *
15 *
16 *
17 *
18 *
19 *
20 * AEP D.C. COOK UNIT2
21 * DISCHARGE PIPING
22 * THIS IS THE NUMBERING SYSTEM FOR UNIT2S' RELAP MODEL
23 * WHERE COMPONENTS NUMBERED IN THE:
24 *   100'S ARE VALVE SV-45C AND ARC 1 LEVEL 669'-2"
25 *   200'S ARE VALVE SV-45B AND ARC 2 LEVEL 670'-10"
26 *   300'S ARE VALVE SV-45A AND ARC 3 LEVEL 672'-6"
27 *   400'S ARE PORV NRV-151 AND ARC "A"
28 *   500'S ARE PORV NRV-153 AND ARC "B"
29 *   600'S ARE PORV NRV-152 AND ARC "C"
30 *   700'S ARE 6" DISCHARGE PIPING
31 *   800'S ARE 12" DISCH.
32 *   900'S QUENCH TANK PORTION
33 *   999 ATMOSPHERE
34 100 NEW TRANSNT
35 101 RUN
36 102 BRITISH BRITISH
37 104 NOACTION
38 *
39 *
40 *   TIME STEP CONTROL
41 *
42 *
43 201 0.400 1.0-7 2.0-4 11001 5 50 250
44 *
45 *
46 *   MINOR EDITS
47 *
48 *
49 301 MFLOWJ 415000000
50 302 MFLOWJ 490000000
51 303 MFLOWJ 493000000
52 304 MFLOWJ 388000000
53 305 MFLOWJ 811140000
54 306 MFLOWJ 811790000
55 307 MFLOWJ 307000000
56 308 MFLOWJ 207000000
    
```

BY KJG DATE 5-17-83
 CHKD. BY cm DATE 6-2-83

W

THE UNIVERSITY OF MICHIGAN

1972

OFF
LIB
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SER
ALL



```

57 309 MFLOWJ 107000000
58 *
59 310 QUALS 400010000
60 311 QUALS 500010000
61 312 QUALS 600010000
62 313 QUALS 410210000
63 314 QUALS 485270000
64 315 QUALS 492110000
65 316 QUALS 389010000
66 317 QUALS 811140000
67 318 QUALS 811790000
68 319 QUALS 106010000
69 320 QUALS 106390000
70 321 QUALS 206010000
71 322 QUALS 206330000
72 323 QUALS 306010000
73 324 QUALS 306250000
74 *
75 325 P 400010000
76 326 P 500010000
77 327 P 600010000
78 328 P 410210000
79 329 P 485270000
80 330 P 492110000
81 331 P 389010000
82 332 P 811140000
83 333 P 811790000
84 334 P 106010000
85 335 P 106390000
86 336 P 206010000
87 337 P 206330000
88 338 P 306010000
89 339 P 306250000
90 *
91 *
92 *
93 *
94 *
95 *****
96 ** **
97 ** FORCE CARDS FOR REPIPE **
98 ** **
99 *****
100 *
101 * ***** ARC 2, ELEVATION 670' 10", SV-45B *****
102 *
103 2001 5, 151
104 2002 206010000, 206020000, 206030000, 206040000, 206050000
105 2003 206060000, 206070000, 206080000, 206090000, 206100000
106 2004 206110000, 206120000, 206130000, 206140000, 206150000
107 2005 206160000, 206170000, 206180000, 206190000, 206200000
108 2006 206210000, 206220000, 206230000, 206240000, 206250000
109 2007 206260000, 206270000, 206280000, 206290000, 206300000
110 2008 206310000, 206320000, 206330000
111 *
112 *
113 *
114 *

```

```

115 *      **** FIRST C.V. DOWNSTREAM OF THE ARC      ****
116 *
117 *
118 2010      805010000
119 *
120 *
121 *
122 *
123 *      ***** 12 INCH DISCHARGE DOWN TO THE QUENCH TANK *****
124 *
125 *
126 2020      811190000,811200000,811210000,811220000,811230000
127 2021      811240000,811250000,811260000,811270000,811280000
128 2022      811290000,811300000,811310000,811320000,811330000
129 2023      811340000,811350000,811360000,811370000,811380000
130 2024      811390000,811400000,811410000,811420000,811430000
131 2025      811440000,811450000,811460000,811470000,811480000
132 2026      811490000,811500000,811510000,811520000,811530000
133 2027      811540000,811550000,811560000,811570000,811580000
134 2028      811590000,811600000,811610000,811620000,811630000
135 2029      811640000,811650000,811660000,811670000,811680000
136 2030      811690000,811700000,811710000,811720000,811730000
137 2031      811740000,811750000,811760000,811770000,811780000
138 2032      811790000,811800000,811810000,811820000,811830000
139 2033      811840000,811850000,811860000,811870000,811880000
140 2034      811890000,811900000,811910000,811920000,811930000
141 2035      811940000,811950000,811960000,811970000,811980000
142 2036      811990000,811180000
143 *
144 2040      813010000,813020000,813030000,813040000,813050000
145 2041      813060000,813070000,813080000,813090000,813100000
146 2042      813110000,813120000,813130000,813140000,813150000
147 2043      813160000,813170000,813180000,813190000,813200000
148 2044      813210000,813220000,813230000,813240000,813250000
149 2045      813260000,813270000,813280000,813290000,813300000
150 *
151 *
152 *
153 *      ***** PIPE DOWN INTO THE QUENCH TANK      ****
154 *
155 *
156 2050      901010000,901020000,903010000,903020000
157 2051      903030000
158 *
159 *
160 *
161 *
162 *
163 *
164 *
165 *
166 *
167 *      ***** PIPING UPSTREAM OF PORV NRV - 153 *****
168 *
169 *
170 *
171 *
172 *

```


835
834
833

388001
388000
388000

0.0 0.0 1
0.0 0.0 0.0

00000000
00000000
00000000

0.0 0.0 0.0 0.0 1000
0.0 0.0 0.0 0.0 1000

3

```

173 *
174 *
175 *
176 *
177 *
178 *****
179 *          TRIPS
180 *****
181 *
182 501 P 907010000 GT NULL 0 114.7 L *QUENCH TANK BLOW OUT PATCH
183 502 TIME 0 GT NULL 0 1.5 L * JOB TERMINATION TRIP
184 503 TIME 0 GE NULL 0 0.0 L * VALVE OPEN
185 504 TIME 0 GE NULL 0 5.0 L * VALVE CLOSED
186 600 502
187 *
188 *****
189 *          *****
190 *          * HYDRODYNAMIC COMPONENTS *
191 *          *****
192 *****
193 *
194 3850000 "PRESS4" TMDPVOL
195 3850101 0.0 20.0 500.0 0.0 0.0 0.0 0.00005 0.0 11
196 3850200 3
197 3850201 0.0 2349.7 400.0 0.8 2420.0 400.0 1.2 2498.7 400.0
198 *
199 *          *****
200 *          * PORV UPSTREAM PIPING *
201 *          *****
202 *
203 *
204 3860000 "NOZ" SNGLJUN
205 3860101 385000000 387000000 0.0 0.0 0.0 1100
206 3860201 1 0.0 0.0 0.0
207 *
208 *          6 INCH SCH. 160 PIPE
209 *
210 3870000 "PORVU" PIPE
211 3870001 12
212 3870101 0.14653 12
213 3870301 0.328 1
214 3870302 0.5227 12
215 3870401 0.0 12
216 3870601 42.733 1
217 3870602 90.0 12
218 3870801 0.000151 0.0 12
219 3870901 0.0964 0.0964 1
220 3870902 0.0 0.0 11
221 3871001 00 12
222 3871101 1000 11
223 3871201 3 2349.7 400.0 0.0 0.0 12
224 3871300 1
225 3871301 0.0 0.0 0.0 11
226 *
227 3880000 "PORVU" SNGLJUN
228 3880101 387010000 389000000 0.0 0.0 0.0 1000
229 3880201 1 0.0 0.0 0.0
230 *

```

588 432001 0 2884 3
581 43201 0 14 2
582 432001 10000 2
583 432001 10000 2

```

231 * 6 X 6 X 3 INCH REDUCING TEE
232 *
233 3890000 "PORVU" BRANCH
234 3890001 0
235 3890101 0.14653 0.25 0.0 0.0 90.0 0.25 0.000151 0.0 00
236 3890200 3 2349.7 400.0 0.0 0.0 0.0
237 *
238 4980000 "PORVU" SNGLJUN
239 4980101 389010000 410000000 0.0 0.1836 0.1836 1000
240 4980201 1 0.0 0.0 0.0
241 *
242 * 3 INCH SCH. 160 PIPING
243 *
244 4100000 "PORV" PIPE
245 4100001 21
246 4100101 0.03757 17
247 4100102 0.03387 18
248 4100103 0.0265 19
249 4100104 0.01912 20
250 4100105 0.01175 21
251 4100301 0.5 5
252 4100302 0.5278 11
253 4100303 0.5313 17
254 4100304 0.2657 21
255 4100401 0.0 21
256 4100601 0.0 5
257 4100602 90.0 11
258 4100603 0.0 21
259 4100801 0.000153 0.0 21
260 4100901 0.0 0.0 4
261 4100902 0.2172 0.2172 5
262 4100903 0.0 0.0 10
263 4100904 0.2172 0.2172 11
264 4100905 0.0 0.0 20
265 4101001 00 21
266 4101101 1000 20
267 4101201 3 2349.7 400.0 0.0 0.0 21
268 4101300 1
269 4101301 0.0 0.0 0.0 20
270 *
271 * PORV VALVE NRV - 153
272 *
273 4150000 "PORV153" VALVE
274 4150101 410010000 500000000 0.00806 0.0 0.0 0100
275 4150201 1 0.0 0.0 0.0
276 4150300 MTRVLV
277 4150301 503 504 1.0 0.0
278 *
279 4200000 "PORV" SNGLJUN
280 4200101 389010000 425000000 0.0 0.0 0.0 1000
281 4200201 1 0.0 0.0 0.0
282 *
283 * 6 INCH SCH. 160 PIPING
284 *
285 4250000 "PORV" PIPE
286 4250001 5
287 4250101 0.1465 5
288 4250301 0.3889 3

```

348 4421001 49 12
342 4420904 0 144 4 1275 8
344 4420803 0.0 1.0 2
341

289	4250302	0.375	5						
290	4250401	0.0	5						
291	4250601	90.0	3						
292	4250602	0.0	5						
293	4250801	0.000151	0.0	5					
294	4250901	0.0	0.0	2					
295	4250902	0.1836	0.1836	3					
296	4250903	0.0	0.0	4					
297	4251001	00	5						
298	4251101	1000	4						
299	4251201	3	2349.7	400.0	0.0	0.0	5		
300	4251300	1							
301	4251301	0.0	0.0	0.0	4				
302	*								
303	4300000	"PORV"	SNGLJUN						
304	4300101	425010000	435000000	0.0	0.0	0.0	1000		
305	4300201	1	0.0	0.0	0.0				
306	*								
307	*	6 INCH	X 4 INCH	REDUCER					
308	*								
309	4350000	"PORV"	PIPE						
310	4350001	2							
311	4350101	0.1465	1						
312	4350102	0.0716	2						
313	4350301	0.2292	2						
314	4350401	0.0	2						
315	4350601	0.0	2						
316	4350801	0.000151	0.0	1					
317	4350802	0.000133	0.0	2					
318	4350901	0.0577	0.0961	1					
319	4351001	00	2						
320	4351101	1000	1						
321	4351201	3	2349.7	400.0	0.0	0.0	2		
322	4351300	1							
323	4351301	0.0	0.0	0.0	1				
324	*								
325	*								
326	4400000	"PORV"	SNGLJUN						
327	4400101	435010000	445000000	0.0	0.0	0.0	1000		
328	4400201	1	0.0	0.0	0.0				
329	*								
330	*	4 INCH	SCH. 120	PIPING					
331	*								
332	4450000	"PORV"	PIPE						
333	4450001	10							
334	4450101	0.0716	10						
335	4450301	0.35833	5						
336	4450302	0.5	10						
337	4450401	0.0	10						
338	4450601	0.0	5						
339	4450602	90.0	9						
340	4450603	0.0	10						
341	4450801	0.000133	0.0	10					
342	4450901	0.0	0.0	4					
343	4450902	0.1944	0.1944	5					
344	4450903	0.0	0.0	8					
345	4450904	0.1944	0.1944	9					
346	4451001	00	10						

```

347 4451101 1000 9
348 4451201 3 2349.7 400.0 0.0 0.0 10
349 4451300 1
350 4451301 0.0 0.0 0.0 9
351 *
352 4500000 "PORV" SNGLJUN
353 4500101 445010000 455000000 0.0 0.0 0.0 1000
354 4500201 1 0.0 0.0 0.0
355 *
356 * 4 X 4 X 3 INCH REDUCING BRANCH
357 *
358 4550000 "PORV" BRANCH
359 4550001 0
360 4550101 0.0716 0.5 0.0 0.0 0.0 0.0 0.000133 0.0 00
361 4550200 3 2349.7 400.0 0.0 0.0 0.0
362 *
363 4600000 "PORV" SNGLJUN
364 4600101 455010000 465000000 0.0 0.0 0.0 1000
365 4600201 1 0.0 0.0 0.0
366 *
367 * 4 INCH SCH. 120 PIPING
368 *
369 4650000 "PORV" PIPE
370 4650001 3
371 4650101 0.0716 3
372 4650301 0.25 3
373 4650401 0.0 3
374 4650601 0.0 3
375 4650801 0.000133 0.0 3
376 4650901 0.0 0.0 2
377 4651001 00 3
378 4651101 1000 2
379 4651201 3 2349.7 400.0 0.0 0.0 3
380 4651300 1
381 4651301 0.0 0.0 0.0 2
382 *
383 4700000 "PORV" SNGLJUN
384 4700101 465010000 475000000 0.0 0.0 0.0 1000
385 4700201 1 0.0 0.0 0.0
386 *
387 * 4 INCH X 3 INCH REDUCER
388 *
389 4750000 "PORV" PIPE
390 4750001 2
391 4750101 0.0716 1
392 4750102 0.0378 2
393 4750301 0.1667 2
394 4750401 0.0 2
395 4750601 0.0 2
396 4750801 0.000133 0.0 1
397 4750802 0.000153 0.0 2
398 4750901 0.0472 0.0730 1
399 4751001 00 2
400 4751101 1000 1
401 4751201 3 2349.7 400.0 0.0 0.0 2
402 4751301 0.0 0.0 0.0 1
403 *
404 4800000 "PORV" SNGLJUN

```

403 402 :
404 401 :
405 400 :
406 399 :




```

405 4800101 475010000 485000000 0.0 0.0 0.0 1000
406 4800201 1 0.0 0.0 0.0
407 *
408 * 3 INCH SCH. 160 PIPING
409 *
410 4850000 "PORV" PIPE
411 4850001 27
412 4850101 0.0376 23
413 4850102 0.0339 24
414 4850103 0.0266 25
415 4850104 0.0192 26
416 4850105 0.0118 27
417 4850301 0.4375 4
418 4850302 0.4690 12
419 4850303 0.500 15
420 4850304 0.368 16
421 4850305 0.367 17
422 4850306 0.5405 23
423 4850307 0.41937 27
424 4850401 0.0 27
425 4850601 0.0 27
426 4850801 0.000153 0.0 27
427 4850901 0.0 0.0 26
428 4851001 00 27
429 4851101 1000 26
430 4851201 3 2349.7 400.0 0.0 0.0 27
431 4851300 1
432 4851301 0.0 0.0 0.0 26
433 *
434 * PORV VALVE NRV - 151
435 *
436 4900000 "PORV" VALVE
437 4900101 485010000 400000000 0.00806 0.0 0.0 0100
438 4900201 1 0.0 0.0 0.0
439 4900300 MTRVLV
440 4900301 503 504 1.0 0.0
441 *
442 4910000 "PORV" SNGLJUN
443 4910101 455010000 492000000 0.0 0.095 0.095 1000
444 4910201 1 0.0 0.0 0.0
445 *
446 * 3 INCH SCH. 160 PIPING
447 *
448 4920000 "PORV" PIPE
449 4920001 11
450 4920101 0.0376 7
451 4920102 0.0339 8
452 4920103 0.0266 9
453 4920104 0.0192 10
454 4920105 0.0118 11
455 4920301 0.4881 7
456 4920302 0.4792 11
457 4920401 0.0 11
458 4920601 0.0 11
459 4920801 0.000153 0.0 11
460 4920901 0.0 0.0 10
461 4921001 00 11
462 4921101 1000 10

```

```

463 4921201 3 2349.7 400.0 0.0 0.0 11
464 4921300 1
465 4921301 0.0 0.0 0.0 10
466 *
467 * PORV VALVE NRV - 152
468 *
469 4930000 "PORV" VALVE
470 4930101 492010000 600000000 0.00806 0.0 0.0 0100
471 4930201 1 0.0 0.0 0.0
472 4930300 MTRVLV
473 4930301 503 504 1.0 0.0
474 *
475 *
476 *****
477 * SAFETY VALVES DISCHARGE SECTION *
478 *****
479 *
480 *
481 *
482 *****
483 * SAFETY VALVE-45C DISCHARGING AT ELÉV. 669'-2" ARC 1 *
484 *****
485 *
486 *
487 **
488 * DISCHARGE PIPING
489 *
490 * 6 INCH SCH. 40 PIPING
491 **
492 1060000 "DISCHA1" PIPE
493 1060001 39
494 1060101 0.20069 39
495 1060301 0.526 4
496 1060302 1.094 14
497 * ARC STARTS HERE LEVEL 669-2"
498 1060303 1.000 20
499 1060304 0.8994 29
500 1060305 0.7436 35
501 * ARC ENDS
502 1060306 0.7980 39
503 1060401 0.0 39
504 1060601 0.0 4
505 1060602 -90.0 14
506 1060603 0.0 39
507 1060801 0.000152 0.0 39
508 1060901 0.0 0.0 3
509 1060902 0.1800 0.1800 4
510 1060903 0.0 0.0 13
511 1060904 0.1800 0.1800 14
512 1060905 0.0 0.0 38
513 1061001 00 39
514 1061101 1000 38
515 1061201 4 17.7 120.0 0.9284 0.0 39
516 1061300 1
517 1061301 0.0 0.0 0.0 38
518 *
519 1070000 "DISCHA1" SNGLJUN
520 1070101 106010000 809000000 0.0 0.1560 0.1560 1000 *LOSSES FOR A 12 IN ELBOW

```



212 5.

```

521 1070201 1 0.0 0.0 0.0
522 *
523 *
524 *
525 *****
526 *      MAIN DISCHARGE 12" HEADER TO QUENCH TANK      *
527 *****
528 *
529 *
530 *      12 X 12 X 6 INCH REDUCING TEE
531 *
532 *      CONNECTS SRV PIPING TO MAIN DISCHARGE
533 *
534 *
535 8090000 "DISCHA1" BRANCH
536 8090001 0
537 8090101 0.77708 0.5 0.0 0.0 -90.0 -0.5 0.000169 0.0 00
538 8090200 4 17.7 120.0 0.9284
539 *
540 8100000 "DISCHA1" SNGLJUN
541 8100101 809010000 811000000 0.0 0.0 0.0 1000
542 8100201 1 0.0 0.0 0.0
543 *
544 *      12 INCH SCH. 40 DISCHARGE PIPING
545 *
546 8110000 "DISCHA1" PIPE
547 8110001 99
548 8110101 0.7771 99
549 8110301 1.039 14
550 8110302 0.53025 18
551 8110303 0.5 22
552 8110304 0.53025 26
553 8110305 0.9875 56
554 8110306 0.475 66
555 8110307 0.49359 79
556 8110308 0.46875 87
557 8110309 0.50 95
558 8110310 0.875 99
559 8110401 0.0 99
560 8110601 -90.0 14
561 8110602 -45.0 18
562 8110603 -90.0 22
563 8110604 -45.0 26
564 8110605 -90.0 56
565 8110606 0.0 87
566 8110607 -90.0 95
567 8110608 0.0 99
568 8110801 0.000169 0.0 99
569 8110901 0.0 0.0 13
570 8110902 0.078 0.078 14
571 8110903 0.0 0.0 17
572 8110904 0.078 0.078 18
573 8110905 0.0 0.0 21
574 8110906 0.078 0.078 22
575 8110907 0.0 0.0 25
576 8110908 0.078 0.078 28
577 8110909 0.0 0.0 55
578 8110910 0.158 0.158 56

```

```

579 8110911 0.0 0.0 65
580 8110912 0.026 0.026 66
581 8110913 0.0 0.0 78
582 8110914 0.13 0.13 79
583 8110915 0.0 0.0 86
584 8110916 0.156 0.156 87
585 8110917 0.0 0.0 94
586 8110918 0.156 0.156 95
587 8110919 0.0 0.0 98
588 8111001 00 99
589 8111101 1000 98
590 8111201 4 17.7 120.0 0.9284 0.0 99
591 8111300 1
592 8111301 0.0 0.0 0.0 98
593 *
594 8120000 "DISCHA1" SNGLJUN
595 8120101 811010000 813000000 0.0 0.0 0.0 1000
596 8120201 1 0.0 0.0 0.0
597 *
598 * 12 INCH SCH. 40 DISCHARGE PIPING
599 *
600 8130000 "DISCHA1" PIPE
601 8130001 30
602 8130101 0.7771 30
603 8130301 0.875 6
604 8130302 1.0 20
605 8130303 0.5 30
606 8130401 0.0 30
607 8130601 0.0 30
608 8130801 0.000169 0.0 30
609 8130901 0.0 0.0 5
610 8130902 0.156 0.156 6
611 8130903 0.0 0.0 19
612 8130904 0.156 0.156 20
613 8130905 0.0 0.0 29
614 8131001 00 30
615 8131101 1000 29
616 8131201 4 17.7 120.0 0.9284 0.0 30
617 8131300 1
618 8131301 0.0 0.0 0.0 29
619 *
620 *
621 *
622 *****
623 * SAFETY VALVE 45B AT ELEV. 670'-10" ARC 2 *
624 *****
625 *
626 *
627 *
628 **
629 * DISCHARGE PIPING
630 *
631 * 6 INCH SCH. 40 PIPING
632 **
633 2060000 "DISCHA2" PIPE
634 2060001 33
635 2060101 0.20069 33
636 2060301 0.4635 4

```

```

637 2060302 0.927 14
638 *ARC STARTS LEVEL 670'-10"
639 2060303 0.955 23
640 2060304 0.727 29
641 2060308 0.7980 33
642 2060401 0.0 33
643 2060601 0.0 4
644 2060602 -90. 14
645 2060603 0.0 33
646 2060801 0.000152 0.0 33
647 2060901 0.0 0.0 3
648 2060902 0.1800 0.1800 4
649 2060903 0.0 0.0 13
650 2060904 0.1800 0.1800 14
651 2060905 0.0 0.0 32
652 2061001 00 33
653 2061101 1000 32
654 2061201 4 17.7 120.0 0.9284 0.0 33
655 2061300 1
656 2061301 0.0 0.0 0.0 32
657 *
658 *****
659 * SAFETY VALVE 45A AT ELEV. 672'-6" ARC. 3 *
660 *****
661 *
662 *
663 *
664 **
665 * DISCHARGE PIPING
666 *
667 * 6 INCH SCH. 40 PIPING
668 **
669 3060000 "DISCHA3" PIPE
670 3060001 25
671 3060101 0.20069 25
672 3060301 0.526 4
673 3060302 0.969 12
674 * ARC STARTS LEVEL 672'-6"
675 3060303 0.635 15
676 3060304 0.991 18
677 3060305 0.991 21
678 3060306 0.799 25
679 * ARC ENDS
680 3060401 0.0 25
681 3060601 0.0 4
682 3060602 -90.0 12
683 3060603 0.0 25
684 3060801 0.000152 0.0 25
685 3060901 0.0 0.0 3
686 3060902 0.1800 0.1800 4
687 3060903 0.0 0.0 11
688 3060904 0.1800 0.1800 12
689 3060905 0.0 0.0 24
690 3061001 00 25
691 3061101 1000 24
692 3061201 4 17.7 120.0 0.9284 0.0 25
693 3061300 1
694 3061301 0.0 0.0 0.0 24

```

```

695 *
698 *
697 *
698 *
699 *****
700 *      PORV PIPING      *
701 *****
702 *
703 *
704 *      PIPING DOWNSTREAM OF VALVE NRV - 153
705 *
706 *      3 INCH SCH. 40 PIPING
707 *
708 *
709 5000000 "PORVB" PIPE
710 5000001 16
711 5000101 0.05132 16 * 3 IN SCH40S
712 5000301 0.497 3
713 5000302 0.556 6
714 *      ARC STARTS LEVEL 684'-9"
715 5000303 0.365 7 *
716 5000304 0.6448 13
717 5000305 0.5892 16
718 5000401 0.0 16
719 5000601 0.0 3
720 5000602 -90.0 6
721 5000603 0.0 16
722 5000801 0.000153 0.0 16
723 5000901 0.0 0.0 2
724 5000902 0.2088 0.2088 3
725 5000903 0.0 0.0 5
726 5000904 0.2088 0.2088 6
727 5000905 0.0 0.0 15
728 5001001 00 16
729 5001101 1000 15
730 5001201 4 17.7 120.0 0.9284 0.0 16
731 5001300 1
732 5001301 0.0 0.0 0.0 15
733 *
734 5010000 "PORVB" SNGLJUN * THIS JUNCTION IS ON ARC B
735 5010101 500010000 502000000 0.0 0.0 0.0 1000
736 5010201 1 0.0 0.0 0.0
737 *
738 *      4 INCH X 3 INCH DIFFUSER
739 *
740 5020000 "PORVB" PIPE * REDUCER ON ARC B 3IN X4IN
741 5020001 2
742 5020101 0.05132 1 * 3IN SCH40S
743 5020102 0.08840 2 * 4IN SCH40S
744 5020301 0.3385 2
745 5020401 0.0 2
746 5020601 0.0 2
747 5020801 0.000153 0.0 1
748 5020802 0.000134 0.0 2
749 5020901 0.0399 0.0544 1
750 5021001 00 2
751 5021101 1000 1
752 5021201 4 17.7 120.0 0.9284 0.0 2

```

```

753 5021300 1
754 5021301 0.0 0.0 0.0 1
755 *
756 *
757 5030000 "PORVB" SNGLJUN * ON ARC B
758 5030101 502010000 504000000 0.0 0.0 0.0 1000
759 5030201 1 0.0 0.0 0.0
760 *
761 * 4 X 4 X 3 INCH BRANCH
762 *
763 5040000 "PORVB" BRANCH * ON ARC B @ 242
764 5040001 0
765 5040101 0.0884 0.361 0.0 0.0 0.0 0.0 0.000134 0.0 00
766 5040200 4 17.7 120.0 0.9284 0.0 0.0
767 *
768 5050000 "PORVB" SNGLJUN * ON ARC B
769 5050101 504010000 506000000 0.0 0.0 0.0 1000
770 5050201 1 0.0 0.0 0.0
771 *
772 * 4 INCH SCH. 40 PIPING
773 *
774 5060000 "PORVB" PIPE * ON ARC B
775 5060001 9
776 5060101 0.0884 9
777 5060301 0.6211 8
778 5060302 0.7607 9
779 5060401 0.0 9
780 5060601 0.0 9
781 5060801 0.000134 0.0 9
782 5060901 0.0 0.0 8
783 5061001 00 9
784 5061101 1000 8
785 5061201 4 17.7 120.0 0.9284 0.0 9
786 5061300 1
787 5061301 0.0 0.0 0.0 8
788 *
789 5070000 "PORVB" SNGLJUN
790 5070101 506010000 508000000 0.0 0.0 0.0 1000
791 5070201 1 0.0 0.0 0.0
792 *
793 * 4 INCH X 6 INCH DIFFUSER
794 *
795 5080000 "PORVB" PIPE
796 5080001 2
797 5080101 0.0884 1
798 5080102 0.20069 2
799 5080301 0.5792 2
800 5080401 0.0 2
801 5080601 0.0 2
802 5080801 0.000134 0.0 1
803 5080802 0.000152 0.0 2
804 5080901 0.1483 0.0815 1
805 5081001 00 2
806 5081101 1000 1
807 5081201 4 17.7 120.0 0.9284 0.0 2
808 5081300 1
809 5081301 0.0 0.0 0.0 1
810 *
    
```



```

811 5090000 "PORVB" SNGLJUN * ON ARC B
812 5090101 508010000 510000000 0.0 0.0 0.0 1000
813 5090201 1 0.0 0.0 0.0
814 *
815 * 6 X 6 X 3 INCH REDUCING TEE
816 *
817 5100000 "PORVB" BRANCH * ON ARC B @ 232
818 5100001 0
819 5100101 0.20069 0.25 0.0 0.0 0.0 0.0 0.000152 0.0 00
820 5100200 4 17.7 120.0 0.9284 0.0 0.0
821 *
822 5110000 "PORVB" SNGLJUN * ON ARC B
823 5110101 510010000 700000000 0.0 0.0 0.0 1000
824 5110201 1 0.0 0.0 0.0
825 *
826 * PIPING DOWNSTREAM OF VALVE NRV - 151
827 *
828 * 3 INCH SCH. 40 PIPING
829 *
830 4000000 "PORVA" PIPE
831 4000001 8
832 4000101 0.05132 8
833 4000301 0.4141 4
834 4000302 0.4375 8
835 4000401 0.0 8
836 4000601 0.0 4
837 4000602 -90.0 8
838 4000801 0.000153 0.0 8
839 4000901 0.0 0.0 3
840 4000902 0.2088 0.2088 4
841 4000903 0.0 0.0 7
842 4001001 00 8
843 4001101 1000 7
844 4001201 4 17.7 120.0 0.9284 0.0 8
845 4001300 1
846 4001301 0.0 0.0 0.0 7
847 *
848 4010000 "PORVAB" SNGLJUN
849 4010101 400010000 510000000 0.0 0.1800 0.1800 1000
850 4010201 1 0.0 0.0 0.0
851 *
852 * DOWNSTREAM PIPING FROM VALVE NRV - 152
853 *
854 * 3 INCH SCH. 40 PIPING
855 *
856 6000000 "PORVC" PIPE
857 6000001 7
858 6000101 0.05132 7
859 6000301 0.4722 3
860 6000302 0.4375 7
861 6000401 0.0 7
862 6000601 0.0 3
863 6000602 -90.0 7
864 6000801 0.000153 0.0 7
865 6000901 0.0 0.0 2
866 6000902 0.2088 0.2088 3
867 6000903 0.0 0.0 8
868 6001001 00 7

```

```

869 6001101 1000 6
870 6001201 4 17.7 120.0 0.9284 0.0 7
871 6001300 1
872 6001301 0.0 0.0 0.0 6
873 *
874 6010000 "PORVBC" SNGLJUN
875 6010101 600010000 504000000 0.0 0.1932 0.1932 1000
876 6010201 1 0.0 0.0 0.0
877 *
878 * MAIN HEADER DOWNSTREAM OF PORV PIPING
879 *
880 7000000 "PORVBD" PIPE
881 7000001 12
882 7000101 0.20069 12
883 7000301 0.75 2
884 7000302 1.075 12
885 7000401 0.0 12
886 7000601 0.0 2
887 7000602 -90. 12
888 7000801 0.000152 0.0 12
889 7000901 0.0 0.0 1
890 7000902 0.1800 0.1800 2
891 7000903 0.0 0.0 11
892 7001001 00 12
893 7001101 1000 11
894 7001201 4 17.7 120.0 0.9284 0.0 12
895 7001300 1
896 7001301 0.0 0.0 0.0 11
897 *
898 7010000 "PORVD" SNGLJUN
899 7010101 700010000 702000000 0.0 0.0 0.0 1000
900 7010201 1 0.0 0.0 0.0
901 *
902 *
903 *
904 *
905 *
906 *****
907 **
908 ** MAIN ARC CONNECTIONS
909 **
910 *****
911 *
912 *
913 *
914 * 12 INCH X 6 INCH DIFFUSER ABOVE SRV ARCS ON MAIN DISCHARGE
915 *
916 *
917 *
918 7020000 "PORVD" PIPE
919 7020001 3
920 7020101 0.20069 1
921 7020102 .77708 3
922 7020301 0.75 1
923 7020302 0.375 3
924 7020401 0.0 3
925 7020601 -90.0 3
926 7020801 0.000152 0.0 1

```

```

927 7020802 0.000169 0.0 3
928 7020901 0.4930 0.2045 1
929 7020902 0.0 0.0 2
930 7021001 00 3
931 7021101 1000 2
932 7021201 4 17.7 120.0 0.9284 0.0 3
933 7021300 1
934 7021301 0.0 0.0 0.0 2
935 *
936 8000000 "PORVD" SNGLJUN
937 8000101 702010000 801000000 0.0 0.0 0.0 1000
938 8000201 1 0.0 0.0 0.0
939 *
940 3070000 "PORVD3" SNGLJUN
941 3070101 306010000 801000000 0.0 0.156 0.156 1000 * 12 IN ELBOW LOSSES
942 3070201 1 0.0 0.0 0.0
943 *
944 * 12 X 12 X 6 INCH REDUCING TEE CONNECTS ARC WITH DISCHARGE
945 *
946 8010000 "PORVD" BRANCH
947 8010001 0
948 8010101 0.77708 0.5 0.0 0.0 -90. -0.5 0.000169 0.0 00
949 8010200 4 17.7 120.0 0.9284 0.0 0.0
950 *
951 8020000 "PORVD" SNGLJUN
952 8020101 801010000 803000000 0.0 0.0 0.0 1000
953 8020201 1 0.0 0.0 0.0
954 *
955 8030000 "PORVD" SNGLVOL
956 8030101 0.77708 1.1667 0.0 0.0 -90. -1.1667 0.000169 0.0 00
957 8030200 4 17.7 120.0 0.9284 0.0 0.0
958 *
959 8040000 "PORVD" SNGLJUN
960 8040101 803010000 805000000 0.0 0.0 0.0 1000
961 8040201 1 0.0 0.0 0.0
962 *
963 2070000 "PORVD" SNGLJUN
964 2070101 206010000 805000000 0.0 0.156 0.156 1000 * 12 IN ELBOW LOSSES
965 2070201 1 0.0 0.0 0.0
966 *
967 * 12 X12 X 6 INCH REDUCING TEE. CONNECTS SRV ARC WITH DISCHARGE PIPING.
968 *
969 8050000 "PORVD" BRANCH
970 8050001 0
971 8050101 0.77708 0.5 0.0 0.0 -90. -0.5 0.000169 0.0 00
972 8050200 4 17.7 120.0 0.9284 0.0 0.0
973 *
974 8060000 "PORVD" SNGLJUN
975 8060101 805010000 807000000 0.0 0.0 0.0 1000
976 8060201 1 0.0 0.0 0.0
977 *
978 8070000 "PORVD" SNGLVOL
979 8070101 0.77708 1.1667 0.0 0.0 -90. -1.1667 0.000169 0.0 00
980 8070200 4 17.7 120.0 0.9284 0.0 0.0
981 *
982 8080000 "PORVD" SNGLJUN
983 8080101 807010000 809000000 0.0 0.0 0.0 1000
984 8080201 1 0.0 0.0 0.0

```

```

985 *
986 9000000 "QTANKD" SNGLJUN
987 9000101 813010000 901000000 0.0 0.1560 0.1560 1000
988 9000201 1 0.0 0.0 0.0
989 *
990 9010000 "QTANKD" PIPE
991 9010001 2
992 9010101 0.77708 2
993 9010301 1.0833 2
994 9010401 0.0 2
995 9010601 -90.0 2
996 9010801 0.000169 0.0 2
997 9010901 0.0 0.0 1
998 9011001 00 2
999 9011101 1000 1
1000 9011201 4 17.7 120.0 0.9284 0.0 2
1001 9011300 1
1002 9011301 0.0 0.0 0.0 1
1003 *
1004 *****
1005 **
1006 ** QUENCH TANK **
1007 **
1008 *****
1009 *
1010 9020000 "QTANK-IN" SNGLJUN
1011 9020101 901010000 903000000 0. 0. 0. 1000
1012 9020201 1 0. 0. 0.
1013 **
1014 * SPARGER 12 IN SCH40 PIPE
1015 **
1016 9030000 "SPARGER" PIPE
1017 * NO OF VOLUMES
1018 9030001 18
1019 * FLOW AREA
1020 9030101 0.7773 18
1021 * VOL. LENGTHS
1022 9030301 1.125 2
1023 9030302 1.1333 7
1024 9030303 1.0 18
1025 * VOL. VOLS.
1026 9030401 0.0 18
1027 *
1028 * VERTICAL ANGLES
1029 9030601 -90. 7
1030 9030602 0.0 18
1031 * PIPE ROUGHNESS
1032 9030801 1.69-4 0.0 18
1033 * JUNCTION LOSS COEFF.
1034 9030901 0.0 0.0 6
1035 9030902 0.156 0.156 7
1036 9030903 0.0 0.0 17
1037 * VOL. CONTROL FLAG
1038 9031001 00 18
1039 * JUN. CONTROL FLAG
1040 9031101 1000 17
1041 * INITIAL COND.
1042 9031201 4 17.7 120. 0.9284 0. 2

```

```

1043 9031202 3 17.7 120. 0.0 0. 18
1044 * JUN. INITIAL COND.
1045 9031300 1
1046 9031301 0.0 0.0 0.0 17
1047 **
1048 * SPARGER EXIT
1049 **
1050 9040000 "EXIT" SNGLJUN
1051 9040101 903010000 905000000 0.0 1.0 1.0 0100
1052 9040201 1 0. 0. 0.
1053 **
1054 * WATER VOL.
1055 **
1056 9050000 "QT. WATER" SNGLVQL
1057 9050101 260.4706 5.6667 0.0 0.0 90. 5.6667 0.003 0.0 01
1058 9050200 3 17.7 120.
1059 **
1060 * INTERFACE
1061 **
1062 9060000 "INTERFACE" SNGLJUN
1063 9060101 905010000 907000000 0.0 0.0 0.0 1000
1064 9060201 1 0.0 0.0 0.0
1065 **
1066 * AIR VOLUME
1067 **
1068 9070000 "QT. AIR" SNGLVQL
1069 9070101 260.4706 1.2439 0.0 0.0 90. 1.2439 0.003 0.0 01
1070 9070200 4 17.7 120. 0.9284
1071 **
1072 * RUPTURE DISC
1073 **
1074 9080000 "RUP.DISC" VALVE
1075 9080101 907010000 999000000 1.77 0. 0. 1100
1076 9080201 1 0. 0. 0.
1077 9080300 TRPVLV
1078 9080301 501 * VALVE OPENING TRIP
1079 **
1080 * PIPE OUTSIDE ENVIRONMENT
1081 **
1082 9990000 "ATMOSPHERE" TMDPVOL
1083 9990101 10000. 10000. 0.0 0.0 0.0 0.0 .00001 0.0 11
1084 9990200 4
1085 9990201 0.0 17.7 120. 0.9284
1086 .END OF CASE

```

Technical Report
TR-5364-2
Revision 0

TELEDYNE ENGINEERING SERVICES

9.1.1.2 PORV Solid 400 Liquid Restart

LISTING OF INPUT DATA FOR CASE 1

```

1 =THIS RESTARS RELAP 3 PORVS OPENING ON SOLID WATER UNIT2 RED
2 *
3 100 RESTART TRANSNT
4 101 RUN
5 *
6 103 2000
7 104 NOACTION
8 201 0.600 1.-7 2.-4 11001 5 50 250
9 *
10 *
11 * MINOR EDITS
12 *
13 301 MFLOWJ 415000000
14 302 MFLOWJ 490000000
15 303 MFLOWJ 493000000
16 304 MFLOWJ 388000000
17 305 MFLOWJ 811140000
18 306 MFLOWJ 811790000
19 307 MFLOWJ 307000000
20 308 MFLOWJ 207000000
21 309 MFLOWJ 107000000
22 *
23 310 QUALS 400010000
24 311 QUALS 500010000
25 312 QUALS 600010000
26 313 QUALS 410210000
27 314 QUALS 485270000
28 315 QUALS 492110000
29 316 QUALS 389010000
30 317 QUALS 811140000
31 318 QUALS 811790000
32 319 QUALS 106010000
33 320 QUALS 106390000
34 321 QUALS 206010000
35 322 QUALS 206330000
36 323 QUALS 306010000
37 324 QUALS 306250000
38 *
39 325 P 400010000
40 326 P 500010000
41 327 P 600010000
42 328 P 410210000
43 329 P 485270000
44 330 P 492110000
45 331 P 389010000
46 332 P 811140000
47 333 P 811790000
48 334 P 106010000
49 335 P 106390000
50 336 P 206010000
51 337 P 206330000
52 338 P 306010000
53 339 P 306250000
54 *
55 2001 5, 151
56 2002 206010000, 206020000, 206030000, 206040000, 206050000

```

BY KTC DATE 5-20-83
 CHKD. BY Jim DATE 6-2-83

57 2003 206060000,206070000,206080000,206090000,206100000
 58 2004 206110000,206120000,206130000,206140000,206150000
 59 2005 206160000,206170000,206180000,206190000,206200000
 60 2006 206210000,206220000,206230000,206240000,206250000
 61 2007 206260000,206270000,206280000,206290000,206300000
 62 2008 206310000,206320000,206330000

63 *

64 *

65 *

66 *

67 *

**** FIRST C.V. DOWNSTREAM OF THE ARC ****

68 *

69 *

70 *

2010 805010000

71 *

72 *

73 *

74 *

75 *

***** 12 INCH DISCHARGE DOWN TO THE QUENCH TANK *****

76 *

77 *

78 *

2020 811190000,811200000,811210000,811220000,811230000

79 *

2021 811240000,811250000,811260000,811270000,811280000

80 *

2022 811290000,811300000,811310000,811320000,811330000

81 *

2023 811340000,811350000,811360000,811370000,811380000

82 *

2024 811390000,811400000,811410000,811420000,811430000

83 *

2025 811440000,811450000,811460000,811470000,811480000

84 *

2026 811490000,811500000,811510000,811520000,811530000

85 *

2027 811540000,811550000,811560000,811570000,811580000

86 *

2028 811590000,811600000,811610000,811620000,811630000

87 *

2029 811640000,811650000,811660000,811670000,811680000

88 *

2030 811690000,811700000,811710000,811720000,811730000

89 *

2031 811740000,811750000,811760000,811770000,811780000

90 *

2032 811790000,811800000,811810000,811820000,811830000

91 *

2033 811840000,811850000,811860000,811870000,811880000

92 *

2034 811890000,811900000,811910000,811920000,811930000

93 *

2035 811940000,811950000,811960000,811970000,811980000

94 *

2036 811990000,811180000

95 *

96 *

2040 813010000,813020000,813030000,813040000,813050000

97 *

2041 813060000,813070000,813080000,813090000,813100000

98 *

2042 813110000,813120000,813130000,813140000,813150000

99 *

2043 813160000,813170000,813180000,813190000,813200000

100 *

2044 813210000,813220000,813230000,813240000,813250000

101 *

2045 813260000,813270000,813280000,813290000,813300000

102 *

103 *

104 *

***** PIPE DOWN INTO THE QUENCH TANK ****

105 *

106 *

107 *

108 *

2050 901010000,901020000,903010000,903020000

109 *

2051 903030000

110 *

111 *

112 *

3880000 "PORVU" SNGLJUN

113 *

3880101 387010000 389000000 0.0 0.0 0.0 1000

115	3880201	1	0.0	0.0	0.0
116	20300100	MFLOWJ	415000000		
117	20300200	MFLOWJ	493000000		
118	20300300	MFLOWJ	490000000		
119	20300400	MFLOWJ	388000000		
120	20300500	MFLOWJ	811140000		
121	20300600	MFLOWJ	811790000		
122	20300700	MFLOWJ	307000000		
123	20300800	MFLOWJ	207000000		
124	20300900	MFLOWJ	107000000		
125	*				
126	20301000	QUALS	400010000		
127	20301100	QUALS	500010000		
128	20301200	QUALS	600010000		
129	20301300	QUALS	410210000		
130	20301400	QUALS	485270000		
131	20301500	QUALS	492110000		
132	20301600	QUALS	389010000		
133	20301700	QUALS	811140000		
134	20301800	QUALS	811790000		
135	20301900	QUALS	106010000		
136	20302000	QUALS	106390000		
137	20302100	QUALS	206010000		
138	20302200	QUALS	206330000		
139	20302300	QUALS	306010000		
140	20302400	QUALS	306250000		
141	*				
142	20302500	P	400010000		
143	20302600	P	500010000		
144	20302700	P	600010000		
145	20302800	P	410210000		
146	20302900	P	485270000		
147	20303000	P	492110000		
148	20303100	P	389010000		
149	20303200	P	811140000		
150	20303300	P	811790000		
151	20303400	P	106010000		
152	20303500	P	106390000		
153	20303600	P	206010000		
154	20303700	P	206330000		
155	20303800	P	306010000		
156	20303900	P	306250000		
157	*				
158	.END				

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TELEDYNE ENGINEERING SERVICES

9.1.1.3 SV Cold Loop Seal (Quarter Model)

LISTING OF INPUT DATA FOR CASE 1

```

1  =AEP UNIT2 1 LINE RELAP5
2  100 NEW TRANSNT
3  101 RUN
4  102 BRITISH BRITISH
5  104 NOACTION
6  * TIME STEP CONTROL
7  *
8  201 0.6000 1.0-7 2.0-4 11001 5 25 250
9  * MINOR EDITS
10 *
11 301 QVALS 007010000
12 302 QVALS 005200000
13 303 QVALS 013200000
14 304 P 005200000
15 305 P 007010000
16 308 P 007380000
17 307 MFLOWJ 006000000
18 308 MFLOWJ 005070000
19 309 MFLOWJ 014000000
20 310 P 007140000
21 311 P 011560000
22 312 P 013300000
23 313 MFLOWJ 007140000
24 314 MFLOWJ 007380000
25 315 MFLOWJ 011560000
26 *
27 *
28 2001 5,192,001010000,003010000,005010000
29 2002 005020000,005030000,005040000,005050000,005080000
30 2003 005070000,005080000,005090000,005100000,005110000
31 2004 005120000,005130000,005140000,005150000,005180000
32 2005 005170000,005180000,005190000,005200000,007010000
33 2006 007020000,007030000,007040000,007050000,007080000,007070000
34 2007 007080000,007090000,007100000,007110000,007120000
35 2008 007130000,007140000,007150000,007180000,007170000
36 2009 007180000,007190000,007200000,007210000,007220000
37 2010 007230000,007240000,007250000,007280000,007270000
38 2011 007280000,007290000,007300000,007310000,007320000
39 2012 007330000,007340000,007350000,007380000,007370000
40 2013 007380000,007390000,009010000,011010000,011020000
41 2014 011030000,011040000,011050000,011080000,011070000
42 2015 011080000,011090000,011100000,011110000,011120000
43 2016 011130000,011140000,011150000,011180000,011170000
44 2017 011180000,011190000,011200000,011210000,011220000
45 2018 011230000,011240000,011250000,011280000,011270000
46 2019 011280000,011290000,011300000,011310000,011320000
47 2020 011330000,011340000,011350000,011380000,011370000
48 2021 011380000,011390000,011400000,011410000,011420000
49 2022 011430000,011440000,011450000,011480000,011470000
50 2023 011480000,011490000,011500000,011510000,011520000
51 2024 011530000,011540000,011550000,011580000,011570000
52 2025 011580000,011590000,011800000,011810000,011820000
53 2026 011830000,011840000,011850000,011880000,011870000
54 2027 011880000,011890000,011700000,011710000,011720000
55 2028 011730000,011740000,011750000,011780000,011770000
56 2029 011780000,011790000,011800000,011810000,011820000

```

BY CLM DATE 2-9-83
CHKD. BY LJS DATE 2-9-83

57 2030 011830000,011840000,011850000,011860000,011870000
 58 2031 011880000,011890000,011900000,011910000,011920000
 59 2032 011930000,011940000,011950000,011960000,011970000
 60 2033 011980000,011990000,013010000,013020000,013030000
 61 2034 013040000,013050000,013060000,013070000,013080000
 62 2035 013090000,013100000,013110000,013120000,013130000
 63 2036 013140000,013150000,013160000,013170000,013180000
 64 2037 013190000,013200000,013210000,013220000,013230000
 65 2038 013240000,013250000,013280000,013270000,013280000
 66 2039 013280000,013300000,015010000

67 *

68 *TRIPS

69 *

70 502 TIME 0 GT NULL 0 1.500 L * JDB TERMINATION TRIP

71 503 TIME 0 GE NULL 0 0.0 L * VALVE OPEN

72 504 TIME 0 GE NULL 0 5.0 L * VALVE CLOSED

73 600 502

74 *

75 * HYDRODYNAMIC COMPONENTS

76 *

77 *

78 * PRESSURIZER

79 *

80 0010000 *PRESS1* TMDPVOL

81 0010101 0.0 20.0 500.0 0.0 0.0 0.0 0.00005 0.0 11

82 0010200 2

83 0010201 0.0 2500.0 1.0 0.1 2514.0 1.0 0.3 2555.0 1.0 0.5 2600.0 1.0

84 0010202 0.7 2687.0 1.0 0.9 2700.0 1.0 1.1 2740.0 1.0 1.3 2745.0 1.0

85 0010203 1.5 2747.0 1.0 1.7 2748.0 1.0 1.9 2750.0 1.0 2.0 2750.0 1.0

86 0010204 2.5 2750.0 1.0

87 *

88 * LOOP SEAL GEOMETRY

89 *

90 0020000 *LPSL* SNGLJUN

91 0020101 001000000 003000000 0.0 0.0 0.0 1000 * THIS IS A SHORT RADIUS ELBOW LEAVING

92 0020201 1 0.0 0.0 0.0

93 *

94 0030000 *LPSL* SNGLVOL

95 0030101 0.1485 1.0 0.0 90.0 0.0 0.0 0.000151 0.0 00

96 0030200 2 2500.0 1.0

97 *

98 0040000 *LPSL* SNGLJUN

99 0040101 003010000 005000000 0.0 0.1838 0.1838 1000

100 0040201 1 0.0 0.0 0.0

101 *

102 0050000 *LPSL* PIPE

103 0050001 20

104 0050101 0.1485 20

105 0050301 0.50 10

106 0050302 0.574 20

107 0050401 0.0 20

108 0050601 -90.0 7

109 0050602 0.0 10

110 0050603 90.0 20

111 0050801 0.000151 0.0 20

112 0050901 0.0 0.0 8

```

115 0050904 0.1838 0.1838 10
116 0050905 0.0 0.0 19
117 0051001 00 20
118 0051101 1000 19
119 0051201 3 2500.0 584.4 0.0 0.0 1
120 0051202 3 2500.0 451.1 0.0 0.0 2
121 0051203 3 2500.0 352.1 0.0 0.0 3
122 0051204 3 2500.0 278.8 0.0 0.0 4
123 0051205 3 2500.0 218.1 0.0 0.0 5
124 0051206 3 2500.0 169.3 0.0 0.0 8
125 0051207 3 2500.0 141.1 0.0 0.0 20
126 0051300 1
127 0051301 0.0 0.0 0.0 19
128 *
129 *****
130 * VALVE 6M8 CROSBY SAFETY
131 *****
132 0060000 "SRV" VALVE
133 0080101 005010000 007000000 0.022 0.0 0.0 0100
134 0060201 1 0.0 0.0 0.0
135 0060300 MTRVLV
136 0060301 503 504 100.0 0.0 * CROSBY 6M8 OPENING IN 10 MSEC
137 *
138 * DISCHARGE PIPING
139 0070000 "DISCHA1" PIPE
140 0070001 39
141 0070101 0.20069 39
142 0070301 0.526 4
143 0070302 1.094 14
144 * ARC STARTS HERE LEVEL 689-2"
145 0070303 0.94187 17
146 0070304 0.942 20
147 0070305 0.8425 23
148 0070306 0.844 26
149 0070307 0.8433 29
150 0070308 0.8333 32
151 0070309 0.8333 35
152 * ARC ENDS
153 0070310 0.91750 39
154 0070401 0.0 39
155 0070601 0.0 4
156 0070602 -90.0 14
157 0070803 0.0 39
158 0070801 0.000152 0.0 39
159 0070901 0.0 0.0 3
160 0070902 0.1800 0.1800 4
161 0070903 0.0 0.0 13
162 0070904 0.1800 0.1800 14
163 0070905 0.0 0.0 38
164 0071001 00 39
165 0071101 1000 38
166 0071201 4 14.7 120.0 0.9284 0.0 39
167 0071300 1
168 0071301 0.0 0.0 0.0 38
169 *
170 0080000 "DISCHA1" SNGLJUN
171 0080101 007010000 009000000 0.0 0.1580 0.1580 1000 *LOSSES FOR A 12 IN ELBOW

```

```

173 *
174 * INPUT A BRANCH HERE FOR A COMPLETE MODEL
175 *
176 0090000 "DISCHA1" SNGLVOL
177 0090101 0.7771 0.5 0.0 0.0 -90.0 -0.5 0.000169 0.0 00
178 0090200 4 14.7 120.0 0.9284
179 *
180 0100000 "DISCHA1" SNGLJUN
181 0100101 009010000 011000000 0.0 0.0 0.0 1000
182 0100201 1 0.0 0.0 0.0
183 *
184 0110000 "DISCHA1" PIPE
185 0110001 99
186 0110101 0.7771 99
187 0110301 1.039 14
188 0110302 0.53025 18
189 0110303 0.5 22
190 0110304 0.53025 28
191 0110305 0.9875 58
192 0110308 0.475 68
193 0110307 0.49359 79
194 0110308 0.46875 87
195 0110309 0.51172 95
196 0110310 0.95 99
197 0110401 0.0 99
198 0110601 -90.0 14
199 0110602 -45.0 18
200 0110603 -90.0 22
201 0110604 -45.0 28
202 0110605 -90.0 58
203 0110606 0.0 87
204 0110607 -90.0 95
205 0110608 0.0 99
206 0110801 0.000169 0.0 99
207 0110901 0.0 0.0 13
208 0110902 0.078 0.078 14
209 0110903 0.0 0.0 17
210 0110904 0.078 0.078 18
211 0110905 0.0 0.0 21
212 0110908 0.078 0.078 22
213 0110907 0.0 0.0 25
214 0110908 0.078 0.078 28
215 0110909 0.0 0.0 55
216 0110910 0.158 0.158 58
217 0110911 0.0 0.0 65
218 0110912 0.158 0.158 68
219 0110913 0.0 0.0 78
220 0110914 0.156 0.158 79
221 0110915 0.0 0.0 86
222 0110918 0.158 0.158 87
223 0110917 0.0 0.0 94
224 0110918 0.158 0.158 95
225 0110919 0.0 0.0 98
226 0111001 00 99
227 0111101 1000 98
228 0111201 4 14.7 120.0 0.9284 0.0 99
229 0111300 1

```

```

231 *
232 0120000 "DISCHA1" SNGLJUN
233 0120101 011010000 013000000 0.0 0.0 0.0 1000
234 0120201 1 0.0 0.0 0.0
235 *
236 0130000 "DISCHA1" PIPE
237 0130001 30
238 0130101 0.7771 30
239 0130301 0.95 8
240 0130302 1.0 20
241 0130303 0.5 30
242 0130401 0.0 30
243 0130501 0.0 30
244 0130801 0.000159 0.0 30
245 0130901 0.0 0.0 5
246 0130902 0.156 0.156 8
247 0130903 0.0 0.0 19
248 0130904 0.156 0.156 20
249 0130905 0.0 0.0 29
250 0131001 00 30
251 0131101 1000 29
252 0131201 4 14.7 120.0 0.9284 0.0 30
253 0131300 1
254 0131301 0.0 0.0 0.0 29
255 *
256 0140000 "DISCHA1" SNGLJUN
257 0140101 013010000 015000000 0.0 0.0 0.0 0100
258 0140201 1 0.0 0.0 0.0
259 *
260 0150000 "ATMOS" TMOPVOL
261 0150101 10000.0 10000.0 0.0 0.0 0.0 0.0 0.00001 0.0 11
262 0150200 4
263 0150201 0.0 14.7 120.0 0.9284
264 *
265 PLOT CARDS
266 *
267 20300100 QUALS 007010000
268 20300200 QUALS 005200000
269 20300300 QUALS 013200000
270 20300400 P 005200000
271 20300500 P 007010000
272 20300600 P 007380000
273 20300700 MFLOWJ 006000000
274 20300800 MFLOWJ 005070000
275 20300900 MFLOWJ 014000000
276 20301000 P 007140000
277 20301100 P 011560000
278 20301200 P 013300000
279 20301300 MFLOWJ 007140000
280 20301400 MFLOWJ 007380000
281 20301500 MFLOWJ 011560000
282 .END OF CASE

```

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 **TELEDYNE ENGINEERING SERVICES**

Section 9.1.2

REPIPE Input

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 **TELEDYNE ENGINEERING SERVICES**

9.1.2.1 Unit 2 - Model Section A

\$PIPES
 INLINE=3,KBLOCK=200,KPIPE=10,KPLOT(1)=1,KWAVE=1,
 KPRINT=-1,KPNV=1,KSTEP=3,
 NDROPV=385010000,206330000,811190000\$

342	386000000	-0.3710	0.6788	0.6340/
340	-387010000	-0.3710	0.6788	0.6340/
339	387010000	0.0	1.0	0.0/
339	387020000	0.0	1.0	0.0/
339	387030000	0.0	1.0	0.0/
339	387040000	0.0	1.0	0.0/
339	387050000	0.0	1.0	0.0/
339	387060000	0.0	1.0	0.0/
339	387070000	0.0	1.0	0.0/
339	387080000	0.0	1.0	0.0/
339	387090000	0.0	1.0	0.0/
339	387100000	0.0	1.0	0.0/
339	387110000	0.0	1.0	0.0/
339	388000000	0.0	1.0	0.0/
339	420000000	0.0	1.0	0.0/
339	425010000	0.0	1.0	0.0/
339	425020000	0.0	1.0	0.0/
338	-387020000	0.0	1.0	0.0/
338	-387030000	0.0	1.0	0.0/
338	-387040000	0.0	1.0	0.0/
338	-387050000	0.0	1.0	0.0/
338	-387060000	0.0	1.0	0.0/
338	-387070000	0.0	1.0	0.0/
338	-387080000	0.0	1.0	0.0/
338	-387090000	0.0	1.0	0.0/
338	-387100000	0.0	1.0	0.0/
338	-387110000	0.0	1.0	0.0/
336	-388000000	0.0	1.0	0.0/
338	-420000000	0.0	1.0	0.0/
336	-498000000	0.0	1.0	0.0/
338	-425010000	0.0	1.0	0.0/
338	-425020000	0.0	1.0	0.0/
338	-425030000	0.0	1.0	0.0/
334	425030000	0.7844	0.0	0.6202/
334	425040000	0.7844	0.0	0.6202/
334	430000000	0.7844	0.0	0.6202/
330	-425040000	0.7844	0.0	0.6202/
330	-430000000	0.7844	0.0	0.6202/
330	-435010000	0.7844	0.0	0.6202/
334	435010000	0.7844	0.0	0.6202/
334	440000000	0.7844	0.0	0.6202/
334	445010000	0.7844	0.0	0.6202/
334	445020000	0.7844	0.0	0.6202/
334	445030000	0.7844	0.0	0.6202/
334	445040000	0.7844	0.0	0.6202/
330	-440000000	0.7844	0.0	0.6202/
330	-445010000	0.7844	0.0	0.6202/
330	-445020000	0.7844	0.0	0.6202/
330	-445030000	0.7844	0.0	0.6202/
330	-445040000	0.7844	0.0	0.6202/
330	-445050000	0.7844	0.0	0.6202/
328	445050000	0.0	1.0	0.0/
328	445060000	0.0	1.0	0.0/
328	445070000	0.0	1.0	0.0/
328	445080000	0.0	1.0	0.0/

BY KJG DATE 5-21-83
 CHKD. BY MR DATE 5/26/83

324	-445060000	0.0	1.0	0.0/
324	-445070000	0.0	1.0	0.0/
324	-445080000	0.0	1.0	0.0/
324	-445090000	0.0	1.0	0.0/
322	445090000	0.9138	0.0	-0.4062/
322	450000000	0.9138	0.0	-0.4062/
322	460000000	0.9138	0.0	-0.4062/
322	465010000	0.9138	0.0	-0.4062/
322	465020000	0.9138	0.0	-0.4062/
322	470000000	0.9138	0.0	-0.4062/
318	-450000000	0.9138	0.0	-0.4062/
318	-460000000	0.9138	0.0	-0.4062/
318	-491000000	0.9138	0.0	-0.4062/
318	-465010000	0.9138	0.0	-0.4062/
318	-465020000	0.9138	0.0	-0.4062/
318	-470000000	0.9138	0.0	-0.4062/
318	-475010000	0.9138	0.0	-0.4062/
3181	475010000	0.8212	0.0	-0.5707/
3181	480000000	0.8212	0.0	-0.5707/
3181	485010000	0.8212	0.0	-0.5707/
3181	485020000	0.8212	0.0	-0.5707/
3181	485030000	0.8212	0.0	-0.5707/
318	-480000000	0.8212	0.0	-0.5707/
318	-485010000	0.8212	0.0	-0.5707/
318	-485020000	0.8212	0.0	-0.5707/
318	-485030000	0.8212	0.0	-0.5707/
318	-485040000	0.8212	0.0	-0.5707/
3181	485040000	0.5557	0.0	-0.8314/
3161	485050000	0.5557	0.0	-0.8314/
3181	485060000	0.5557	0.0	-0.8314/
3161	485070000	0.5557	0.0	-0.8314/
314	-485050000	0.5557	0.0	-0.8314/
314	-485060000	0.5557	0.0	-0.8314/
314	-485070000	0.5557	0.0	-0.8314/
314	-485080000	0.5557	0.0	-0.8314/
3141	485080000	0.2178	0.0	-0.9760/
3141	485090000	0.2178	0.0	-0.9760/
3141	485100000	0.2178	0.0	-0.9760/
3141	485110000	0.2178	0.0	-0.9760/
312	-485090000	0.2178	0.0	-0.9760/
312	-485100000	0.2178	0.0	-0.9760/
312	-485110000	0.2178	0.0	-0.9760/
312	-485120000	0.2178	0.0	-0.9760/
3121	485120000	-0.1543	0.0	-0.9880/
3121	485130000	-0.1543	0.0	-0.9880/
3121	485140000	-0.1543	0.0	-0.9880/
3121	485150000	-0.1543	0.0	-0.9880/
310	-485130000	-0.1543	0.0	-0.9880/
310	-485140000	-0.1543	0.0	-0.9880/
310	-485150000	-0.1543	0.0	-0.9880/
310	-485160000	-0.1543	0.0	-0.9880/
3101	485160000	-0.9272	-0.0262	-0.3745/
308	485170000	-0.9272	-0.0262	-0.3745/
308	485180000	-0.9272	-0.0262	-0.3745/
308	485190000	-0.9272	-0.0262	-0.3745/
308	485200000	-0.9272	-0.0262	-0.3745/
308	485210000	-0.9272	-0.0262	-0.3745/
308	485220000	-0.9272	-0.0262	-0.3745/
308	485230000	-0.9272	-0.0262	-0.3745/
308	485240000	-0.9272	-0.0262	-0.3745/

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308	485250000	-0.9272	-0.0262	-0.3745/	
308	485260000	-0.9272	-0.0262	-0.3745/	
308	1	-485170000	-0.9272	-0.0262	-0.3745/
294	-485180000	-0.9272	-0.0262	-0.3745/	
294	-485190000	-0.9272	-0.0262	-0.3745/	
294	-485200000	-0.9272	-0.0262	-0.3745/	
294	-485210000	-0.9272	-0.0262	-0.3745/	
294	-485220000	-0.9272	-0.0262	-0.3745/	
294	-485230000	-0.9272	-0.0262	-0.3745/	
294	-485240000	-0.9272	-0.0262	-0.3745/	
294	-485250000	-0.9272	-0.0262	-0.3745/	
294	-485260000	-0.9272	-0.0262	-0.3745/	
294	-490000000	-0.9272	-0.0262	-0.3745/	
292	490000000	-0.9272	-0.0262	-0.3745/	
292	400010000	-0.9272	-0.0262	-0.3745/	
292	400020000	-0.9272	-0.0262	-0.3745/	
292	400030000	-0.9272	-0.0262	-0.3745/	
288	-400010000	-0.9272	-0.0262	-0.3745/	
288	-400020000	-0.9272	-0.0262	-0.3745/	
288	-400030000	-0.9272	-0.0262	-0.3745/	
288	-400040000	-0.9272	-0.0262	-0.3745/	
288	400040000	0.0	-1.0	0.0/	
288	400050000	0.0	-1.0	0.0/	
288	400060000	0.0	-1.0	0.0/	
288	400070000	0.0	-1.0	0.0/	
230	-400050000	0.0	-1.0	0.0/	
230	-400060000	0.0	-1.0	0.0/	
230	-400070000	0.0	-1.0	0.0/	
230	-401000000	0.0	-1.0	0.0/	
320	491000000	0.3746	0.0185	-0.9272/	
320	492010000	0.3746	0.0185	-0.9272/	
320	492020000	0.3746	0.0185	-0.9272/	
320	492030000	0.3746	0.0185	-0.9272/	
320	492040000	0.3746	0.0185	-0.9272/	
320	492050000	0.3746	0.0185	-0.9272/	
320	492060000	0.3746	0.0185	-0.9272/	
320	492070000	0.3746	0.0185	-0.9272/	
320	492080000	0.3746	0.0185	-0.9272/	
320	492090000	0.3746	0.0185	-0.9272/	
320	492100000	0.3746	0.0185	-0.9272/	
348	-492010000	0.3746	0.0185	-0.9272/	
348	-492020000	0.3746	0.0185	-0.9272/	
348	-492030000	0.3746	0.0185	-0.9272/	
348	-492040000	0.3746	0.0185	-0.9272/	
348	-492050000	0.3746	0.0185	-0.9272/	
348	-492060000	0.3746	0.0185	-0.9272/	
348	-492070000	0.3746	0.0185	-0.9272/	
348	-492080000	0.3746	0.0185	-0.9272/	
348	-492090000	0.3746	0.0185	-0.9272/	
348	-492100000	0.3746	0.0185	-0.9272/	
348	-493000000	0.3746	0.0185	-0.9272/	
348	493000000	0.3746	0.0185	-0.9272/	
348	600010000	0.3746	0.0185	-0.9272/	
348	600020000	0.3746	0.0185	-0.9272/	
344	-800010000	0.3746	0.0185	-0.9272/	
344	-800020000	0.3746	0.0185	-0.9272/	
344	-800030000	0.3746	0.0185	-0.9272/	
404	800030000	0.0	-1.0	0.0/	
404	800040000	0.0	-1.0	0.0/	
404	800050000	0.0	-1.0	0.0/	

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404	600060000	0.0	-1.0	0.0/
240	-600040000	0.0	-1.0	0.0/
2402	-600050000	0.0	-1.0	0.0/
2402	-600060000	0.0	-1.0	0.0/
2402	-601000000	0.0	-1.0	0.0/
284	498000000	-0.9272	0.0	-0.3746/
284	410010000	-0.9272	0.0	-0.3746/
284	410020000	-0.9272	0.0	-0.3746/
284	410030000	-0.9272	0.0	-0.3746/
284	410040000	-0.9272	0.0	-0.3746/
282	-410010000	-0.9272	0.0	-0.3746/
282	-410020000	-0.9272	0.0	-0.3746/
282	-410030000	-0.9272	0.0	-0.3746/
282	-410040000	-0.9272	0.0	-0.3746/
282	-410050000	-0.9272	0.0	-0.3746/
280	410050000	0.0	1.0	0.0/
280	410060000	0.0	1.0	0.0/
280	410070000	0.0	1.0	0.0/
280	410080000	0.0	1.0	0.0/
280	410090000	0.0	1.0	0.0/
280	410100000	0.0	1.0	0.0/
278	-410060000	0.0	1.0	0.0/
278	-410070000	0.0	1.0	0.0/
278	-410080000	0.0	1.0	0.0/
278	-410090000	0.0	1.0	0.0/
278	-410100000	0.0	1.0	0.0/
278	-410110000	0.0	1.0	0.0/
278	410110000	0.9270	-0.0218	0.3745/
276	410120000	0.9270	-0.0218	0.3745/
278	410130000	0.9270	-0.0218	0.3745/
278	410140000	0.9270	-0.0218	0.3745/
278	410150000	0.9270	-0.0218	0.3745/
278	410160000	0.9270	-0.0218	0.3745/
278	410170000	0.9270	-0.0218	0.3745/
278	410180000	0.9270	-0.0218	0.3745/
278	410190000	0.9270	-0.0218	0.3745/
278	410200000	0.9270	-0.0218	0.3745/
264	-410120000	0.9270	-0.0218	0.3745/
264	-410130000	0.9270	-0.0218	0.3745/
264	-410140000	0.9270	-0.0218	0.3745/
264	-410150000	0.9270	-0.0218	0.3745/
264	-410160000	0.9270	-0.0218	0.3745/
264	-410170000	0.9270	-0.0218	0.3745/
264	-410180000	0.9270	-0.0218	0.3745/
264	-410190000	0.9270	-0.0218	0.3745/
264	-410200000	0.9270	-0.0218	0.3745/
264	-415000000	0.9270	-0.0218	0.3745/
262	415000000	0.9270	-0.0218	0.3745/
262	500010000	0.9270	-0.0218	0.3745/
262	500020000	0.9270	-0.0218	0.3745/
260	-500010000	0.9270	-0.0218	0.3745/
260	-500020000	0.9270	-0.0218	0.3745/
260	-500030000	0.9270	-0.0218	0.3745/
257	500030000	0.0	-1.0	0.0/
257	500040000	0.0	-1.0	0.0/
257	500050000	0.0	-1.0	0.0/
252	-500040000	0.0	-1.0	0.0/
252	-500050000	0.0	-1.0	0.0/
252	-500060000	0.0	-1.0	0.0/
250	500060000	0.7559	0.0	-0.6547/

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248	-500070000	0.7559	0.0	-0.6547/
2481	500070000	0.7170	0.0	-0.6971/
2481	500080000	0.7170	0.0	-0.6971/
2481	500090000	0.7170	0.0	-0.6971/
246	-500080000	0.7170	0.0	-0.6971/
246	-500090000	0.7170	0.0	-0.6971/
246	-500100000	0.7170	0.0	-0.6971/
2461	500100000	0.3736	0.0	-0.9276/
2461	500110000	0.3736	0.0	-0.9276/
2461	500120000	0.3736	0.0	-0.9276/
244	-500110000	0.3736	0.0	-0.9276/
244	-500120000	0.3736	0.0	-0.9276/
244	-500130000	0.3736	0.0	-0.9276/
2441	500130000	0.0282	0.0	-0.9996/
2441	500140000	0.0282	0.0	-0.9996/
2441	500150000	0.0282	0.0	-0.9996/
2441	501000000	0.0282	0.0	-0.9996/
242	-500140000	0.0282	0.0	-0.9996/
242	-500150000	0.0282	0.0	-0.9996/
242	-501000000	0.0282	0.0	-0.9996/
242	-502010000	0.0282	0.0	-0.9996/
2421	502010000	-0.2531	0.0	-0.9674/
240	-503000000	-0.2531	0.0	-0.9674/
2401	503000000	-0.3508	0.0	-0.9364/
2401	601000000	-0.3508	0.0	-0.9364/
238	-505000000	-0.3508	0.0	-0.9384/
2381	505000000	-0.6395	0.0	-0.7688/
2381	506010000	-0.6395	0.0	-0.7688/
2381	506020000	-0.6395	0.0	-0.7688/
2381	506030000	-0.6395	0.0	-0.7688/
236	-506010000	-0.6395	0.0	-0.7688/
236	-506020000	-0.6395	0.0	-0.7688/
236	-506030000	-0.6395	0.0	-0.7688/
236	-506040000	-0.6395	0.0	-0.7688/
2361	506040000	-0.9576	0.0	-0.2882/
2361	506050000	-0.9576	0.0	-0.2882/
2361	506060000	-0.9576	0.0	-0.2882/
2361	506070000	-0.9576	0.0	-0.2882/
234	-506050000	-0.9576	0.0	-0.2882/
234	-506060000	-0.9576	0.0	-0.2882/
234	-506070000	-0.9576	0.0	-0.2882/
234	-506080000	-0.9576	0.0	-0.2882/
2341	506080000	-0.9998	0.0	-0.0175/
2341	507000000	-0.9998	0.0	-0.0175/
2341	508010000	-0.9998	0.0	-0.0175/
2341	509000000	-0.9998	0.0	-0.0175/
2341	511000000	-0.9998	0.0	-0.0175/
228	-507000000	-0.9998	0.0	-0.0175/
228	-508010000	-0.9998	0.0	-0.0175/
228	-509010000	-0.9998	0.0	-0.0175/
226	-511000000	-0.9998	0.0	-0.0175/
228	-700010000	-0.9998	0.0	-0.0175/
224	700010000	0.0	-1.0	0.0/
224	700020000	0.0	-1.0	0.0/
224	700030000	0.0	-1.0	0.0/
224	700040000	0.0	-1.0	0.0/
224	700050000	0.0	-1.0	0.0/
224	700060000	0.0	-1.0	0.0/
224	700070000	0.0	-1.0	0.0/

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224	700090000	0.0	-1.0	0.0/
224	700100000	0.0	-1.0	0.0/
224	700110000	0.0	-1.0	0.0/
224	701000000	0.0	-1.0	0.0/
68	-700030000	0.0	-1.0	0.0/
68	-700040000	0.0	-1.0	0.0/
68	-700050000	0.0	-1.0	0.0/
68	-700060000	0.0	-1.0	0.0/
68	-700070000	0.0	-1.0	0.0/
68	-700080000	0.0	-1.0	0.0/
68	-700090000	0.0	-1.0	0.0/
68	-700100000	0.0	-1.0	0.0/
68	-700110000	0.0	-1.0	0.0/
68	-701000000	0.0	-1.0	0.0/
68	-702010000	0.0	-1.0	0.0/
224	702010000	0.0	-1.0	0.0/
224	702020000	0.0	-1.0	0.0/
224	800000000	0.0	-1.0	0.0/
224	307000000	0.0	-1.0	0.0/
224	802000000	0.0	-1.0	0.0/
224	804000000	0.0	-1.0	0.0/
224	207000000	0.0	-1.0	0.0/
224	806000000	0.0	-1.0	0.0/
224	808000000	0.0	-1.0	0.0/
224	107000000	0.0	-1.0	0.0/
224	810000000	0.0	-1.0	0.0/
224	811010000	0.0	-1.0	0.0/
224	811020000	0.0	-1.0	0.0/
224	811030000	0.0	-1.0	0.0/
224	811040000	0.0	-1.0	0.0/
224	811050000	0.0	-1.0	0.0/
224	811060000	0.0	-1.0	0.0/
224	811070000	0.0	-1.0	0.0/
224	811080000	0.0	-1.0	0.0/
224	811090000	0.0	-1.0	0.0/
224	811100000	0.0	-1.0	0.0/
224	811110000	0.0	-1.0	0.0/
224	811120000	0.0	-1.0	0.0/
224	811130000	0.0	-1.0	0.0/
68	-700020000	0.0	-1.0	0.0/
68	-800000000	0.0	-1.0	0.0/
68	-802000000	0.0	-1.0	0.0/
68	-804000000	0.0	-1.0	0.0/
68	-806000000	0.0	-1.0	0.0/
68	-808000000	0.0	-1.0	0.0/
68	-810000000	0.0	-1.0	0.0/
68	-811010000	0.0	-1.0	0.0/
68	-811020000	0.0	-1.0	0.0/
68	-811030000	0.0	-1.0	0.0/
68	-811040000	0.0	-1.0	0.0/
68	-811050000	0.0	-1.0	0.0/
68	-811060000	0.0	-1.0	0.0/
68	-811070000	0.0	-1.0	0.0/
68	-811080000	0.0	-1.0	0.0/
68	-811090000	0.0	-1.0	0.0/
68	-811100000	0.0	-1.0	0.0/
68	-811110000	0.0	-1.0	0.0/
68	-811120000	0.0	-1.0	0.0/
68	-811130000	0.0	-1.0	0.0/

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68	811140000	-0.2356	-0.7071	0.6667/
68	811150000	-0.2356	-0.7071	0.6667/
68	811160000	-0.2356	-0.7071	0.6667/
66	811170000	-0.2356	-0.7071	0.6667/
64	-811150000	-0.2356	-0.7071	0.6667/
64	-811160000	-0.2356	-0.7071	0.6667/
64	-811170000	-0.2356	-0.7071	0.6667/
64	-811180000	-0.2356	-0.7071	0.6667/
198	305000000	-0.9975	0.0	0.0709/
198	306010000	-0.9975	0.0	0.0709/
198	306020000	-0.9975	0.0	0.0709/
198	306030000	-0.9975	0.0	0.0709/
195	-306010000	-0.9975	0.0	0.0709/
195	-306020000	-0.9975	0.0	0.0709/
195	-306030000	-0.9975	0.0	0.0709/
195	-306040000	-0.9975	0.0	0.0709/
190	306040000	0.0	-1.0	0.0/
190	306050000	0.0	-1.0	0.0/
190	306060000	0.0	-1.0	0.0/
190	306070000	0.0	-1.0	0.0/
190	306080000	0.0	-1.0	0.0/
190	306090000	0.0	-1.0	0.0/
190	306100000	0.0	-1.0	0.0/
190	306110000	0.0	-1.0	0.0/
186	-306050000	0.0	-1.0	0.0/
186	-306060000	0.0	-1.0	0.0/
186	-306070000	0.0	-1.0	0.0/
186	-306080000	0.0	-1.0	0.0/
186	-306090000	0.0	-1.0	0.0/
186	-306100000	0.0	-1.0	0.0/
186	-306110000	0.0	-1.0	0.0/
186	-306120000	0.0	-1.0	0.0/
184	306120000	-0.9359	0.0	-0.3523/
184	306130000	-0.9359	0.0	-0.3523/
184	306140000	-0.9359	0.0	-0.3523/
182	-306130000	-0.9359	0.0	-0.3523/
182	-306140000	-0.9359	0.0	-0.3523/
182	-306150000	-0.9359	0.0	-0.3523/
182.1	306150000	-0.6354	0.0	-0.7722/
182.1	306160000	-0.6354	0.0	-0.7722/
182.1	306170000	-0.6354	0.0	-0.7722/
180	-306160000	-0.6354	0.0	-0.7722/
180	-306170000	-0.6354	0.0	-0.7722/
180	-306180000	-0.6354	0.0	-0.7722/
180.1	306180000	-0.0516	0.0	-0.9987/
180.1	306190000	-0.0516	0.0	-0.9987/
180.1	306200000	-0.0516	0.0	-0.9987/
178	-306190000	-0.0516	0.0	-0.9987/
178	-306200000	-0.0516	0.0	-0.9987/
178	-306210000	-0.0516	0.0	-0.9987/
178.1	306210000	0.2639	0.0	-0.9645/
178.1	306220000	0.2639	0.0	-0.9645/
178.1	306230000	0.2639	0.0	-0.9645/
178.1	306240000	0.2639	0.0	-0.9645/
176	-306220000	0.2639	0.0	-0.9645/
176	-306230000	0.2639	0.0	-0.9645/
176	-306240000	0.2639	0.0	-0.9645/
176	-307000000	0.2639	0.0	-0.8645/
104	105000000	0.7169	0.0	0.6972/
104	106010000	0.7169	0.0	0.6972/

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104	106020000	0.7169	0 0	0.6972/
104	106030000	0.7169	0.0	0.6972/
98	-106010000	0.7169	0.0	0.6972/
98	-106020000	0.7169	0.0	0.6972/
98	-106030000	0.7169	0.0	0.6972/
98	-106040000	0.7169	0.0	0.6972/
96	106040000	0.0	-1.0	0.0/
98	106050000	0.0	-1.0	0.0/
96	106060000	0.0	-1.0	0.0/
96	106070000	0.0	-1.0	0.0/
96	106080000	0.0	-1.0	0.0/
96	106090000	0.0	-1.0	0.0/
96	106100000	0.0	-1.0	0.0/
98	106110000	0.0	-1.0	0.0/
96	106120000	0.0	-1.0	0.0/
96	106130000	0.0	-1.0	0.0/
90	-106050000	0.0	-1.0	0.0/
90	-106060000	0.0	-1.0	0.0/
90	-106070000	0.0	-1.0	0.0/
90	-106080000	0.0	-1.0	0.0/
90	-106090000	0.0	-1.0	0.0/
90	-106100000	0.0	-1.0	0.0/
90	-106110000	0.0	-1.0	0.0/
90	-106120000	0.0	-1.0	0.0/
90	-106130000	0.0	-1.0	0.0/
90	-106140000	0.0	-1.0	0.0/
88	106140000	0.2657	0.0	0.9641/
88	106150000	0.2657	0.0	0.9641/
88	106160000	0.2657	0.0	0.9641/
86	-106150000	0.2657	0.0	0.9641/
88	-106160000	0.2657	0.0	0.9641/
86	-106170000	0.2657	0.0	0.9641/
861	106170000	-0.3889	0.0	0.9213/
861	106180000	-0.3889	0.0	0.9213/
861	106190000	-0.3889	0.0	0.9213/
84	-106180000	-0.3889	0.0	0.9213/
84	-106190000	-0.3889	0.0	0.9213/
84	-106200000	-0.3889	0.0	0.9213/
841	106200000	-0.8464	0.0	0.5326/
841	106210000	-0.8464	0.0	0.5326/
841	106220000	-0.8464	0.0	0.5326/
82	-106210000	-0.8464	0.0	0.5326/
82	-106220000	-0.8464	0.0	0.5326/
82	-106230000	-0.8464	0.0	0.5326/
821	106230000	-0.9999	0.0	0.0162/
821	106240000	-0.9999	0.0	0.0162/
821	106250000	-0.9999	0.0	0.0162/
80	-106240000	-0.9999	0.0	0.0162/
80	-106250000	-0.9999	0.0	0.0162/
80	-106260000	-0.9999	0.0	0.0162/
801	106260000	-0.8289	0.0	-0.5595/
801	106270000	-0.8289	0.0	-0.5595/
801	106280000	-0.8289	0.0	-0.5595/
78	-106270000	-0.8289	0.0	-0.5595/
78	-106280000	-0.8289	0.0	-0.5595/
78	-106290000	-0.8289	0.0	-0.5595/
781	106290000	-0.4813	0.0	-0.8766/
781	106300000	-0.4813	0.0	-0.8766/
781	106310000	-0.4813	0.0	-0.8766/
78	-106300000	-0.4813	0.0	-0.8766/

76	-106310000	-0.4813	0.0	-0.8766/
76	-106320000	-0.4813	0.0	-0.8766/
761	106320000	-0.2356	-0.7071	0.6667/
781	106330000	-0.2356	-0.7071	0.6667/
781	106340000	-0.2356	-0.7071	0.6667/
74	-106330000	-0.2356	-0.7071	0.6667/
74	-106340000	-0.2356	-0.7071	0.6667/
74	-106350000	-0.2356	-0.7071	0.6667/
741	106350000	0.2639	0.0	-0.9645/
741	106360000	0.2639	0.0	-0.9645/
741	106370000	0.2639	0.0	-0.9645/
741	106380000	0.2639	0.0	-0.9645/
72	-106360000	0.2639	0.0	-0.9645/
72	-106370000	0.2639	0.0	-0.9645/
72	-106380000	0.2639	0.0	-0.9645/
72	-107000000	0.2639	0.0	-0.9645/

99999/

\$STEPS TSTEP(1)=0.001,0.200,-1,-1\$

Technical Report
TR-5364-2
Revision 0

TELEDYNE ENGINEERING SERVICES

9.1.2.2 Unit 2 - Model Section B

138 30237000 2 1 133
138 30237000 0 2 133
138 30237000 0 2 133

\$PIPES

INLINE=3,KBLOCK=200,KPIPE=10,KPLOT(1)=i,KWAVE=i,
 KPRINT=-1,KPNV=1,KSTEP=3,
 NDROPV=206010000,903030000,805010000,811180000\$

154	206010000	-0.4181	0.0	0.9084/
154	206020000	-0.4181	0.0	0.9084/
154	206030000	-0.4181	0.0	0.9084/
148	-206020000	-0.4181	0.0	0.9084/
148	-206030000	-0.4181	0.0	0.9084/
148	-206040000	-0.4181	0.0	0.9084/
148	206040000	0.0	-1.0	0.0/
148	206050000	0.0	-1.0	0.0/
146	206060000	0.0	-1.0	0.0/
146	206070000	0.0	-1.0	0.0/
146	206080000	0.0	-1.0	0.0/
146	206090000	0.0	-1.0	0.0/
146	206100000	0.0	-1.0	0.0/
148	206110000	0.0	-1.0	0.0/
148	206120000	0.0	-1.0	0.0/
146	206130000	0.0	-1.0	0.0/
140	-206050000	0.0	-1.0	0.0/
140	-206060000	0.0	-1.0	0.0/
140	-206070000	0.0	-1.0	0.0/
140	-206080000	0.0	-1.0	0.0/
140	-206090000	0.0	-1.0	0.0/
140	-206100000	0.0	-1.0	0.0/
140	-206110000	0.0	-1.0	0.0/
140	-206120000	0.0	-1.0	0.0/
140	-206130000	0.0	-1.0	0.0/
140	-206140000	0.0	-1.0	0.0/
138	206140000	-0.8064	0.0	0.5913/
138	206150000	-0.8064	0.0	0.5913/
138	206160000	-0.8064	0.0	0.5913/
138	-206150000	-0.8064	0.0	0.5913/
138	-206160000	-0.8064	0.0	0.5913/
138	-206170000	-0.8064	0.0	0.5913/
1361	206170000	-0.9998	0.0	0.0191/
1361	206180000	-0.9998	0.0	0.0191/
1361	206190000	-0.9998	0.0	0.0191/
134	-206180000	-0.9998	0.0	0.0191/
134	-206190000	-0.9998	0.0	0.0191/
134	-206200000	-0.9998	0.0	0.0191/
1341	206200000	-0.8285	0.0	-0.5599/
1341	206210000	-0.8285	0.0	-0.5599/
1341	206220000	-0.8285	0.0	-0.5599/
132	-206210000	-0.8285	0.0	-0.5599/
132	-206220000	-0.8285	0.0	-0.5599/
132	-206230000	-0.8285	0.0	-0.5599/
1321	206230000	-0.4217	0.0	-0.9067/
1321	206240000	-0.4217	0.0	-0.9067/
1321	206250000	-0.4217	0.0	-0.9067/
130	-206240000	-0.4217	0.0	-0.9067/
130	-206250000	-0.4217	0.0	-0.9067/
130	-206260000	-0.4217	0.0	-0.9067/
1301	206260000	0.0323	0.0	-0.9995/
1301	206270000	0.0323	0.0	-0.9995/
1301	206280000	0.0323	0.0	-0.9995/
128	-206270000	0.0323	0.0	-0.9995/
128	-206280000	0.0323	0.0	-0.9995/

BY KJG DATE 5-21-83
 CHKD. BY MIL DATE 5-26-83

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128	-206290000	0.0323	0.0	-0.9995/
128 1	206290000	0.2639	0.0	-0.9645/
128 i	206300000	0.2639	0.0	-0.9645/
128 1	206310000	0.2639	0.0	-0.9645/
123 i	206320000	0.2639	0.0	-0.9645/
126	-206300000	0.2639	0.0	-0.9645/
126	-206310000	0.2639	0.0	-0.9645/
126	-206320000	0.2639	0.0	-0.9645/
126	-207000000	0.2639	0.0	-0.9645/
62	811180000	0.0	-1.0	0.0/
62	811190000	0.0	-1.0	0.0/
62	811200000	0.0	-1.0	0.0/
62	811210000	0.0	-1.0	0.0/
58	-811190000	0.0	-1.0	0.0/
58	-811200000	0.0	-1.0	0.0/
58	-811210000	0.0	-1.0	0.0/
58	-811220000	0.0	-1.0	0.0/
56	811220000	0.2356	-0.7071	-0.6667/
56	811230000	0.2356	-0.7071	-0.6667/
56	811240000	0.2358	-0.7071	-0.6667/
56	811250000	0.2356	-0.7071	-0.6667/
54	-811230000	0.2356	-0.7071	-0.6667/
54	-811240000	0.2356	-0.7071	-0.6667/
54	-811250000	0.2356	-0.7071	-0.6667/
54	-811260000	0.2356	-0.7071	-0.6667/
52	811260000	0.0	-1.0	0.0/
52	811270000	0.0	-1.0	0.0/
52	811280000	0.0	-1.0	0.0/
52	811290000	0.0	-1.0	0.0/
52	811300000	0.0	-1.0	0.0/
52	811310000	0.0	-1.0	0.0/
52	811320000	0.0	-1.0	0.0/
52	811330000	0.0	-1.0	0.0/
52	811340000	0.0	-1.0	0.0/
52	811350000	0.0	-1.0	0.0/
52	811360000	0.0	-1.0	0.0/
52	811370000	0.0	-1.0	0.0/
52	811380000	0.0	-1.0	0.0/
52	811390000	0.0	-1.0	0.0/
52	811400000	0.0	-1.0	0.0/
52	811410000	0.0	-1.0	0.0/
52	811420000	0.0	-1.0	0.0/
52	811430000	0.0	-1.0	0.0/
52	811440000	0.0	-1.0	0.0/
52	811450000	0.0	-1.0	0.0/
52	811460000	0.0	-1.0	0.0/
52	811470000	0.0	-1.0	0.0/
52	811480000	0.0	-1.0	0.0/
52	811490000	0.0	-1.0	0.0/
52	811500000	0.0	-1.0	0.0/
52	811510000	0.0	-1.0	0.0/
52	811520000	0.0	-1.0	0.0/
52	811530000	0.0	-1.0	0.0/
52	811540000	0.0	-1.0	0.0/
52	811550000	0.0	-1.0	0.0/
46	-811270000	0.0	-1.0	0.0/
46	-811280000	0.0	-1.0	0.0/
46	-811290000	0.0	-1.0	0.0/
46	-811300000	0.0	-1.0	0.0/
46	-811310000	0.0	-1.0	0.0/

48	-811320000	0.0	-1.0	0.0/
46	-811330000	0.0	-1.0	0.0/
48	-811340000	0.0	-1.0	0.0/
48	-811350000	0.0	-1.0	0.0/
48	-811360000	0.0	-1.0	0.0/
46	-811370000	0.0	-1.0	0.0/
48	-811380000	0.0	-1.0	0.0/
46	-811390000	0.0	-1.0	0.0/
46	-811400000	0.0	-1.0	0.0/
48	-811410000	0.0	-1.0	0.0/
46	-811420000	0.0	-1.0	0.0/
46	-811430000	0.0	-1.0	0.0/
46	-811440000	0.0	-1.0	0.0/
46	-811450000	0.0	-1.0	0.0/
46	-811460000	0.0	-1.0	0.0/
48	-811470000	0.0	-1.0	0.0/
48	-811480000	0.0	-1.0	0.0/
48	-811490000	0.0	-1.0	0.0/
46	-811500000	0.0	-1.0	0.0/
46	-811510000	0.0	-1.0	0.0/
48	-811520000	0.0	-1.0	0.0/
46	-811530000	0.0	-1.0	0.0/
46	-811540000	0.0	-1.0	0.0/
46	-811550000	0.0	-1.0	0.0/
48	-811560000	0.0	-1.0	0.0/
44	811560000	0.0	0.0	-1.0/
44	811570000	0.0	0.0	-1.0/
44	811580000	0.0	0.0	-1.0/
44	811590000	0.0	0.0	-1.0/
44	811600000	0.0	0.0	-1.0/
44	811610000	0.0	0.0	-1.0/
44	811620000	0.0	0.0	-1.0/
44	811630000	0.0	0.0	-1.0/
44	811640000	0.0	0.0	-1.0/
44	811650000	0.0	0.0	-1.0/
42	-811570000	0.0	0.0	-1.0/
42	-811580000	0.0	0.0	-1.0/
42	-811590000	0.0	0.0	-1.0/
42	-811600000	0.0	0.0	-1.0/
42	-811610000	0.0	0.0	-1.0/
42	-811620000	0.0	0.0	-1.0/
42	-811630000	0.0	0.0	-1.0/
42	-811640000	0.0	0.0	-1.0/
42	-811650000	0.0	0.0	-1.0/
42	-811660000	0.0	0.0	-1.0/
40	811660000	0.2588	0.0	-0.9659/
40	811670000	0.2588	0.0	-0.9659/
40	811680000	0.2588	0.0	-0.9659/
40	811690000	0.2588	0.0	-0.9659/
40	811700000	0.2588	0.0	-0.9659/
40	811710000	0.2588	0.0	-0.9659/
40	811720000	0.2588	0.0	-0.9659/
40	811730000	0.2588	0.0	-0.9659/
40	811740000	0.2588	0.0	-0.9659/
40	811750000	0.2588	0.0	-0.9659/
40	811760000	0.2588	0.0	-0.9659/
40	811770000	0.2588	0.0	-0.9659/
40	811780000	0.2588	0.0	-0.9659/
38	-811670000	0.2588	0.0	-0.9659/
38	-811680000	0.2588	0.0	-0.9659/

30

813030065

1'0

0'0

0'0

30

813030000

1'0

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30

813030000

1'0

0'0

0'0

38	-811690000	0.2588	0.0	-0.9659/
38	-811700000	0.2588	0.0	-0.9659/
38	-811710000	0.2588	0.0	-0.9659/
38	-811720000	0.2588	0.0	-0.9659/
38	-811730000	0.2588	0.0	-0.9659/
38	-811740000	0.2588	0.0	-0.9659/
38	-811750000	0.2588	0.0	-0.9659/
38	-811760000	0.2588	0.0	-0.9659/
38	-811770000	0.2588	0.0	-0.9659/
38	-811780000	0.2588	0.0	-0.9659/
38	-811790000	0.2588	0.0	-0.9659/
38	811790000	1.0	0.0	0.0/
38	811800000	1.0	0.0	0.0/
38	811810000	1.0	0.0	0.0/
38	811820000	1.0	0.0	0.0/
36	811830000	1.0	0.0	0.0/
36	811840000	1.0	0.0	0.0/
36	811850000	1.0	0.0	0.0/
36	811860000	1.0	0.0	0.0/
34	-811800000	1.0	0.0	0.0/
34	-811810000	1.0	0.0	0.0/
34	-811820000	1.0	0.0	0.0/
34	-811830000	1.0	0.0	0.0/
34	-811840000	1.0	0.0	0.0/
34	-811850000	1.0	0.0	0.0/
34	-811860000	1.0	0.0	0.0/
34	-811870000	1.0	0.0	0.0/
33	811870000	0.0	-1.0	0.0/
33	811880000	0.0	-1.0	0.0/
33	811890000	0.0	-1.0	0.0/
33	811900000	0.0	-1.0	0.0/
33	811910000	0.0	-1.0	0.0/
33	811920000	0.0	-1.0	0.0/
33	811930000	0.0	-1.0	0.0/
33	811940000	0.0	-1.0	0.0/
28	-811880000	0.0	-1.0	0.0/
28	-811890000	0.0	-1.0	0.0/
28	-811900000	0.0	-1.0	0.0/
28	-811910000	0.0	-1.0	0.0/
28	-811920000	0.0	-1.0	0.0/
28	-811930000	0.0	-1.0	0.0/
28	-811940000	0.0	-1.0	0.0/
28	-811950000	0.0	-1.0	0.0/
26	811950000	1.0	0.0	0.0/
26	811960000	1.0	0.0	0.0/
26	811970000	1.0	0.0	0.0/
26	811980000	1.0	0.0	0.0/
26	812000000	1.0	0.0	0.0/
26	813010000	1.0	0.0	0.0/
26	813020000	1.0	0.0	0.0/
26	813030000	1.0	0.0	0.0/
26	813040000	1.0	0.0	0.0/
26	813050000	1.0	0.0	0.0/
20	-811960000	1.0	0.0	0.0/
20	-811970000	1.0	0.0	0.0/
20	-811980000	1.0	0.0	0.0/
20	-812000000	1.0	0.0	0.0/
20	-813010000	1.0	0.0	0.0/
20	-813020000	1.0	0.0	0.0/
20	-813030000	1.0	0.0	0.0/

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000010200
000010300

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20	-813040000	1.0	0.0	0.0/
20	-813050000	1.0	0.0	0.0/
20	-813060000	1.0	0.0	0.0/
18	813060000	0.0	0.0	1.0/
18	813070000	0.0	0.0	1.0/
18	813080000	0.0	0.0	1.0/
18	813090000	0.0	0.0	1.0/
18	813100000	0.0	0.0	1.0/
18	813110000	0.0	0.0	1.0/
18	813120000	0.0	0.0	1.0/
18	813130000	0.0	0.0	1.0/
18	813140000	0.0	0.0	1.0/
18	813150000	0.0	0.0	1.0/
18	813160000	0.0	0.0	1.0/
18	813170000	0.0	0.0	1.0/
18	813180000	0.0	0.0	1.0/
18	813190000	0.0	0.0	1.0/
12	-813070000	0.0	0.0	1.0/
12	-813080000	0.0	0.0	1.0/
12	-813090000	0.0	0.0	1.0/
12	-813100000	0.0	0.0	1.0/
12	-813110000	0.0	0.0	1.0/
12	-813120000	0.0	0.0	1.0/
12	-813130000	0.0	0.0	1.0/
12	-813140000	0.0	0.0	1.0/
12	-813150000	0.0	0.0	1.0/
12	-813160000	0.0	0.0	1.0/
12	-813170000	0.0	0.0	1.0/
12	-813180000	0.0	0.0	1.0/
12	-813190000	0.0	0.0	1.0/
12	-813200000	0.0	0.0	1.0/
10	813200000	-1.0	0.0	0.0/
10	813210000	-1.0	0.0	0.0/
10	813220000	-1.0	0.0	0.0/
10	813230000	-1.0	0.0	0.0/
10	813240000	-1.0	0.0	0.0/
10	813250000	-1.0	0.0	0.0/
10	813260000	-1.0	0.0	0.0/
10	813270000	-1.0	0.0	0.0/
10	813280000	-1.0	0.0	0.0/
10	813290000	-1.0	0.0	0.0/
8	-813210000	-1.0	0.0	0.0/
8	-813220000	-1.0	0.0	0.0/
6	-813230000	-1.0	0.0	0.0/
6	-813240000	-1.0	0.0	0.0/
6	-813250000	-1.0	0.0	0.0/
6	-813260000	-1.0	0.0	0.0/
6	-813270000	-1.0	0.0	0.0/
6	-813280000	-1.0	0.0	0.0/
6	-813290000	-1.0	0.0	0.0/
6	-813300000	-1.0	0.0	0.0/
4	900000000	0.0	-1.0	0.0/
4	901010000	0.0	-1.0	0.0/
4	901020000	0.0	-1.0	0.0/
4	902000000	0.0	-1.0	0.0/
4	903010000	0.0	-1.0	0.0/
2	-901010000	0.0	-1.0	0.0/
2	-902000000	0.0	-1.0	0.0/
2	-903010000	0.0	-1.0	0.0/
2	-903020000	0.0	-1.0	0.0/

99999/
\$STEPS TSTEP(1)=0.001, 1.0, -1, -1\$

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TR-5364-2
Revision 0

 TELEDYNE ENGINEERING SERVICES

9.1.2.3 Unit 2 - Quarter Model

001030000
0000200100
(001030000)
0000200100

\$PIPES
IN LINE=3,KBLOCK=601,KPIPE=0,KPLOT(1)=1,KWAVE=1,
KPRINT=-1,KPNV=1,KSTEP=3,NDRQPV=1010000,15010000\$

1	00200000	-1.0	0.0	0.0/
2	-00400000	-1.0	0.0	0.0/
3	00400000	0.0	-1.0	0.0/
3	005010000	0.0	-1.0	0.0/
3	005020000	0.0	-1.0	0.0/
3	005040000	0.0	-1.0	0.0/
3	005050000	0.0	-1.0	0.0/
3	005060000	0.0	-1.0	0.0/
4	-005010000	0.0	-1.0	0.0/
4	-005020000	0.0	-1.0	0.0/
4	-005030000	0.0	-1.0	0.0/
4	-005040000	0.0	-1.0	0.0/
4	-005050000	0.0	-1.0	0.0/
4	-005060000	0.0	-1.0	0.0/
4	-005070000	0.0	-1.0	0.0/
5	005070000	-1.0	0.0	0.0/
5	005080000	-1.0	0.0	0.0/
5	005090000	-1.0	0.0	0.0/
6	-005080000	-1.0	0.0	0.0/
6	-005090000	-1.0	0.0	0.0/
6	-005100000	-1.0	0.0	0.0/
7	005100000	0.0	1.0	0.0/
7	005110000	0.0	1.0	0.0/
7	005120000	0.0	1.0	0.0/
7	005130000	0.0	1.0	0.0/
7	005140000	0.0	1.0	0.0/
7	005150000	0.0	1.0	0.0/
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7	005190000	0.0	1.0	0.0/
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8	-005120000	0.0	1.0	0.0/
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8	-005140000	0.0	1.0	0.0/
8	-005150000	0.0	1.0	0.0/
8	-005160000	0.0	1.0	0.0/
8	-005170000	0.0	1.0	0.0/
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11	007070000	0.0	-1.0	0.0/
11	007080000	0.0	-1.0	0.0/
11	007090000	0.0	-1.0	0.0/

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CHKD. BY LOS DATE 2-9-83

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31	-011080000	0.0	-1.0	0.0/
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36	011250000	-.316	-.707	-.948/
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 Revision 0

TELEDYNE
 ENGINEERING SERVICES

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39	-011410000	0.0	-1.0	0.0/
39	-011420000	0.0	-1.0	0.0/
39	-011430000	0.0	-1.0	0.0/
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21

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44	011820000	-1.0	0.0	0.0/
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53 -014000000 1.0 0.0 0.0/

99999/

\$\$STEPS TSTEP(1)=0.001,0.600\$

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Revision 0.

 **TELEDYNE**
ENGINEERING SERVICE



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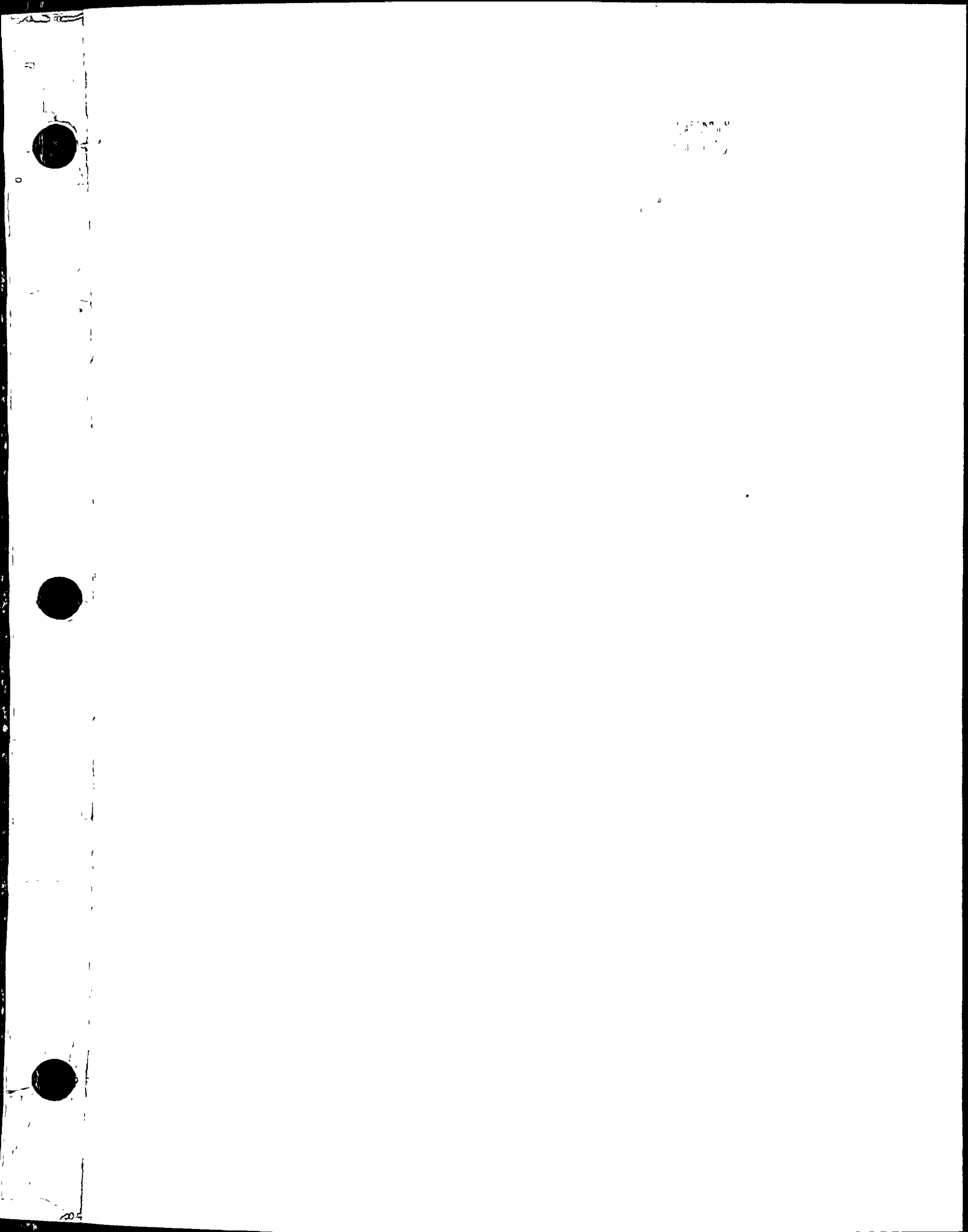
TECHNICAL REPORT TR-5364-1 M
REVISION 0

BOOK 2 OF 15

DONALD C. COOK NUCLEAR GENERATING PLANT

ANALYSIS OF PRESSURIZER SAFETY/RELIEF VALVES
DISCHARGE PIPING SYSTEM PER NUREG 0737, I.L.D.1,
UNIT 1

JUNE 6, 1983



AMERICAN ELECTRIC POWER SERVICE CORPORATION
2 BROADWAY
NEW YORK, NEW YORK 10004

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REVISION 0

BOOK 2 OF 15

DONALD C. COOK NUCLEAR GENERATING STATION

ANALYSIS OF PRESSURIZER SAFETY/RELIEF VALVES
DISCHARGE PIPING SYSTEM PER NUREG 0737, II. D.1,
UNIT 1

JUNE 6, 1983

TELEDYNE ENGINEERING SERVICES

130 SECOND AVENUE
WALTHAM, MASSACHUSETTS 02254
617-890-3350

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4.8 Force Time History Plots

The following are force versus time plots for each pipe segment at a node point described by the structural model. A drawing indicating force placement precedes each set (Unit 1, Unit 2). Since the force time histories were plotted after balancing and merging (i.e. SAP2SAP and MERGE), each plot is unbalanced force versus time from 0.0 to 0.6 seconds. The problem was run to 0.6 seconds because all significant forces in the area of concern (piping about the PORV's) had diminished in this time.

Unit 1 (PORV)	71 segments
Quarter Model	26 segments

Plot Set

Transient

4.8.1 Unit 1	Condensate/Steam Case (75% of model)
4.8.2 Unit 1	400° Solid Liquid Case
4.8.3 Quarter Model	Cold Loop Seal/Steam Case

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4.8.1 Unit 1 - Condensate/Steam Case (75% of model)

BY RHM DATE 4-14-83
CHKD. BY LBS DATE 4-14-83

UNIT 1 STRUCTURAL NODE POINTS
PURV SECTION

SHEET NO. 1 OF 3
PROJ. NO. 5364

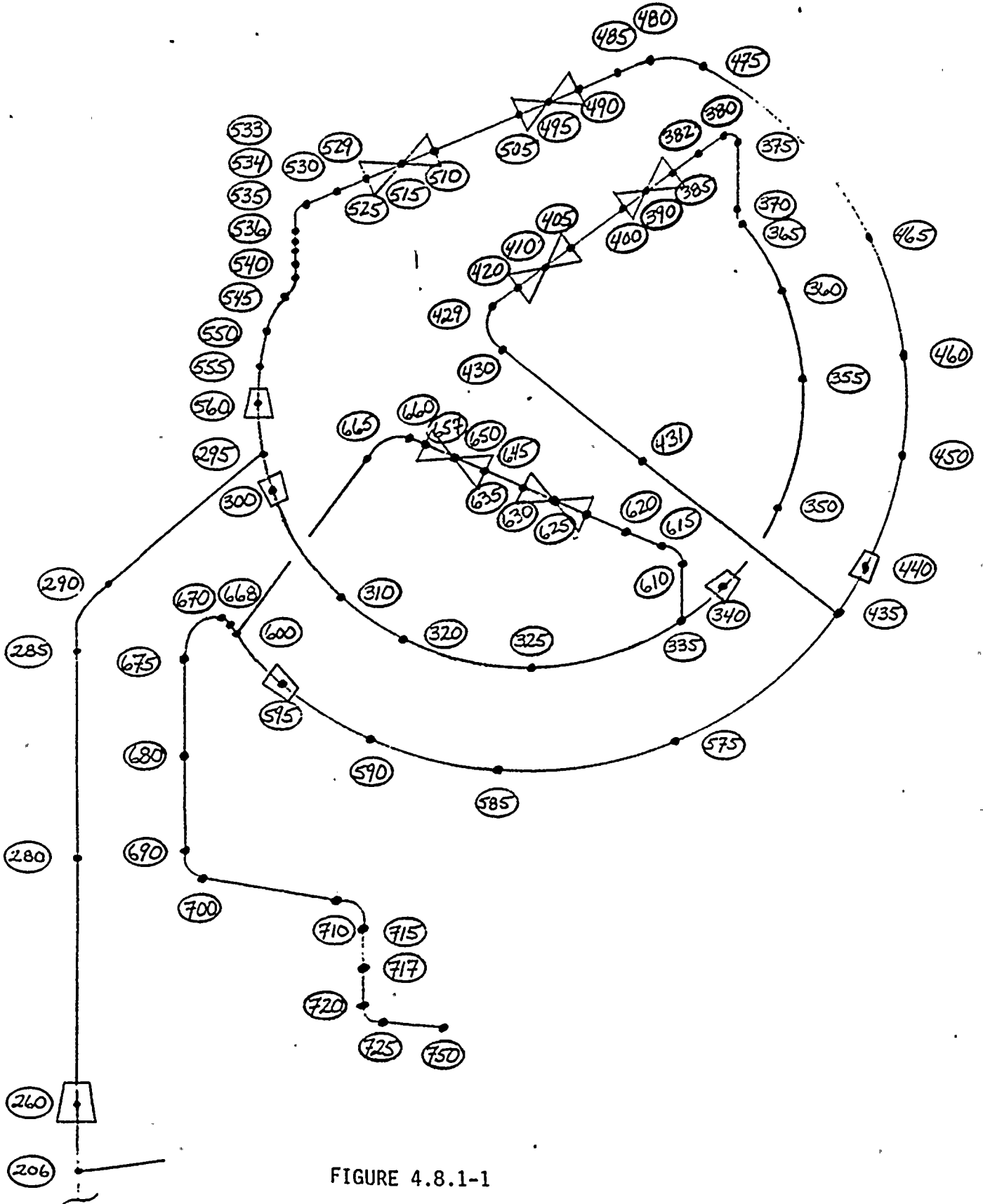


FIGURE 4.8.1-1

BY RAM DATE 4-14-83
CHKD. BY LBS DATE 4-14-83

UNIT 1 STRUCTURAL NODES POINTS
MAIN ARCS

SHEET NO. 2 OF 3
PROJ. NO. 5364

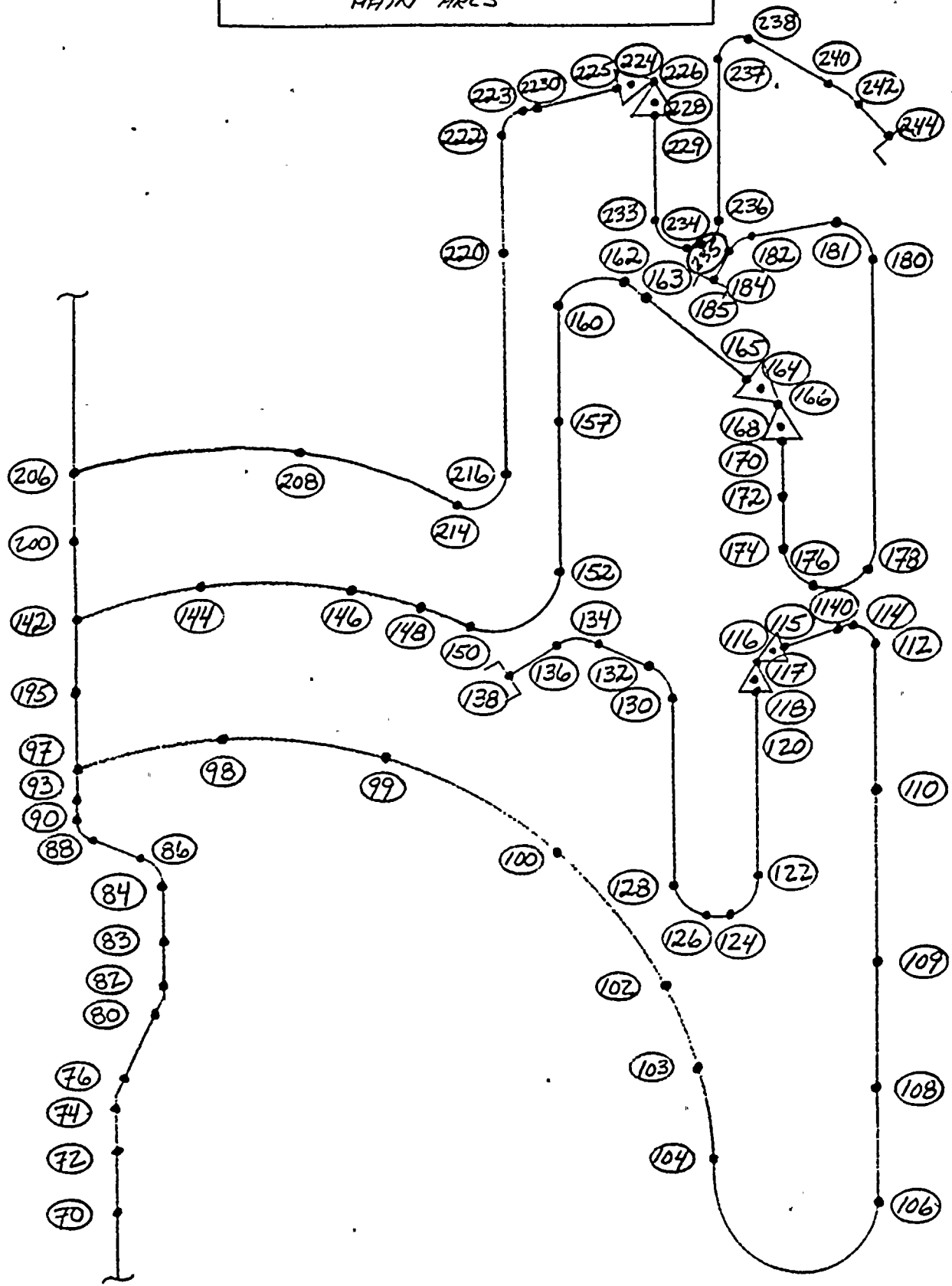


FIGURE 4.8.1-2

BY RAM DATE 4-14-83
CHKD. BY LBS DATE 4-14-83

UNIT 1 STRUCTURAL NODE POINTS
DOWNSTREAM (12 IN)

SHEET NO. 2 OF 3
PROJ. NO. 5364

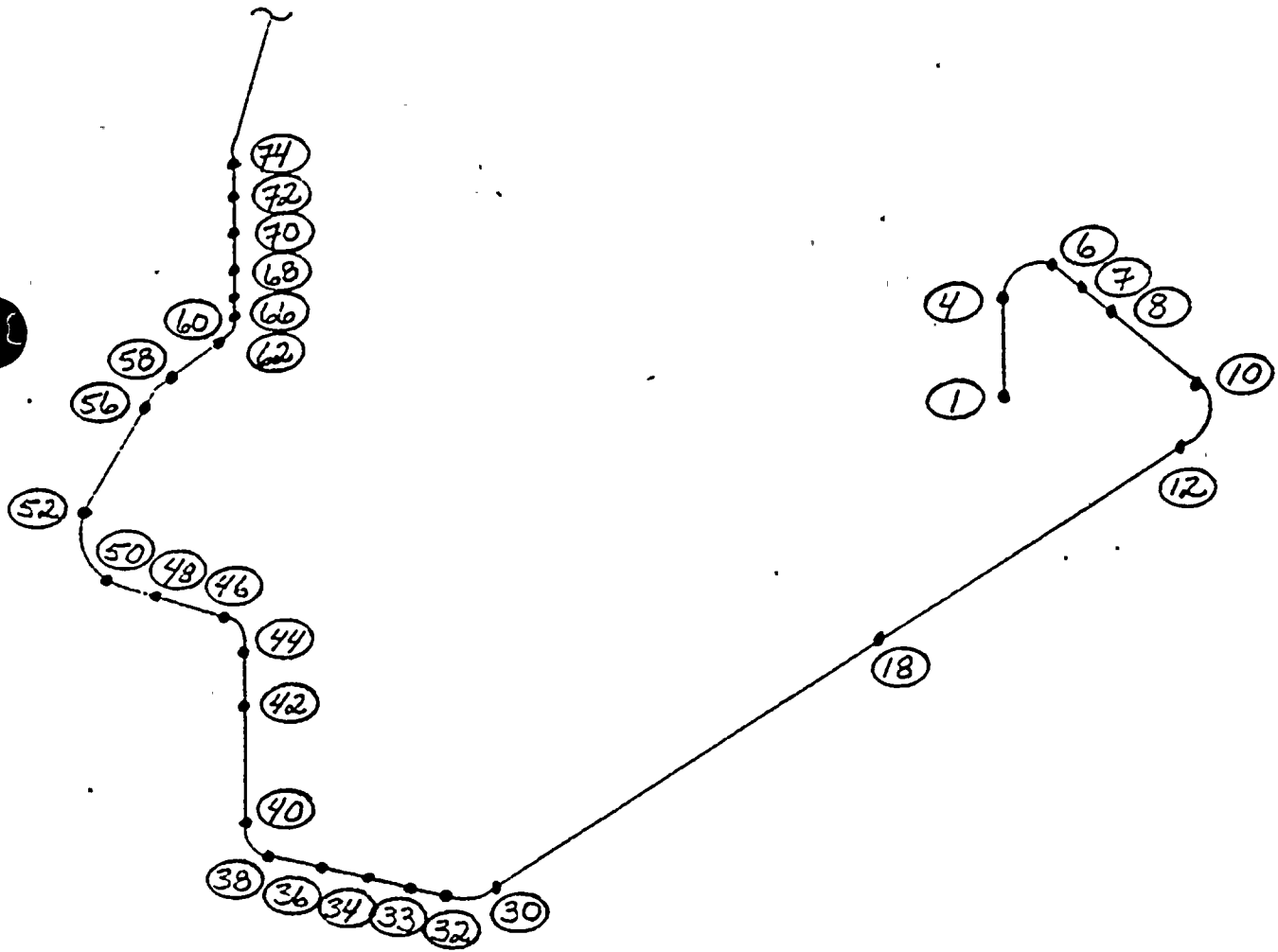


FIGURE 4.8.1-3



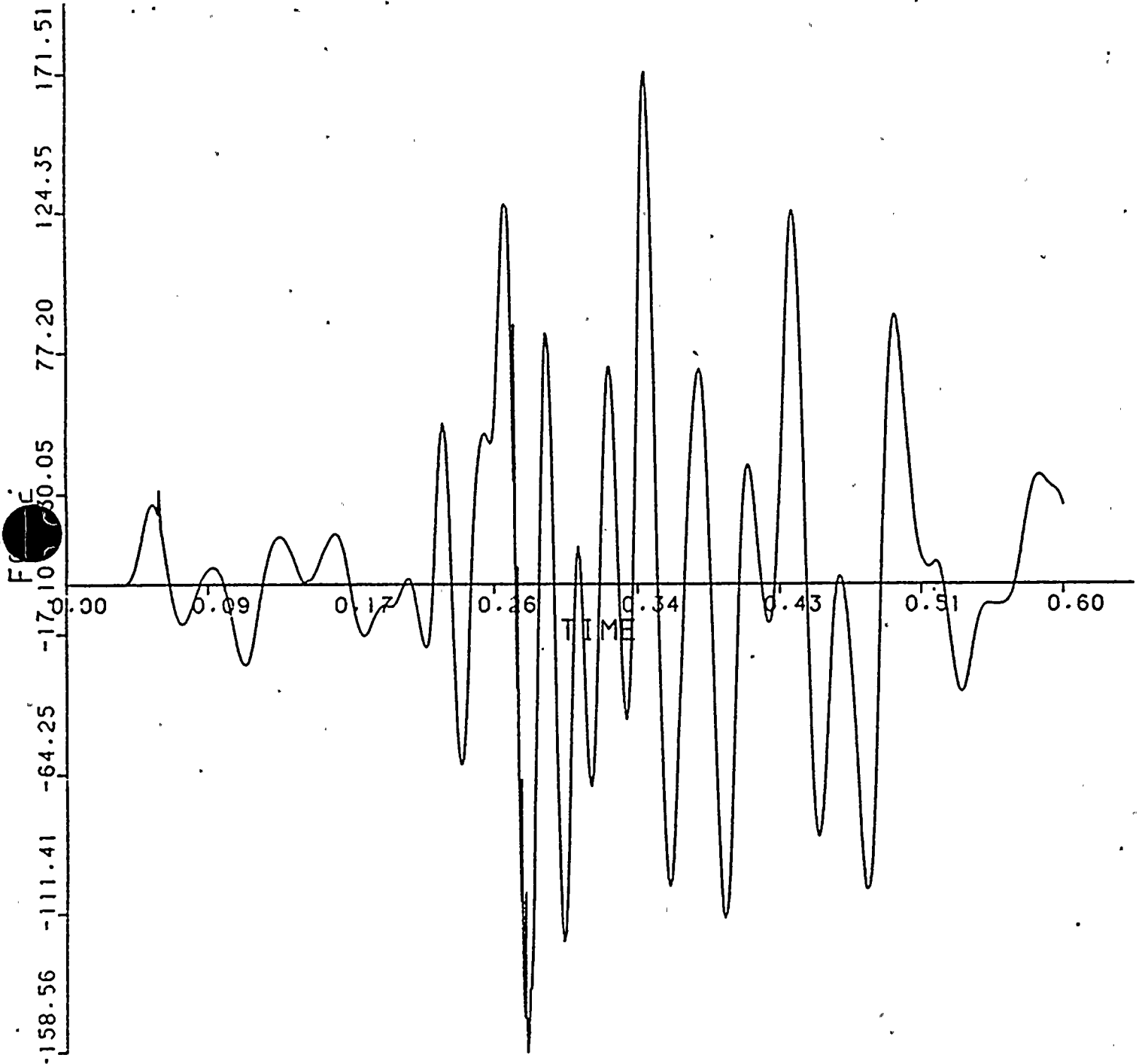
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YELLOW LOOP SEAL - YELPSL.TMP

TIME/FORCE TABLE 1, MAGNITUDE AT NODE POINT

109



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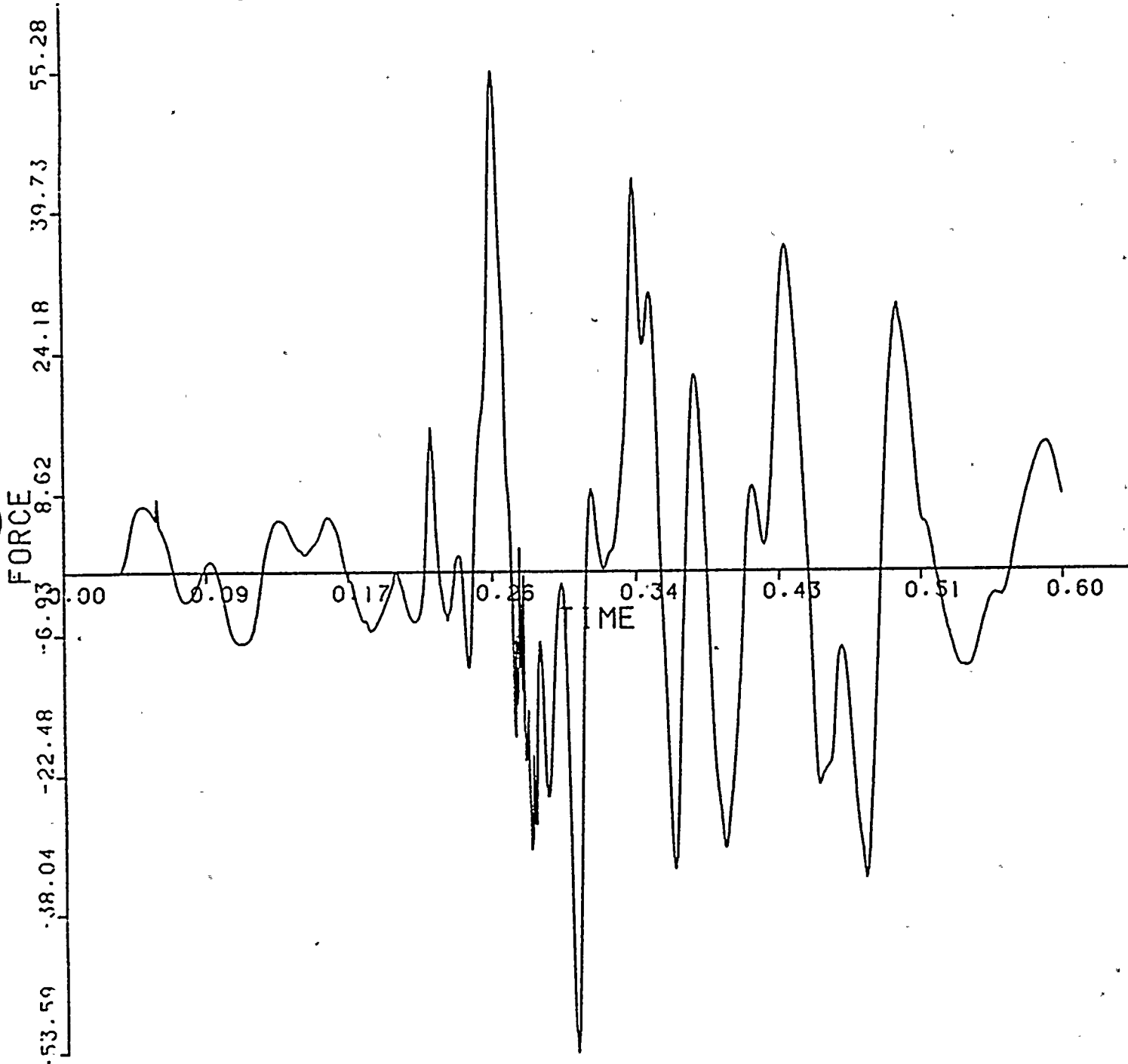
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TIME/FORCE TABLE 2. MAGNITUDE AT NODE POINT



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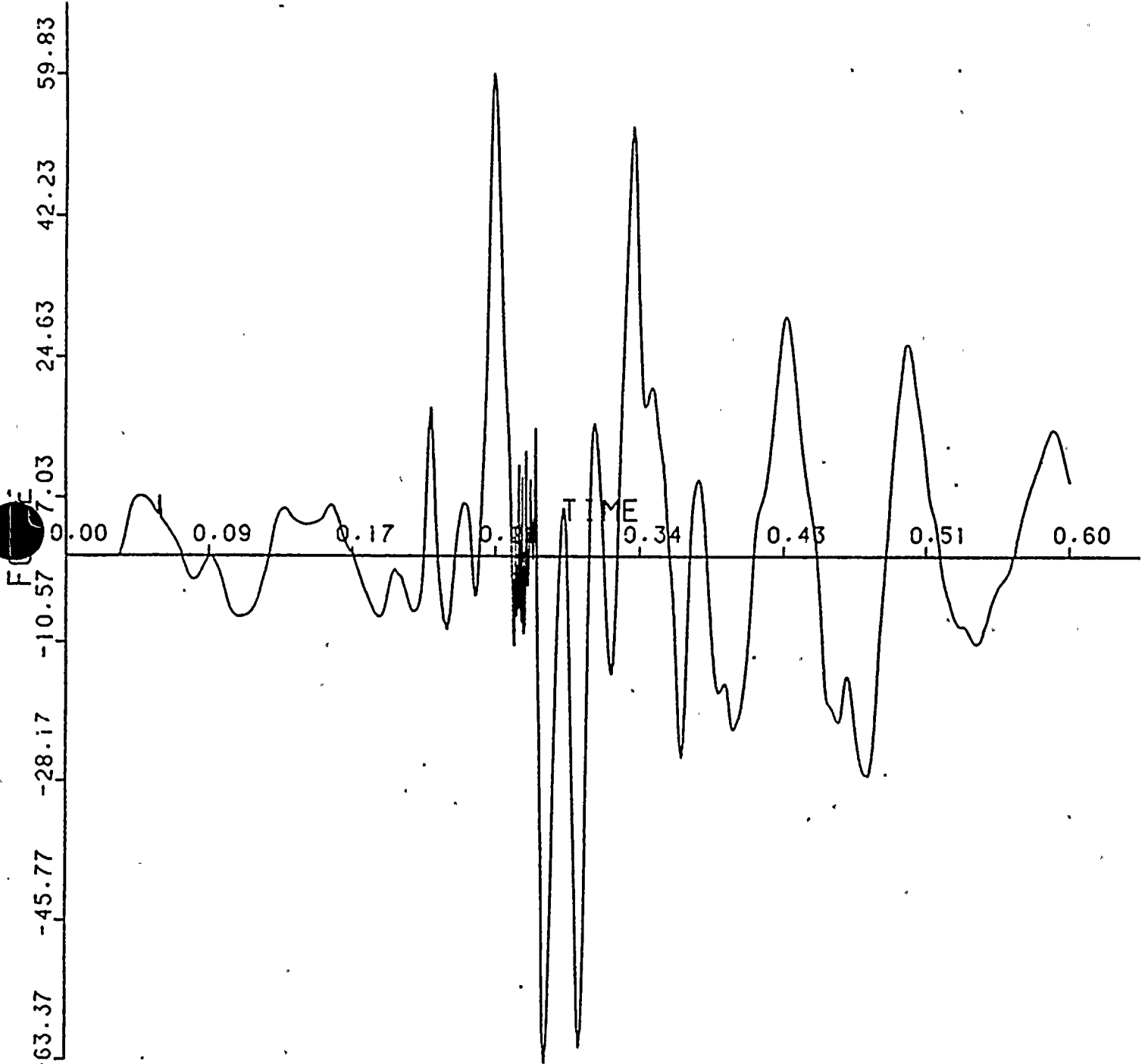
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TIME/FORCE TABLE 3, MAGNITUDE AT NODE POINT

103



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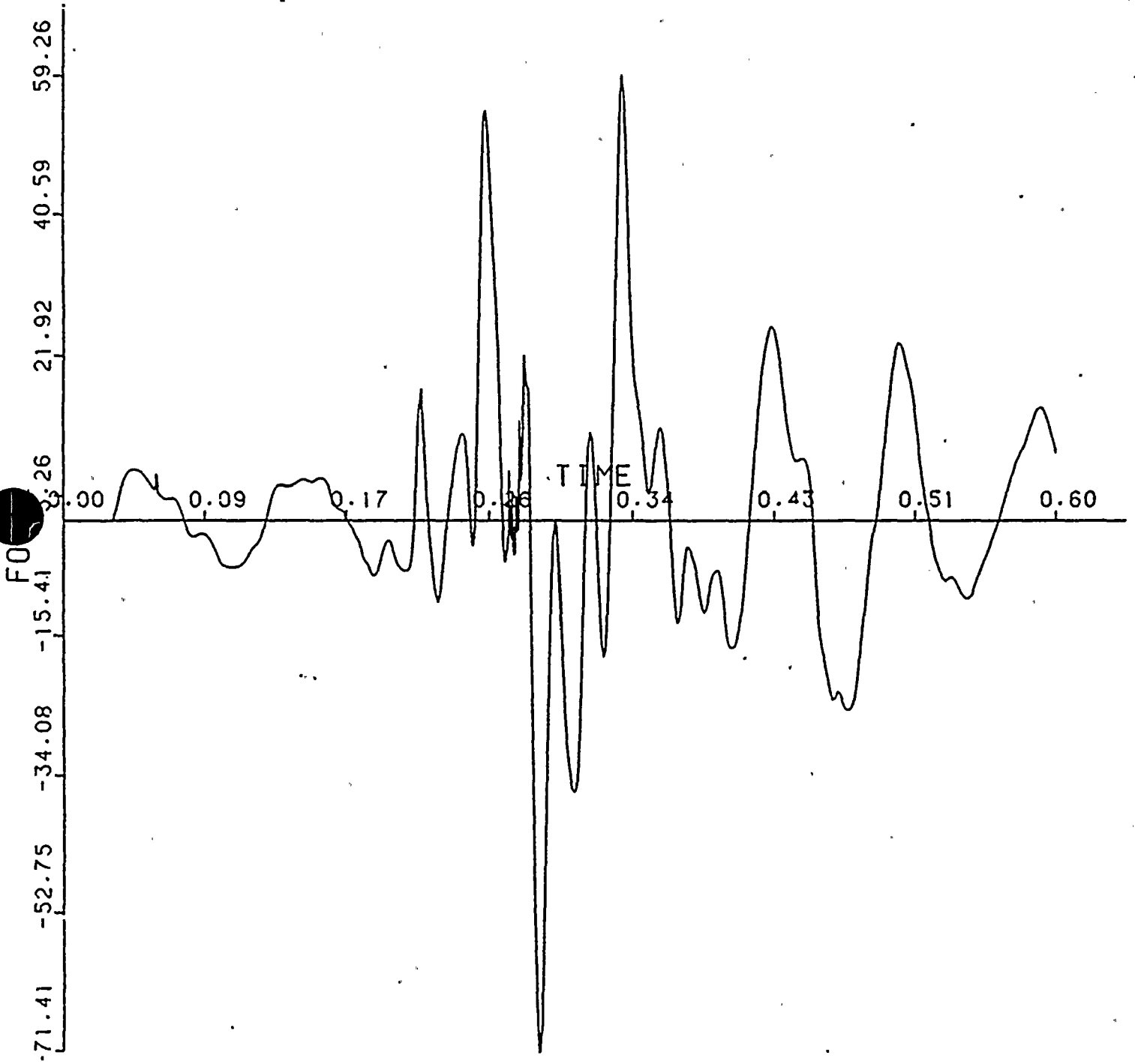
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YELLOW LOOP SEAL - YELLPSL.TMP

TIME/FORCE TABLE 4. MAGNITUDE AT NODE POINT

102



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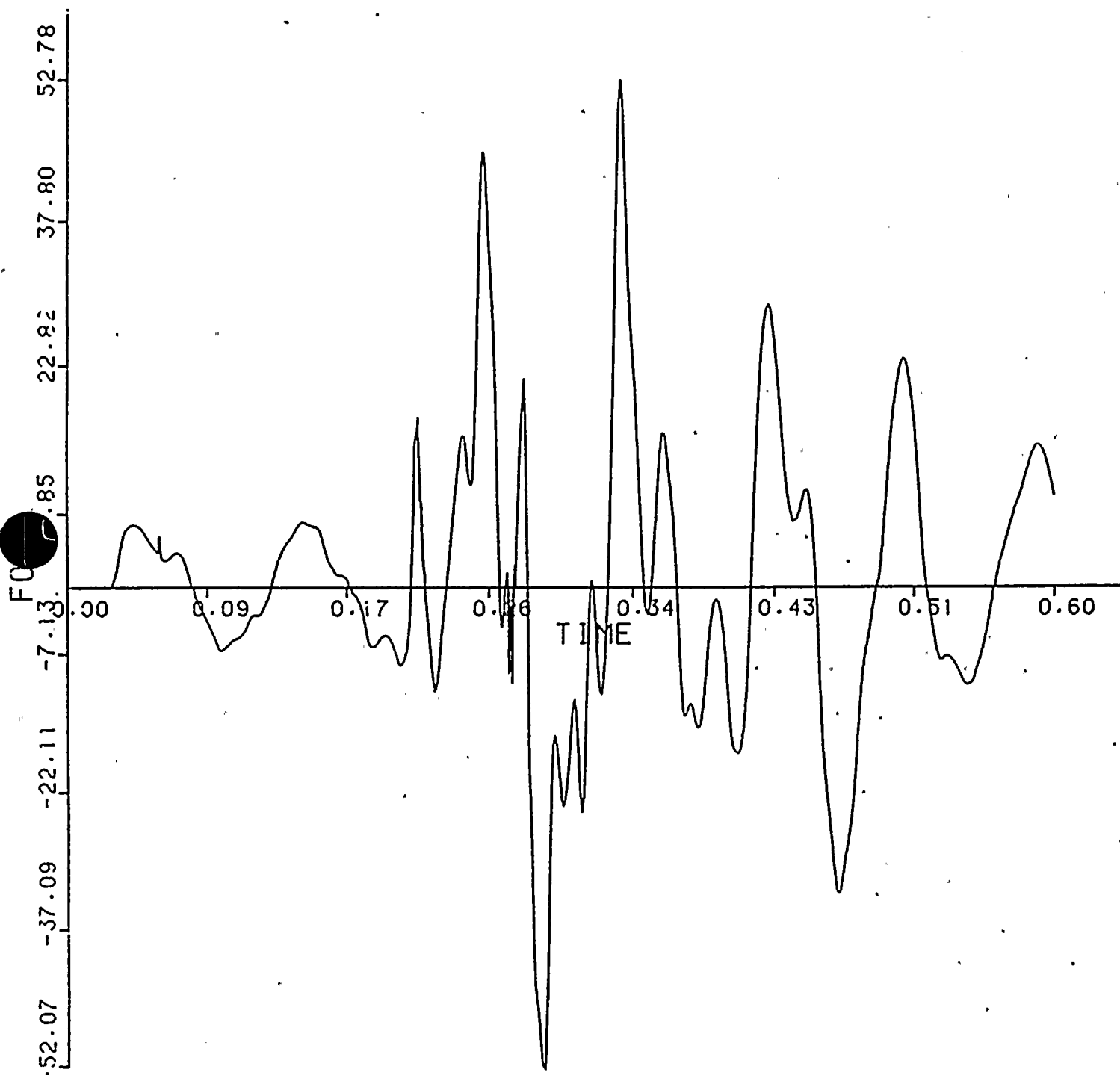
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YELLOW LOOP SEAL - YELLPSL.TMP

TIME/FORCE TABLE 5, MAGNITUDE AT NODE POINT

100



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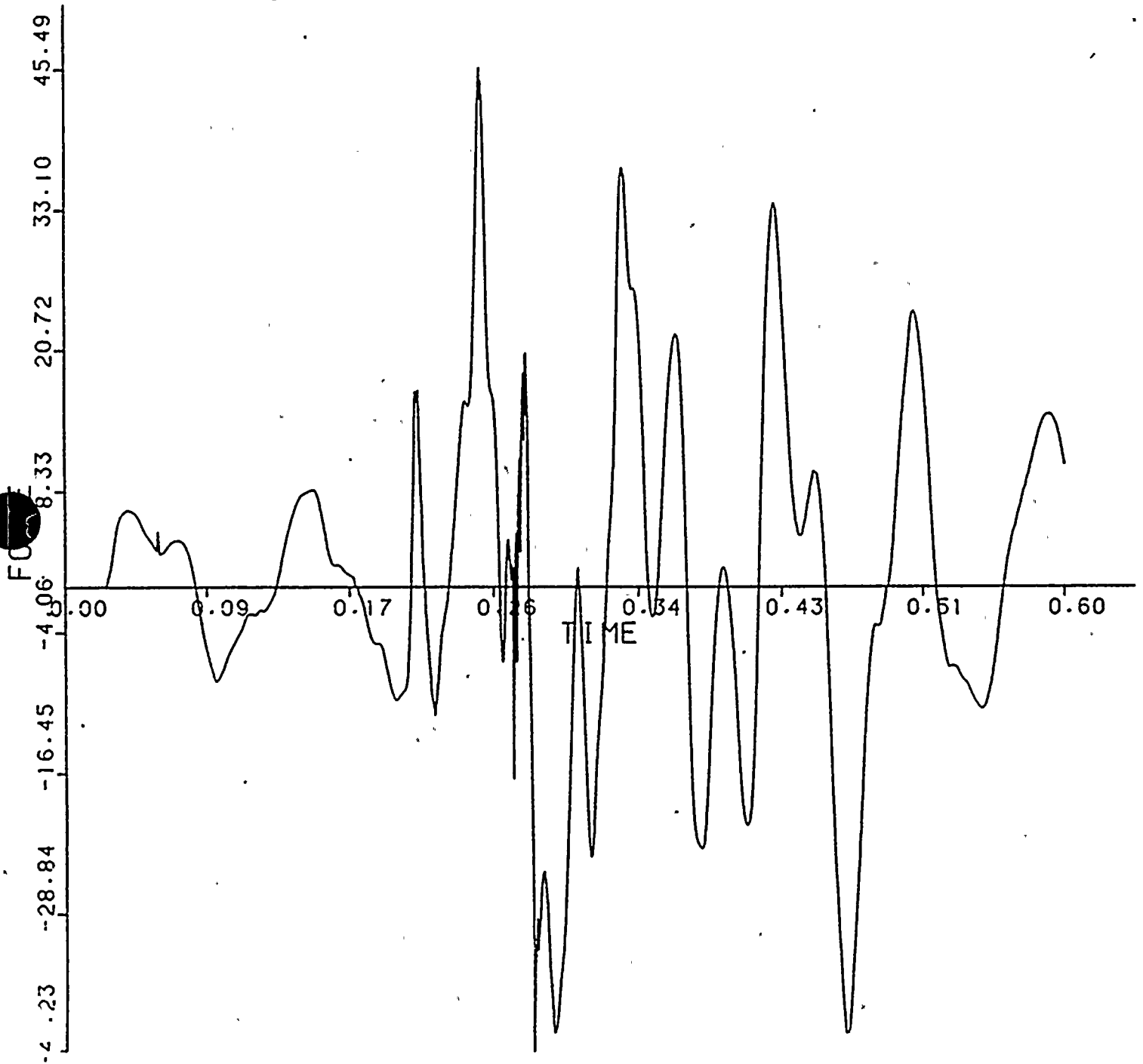
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YELLOW LOOP SEAL - YELLPSL.TMP

TIME/FORCE TABLE 6. MAGNITUDE AT NODE POINT

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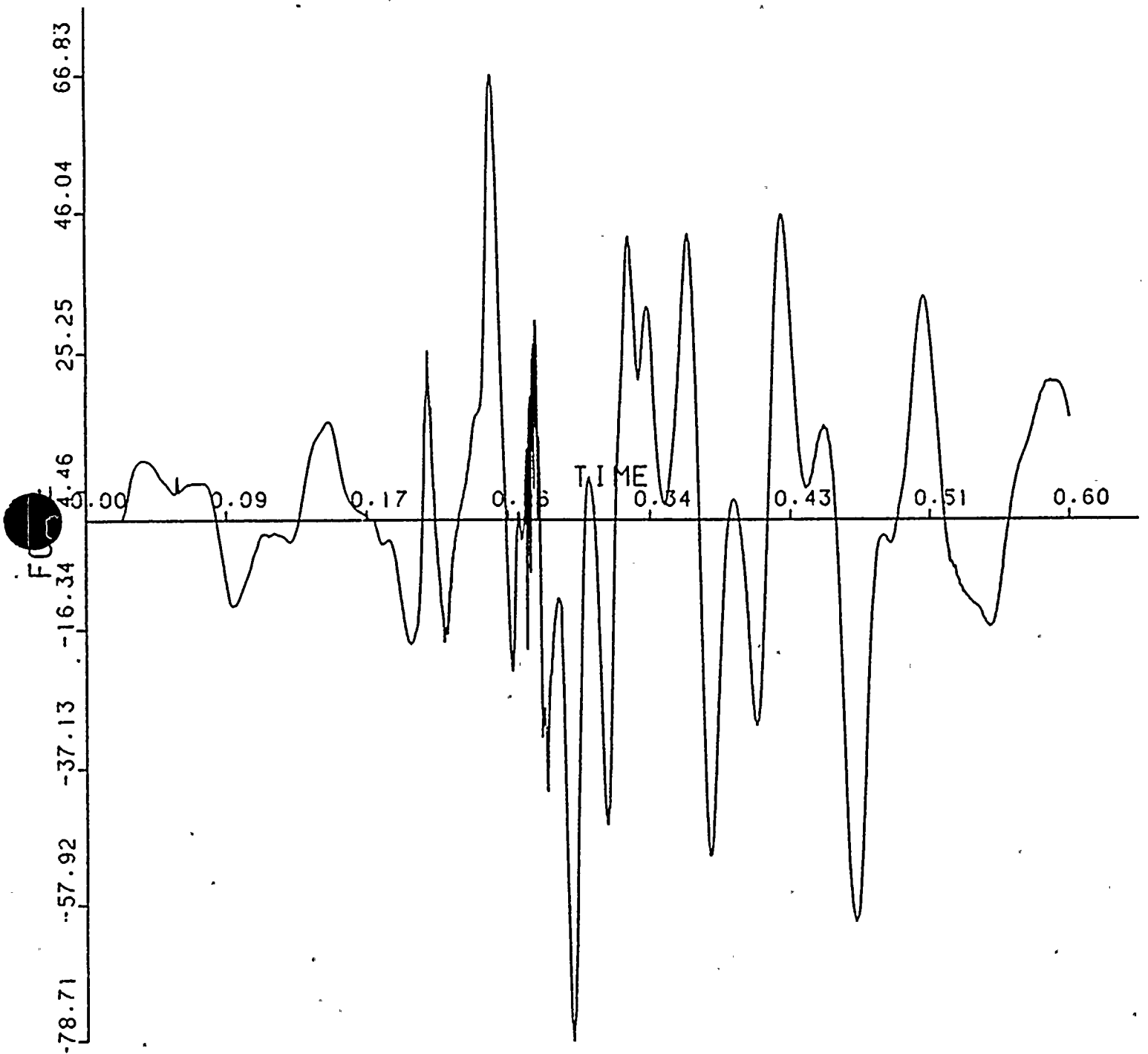
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YELLOW LOOP SEAL - YELPSL.TMP

TIME/FORCE TABLE 7, MAGNITUDE AT NODE POINT 98



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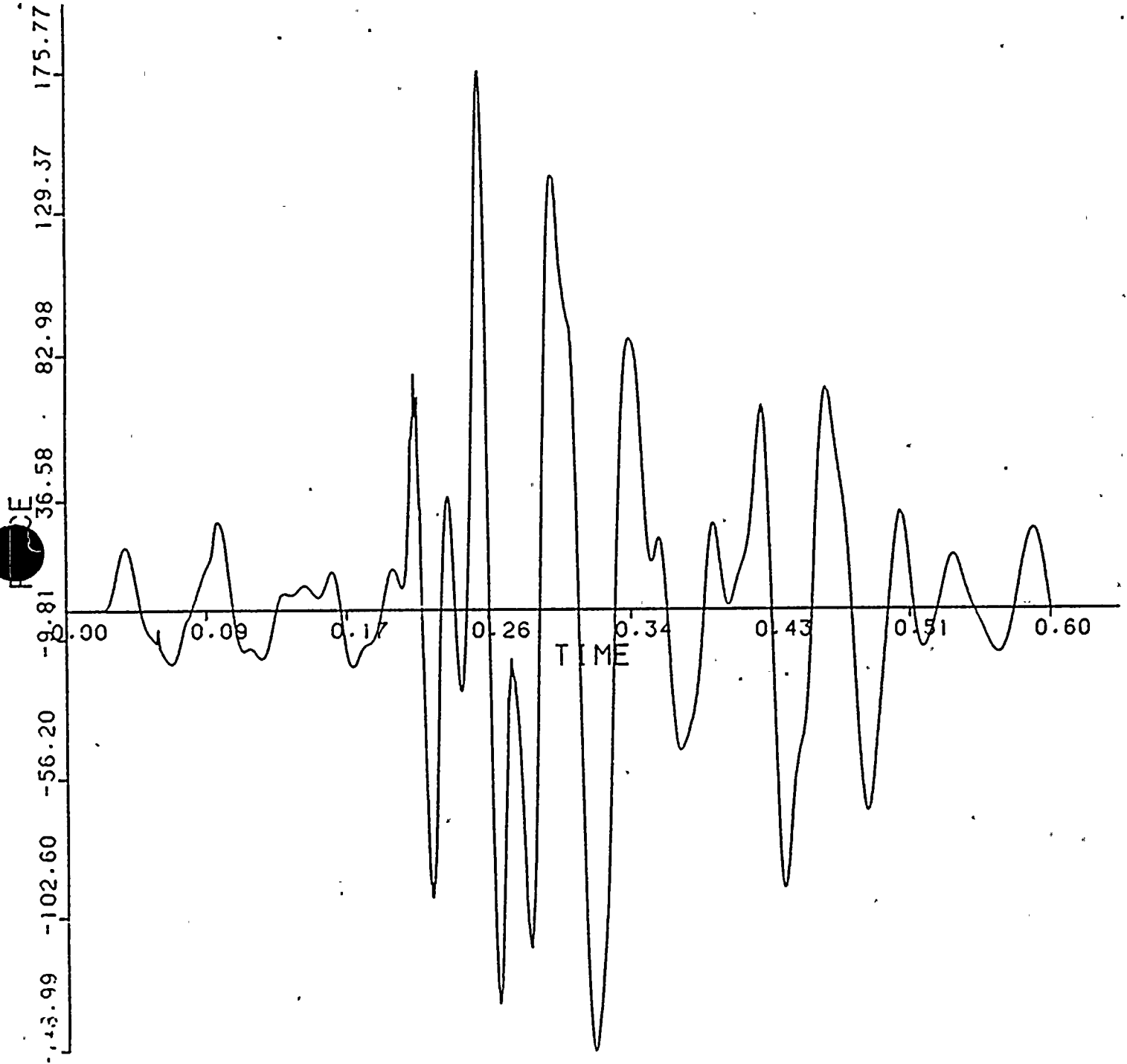
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YELLOW LOOP SEAL - YELLPSL.TMP

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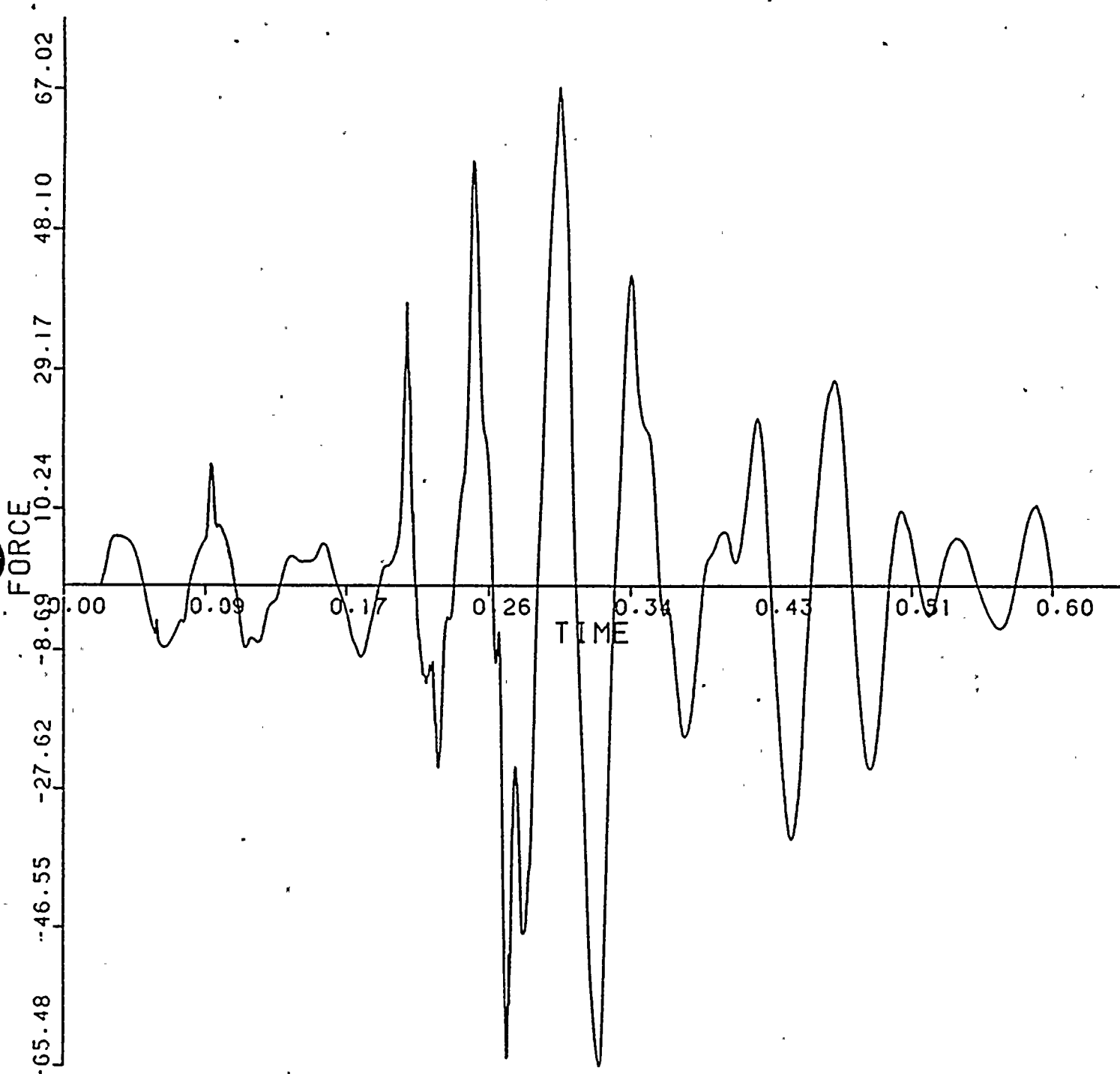
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YELLOW LOOP SEAL - YELLPSL.TMP

TIME/FORCE TABLE 9. MAGNITUDE AT NODE POINT

214

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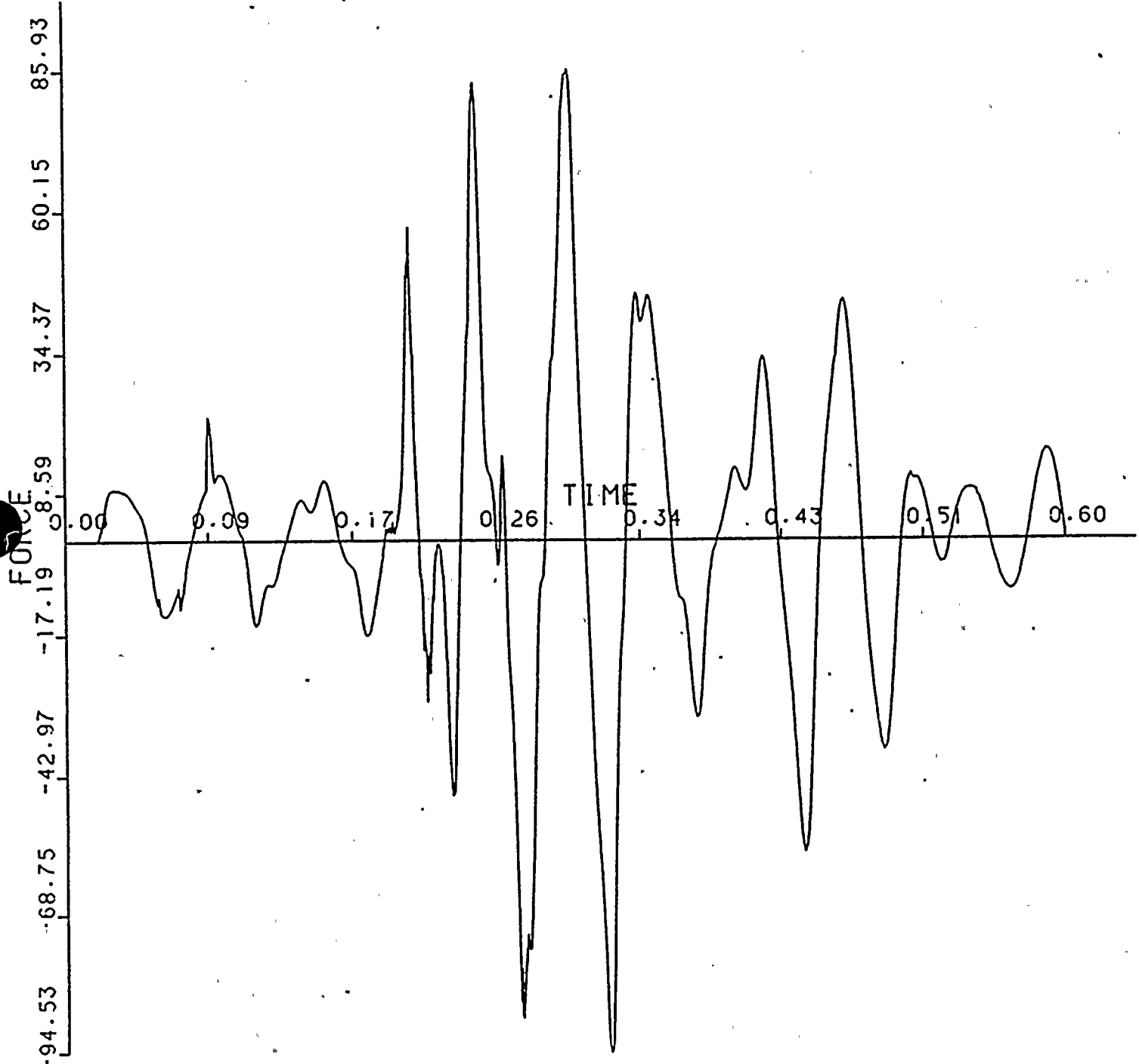
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YELLOW LOOP SEAL - YELLPSL.TMP

TIME/FORCE TABLE 10. MAGNITUDE AT NODE POINT

208



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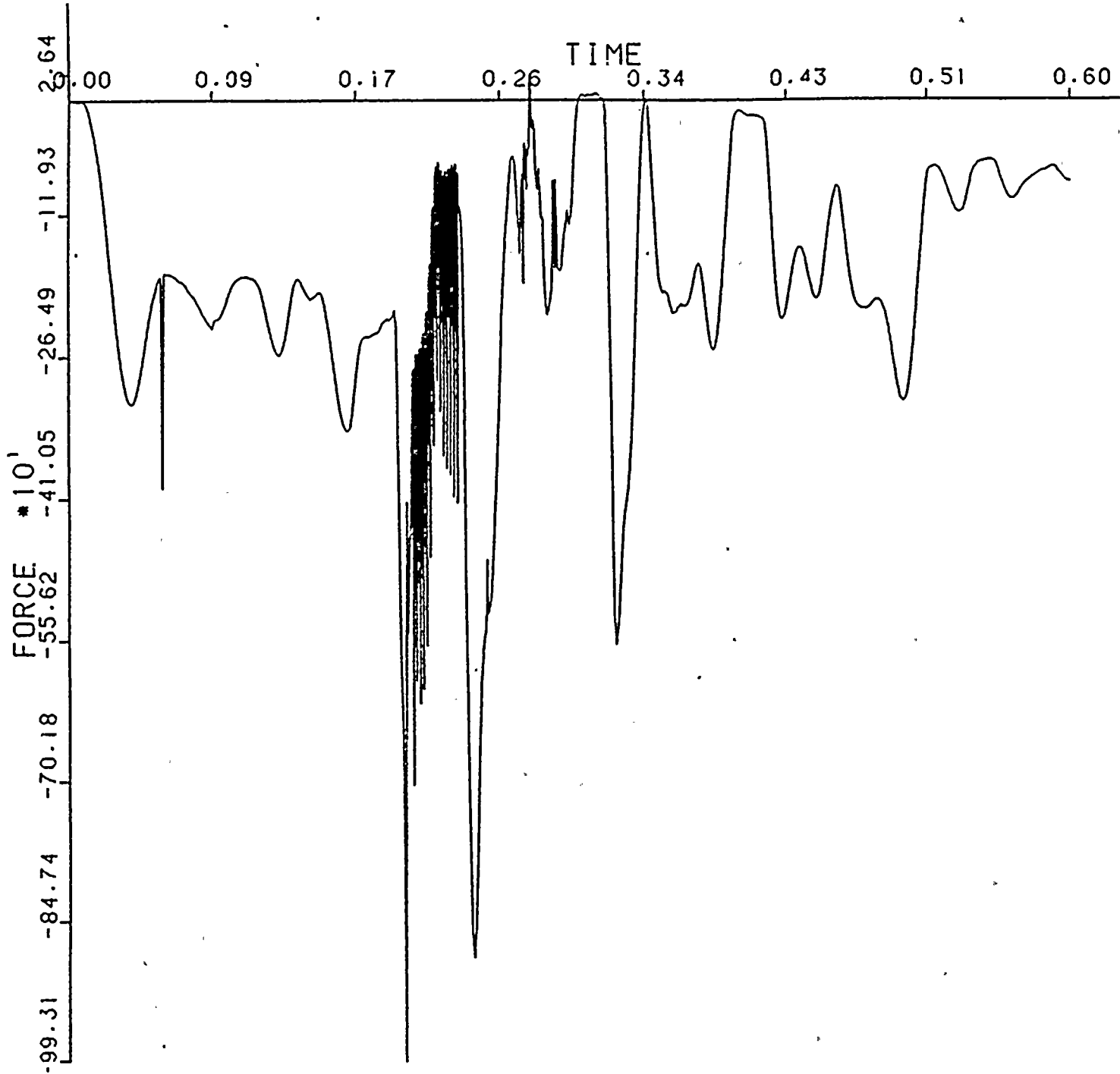
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TIME/FORCE TABLE 11. MAGNITUDE AT NODE POINT



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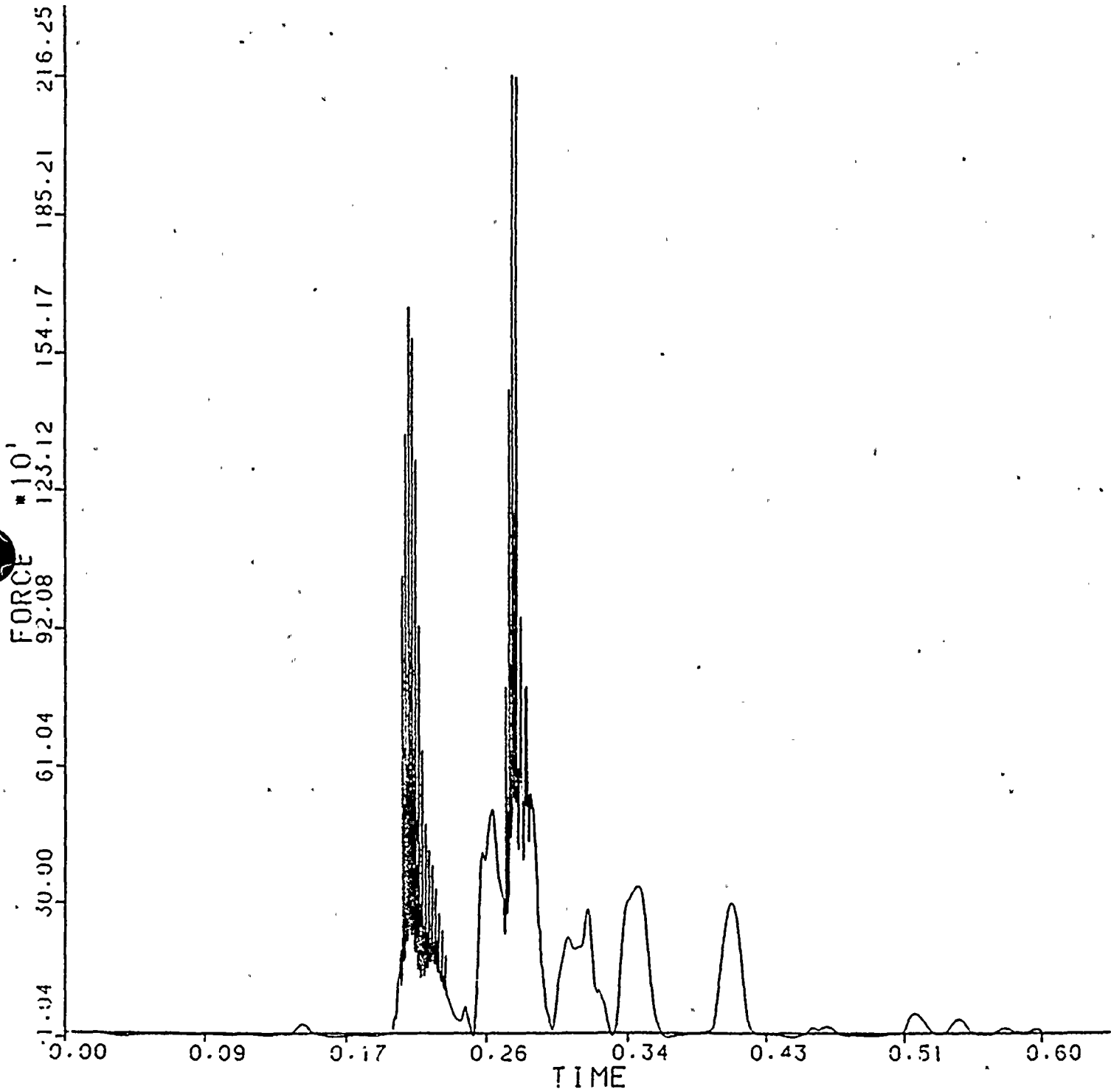
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TIME/FORCE TABLE

12. MAGNITUDE AT NODE POINT



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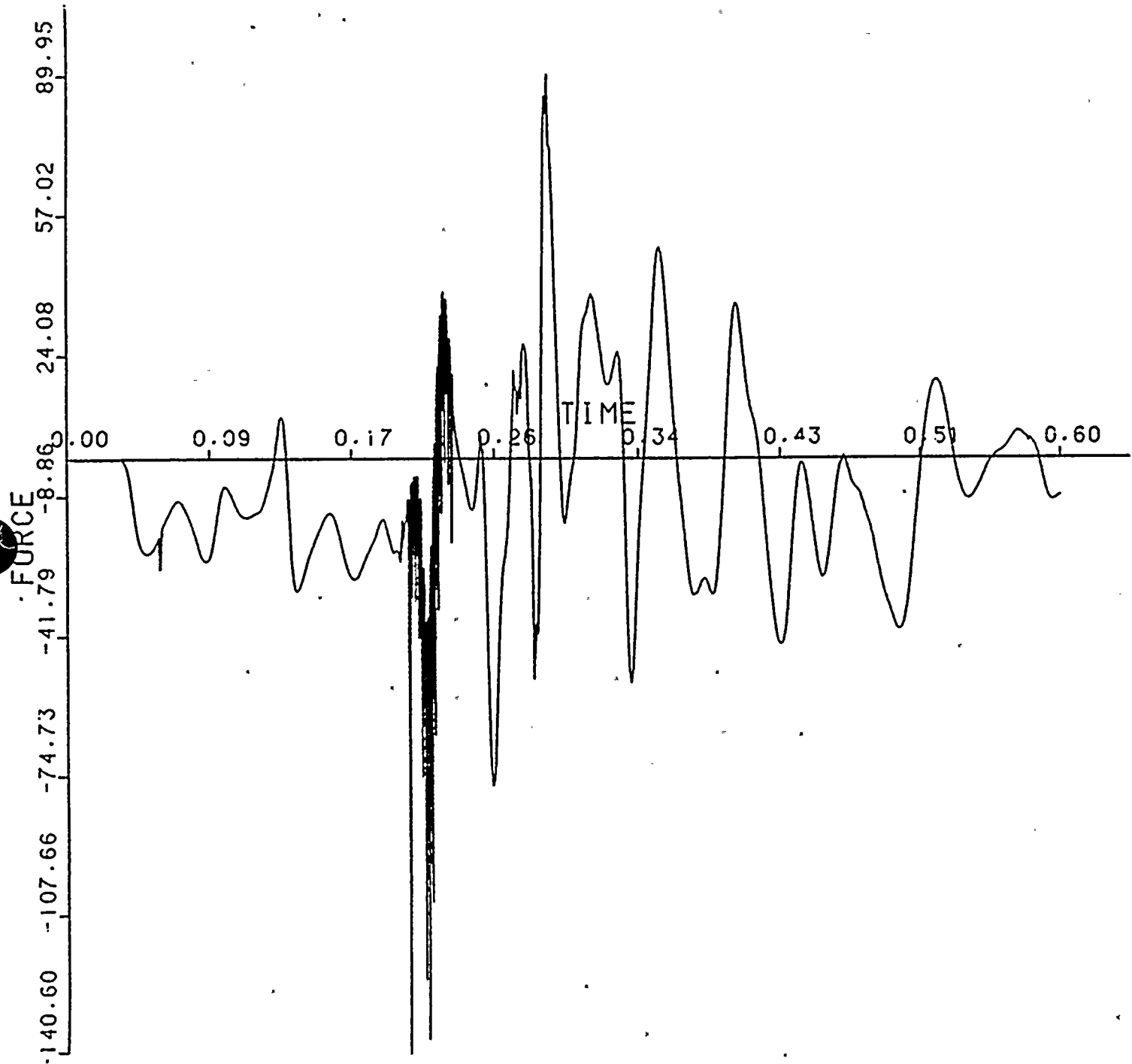
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YELLOW LOOP SEAL - YELLPSL.TMP

TIME/FORCE TABLE 13. MAGNITUDE AT NODE POINT

88



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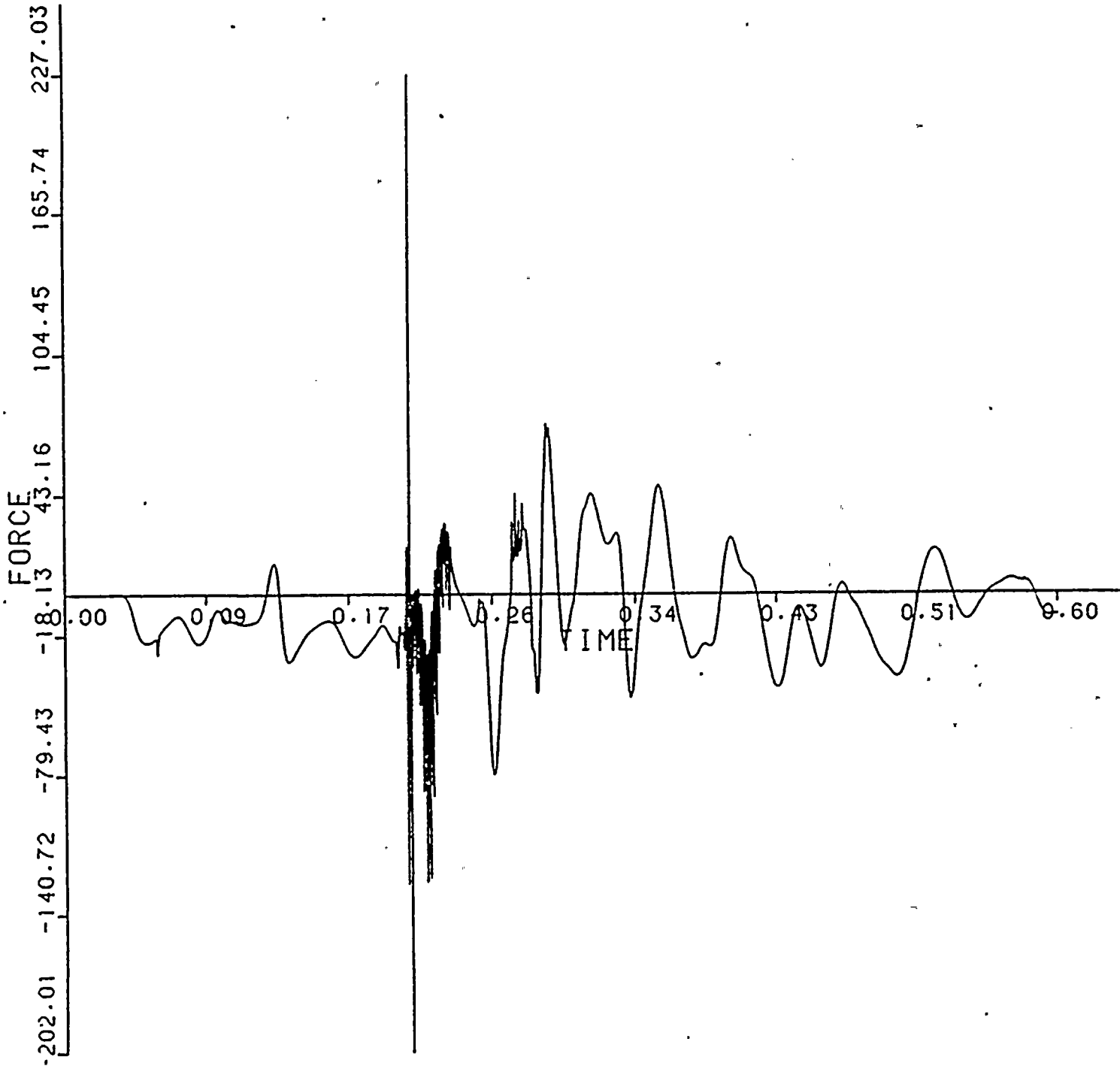
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83



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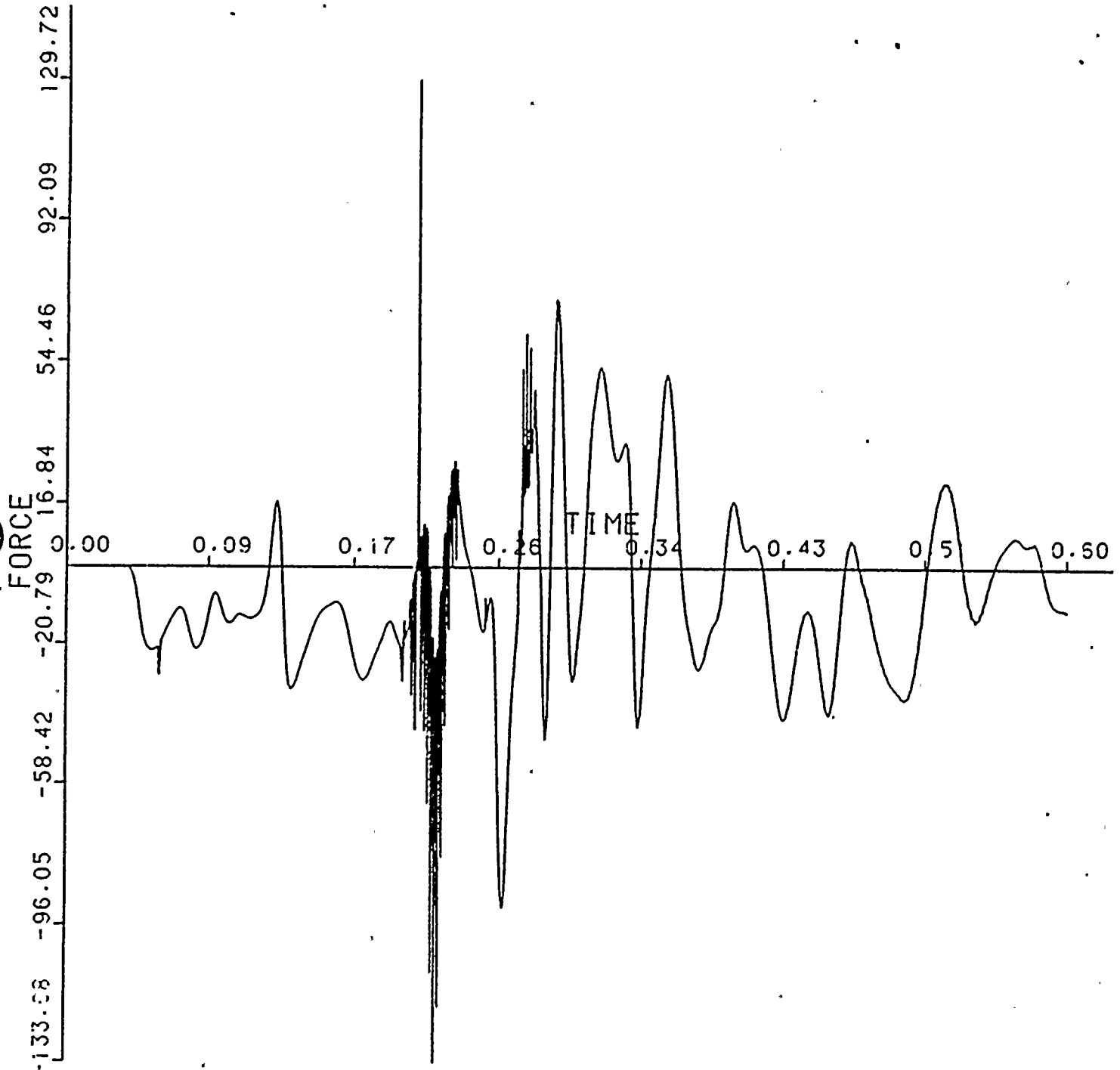
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80



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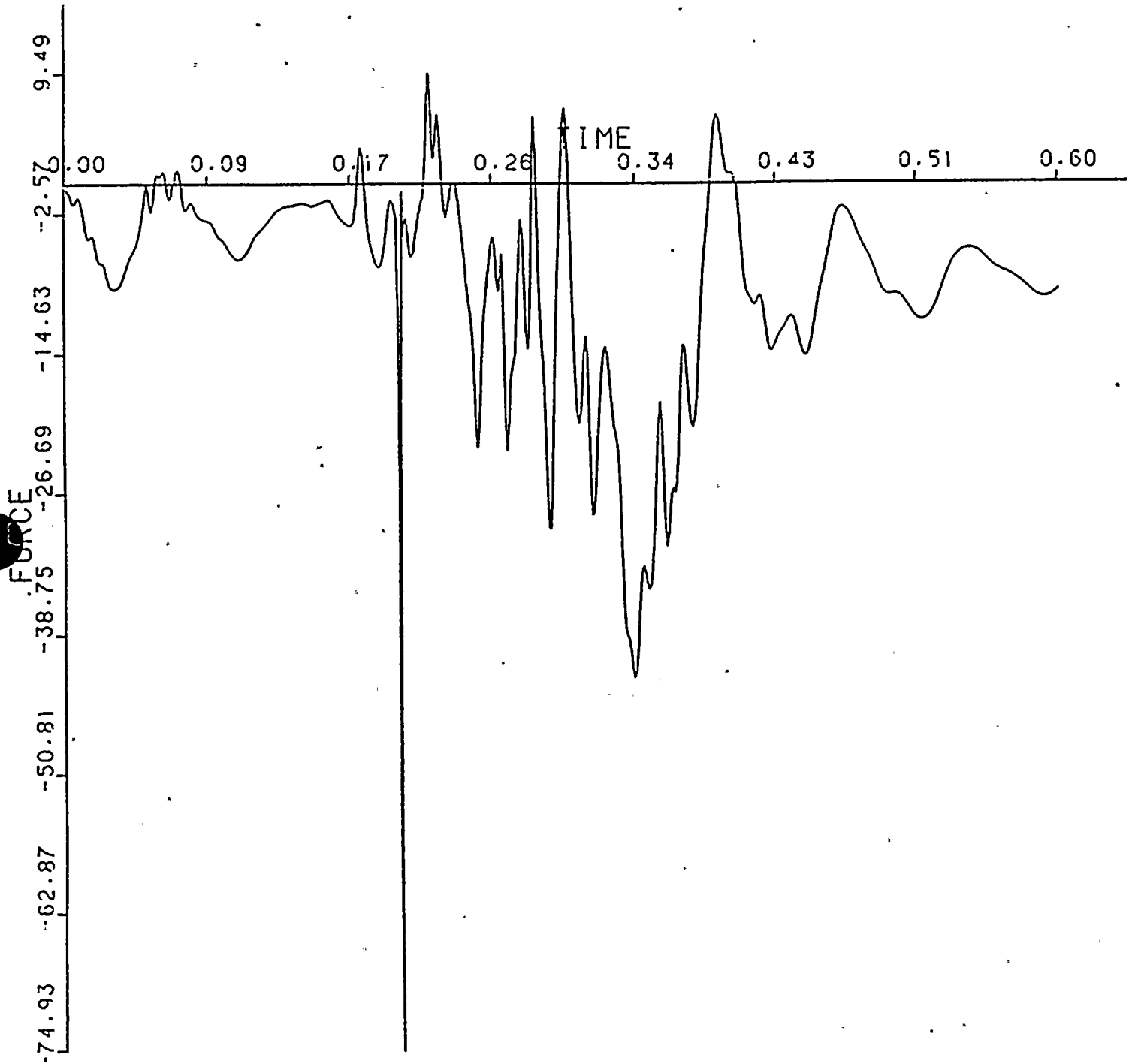
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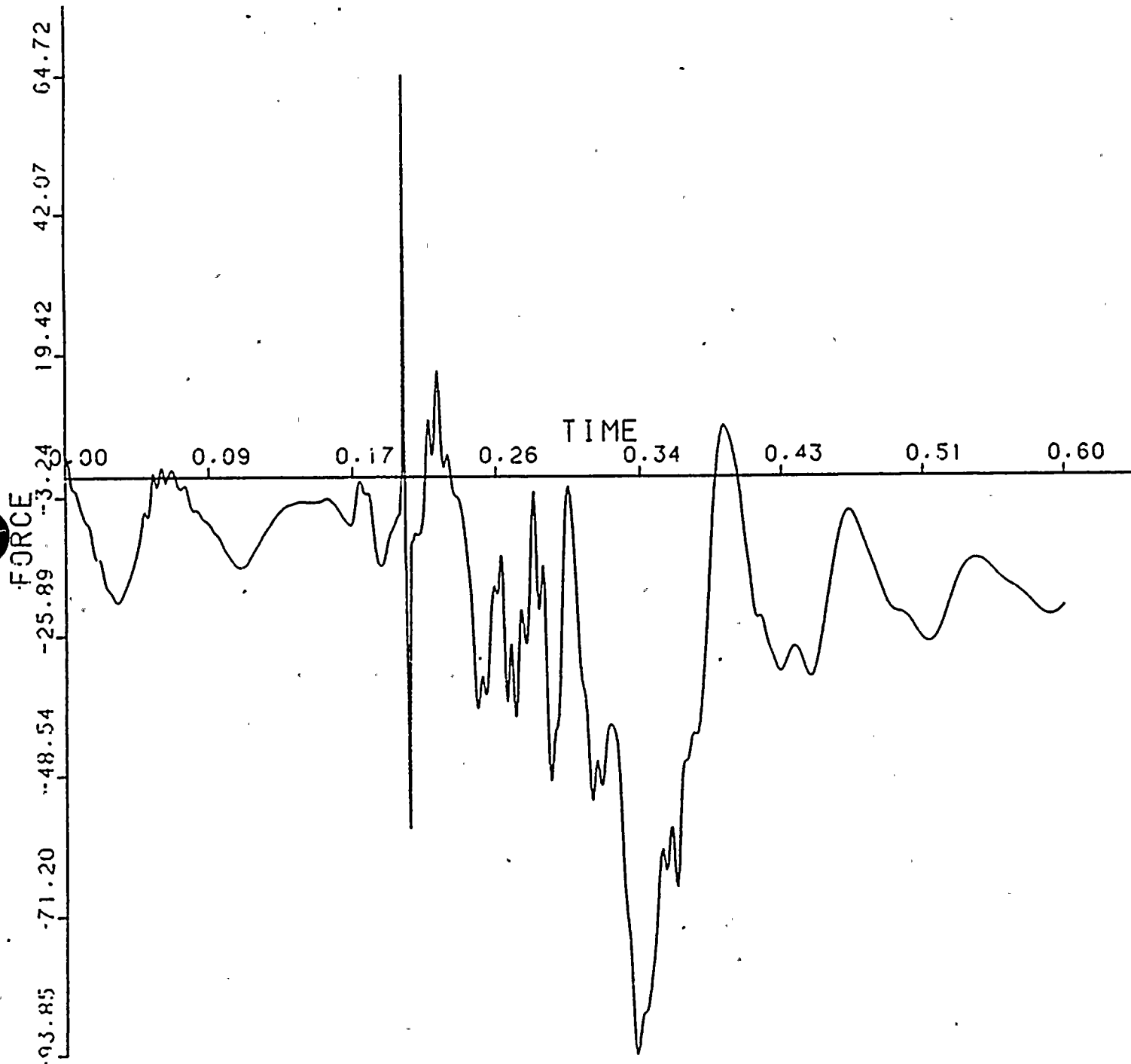
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YELLOW LOOP SEAL

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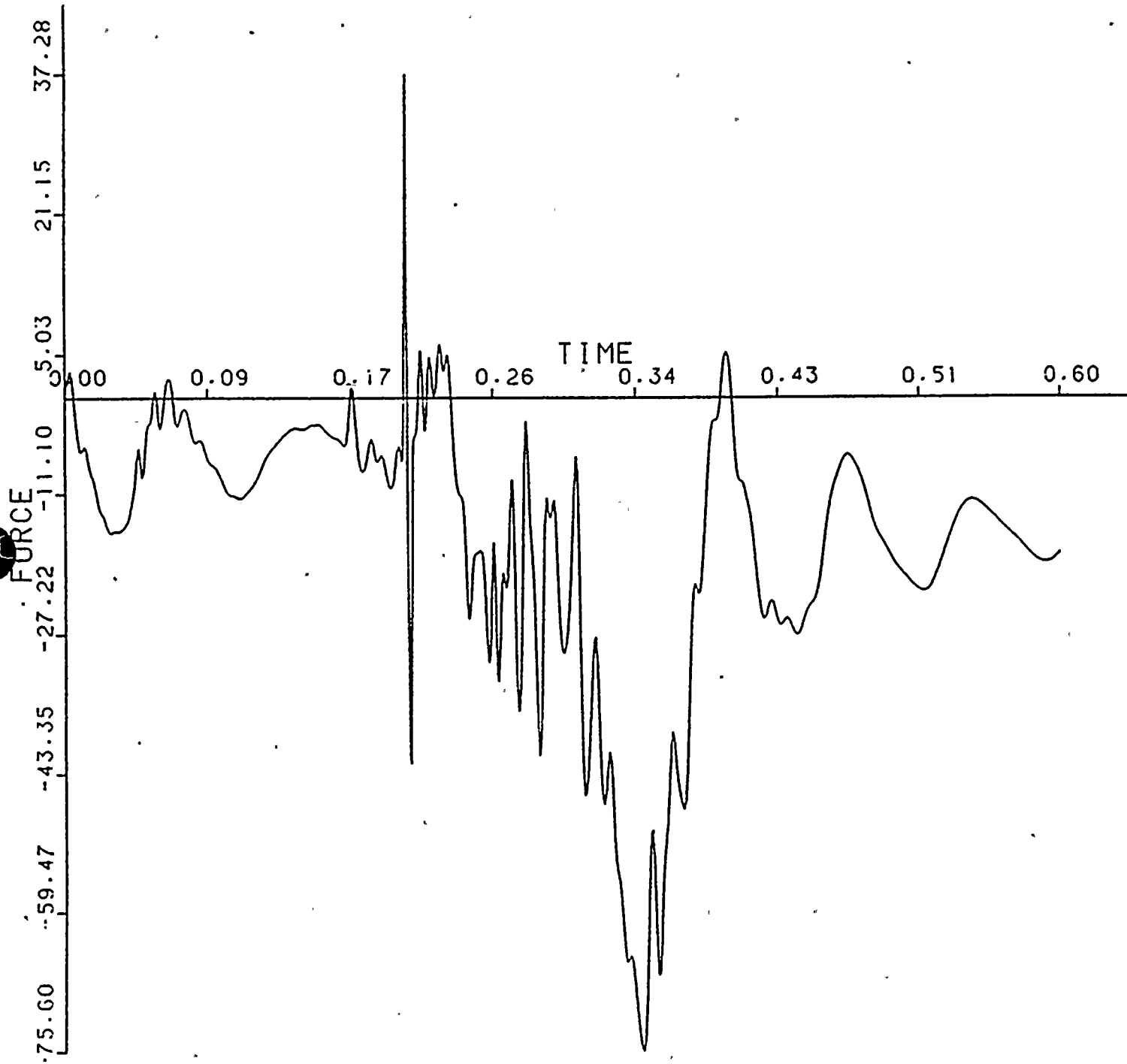


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YELLOW LOOP SEAL - YELLPSL.TMP

TIME/FORCE TABLE 18. MAGNITUDE AT NODE POINT



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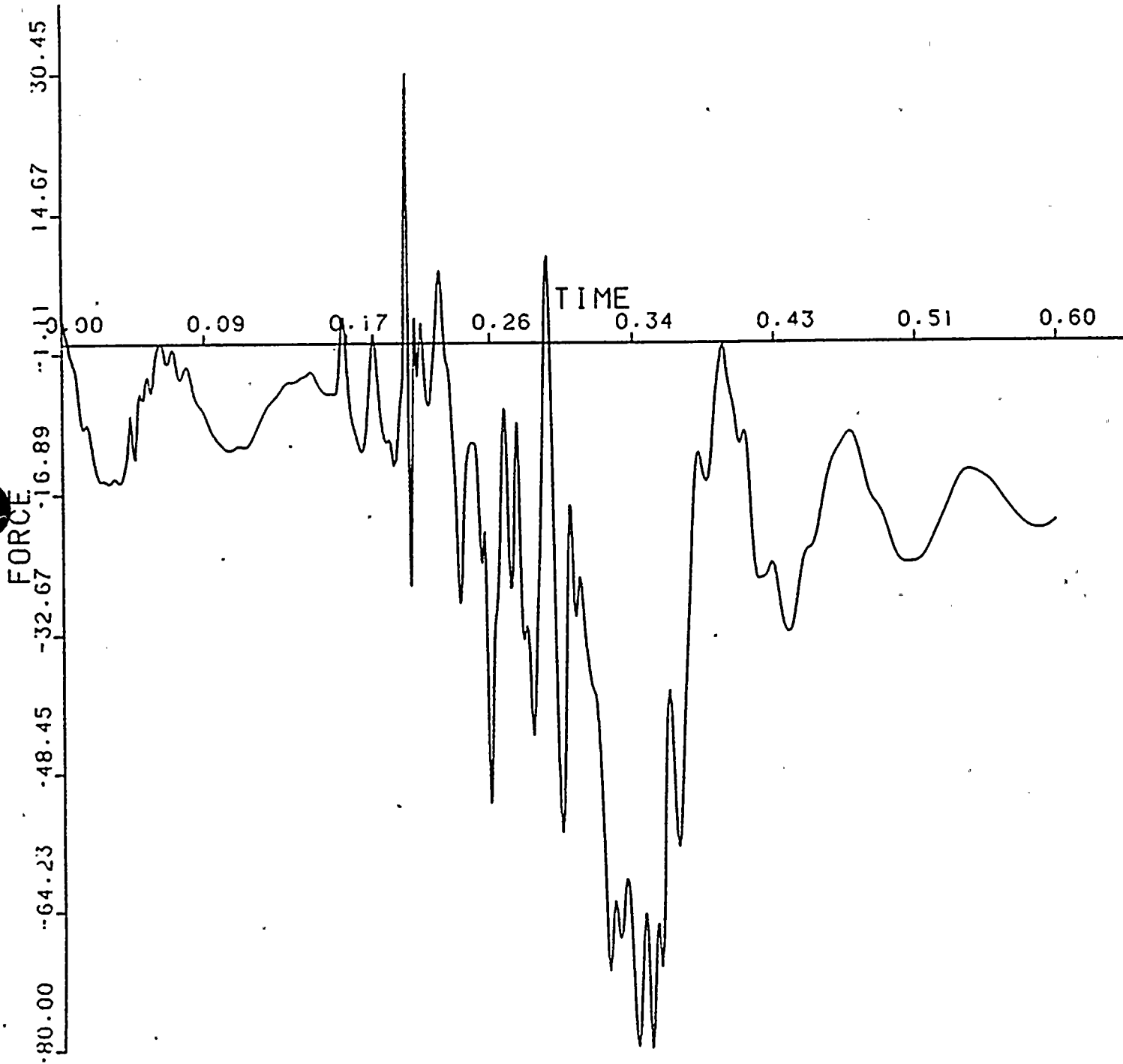
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YELLOW LOOP SEAL - YELLPSL.TMP

TIME/FORCE TABLE 19, MAGNITUDE AT NODE POINT

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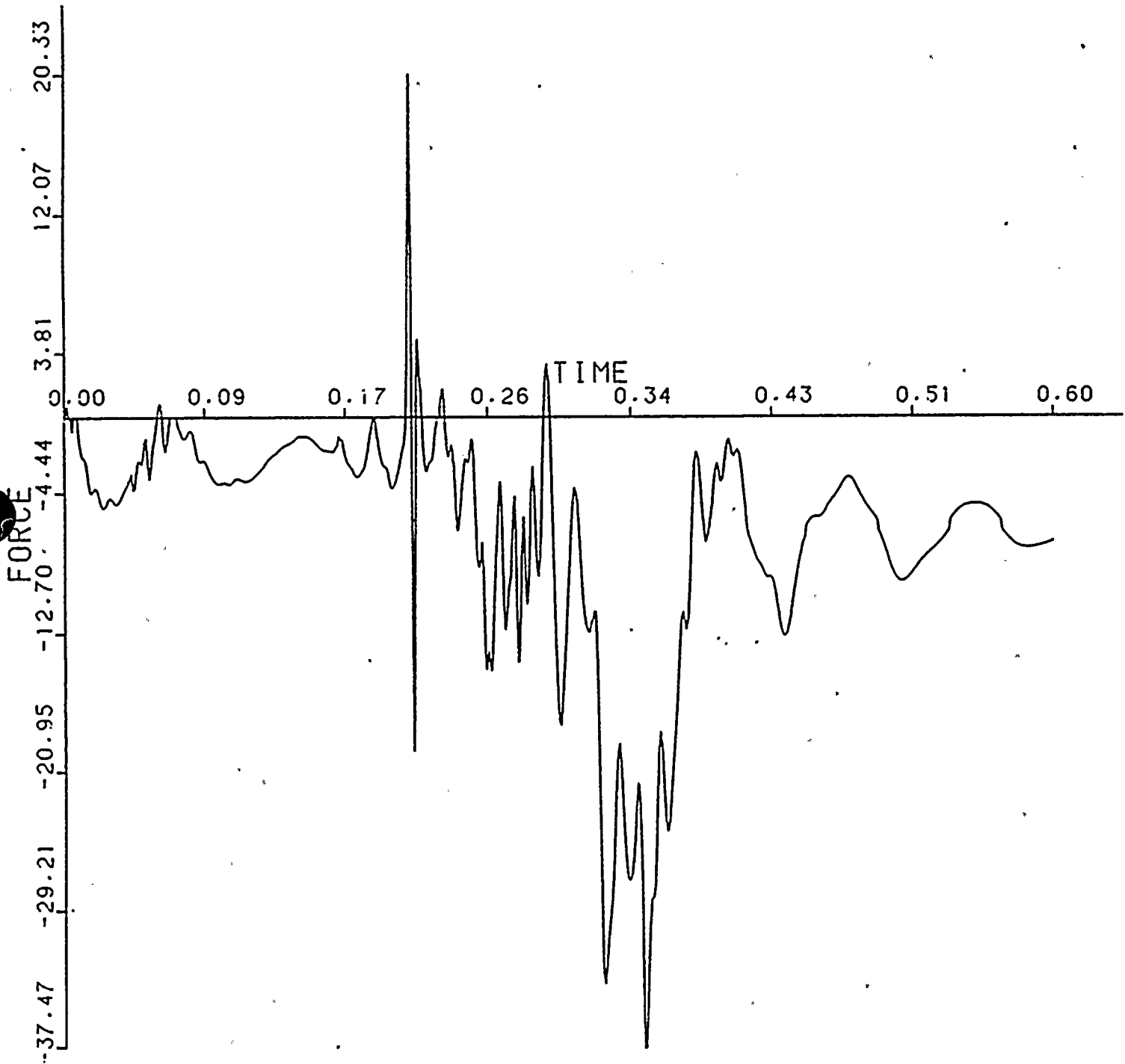
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YELLOW LOOP SEAL - YELLPSL.TMP

TIME/FORCE TABLE 20, MAGNITUDE AT NODE POINT

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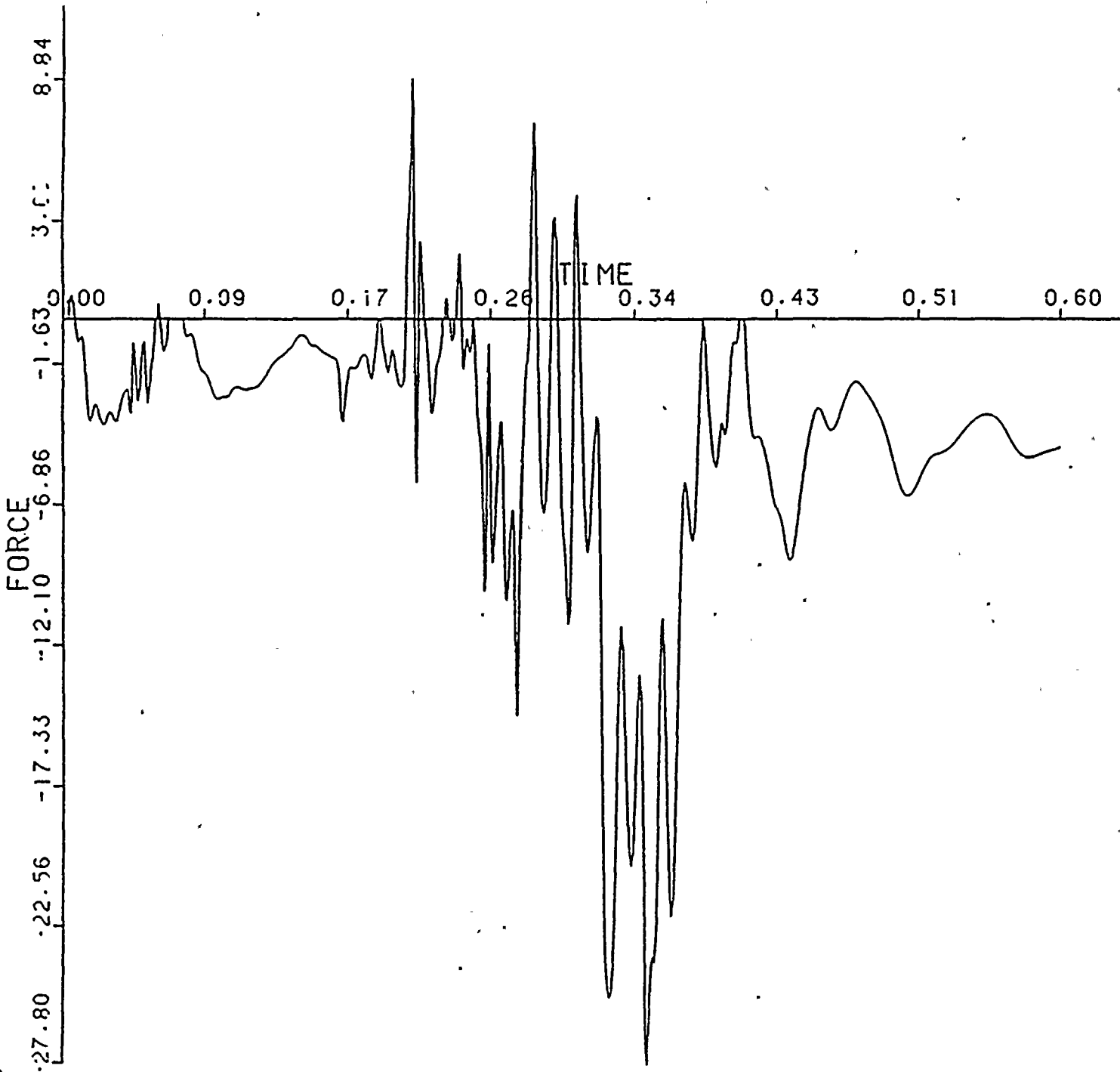
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YELLOW LOOP SEAL - YELLPSL.TMP

TIME/FORCE TABLE

21. MAGNITUDE AT NODE POINT

590



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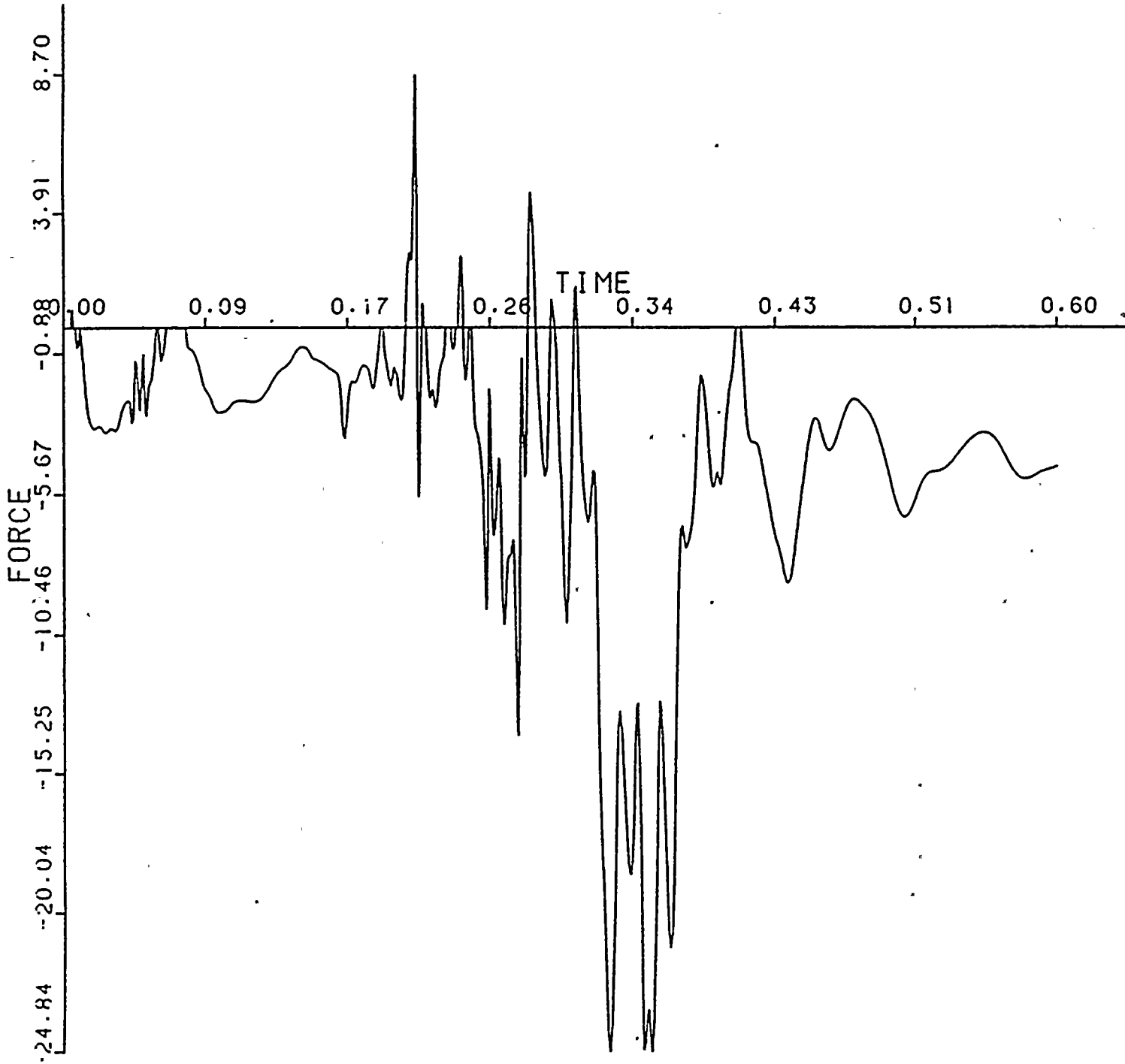
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YELLOW LOOP SEAL - YELLSL.TMP

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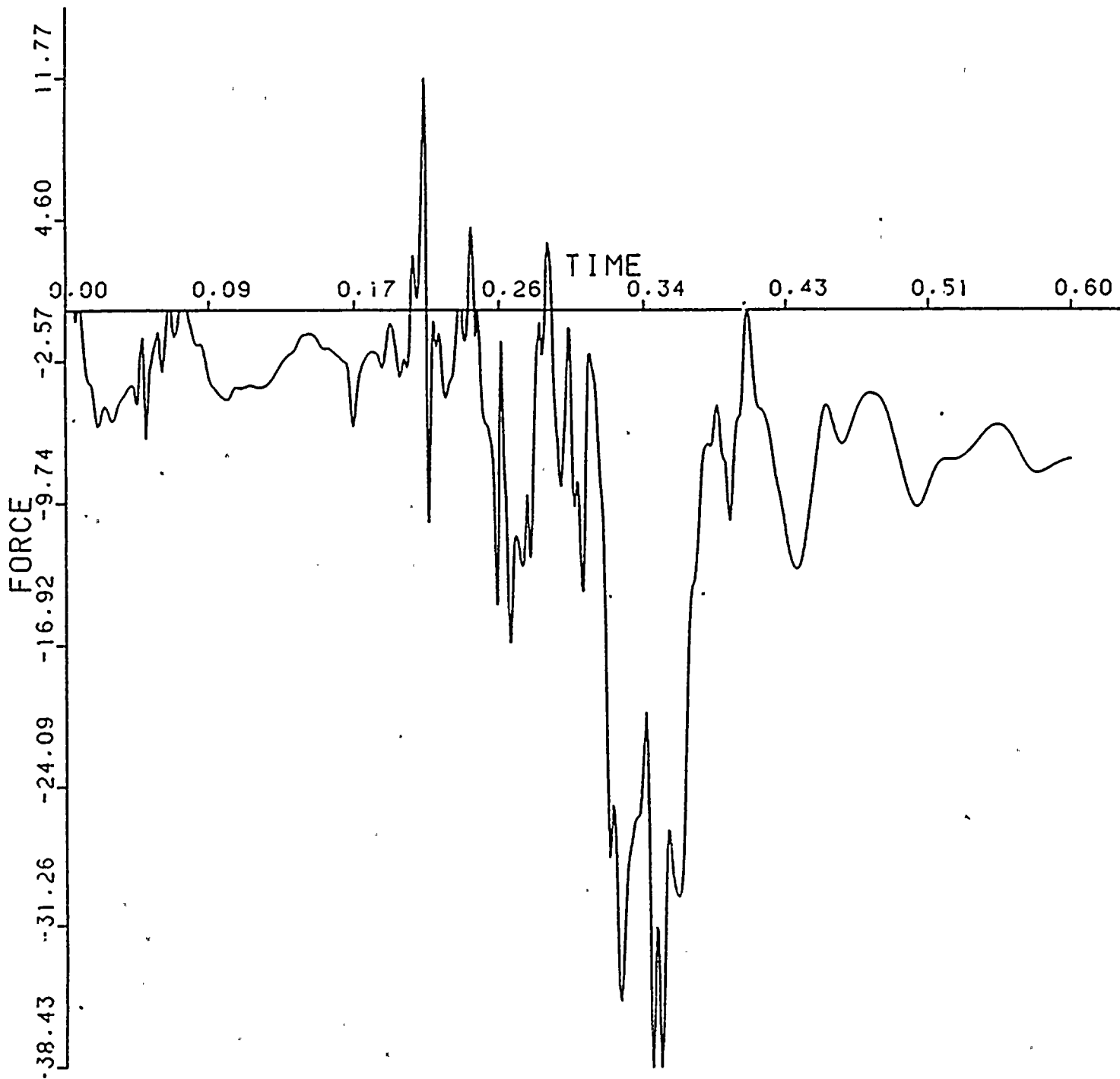
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TIME/FORCE TABLE

23. MAGNITUDE AT NODE POINT

575



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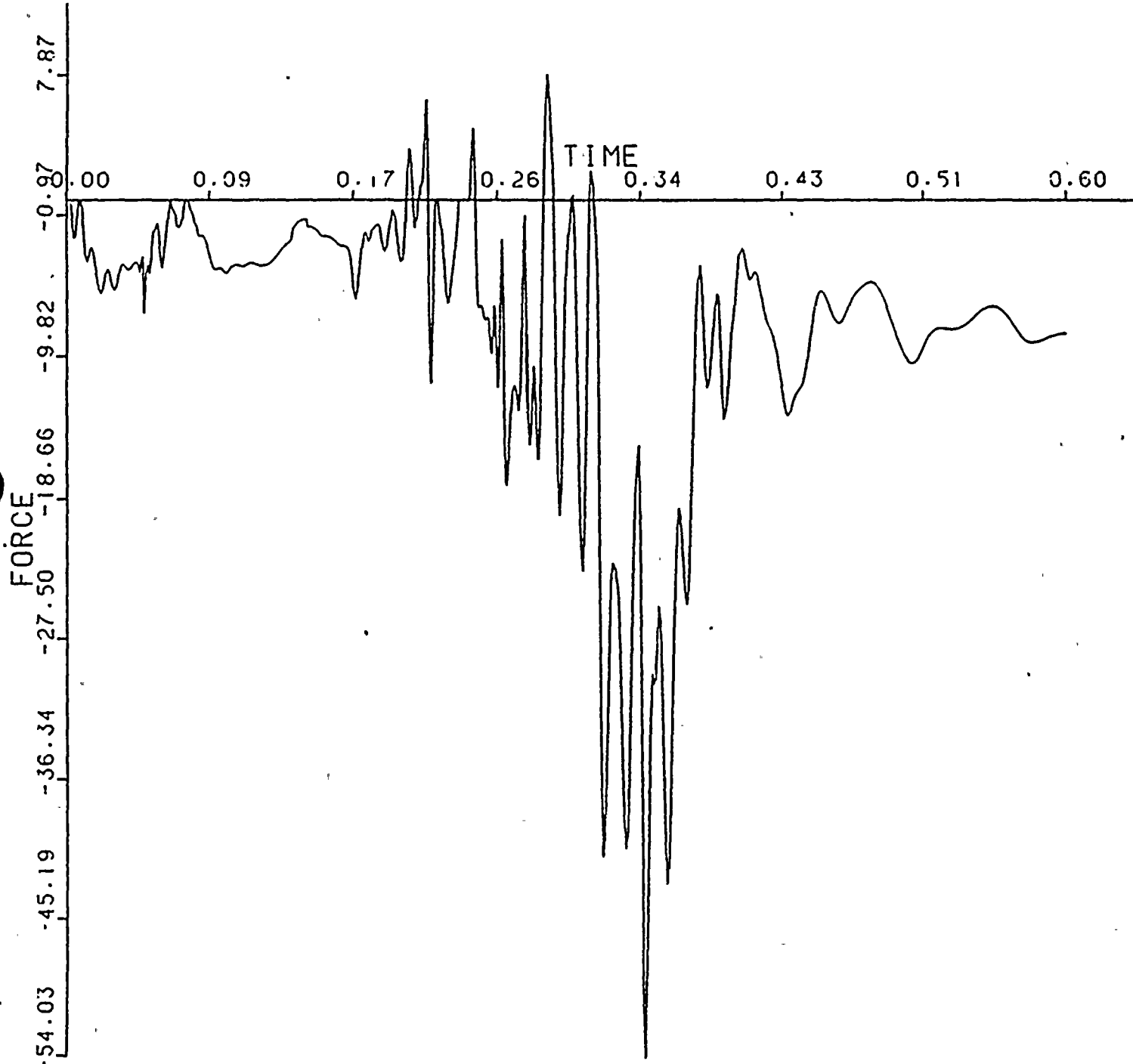
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YELLOW LOOP SEAL - YELLPSL.TMP

TIME/FORCE TABLE

24, MAGNITUDE AT NODE POINT

435



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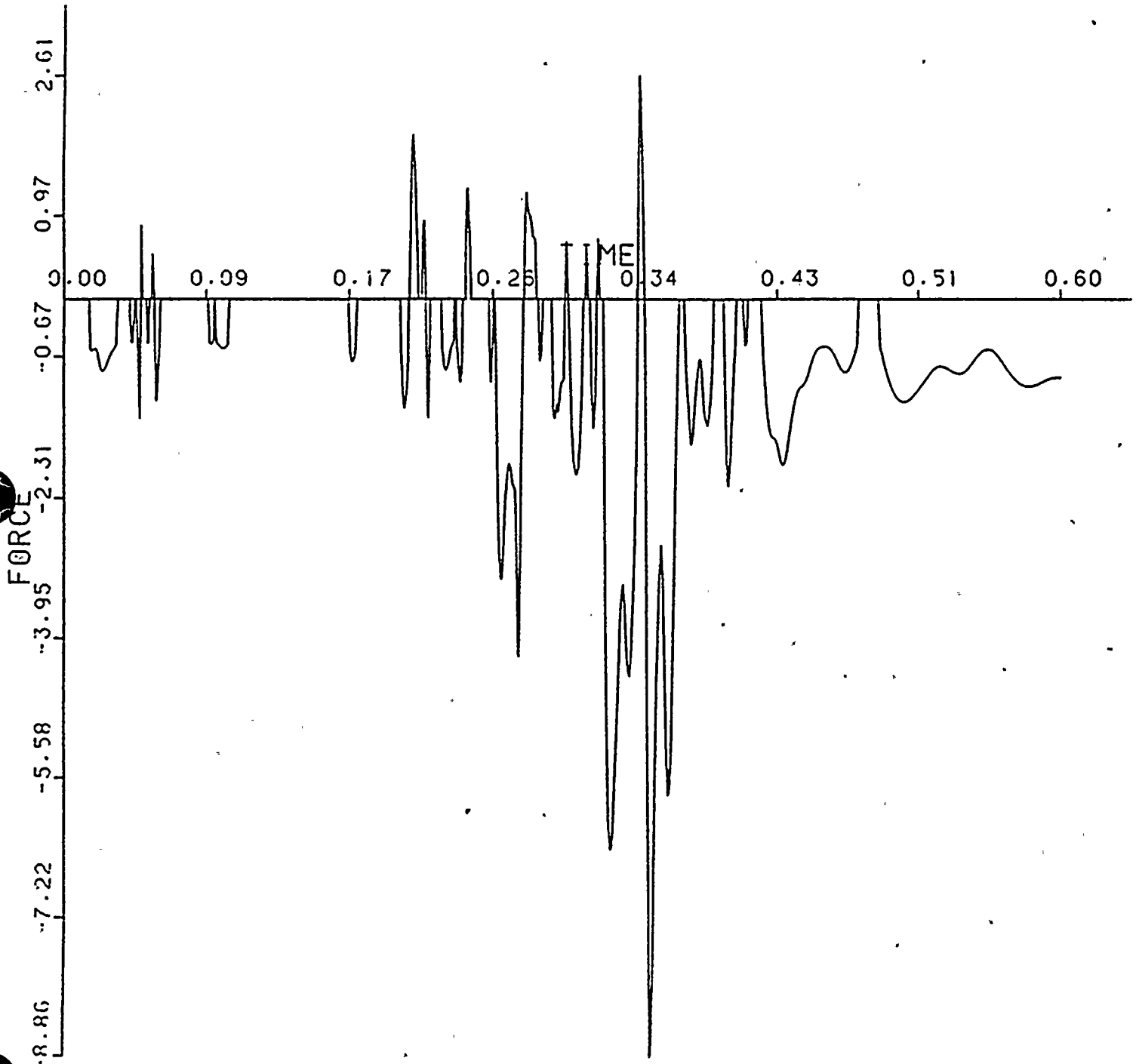
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YELLOW LOOP SEAL - YELLPSL.TMP

TIME/FORCE TABLE 25, MAGNITUDE AT NODE POINT

440



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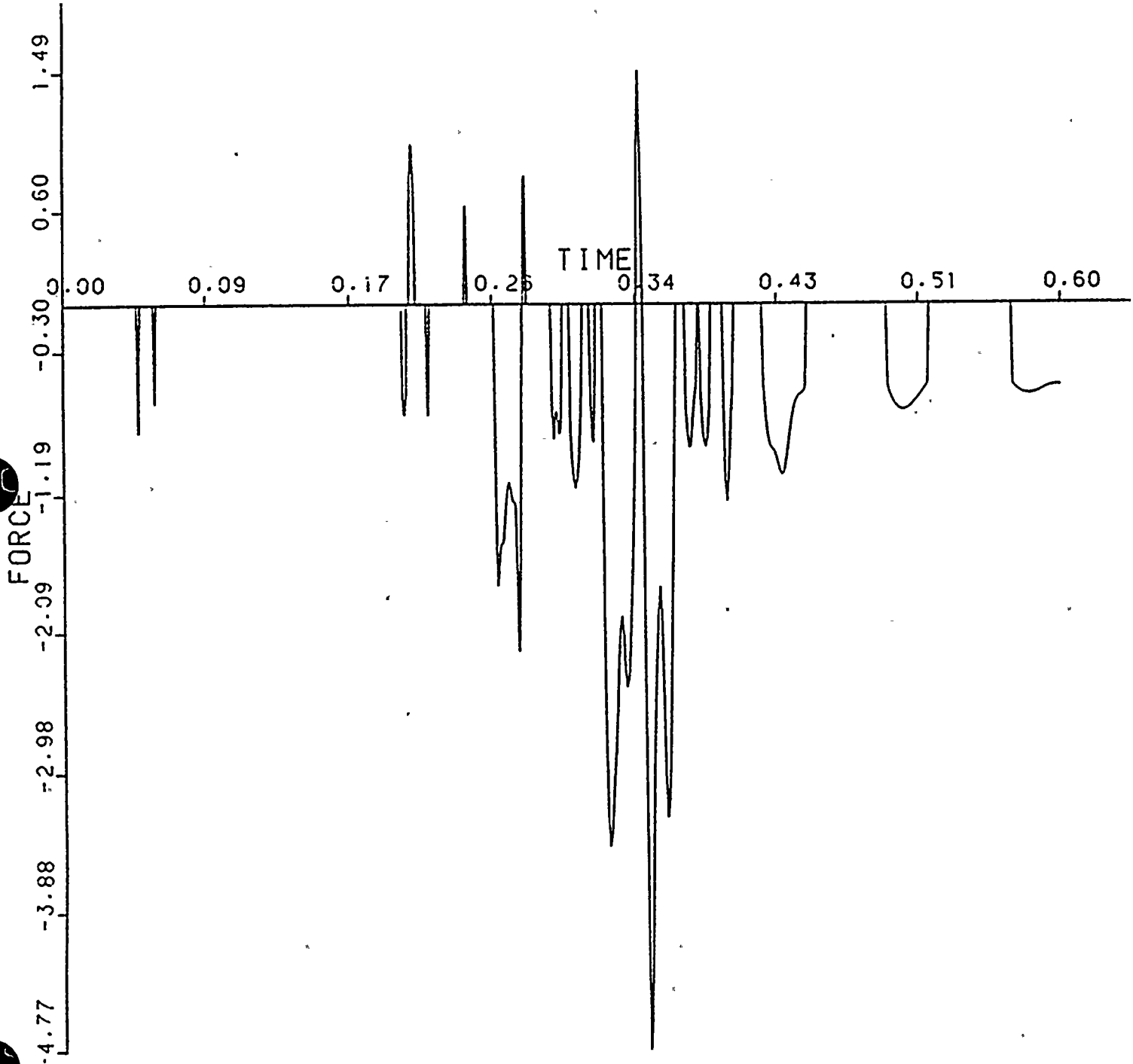
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YELLOW LOOP SEAL - YELLPSL.TMP

TIME/FORCE TABLE 26. MAGNITUDE AT NODE POINT

450



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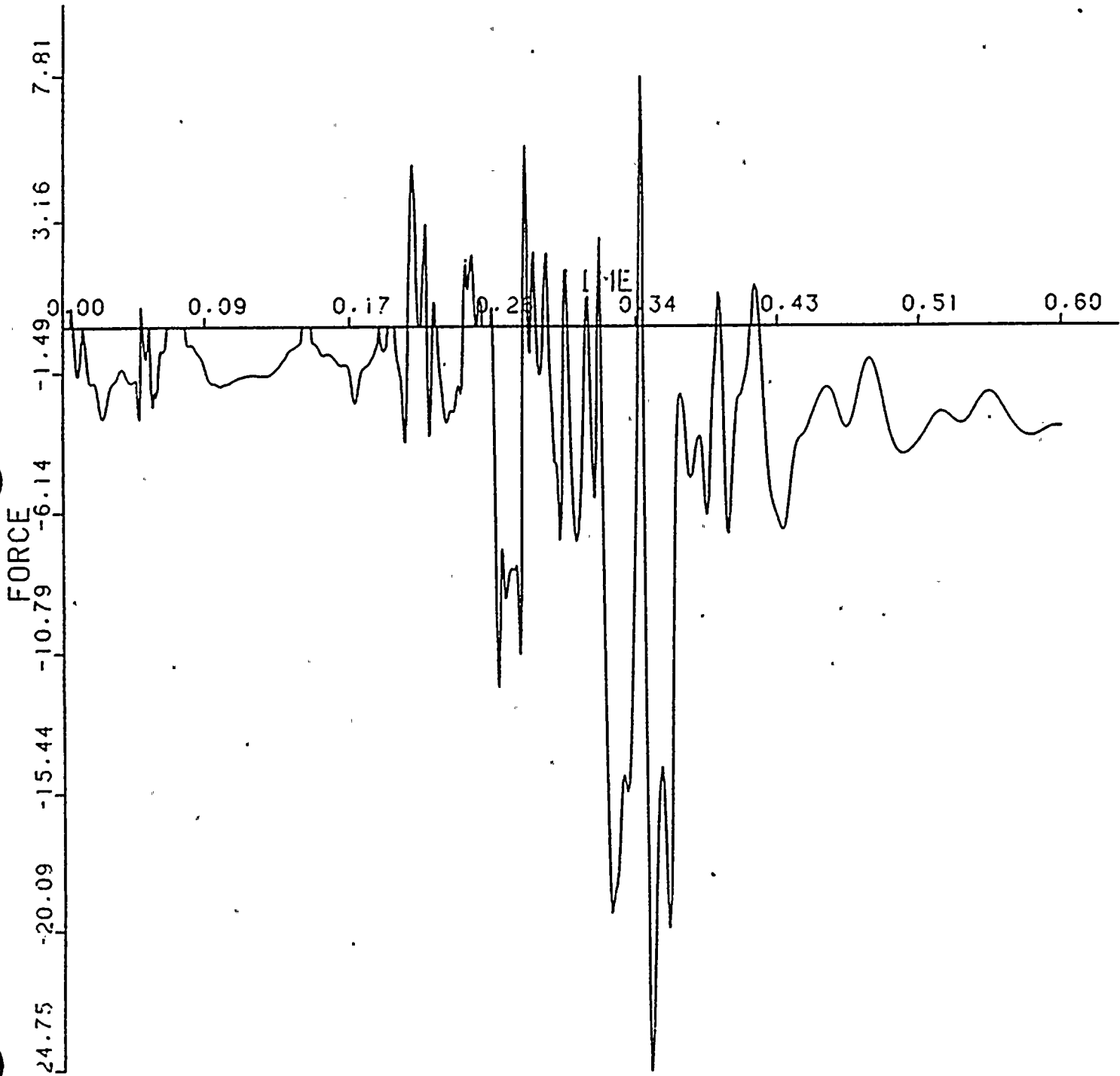
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YELLOW LOOP SEAL - YELLSL.TMP

TIME/FORCE TABLE

27. MAGNITUDE AT NODE POINT.

460



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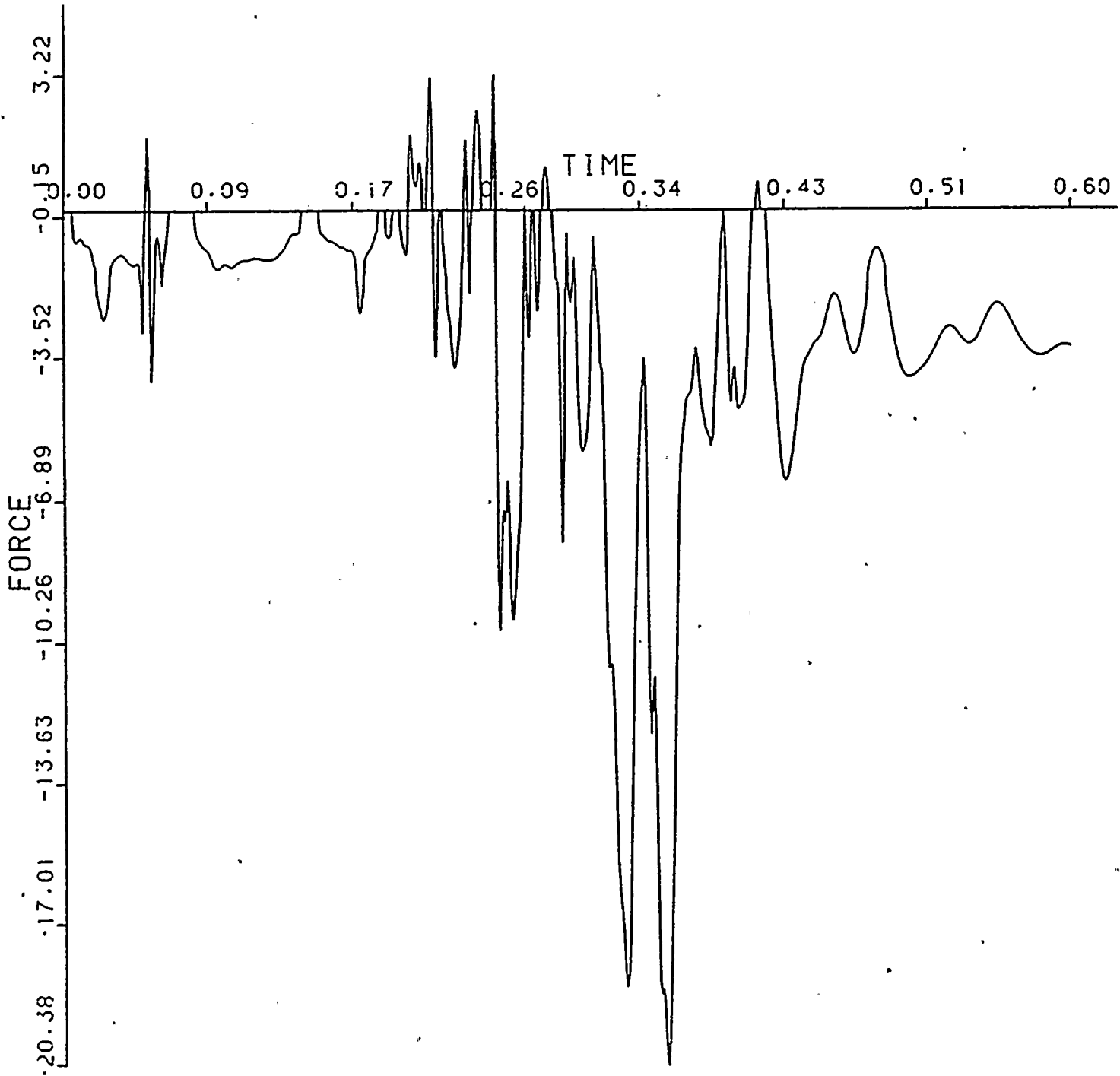
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YELLOW LOOP SEAL - YELLPSL.TMP

TIME/FORCE TABLE 28. MAGNITUDE AT NODE POINT . 465



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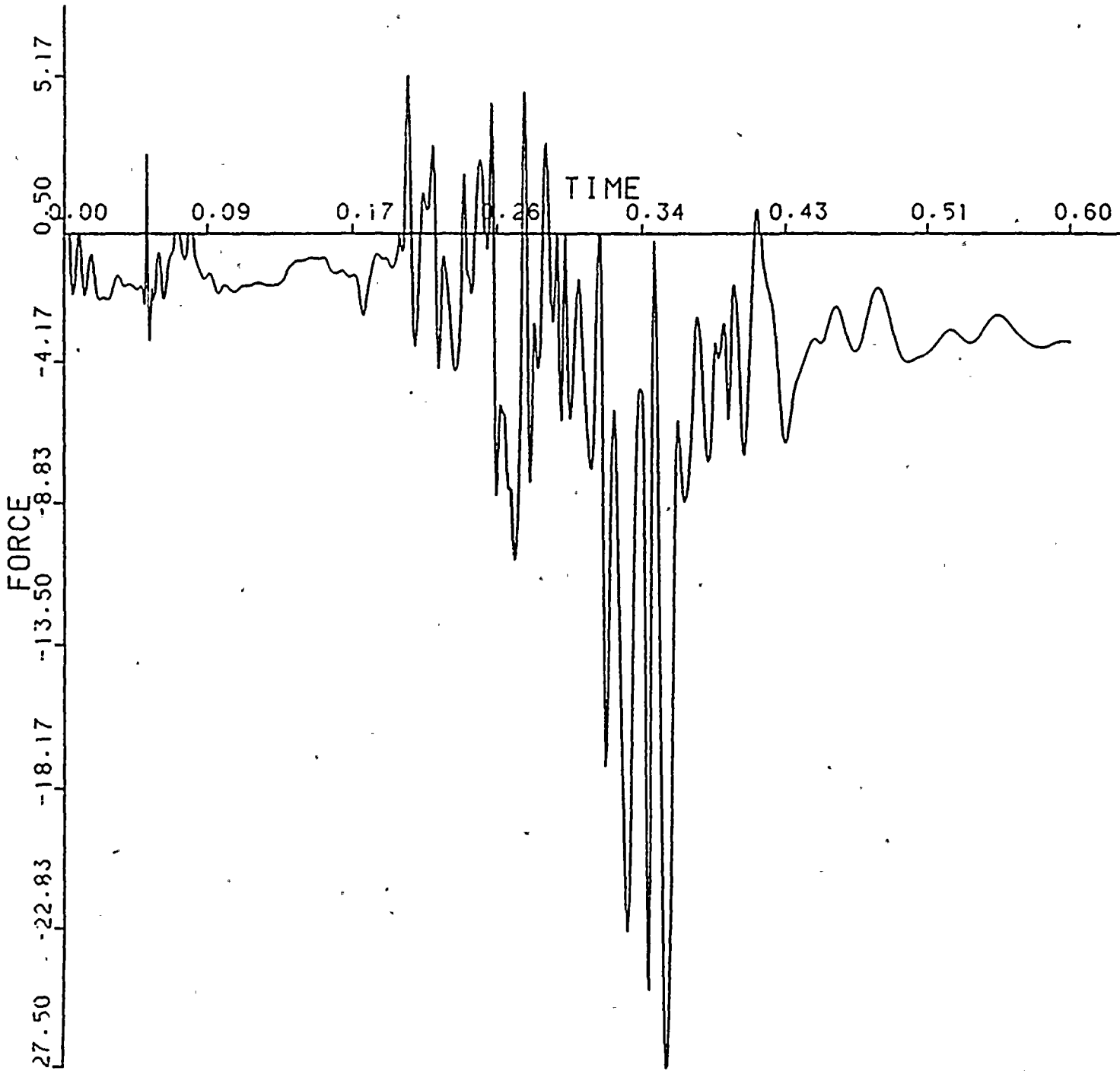
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YELLOW LOOP SEAL - YELLPSL.TMP

TIME/FORCE TABLE 29, MAGNITUDE AT NODE POINT

475



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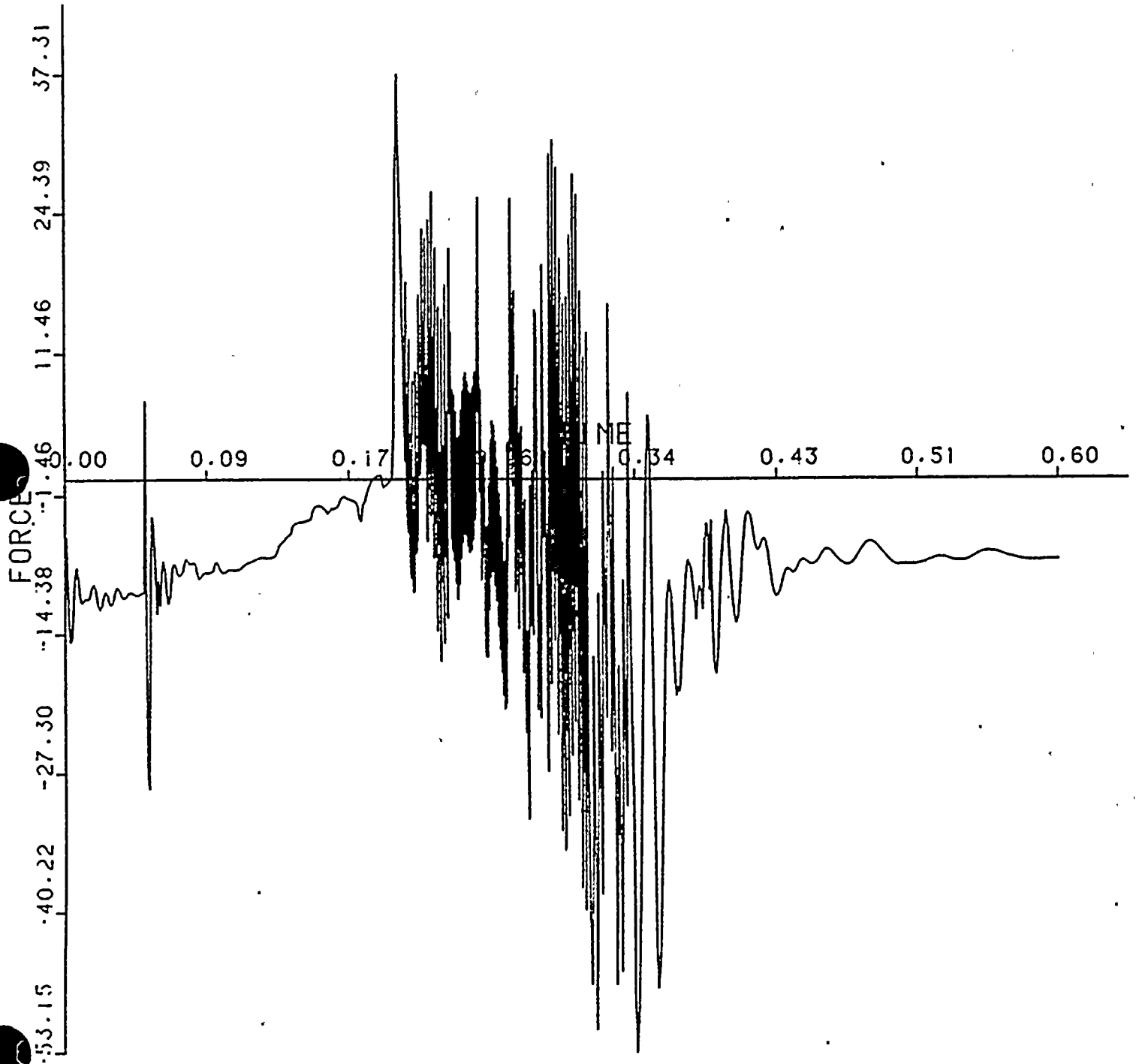
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YELLOW LOOP SEAL - YELLPSL.TMP

TIME/FORCE TABLE 30, MAGNITUDE AT NODE POINT

485



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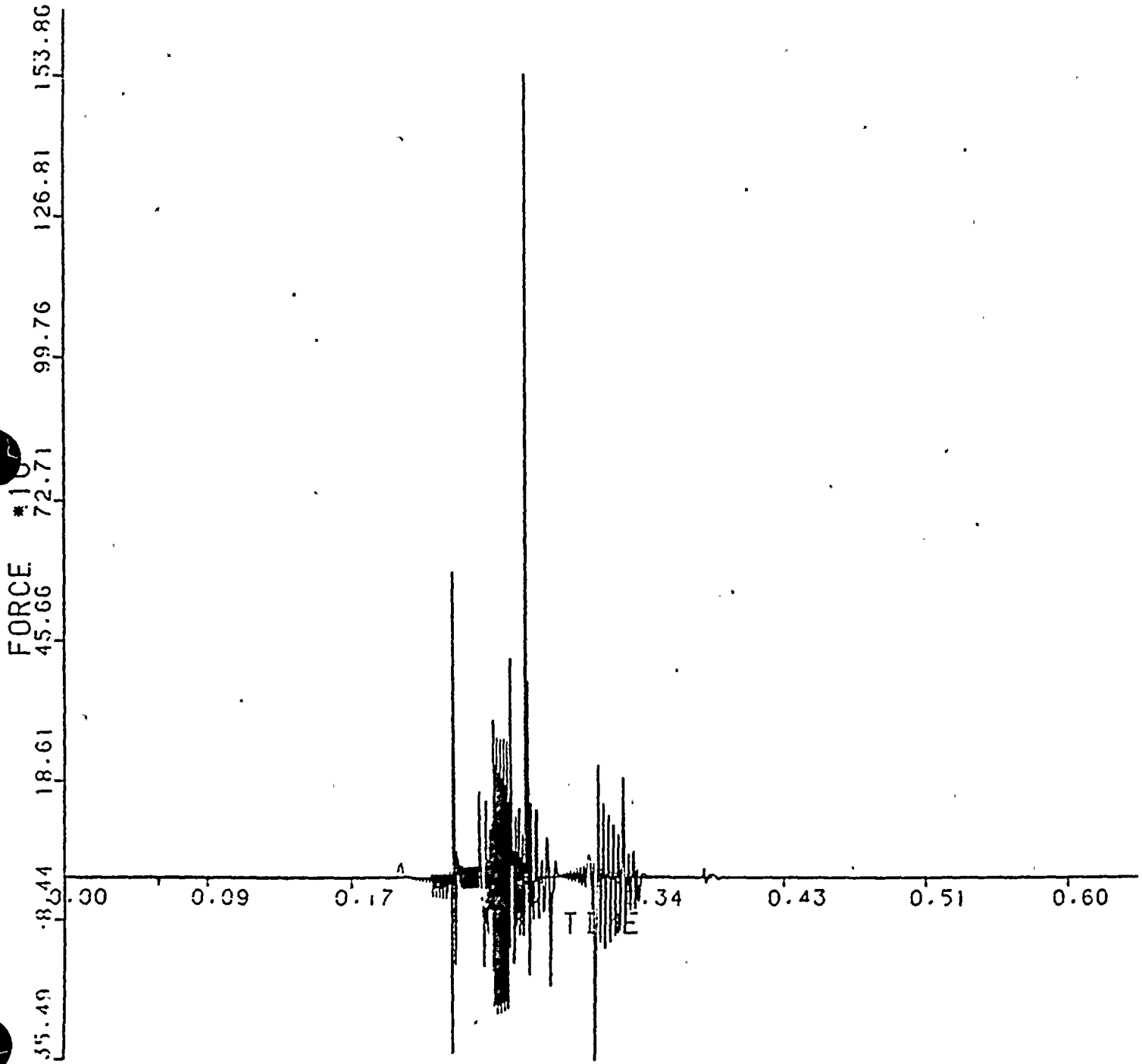
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YELLOW LOOP SEAL - YELLPSL.TMP

TIME/FORCE TABLE 31. MAGNITUDE AT NODE POINT

529



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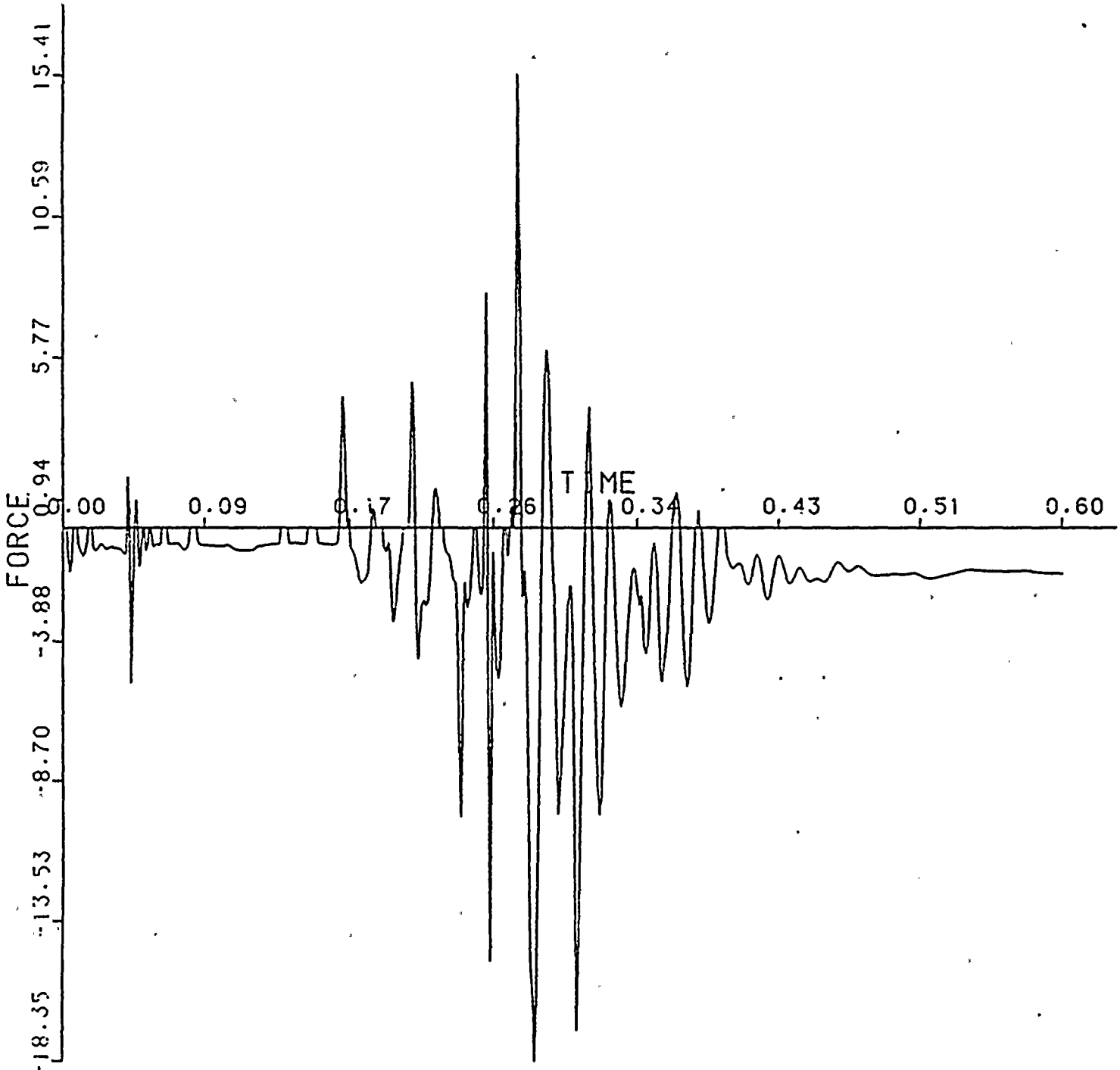
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YELLOW LOOP SEAL - YELLPSL.TMP

TIME/FORCE TABLE

32. MAGNITUDE AT NODE POINT

665



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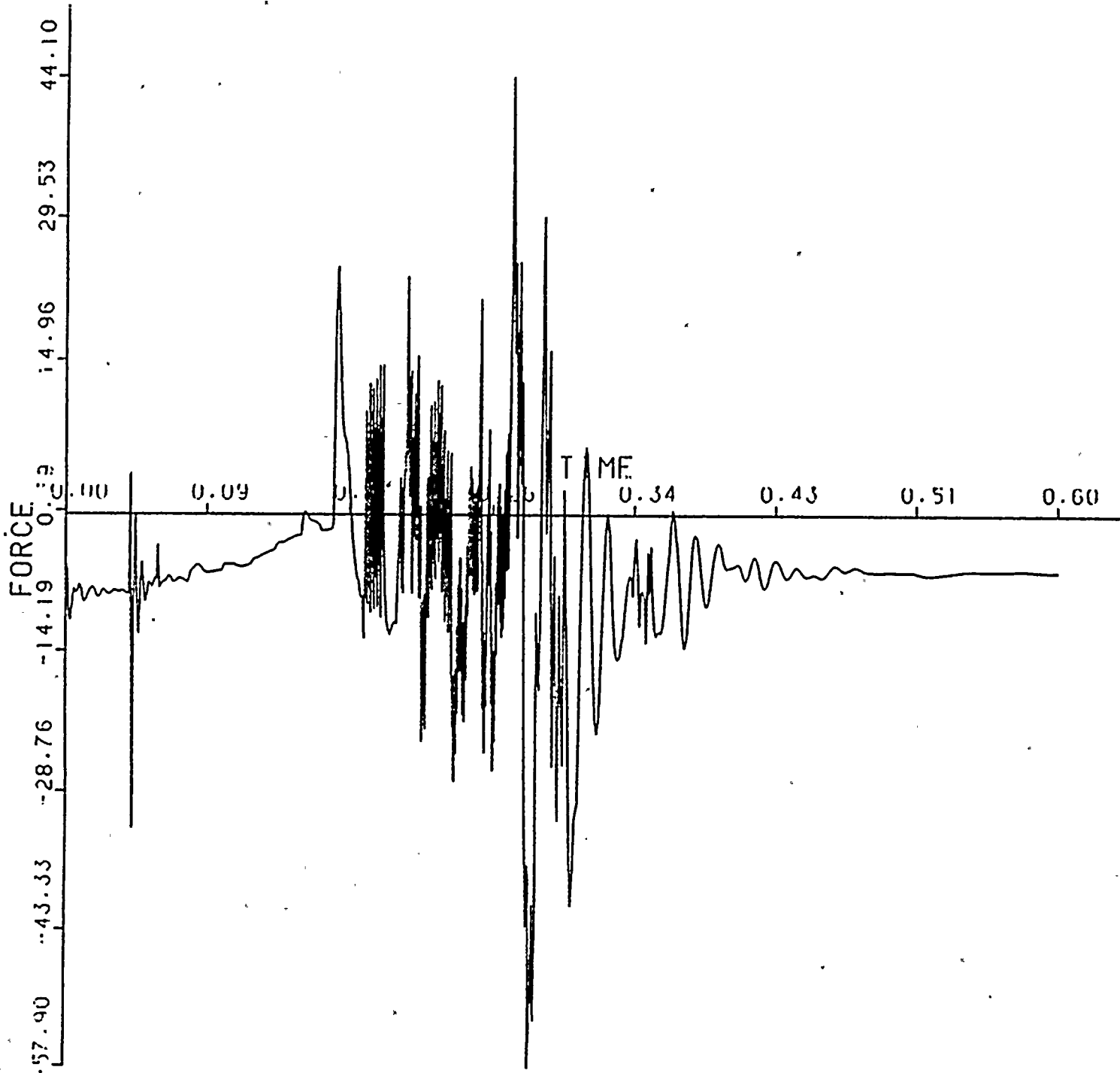
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SAP2SAP VERIFICATION 5364

YELLOW LOOP SEAL - YELLPSL.TMP

TIME/FORCE TABLE 33. MAGNITUDE AT NODE POINT



DONE BY: MR DATE: 5-12-83
CHKD BY: XL DATE: 5-12-83

Technical Report
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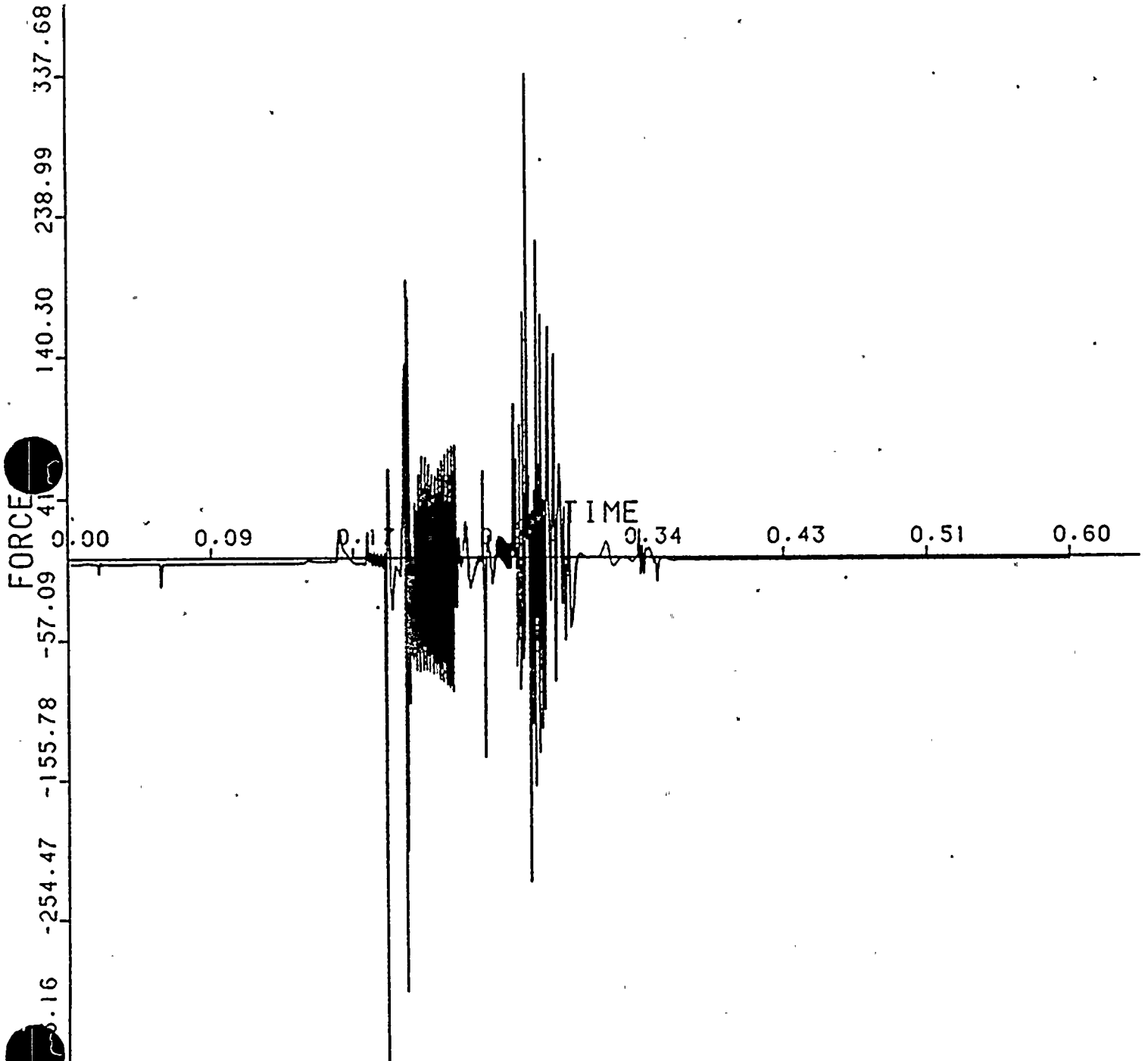
SAP2SAP VERIFICATION 5364

12-MAY-83

YELLOW LOOP SEAL - YELLPSL.TMP

TIME/FORCE TABLE 34, MAGNITUDE AT NODE POINT

620



DONE BY: ML DATE: 5-12-83

CHKD BY: ML DATE: 5-12-83

Technical Report
TR-5364-1
Revision 0

ILLIINOIS ENGINEERING SERVICES

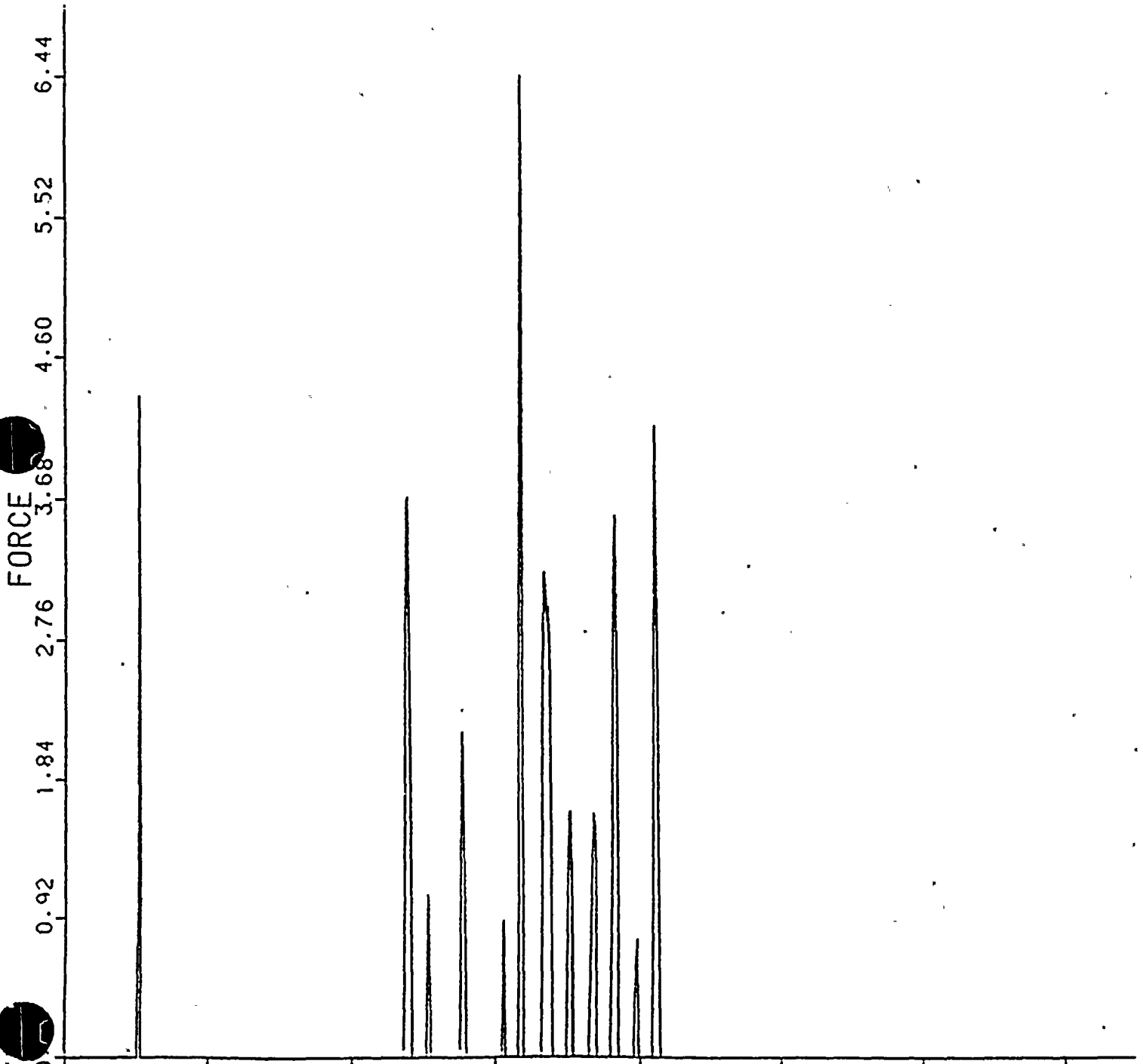
SAP2SAP VERIFICATION 5364

12-MAY-83

YELLOW LOOP SEAL - YELLPSL.TMP

TIME/FORCE TABLE 35. MAGNITUDE AT NODE POINT

431



DONE BY: JK DATE: 5-12-83
 CHKD BY: JK DATE: 5-12-83

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 Revision 0

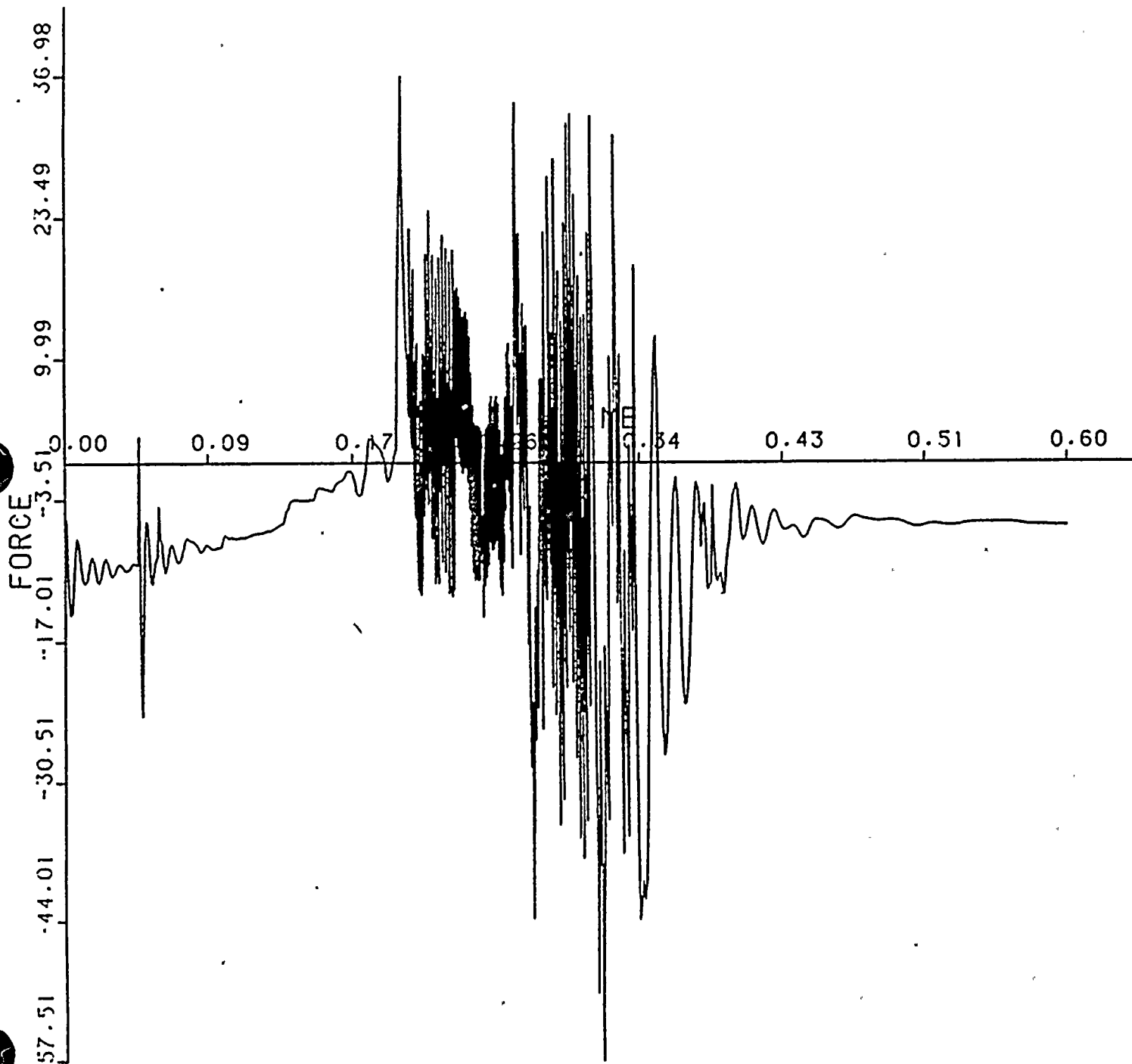
SAP2SAP VERIFICATION 5364

12-MAY-83

YELLOW LOOP SEAL - YELLPSL.TMP

TIME/FORCE TABLE 36, MAGNITUDE AT NODE POINT

405



DONE BY: ML DATE: 5-12-83

CHKD BY: ML DATE: 5-12-83

Technical Report
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Revision 0

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TELEDYNE
ENGINEERING SERVICES

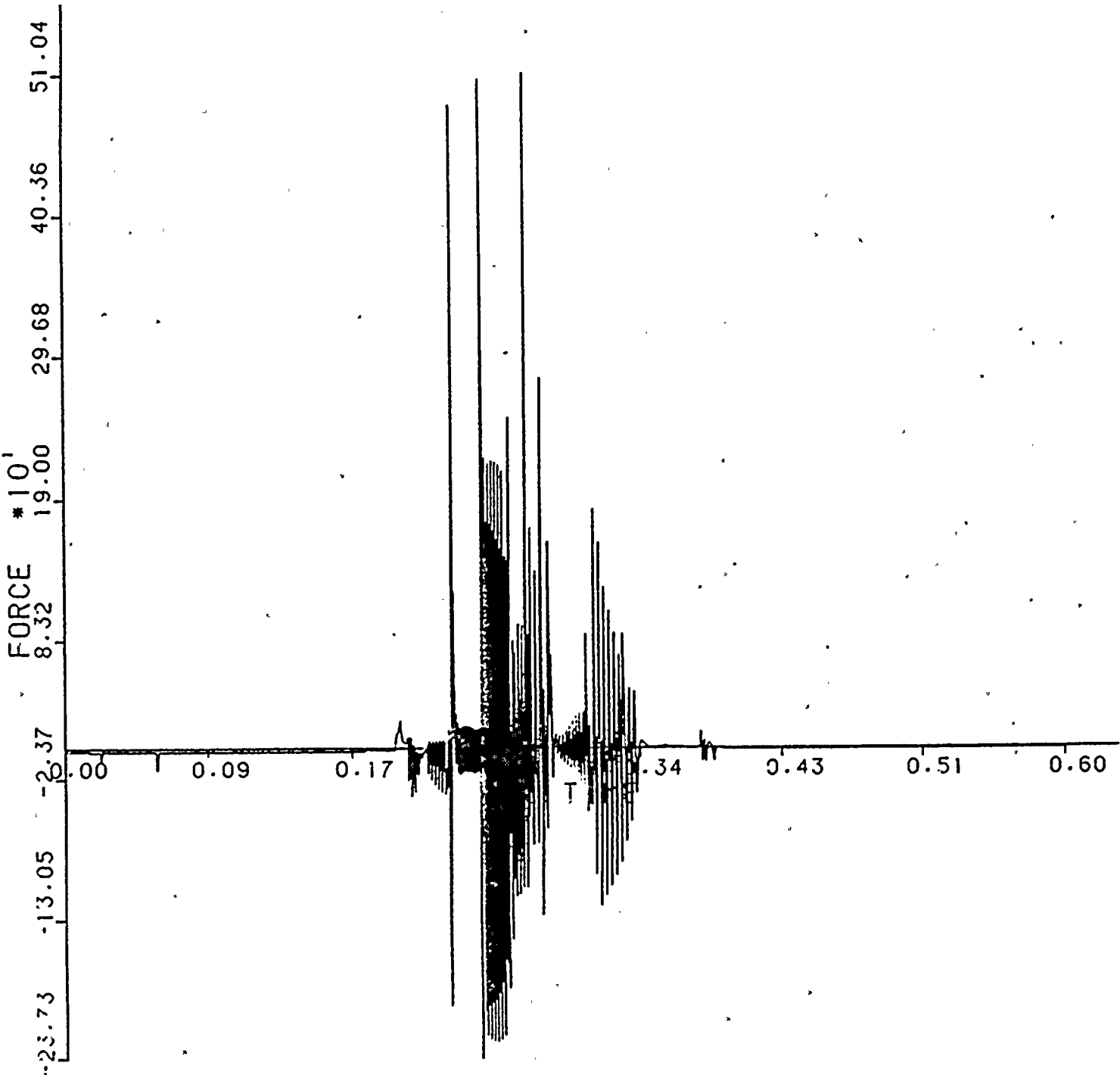
SAP2SAP VERIFICATION 5364

12-MAY-83

YELLOW LOOP SEAL - YELLPSL.TMP

TIME/FORCE TABLE 37. MAGNITUDE AT NODE POINT

382



DONE BY: ML DATE: 5-12-83

CHKD BY: ML DATE: 5-12-83

Technical Report

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SAP2SAP VERIFICATION 5364

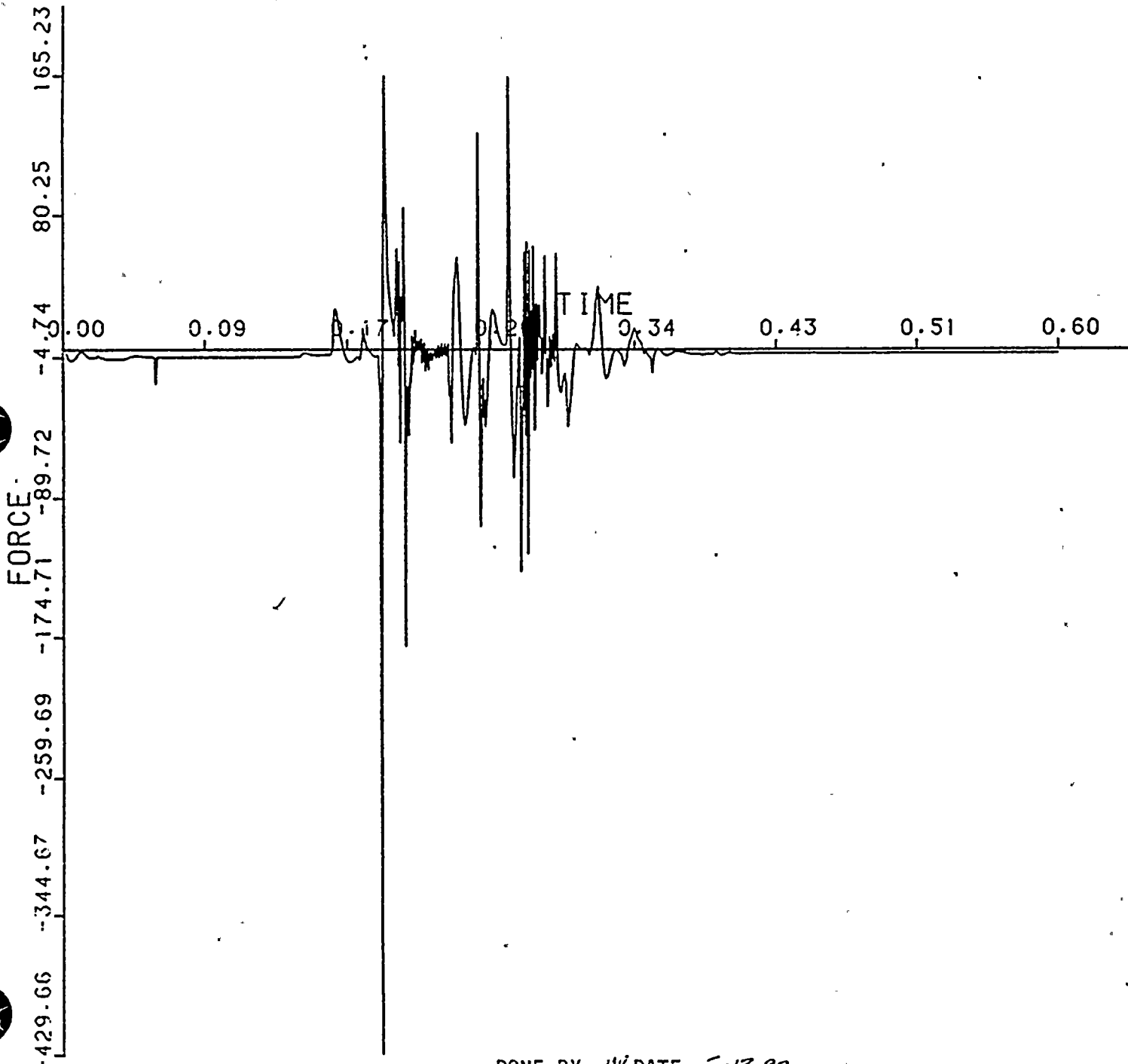
12 MAY 83

YELLOW LOOP SEAL YELTPEI.TMP

TIME/FORCE TABLE

38. MAGNITUDE AT NODE POINT

610



DONE BY: ML DATE: 5-12-83

CHKD BY: ML DATE: 5-12-83

Technical Report
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Revision 0

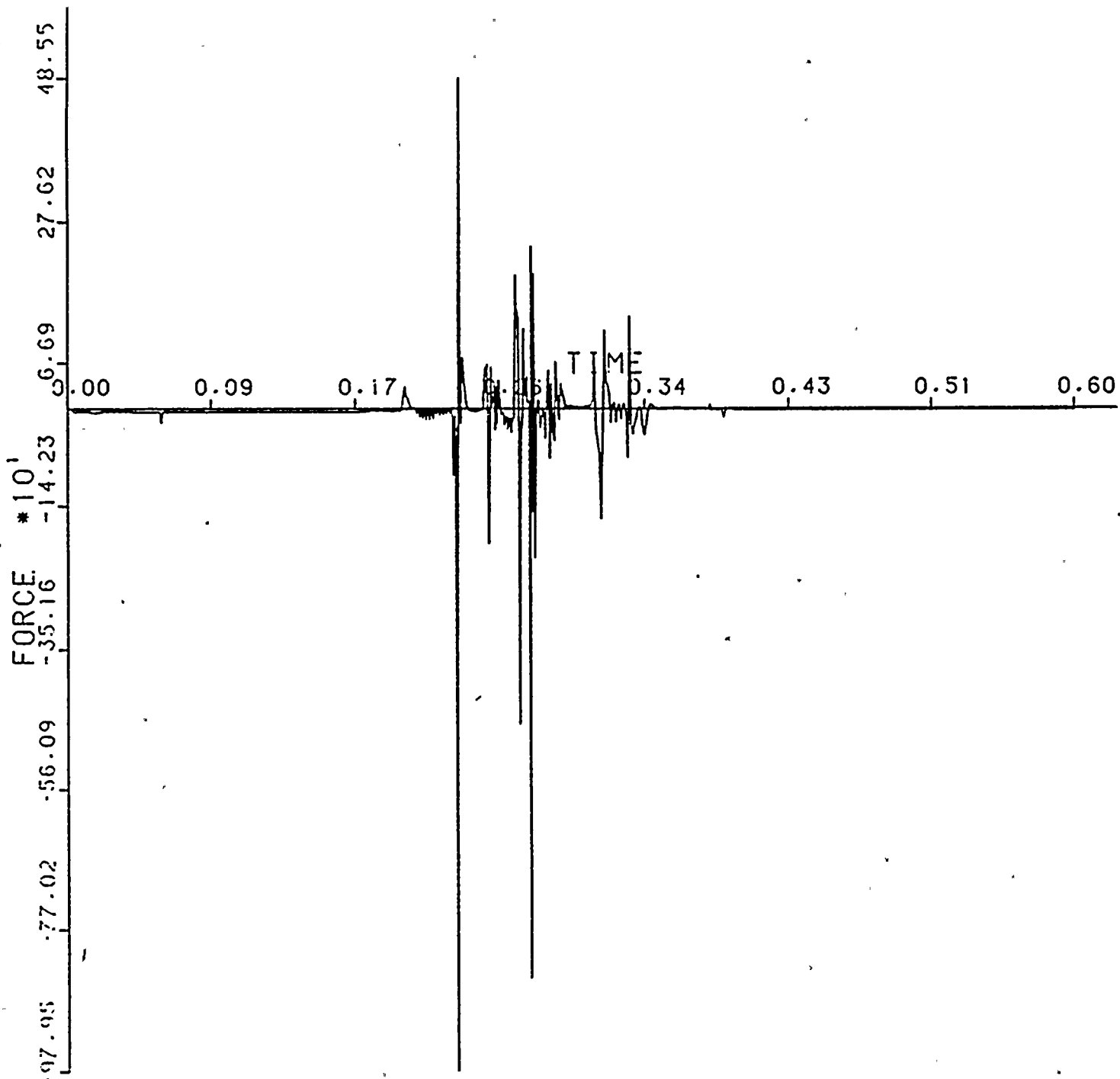
SAP2SAP VERIFICATION 5364

12-MAY-83

YELLOW LOOP SEAL - YELLPSL.TMP

TIME/FORCE TABLE 39, MAGNITUDE AT NODE POINT

535



DONE BY: ML DATE: 5-12-83

CHKD BY: ML DATE: 5-12-83

Technical Report

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Revision 0



TELEDYNE
ENGINEERING SERVICES

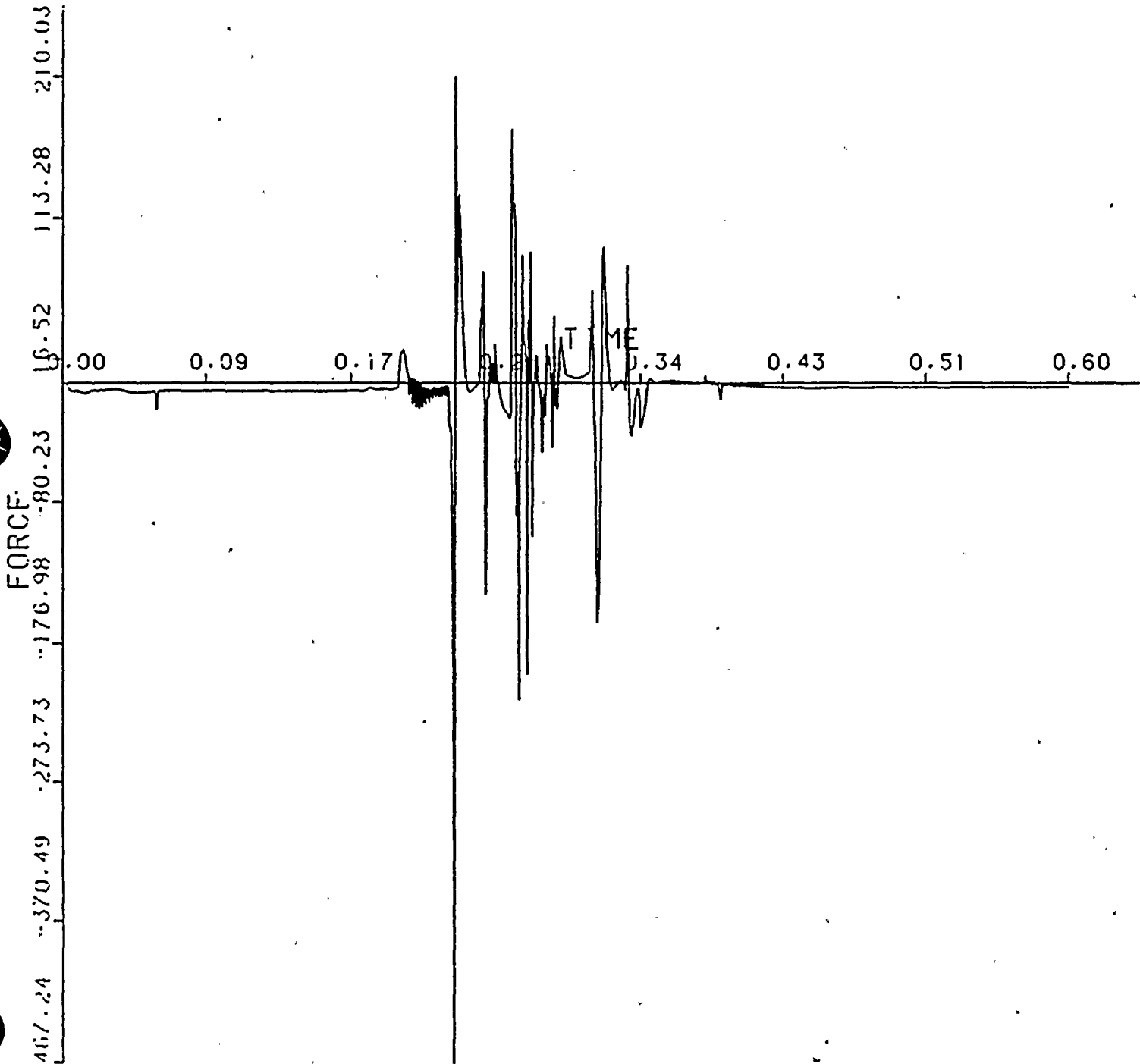
SAP2SAP VERIFICATION 5364

12-MAY-83

YELLOW LOOP SEAL - YELLPSL.TMP

TIME/FORCE TABLE 40. MAGNITUDE AT NODE POINT

545



DONE BY: ML DATE: 5-12-83

CHKD BY: ML DATE: 5-12-83

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SAP2SAP VERIFICATION 5364

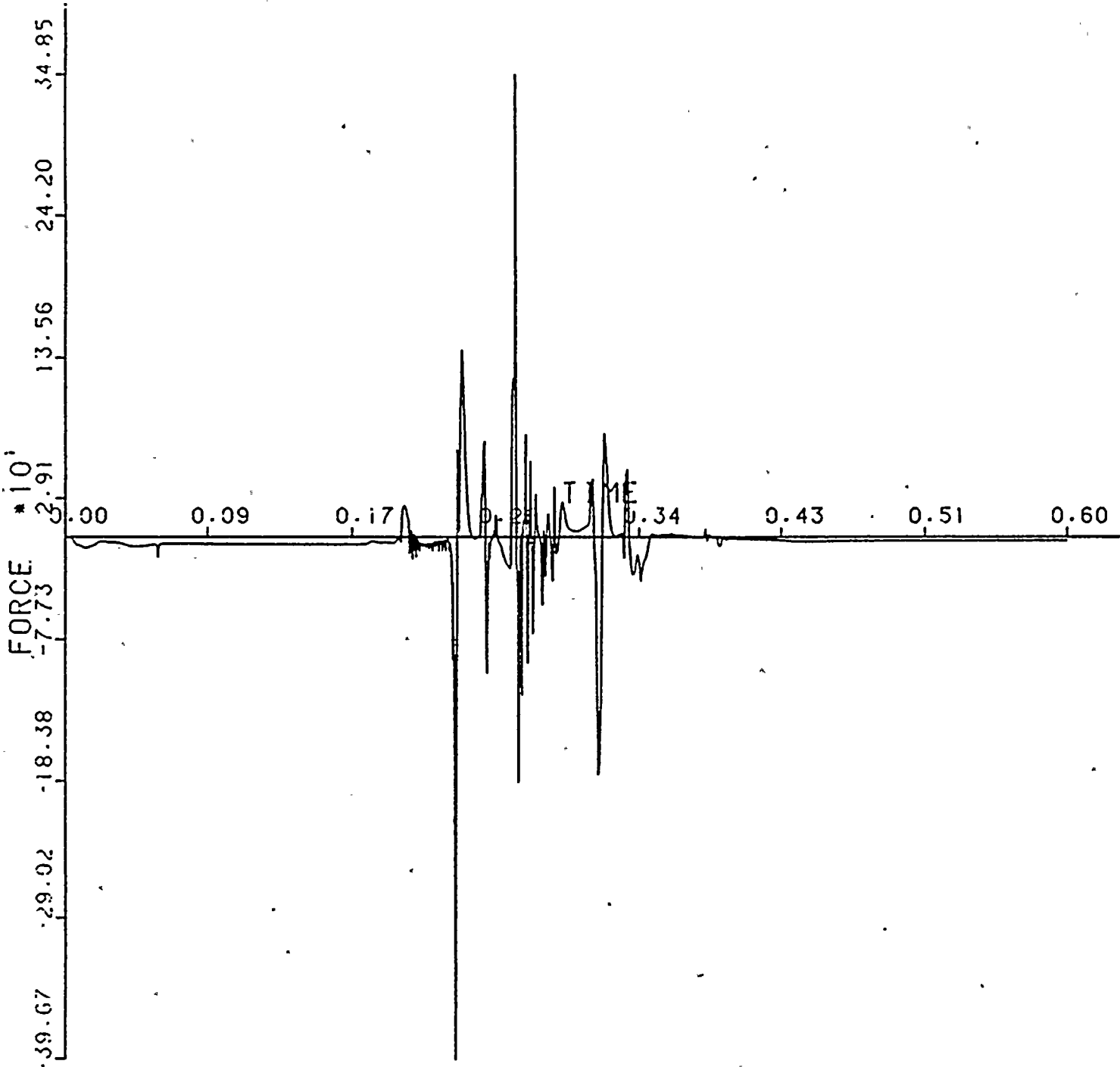
12-MAY-83

YELLOW LOOP SEAL - YELLPSL.TMP

TIME/FORCE TABLE

41, MAGNITUDE AT NODE POINT

550



DONE BY: ML DATE: 5-12-83

CHKD BY: ML DATE: 5-12-83

Technical Report
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Revision 0

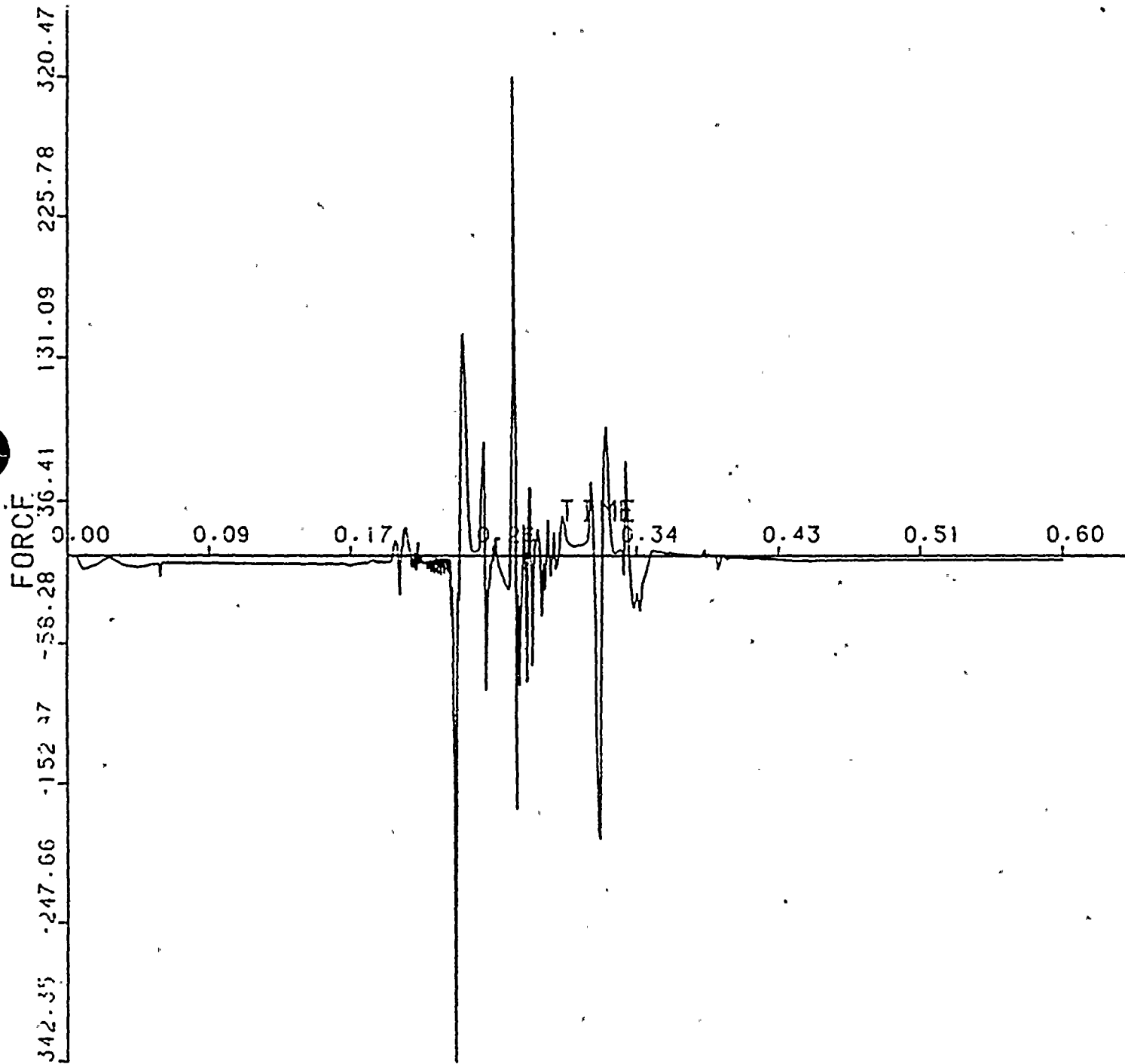
SAP2SAP VERIFICATION 5364

12-MAY-83

YELLOW LOOP SEAL - YELLPSL.TMP

TIME/FORCE TABLE 42. MAGNITUDE AT NODE POINT

555



DONE BY: MZ DATE: 5-12-83

CHKD BY: MZ DATE: 5-12-83

Technical Report
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SAP2SAP VERIFICATION 5364

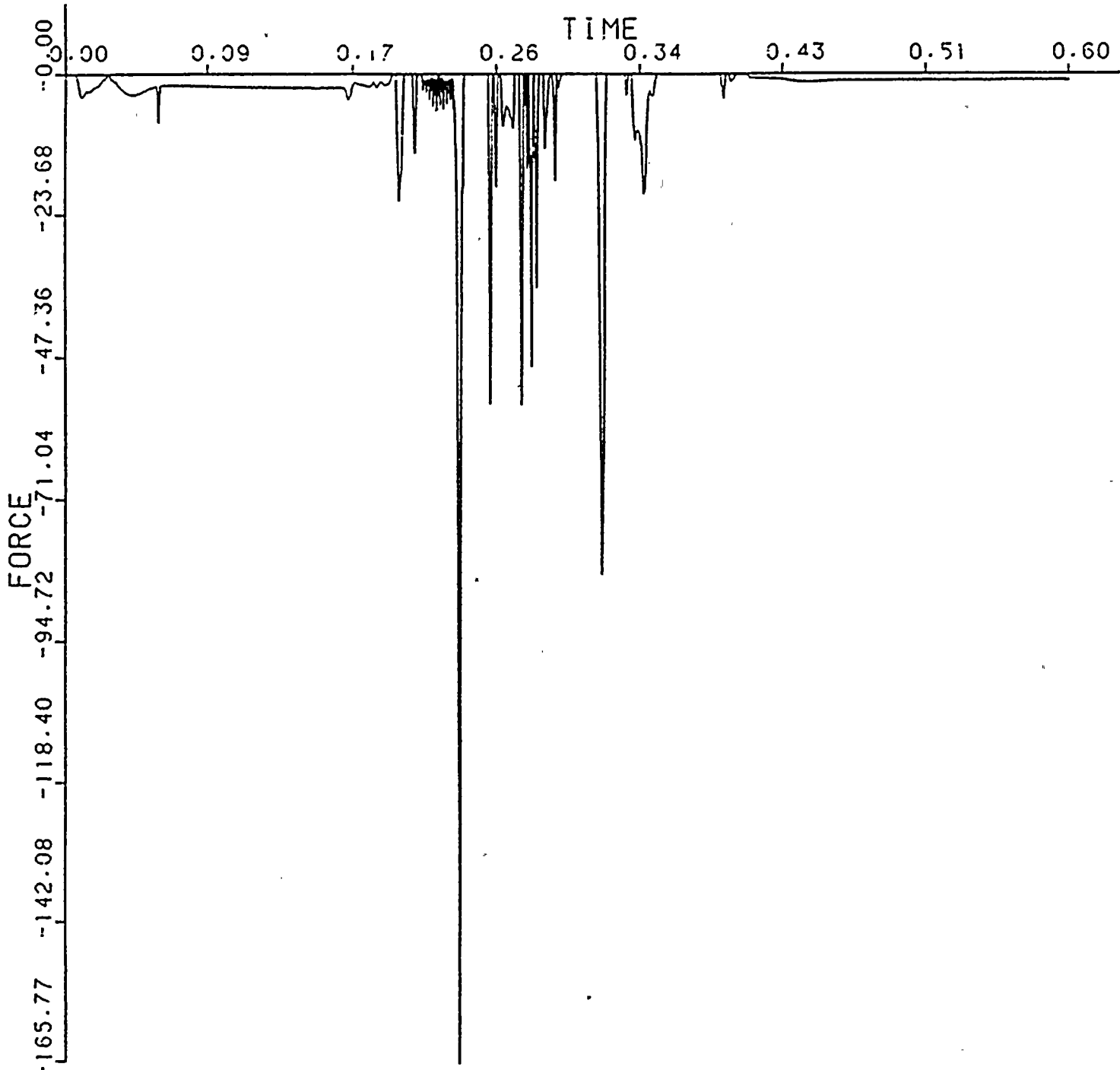
12-MAY-83

YELLOW LOOP SEAL - YELLPSL.TMP

TIME/FORCE TABLE

43. MAGNITUDE AT NODE POINT

560



DONE BY: MR DATE: 5-12-83

CHKD BY: MM DATE: 5-12-83

Technical Report

TR-5364-1

Revision 0

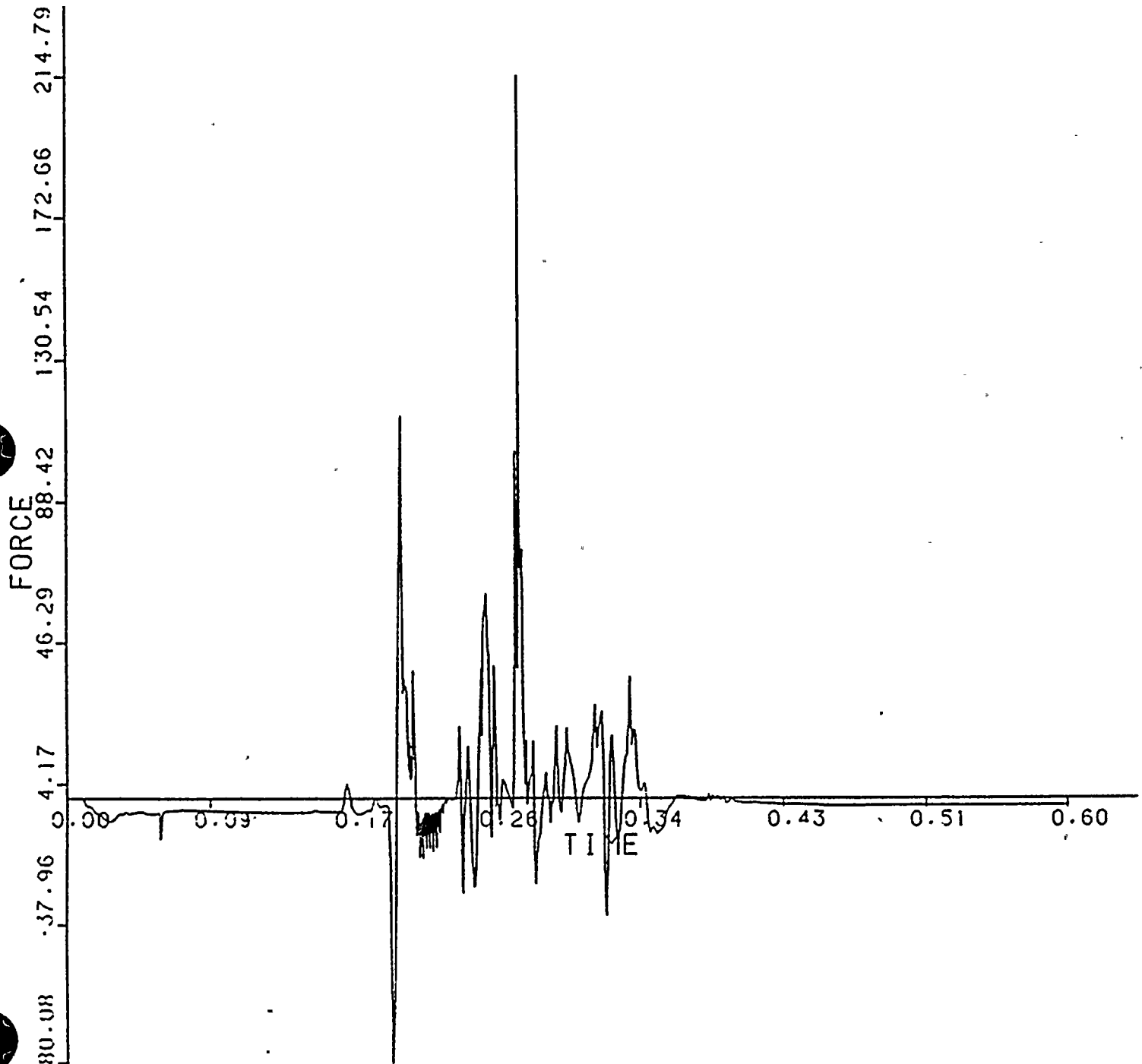
SAP2SAP VERIFICATION 5364

12-MAY-83

YELLOW LOOP SEAL - YELLPSL.TMP

TIME/FORCE TABLE 44. MAGNITUDE AT NODE POINT

300



DONE BY: HL DATE: 5-12-83

CHKD BY: ML DATE: 5-12-83

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TELEDYNE
ENGINEERING SERVICES

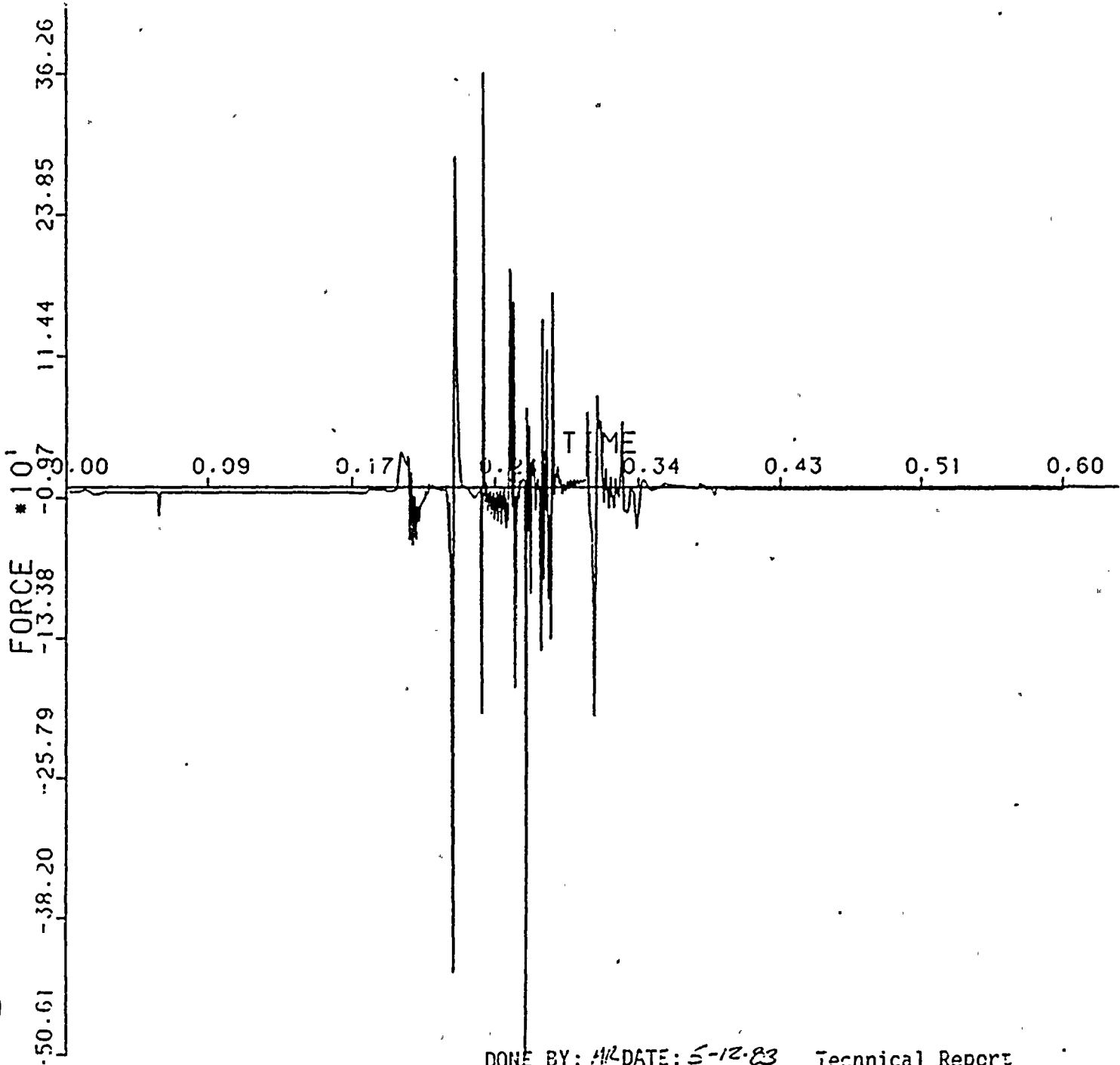
SAP2SAP VERIFICATION 5364

12-MAY-83

YELLQW LOOP SEAL - YELLPSL.TMP

TIME/FORCE TABLE 45. MAGNITUDE AT NODE POINT

375



DONE BY: ML DATE: 5-12-83

CHKD BY: ML DATE: 5-12-83

Technical Report
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Revision C

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TELEDYNE
ENGINEERING SERVICES

SAP2SAP VERIFICATION 5364

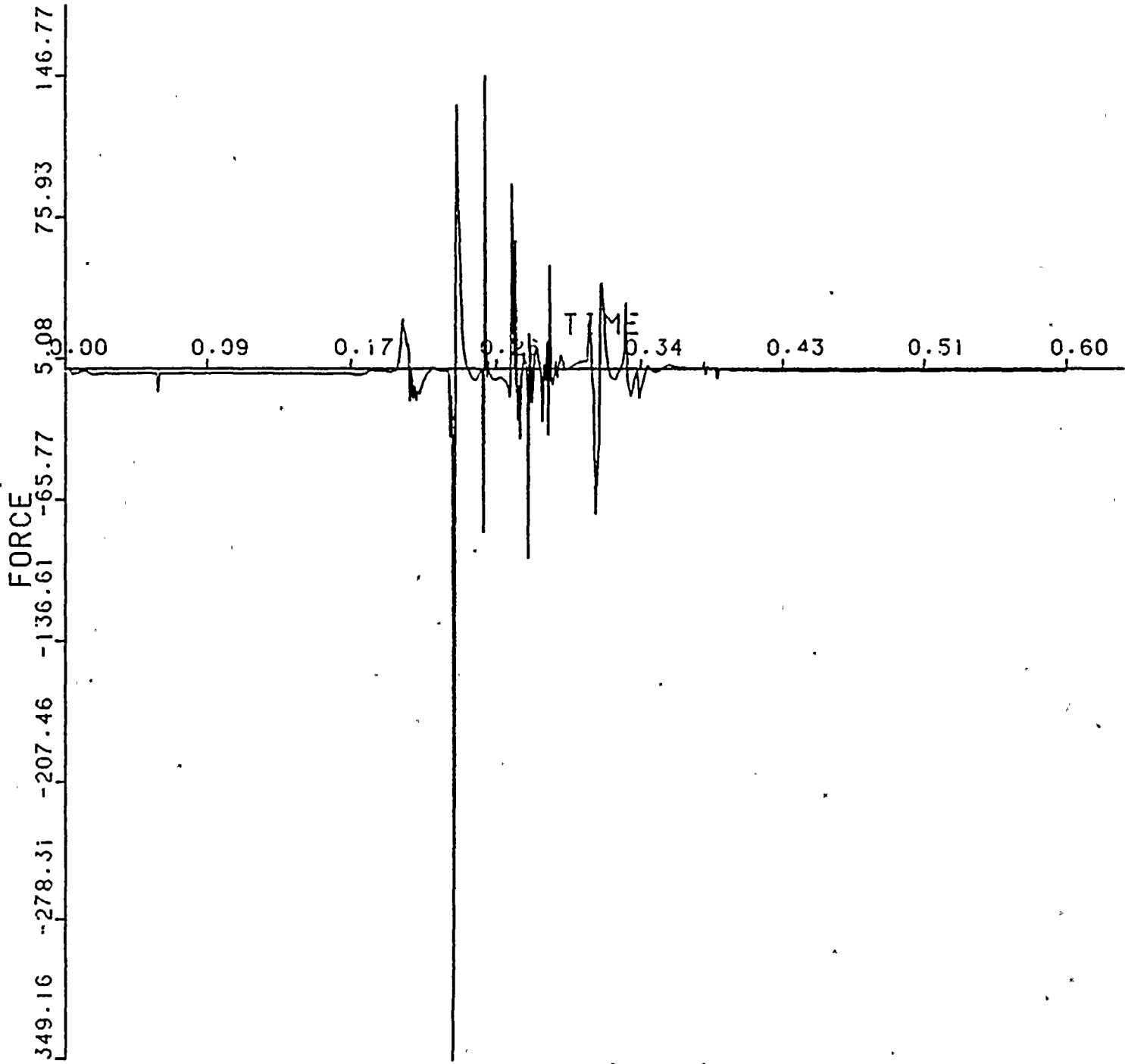
12-MAY-83

YELLOW LOOP SEAL - YELLPSL.TMP

TIME/FORCE TABLE

46. MAGNITUDE AT NODE POINT

365



DONE BY: AVL DATE: 5-12-83

CHKD BY: AVL DATE: 5-12-83

Technical Report
TR-5364-1
Revision 0



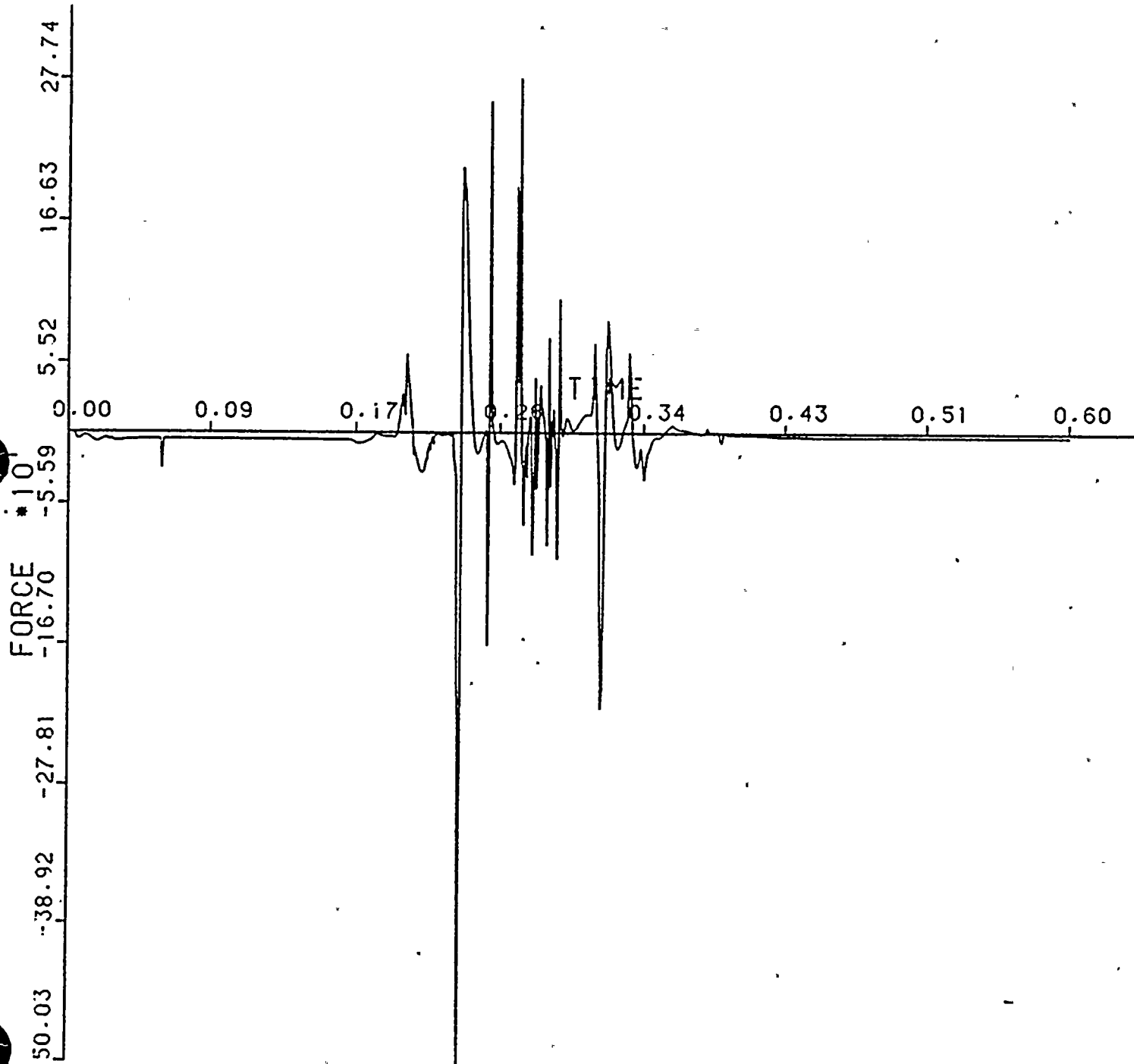
SAP2SAP VERIFICATION 5364

12-MAY-83

YELLOW LOOP SEAL - YELLPSL.TMP

TIME/FORCE TABLE .47, MAGNITUDE AT NODE POINT

360



DONE BY: ML DATE: 5-12-83

CHKD BY: LL DATE: 5-12-83

Technical Report
TR-5364-1
Revision C

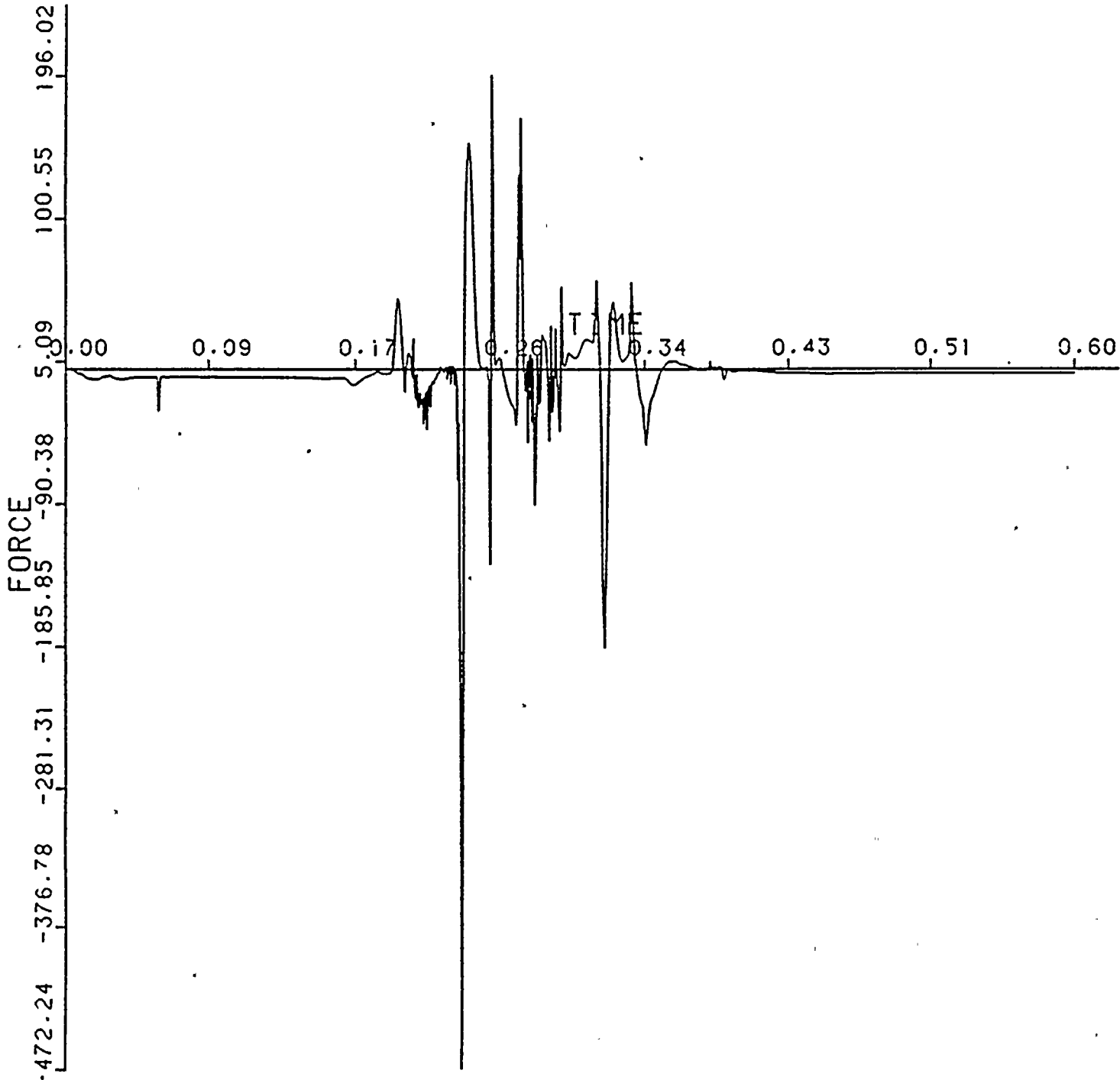
SAP2SAP VERIFICATION 5364

12-MAY-83

YELLOW LOOP SEAL - YELLPSL.TMP

TIME/FORCE TABLE 48. MAGNITUDE AT NODE POINT

355



DONE BY: ML DATE: 5-12-83

CHKD BY: ML DATE: 5-12-83

Technical Report
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TELEDYNE
ENGINEERING SERVICES

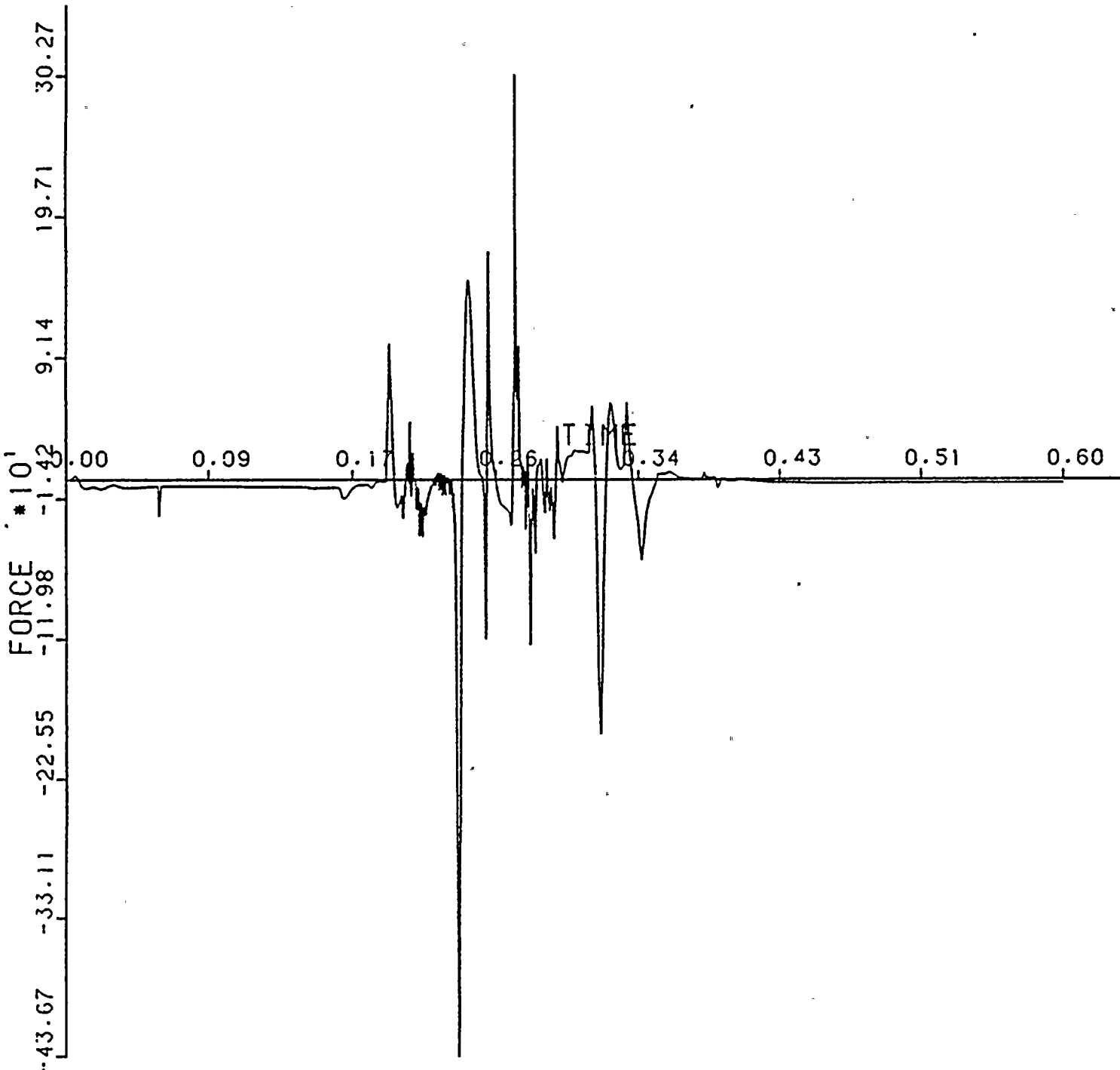
SAP2SAP VERIFICATION 5364

12-MAY-83

YELLOW LOOP SEAL - YELLPSL.TMP.

TIME/FORCE TABLE 49. MAGNITUDE AT NODE POINT

350



DONE BY: MZ DATE: 5-12-83

CHKD BY: UL DATE: 5-12-83

Technical Report
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Revision 0

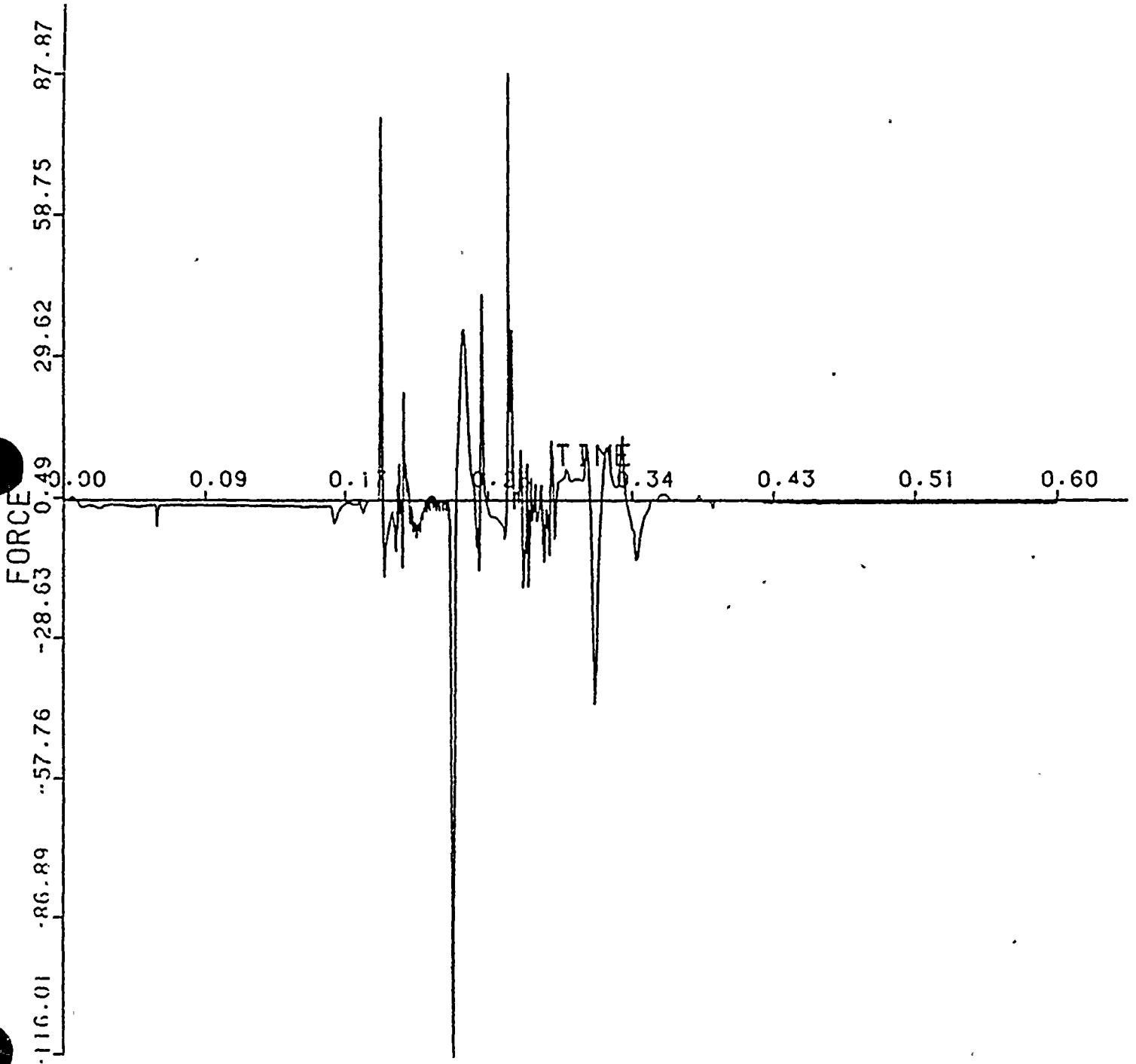
SAP2SAP VERIFICATION 5364

12-MAY-83

YELLOW LOOP SEAL - YELPSL.TMP

TIME/FORCE TABLE 50. MAGNITUDE AT NODE POINT

340



DONE BY: ML DATE: 5-12-83

CHKD BY: ML DATE: 5-12-83

Technical Report
TR-5364-1
Revision 0

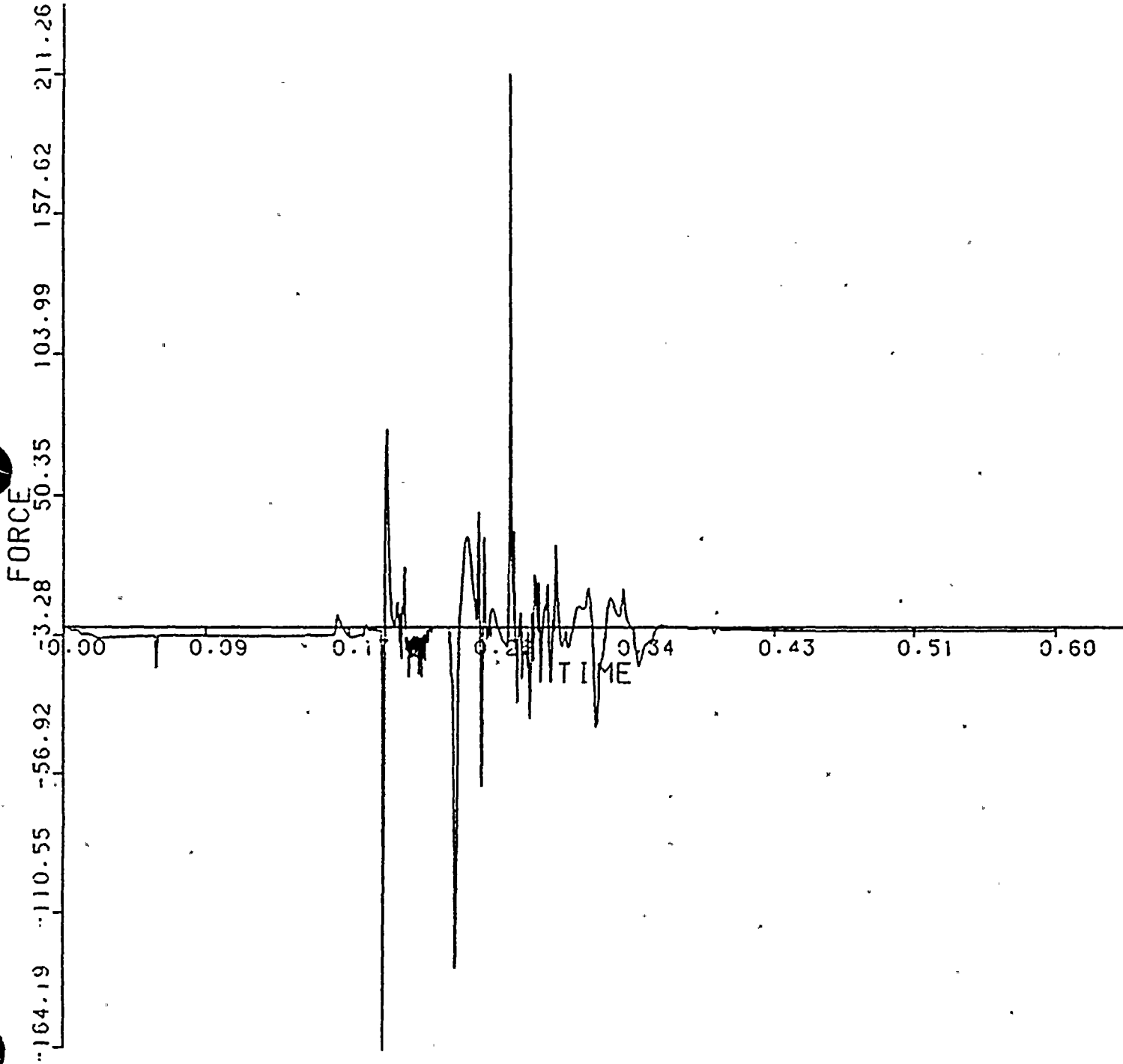
SAP2SAP VERIFICATION 5364

12-MAY-83

YELLOW LOOP SEAL - YELLP.L.TMP

TIME/FORCE TABLE 51. MAGNITUDE AT NODE POINT

335



DONE BY: ML DATE: 5-12-83

CHKD BY: ML DATE: 5-12-83

Technical Report
TR-5364-1
Revision 0

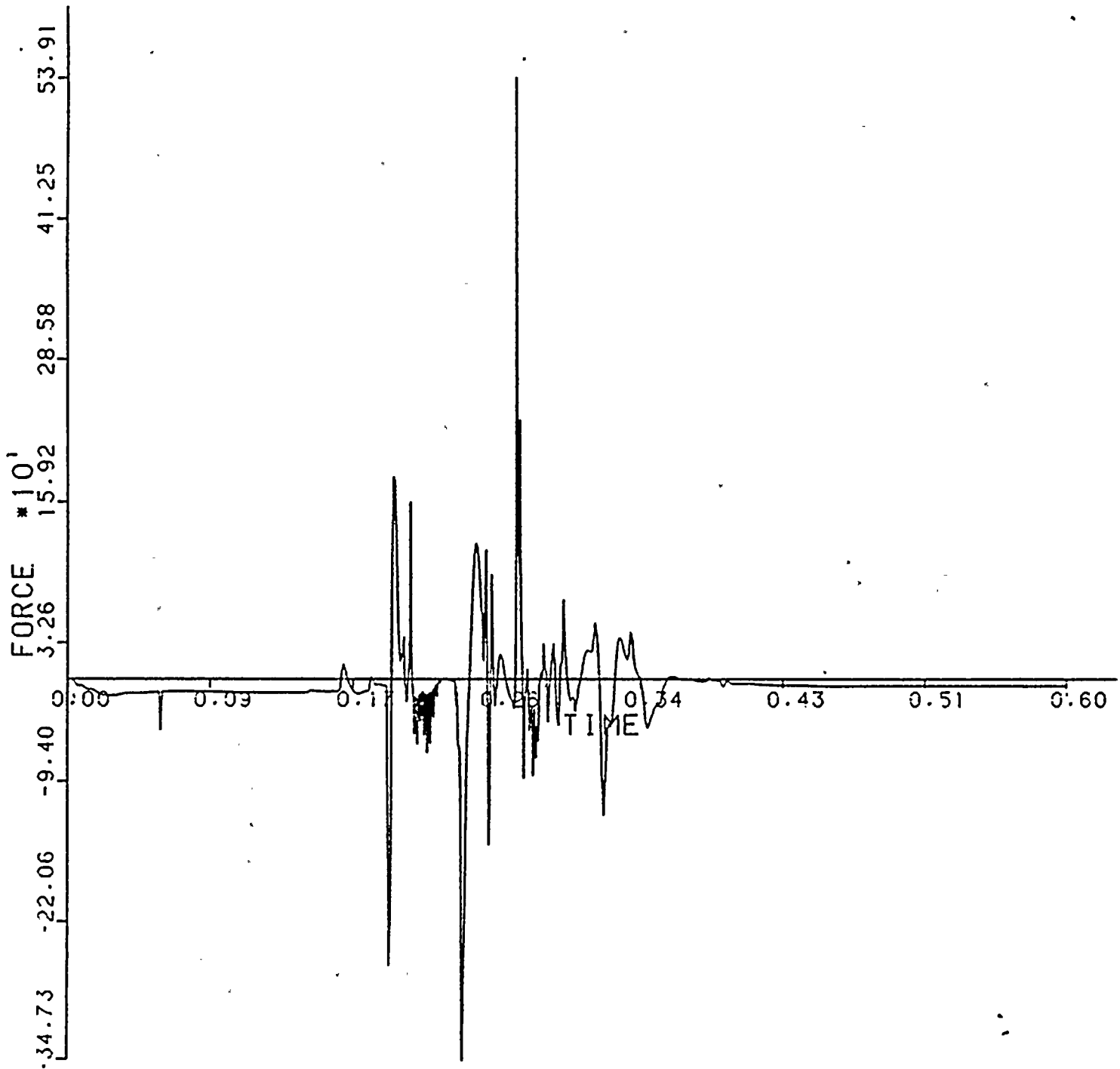
SAP2SAP VERIFICATION 5364

12-MAY-83

YELLOW LOOP SEAL - YELLPSL.TMP

TIME/FORCE TABLE '52, MAGNITUDE AT NODE POINT

325



DONE BY: HL DATE: 5-12-83

CHKD BY: LL DATE: 5-12-83

Technical Report
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Revision C



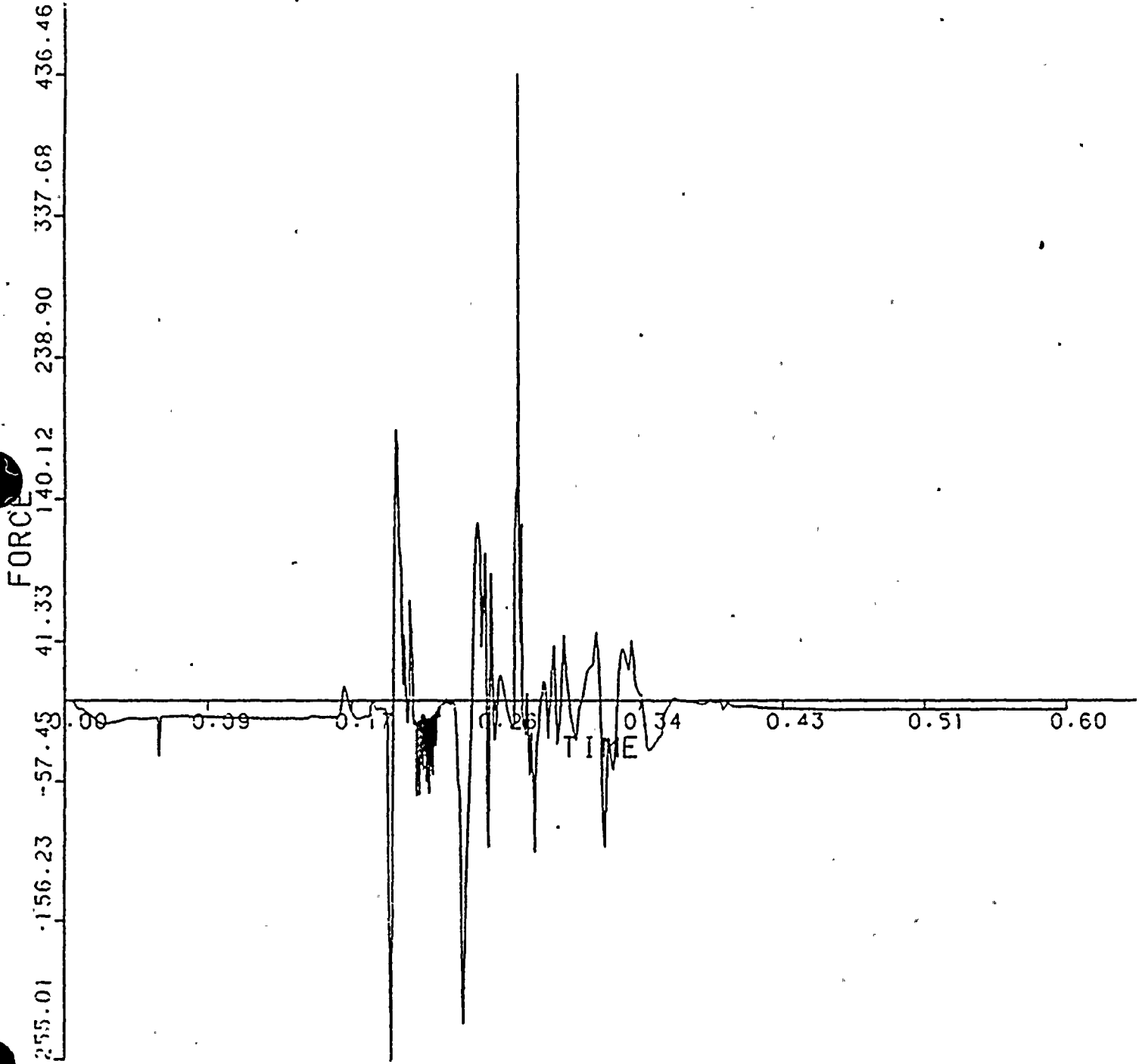
SAP2SAP VERIFICATION 5364

12-MAY-83

YELLOW LOOP SEAL - YELLPSL.TMP

TIME/FORCE TABLE '53. MAGNITUDE AT NODE POINT

320



DONE BY: ML DATE: 5-12-83

CHKD BY: ML DATE: 5-12-83

Technical Report
TR-5364-j
Revision 0

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WTFLEDYNE
ENGINEERING SERVICES

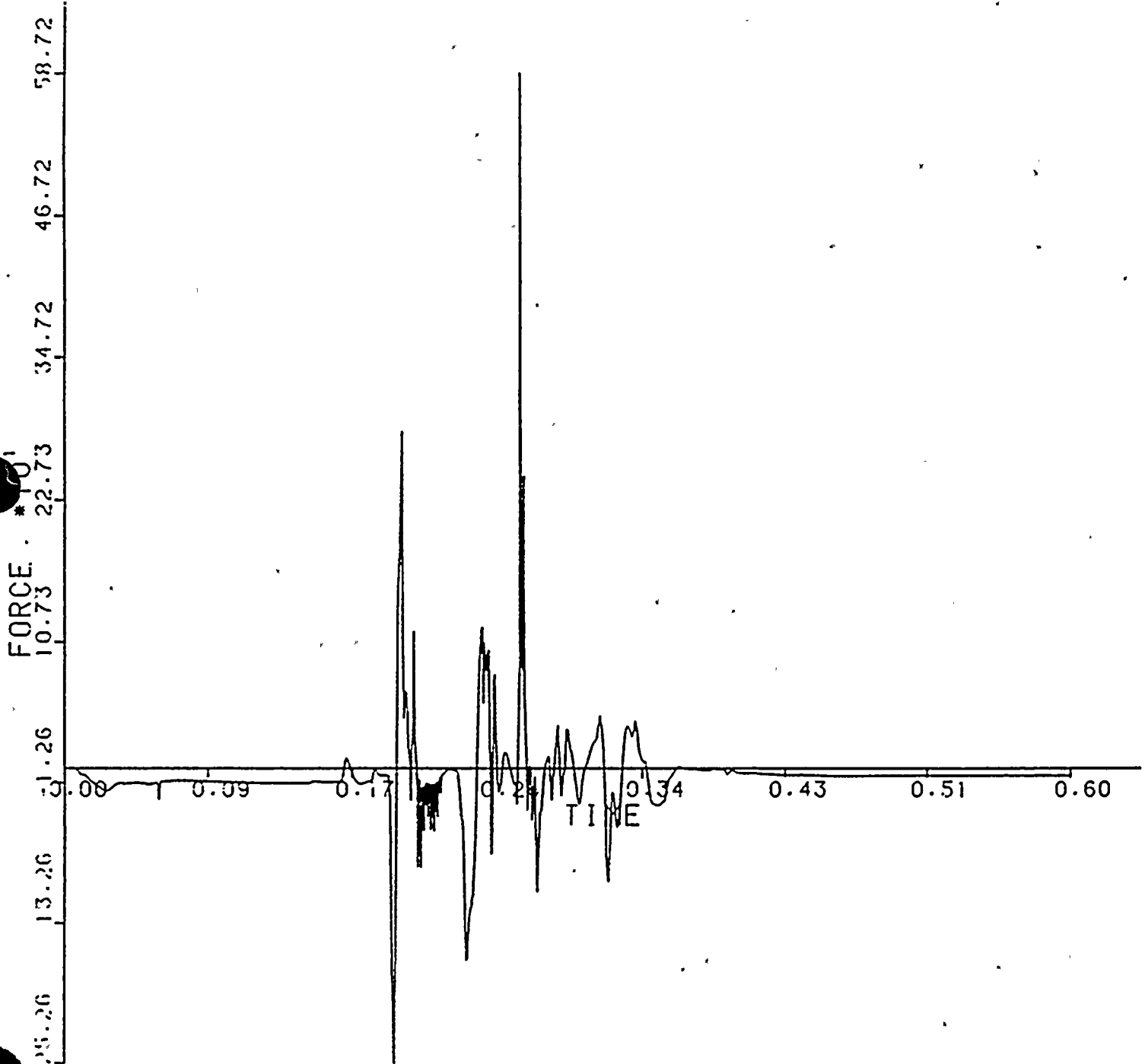
SAP2SAP VERIFICATION 5364

12-MAY-83

YELLOW LOOP SEAL - YELLPSL.TMP

TIME/FORCE TABLE 54, MAGNITUDE AT NODE POINT

310



DONE BY: MK DATE: 5-12-83

CHKD BY: LIL DATE: 5-12-83

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Revision 0

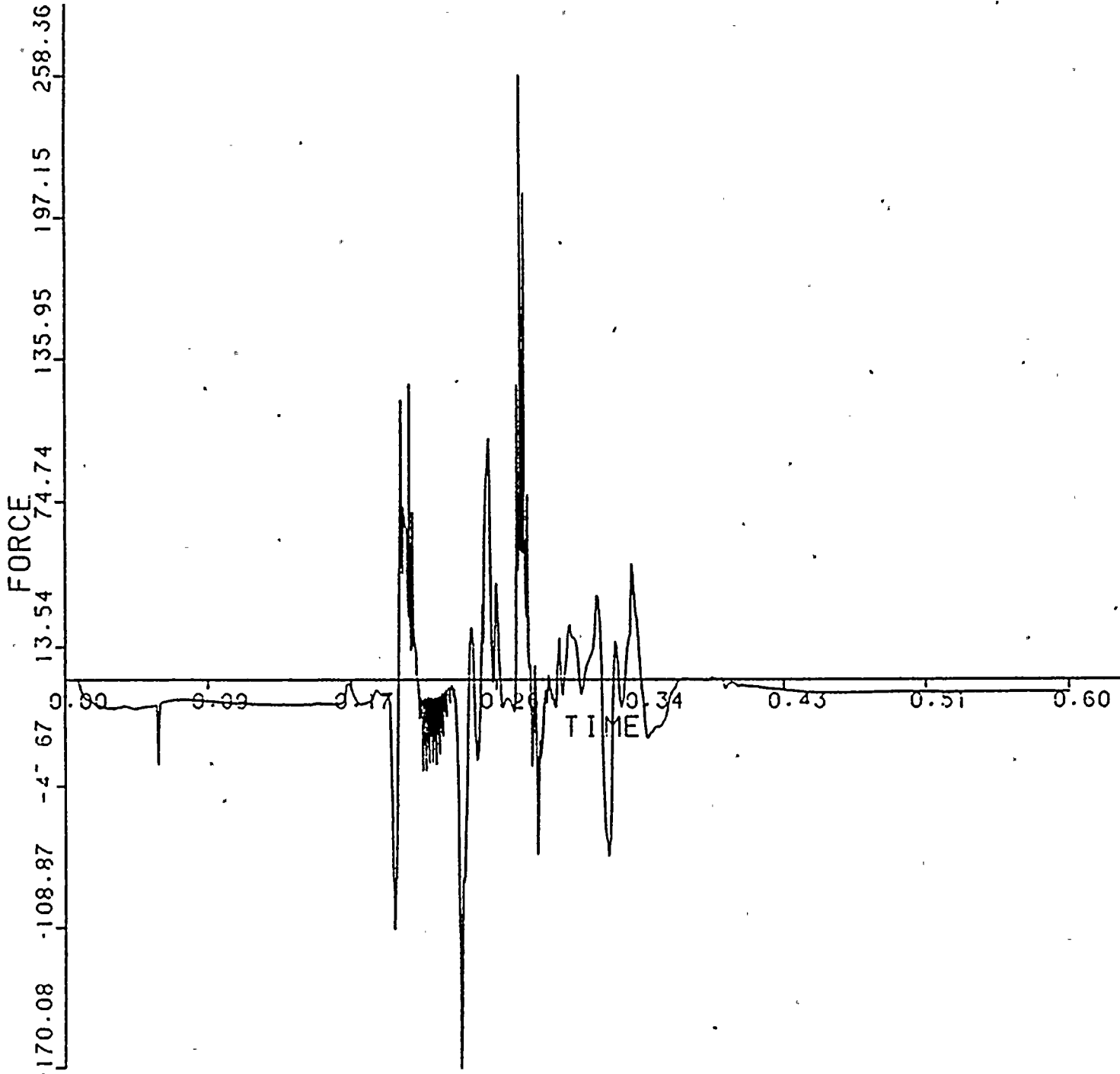
SAP2SAP VERIFICATION 5364

12-MAY-83

YELLOW LOOP SEAL - YELLPSL.TMP

TIME/FORCE TABLE 55, MAGNITUDE AT NODE POINT

295



DONE BY: ML DATE: 5-12-83

CHKD BY: ML DATE: 5-12-83

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 **TELEDYNE
ENGINEERING SERVICES**

4.8.2 Unit 1 - 400⁰ Solid Liquid Case

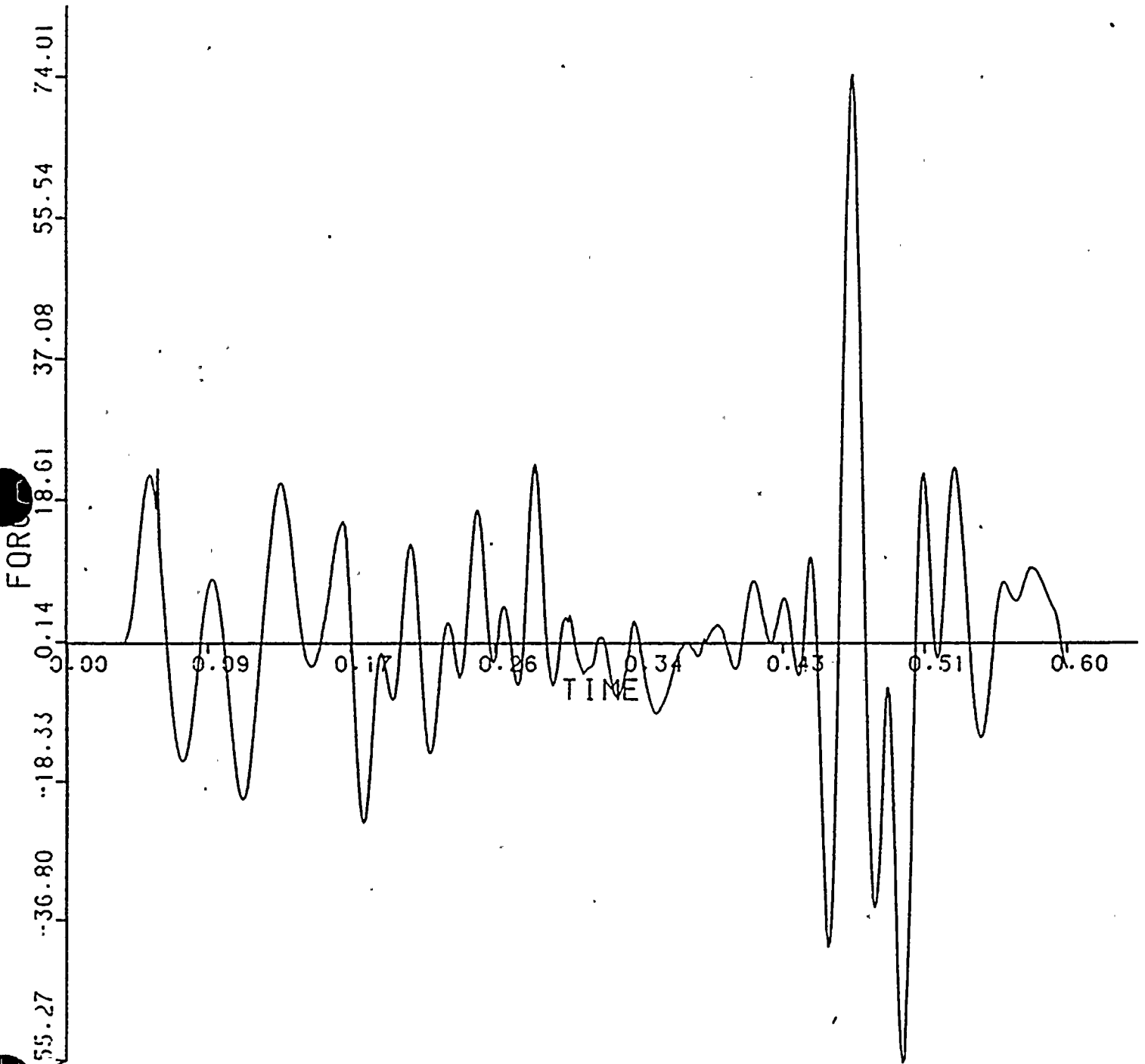
SAP2SAP VERIFICATION 5364

23-MAY-83

YEL-RED SOLID UNIT 1, 0-600 MS

TIME/FORCE TABLE 1, MAGNITUDE AT NODE POINT

.109



DONE BY: M DATE: 5-23-83

CHKD BY: M DATE: 5-25-83

SAP2SAP VERIFICATION 5364

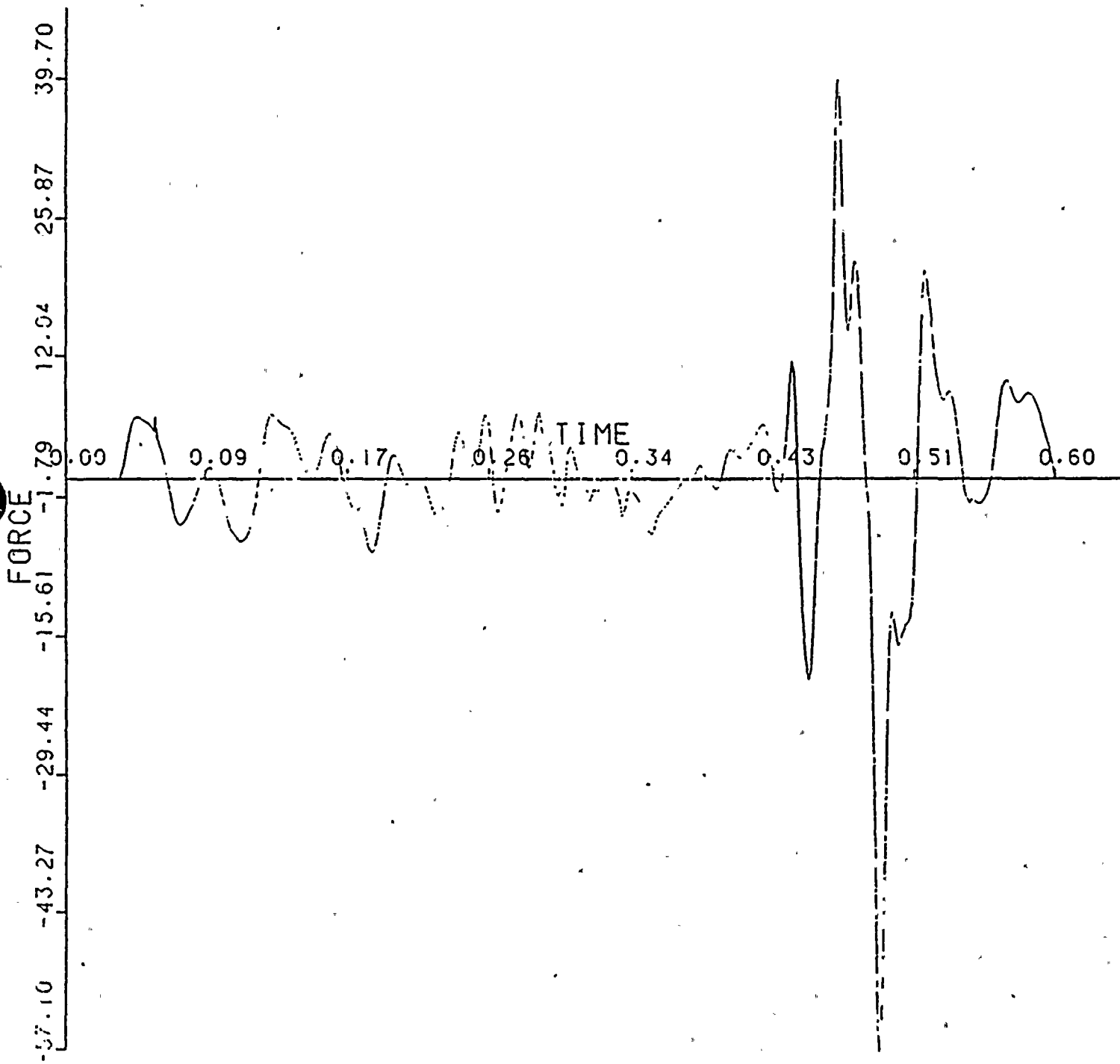
23-MAY-83

YEL-RED SOLID UNIT 1, 0-600 MS

TIME/FORCE TABLE

2, MAGNITUDE AT NODE POINT

104



DONE BY: 4/2 DATE: 5-17-83

CHKD BY: 3/4 DATE: 5-25-83

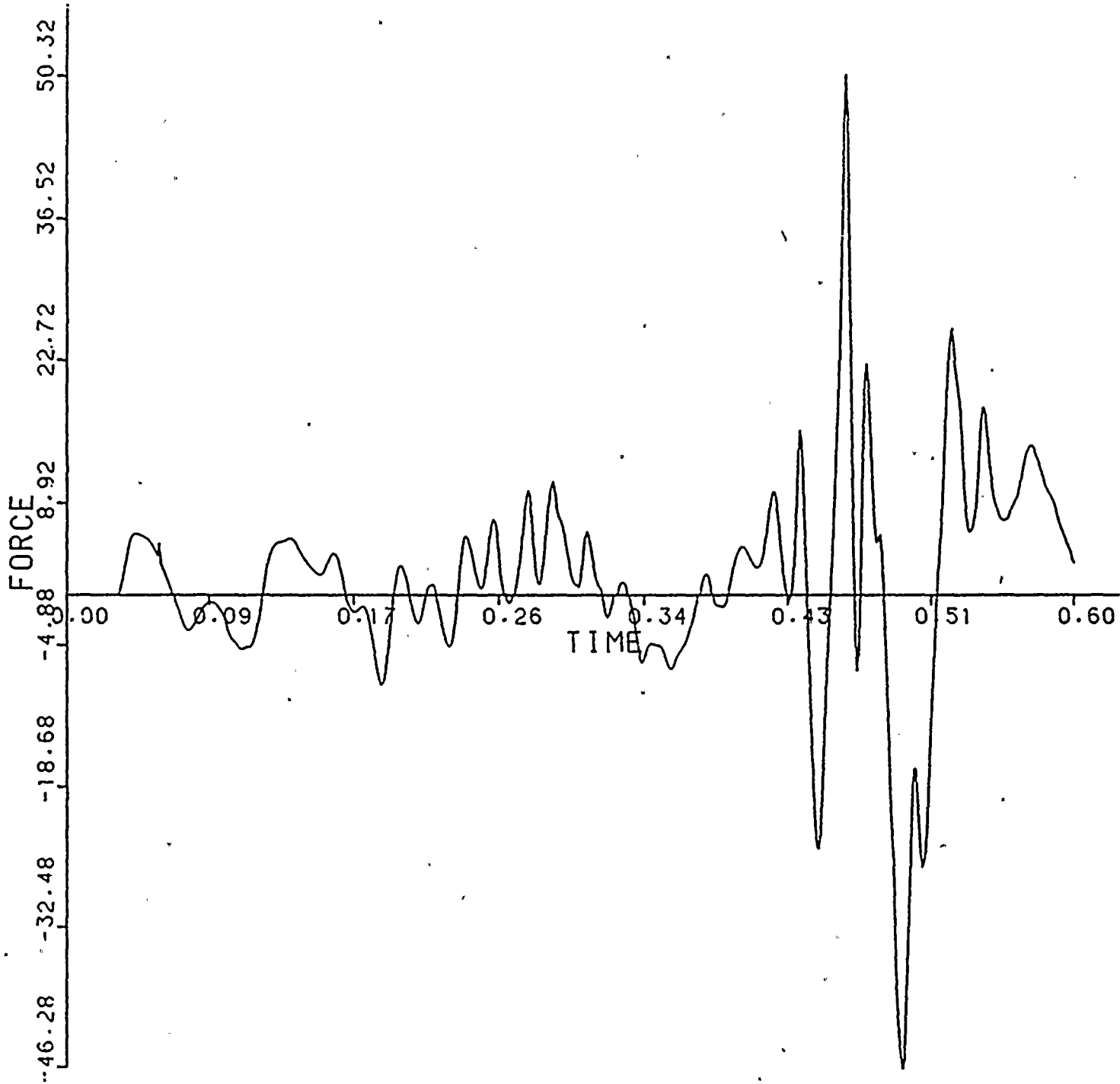
SAP2SAP VERIFICATION 5364

23-MAY-83

YEL-RED SOLID UNIT 1, 0-600 MS

TIME/FORCE TABLE 3. MAGNITUDE AT NODE POINT

103



DONE BY: 4/2 DATE: 5-12-83

CHKD BY: 1/1 DATE: 5-25-83



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TELEDYNE
ENGINEERING SERVICES

SAP2SAP VERIFICATION 5364

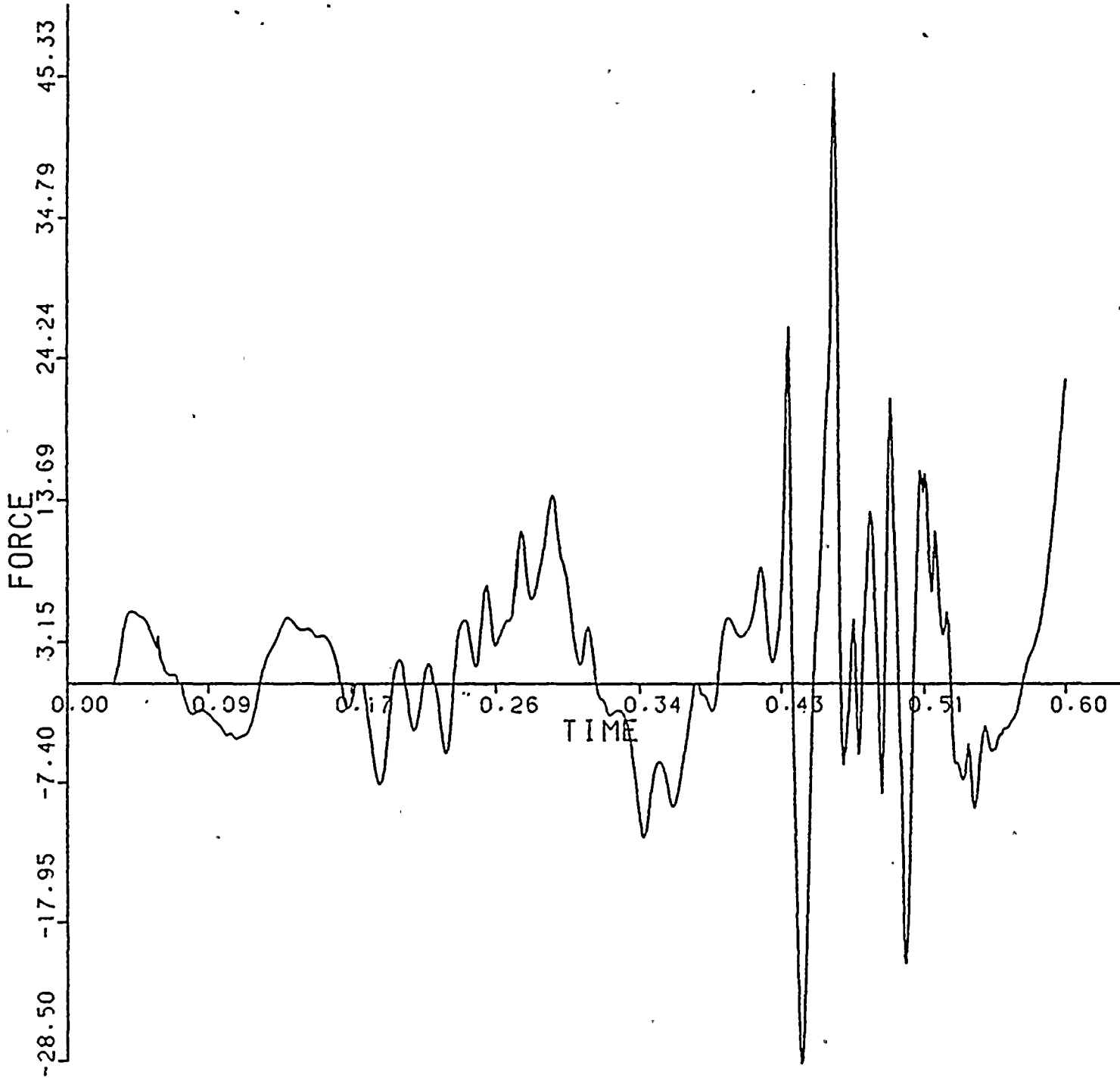
23-MAY-83

YEL-RED SOLID UNIT 1, 0-600 MS

TIME/FORCE TABLE

4. MAGNITUDE AT NODE POINT

102



DONE BY: ME DATE: 5-2-83

CHKD BY: JM DATE: 5-25-83

Technical Report
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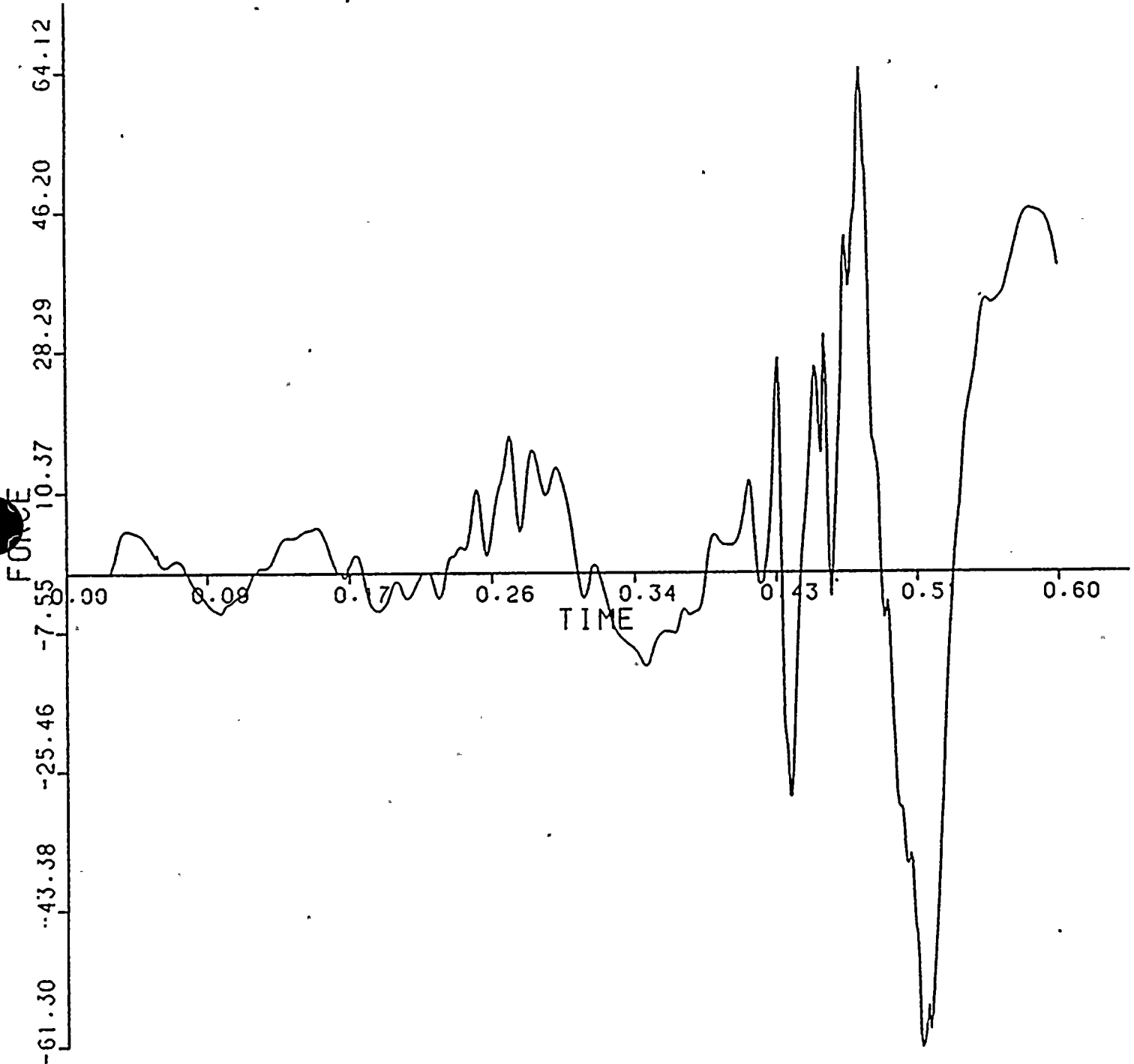
TELEDYNE
ENGINEERING SERVICES

23-MAY-83

SAP2SAP VERIFICATION 5364

YEL-RED SOLID UNIT 1, 0-600 MS

TIME/FORCE TABLE 5, MAGNITUDE AT NODE POINT 100



DONE BY: ME DATE: 5-23-83

CHKD BY: ME DATE: 5-25-83



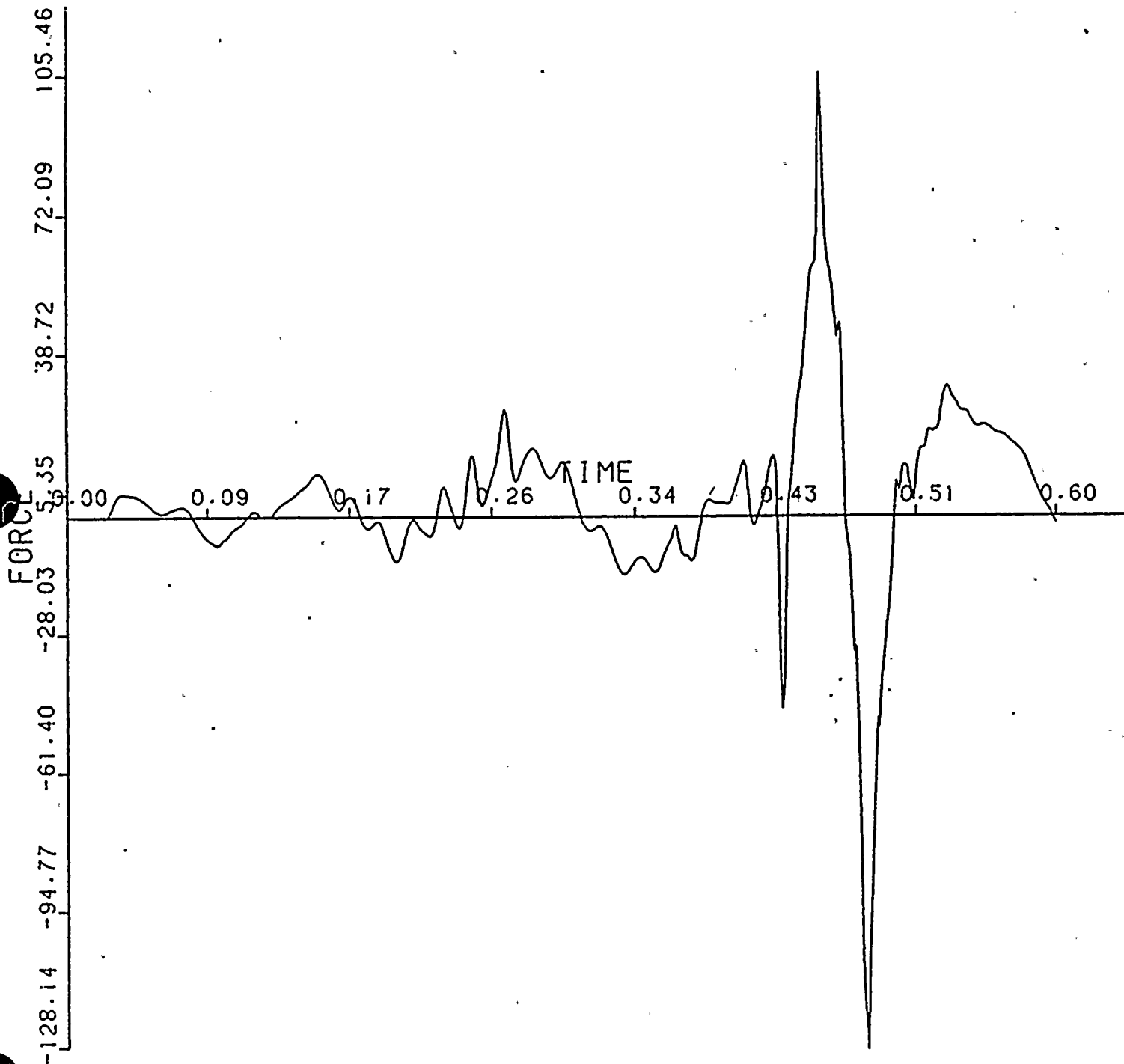
SAP2SAP VERIFICATION 5364

23-MAY-83

YEL-RED SOLID UNIT 1, 0-600 MS

TIME/FORCE TABLE 6, MAGNITUDE AT NODE POINT

99



DONE BY: 42 DATE: 5-12-83
CHKD BY: 11 DATE: 5-25-83

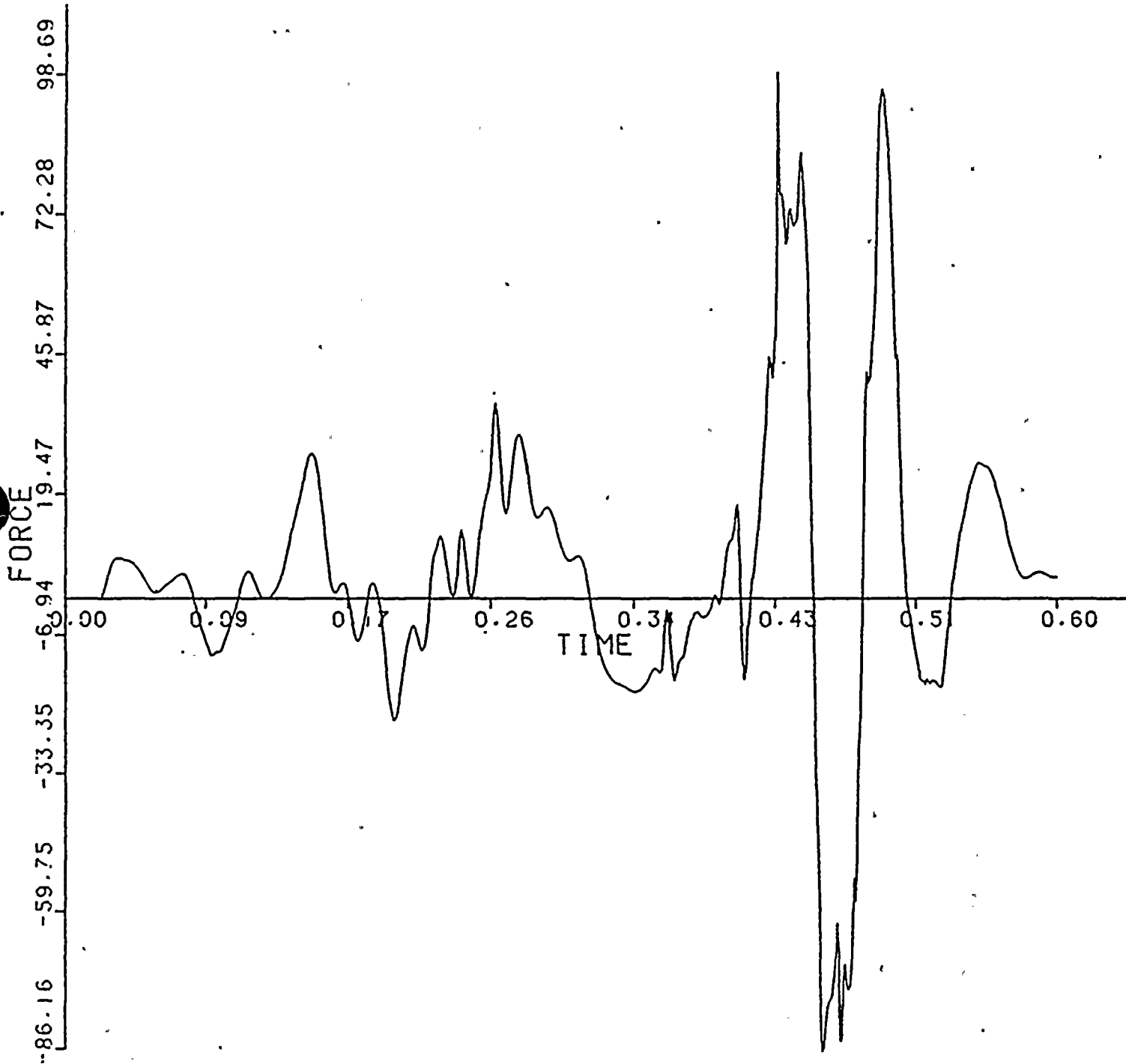


SAP2SAP VERIFICATION 5364

23-MAY-83

YEL-RED SOLID UNIT 1, 0-600 MS

TIME/FORCE TABLE 7, MAGNITUDE AT NODE POINT



DONE BY: VZ DATE: 5-2-83

CHKD BY: JH DATE: 5-25-83

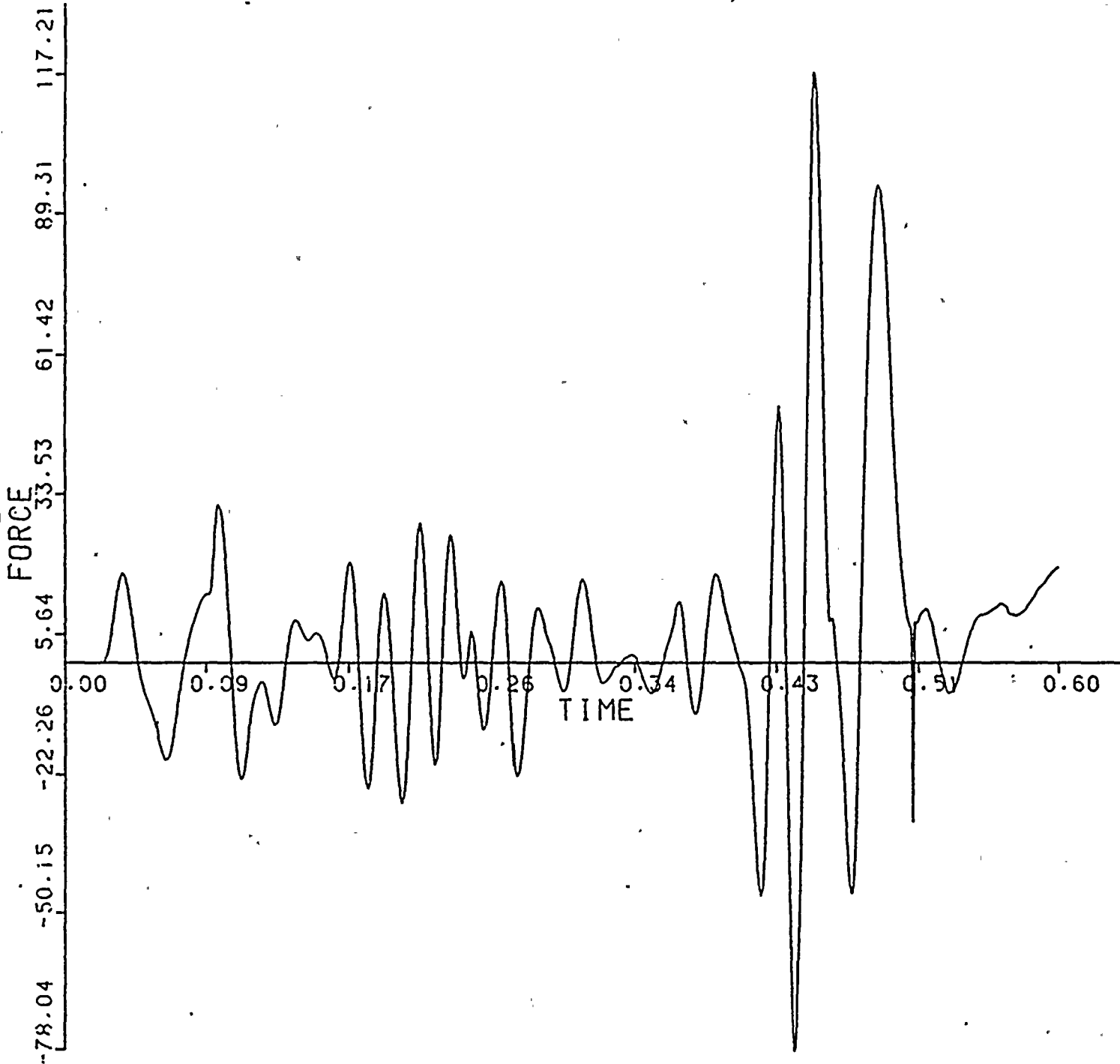
SAP2SAP VERIFICATION 5364

23-MAY-83

YEL-RED SOLID UNIT 1, 0-600 MS

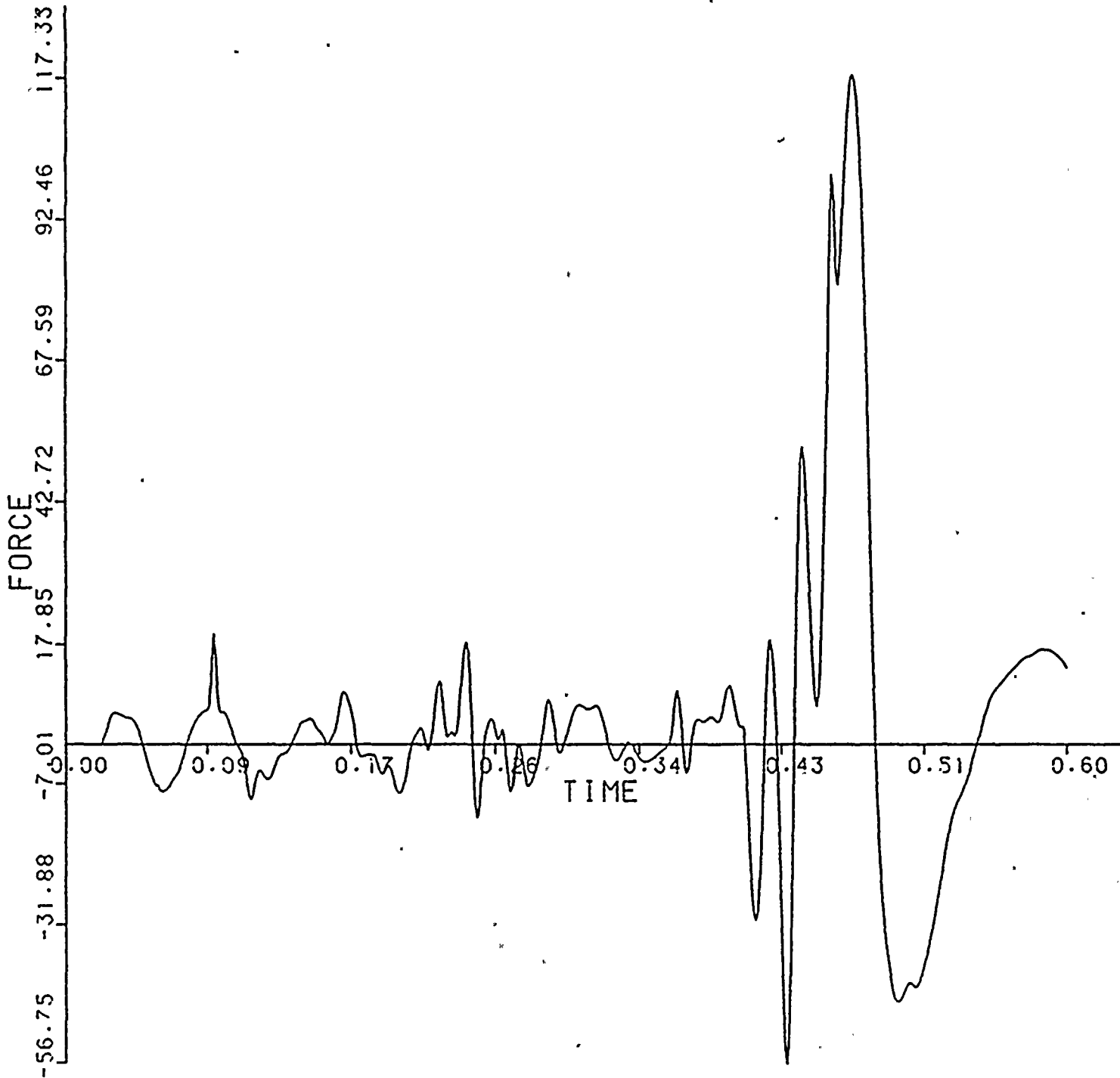
TIME/FORCE TABLE 8, MAGNITUDE AT NODE POINT

216



DONE BY: WZ DATE: 5-2-83

CHKD BY: MM DATE: 5-25-83



DONE BY: DATE: 5-23-83

CHKD BY: DATE: 5-25-83

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WILEY ENGINEERING SERVICES

SAP2SAP VERIFICATION 5364

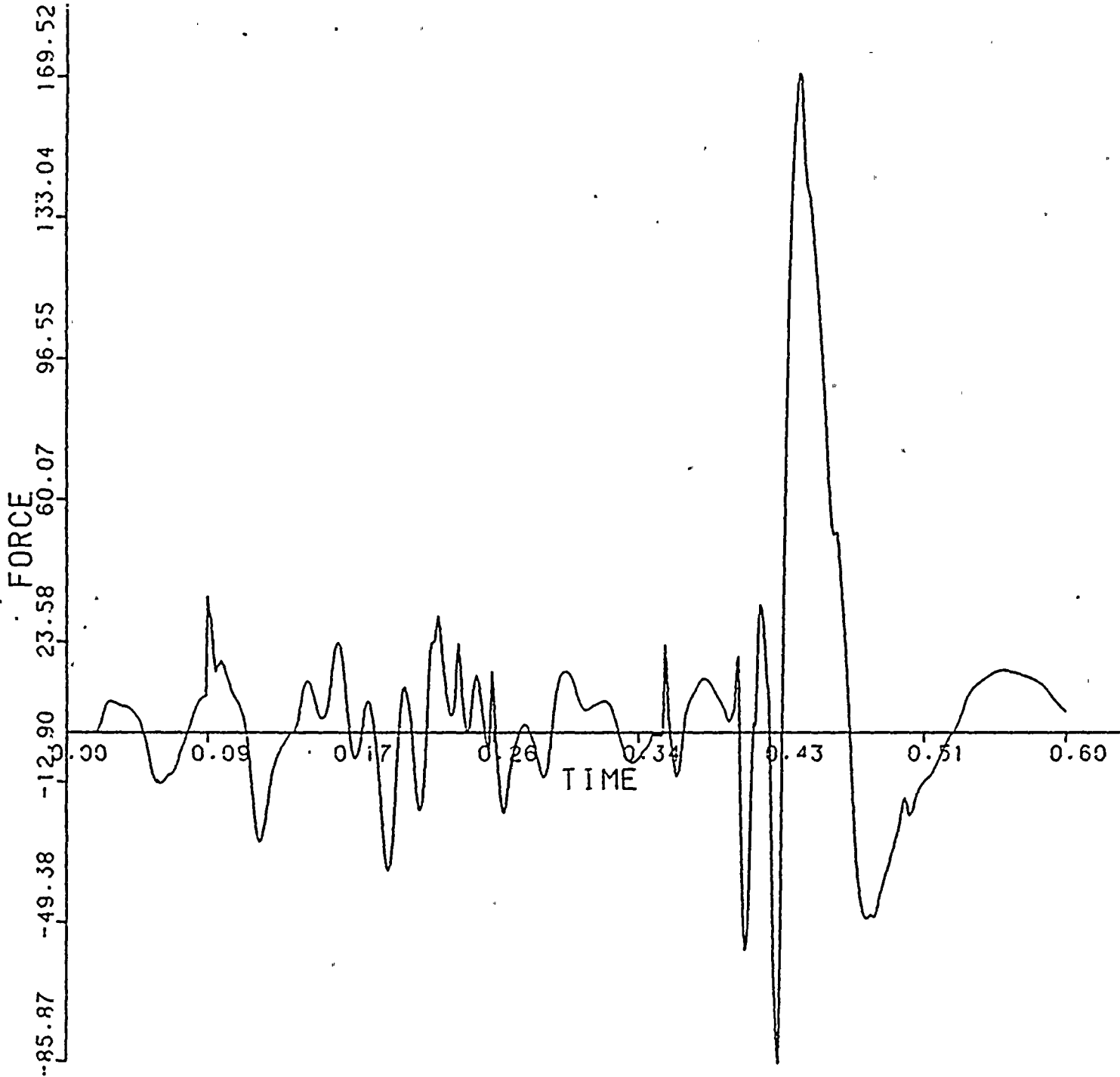
23-MAY-83

YEL-RED SOLID UNIT 1, 0-600 MS

TIME/FORCE TABLE

10. MAGNITUDE AT NODE POINT

208



DONE BY: VR DATE: 5-12-83

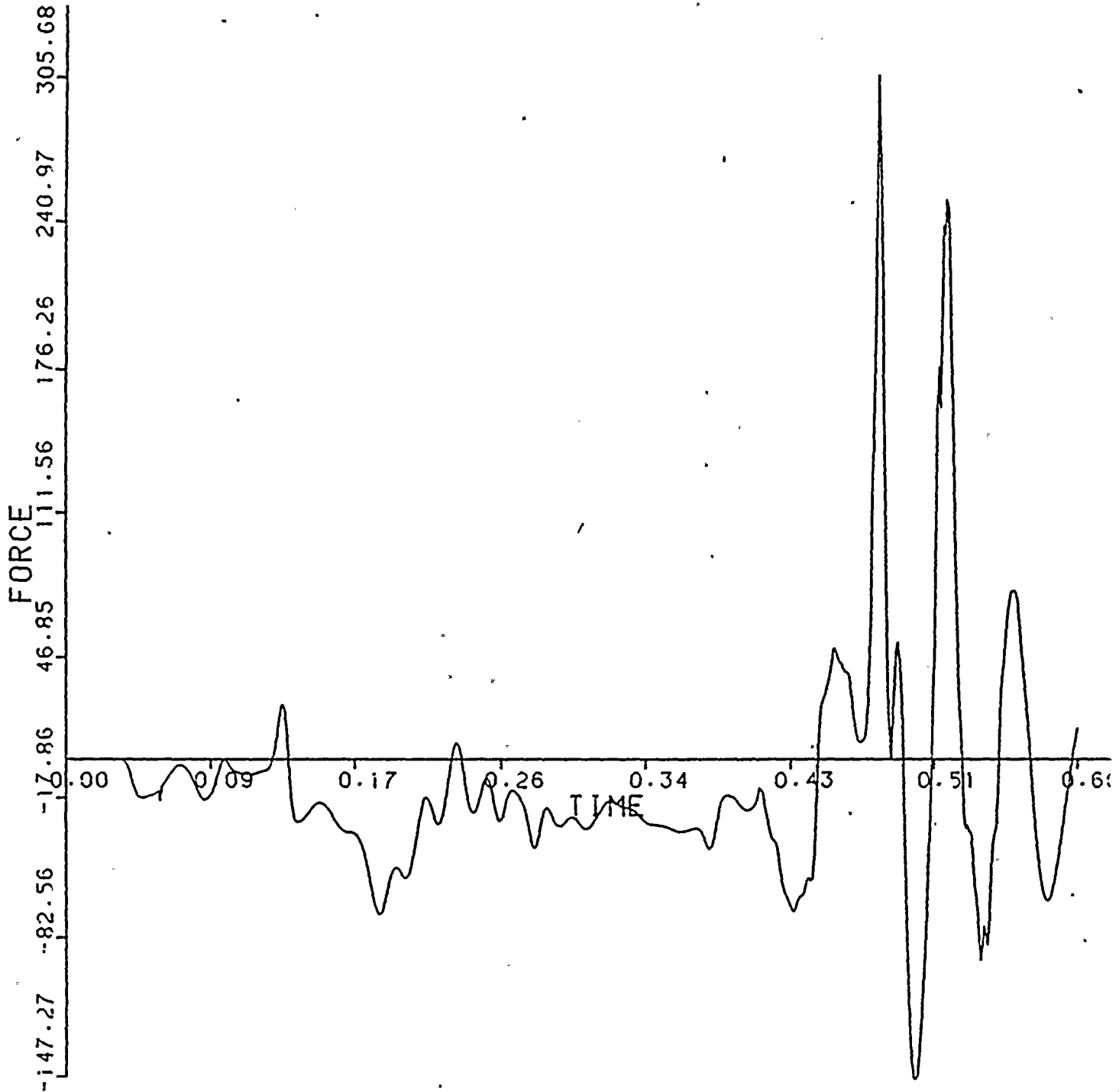
CHKD BY: MM DATE: 5-25-83

SAP2SAP VERIFICATION 5364

23-MAY-83

YEL-RED SOLID UNIT 1, 0-600 MS

TIME/FORCE TABLE 11, MAGNITUDE AT NODE POINT



DONE BY: HR DATE: 5-12-83

CHKD BY: MM DATE: 5-25-83

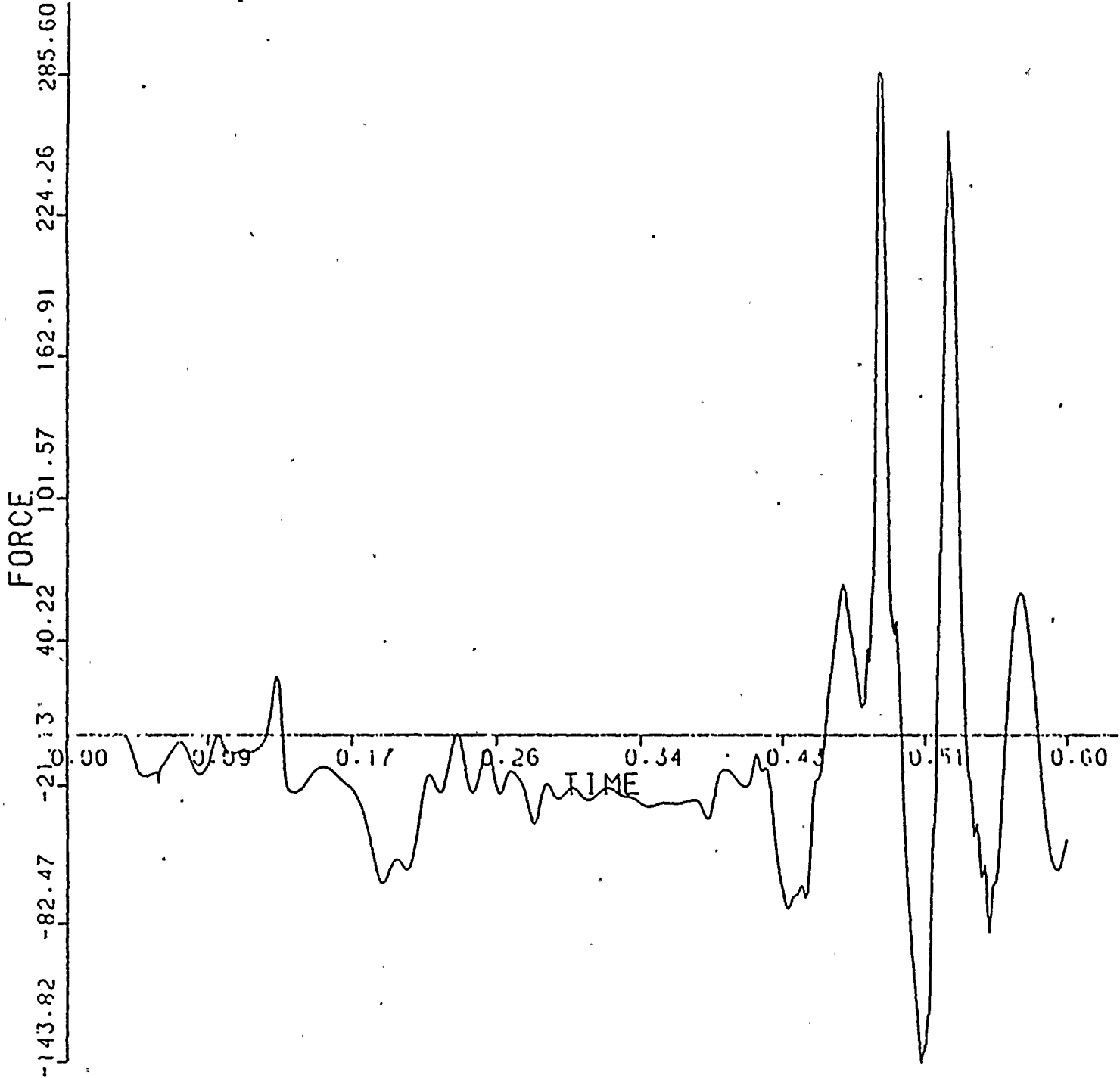
SAP2SAP VERIFICATION 5364

23-MAY-83

YEL-RED SOLID UNIT 1, 0-600 MS

TIME/FORCE TABLE 12, MAGNITUDE AT NODE POINT

83



DONE BY: MS DATE: 5-12-83

CHKD BY: 14 DATE: 5-25-83



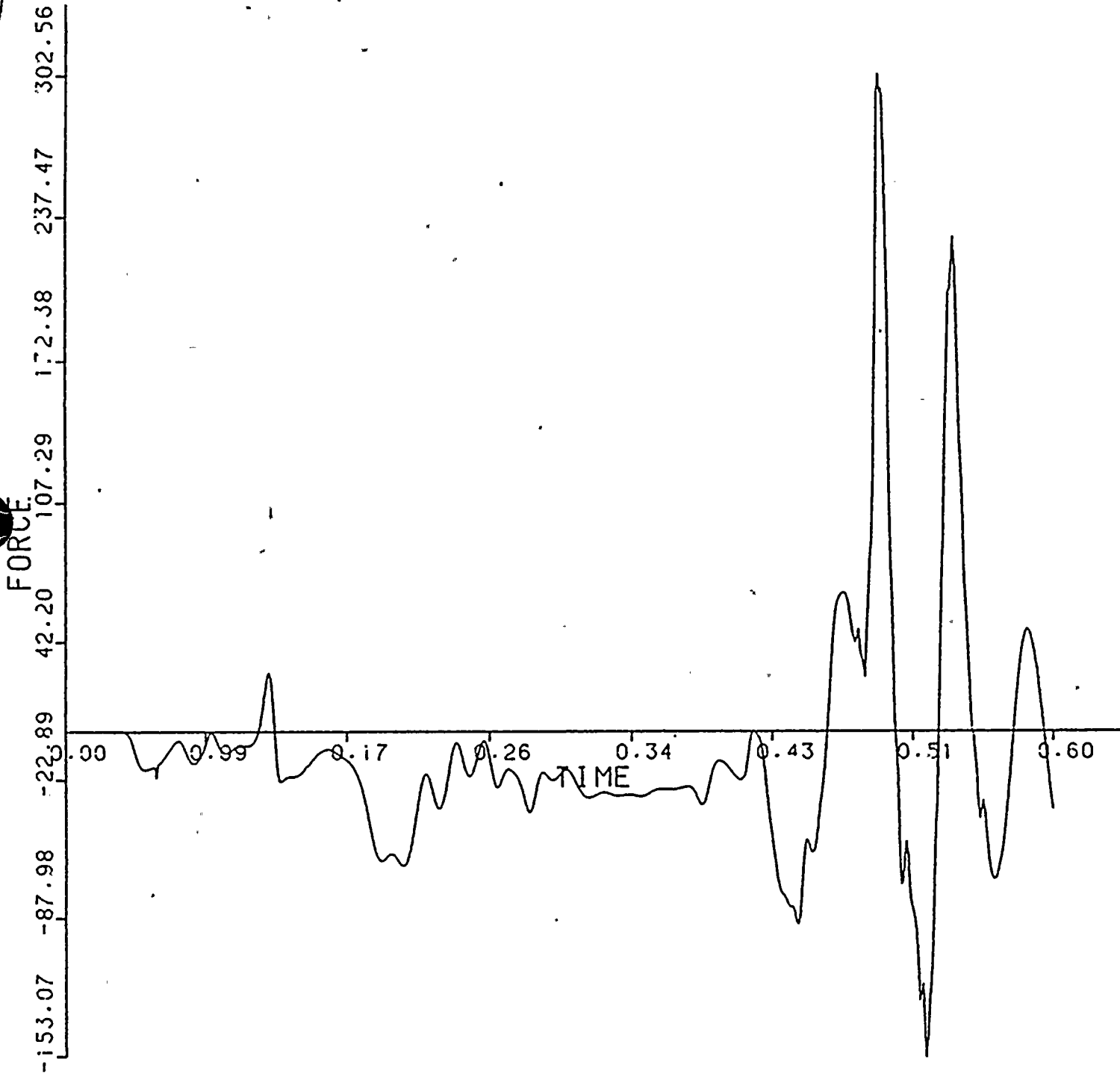
23-MAY-83

SAP2SAP VERIFICATION 5364

YEL-RED SOLID UNIT 1, 0-600 MS

TIME/FORCE TABLE 13, MAGNITUDE AT NODE POINT

80,



DONE BY: WZ DATE: 5-2-83

CHKD BY: WZ DATE: 5-2-83

SAP2SAP VERIFICATION 5364

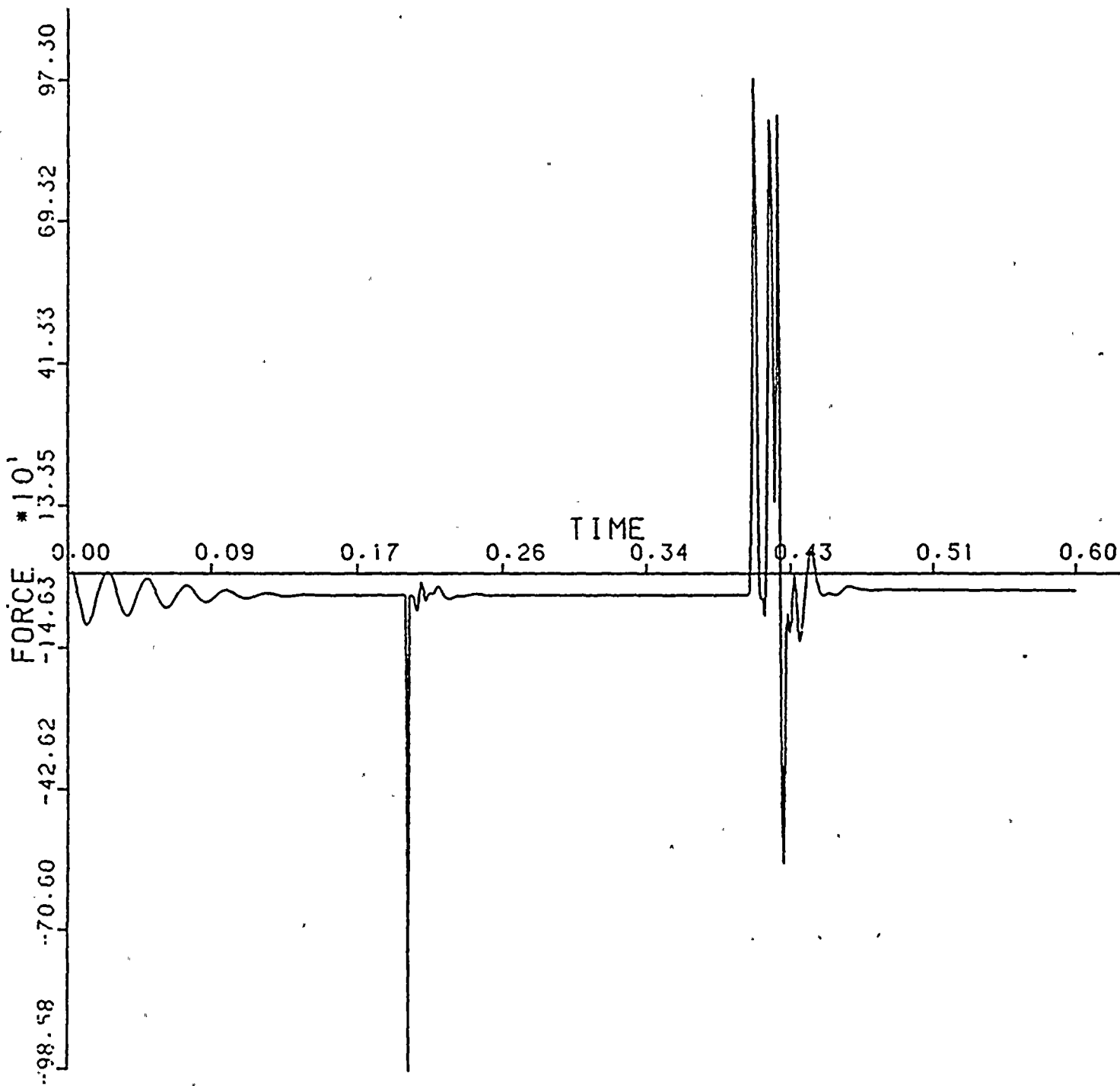
23-MAY-83

YEL-RED SOLID UNIT 1, 0-600 MS

TIME/FORCE TABLE

14, MAGNITUDE AT NODE POINT

725



DONE BY: DATE: 5-25-83

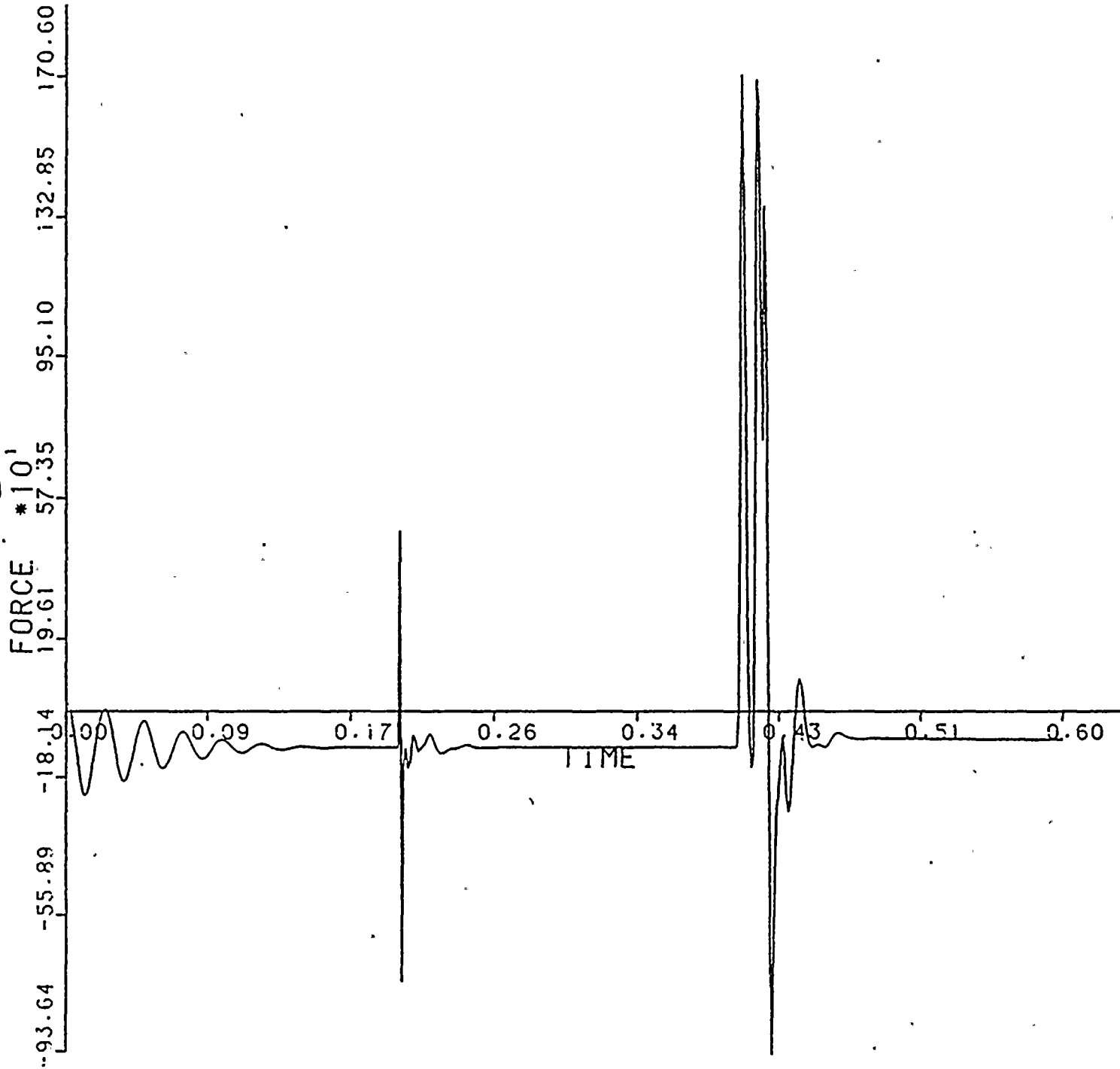
CHKD BY: DATE: 5-25-83

SAP2SAP VERIFICATION 5364

23-MAY-83

YEL-RED SOLID UNIT 1, 0-600 MS

TIME/FORCE TABLE 15, MAGNITUDE AT NODE POINT 717



DONE BY: DATE: 5-2-83

CHKD BY: DATE: 5-25-83

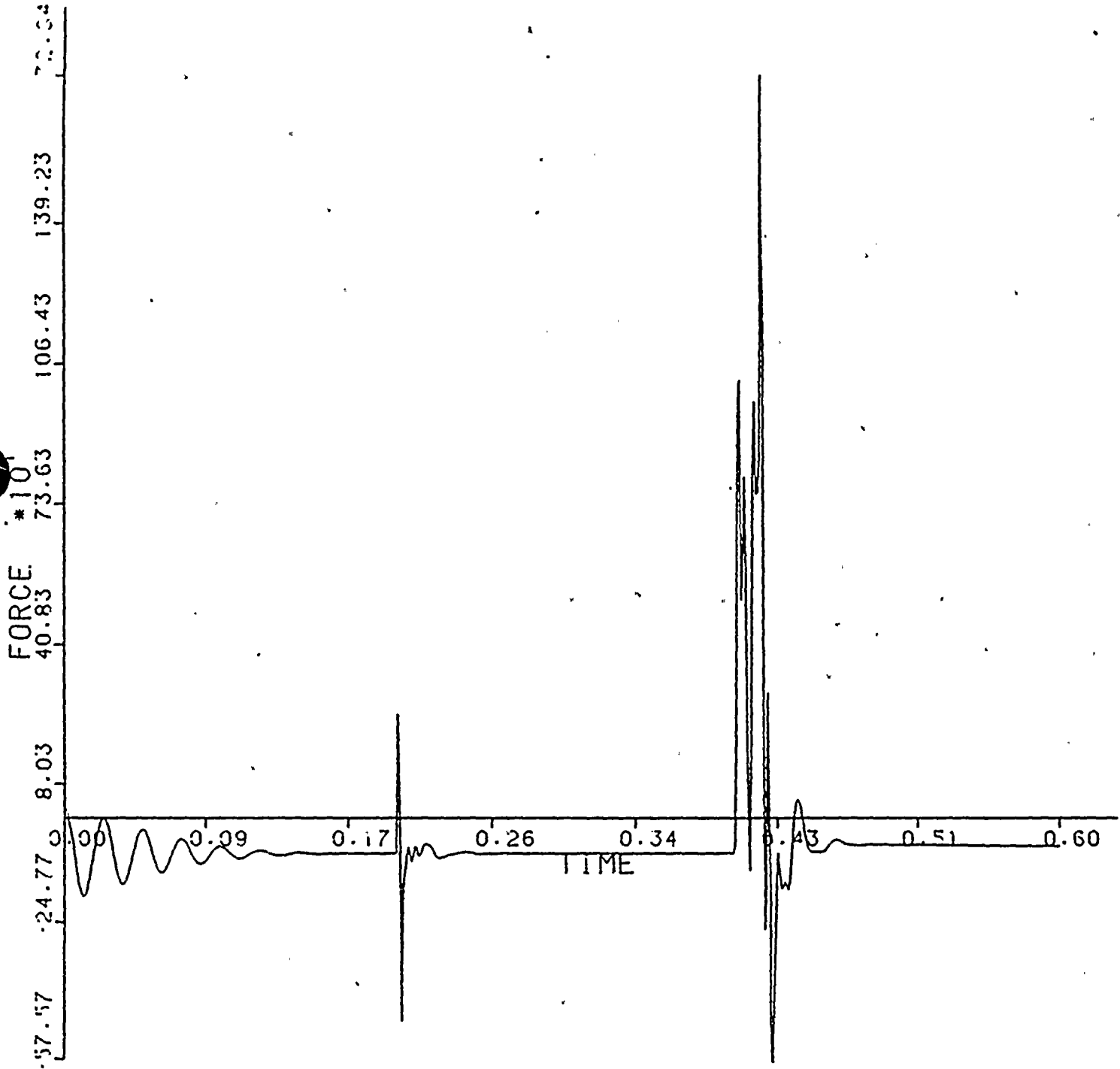
SAP2SAP VERIFICATION 5364

23-MAY-83

YEL-RED SOLID UNIT 1, 0-600 MS

TIME/FORCE TABLE 16, MAGNITUDE AT NODE POINT

710



DONE BY: WZ DATE: 5-25-83

CHKD BY: WZ DATE: 5-25-83

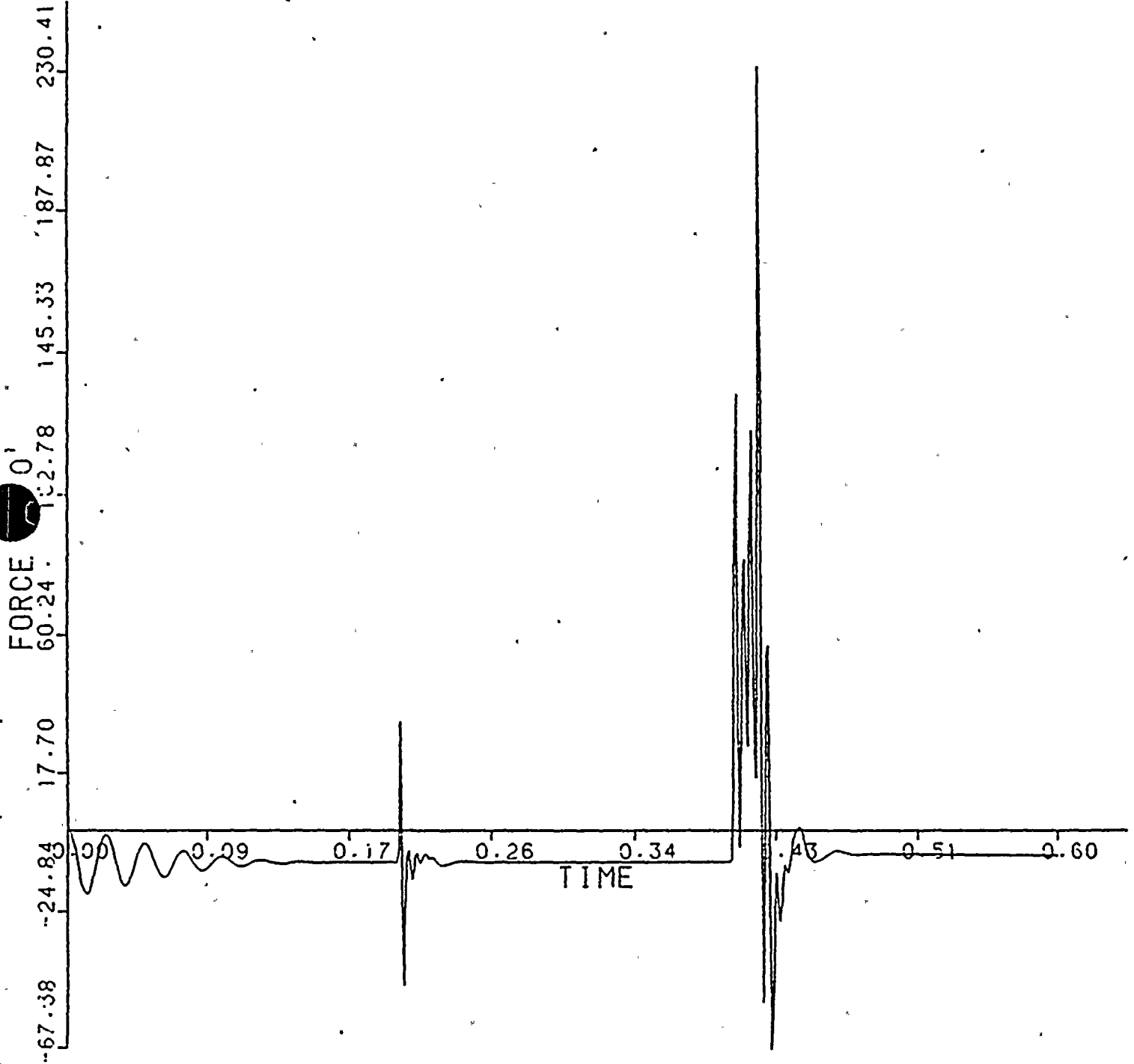
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ENGINEERING SERVICES

SAP2SAP VERIFICATION 5364 23-MAY-83

YEL-RED SOLID UNIT 1, 0-600 MS

TIME/FORCE TABLE 17, MAGNITUDE AT NODE POINT 680



DONE BY: ML DATE: 5-23-83

CHKD BY: ML DATE: 5-23-83

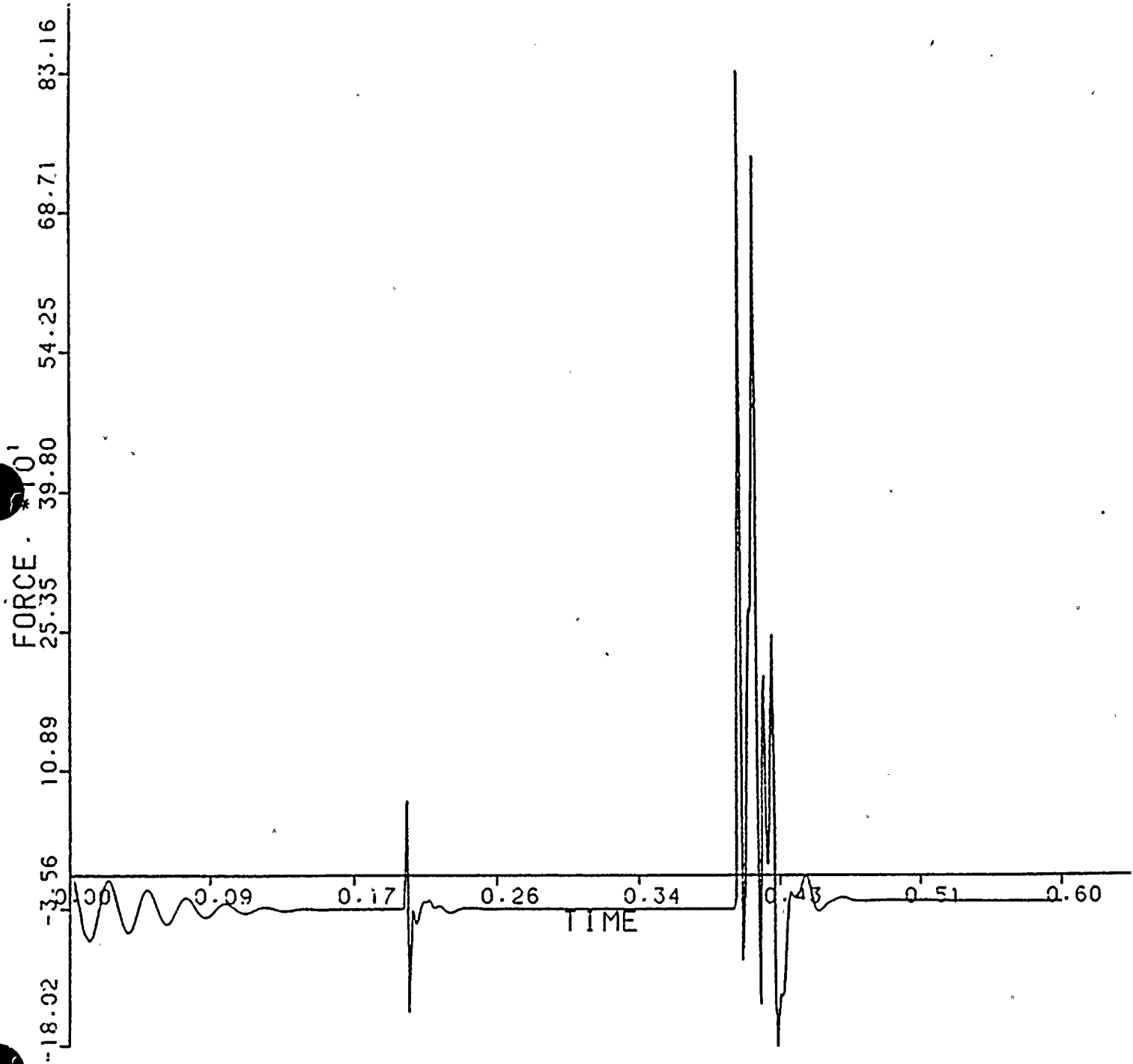
SAP2SAP VERIFICATION 5364

23-MAY-83

YEL-RED SOLID UNIT 1, 0-600 MS

TIME/FORCE TABLE .18, MAGNITUDE AT NODE POINT

600



DONE BY: DATE: 5-23-83

CHKD BY: DATE: 5-25-83

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Revision 0

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TELEDYNE
ENGINEERING SERVICES

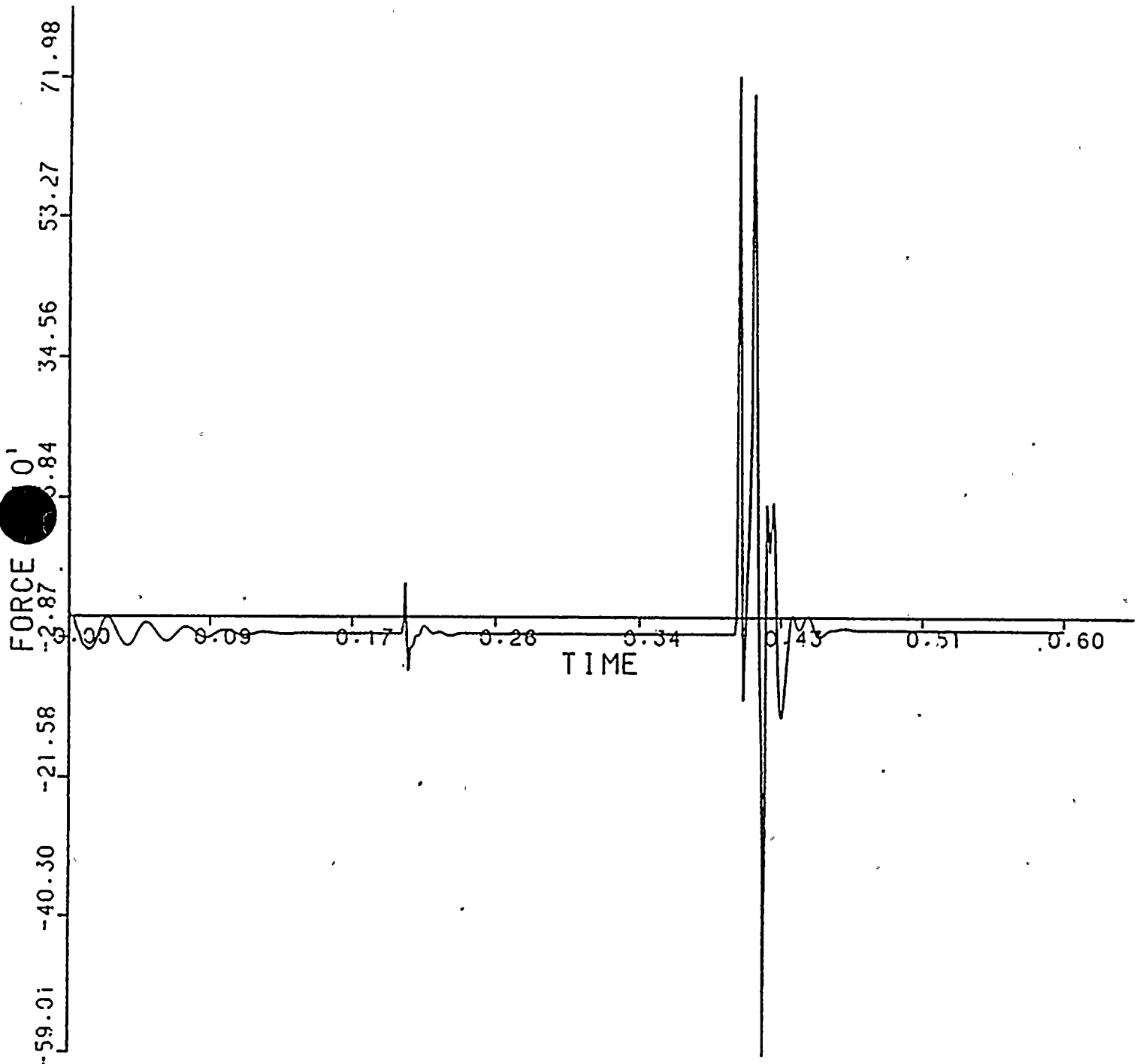
SAP2SAP VERIFICATION 5364

23-MAY-83

YEL-RED SOLID UNIT 1, 0-600 MS

TIME/FORCE TABLE 19, MAGNITUDE. AT NODE POINT

590



DONE BY: 4/2 DATE: 5-11-83

CHKD BY: CM DATE: 5-25-83

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TELEDYNE
ENGINEERING SERVICES

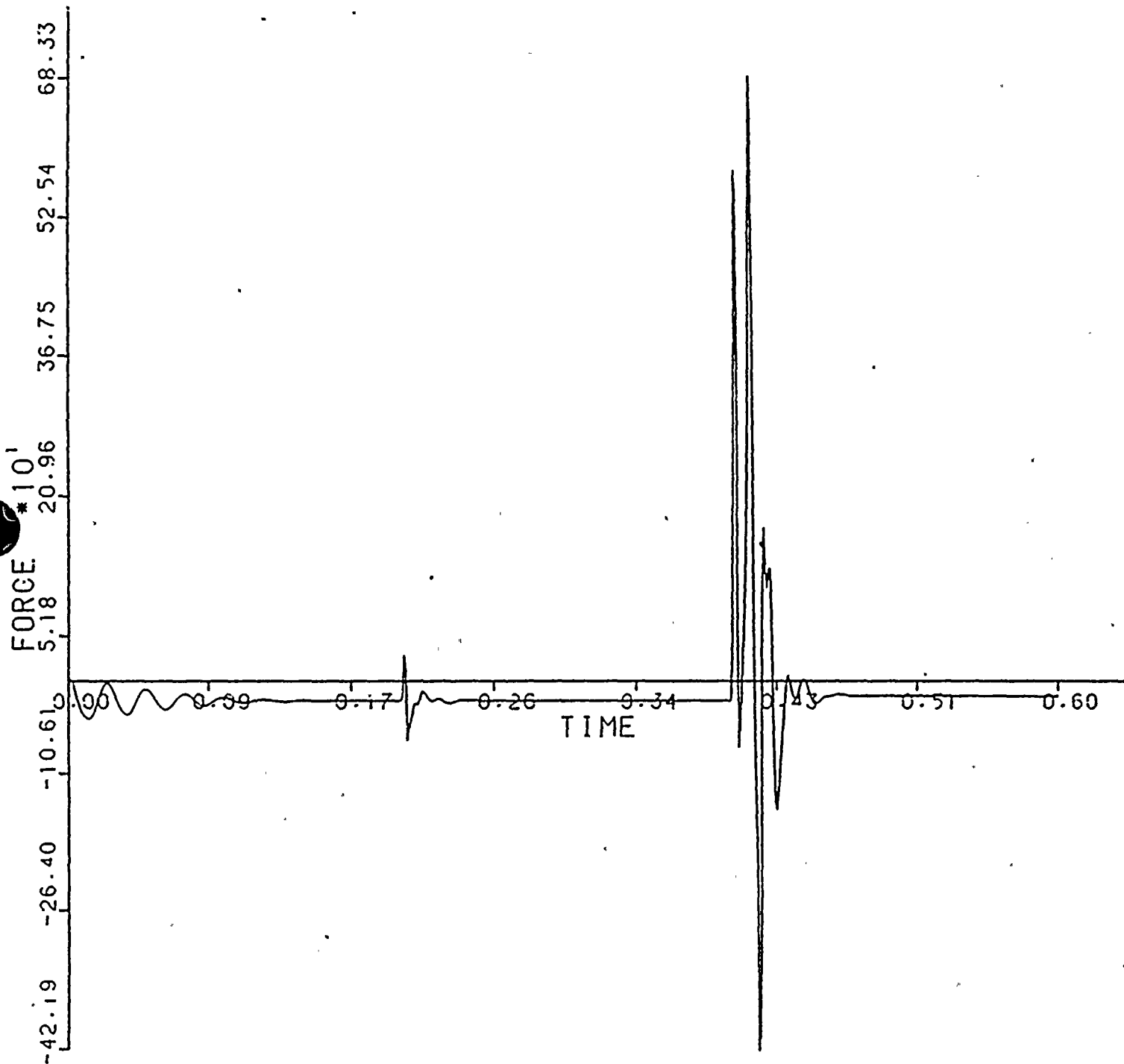
SAP2SAP VERIFICATION 5364

23-MAY-83

YEL-RED SOLID UNIT 1, 0-600 MS

TIME/FORCE TABLE 20, MAGNITUDE AT NODE POINT

585



DONE BY: VR DATE: 5-23-83

CHKD BY: VR DATE: 5-23-83

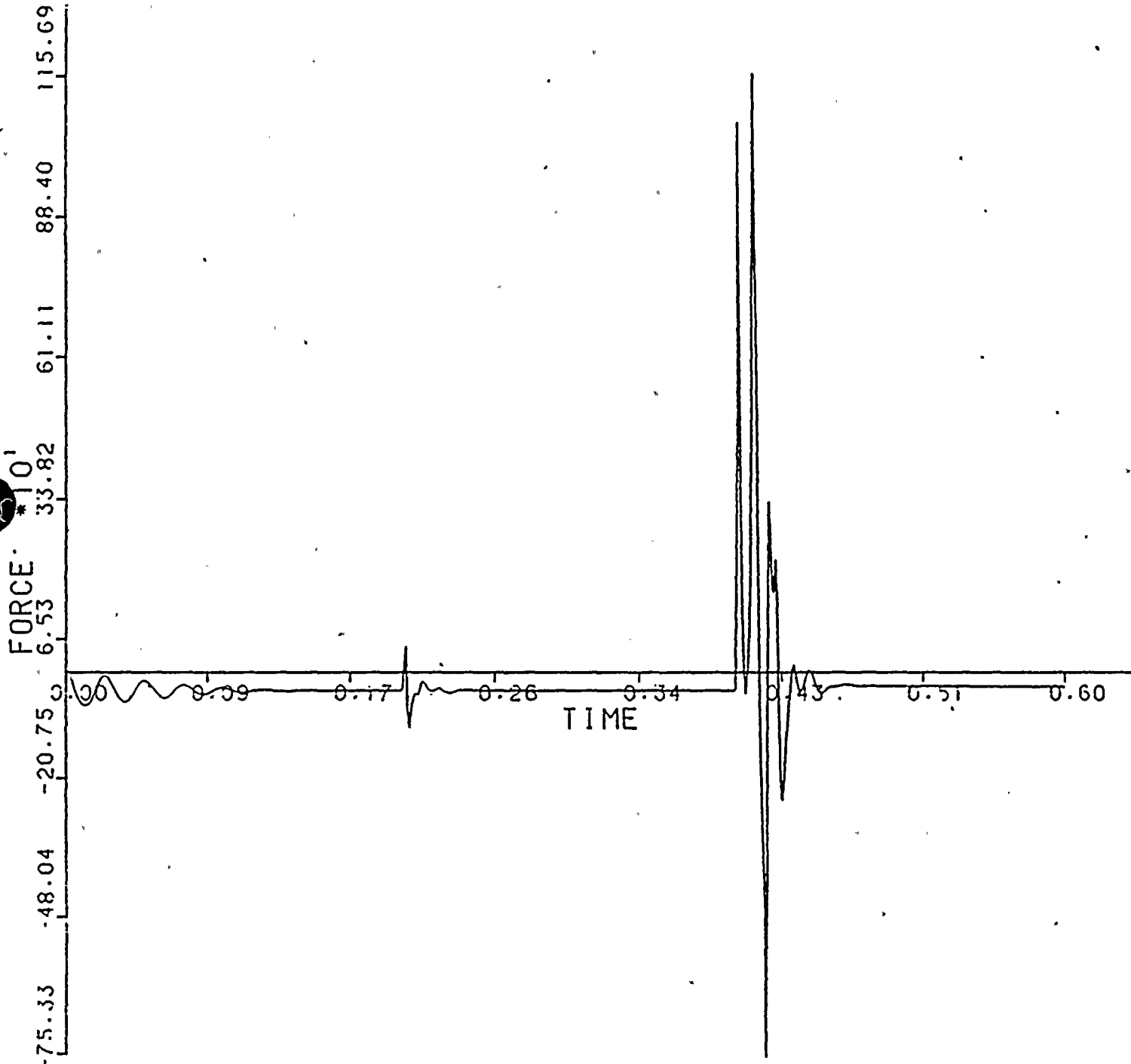


SAP2SAP, VERIFICATION 5364

23-MAY-83

YEL-RED SOLID UNIT 1, 0-600 MS

TIME/FORCE TABLE 21, MAGNITUDE AT NODE POINT 575



DONE BY: ME DATE: 5-1-83

CHKD BY: JM DATE: 5-25-83

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TELEDYNE
ENGINEERING SERVICES

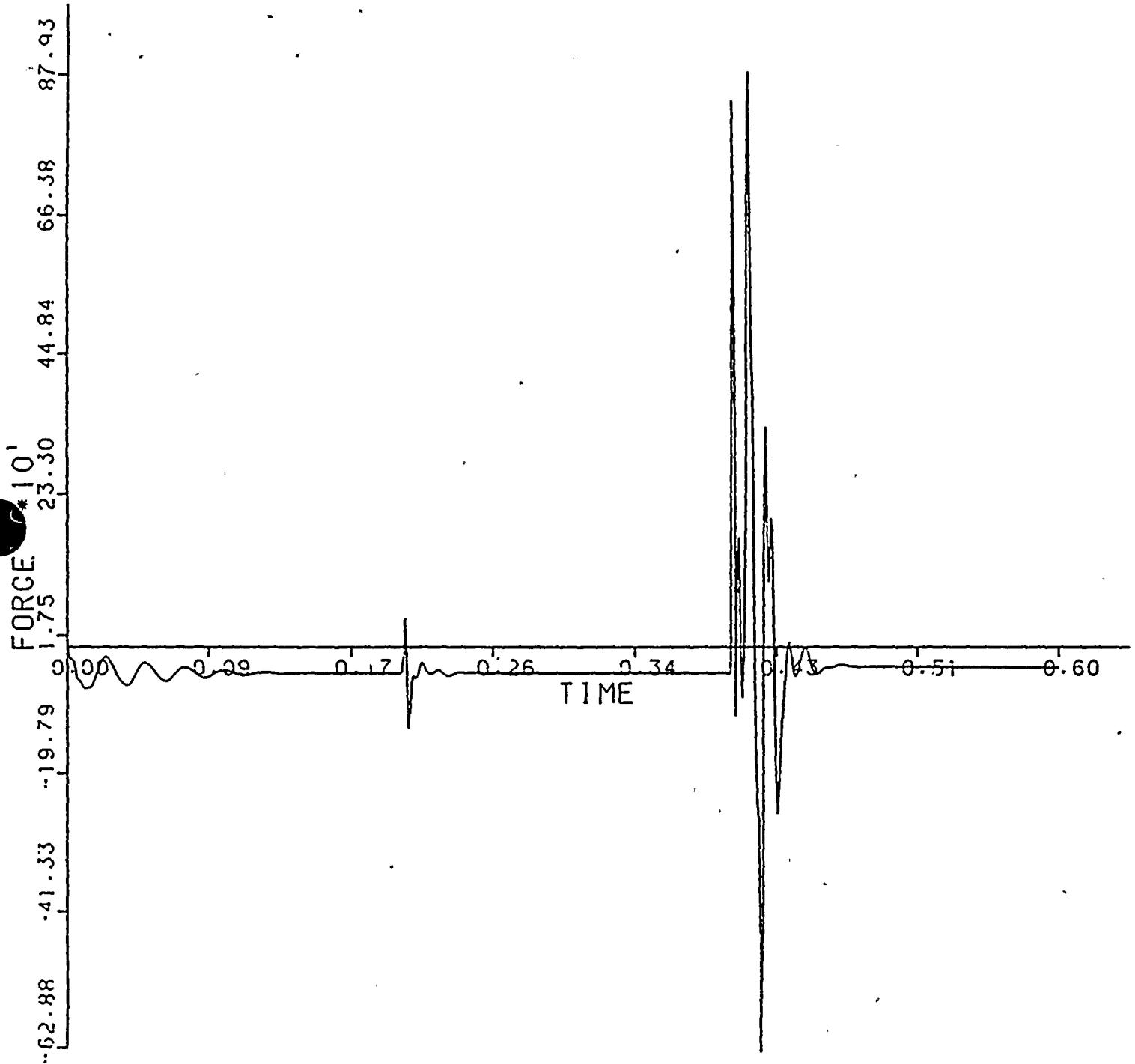
SAP2SAP VERIFICATION 5364

23-MAY-83

YEL-RED SOLID UNIT 1, 0-600 MS

TIME/FORCE TABLE 22, MAGNITUDE AT NODE POINT

435



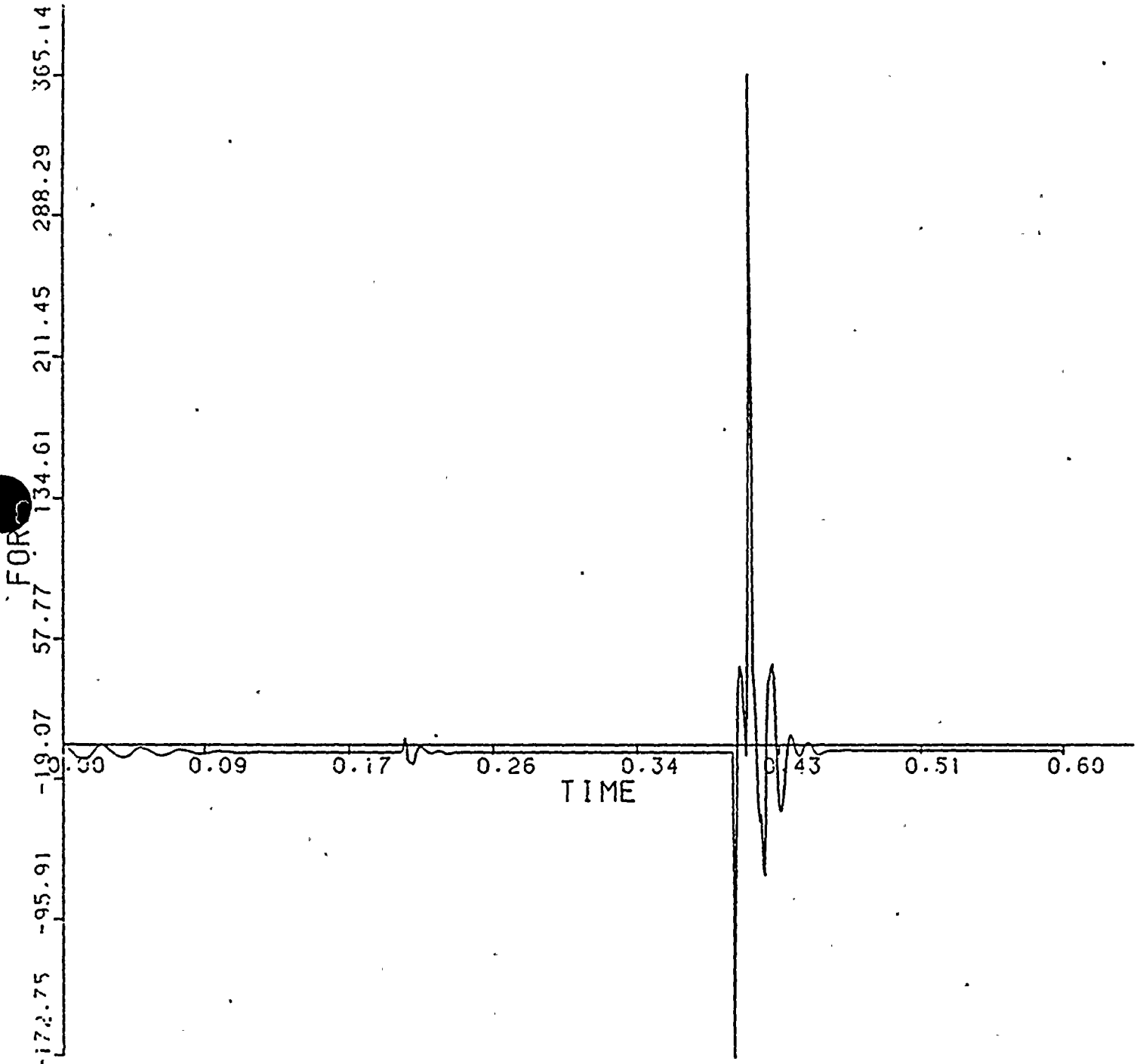
DONE BY: DATE: 5-25-83

CHKD BY: DATE: 5-25-83

Technical Report
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4-343  TELEDYNE
ENGINEERING SERVICES

SAP2SAP VERIFICATION 5364 23-MAY-83
YEL-RED SOLID UNIT 1, 0-600 MS
TIME/FORCE TABLE 23, MAGNITUDE AT NODE POINT 440



DONE BY: WZ DATE: 5-1-83
CHKD BY: LL DATE: 5-25-83

4-344

TELEDYNE
ENGINEERING SERVICES

SAP2SAP VERIFICATION 5364

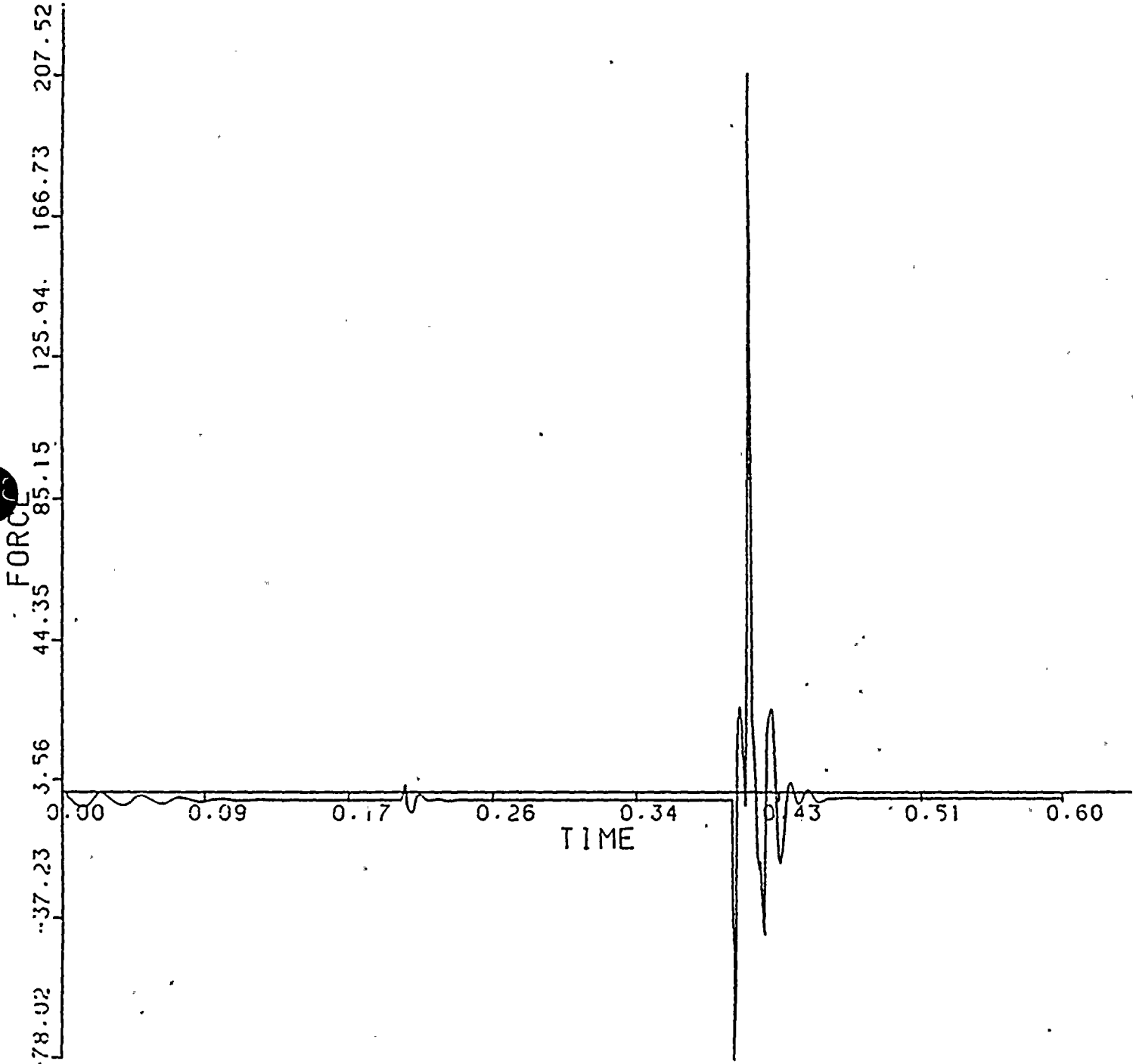
23-MAY-83

YEL-RED SOLID UNIT 1, 0-600 MS

TIME/FORCE TABLE

24, MAGNITUDE AT NODE POINT

450



DONE BY: WZ DATE: 5-2-83

CHKD BY: MM DATE: 5-2-83

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TELEDYNE
ENGINEERING SERVICES

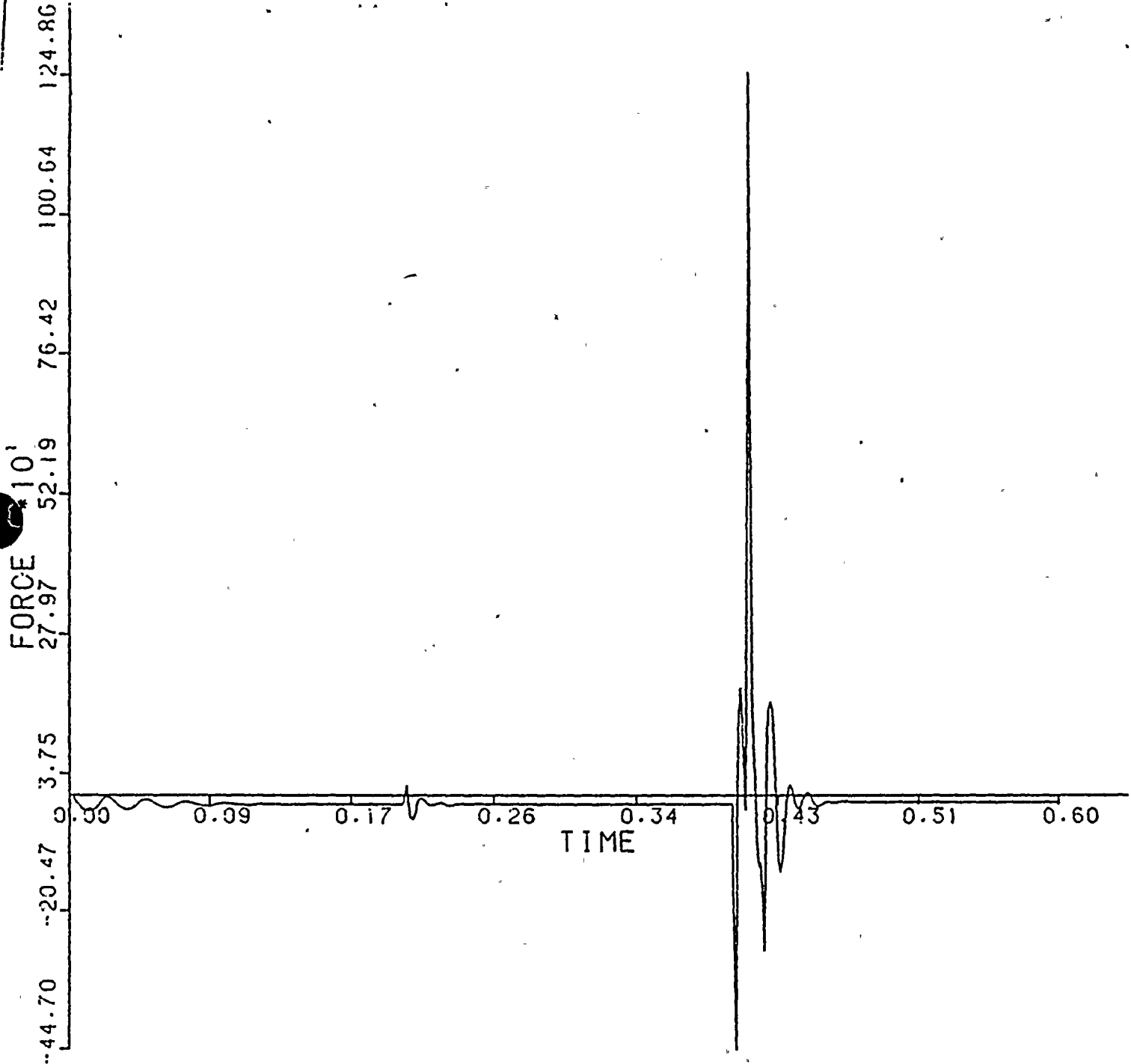
SAP2SAP VERIFICATION 5364

23-MAY-83

YEL-RED SOLID UNIT 1, 0-600 MS

TIME/FORCE TABLE 25, MAGNITUDE AT NODE POINT

460



DONE BY: MR DATE: 5-2-83

CHKD BY: JH DATE: 5-25-83

TELEDYNE
ENGINEERING SERVICES

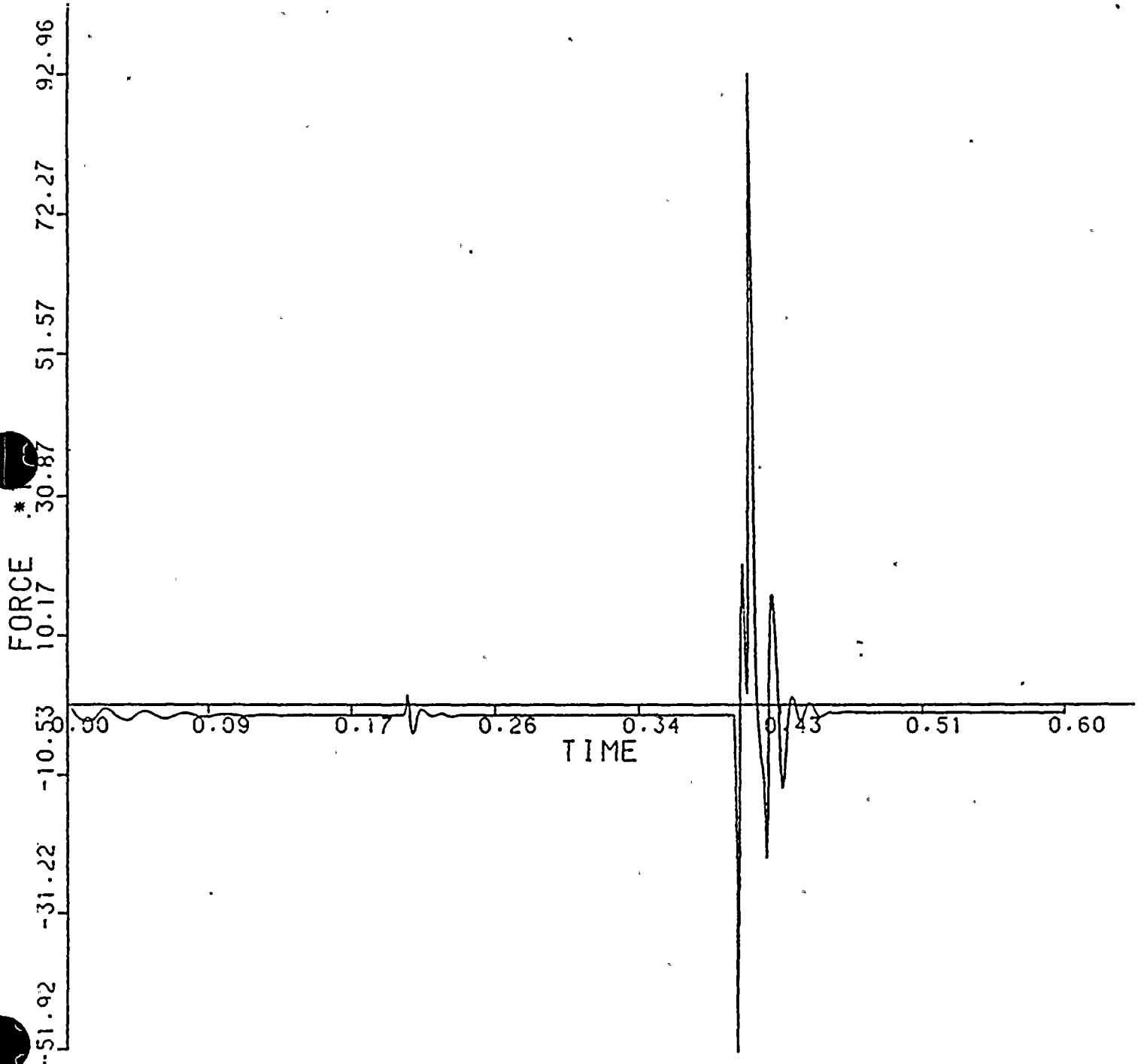
SAP2SAP VERIFICATION 5364

23-MAY-83

YEL-RED SOLID UNIT 1, 0-600 MS

TIME/FORCE TABLE 26, MAGNITUDE AT NODE POINT

465



DONE BY: DATE: 5-11-83

CHKD BY: DATE: 5-11-83



TELEDYNE
ENGINEERING SERVICES

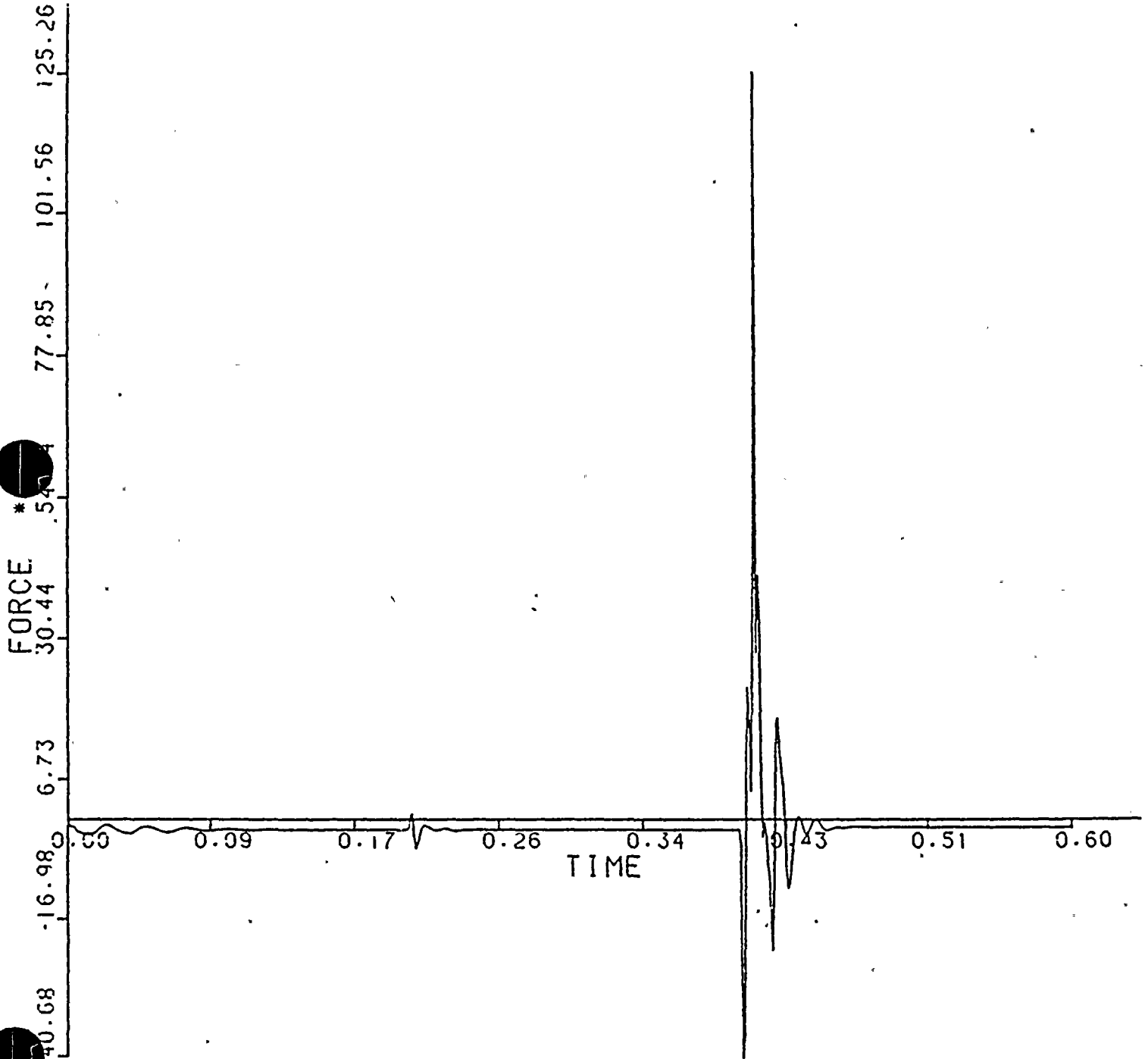
SAP2SAP VERIFICATION 5364

23-MAY-83

YEL-RED SOLID UNIT 1, 0-600 MS

TIME/FORCE TABLE 27, MAGNITUDE' AT NODE POINT

475



DONE BY: DATE:

CHKD BY: DATE:

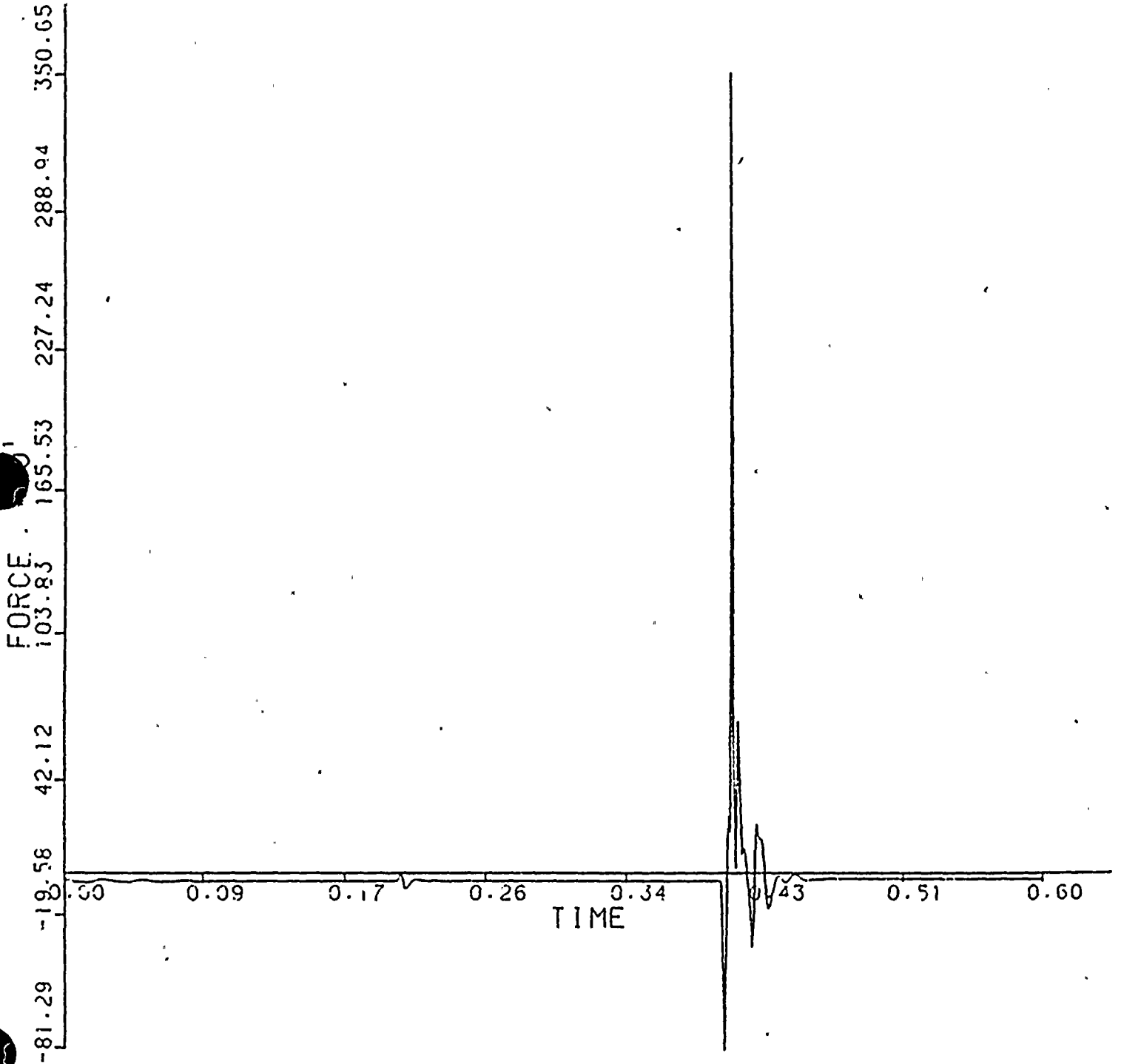
SAP2SAP VERIFICATION 5364

23-MAY-83

YEL-RED SOLID UNIT 1, 0-600 MS

TIME/FORCE TABLE 28. MAGNITUDE AT NODE POINT

485



DONE BY: DATE: 5-2-83

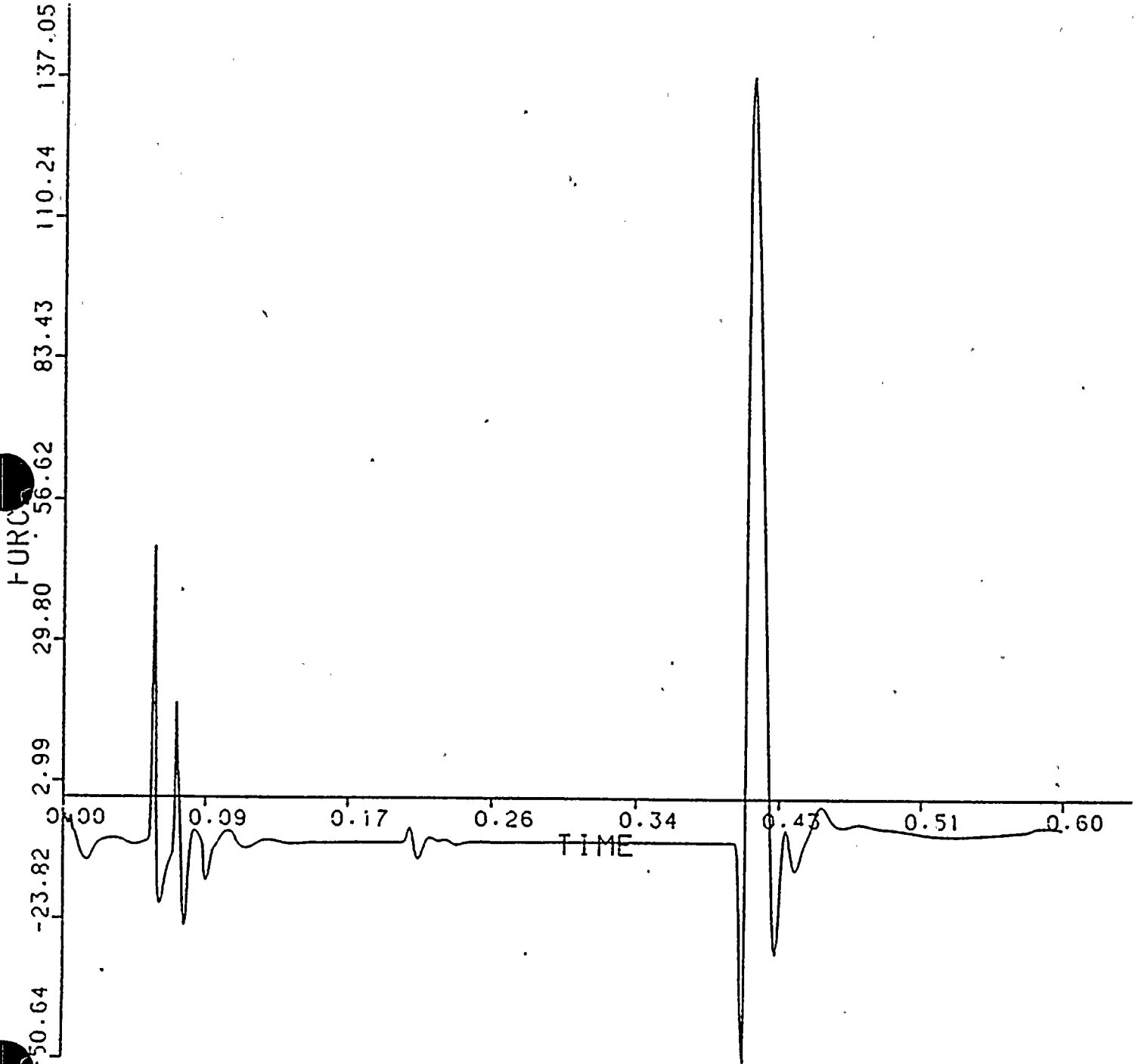
CHKD BY: DATE: 5-2-83

SAP2SAP VERIFICATION 5364

YEL-RED SOLID UNIT 1, 0-600 MS

TIME/FORCE TABLE 29, MAGNITUDE AT NODE POINT

529



DONE BY: DATE: 5-1-83
CHKD BY: DATE: 5-1-83



TELEDYNE
ENGINEERING SERVICES

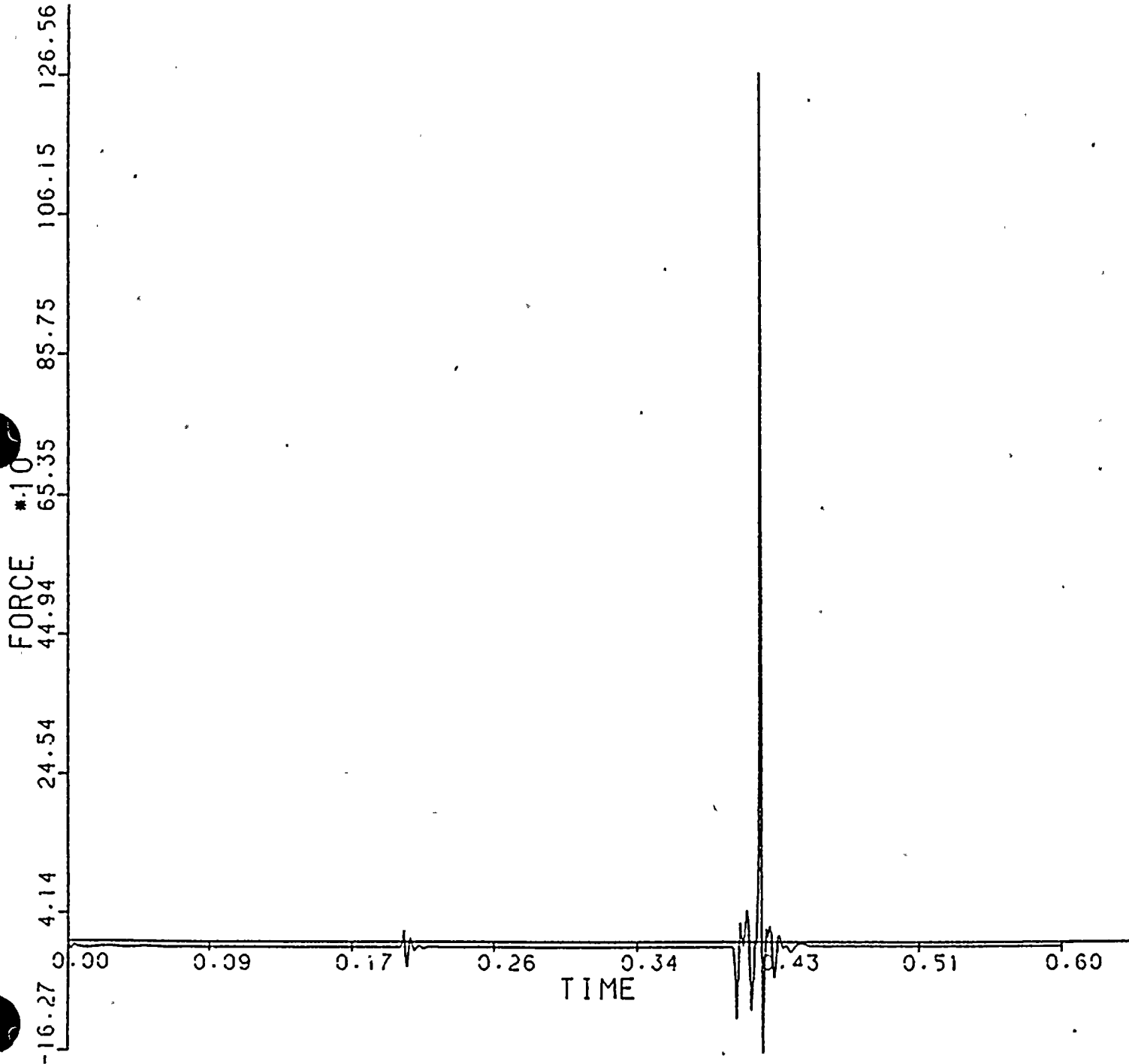
SAP2SAP VERIFICATION 5364

23-MAY-83

YEL-RED SOLID UNIT 1, 0-600 MS

TIME/FORCE TABLE 30, MAGNITUDE AT NODE POINT

665



DONE BY: DATE: 5-23-83

CHKD BY: DATE: 5-23-83



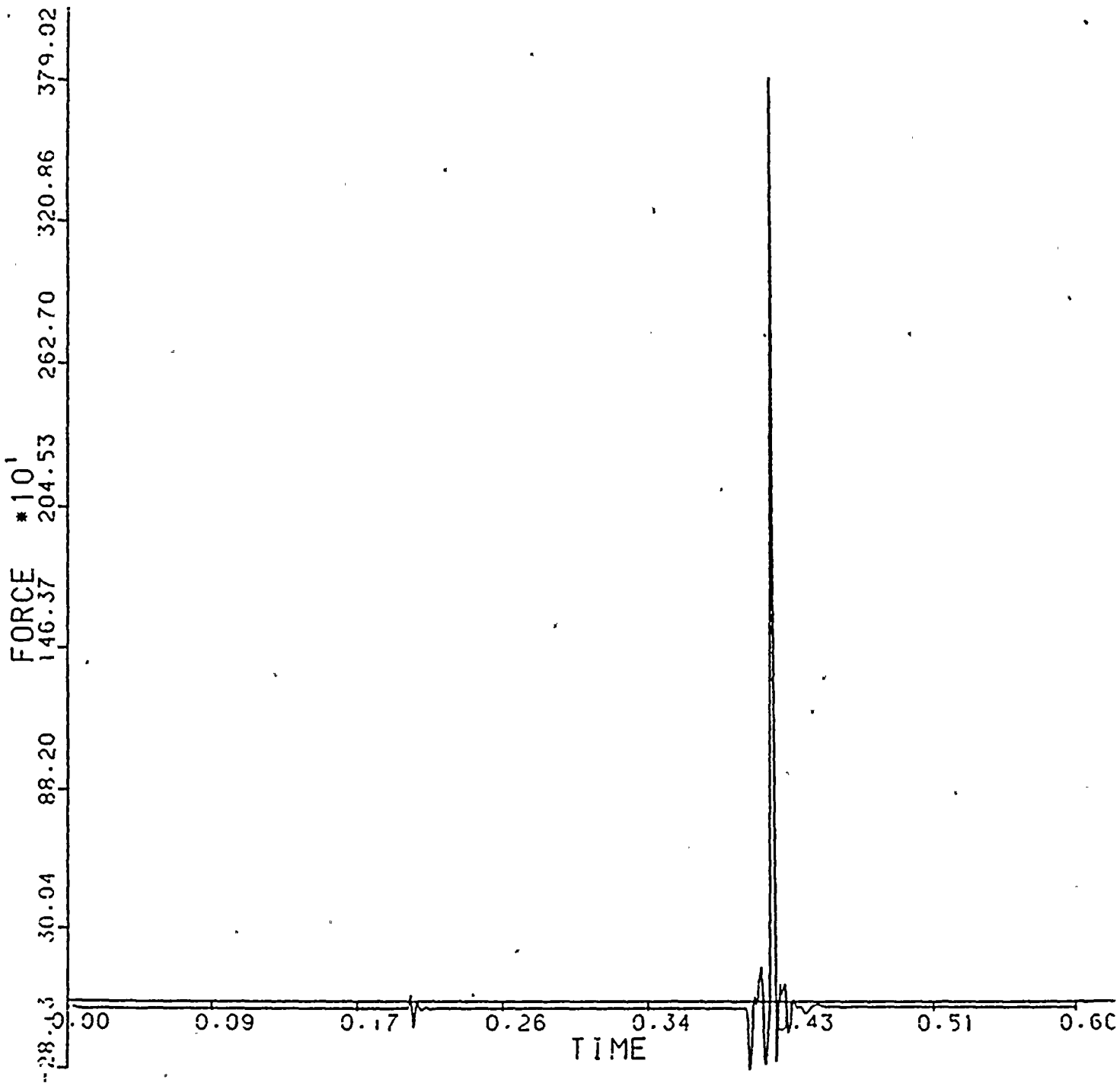
SAP2SAP VERIFICATION 5364

23-MAY-83

YEL-RED SOLID UNIT 1, 0-600 MS

TIME/FORCE TABLE ' 31, MAGNITUDE AT NODE POINT

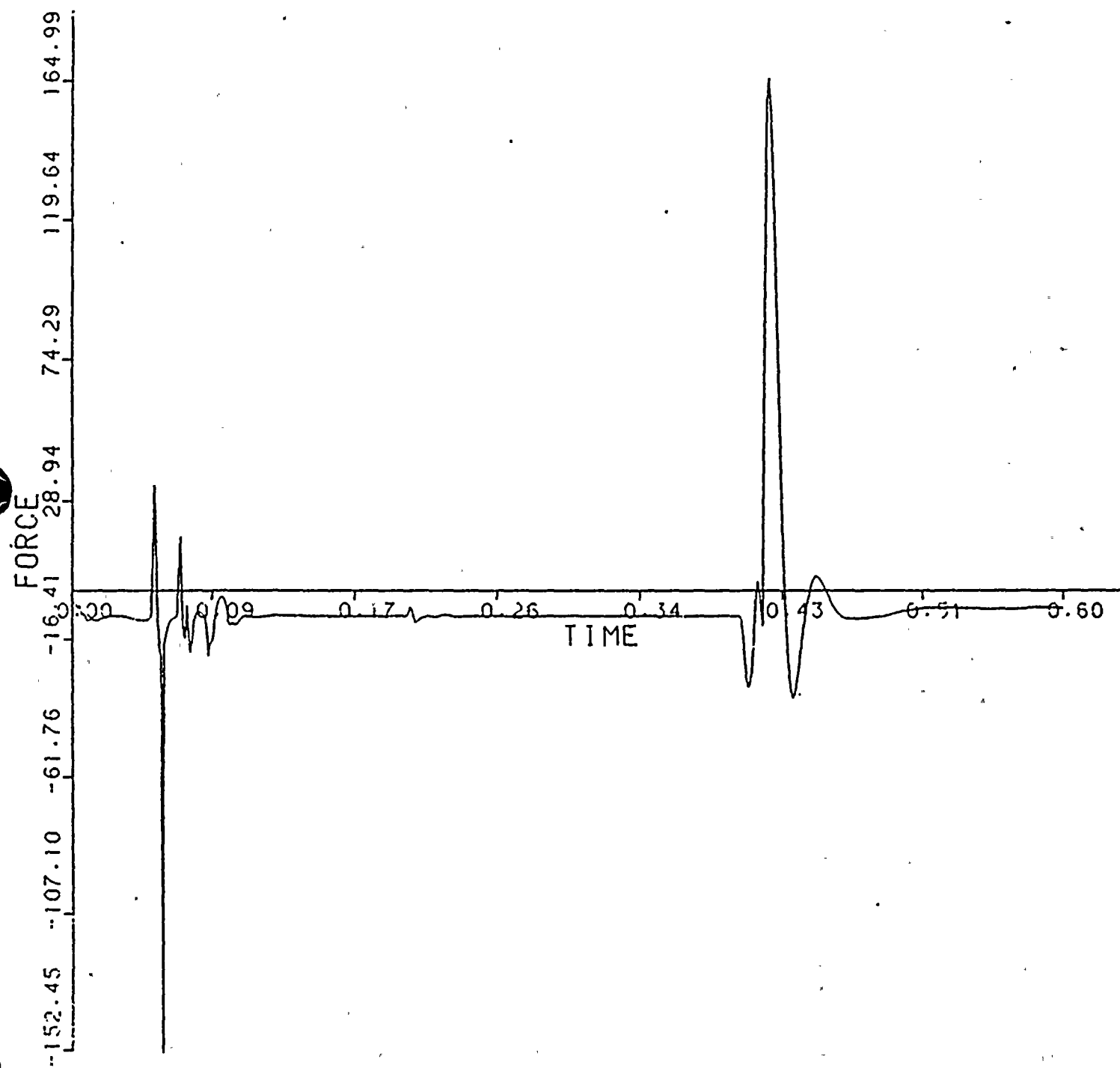
657



DONE BY: DATE:
CHKD BY: DATE:



SAP2SAP VERIFICATION 5364 23-MAY-83
YEL-RED SOLID UNIT 1, 0-600 MS
TIME/FORCE TABLE, 32, MAGNITUDE AT NODE POINT 620



DONE BY: DATE: 5-23-83
CHKD BY: DATE: 5-23-83



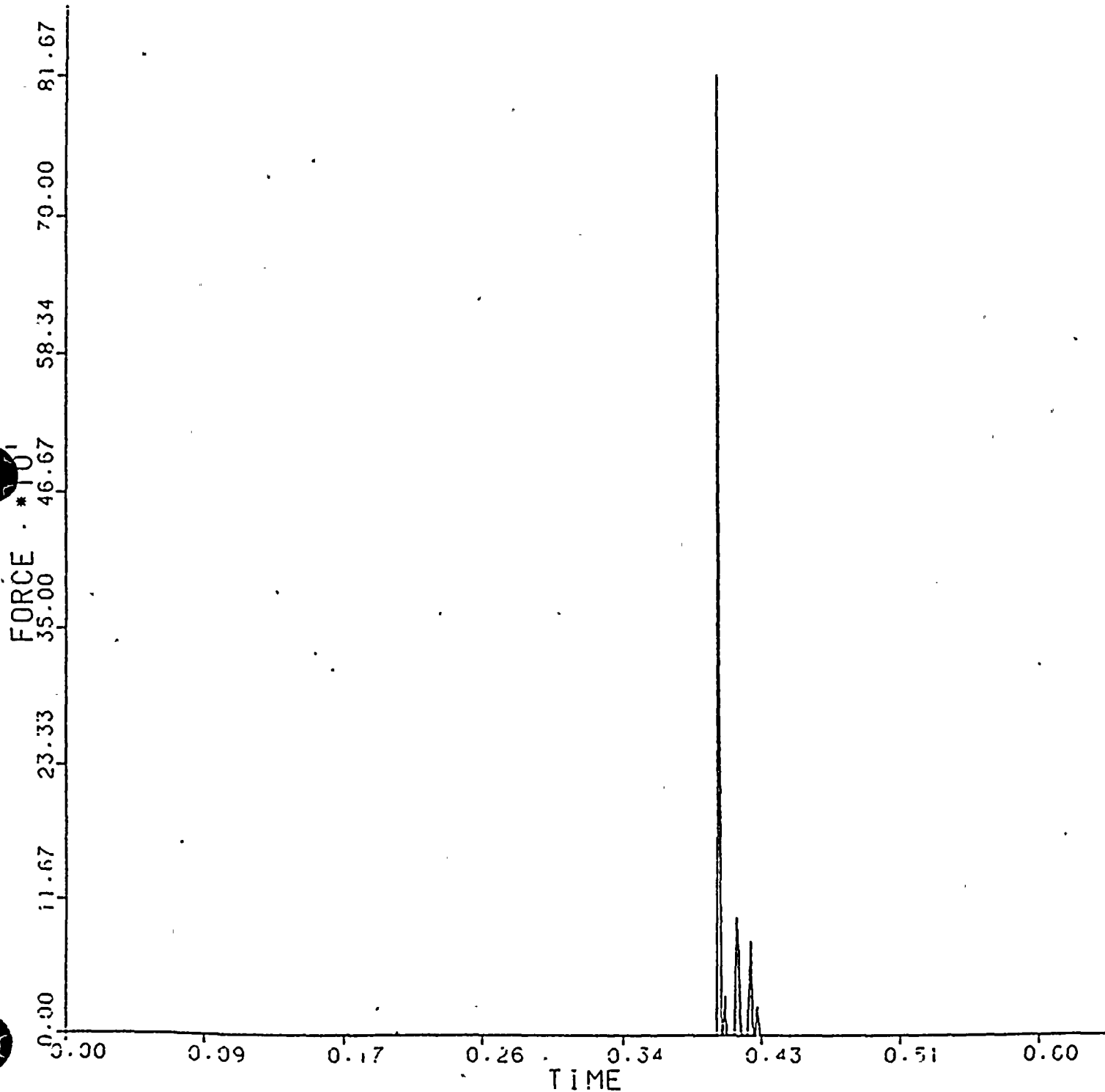
SAP2SAP VERIFICATION 5364

23-MAY-83

YEL-RED SOLID UNIT 1. 0-600 MS

TIME/FORCE TABLE 33, MAGNITUDE AT NODE POINT

431



DONE BY: DATE: 5-2-83

CHKD BY: DATE: 5-15-83



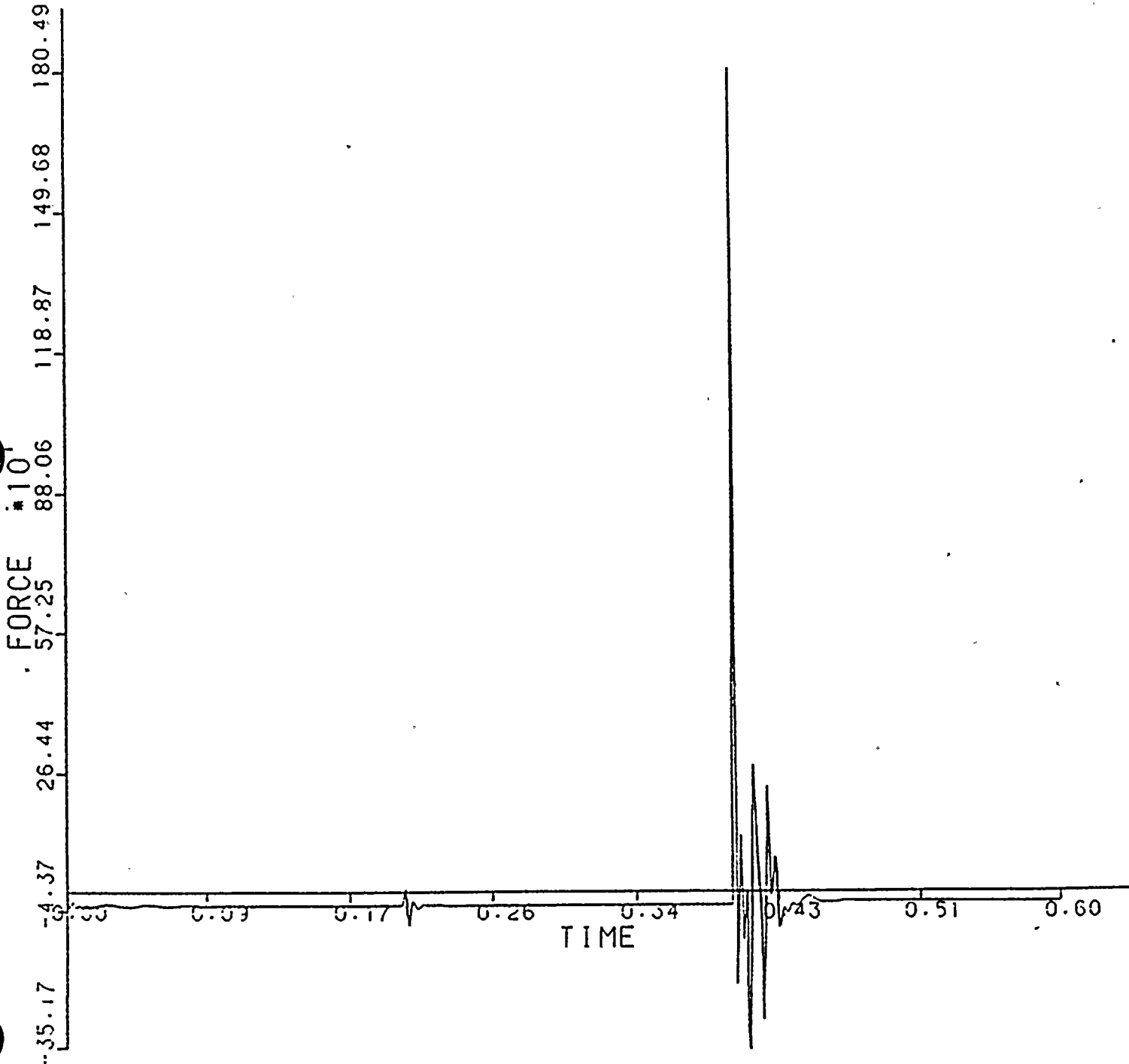
SAP2SAP VERIFICATION 5364

23-MAY-83

YEL-RED SOLID UNIT 1, 0-600 MS

TIME/FORCE TABLE 34, MAGNITUDE AT NODE POINT

405



DONE BY: DATE: 5/23/83
CHKD BY: DATE: 5/25/83

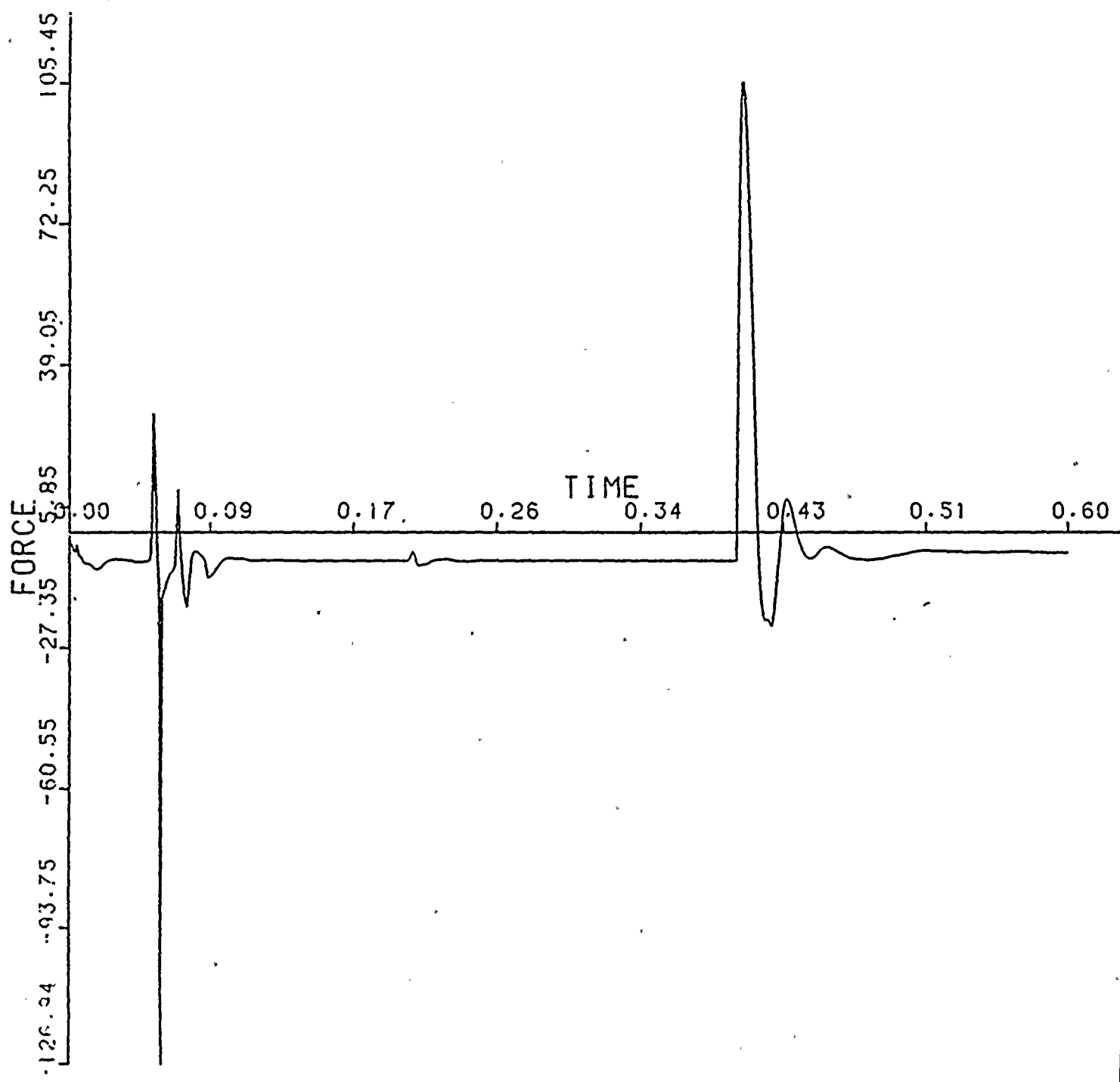
SAP2SAP VERIFICATION 5364

23-MAY-83

YEL-RED SOLID UNIT 1, 0-600 MS

TIME/FORCE TABLE 35. MAGNITUDE AT NODE POINT

382



DONE BY: DATE: 5 2 83
CHKD BY: DATE: 5 2 83



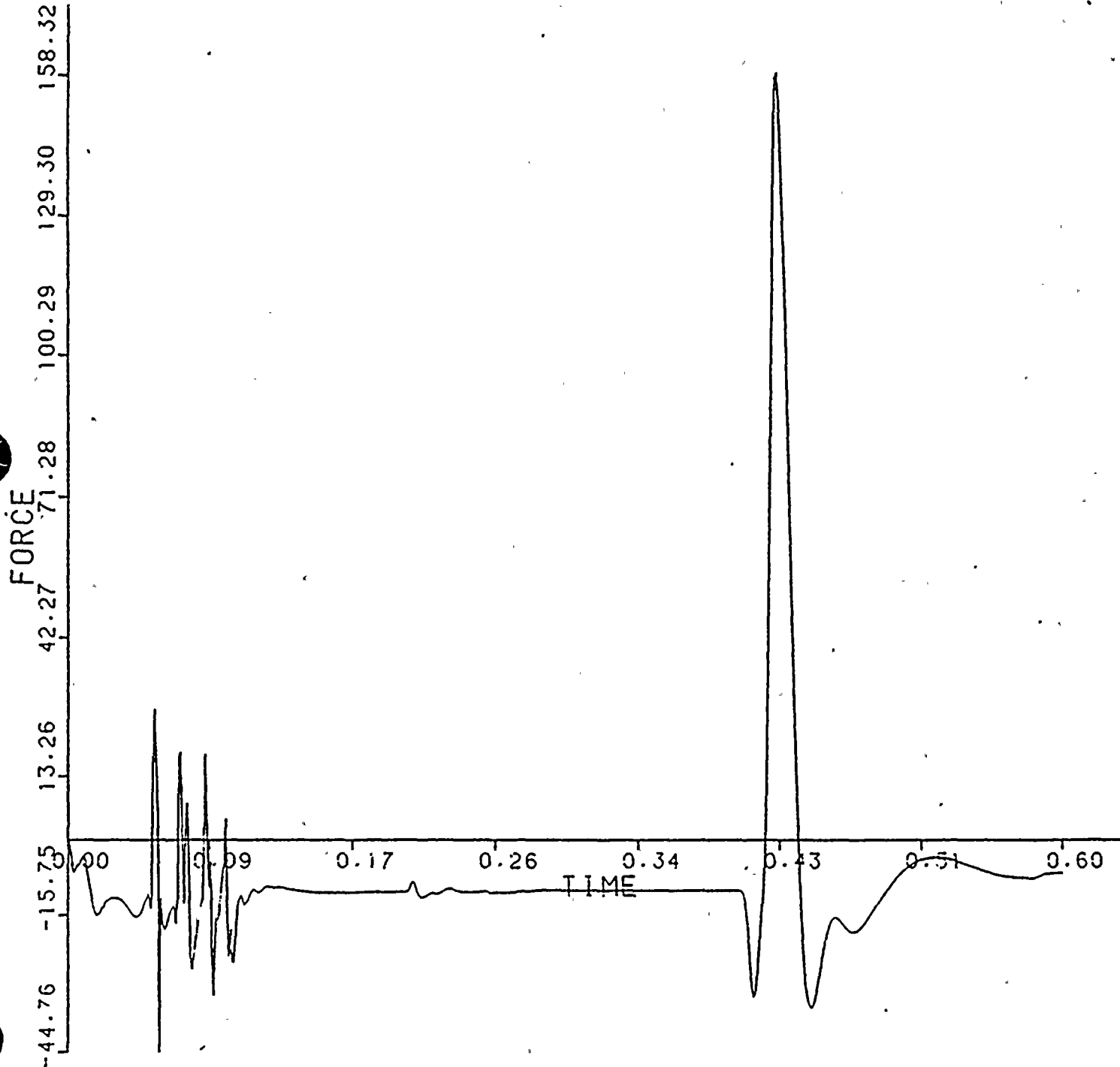
SAP2SAP VERIFICATION 5364

23-MAY-83

YEL-RED SOLID UNIT 1, 0-600 MS

TIME/FORCE TABLE 36, MAGNITUDE AT NODE POINT

610



DONE BY: DATE:

CHKD BY: DATE:

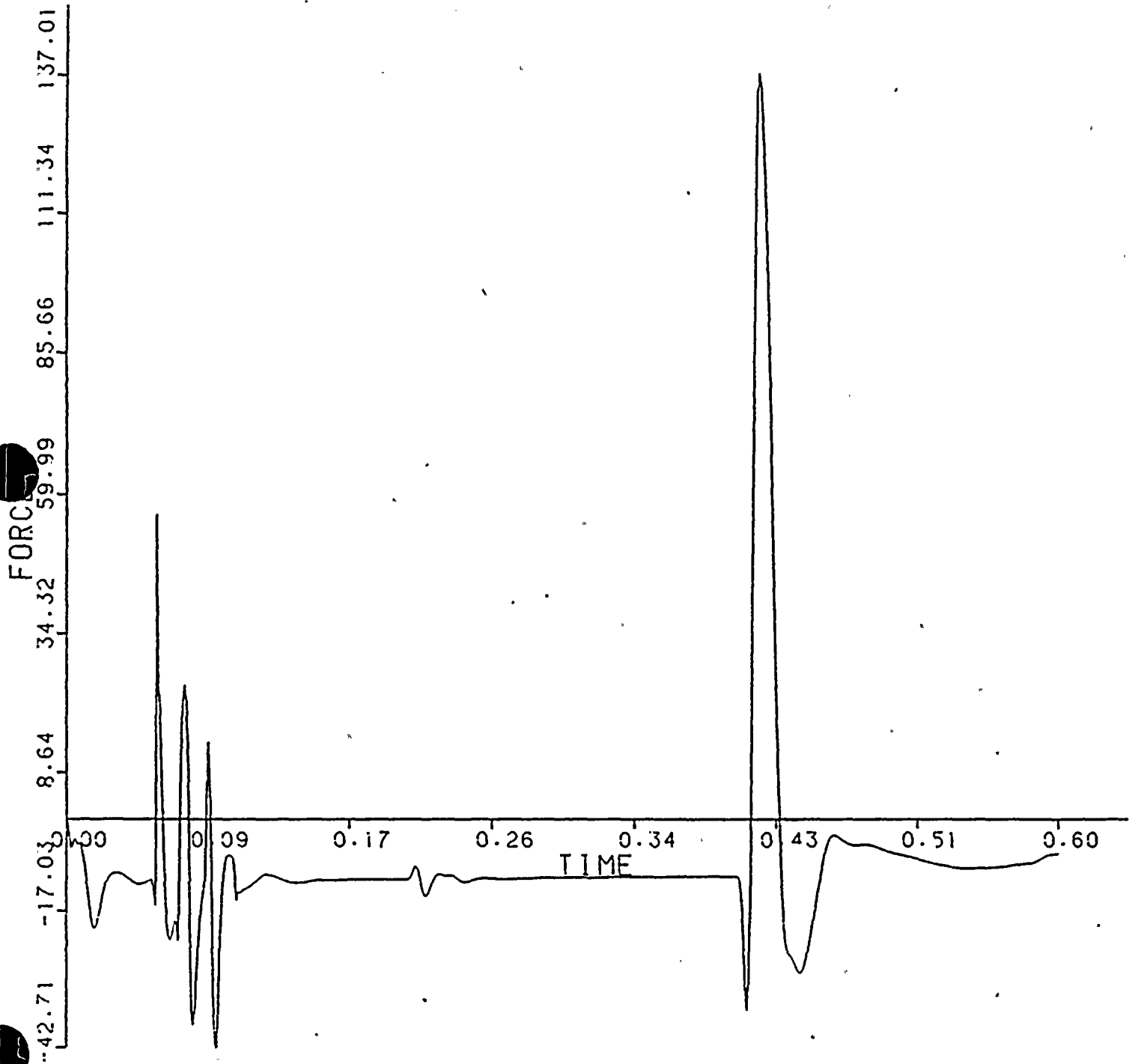
SAP2SAP VERIFICATION 5364

23-MAY-83

YEL-RED SOLID UNIT 1, 0-600 MS

TIME/FORCE TABLE 37, MAGNITUDE AT NODE POINT

535



DONE BY: DATE: 5-2-83

CHKD BY: DATE: 5-2-83



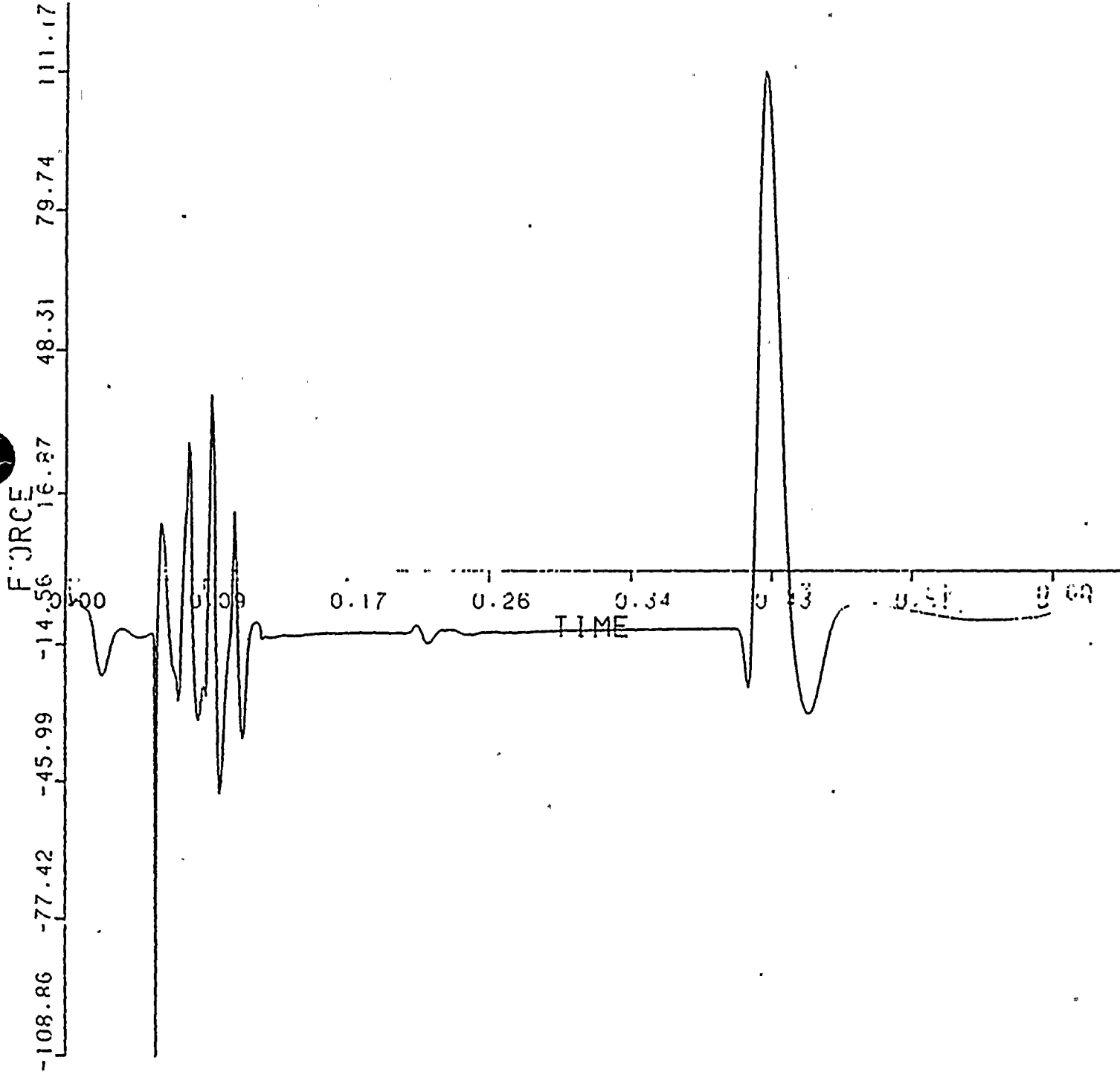
SAP2SAP VERIFICATION 5364

23-MAY-83

YEL-RED SOLID UNIT 1, 0-600 MS

TIME/FORCE TABLE 38, MAGNITUDE AT NODE POINT

545



DONE BY: MZ DATE: 5-2-83

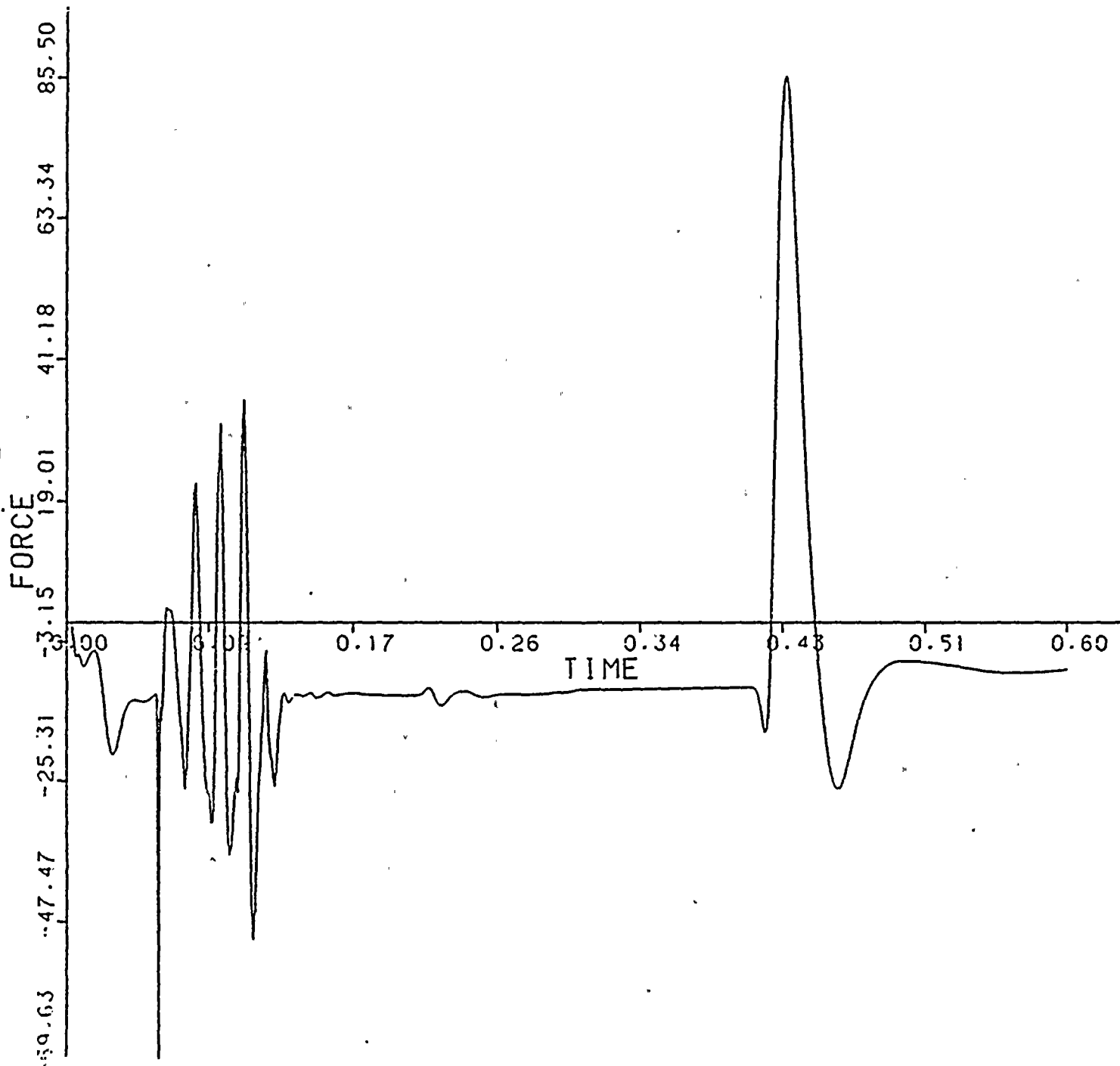
CHKD BY: MM DATE: 5-25-83

SAP2SAP VERIFICATION 5364 23-MAY-83

YEL-RED SOLID UNIT 1, 0-600 MS

TIME/FORCE TABLE 39. MAGNITUDE AT NODE POINT

550



DONE BY: MZ DATE: 5-23-83
CHKD BY: JM DATE: 5-25-83

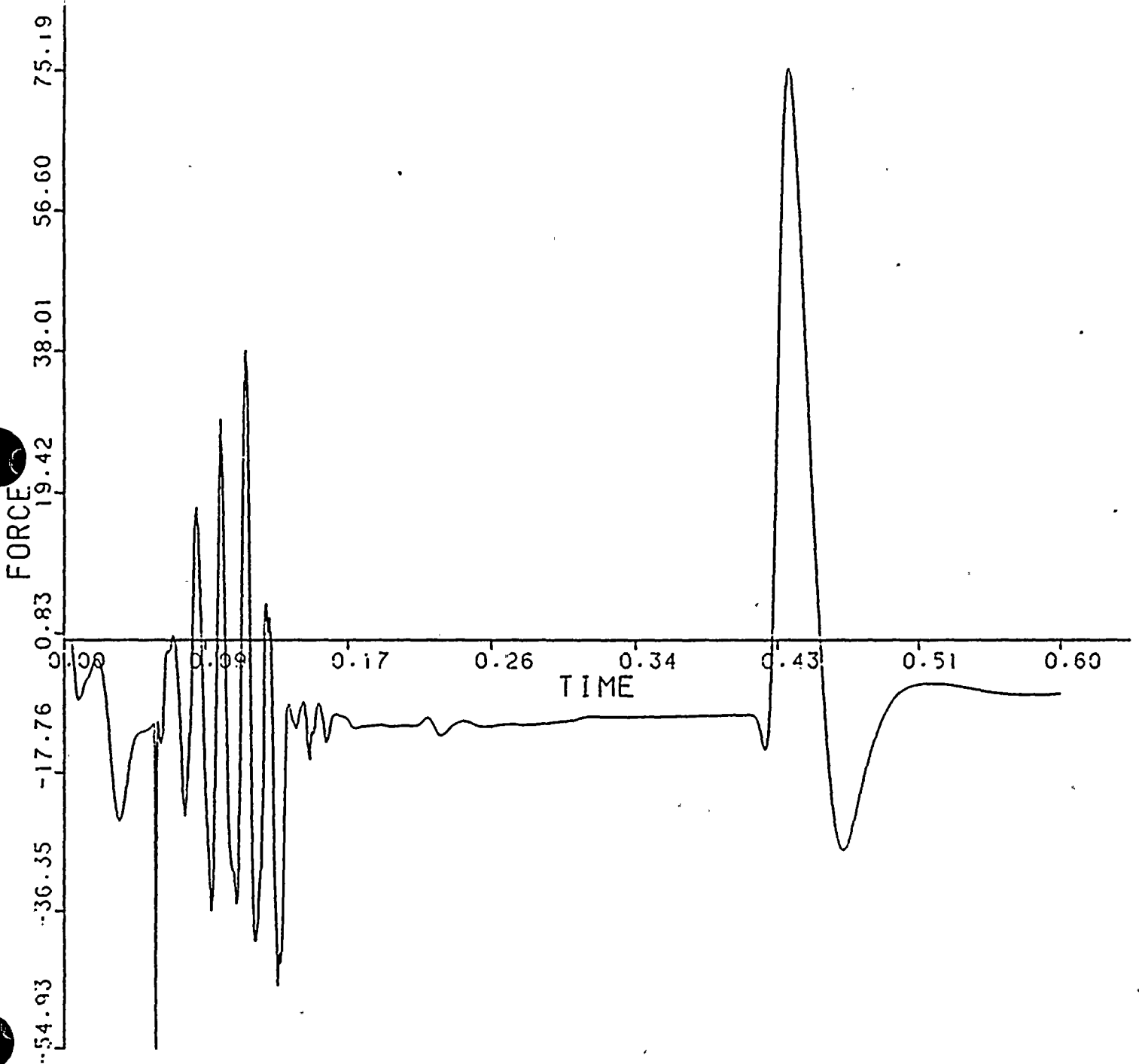


SAP2SAP VERIFICATION 5364

YEL-RED SOLID UNIT 1, 0-600 MS

TIME/FORCE TABLE 40, MAGNITUDE AT NODE POINT

555



DONE BY: KZ DATE: 5-2-83

CHKD BY: MI DATE: 5-25-83

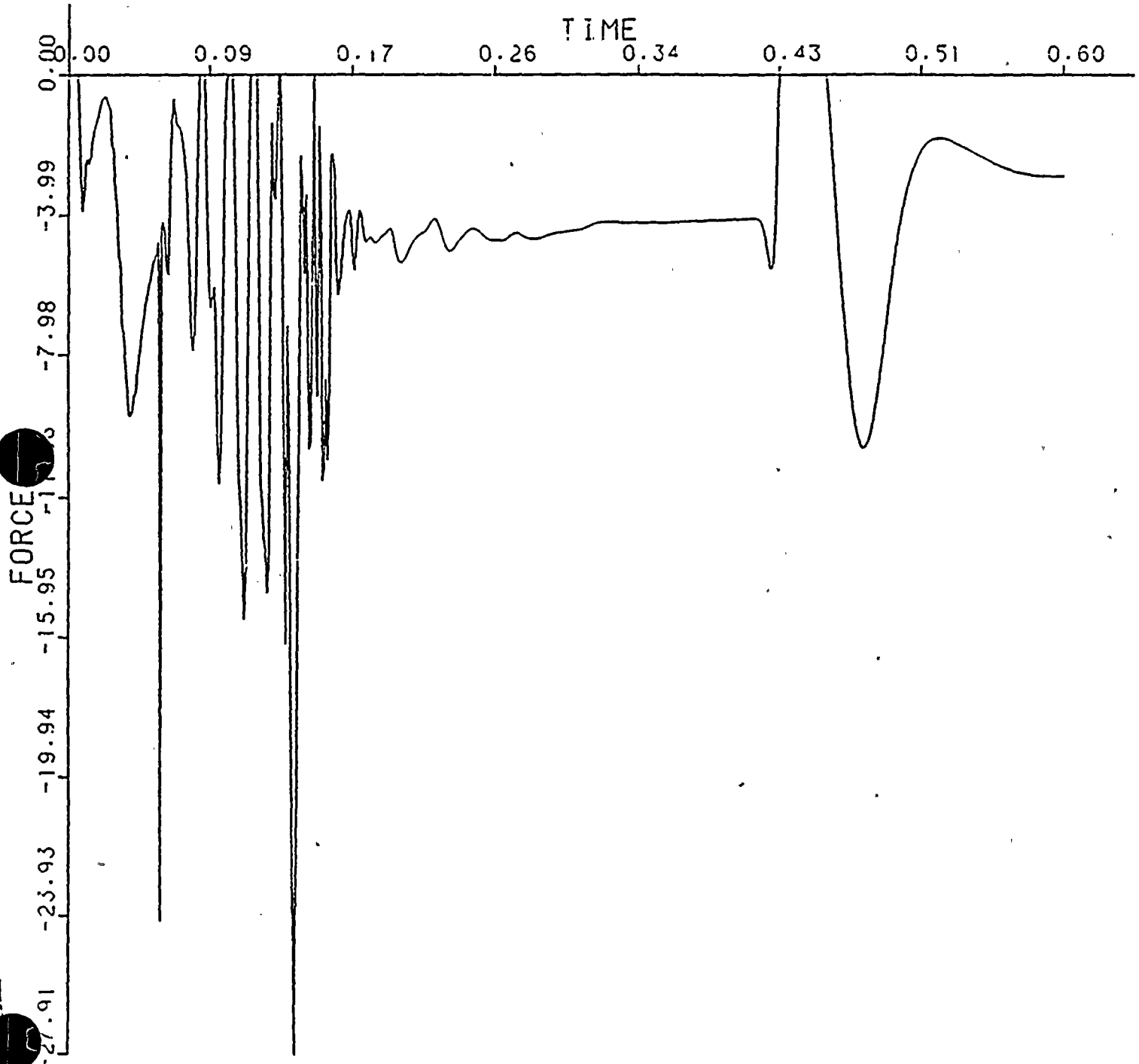
SAP2SAP VERIFICATION 5364

23-MAY-83

YEL-RED SOLID UNIT 1, 0-600 MS

TIME/FORCE TABLE 41, MAGNITUDE AT NODE POINT

560



DONE BY: MZ DATE: 5-21-83

CHKD BY: JM DATE: 5-25-83

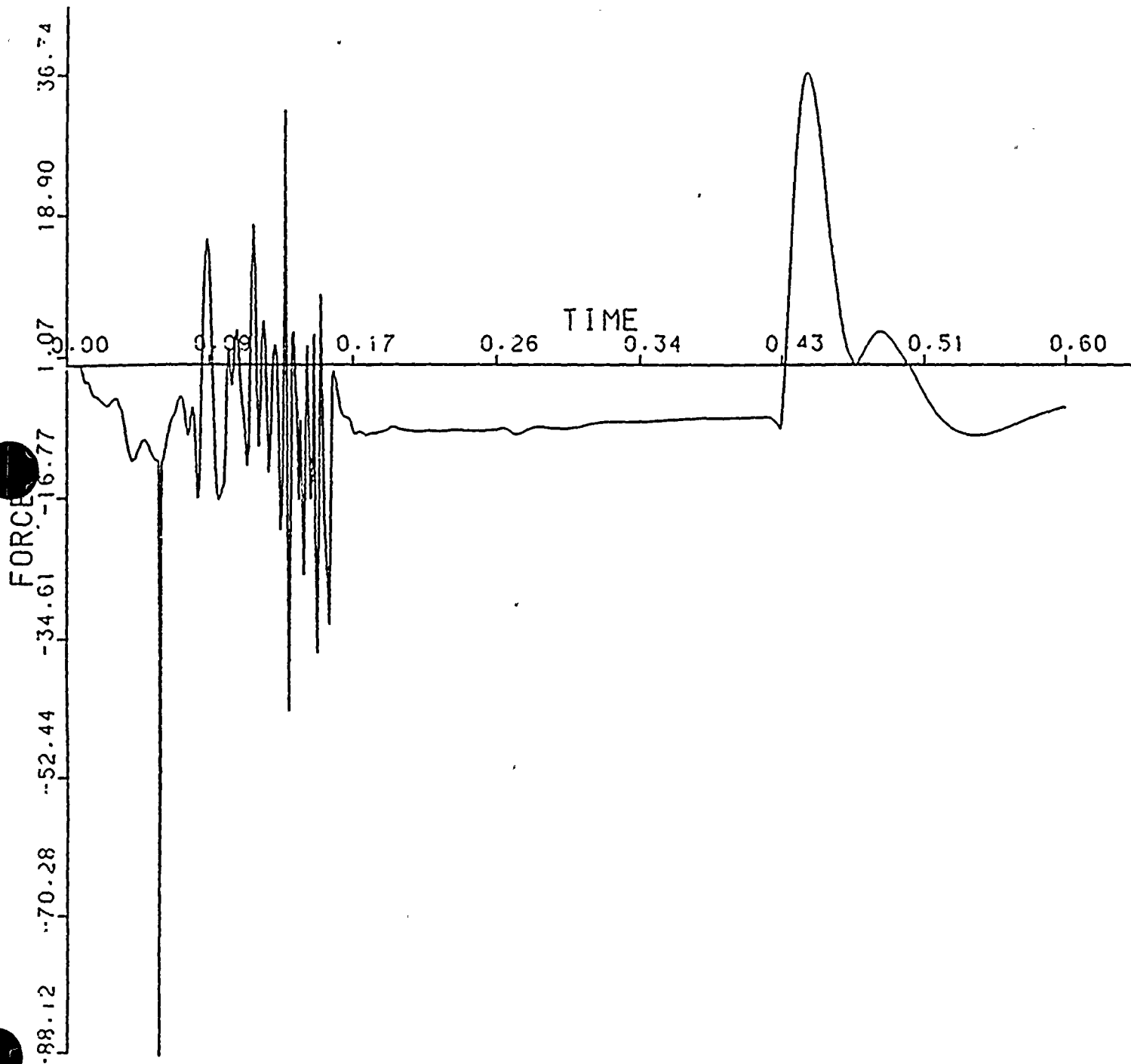
SAP2SAP VERIFICATION 5364

23-MAY-83

YEL-RED SOLID UNIT 1, 0-600 MS

TIME/FORCE TABLE 42, MAGNITUDE-AT NODE POINT

300



DONE BY: MR DATE: 5-2-83

CHKD BY: JA DATE: 5-25-83



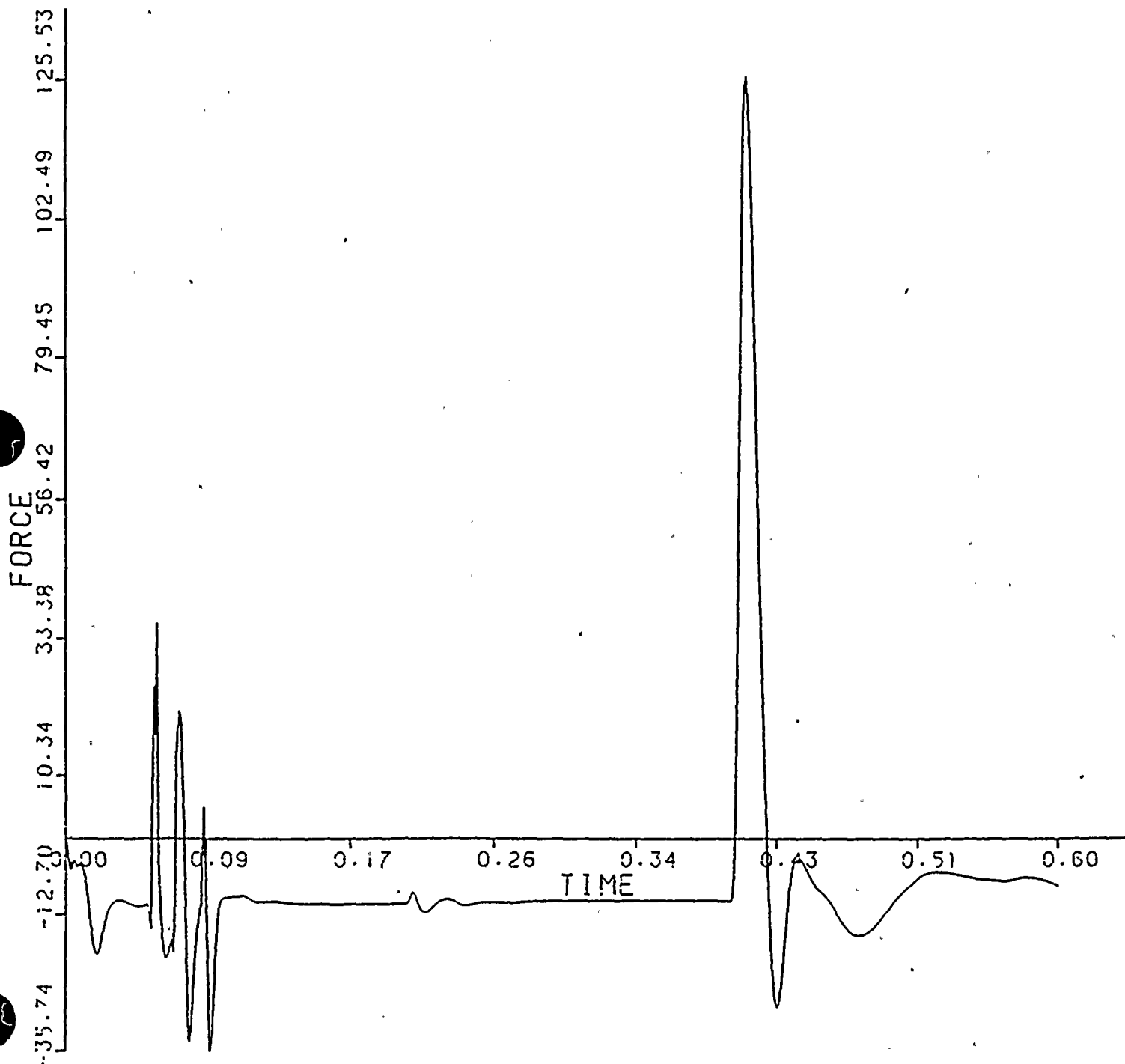
SAP2SAP VERIFICATION 5364

23 MAY-83

YEL-RED SOLID UNIT 1, 0-600 MS

TIME/FORCE TABLE 43, MAGNITUDE AT NODE POINT

375



DONE BY: MR DATE: 5-25-83

CHKD BY: JA DATE: 5-25-83

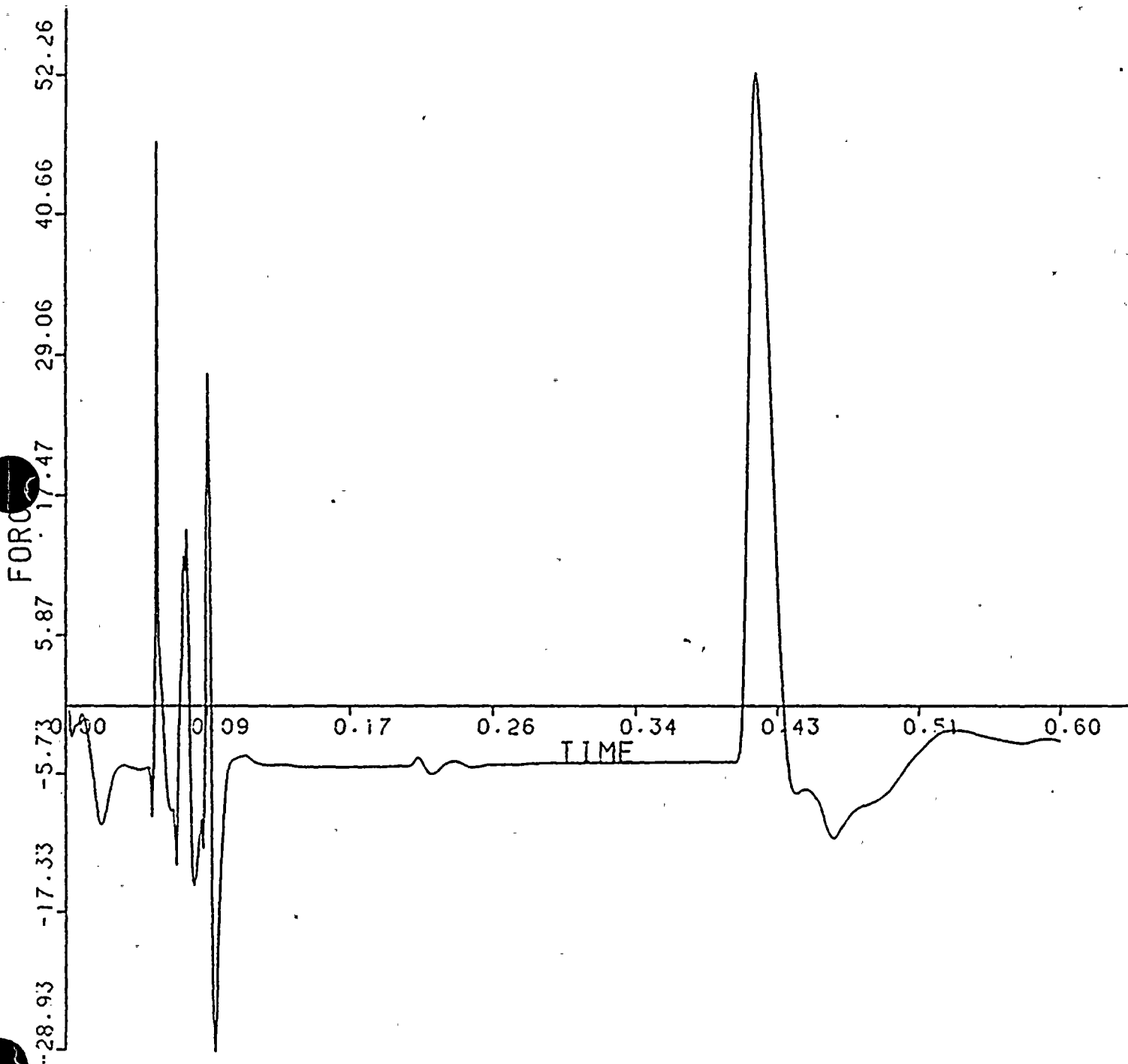
SAP2SAP VERIFICATION 5364

23-MAY-83

YEL-RED SOLID UNIT 1, 0-600 MS

TIME/FORCE TABLE 44, MAGNITUDE AT NODE POINT

365



DONE BY: WZ DATE: 5-2-83

CHKD BY: WZ DATE: 5-25-83

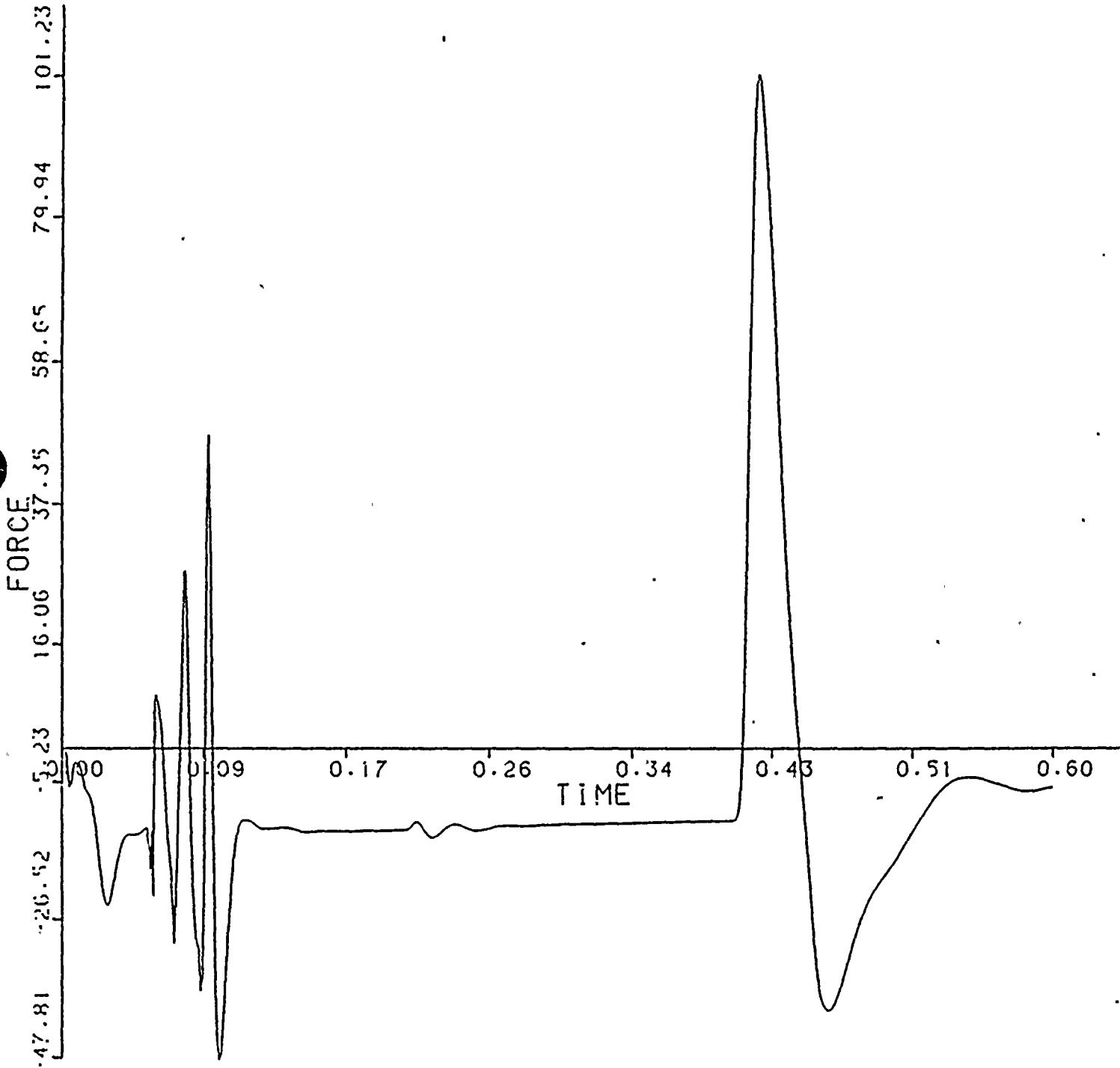
SAP2SAP VERIFICATION 5364

23 MAY 83

YEL-RED SOLID UNIT 1, 0-600 MS

TIME/FORCE TABLE 45, MAGNITUDE AT NODE POINT

360



DONE BY: 42 DATE: 5-2-83

CHKD BY: 11 DATE: 5-25-83

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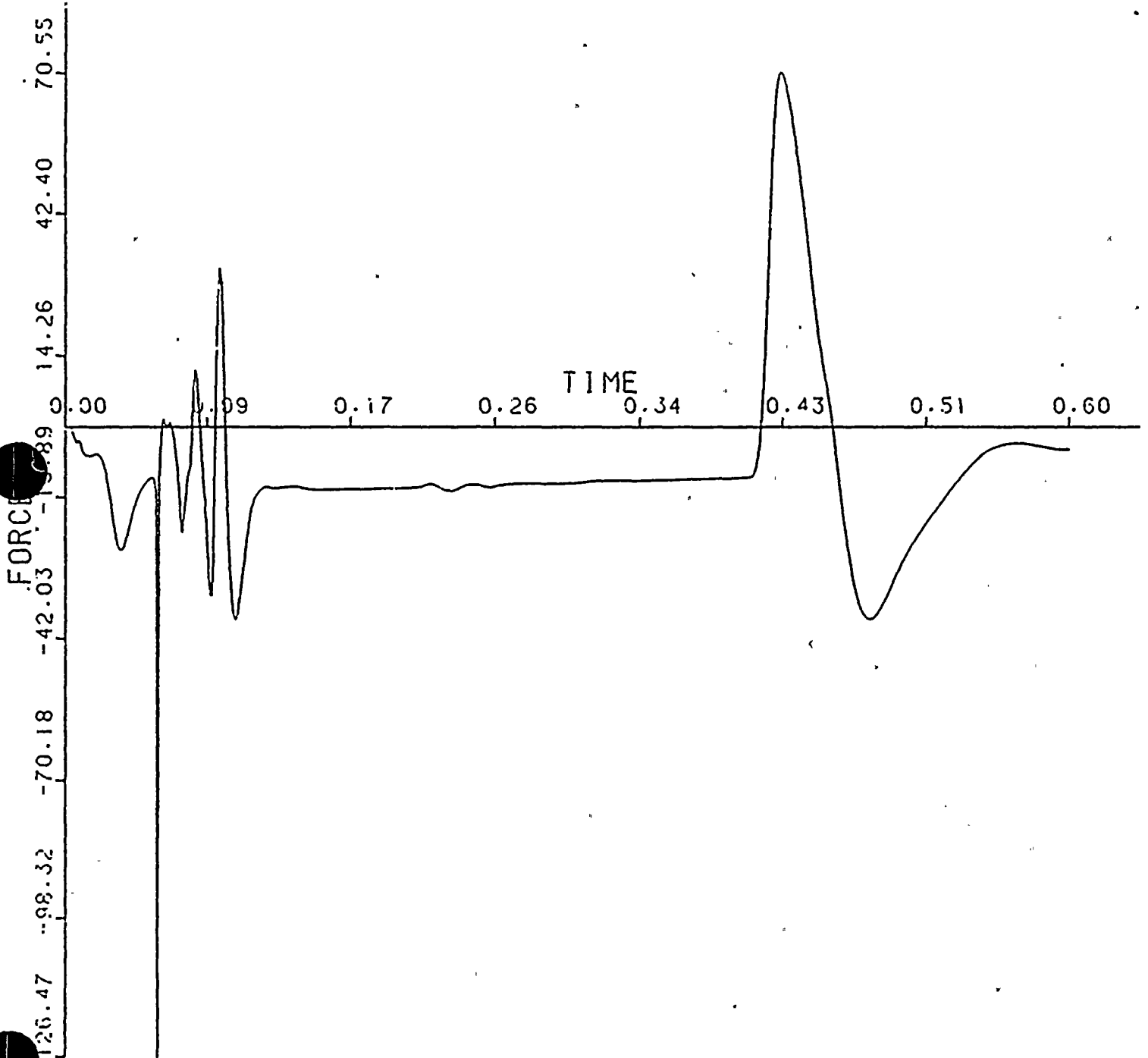
SAP2SAP VERIFICATION 5364

23 MAY 93

YEL-RED SOLID UNIT 1, 0-600 MS

TIME/FORCE TABLE 46, MAGNITUDE AT NODE POINT

355.



DONE BY: MR DATE: 5-12-93

CHKD BY: JK DATE: 5-25-93

SAP2SAP VERIFICATION 5364

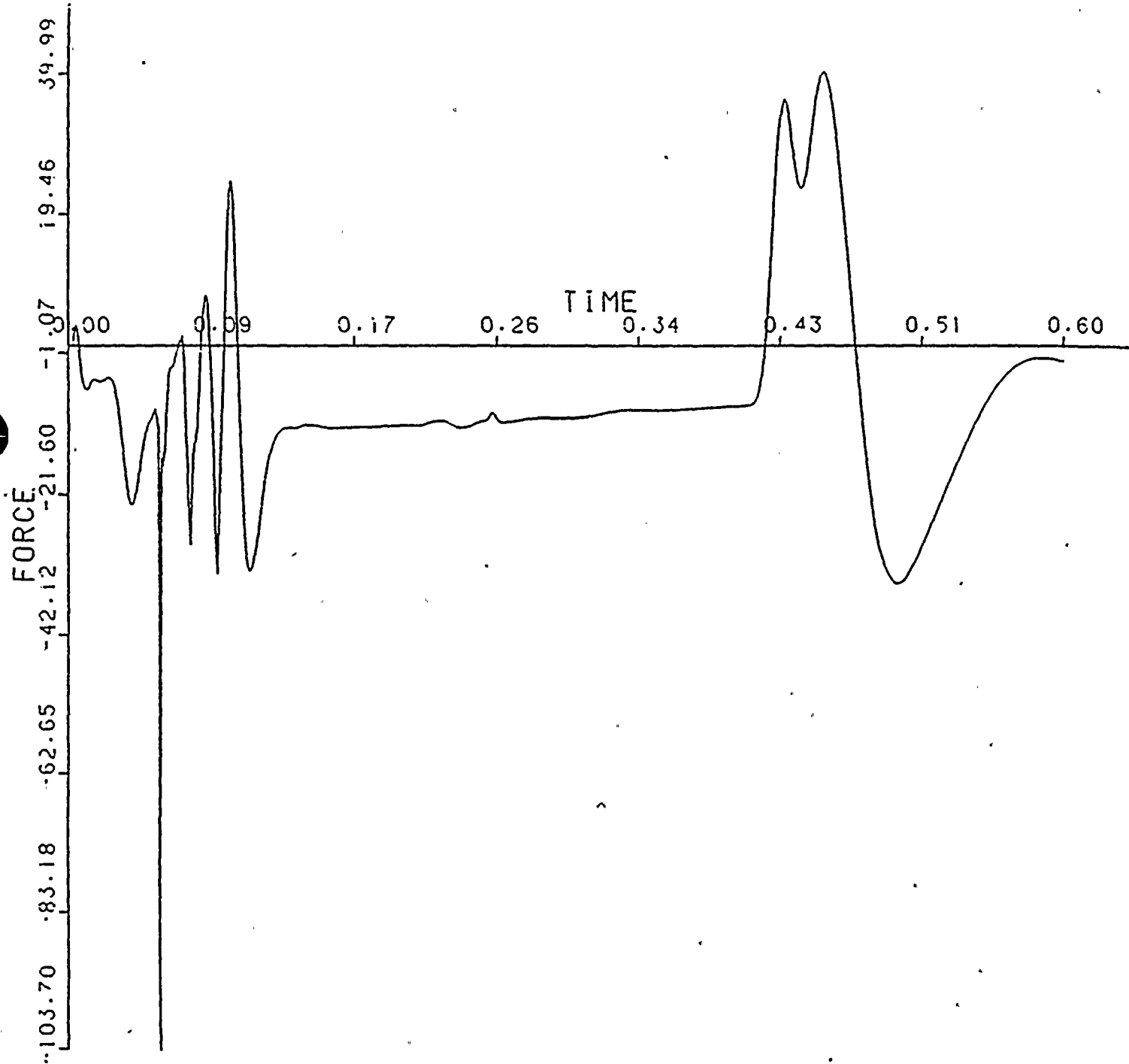
23-MAY-83

YEL-RED SOLID UNIT 1, 0-600 MS

TIME/FORCE TABLE

47, MAGNITUDE AT NODE POINT

350



DONE BY: 42 DATE: 5-2-83
CHKD BY: 14 DATE: 5-25-83

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ENGINEERING SERVICES

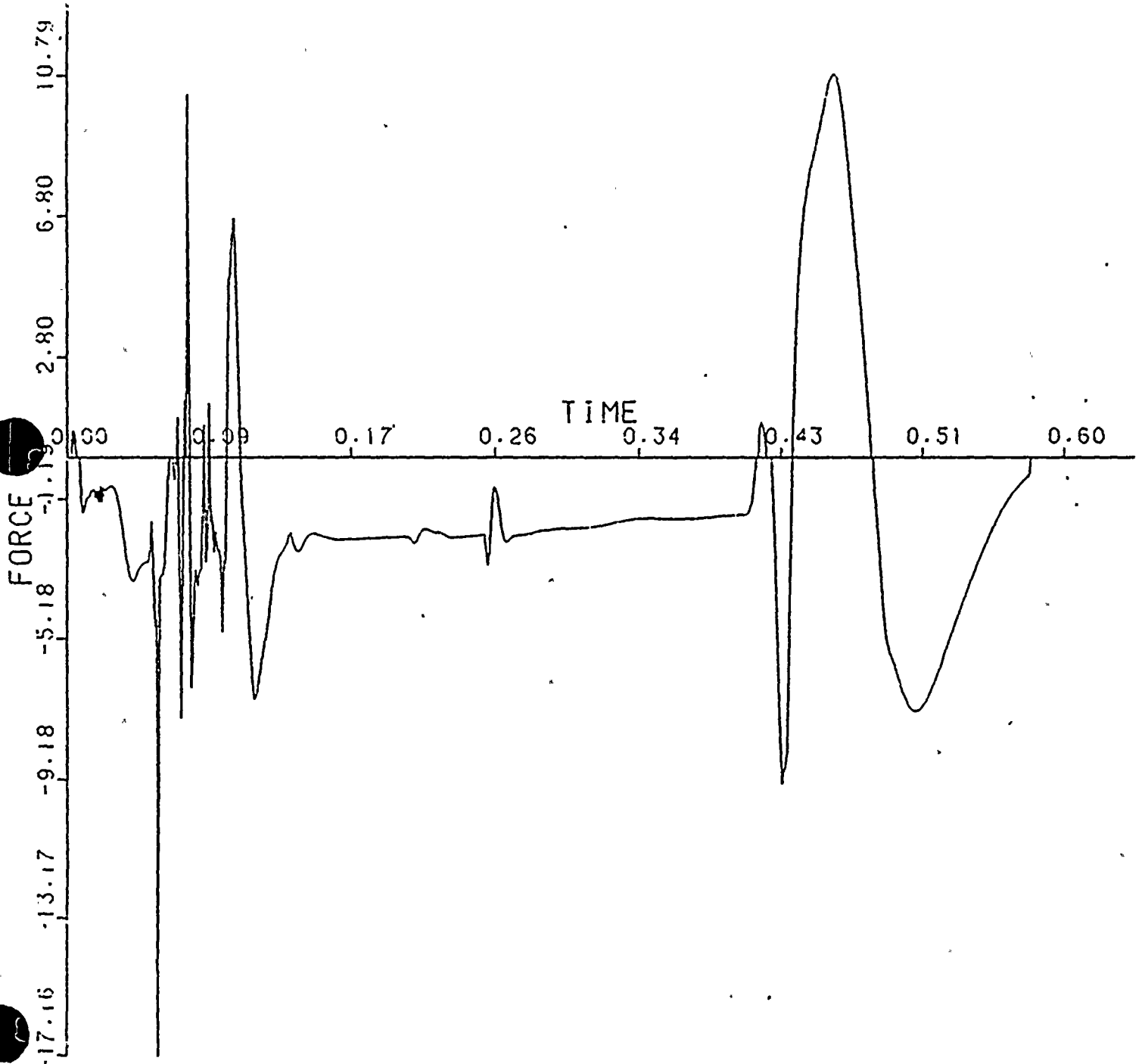
SAP2SAP VERIFICATION 5364

23-MAY-83

YEL-RED SOLID UNIT 1. 0-600 MS

TIME/FORCE TABLE 48. MAGNITUDE AT NODE POINT

340



DONE BY: 42 DATE: 5-25-83

CHKD BY: 1/4 DATE: 5-25-83

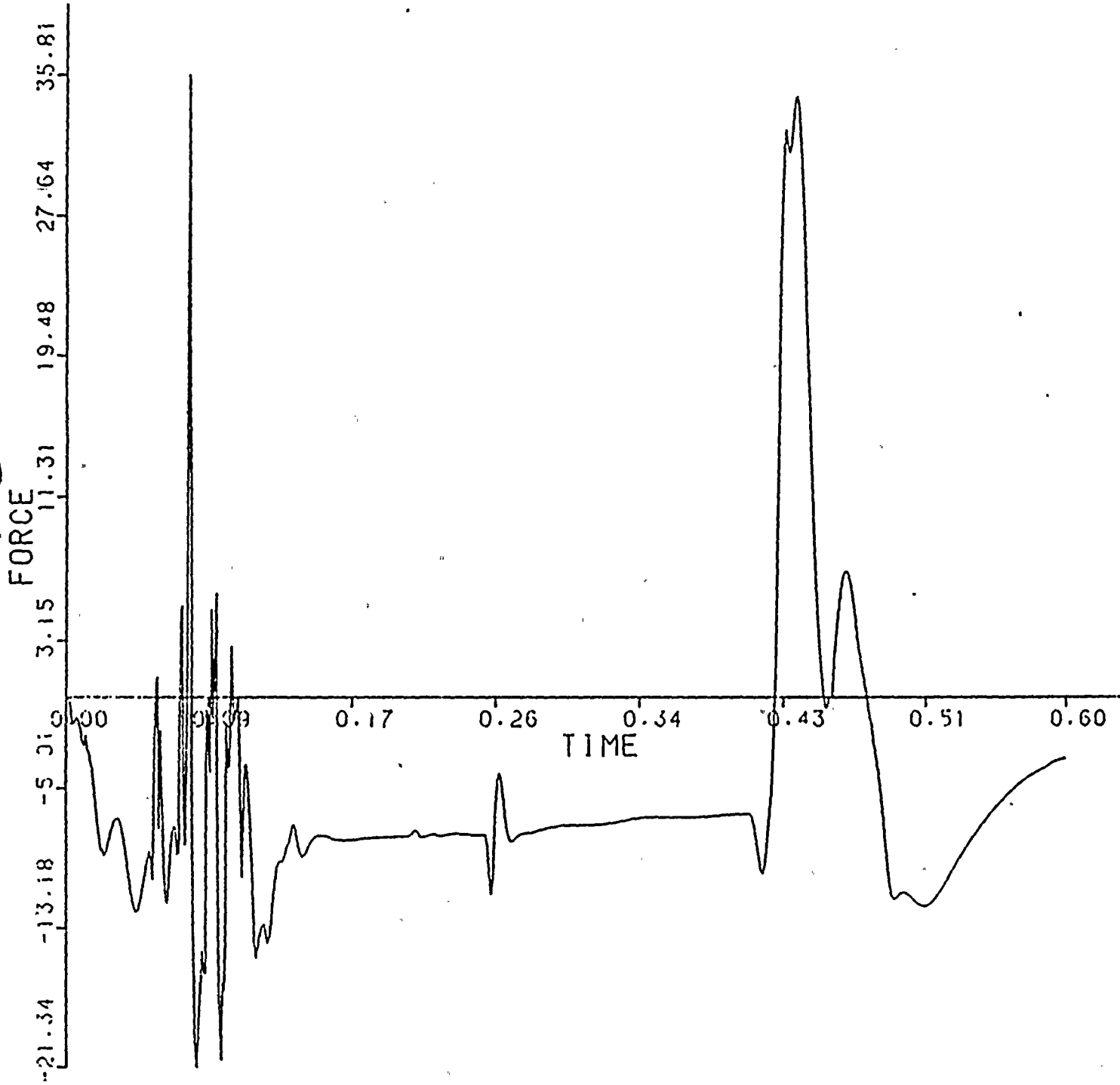
SAP2SAP VERIFICATION 5364

23-MAY-83

YEL-RED SOLID UNIT 1, 0-600 MS

TIME/FORCE TABLE 49, MAGNITUDE AT NODE POINT

335



DONE BY: MM DATE: 5-2-83

CHKD BY: MM DATE: 5-25-83

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TELEDYNE-
ENGINEERING SERVICES

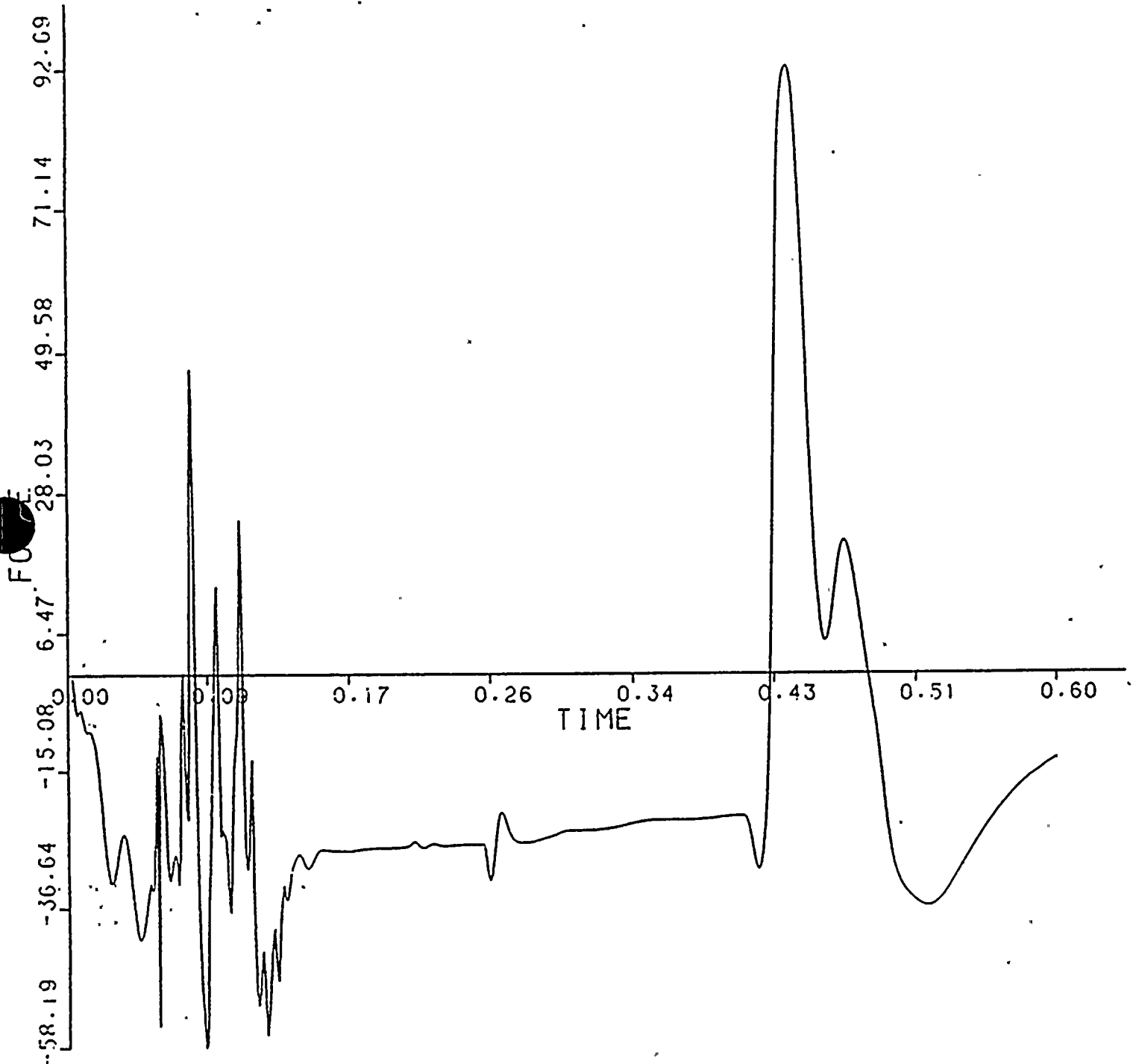
SAP2SAP VERIFICATION 5364

23-MAY-83

YEL-RED SOLID UNIT i, 0-600 MS

TIME/FORCE TABLE . 50. MAGNITUDE AT NODE POINT

325



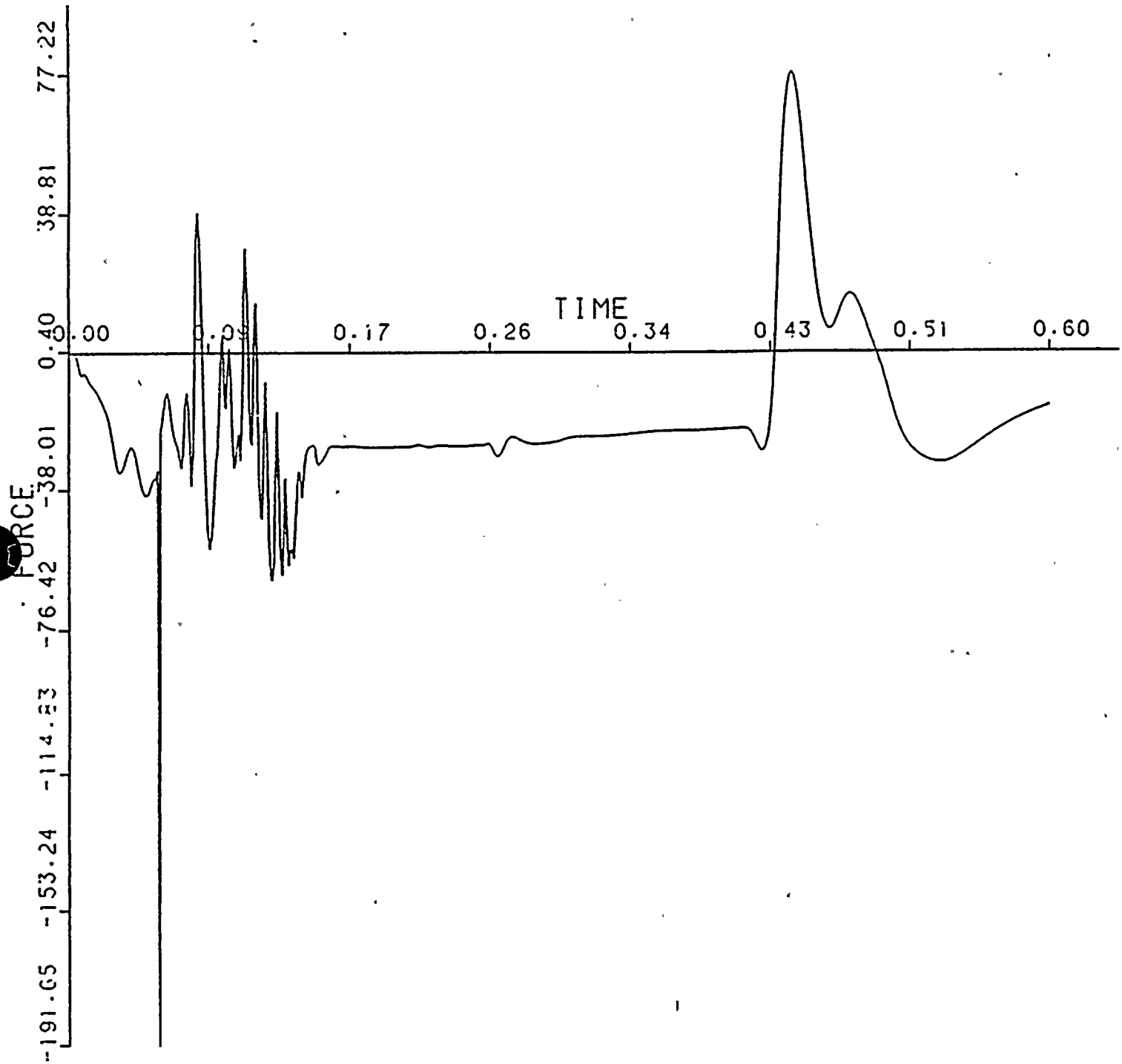
DONE BY: DATE: 5-25-83

CHKD BY: DATE: 5-25-83

SAP2SAP VERIFICATION 5364

YEL-RED SOLID UNIT 1, 0-600 MS

TIME/FORCE TABLE 51. MAGNITUDE AT NODE POINT



DONE BY: MR DATE: 5-21-83

CHKD BY: MM DATE: 5-25-83



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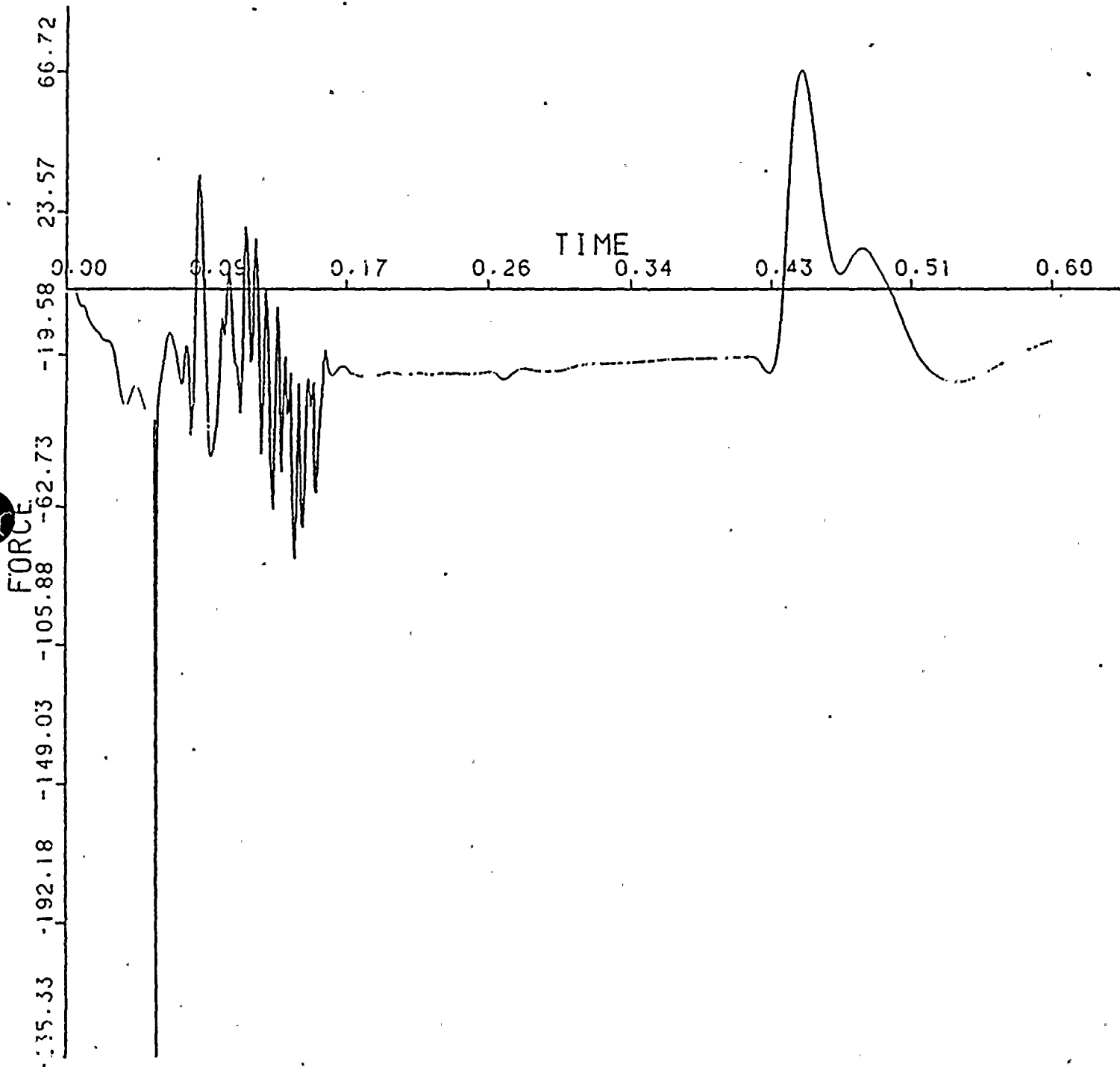
SAP2SAP VERIFICATION 5364

23-MAY-83

YEL-RED SOLID UNIT 1, 0-600 MS

TIME/FORCE TABLE 52, MAGNITUDE AT NODE POINT

310



DONE BY: DATE: 5-2-83

CHKD BY: DATE: 5-2-83

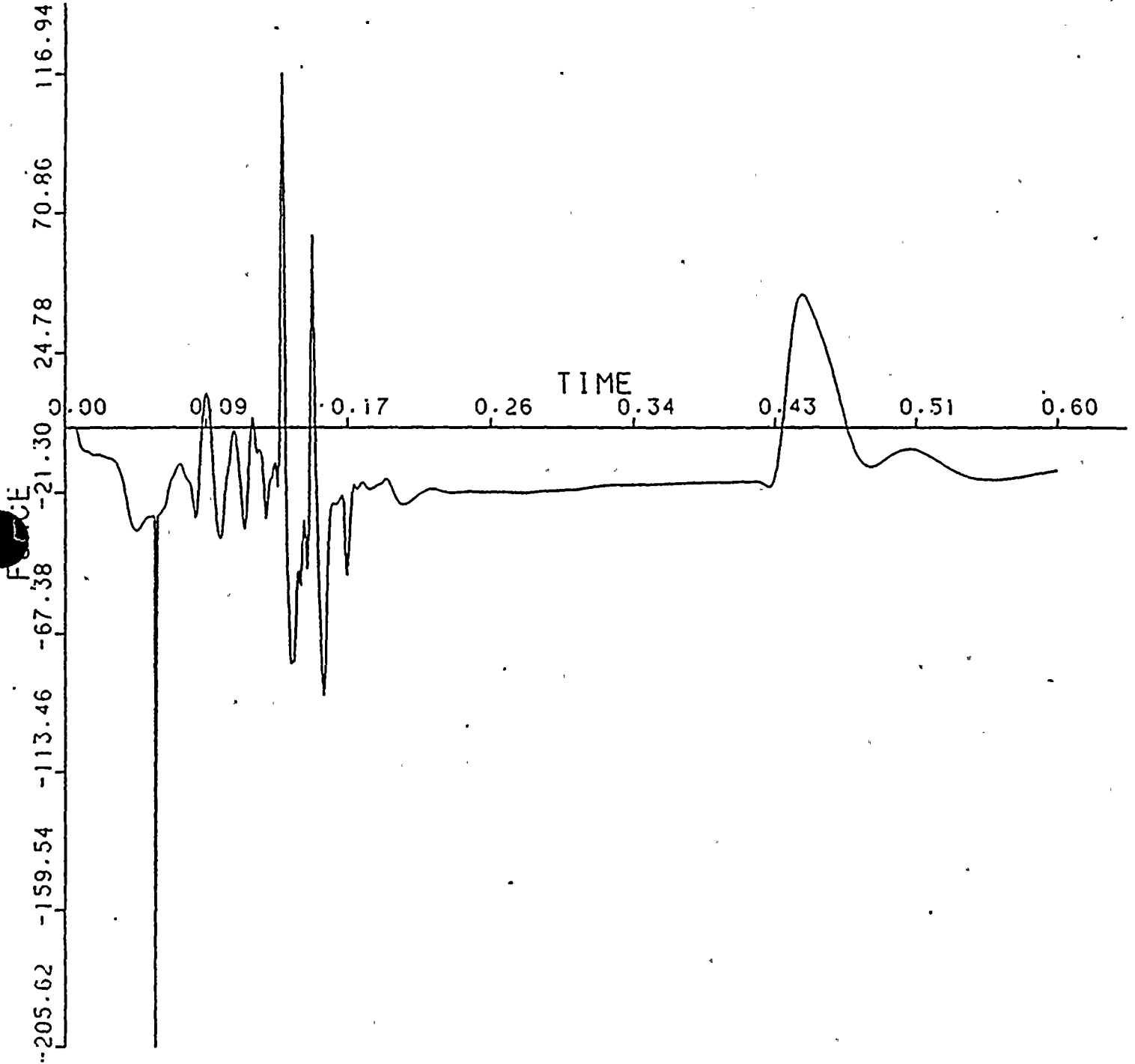


SAP2SAP VERIFICATION 5364

23-MAY-83

YEL-RED SOLID UNIT 1, 0-600 MS

TIME/FORCE TABLE 53, MAGNITUDE AT NODE POINT



DONE BY: MD DATE: 5-23-83
CHKD BY: MD DATE: 5-23-83



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TELEDYNE
ENGINEERING SERVICES

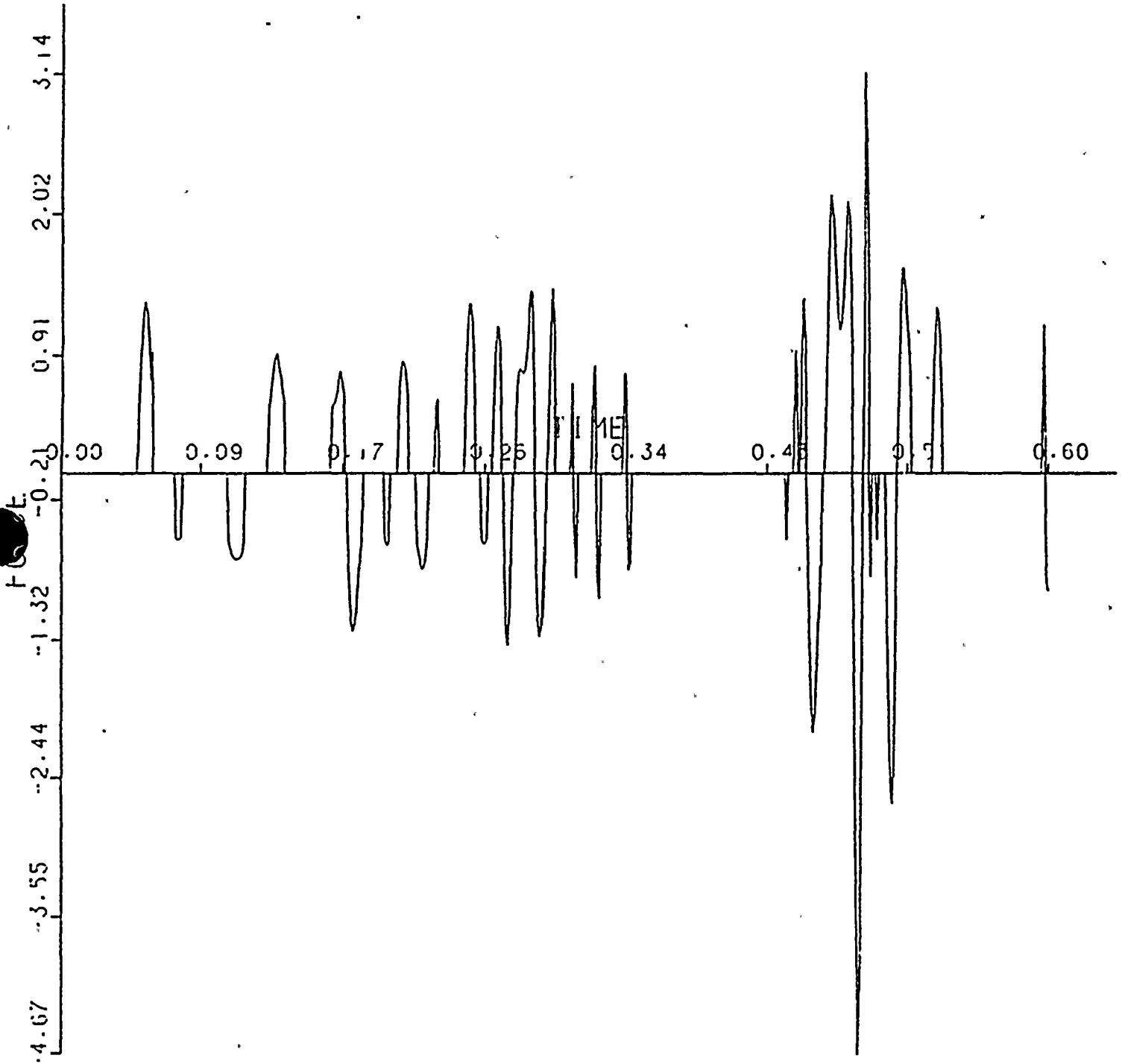
SAP2SAP VERIFICATION 5364

23-MAY-83

YEL-RED SOLID UNIT 1, 0-600 MS

TIME/FORCE TABLE 54, MAGNITUDE AT NODE POINT

114



DONE BY: VE DATE: 5-12-83

CHKD BY: MM DATE: 5-25-83

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TELEDYNE
ENGINEERING SERVICES

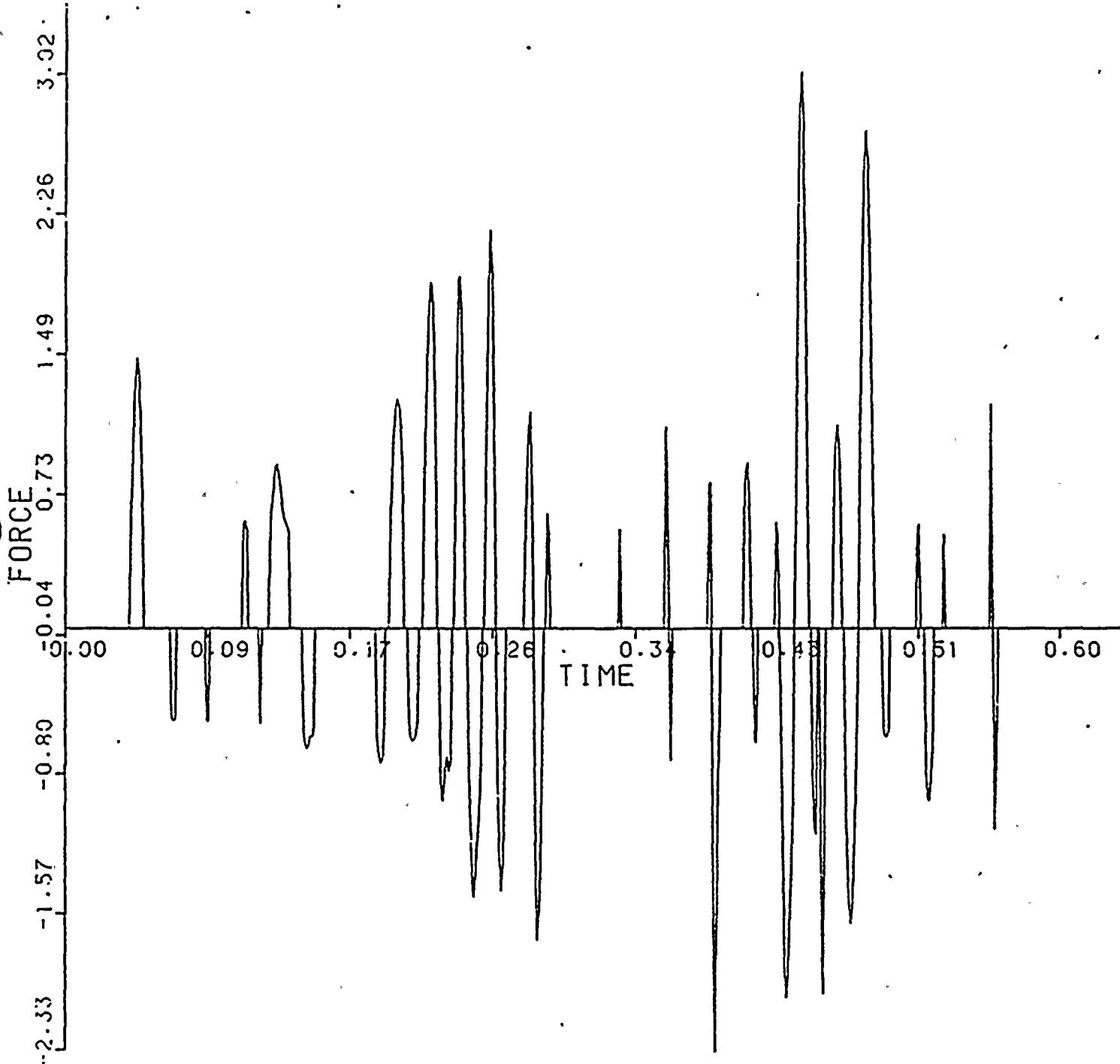
SAP2SAP VERIFICATION 5364

23-MAY-83

YEL-RED. SOLID UNIT 1, 0-600 MS

TIME/FORCE TABLE 55. MAGNITUDE AT NODE POINT

162



DONE BY: ME DATE: 5-2-83

CHKD BY: ME DATE: 5-2-83

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WILEY ENGINEERING SERVICES

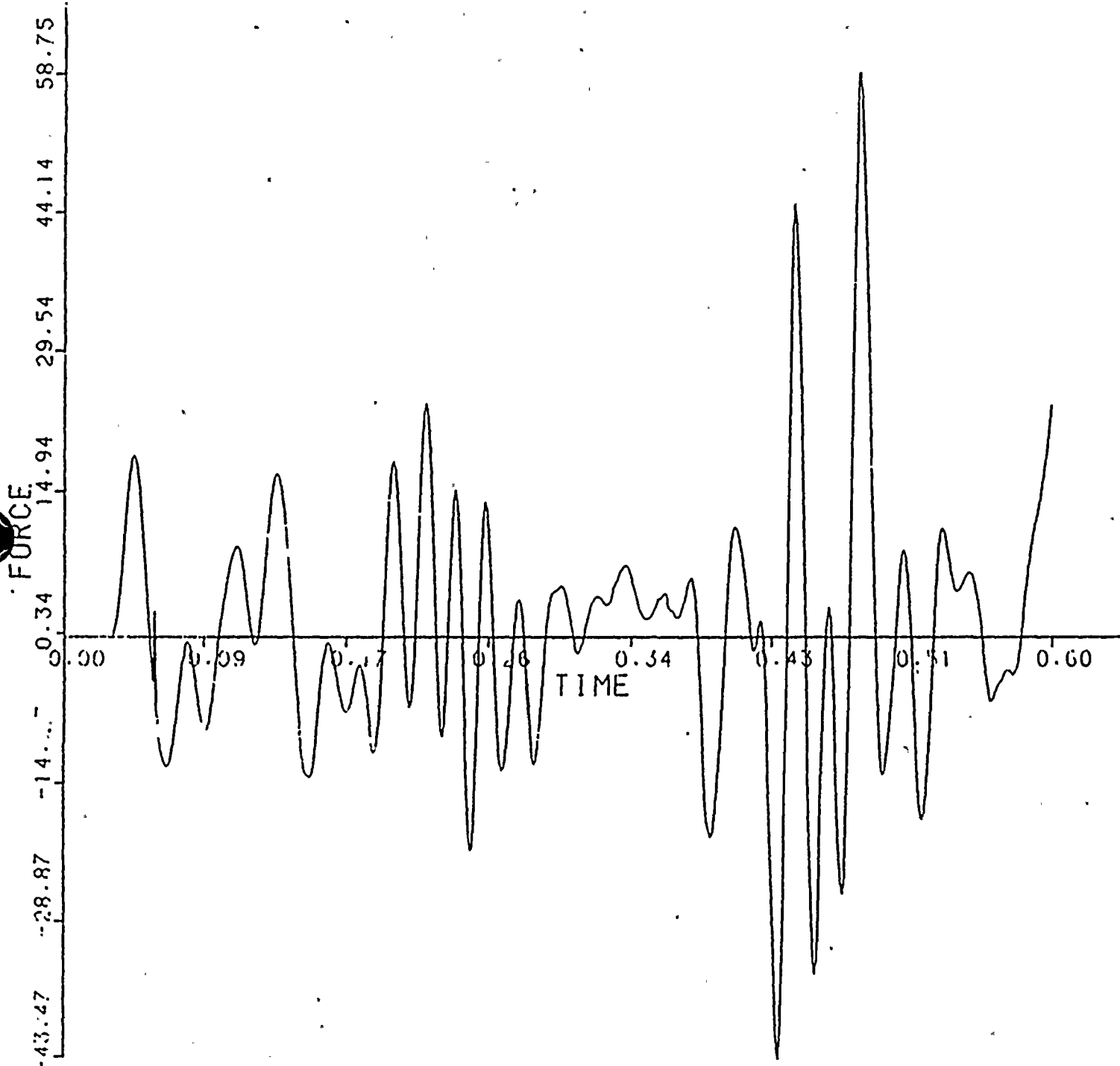
SAP2SAP VERIFICATION 5364

23-MAY-63

YEL-RED SOLID UNIT 1, 0.600 MS

TIME/FORCE TABLE 56. MAGNITUDE AT NODE POINT

157



DONE BY: ER DATE: 5-22-63

CHKD BY: LD DATE: 5-22-63

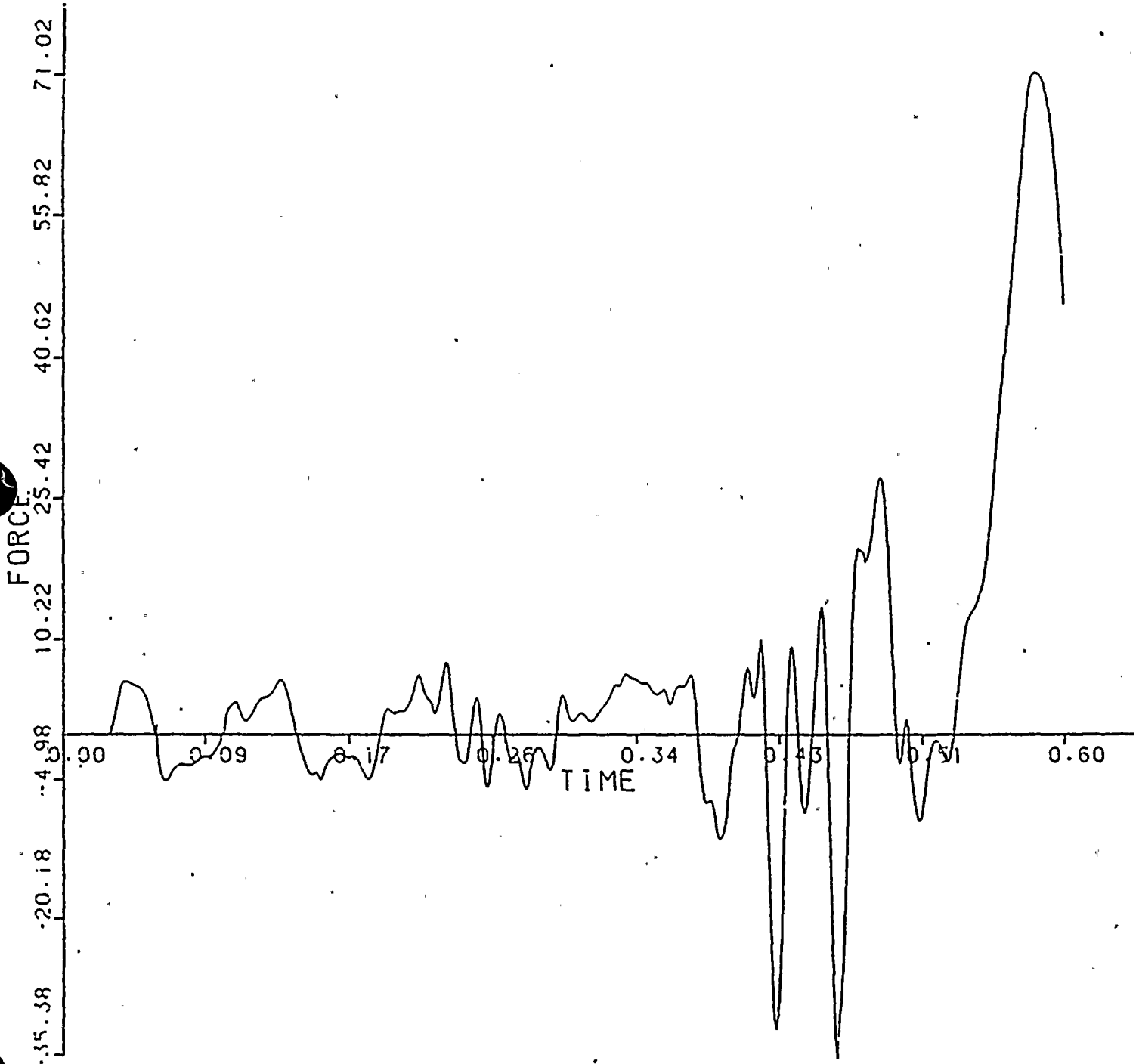
SAP2SAP VERIFICATION 5364

23-MAY-83

YEL-RED SOLID UNIT 1, 0-600 MS

TIME/FORCE TABLE 57. MAGNITUDE AT NODE POINT

150



DONE BY: DATE:

CHKD BY: DATE:

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TELEDYNE
ENGINEERING SERVICES

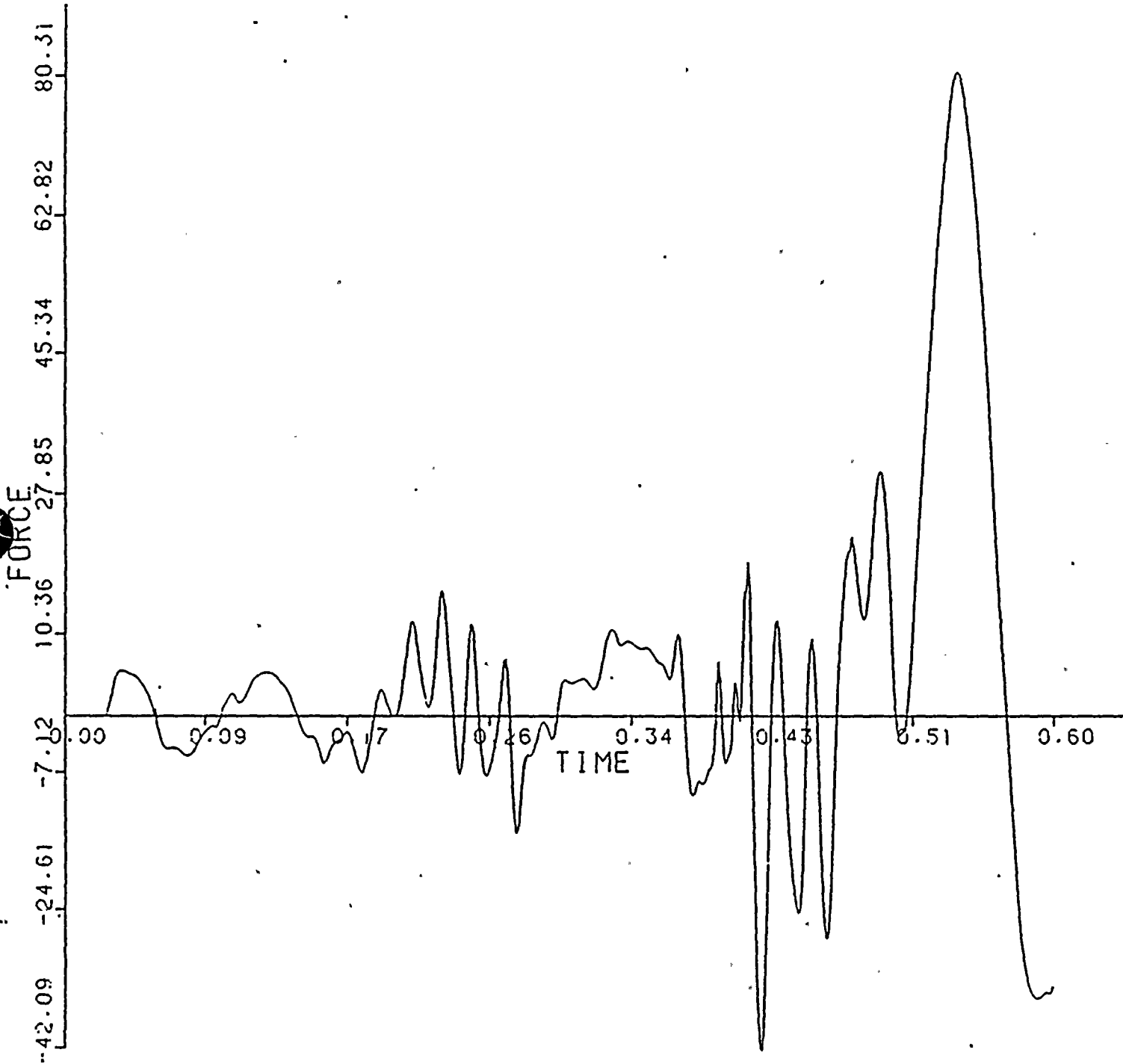
SAP2SAP VERIFICATION 5364

23-MAY-83

YEL-RED SOLID UNIT 1, 0-600 MS

TIME/FORCE TABLE 58, MAGNITUDE AT NODE POINT

148



DONE BY: DATE: 5-2-83

CHKD BY: DATE: 5-23-83

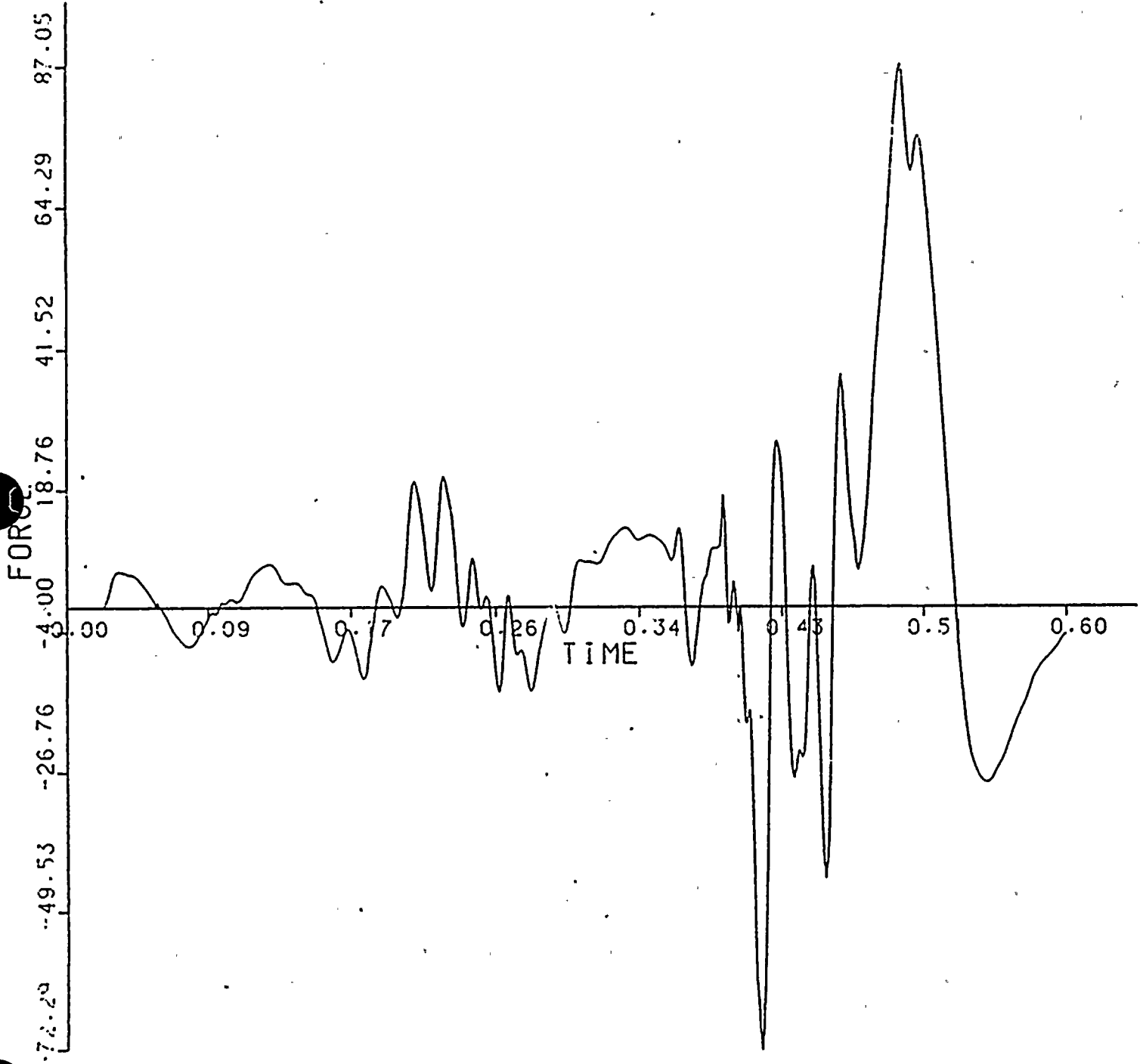
SAP2SAP VERIFICATION 5364

23-MAY-83

YEL-RED SOLID UNIT 1, 0-600 MS

TIME/FORCE TABLE 59, MAGNITUDE, AT NODE POINT

i46



DONE BY: VR DATE: 5-2-83

CHKD BY: MM DATE: 5-15-83

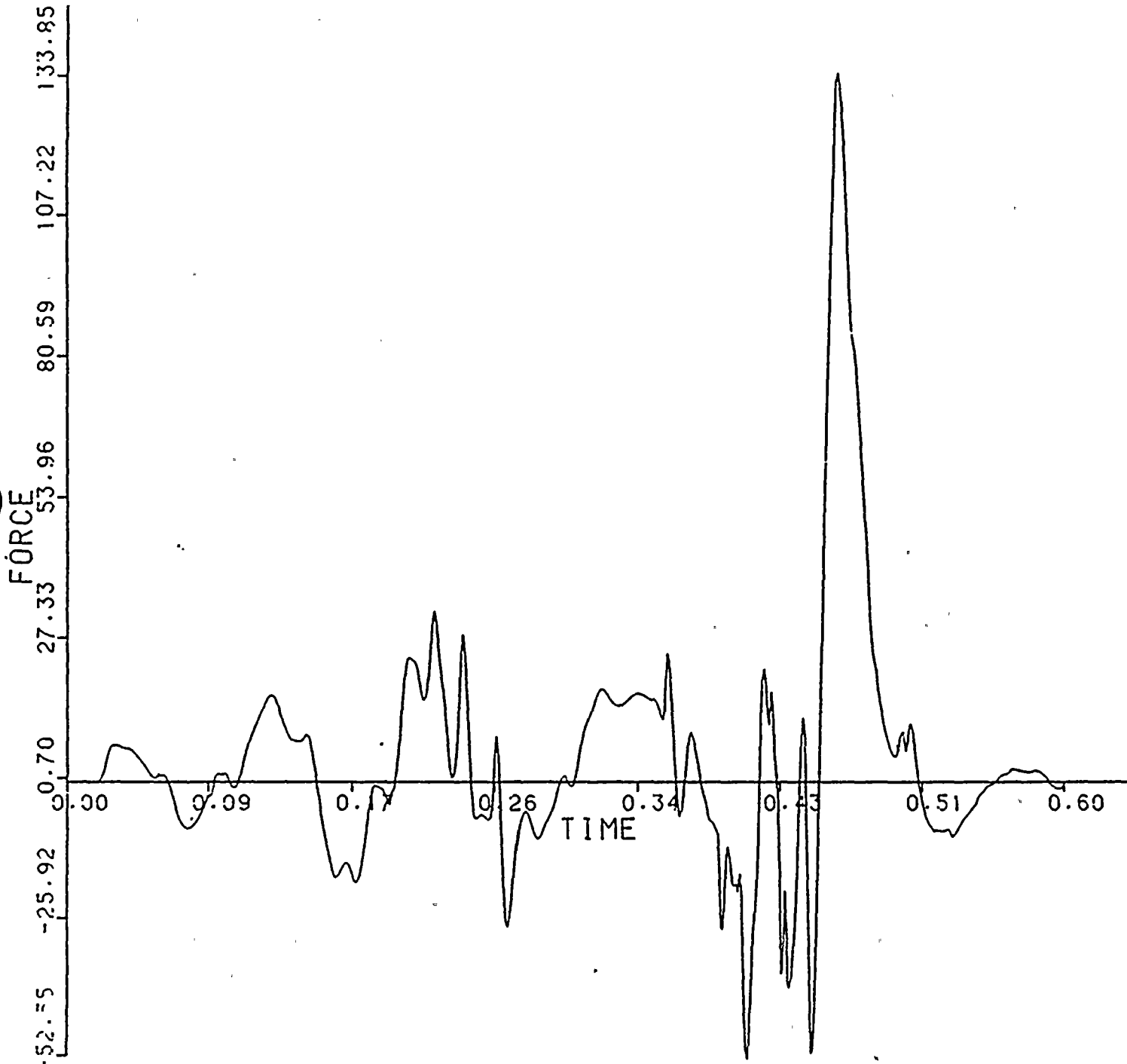


SAP2SAP VERIFICATION 5364

23-MAY-83

YEL-RED SOLID UNIT 1, 0-600 MS

TIME/FORCE TABLE 60, MAGNITUDE. AT NODE:POINT



DONE BY: DATE: 5-23-83

CHKD BY: DATE: 5-23-83

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WILSON ENGINEERING SERVICES

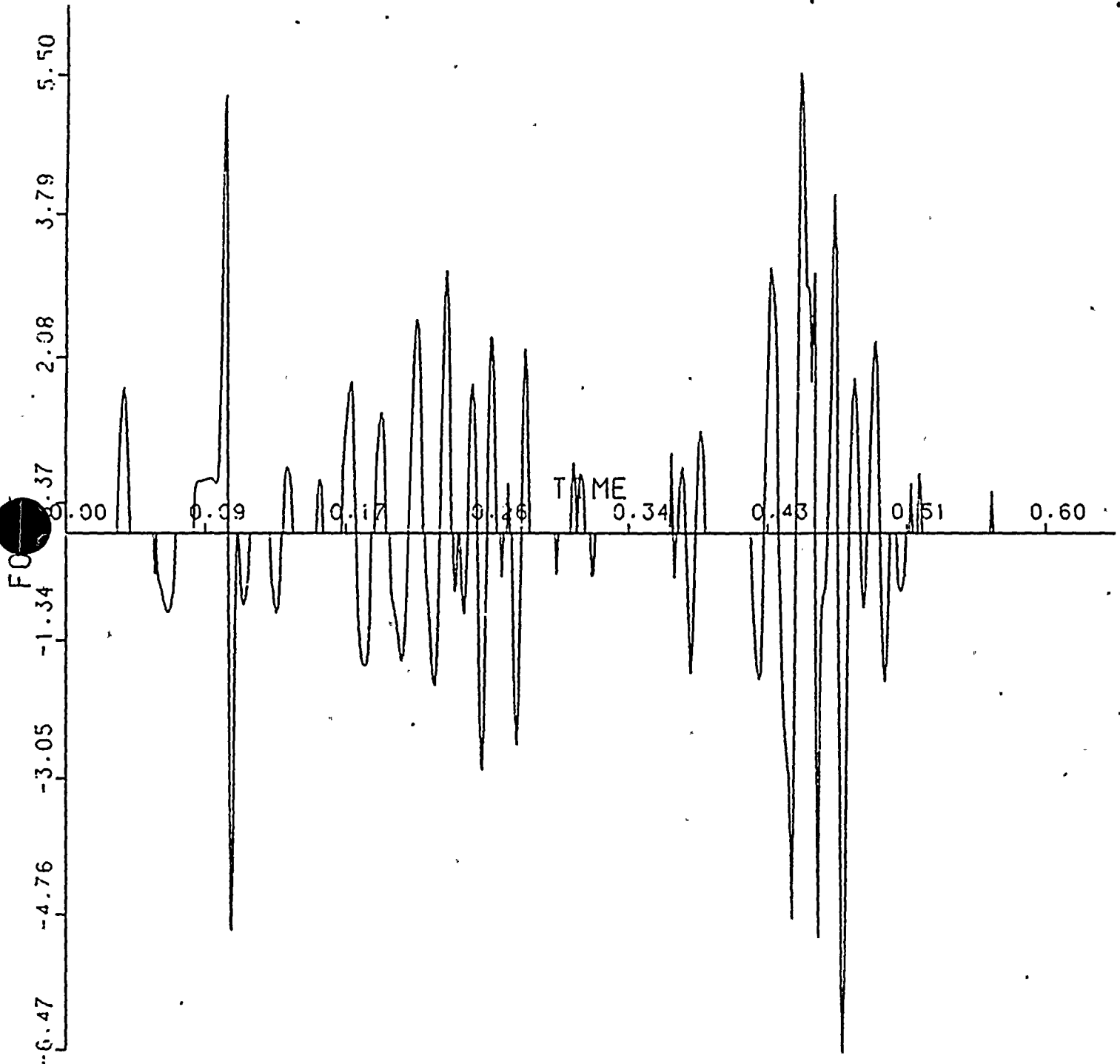
SAP2SAP VERIFICATION 5364

23-MAY-83

YEL-RED SOLID UNIT 1, 0-600 MS

TIME/FORCE TABLE 61. MAGNITUDE AT NODE POINT

223



DONE BY: ME DATE: 5-25-83

CHKD BY: JA DATE: 5-25-83

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SAP2SAP VERIFICATION 5364

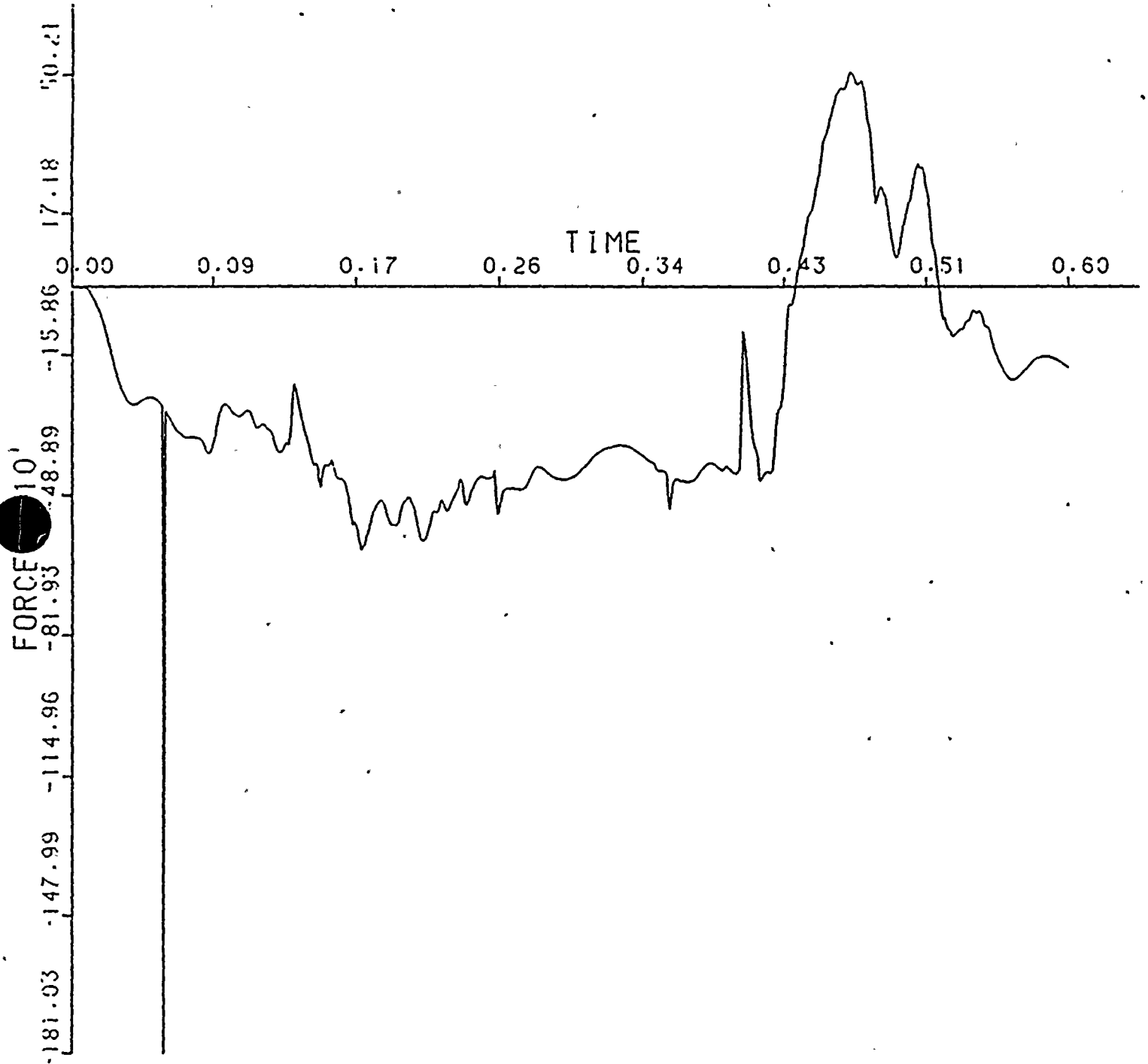
23-MAY-83

YEL-RED SOLID UNIT 1, 0-600 MS

TIME/FORCE TABLE

62. MAGNITUDE AT NODE POINT

260



DONE BY: MZ DATE: 5-2-83
CHKD BY: JM DATE: 5-25-83



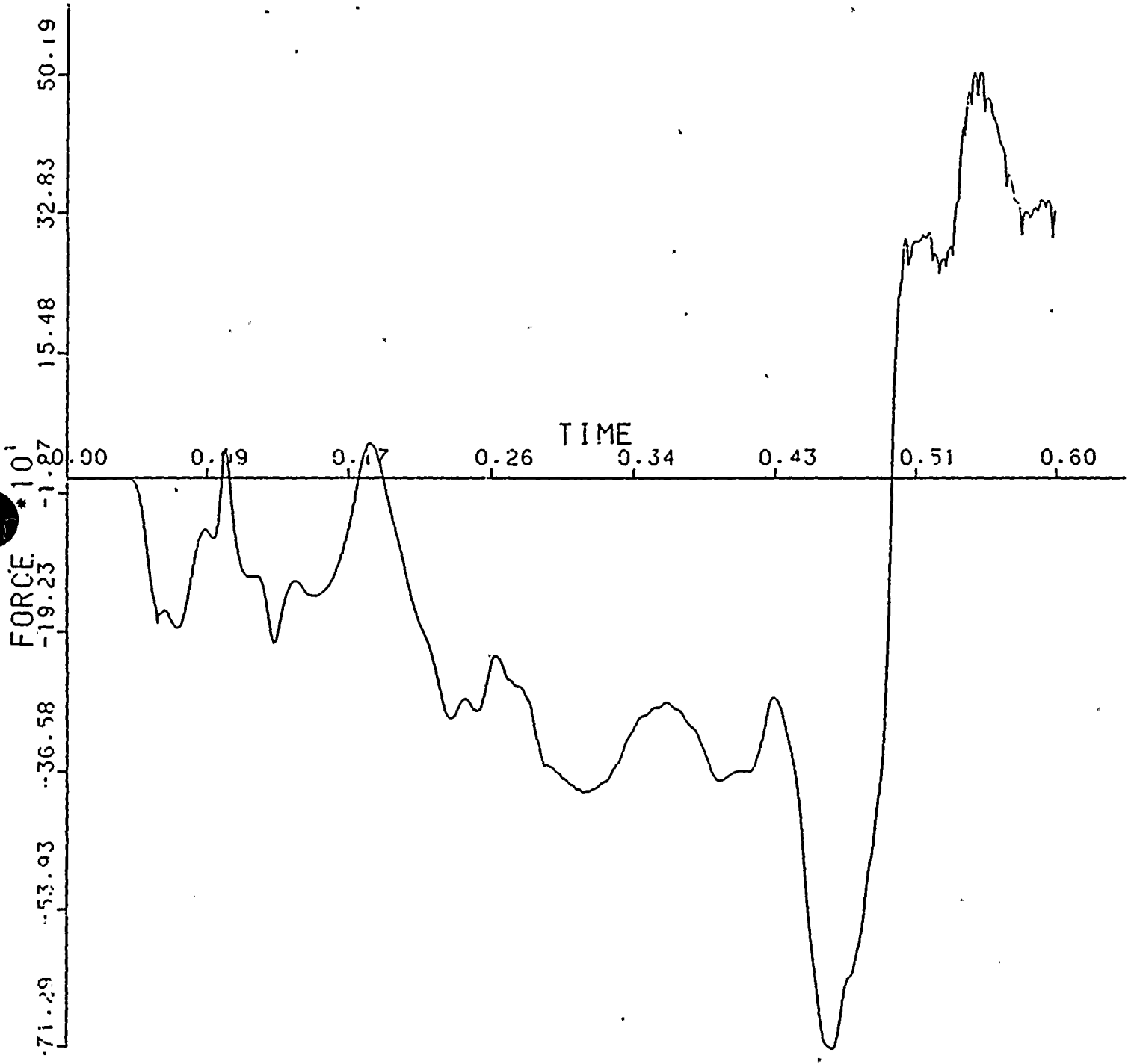
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4-383 W ENGINEERING SERVICES
23-MAY-83

SAP2SAP VERIFICATION 5364

YFL-RFD SOLID UNIT 1, 0-600 MS

TIME / FORCE LABEL G.S. MAGNITUDE AT NODE POINT GR



DONE BY: MR DATE: 5/2/83
CHKD BY: CM DATE: 5-23-83

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ENGINEERING SERVICES

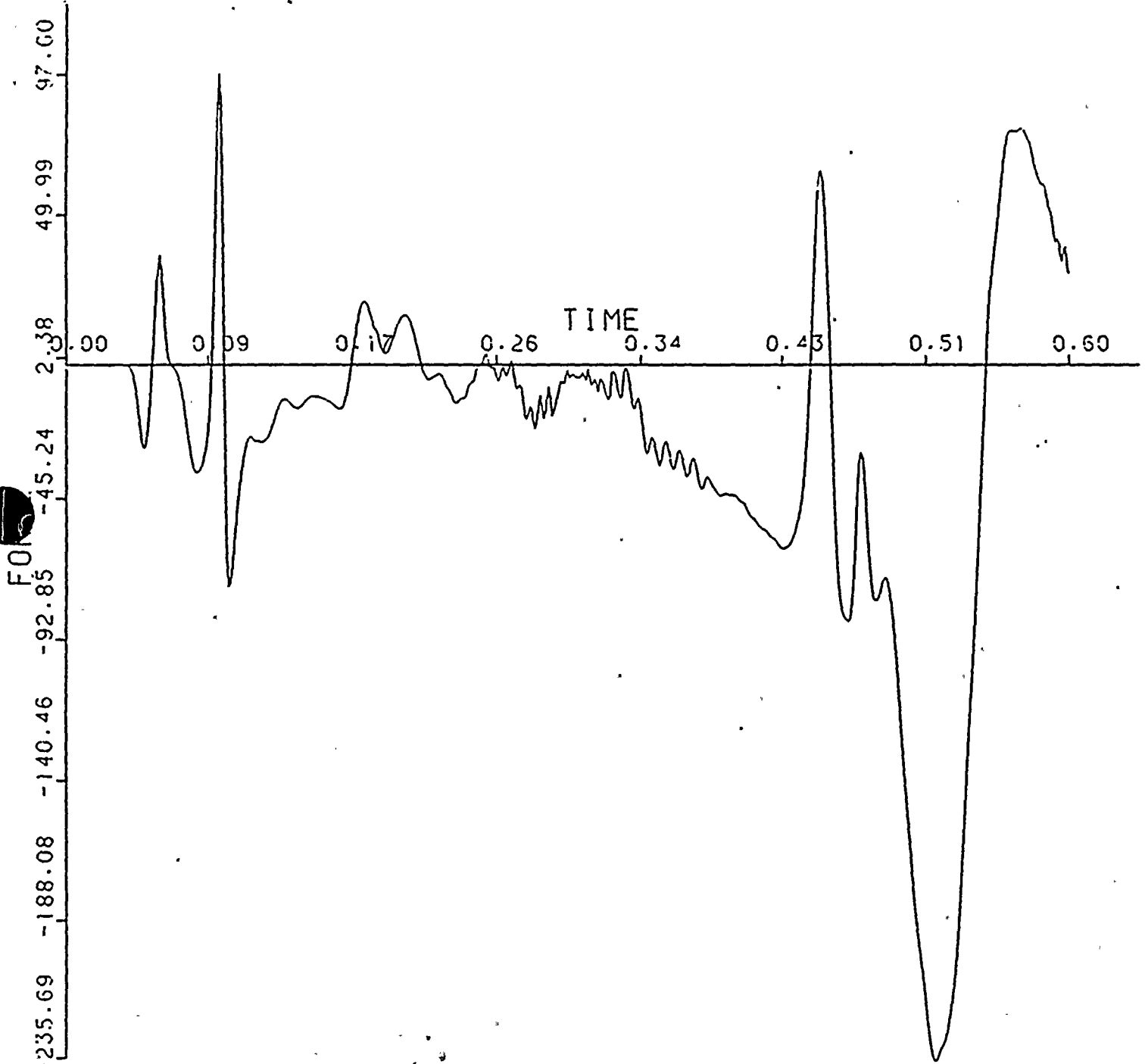
SAP2SAP VERIFICATION 5364

23-MAY-83

YEL-RED SOLID UNIT i. 0-600 MS

TIME/FORCE TABLE 64. MAGNITUDE AT NODE POINT

58



DONE BY: MZ DATE: 5-12-83

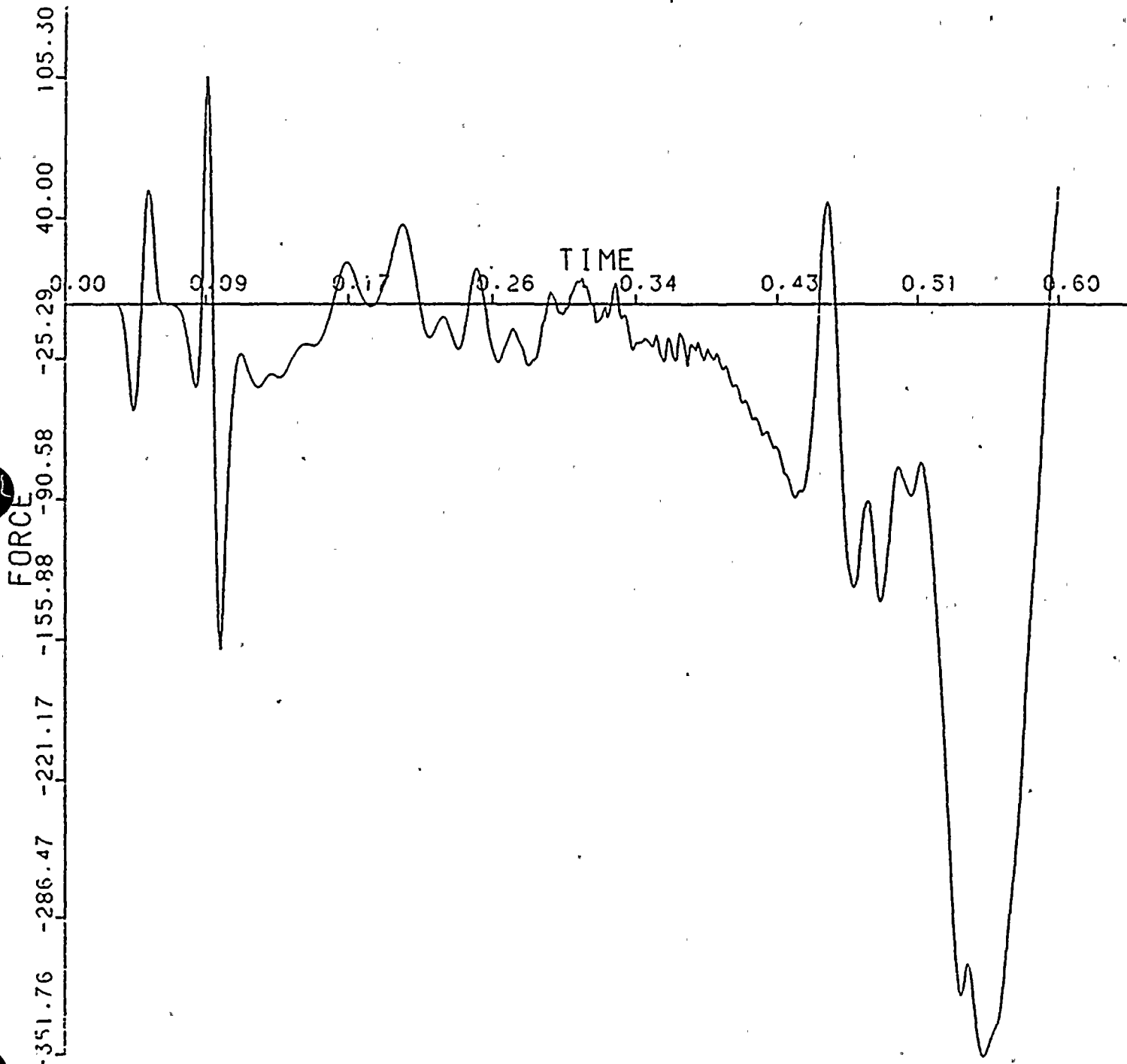
CHKD BY: JH DATE: 5-23-83

SAP2SAP VERIFICATION 5364

23-MAY-83

Y11 RFD SOLID UNIT 1, 0 600 MS

TIME / FORCE LABEL 65, MAGNITUDE AT NODE POINT



DONE BY: M DATE: 5-12-83

CHKD BY: M DATE: 5-25-83

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WELDING ENGINEERING SERVICES

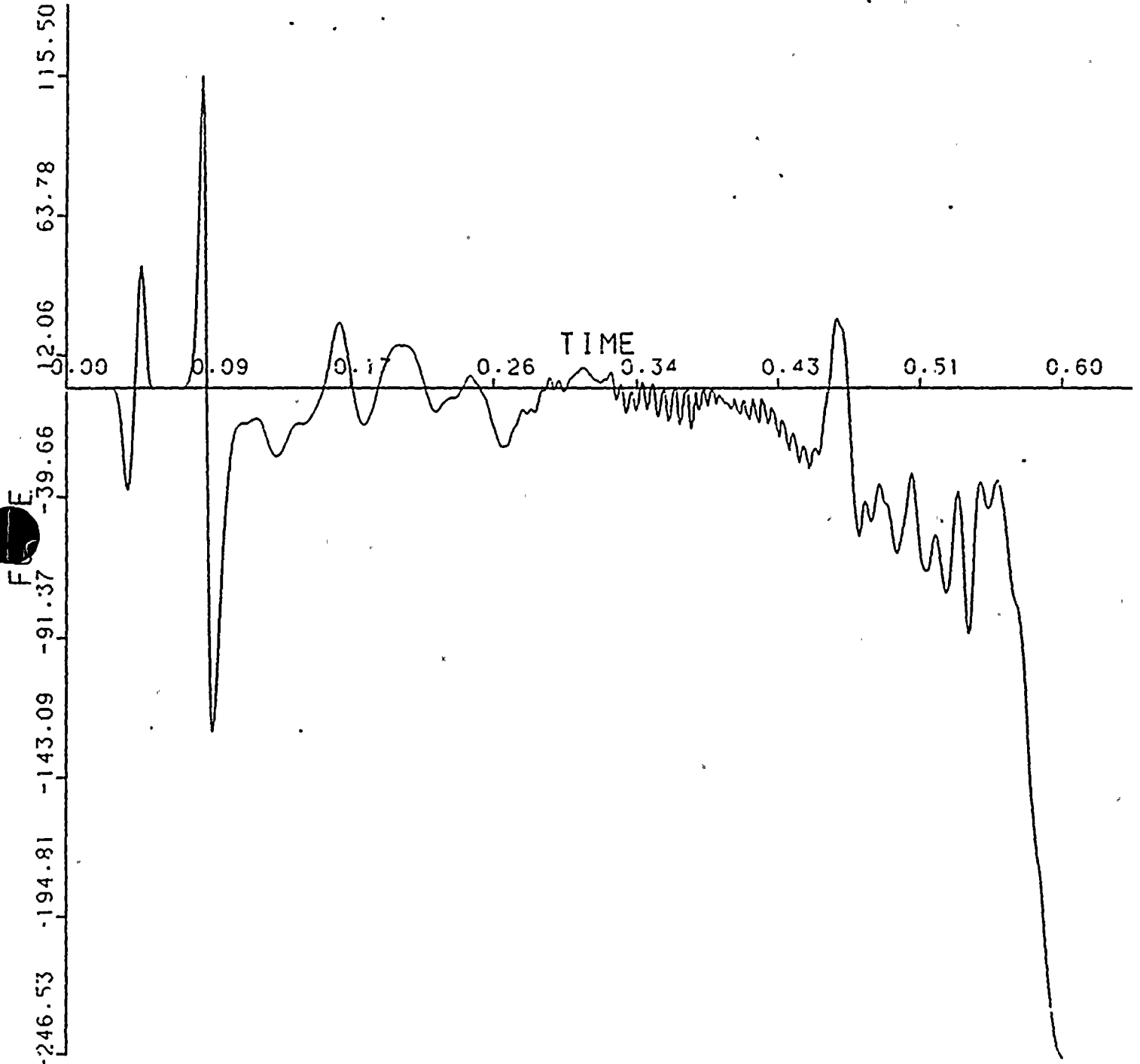
23 MAY 83

SAP2SAP VERIFICATION 5364

YEL-RED SOLID UNIT 1, 0-600 MS

TIME/FORCE TABLE 66. MAGNITUDE AT NODE POINT

48



DONE BY: MR DATE: 5-14-83

CHKD BY: MR DATE: 5-23-83

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TELEDYNE
ENGINEERING SERVICES

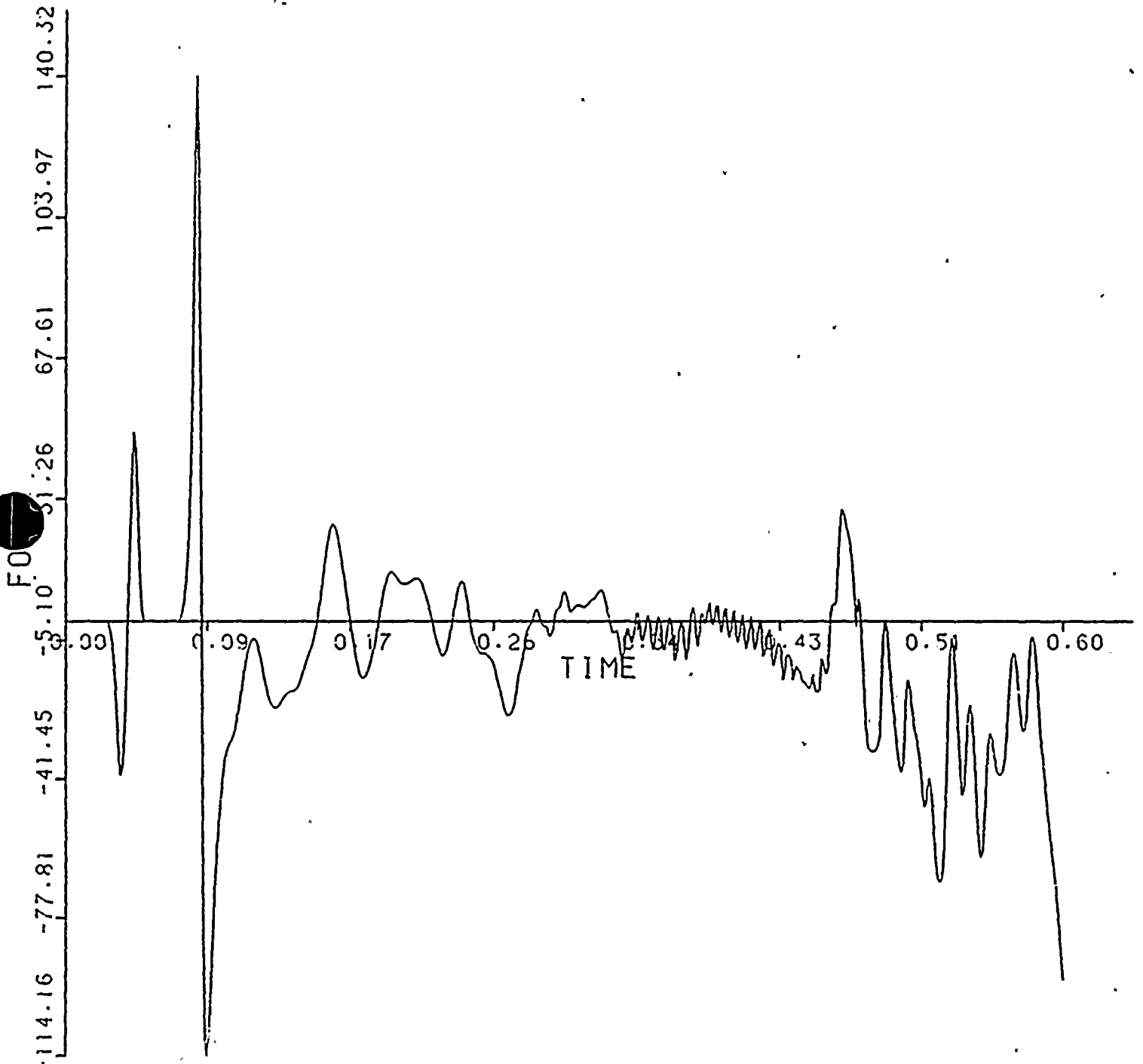
SAP2SAP VERIFICATION 5364

23-MAY-83

YEL-RED SOLID UNIT 1, 0-600 MS

TIME/FORCE TABLE 67, MAGNITUDE AT NODE POINT

40



DONE BY: MR DATE: 5-12-83

CHKD BY: MM DATE: 5-23-83

4-388

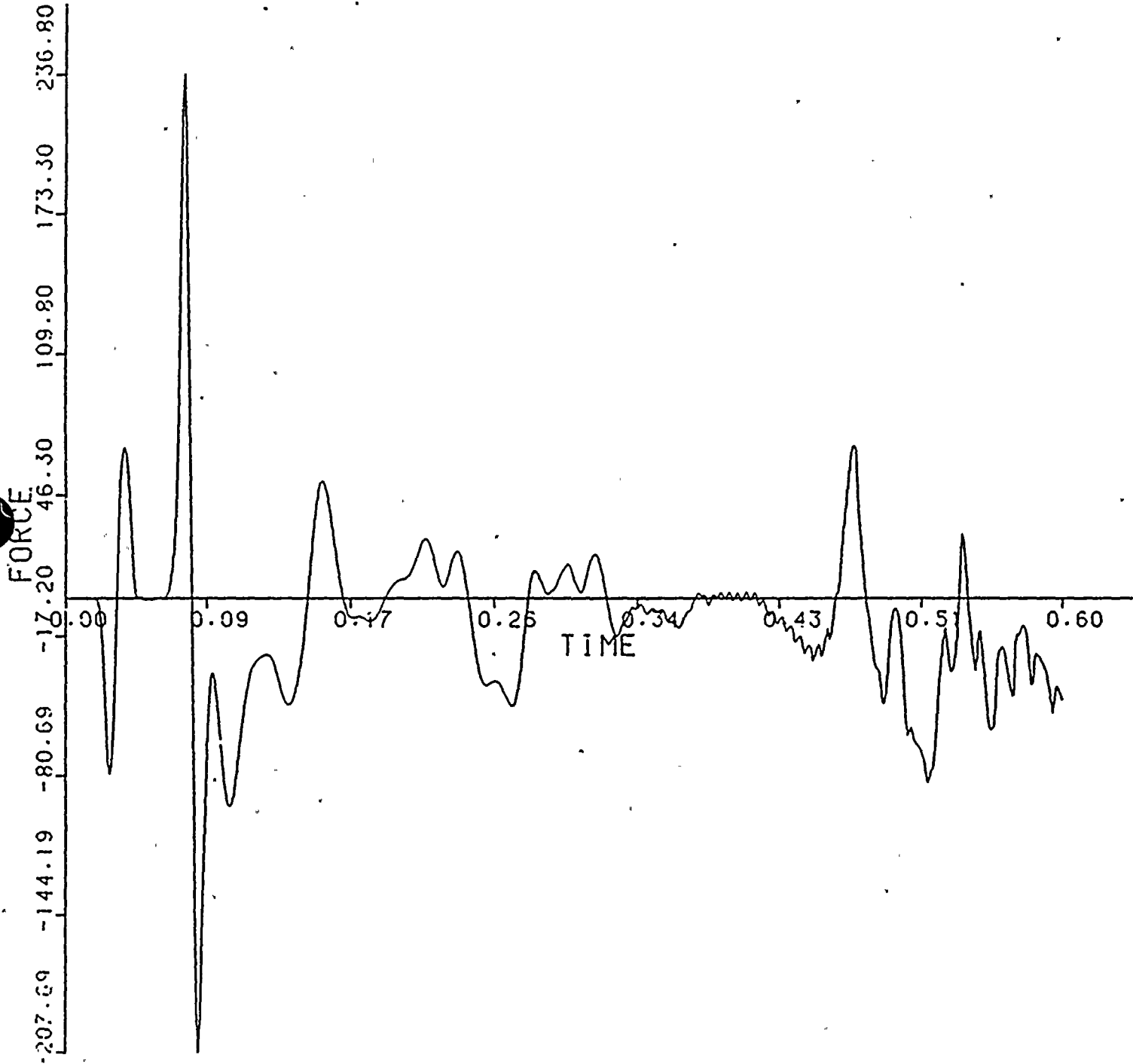
23-MAY-83

SAP2SAP VERIFICATION 5364

YEL-RED SOLID UNIT 1, 0-600 MS

TIME/FORCE TABLE 68, MAGNITUDE AT NODE POINT

34



DONE BY: 4/2 DATE: 5-15-83

CHKD BY: 3/11 DATE: 5-22-83



Technical Report

TR-5364-1

Revision 0

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ENGINEERING SERVICES

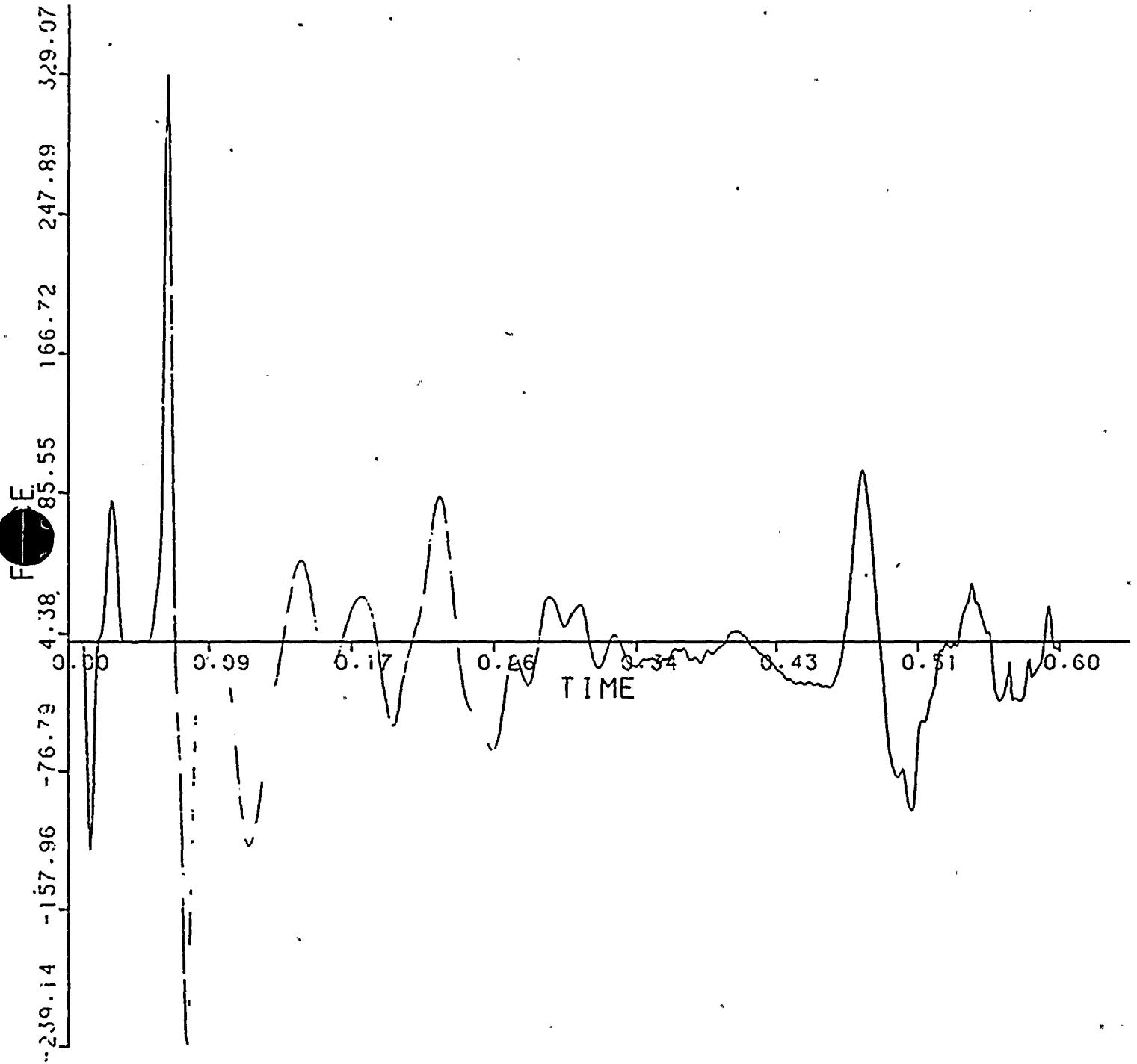
SAP2SAP VERIFICATION 5364

23-MAY-83

YEL-RED SOLID UNIT 1, 0-600 MS

TIME/FORCE TABLE 69, MAGNITUDE AT NODE POINT

18



DONE BY: MR DATE: 5/2/83

CHKD BY: CH DATE: 5-23-83

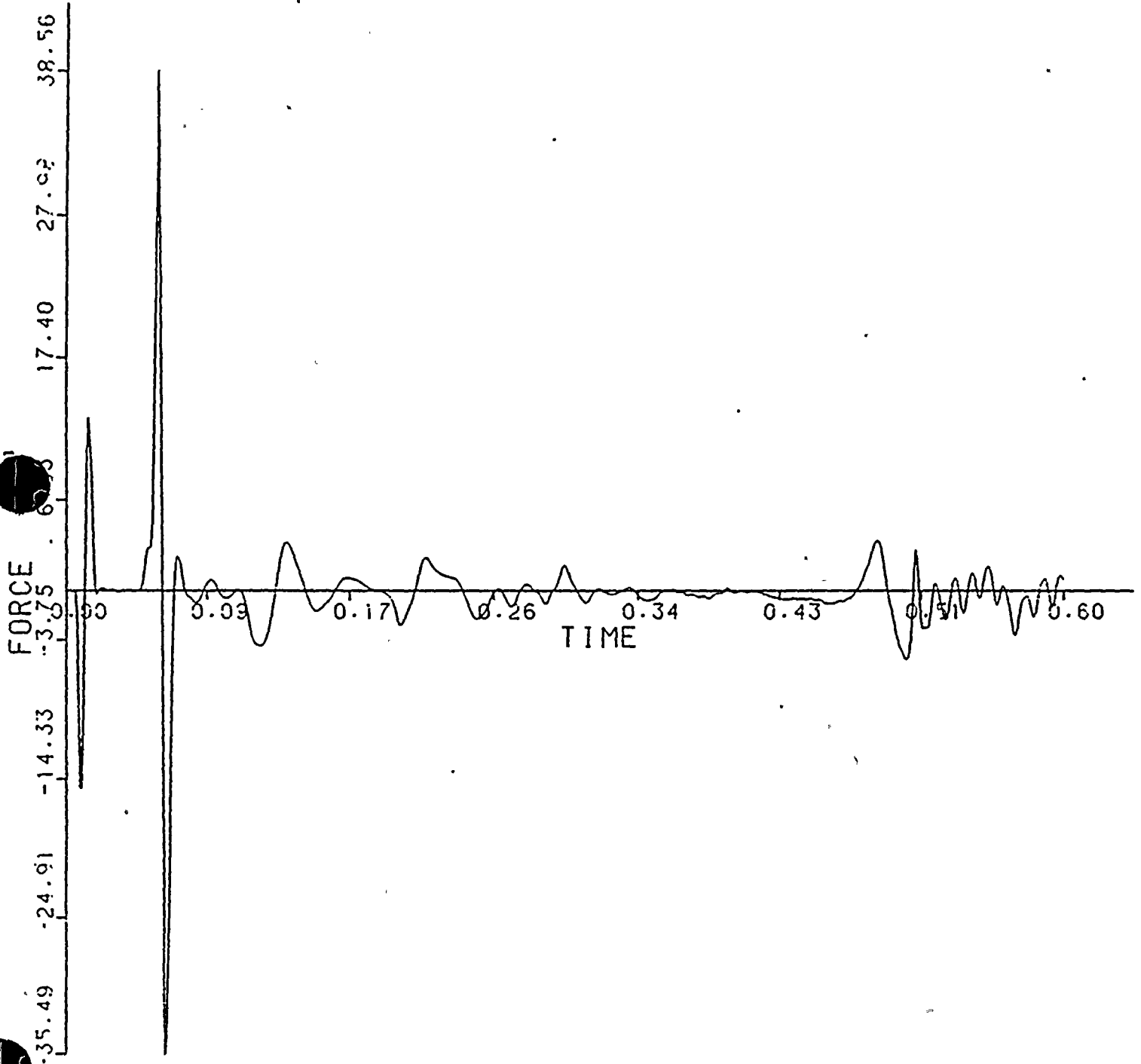
SAP2SAP VERIFICATION 5364

23-MAY-83

YEL-RED SOLID UNIT 1, 0-600 MS

TIME/FORCE TABLE 70. MAGNITUDE AT NODE POINT

8



DONE BY: MR DATE: 5-14-83

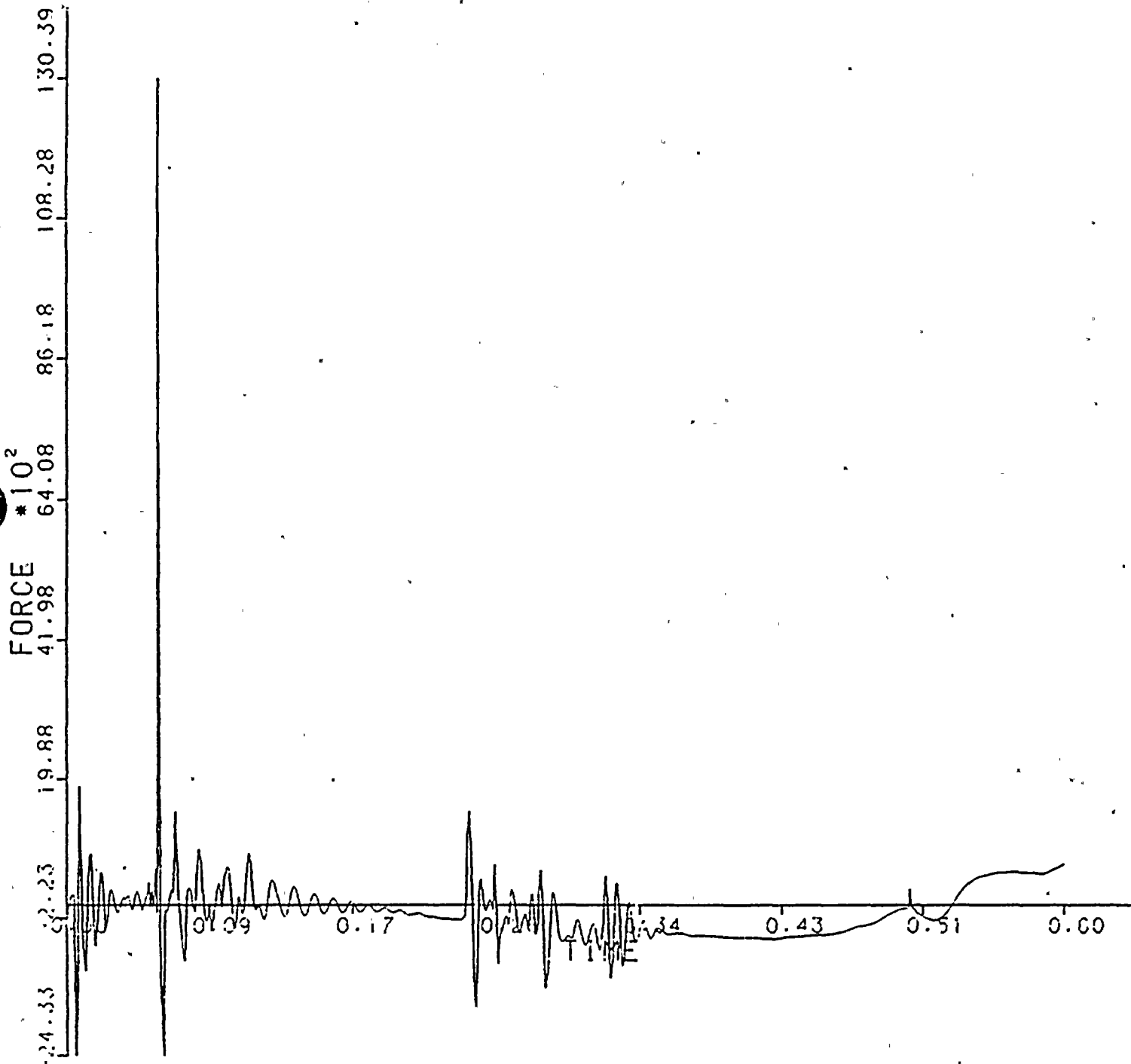
CHKD BY: CA DATE: 5-23-83

SAP2SAP VERIFICATION 5364

23-MAY-83

YEL-RED SOLID UNIT 1, 0-600 MS

TIME/FORCE TABLE 71, MAGNITUDE AT NODE POINT



DONE BY: MR DATE: 5-14-83

CHKD BY: SM DATE: 5-23-83



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TR-5364-1
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4.8.3 Quarter Model - Cold Loop Seal/Steam Case

BY CMH DATE 3-16-83
 CHKD. BY KTG DATE 5-24-83

**1/4 MODEL LENGTHS ;
 NODES (SRV) ANALYSIS**

SHEET NO. 1 OF 1
 PROJ. NO. 5364

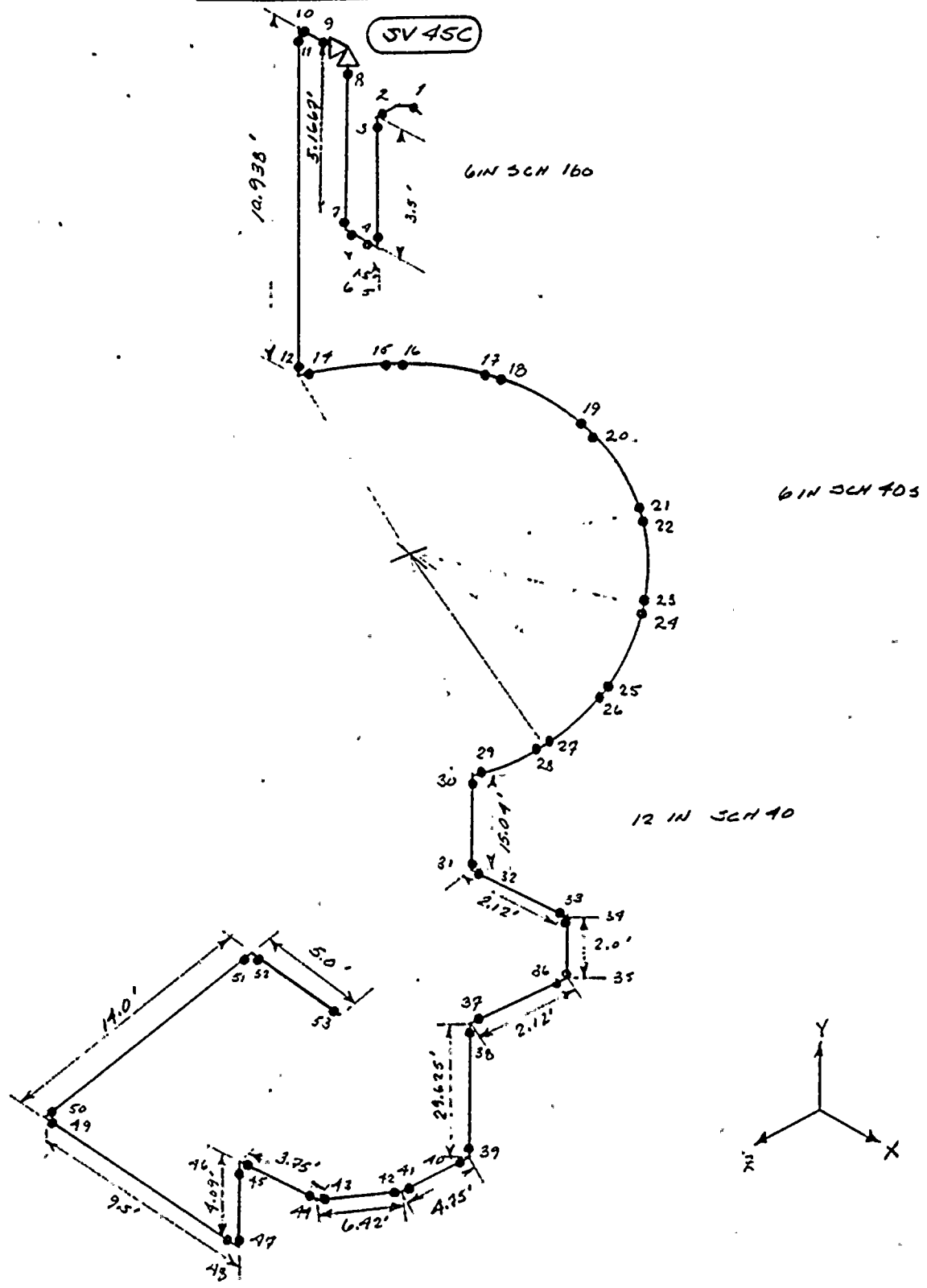


FIGURE 4.8.2-1

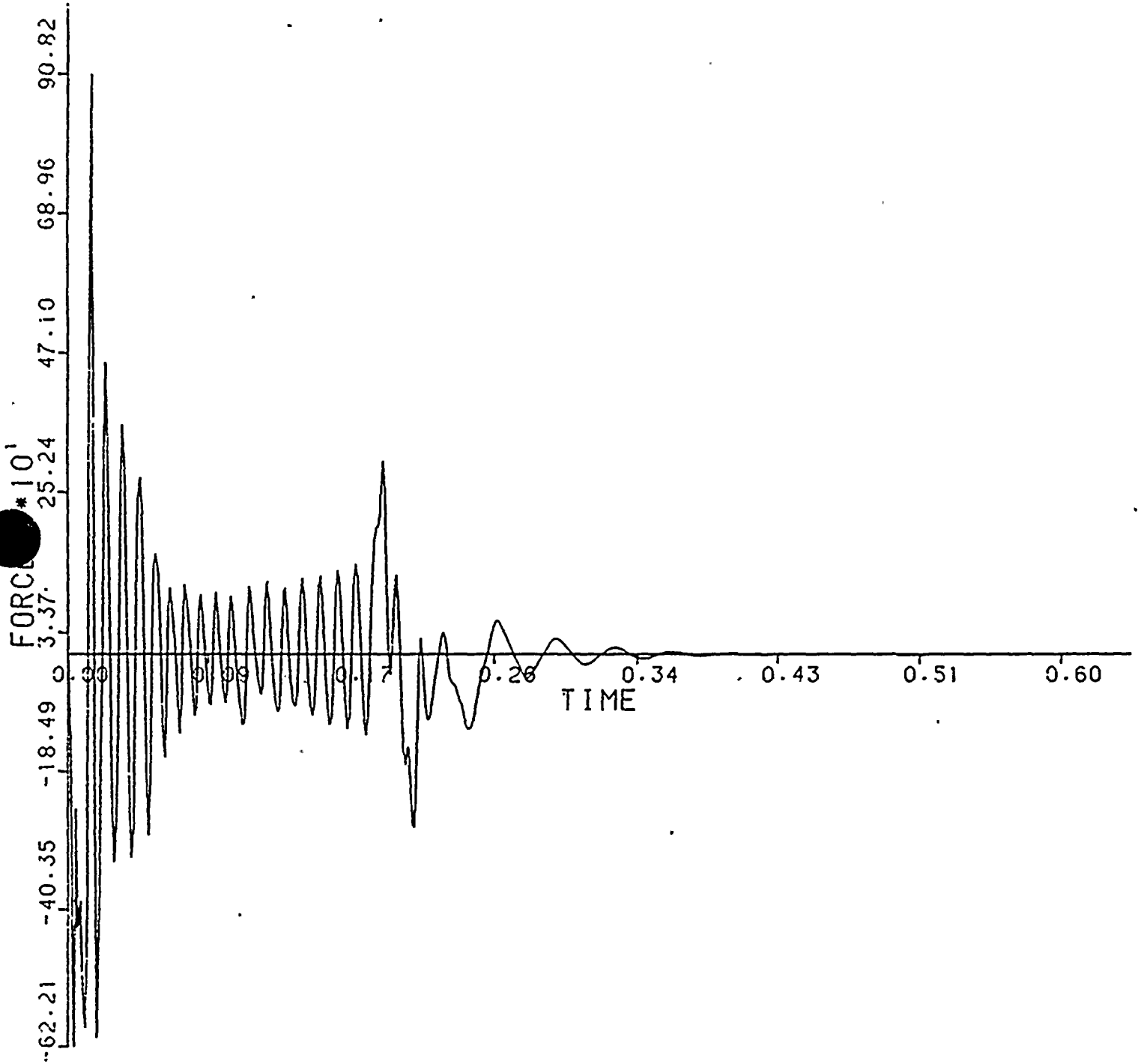
SAP2SAP VERIFICATION 5364

24-MAY-83

QUARTER MODEL UNIT 2 LOOPSEAL

TIME/FORCE TABLE 1. MAGNITUDE AT NODE POINT

118



DONE BY: LM DATE: 5-26-83

CHKD BY: KJ DATE: 5-27-83

Technical Report
TR-5364-1
Revision 0

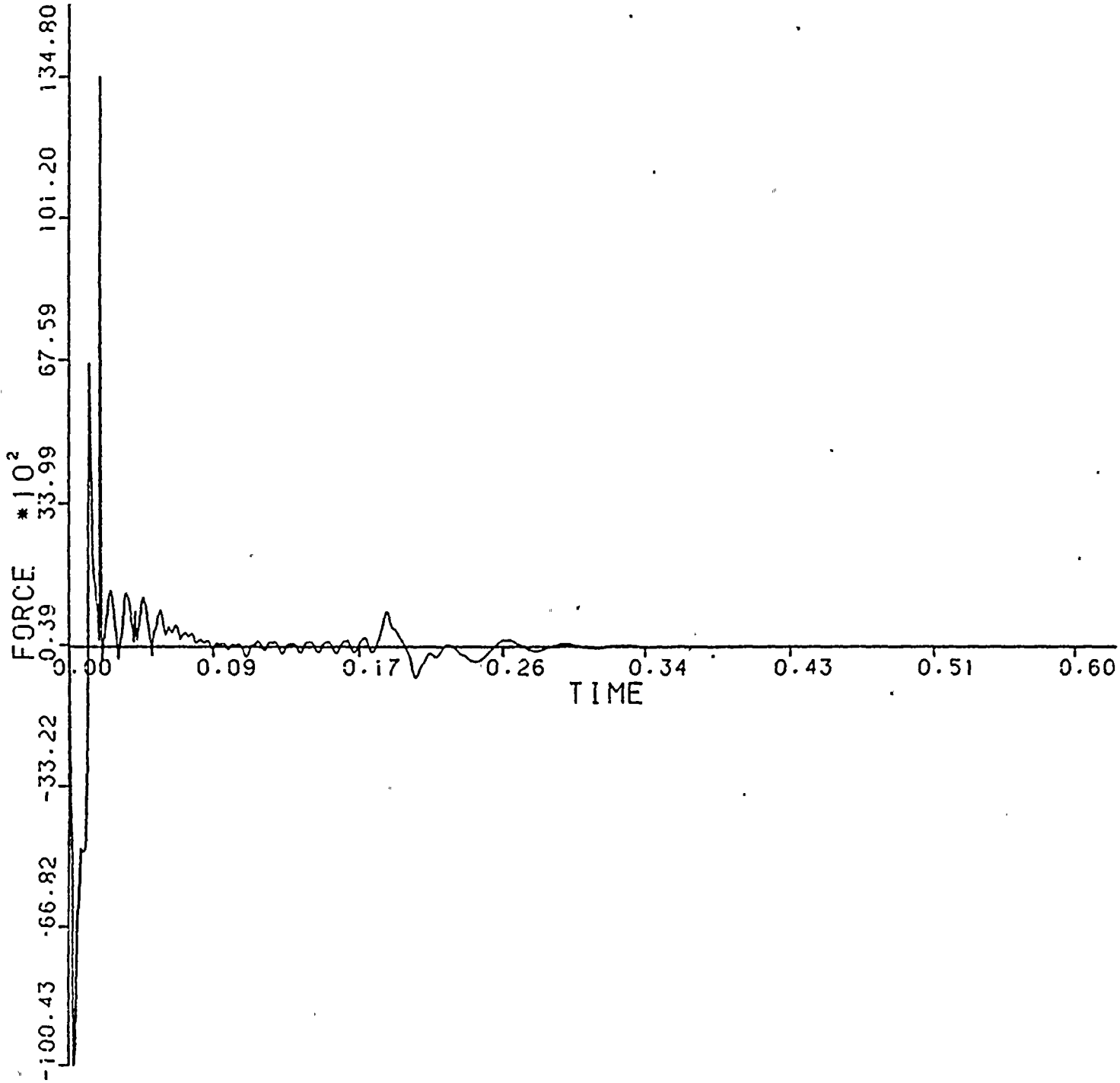
CAPACITANCE VERIFICATION 5364

24 MAY 83

QUARTER MODEL UNIT 2.1000E4

THE FORCE TABLE 2. MAGNITUDE AT NODE POINT 114

114



DONE BY DL DATE: 5-26-83

CHKD BY: KT DATE: 5-27-83

Technical Report

TR-5364-1

Revision 0

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TELEDYNE
ENGINEERING SERVICES

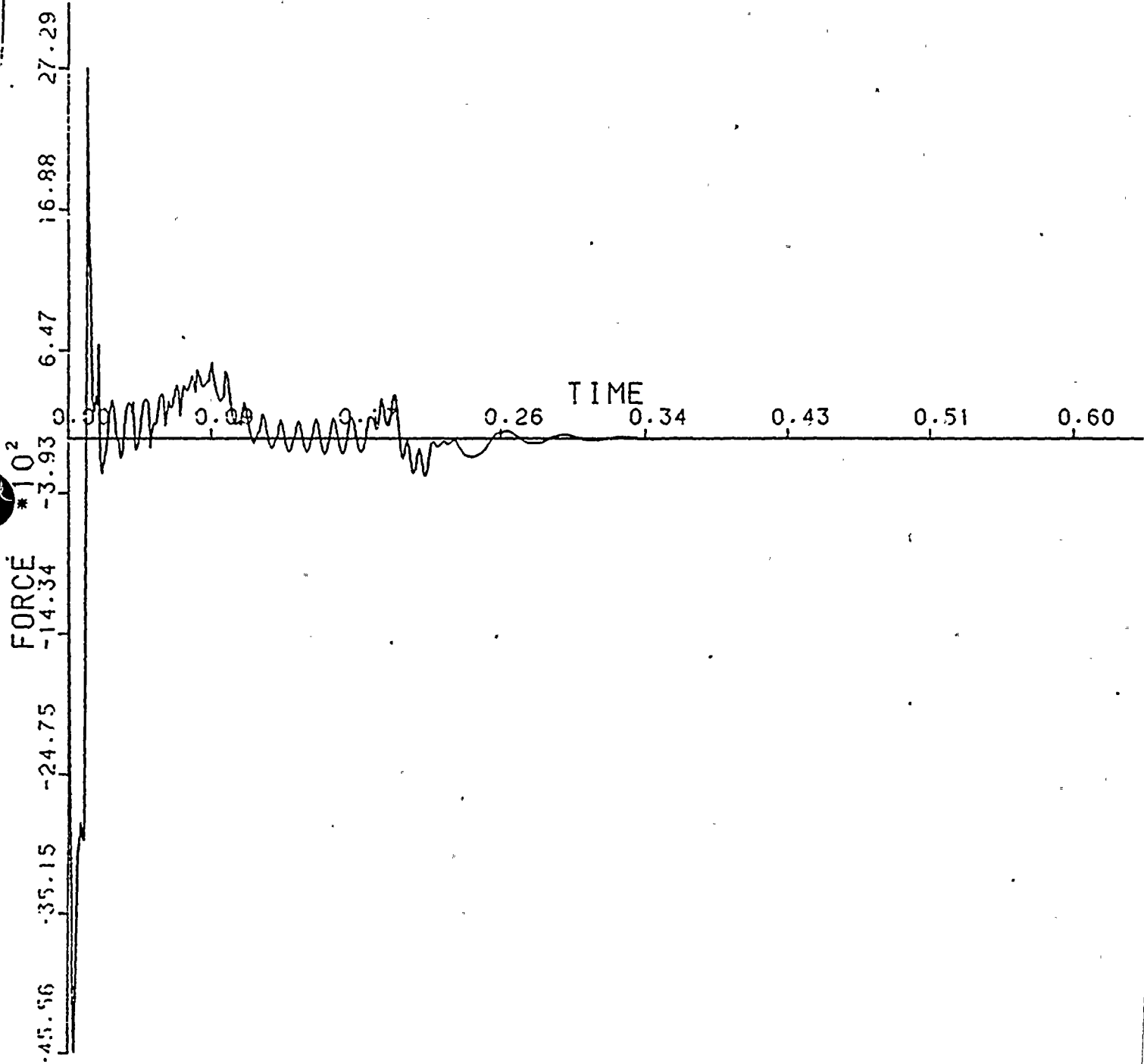
24-MAY-83

SAP2SAP VERIFICATION 5364

QUARTER MODEL UNIT 2 LOOPSEAL

TIME/FORCE TABLE 3. MAGNITUDE AT NODE POINT

111



DONE BY: Bill DATE: 5-26-83

CHKD BY: ET DATE: 5-27-83

Technical Report
TR-5364-1
Revision 0



4-397

TELEDYNE-
ENGINEERING SERVICES

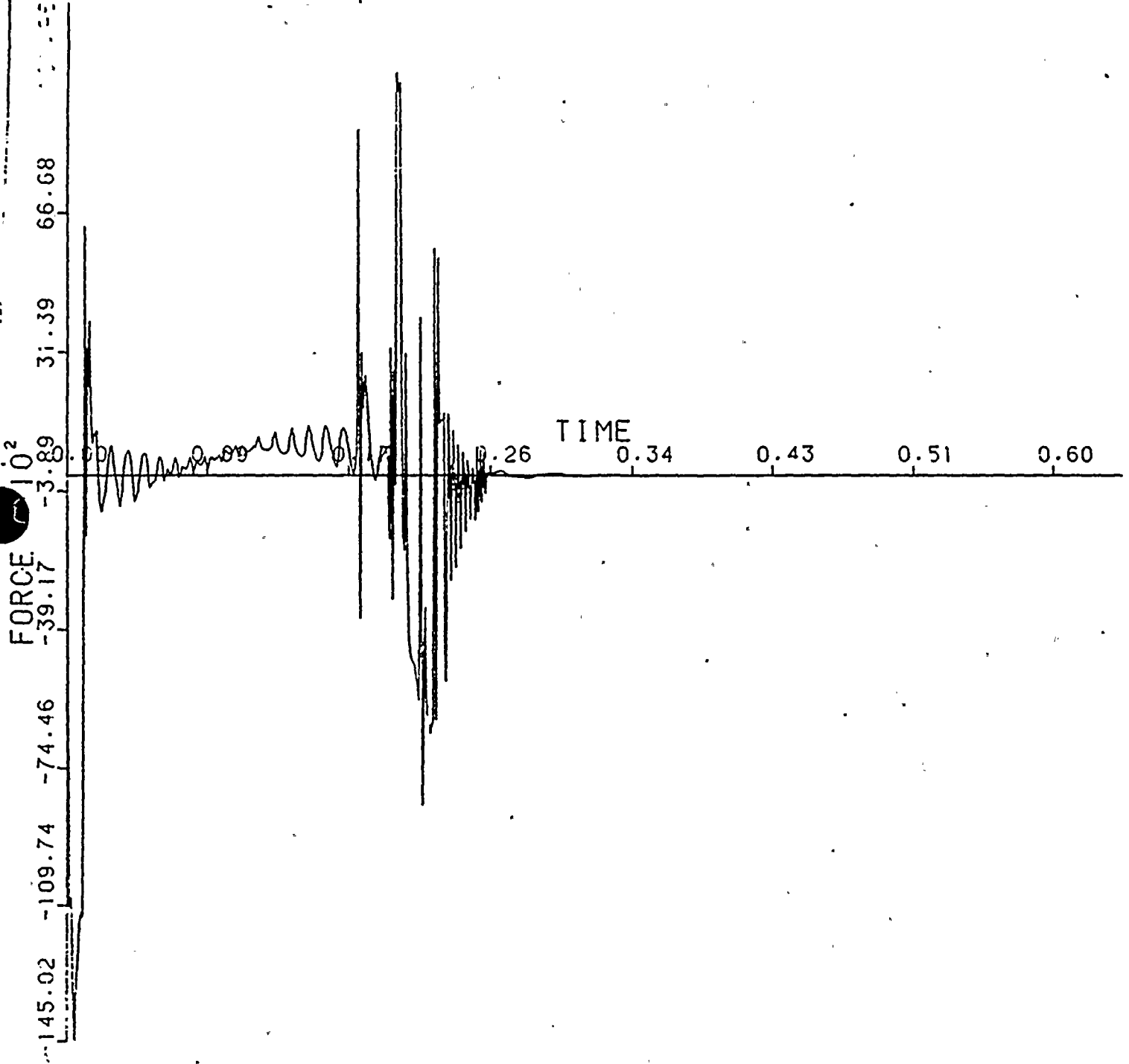
SAP2SAP VERIFICATION 5364

24-MAY-83

QUARTER MODEL UNIT 2 LOOPSEAL

TIME/FORCE TABLE 4. MAGNITUDE AT NODE POINT

107



DONE BY DL DATE: 5-25-83

CHKD BY: 174 DATE: 5-27-83

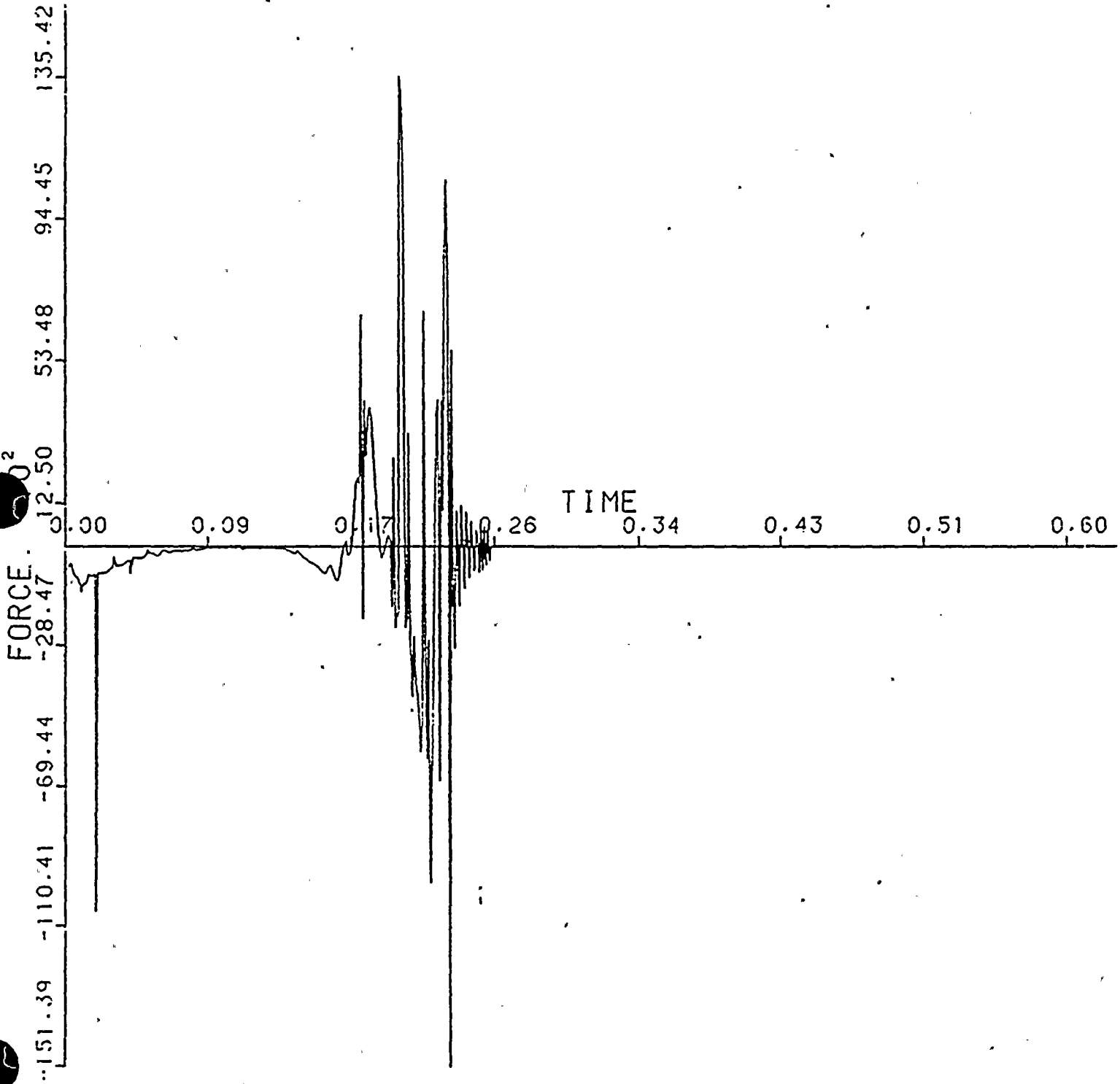
Technical Report
TR-5364-1
Revision 0

SAP2SAP VERIFICATION 5364

24-MAY-83

QUARTER MODEL UNIT 2 LOOPSEAL

TIME/FORCE TABLE 5. MAGNITUDE AT NODE POINT



DONE BY DM DATE: 5-26-83

CHKD BY: KJG DATE: 5-27-83

Technical Report

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Revision 0

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TELEDYNE
ENGINEERING SERVICES

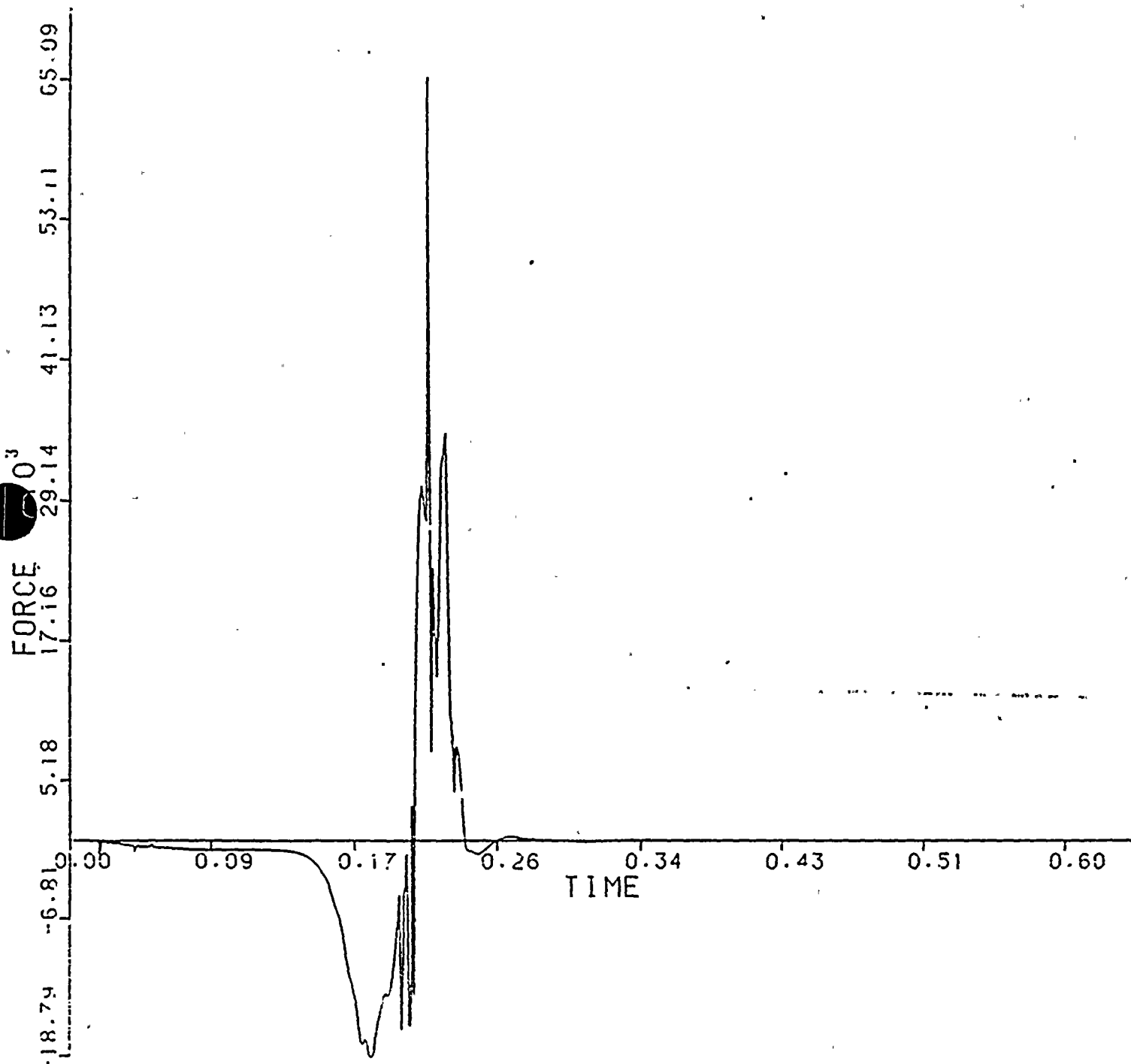
SAP2SAP VERIFICATION 5364

24-MAY-83

QUARTER MODEL UNIT 2 LOOPSEAL

TIME/FORCE TABLE · G, MAGNITUDE AT NODE POINT

90



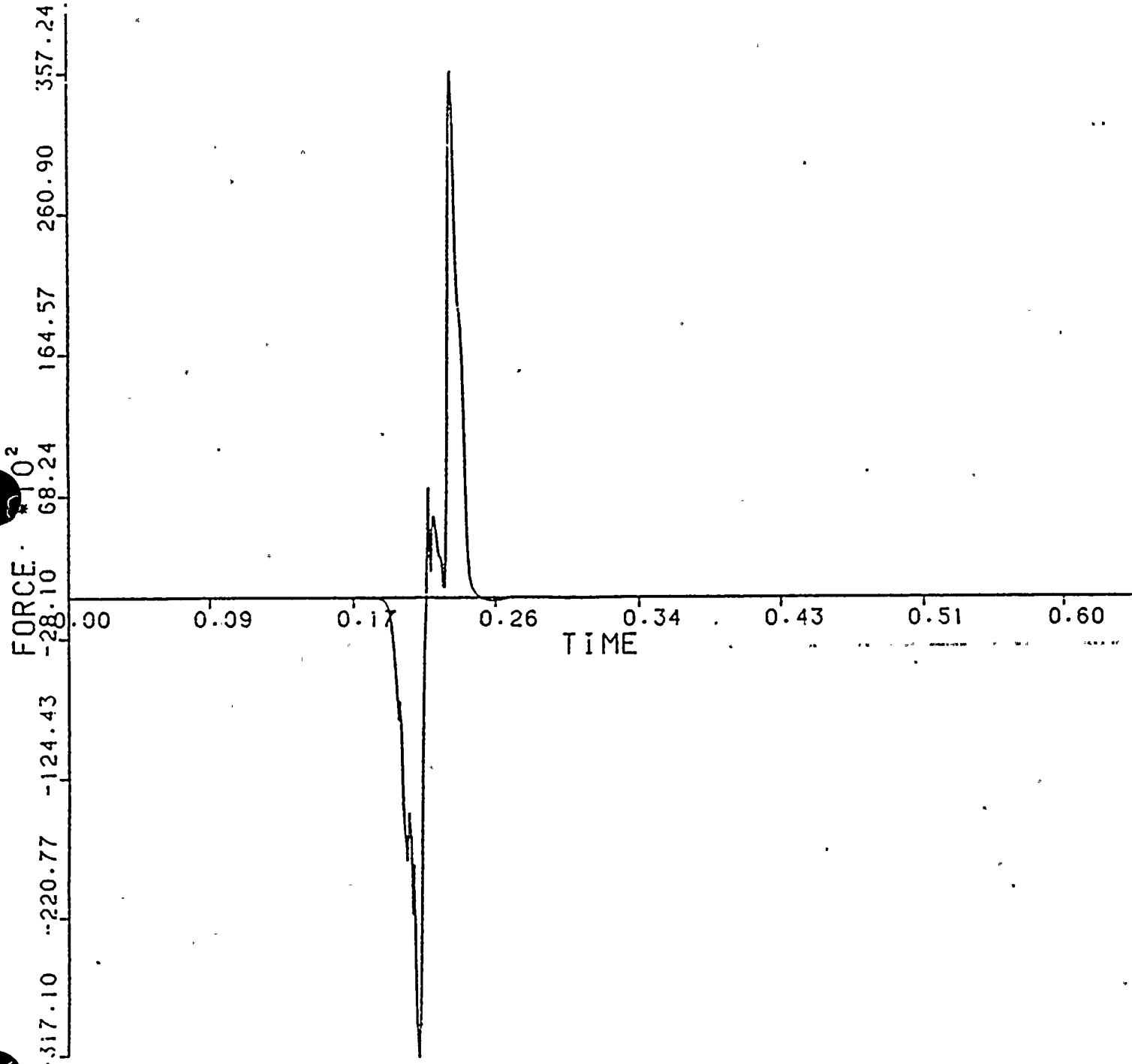
DONE BY: DML DATE: 5-25-83

CHKD BY: DT DATE: 5-27-83

Technical Report
TR-5364-1
Revision 0

SAP2SAP VERIFICATION 5364
QUARTER MODEL UNIT 2 LOOPSEAL

TIME/FORCE TABLE 7. MAGNITUDE AT NODE POINT



DONE BY: SM DATE: 5-26-83
CHKD BY: KJG DATE: 5-27-83

Technical Report:
TR-5364-1
Revision 0

4-401

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ENGINEERING SERVICES

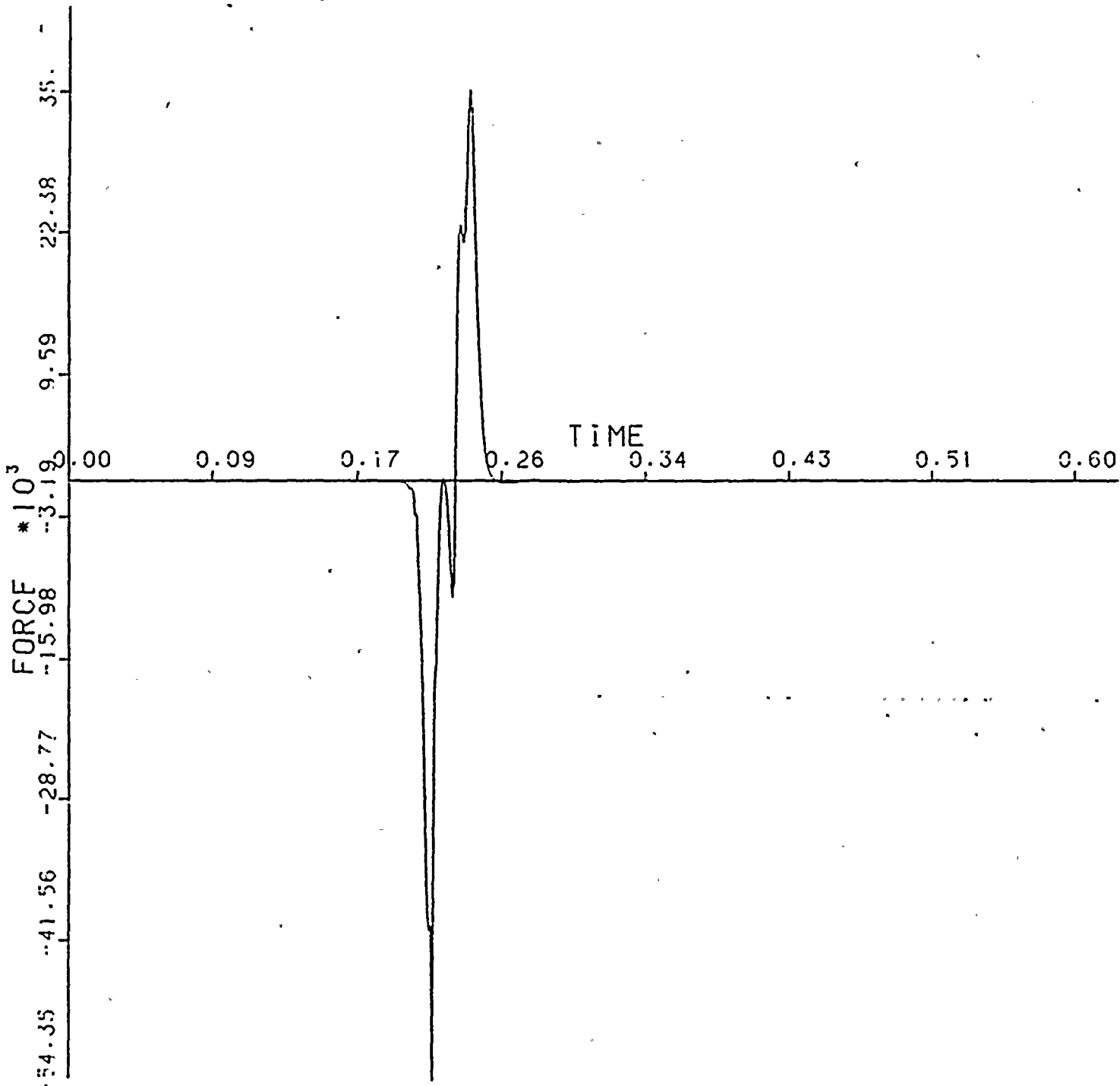
SAP2SAP VERIFICATION 5364

24-MAY-83

QUARTER MODEL UNIT 2 LOOPSEAL

TIME/FORCE TABLE S. MAGNITUDE AT NODE POINT

86

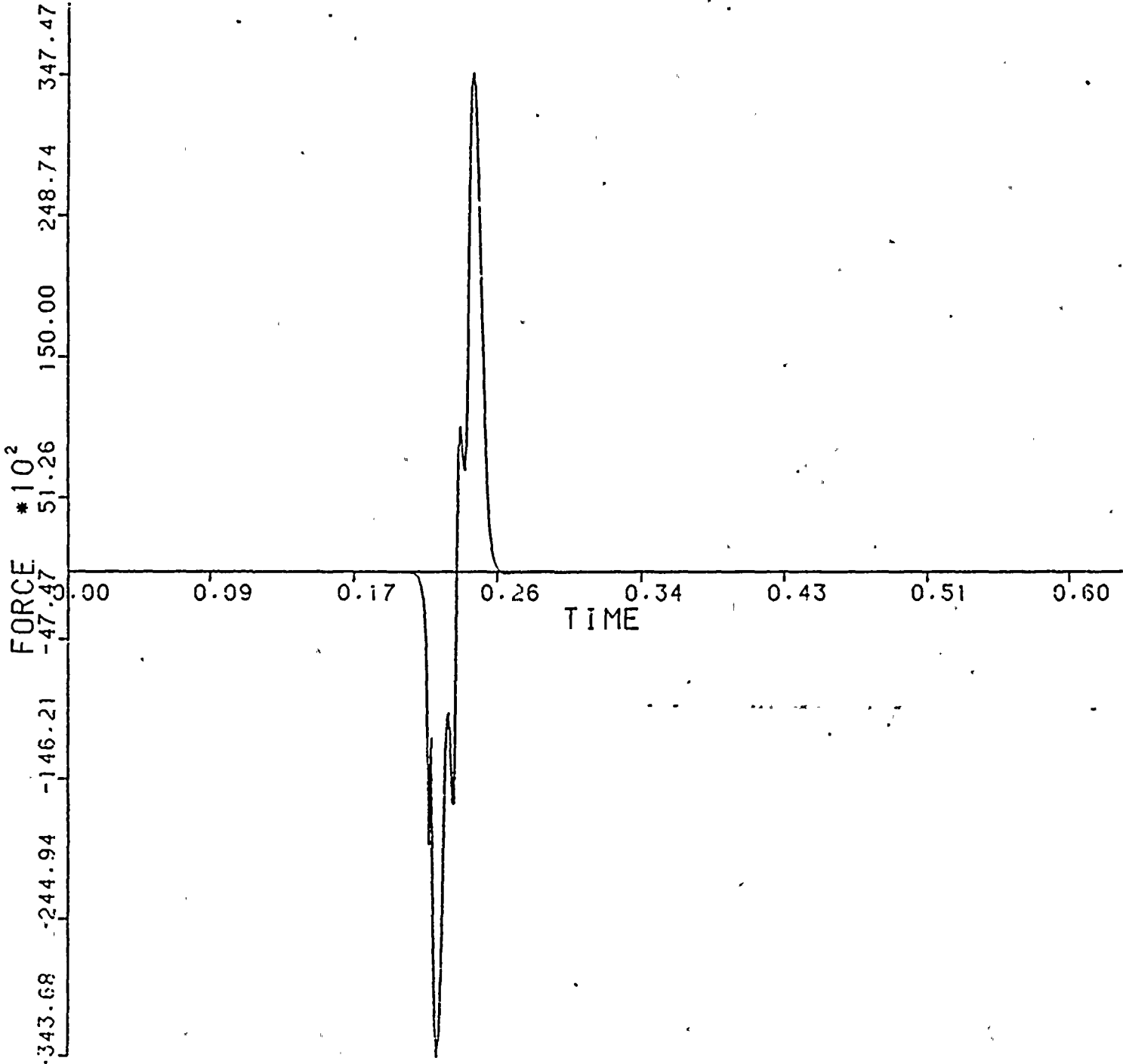


DONE BY: DW DATE: 5-26-83

CHKD BY: KTG DATE: 5-27-83

Technical Report
TR-5364-1
Revision 0





DONE BY DL DATE: 5-26-83

CHKD BY: ST DATE: 5-27-83

Technical Report
TR-5364-1
Revision 0

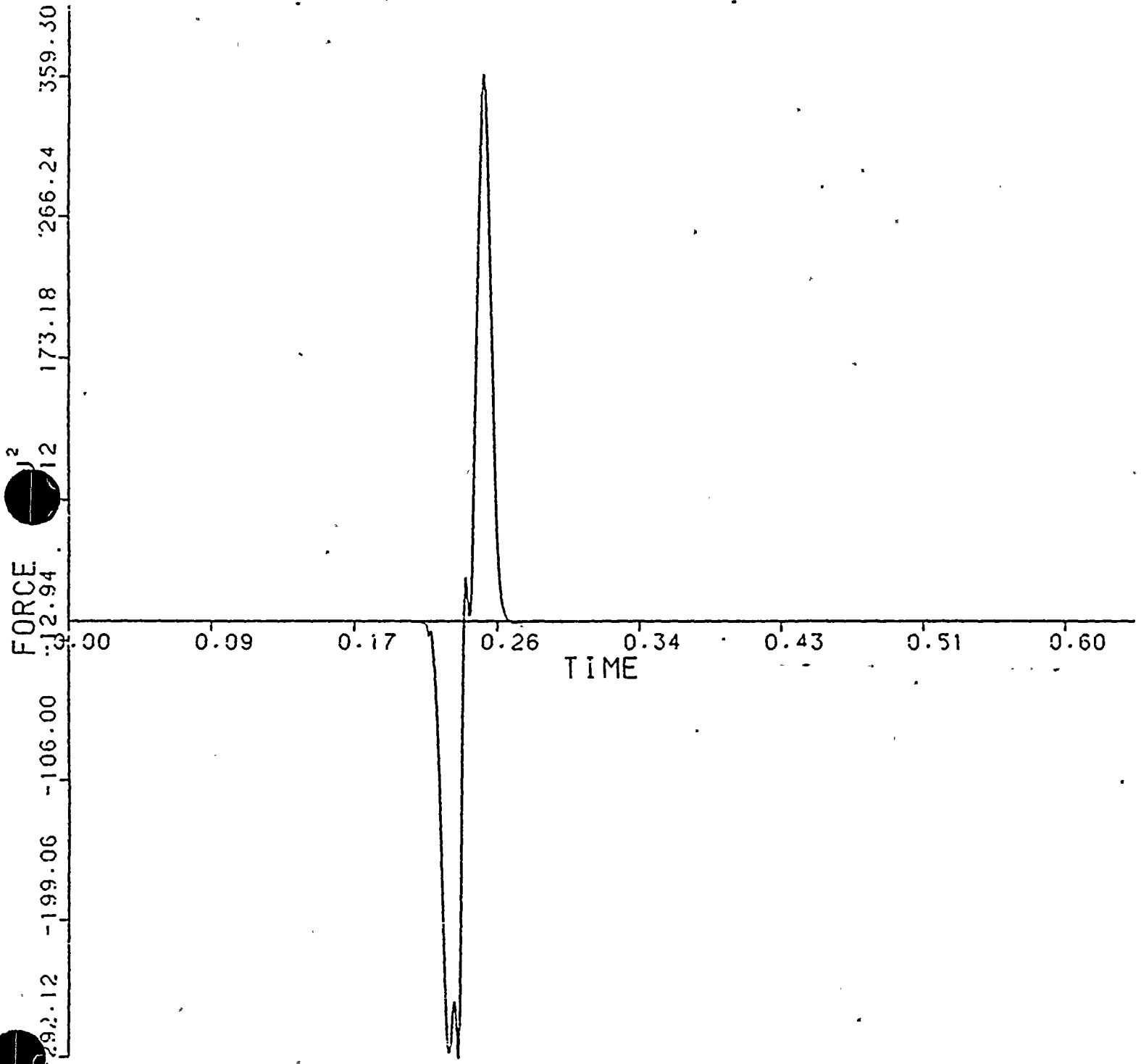


24-MAY-83

SAP2SAP VERIFICATION 5364

QUARTER MODEL UNIT 2 LOOPSEAL

TIME/FORCE TABLE 10, MAGNITUDE AT NODE POINT



DONE BY: DL DATE: 5-26-83 Technical Report
 CHKD BY: LT DATE: 5-27-83 TR-5364-1
 Revision 0

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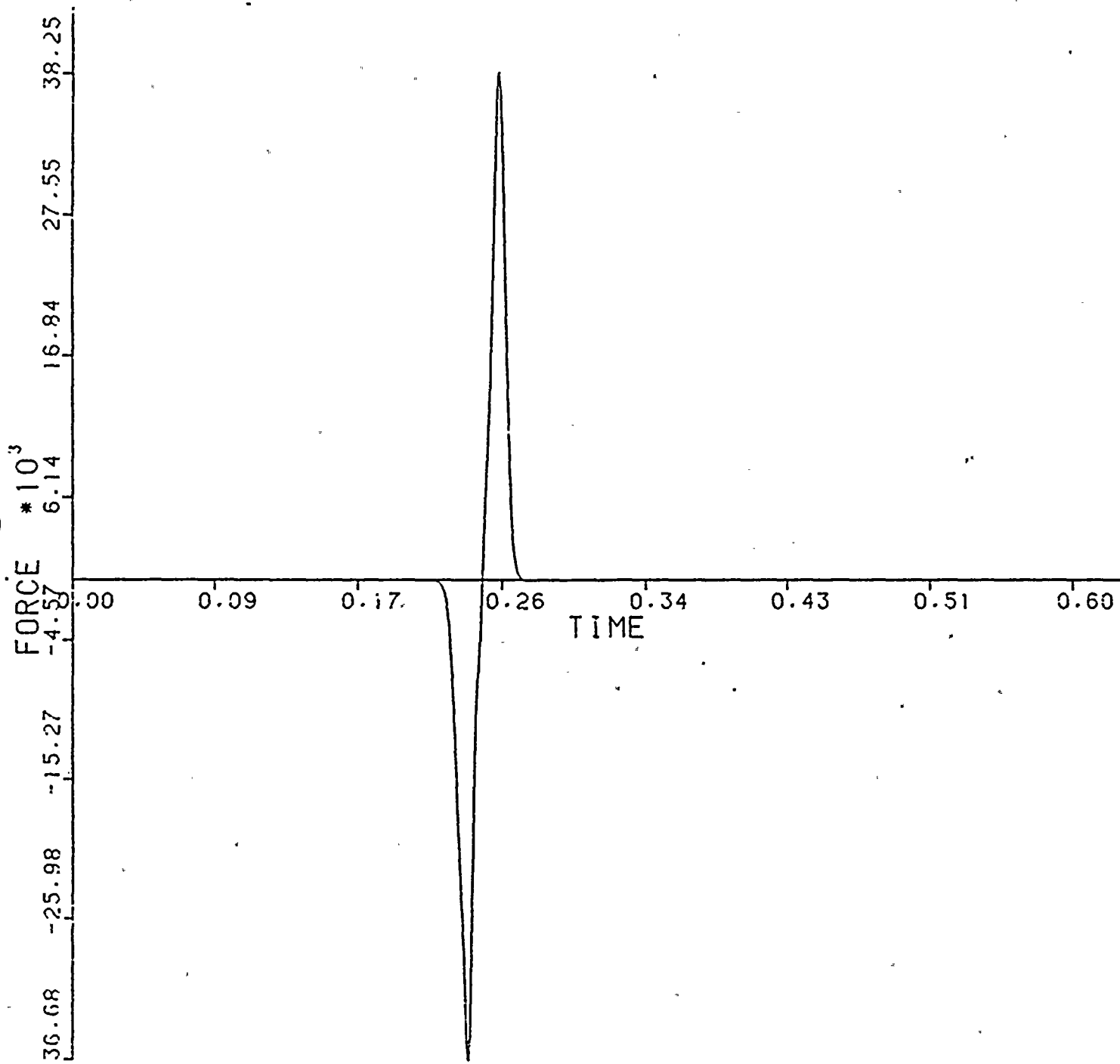
SAP2SAP VERIFICATION 5364

24-MAY-83

QUARTER MODEL UNIT 2 LOOPSEAL

TIME/FORCE TABLE 11. MAGNITUDE AT NODE POINT

80



DONE BY: DM DATE: 5-26-83

CHKD BY: HT DATE: 5-27-83

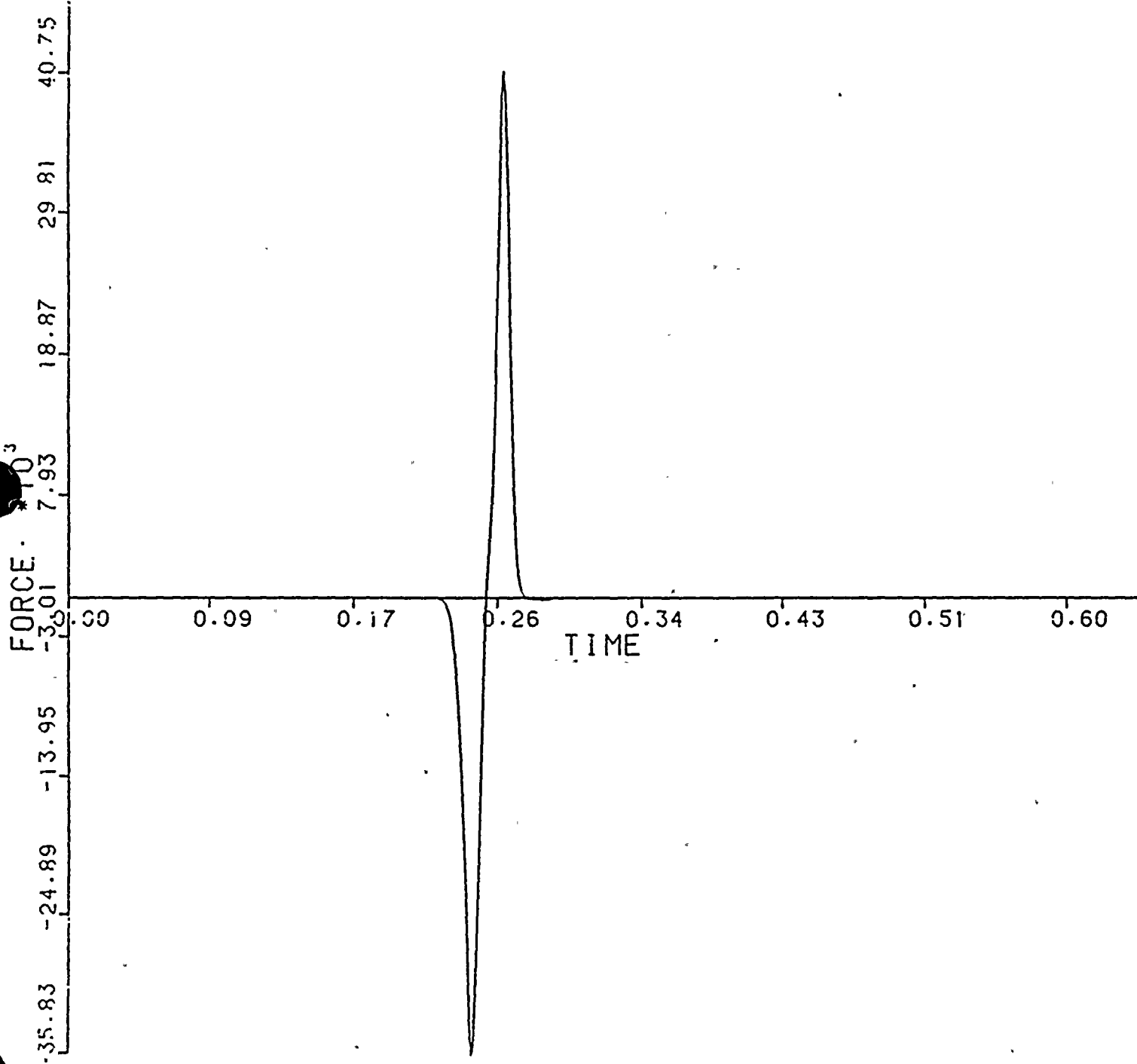
Technical Report
TR-5364-1
Revision 0

SAP2SAP VERIFICATION 5364

QUARTER MODEL UNIT 2 LOOPSEAL

TIME/FORCE TABLE 12, MAGNITUDE AT NODE POINT

78



DONE BY DHL DATE: 5-26-83

CHKD BY: K74 DATE: 5-27-83

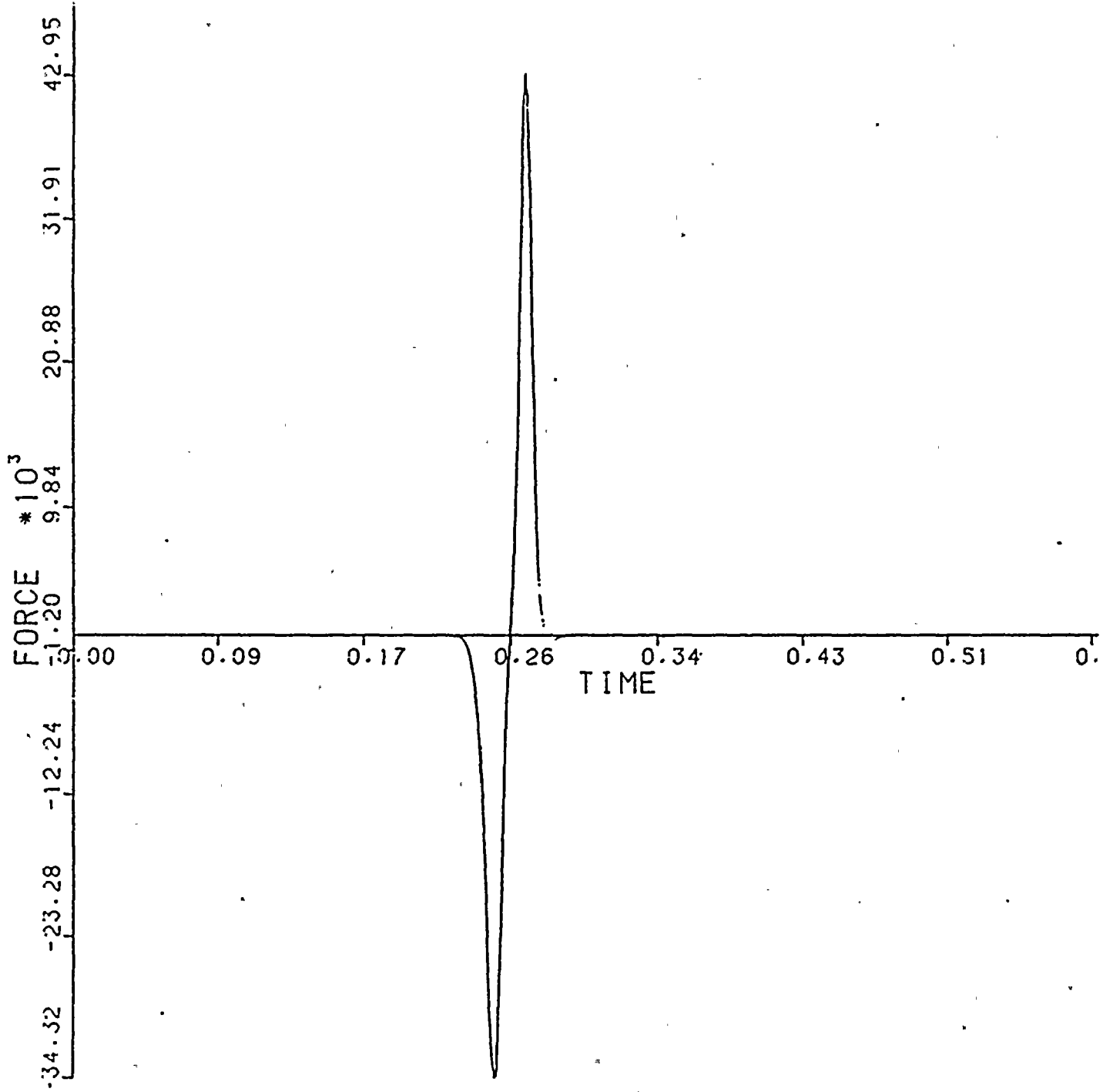
Technical Report
TR-5364-1
Revision 0

SAP2SAP VERIFICATION 5364

24-MAY-83

QUARTER MODEL UNIT 2 LOOPSEAL

TIME/FORCE TABLE 13. MAGNITUDE AT NODE POINT



DONE BY Qu DATE: 5-26-83

CHKD BY: K74 DATE: 5-27-83

Technical Report

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Revision 0





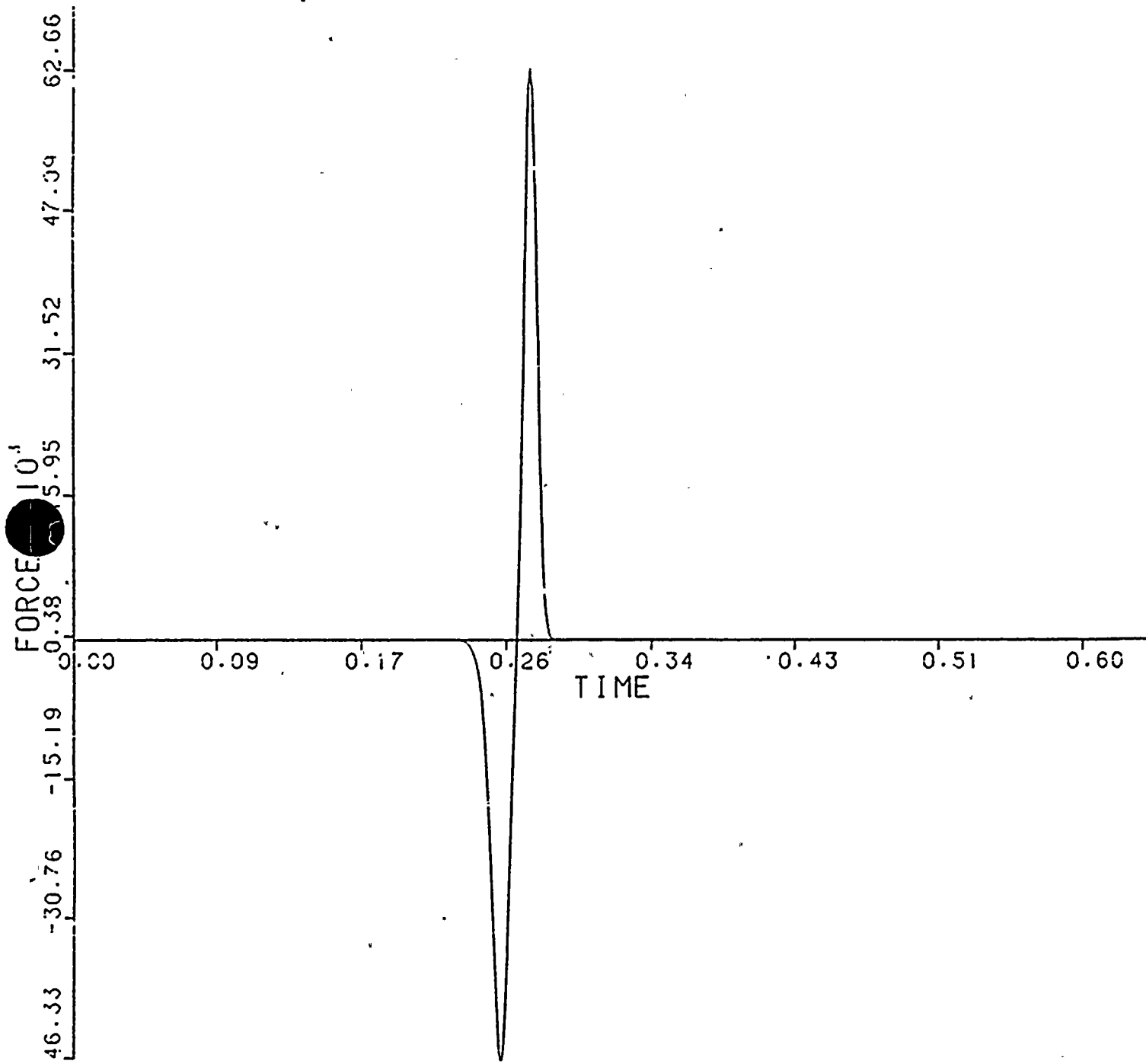
SAP2SAP VERIFICATION 5364

24-MAY-83

QUARTER MODEL UNIT 2 LOOPSEAL

TIME/FORCE TABLE 14, MAGNITUDE AT NODE POINT

74



DONE BY DM DATE: 5-26-83

CHKD BY: K76 DATE: 5-27-83

Technical Report
TR-5364-1
Revision 0

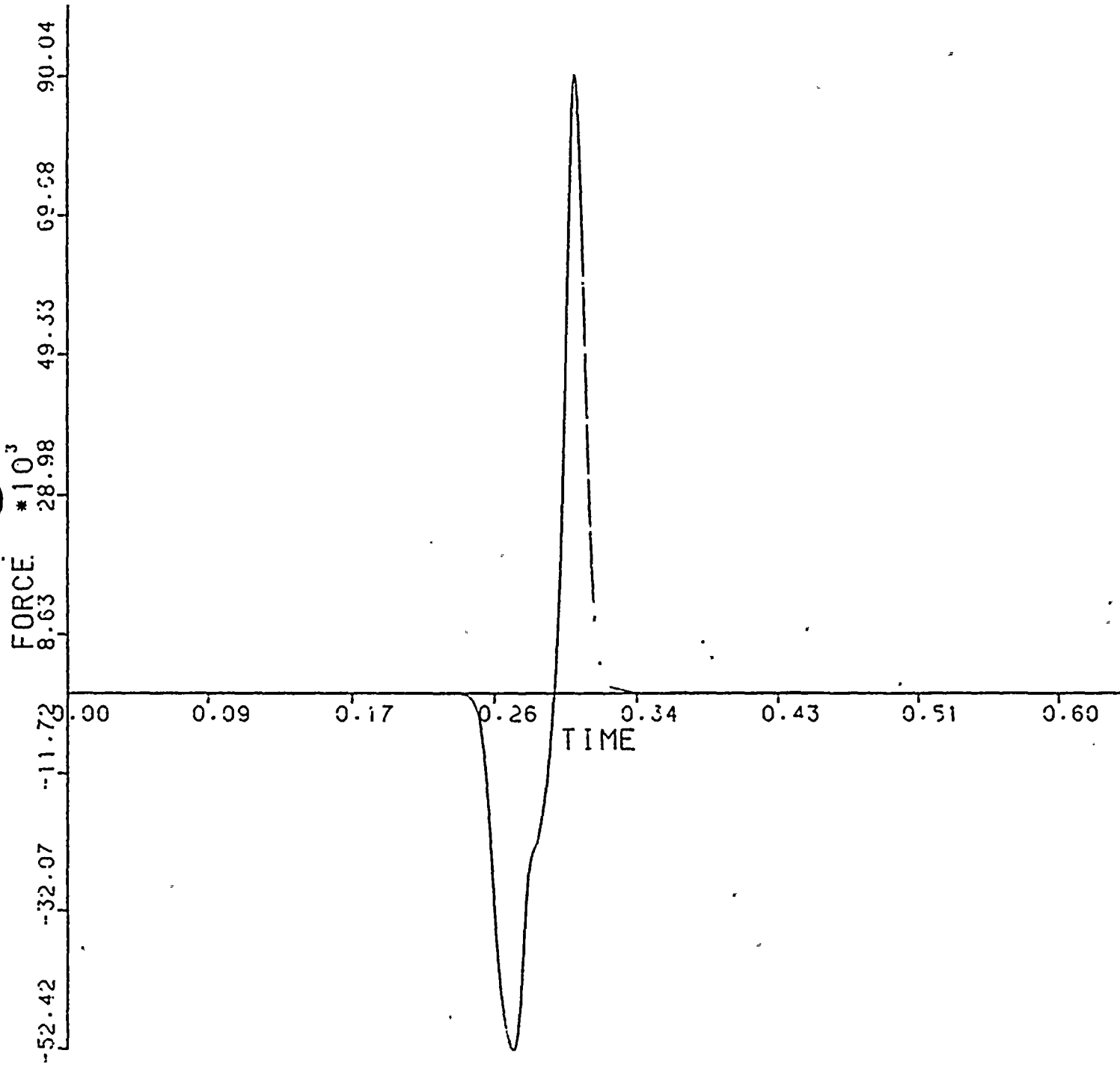
SAP2SAP VERIFICATION 5364

24-MAY-83

QUARTER MODEL UNIT 2 LOOPSEAL

TIME/FORCE TABLE 15, MAGNITUDE AT NODE POINT

70



DONE BY DJM DATE: 5-26-83

CHKD BY: KTG DATE: 5-27-83

Technical Report
TR-5364-1
Revision 0

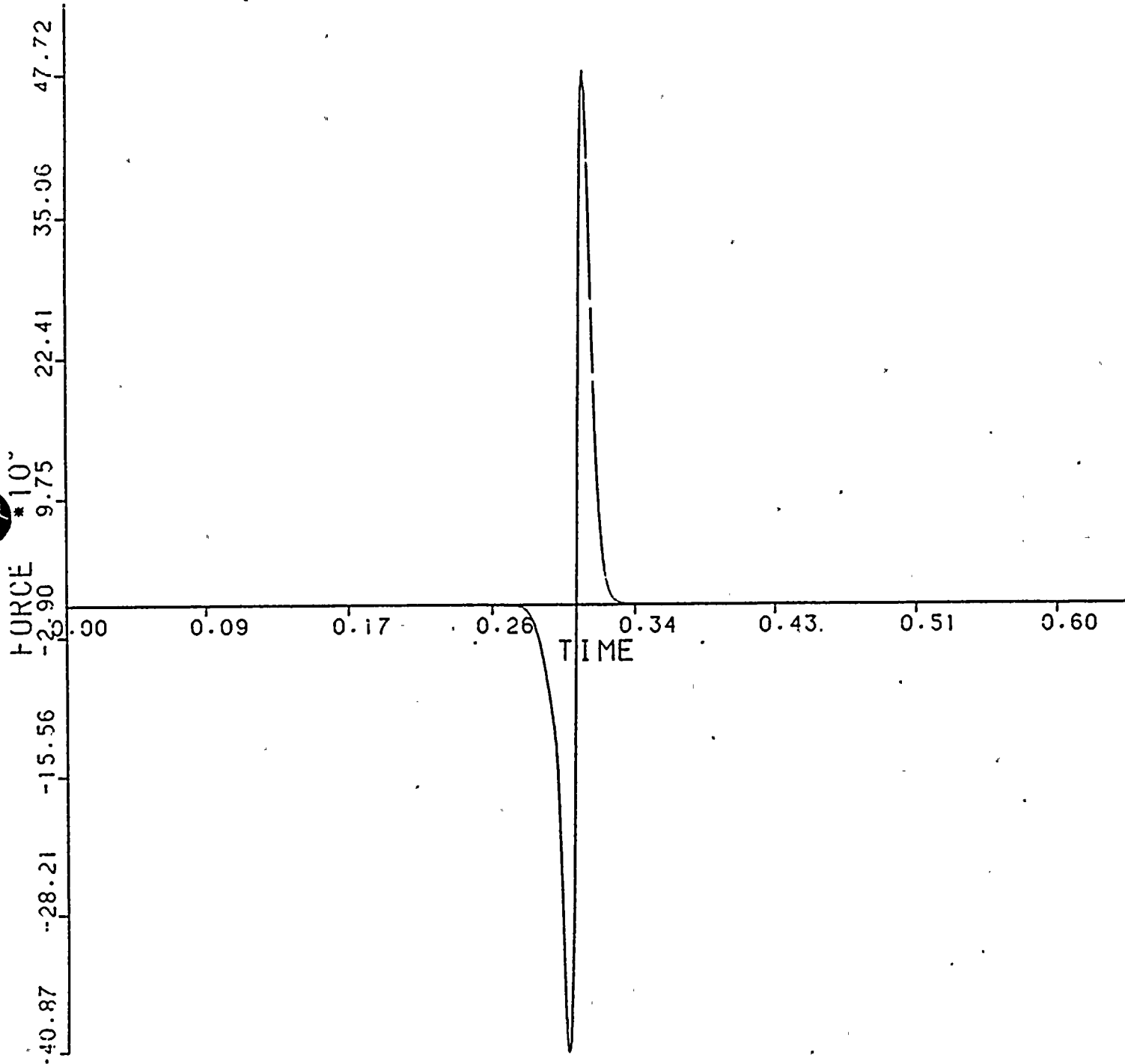


24-MAY-83

SAP2SAP VERIFICATION 5364

QUARTER MODEL UNIT 2 LOOPSEAL

TIME/FORCE TABLE 16. MAGNITUDE AT NODE POINT



DONE BY: CHL DATE: 5-26-83

CHKD BY: KW DATE: 5-27-83

Technical Report
TR-5364-1
Revision 0

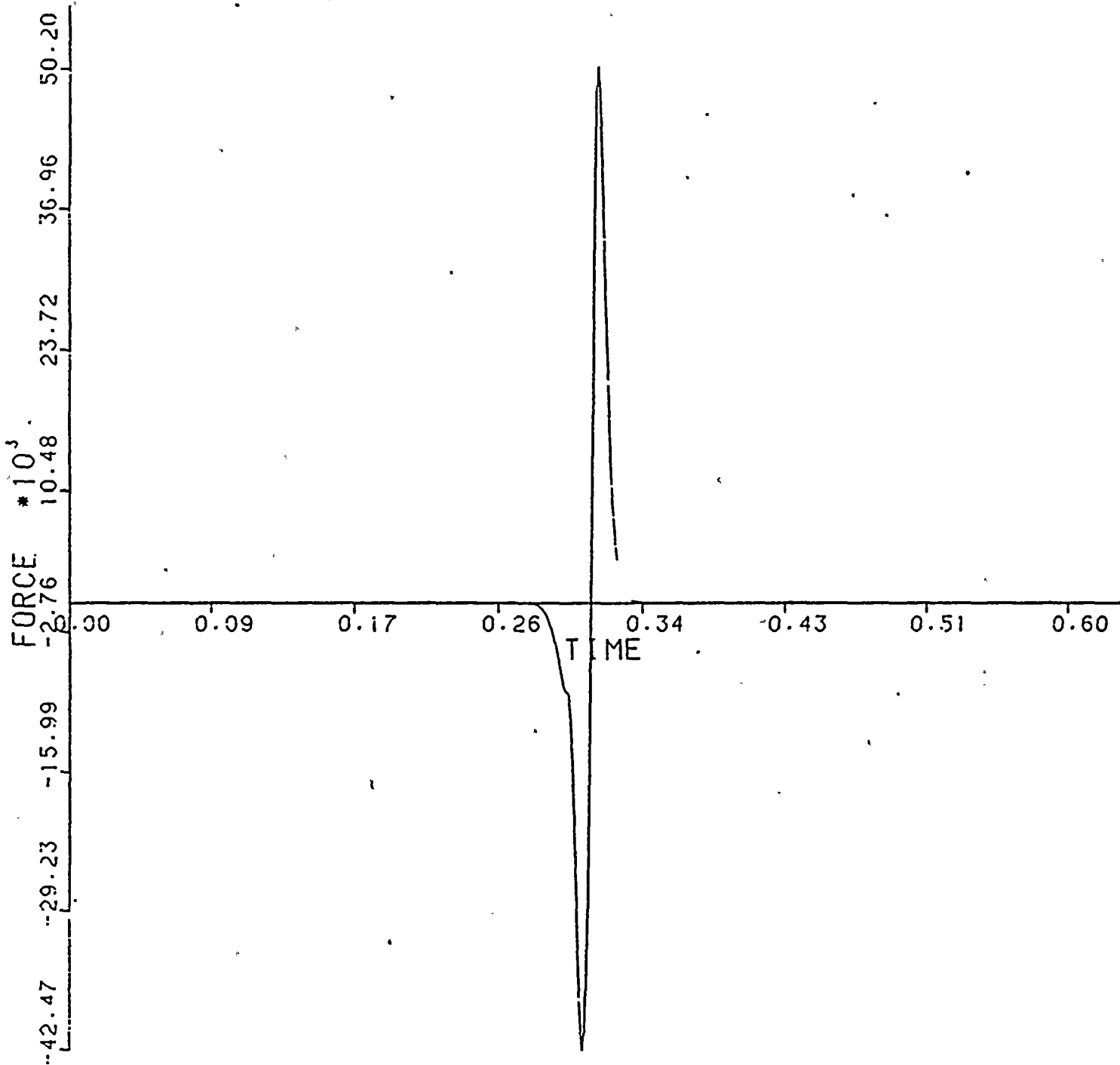
24-MAY-83

SAP2SAP VERIFICATION 5364

QUARTER MODEL UNIT 2 LOOPSEAL

TIME/FORCE TABLE 17. MAGNITUDE AT NODE POINT

60



DONE BY: SM DATE: 5-26-83

CHKD BY: KTG DATE: 5-27-83

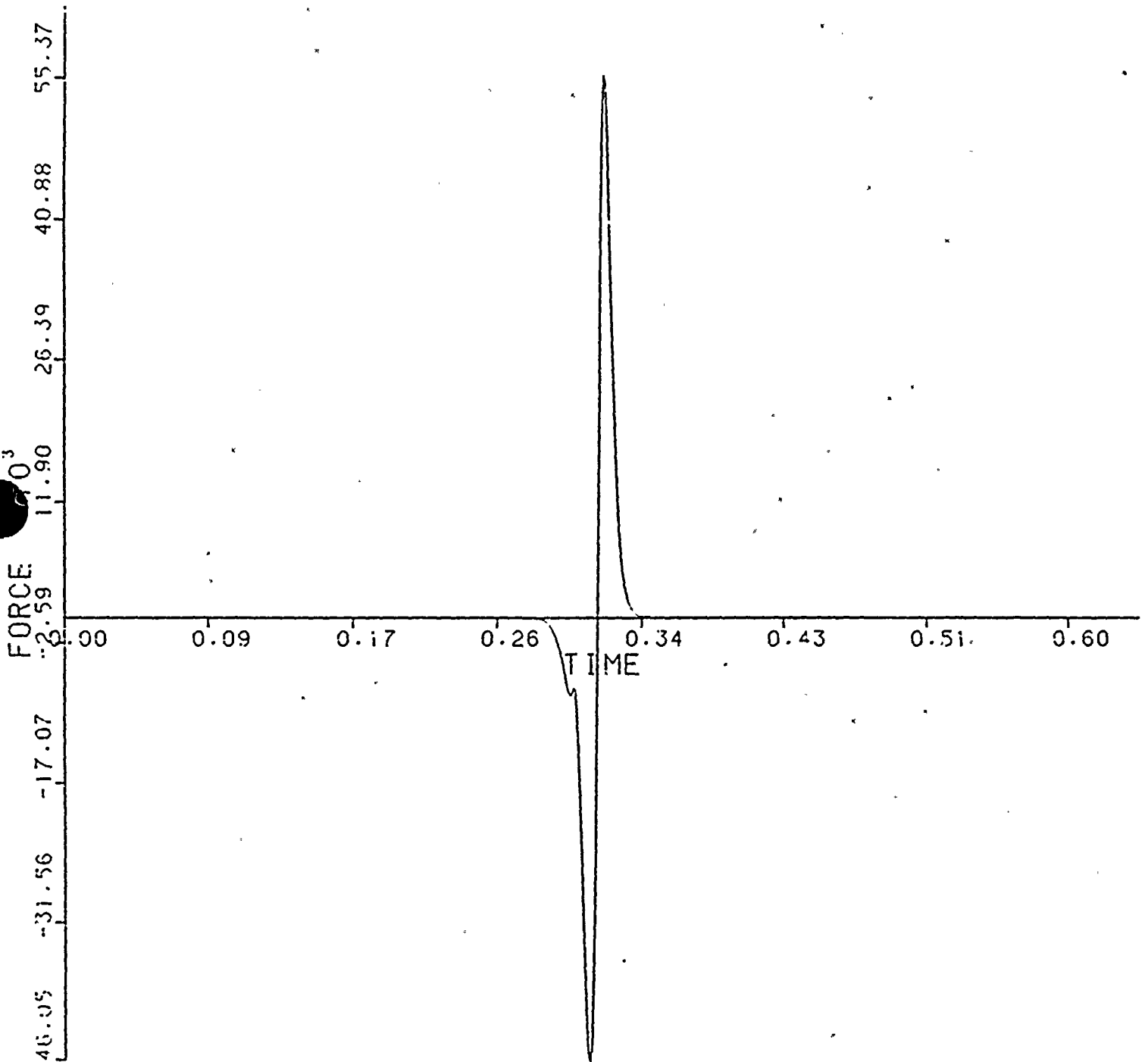
Technical Report
TR-5364-1
Revision 0



SAP2SAP VERIFICATION 5364 24-MAY-83

QUARTER MODEL UNIT 2 LOOPSEAL

TIME/FORCE TABLE 18. MAGNITUDE AT NODE POINT



DONE BY: SM DATE: 5-26-83
CHKD BY: KTG DATE: 5-27-83

Technical Report
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Revision 0

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TELEDYNE
ENGINEERING SERVICES

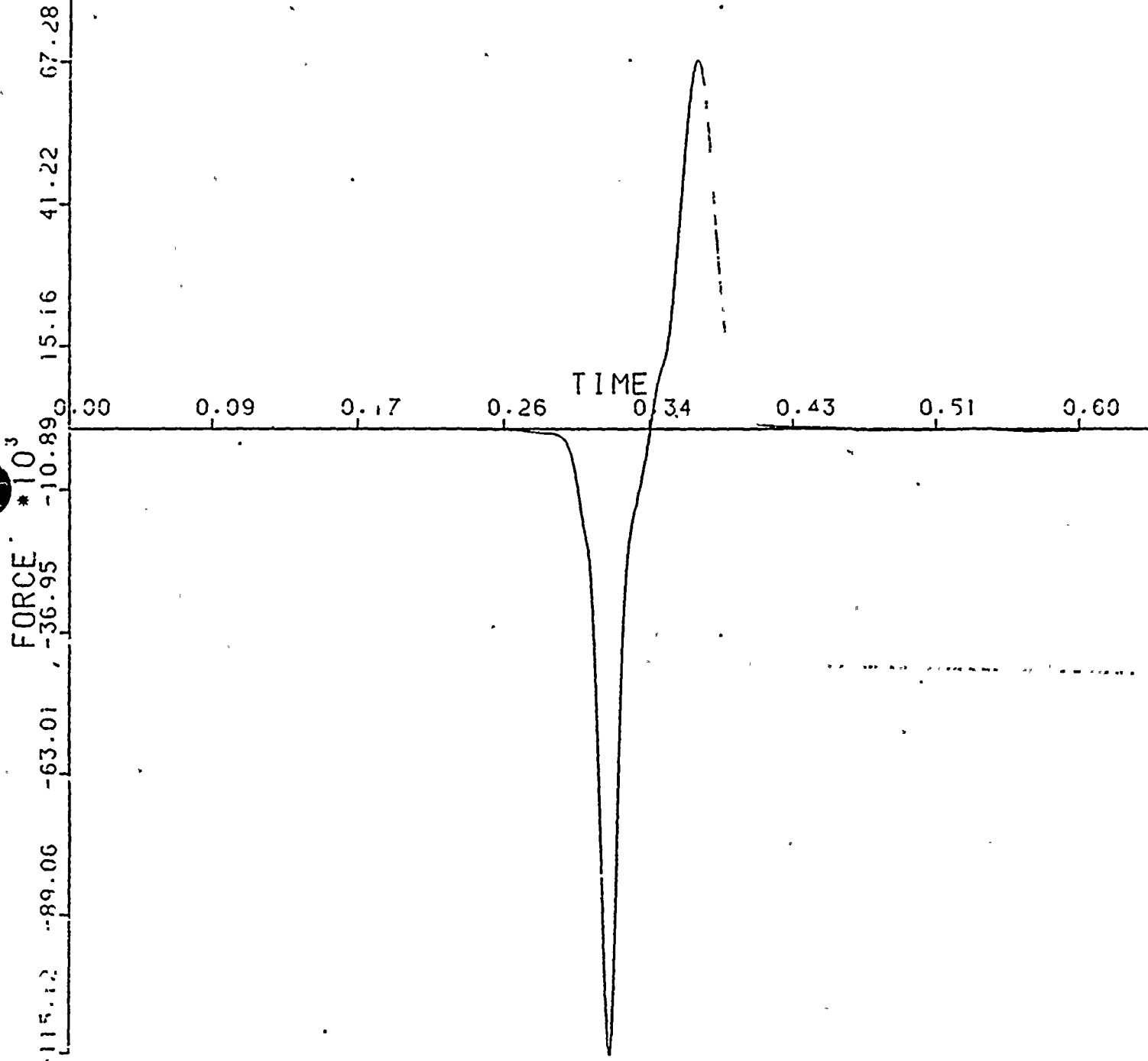
SAP2SAP VERIFICATION 5364

24-MAY-83

QUARTER, MODEL UNIT 2 LOOPSEAL

TIME/FORCE TABLE 19, MAGNITUDE AT NODE POINT

48



DONE BY DW DATE: 5-26-83

CHKD BY: KTG DATE: 5-27-83

Technical Report
TR-5364-1
Revision 0

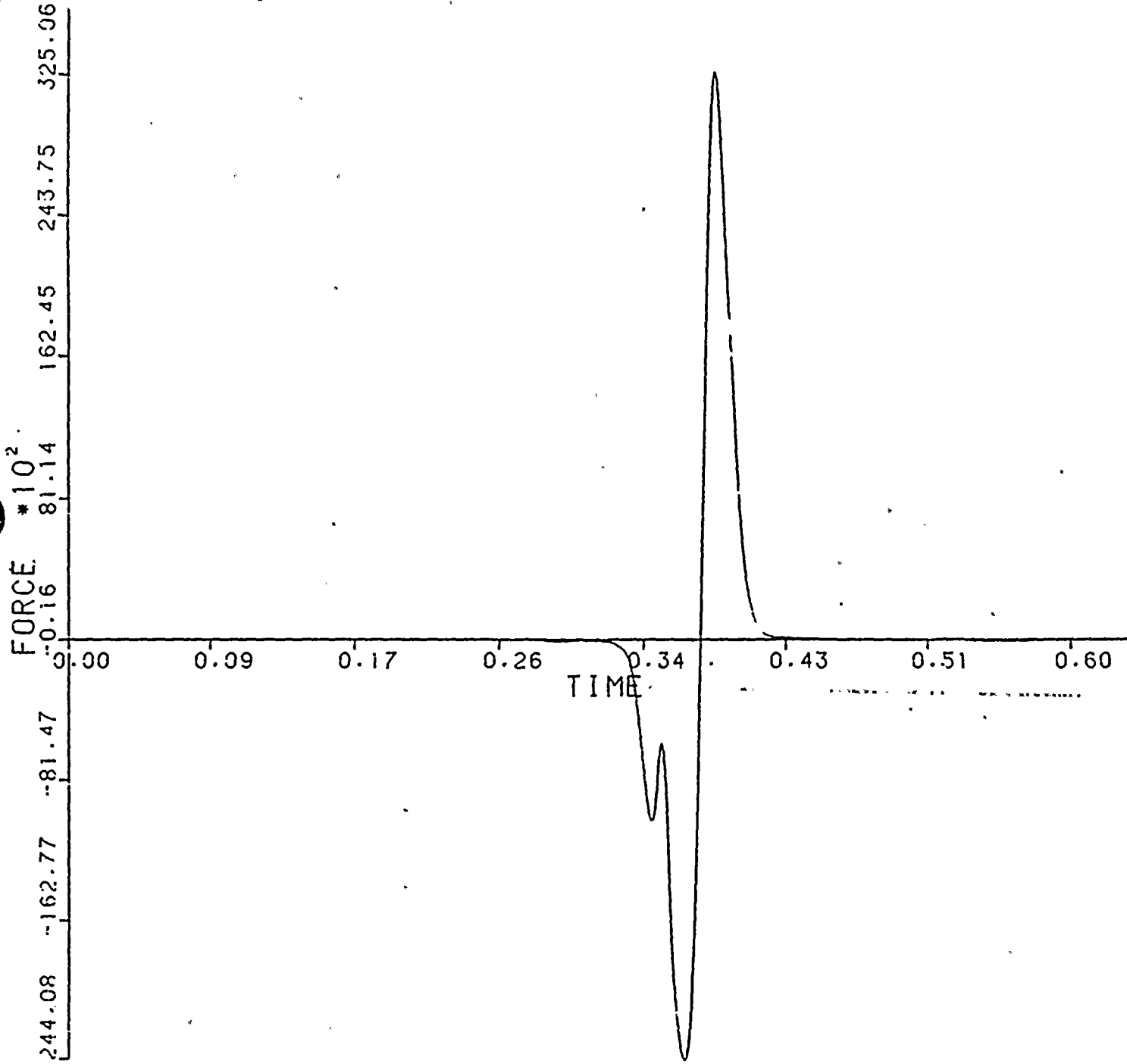


SAP2SAP VERIFICATION 5364

24-MAY-83

QUARTER MODEL UNIT 2 LOOPSEAL

TIME/FORCE TABLE 20. MAGNITUDE AT NODE POINT



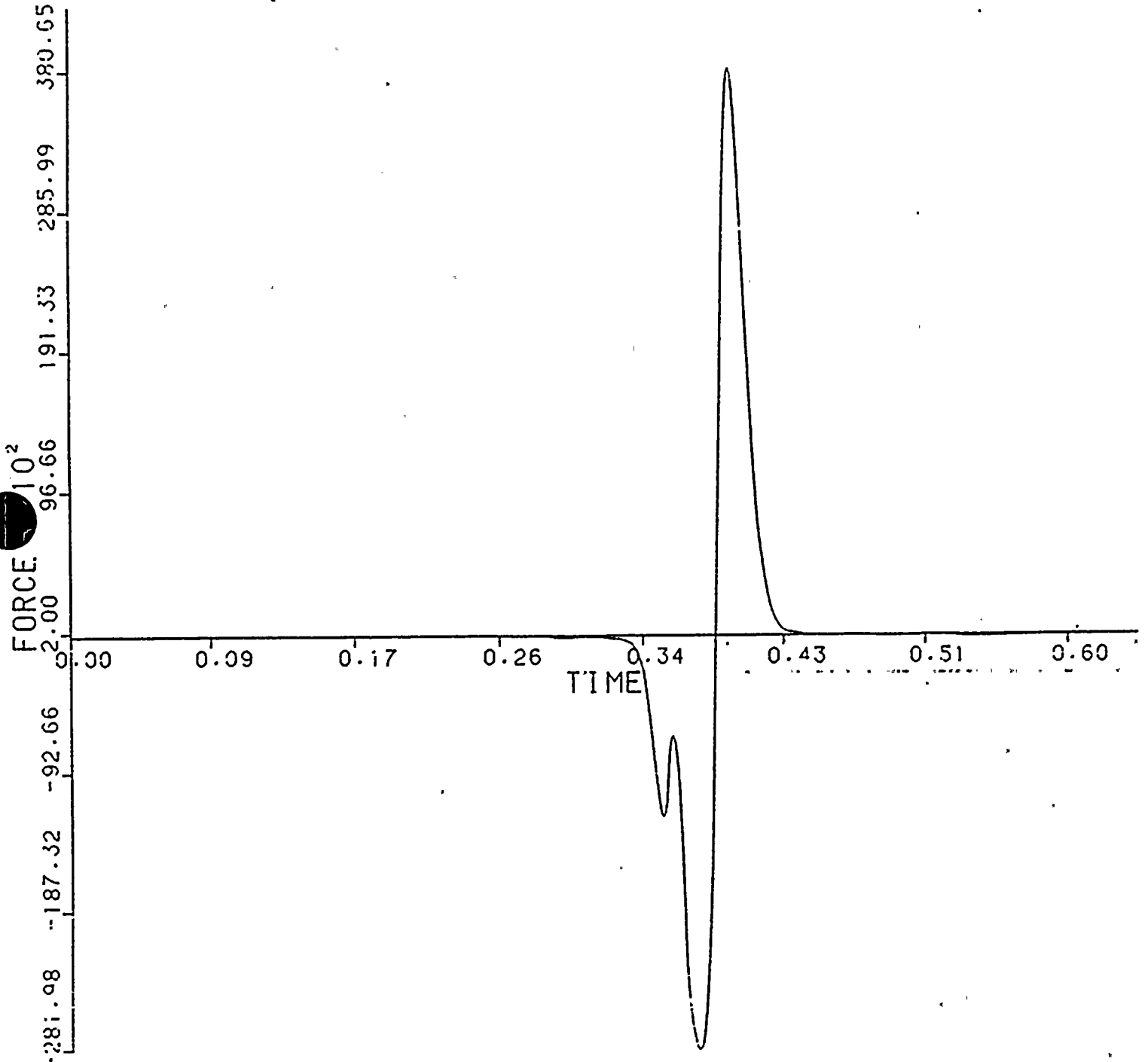
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CHKD BY: MT DATE: 5-27-83

Technical Report
TR-5364-1
Revision 0

SAP2SAP VERIFICATION 5364
QUARTER MODEL UNIT 2 LOOPSEAL
TIME/FORCE TABLE 21. MAGNITUDE AT NODE POINT

24-MAY-83



DONE BY LM DATE: 5-26-83
CHKD BY: KTG DATE: 5-27-83

Technical Report
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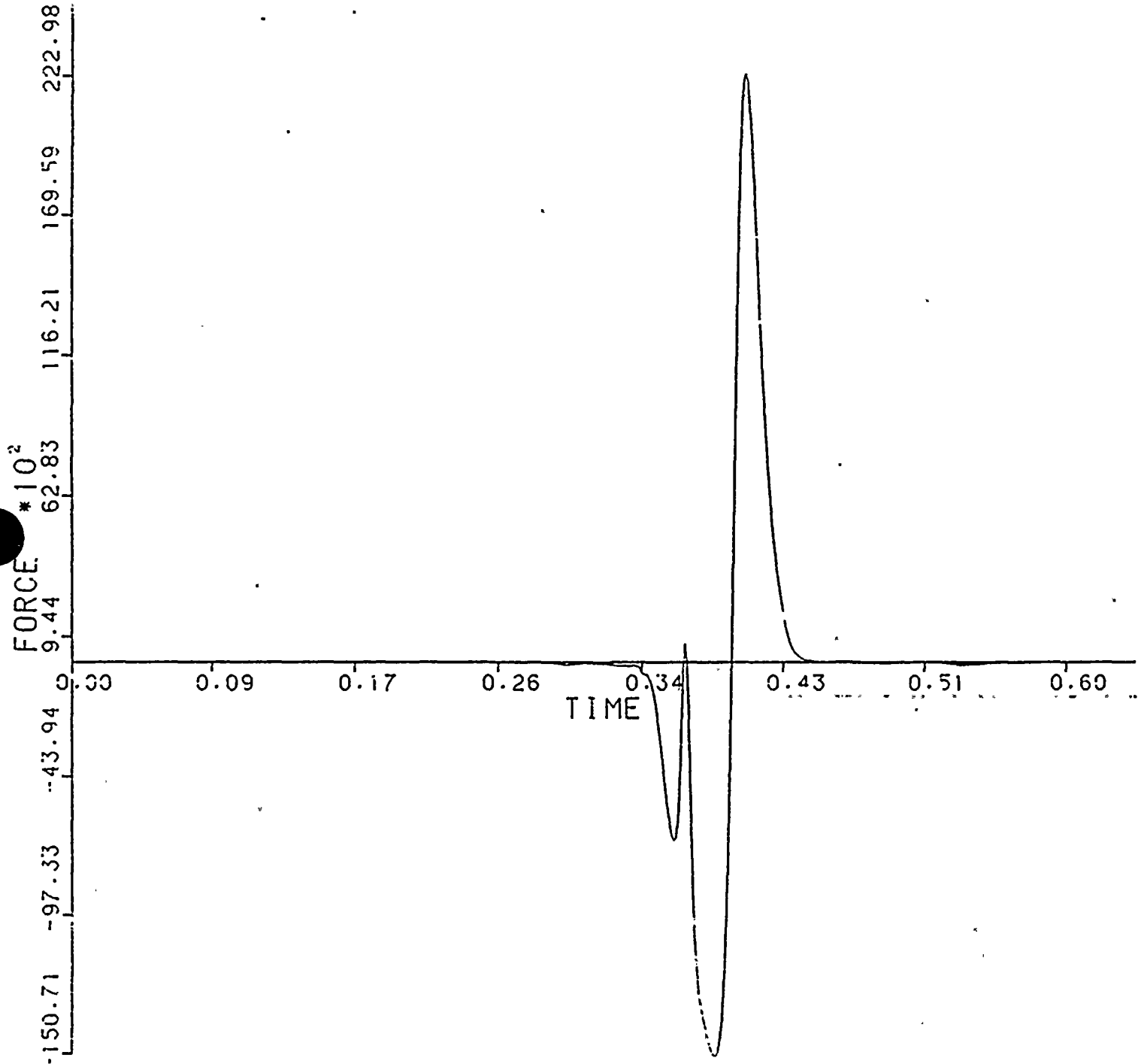
SAP/SAP VERIFICATION 5364

24-MAY-83

QUARTER MODEL UNIT 2 LOOPSEAL

TIME/FORCE TABLE 22. MAGNITUDE AT NODE POINT

34



DONE BY: SM DATE: 5-26-83

CHKD BY: ST DATE: 5-27-83

Technical Report

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Revision 0

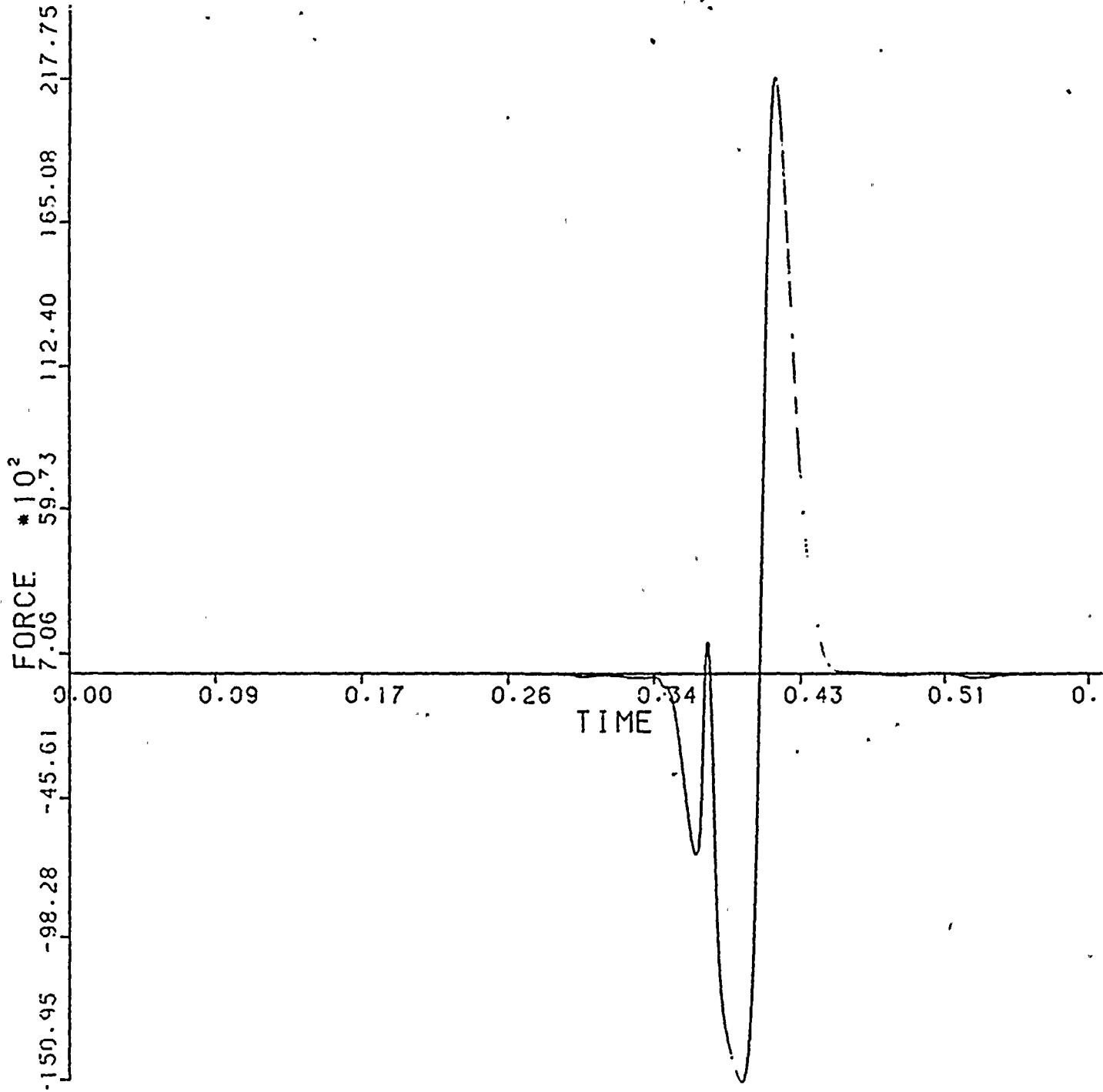


SAP2SAP VERIFICATION 5364

24-MAY-83

QUARTER MODEL UNIT 2 LOOPSEAL

TIME/FORCE TABLE 23, MAGNITUDE AT NODE POINT



DONE BY DL DATE: 5-28-83

CHKD BY: ST DATE: 5-27-83

Technical Report
TR-5364-1
Revision 0

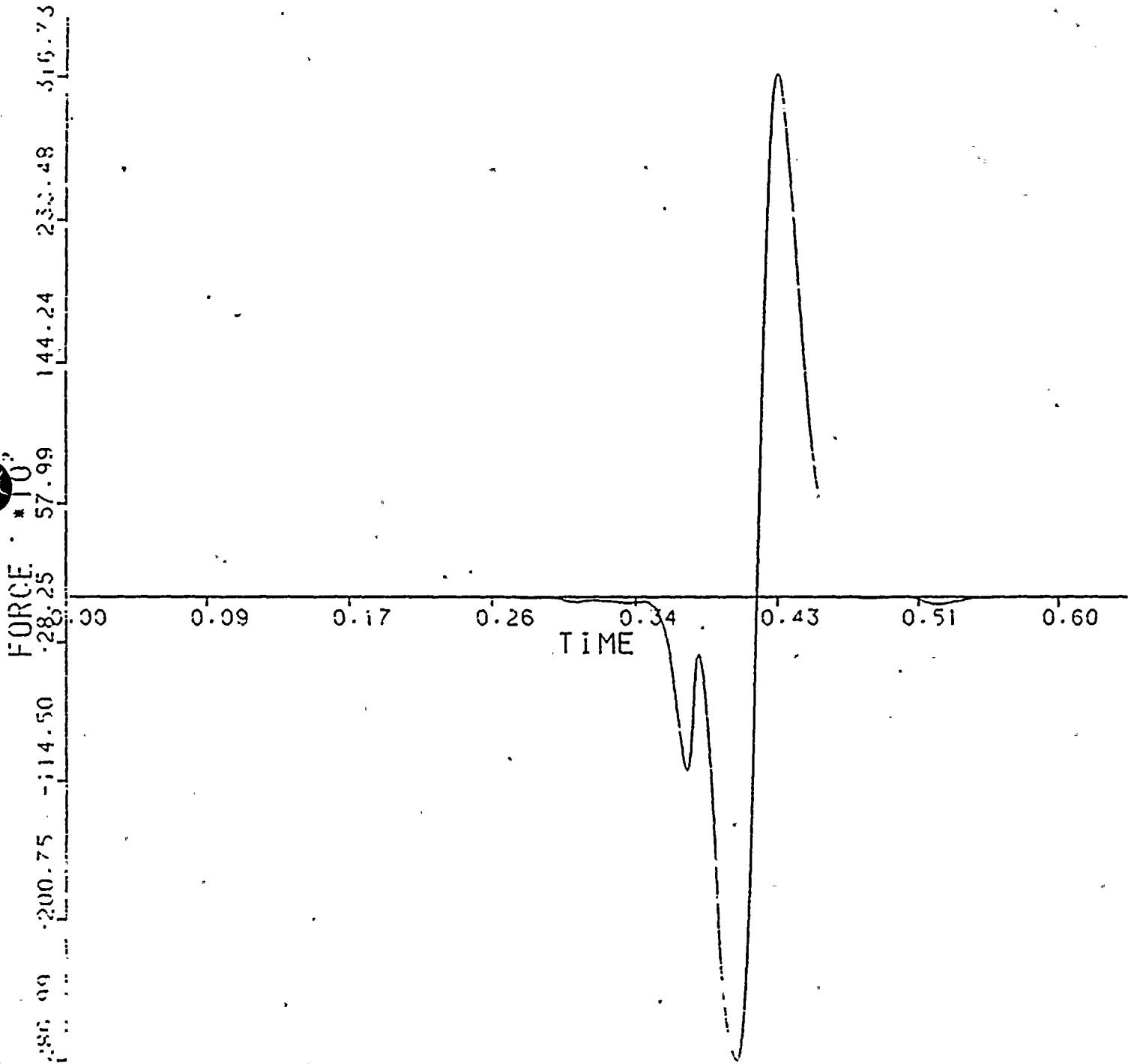


SAP2SAP VERIFICATION 5364

24-MAY-83

QUARTER MODEL UNIT 2 LOOPSEAL

TIME/FORCE TABLE 24. MAGNITUDE AT NODE POINT



DONE BY DW DATE: 5-28-83

CHKD BY: KMG DATE: 5-27-83

Technical Report

TR-5364-1

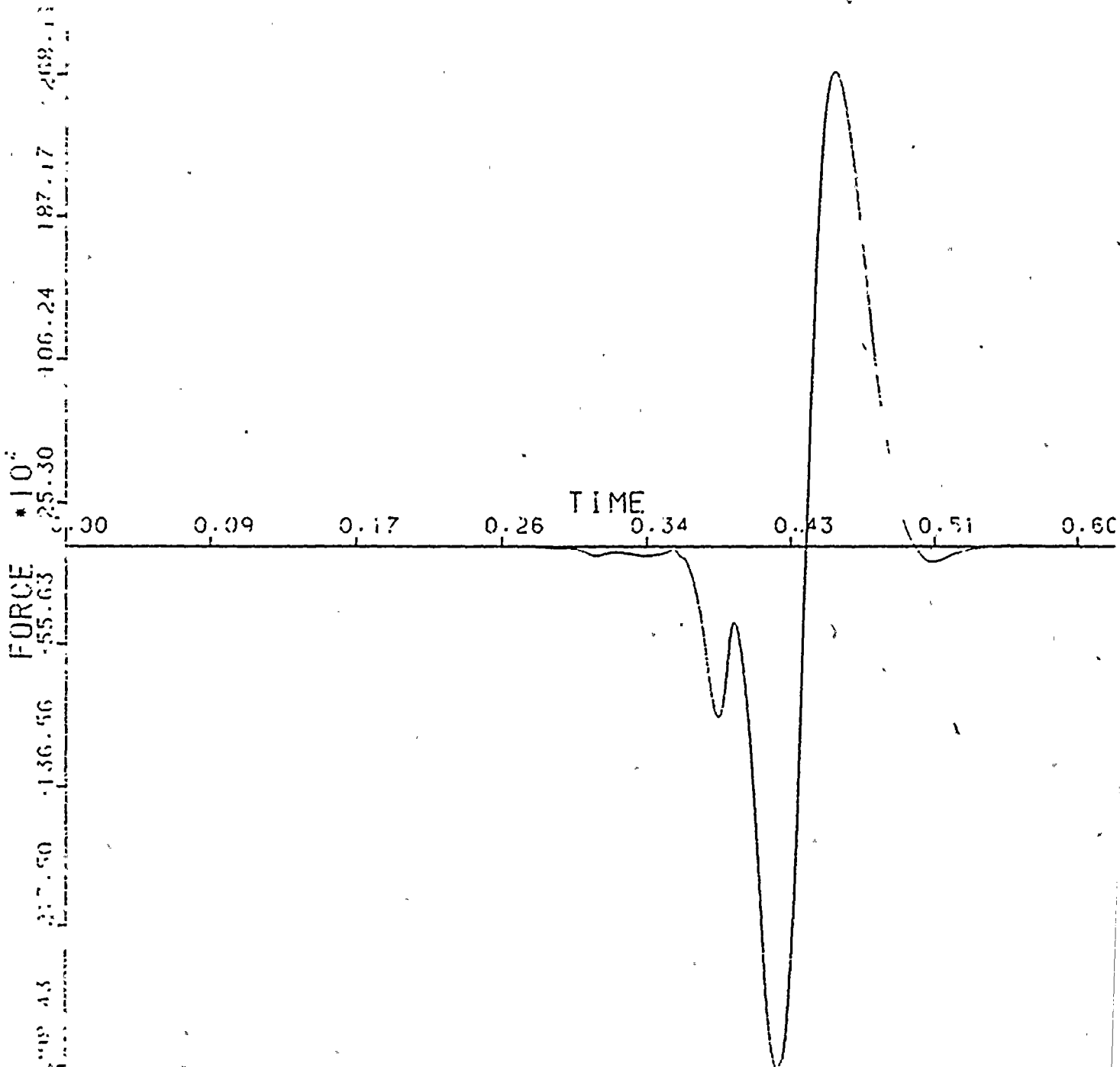
Revision 0



SAP2SAP VERIFICATION 5364

QUARTER MODEL UNIT 3 LOOPS/FAL

TIME SHEET TABLE 1.5. MAGNITUDE AT NODE POINT



DONE BY DL DATE: 5-28-83

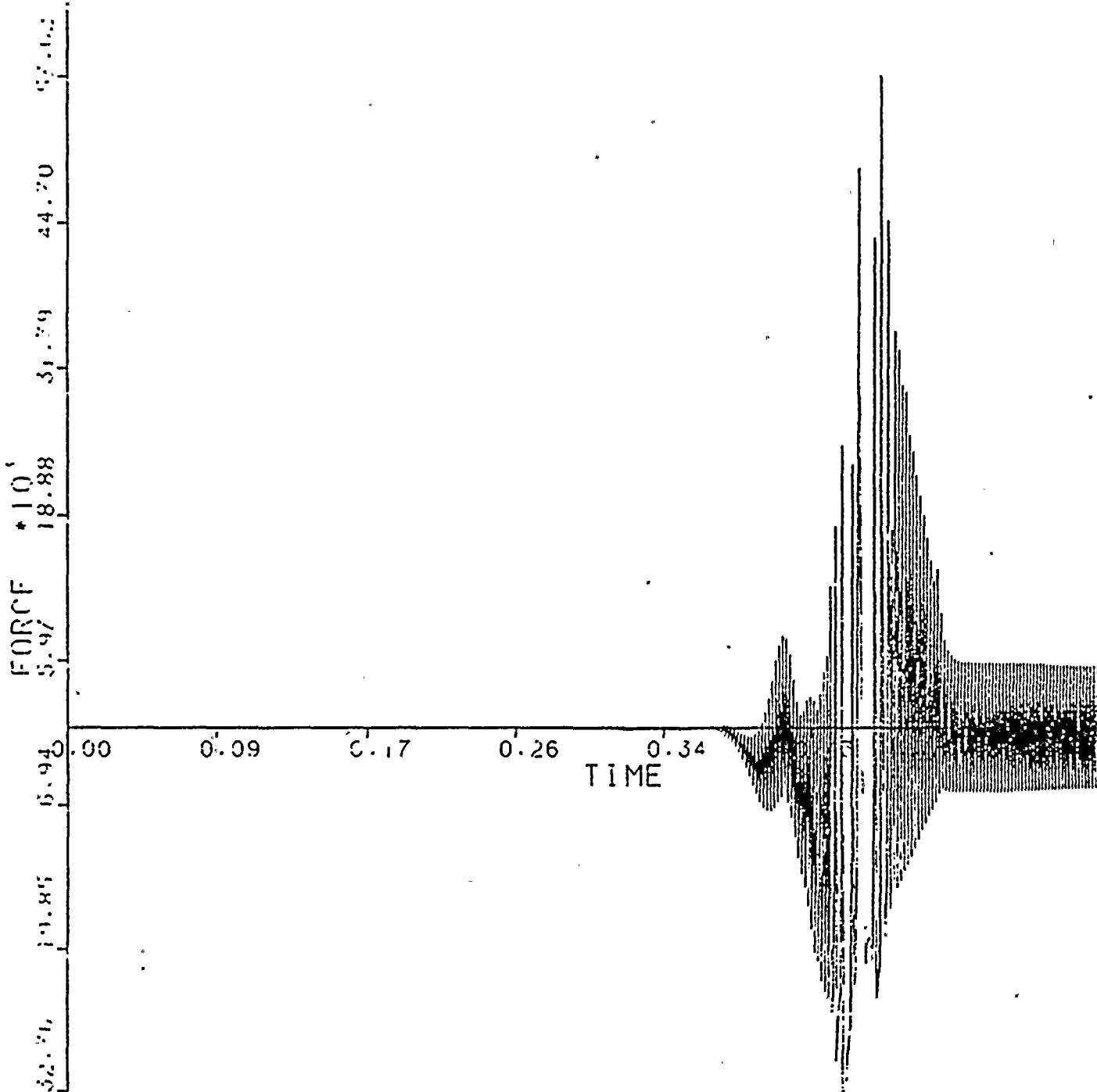
CHKD-BY: FT DATE: 5-27-83

Technical Report
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Revision 0



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SAP2SAP VERIFICATION 5364 24-MAY-83.
QUARTER MODEL UNIT 2 LOOPSEAL
TIME/FORCE TABLE 26. MAGNITUDE AT NODE POINT



DONE BY: ML DATE: 5-26-83
CHKD BY: ETG DATE: 5-27-83

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4.9 RELAP Input

The RELAP5 MOD1 input listings are included for each of the transient conditions.

<u>Input Listing</u>	<u>Unit</u>	<u>Transient Case</u>
4.9.1	1	PORV Condensate/Steam 0-200 msec
4.9.2	1	Condensate/Steam Restart 200-400 msec 400-600 msec
4.9.3	1	PORV Solid 400° Liquid 0-200 msec
4.9.4	1	PORV Solid 400° Liquid Restart 200-600 msec
4.9.5	2	SV Cold Loop Seal (Quarter Model)

The PORV model has:

- 396 volumes
- 397 junctions
- 7 tee branches

The SRV model has:

- 190 volumes
- 191 junctions

Heat structures were not included in the RELAP model because of the program capacity. Including heat structures would have further reduced the number of available control volumes. This is a conservative assumption, ITI (Reference 18) showed higher loads were computed without heat structures.

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 **TELEDYNE
ENGINEERING SERVICES**

4.9.1 PORV Condensate/Steam



LISTING OF INPUT DATA FOR CASE 1

```

1  =D.C.COOK UNIT1 PORV OPEN
2  *
3  * DISCHARGE PIPING
4  * THIS IS THE NUMBERING SYSTEM FOR UNIT1'S RELAP MODEL
5  * WHERE COMPONENTS NUMBERED IN THE:
6  *   100'S ARE VALVE SV-45C AND ARC 1 LEVEL 669'-2"
7  *   200'S ARE VALVE SV-45B AND ARC 2 LEVEL 670'-10"
8  *   300'S ARE VALVE SV-45A AND ARC 3 LEVEL 672'-8"
9  *   400'S ARE PORV NRV-151 AND ARC "A"
10 *   500'S ARE PORV NRV-153 AND ARC "B"
11 *   600'S ARE PORV NRV-152 AND ARC "C"
12 *   700'S AND 800'S ARE 6" AND 12" MAIN DISCHARGE PIPING
13 *   900'S QUENCH TANK PORTION
14 *   999 ATMOSPHERE
15 *
16 *
17 *

```

```

18 100 NEW TRANSNT
19 101 RUN
20 102 BRITISH BRITISH
21 104 NOACTION
22 *

```

```

23 *****
24 * TIME STEP CONTROL *
25 *****
26 *
27 201 0.200,1.-7,2.-4,11001,5,50,250
28 *
29 *

```

```

30 *****
31 * MINOR EDITS *
32 *****
33 *

```

```

34 301 MFLOWJ 41000000
35 302 MFLOWJ 51000000
36 303 MFLOWJ 61000000
37 304 MFLOWJ 40200000
38 305 MFLOWJ 81114000
39 306 MFLOWJ 81157000
40 307 MFLOWJ 30800000
41 308 MFLOWJ 20800000
42 309 MFLOWJ 10800000
43 *
44 310 QUALS 41101000
45 311 QUALS 51101000
46 312 QUALS 61101000
47 313 QUALS 40926000
48 314 QUALS 50912000
49 315 QUALS 60911000
50 316 QUALS 40128000
51 317 QUALS 81114000
52 318 QUALS 81157000
53 319 QUALS 30701000
54 320 QUALS 30718000
55 321 QUALS 20701000
56 322 QUALS 20726000

```

BY CMM DATE 4-12-83

CHKD. BY JBM DATE 4-20-83

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```

57 323 QUALS 107010000
58 324 QUALS 107330000
59 *
60 325 P 411010000
61 326 P 511010000
62 327 P 611010000
63 328 P 409260000
64 329 P 509120000
65 330 P 609110000
66 331 P 401280000
67 332 P 811140000
68 333 P 811570000
69 334 P 307010000
70 335 P 307180000
71 336 P 207010000
72 337 P 207260000
73 338 P 107010000
74 339 P 107330000

```

75 *

76 *

77 *****

78 * FORCE CARDS FOR REPIPE *

79 *****

80 *

81 *****

82 *THIS RELAP RUN INCLUDES FORCE CARDS OF THE MAIN HEADER, DOWNSTREAM

83 *DISCHARGE TOWARDS THE QUENCH TANK AS WELL AS THE SEGEMENTS DOWNSTREAM

84 *OF THE SAFETY VALVES AND ARC "2" ENTIRE MODEL.

85 *****

86 *

87 *

88 *****ARC-2*****

89 *

90 *

91 2001 5, 178, 207010000, 207020000, 207030000, 207040000, 207050000

92 2019 207060000, 207070000, 207080000, 207090000, 207100000

93 2020 207110000, 207120000, 207130000, 207140000, 207150000

94 2021 207160000, 207170000, 207180000, 207190000, 207200000

95 2022 207210000, 207220000, 207230000, 207240000, 207250000

96 2023 207260000, 307010000, 307020000, 307030000, 307040000

97 2024 307050000, 107010000, 107020000, 107030000, 107040000

98 2025 107050000

99 *

100 * MAIN HEADER 6 BY 12 IN

101 *

102 2033 703020000, 703030000, 703040000, 703050000, 703060000

103 2034 703070000, 703080000, 703090000, 703100000, 703110000

104 2035 703120000, 703130000, 703140000, 801010000, 803010000

105 2036 805010000, 807010000, 703010000

108 2037 809010000, 811010000, 811020000, 811030000, 811040000

107 2038 811050000, 811060000, 811070000, 811080000, 811090000

108 2039 811100000, 811110000, 811120000, 811130000, 811140000

109 2040 811150000, 307180000, 107330000

110 2042 811260000

111 *

112 *

113 * MAIN DISCHARGE DOWSTREAM TOWARDS QUENCH TANK

114 *

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115 2013 811270000,811280000,811290000,811300000,811310000
 116 2014 811320000,811330000,811340000,811350000,811360000
 117 2015 811370000,811380000,811390000,811400000,811410000
 118 2016 811420000,811430000,811440000,811450000,811460000
 119 2017 811470000,811480000,811490000,811500000,811510000
 120 2018 811520000,811530000,811540000,811550000,811560000
 121 2043 811570000,811580000,811590000,811600000,811610000
 122 2044 811620000,811630000,811640000,811650000,811660000
 123 2045 811670000,811680000,811690000,811700000,811710000
 124 2046 811720000,811730000,811740000,811750000,811760000
 125 2047 811770000,811780000,811790000,811800000,811810000
 126 2048 811820000,811830000,811840000,811850000,811860000
 127 2049 811870000,811880000,811890000,811900000,811910000
 128 2026 811920000,811930000,811940000,811950000,811960000
 129 2027 811970000,813010000,813020000,813030000,813040000
 130 2028 813050000,813060000,813070000,813080000,813090000
 131 2029 813100000,813110000,813120000,813130000,813140000
 132 2030 813150000,813160000,813170000,813180000,813190000
 133 2031 813200000,813210000,813220000,813230000,813240000
 134 2032 813250000,813260000,978010000,978020000,978030000
 135 2050 978040000,978050000,978060000,978070000,978080000

136 *
 137 *****

138 * TRIPS *
 139 *****

140 *
 141 *

142 501 TIME 0 GE NULL 0 0.0 L * VALVE OPENING TRIP
 143 502 TIME 0 GE NULL 0 5.0 L * JOB TERMINATION TRIP

144 515 P 982010000 GE NULL 0 114.7 L * QUENCH TANK RUPTURE PRESS.
 145 600 502

146 *
 147 *****

148 *
 149 * HYDRODYNAMIC COMPONENTS *
 150 *
 151 *****

152 *
 153 *

154 * PRESSURIZER COMPONENT

155 3990000 "PRESS" TMDPVOL
 156 3990101 0.0 20.0 500.0 0.0 0.0 0.0 0.00005 0.0 11
 157 3990200 2

158 3990201 0.0 2349.7 1.0 0.8 2420.0 1.0 1.2 2498.7 1.0
 159 *

160 4000000 "PORV" SNGLJUN
 161 4000101 399000000 401000000 0.0 0.0 0.0 1100
 162 4000201 1 0.0 0.0 0.0

163 *
 164 4010000 "PORV" PIPE

165 4010001 28
 166 4010101 0.1465 28
 167 4010301 .4375 4
 168 4010302 .5104 12
 169 4010303 .5 19
 170 4010304 .5 27
 171 4010305 0.72 28
 172 4010401 0.0 28

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173	4010601	45.	4							
174	4010602	90.	12							
175	4010603	0.0	19							
176	4010604	90.	27							
177	4010605	0.0	28							
178	4010801	1.51E-4	0.0	28						
179	4010901	0.0	0.0	3						
180	4010902	.092	.092	4						
181	4010903	0.0	0.0	11						
182	4010904	.1836	.1836	12						
183	4010905	0.0	0.0	18						
184	4010906	.1836	.1836	19						
185	4010907	0.0	0.0	28						
186	4010908	0.1836	0.1836	27						
187	4011001	00	28							
188	4011101	1000	27							
189	4011201	2	2349.7	1.0	0.0	0.0	0.0	28		
190	4011300	1								
191	4011301	0.0	0.0	0.0	27					
192	*									
193	4020000	"PORV"	SNGLJUN							
194	4020101	401010000	403000000	0.0	0.0	0.0	1000			
195	4020201	1	0.0	0.0	0.0					
196	*									
197	4030000	"PORV"	BRANCH							
198	4030001	0								
199	4030101	0.1465	0.5	0.0	0.0	0.0	0.0	1.51E-4	0.0	00
200	4030200	2	2349.7	1.0	0.0	0.0	0.0			
201	*									
202	4040000	"PORV"	SNGLJUN							
203	4040101	403010000	405000000	0.1465	0.0	0.0	1000			
204	4040201	1	0.0	0.0	0.0					
205	*									
206	4050000	"PORV"	PIPE							
207	4050001	16								
208	4050101	0.1465	1							
209	4050102	0.0718	16							
210	4050301	0.698	1							
211	4050302	0.471	7							
212	4050303	0.451	16							
213	4050401	0.0	.16							
214	4050601	0.0	.16							
215	4050801	1.51E-4	0.0	1						
216	4050802	1.33E-4	0.0	16						
217	4050901	0.0577	0.0981	1						
218	4050902	0.0	0.0	15						
219	4051001	00	.16							
220	4051101	1000	15							
221	4051201	2	2349.7	1.0	0.0	0.0	16			
222	4051300	1								
223	4051301	0.0	0.0	0.0	15					
224	*									
225	4060000	"PORV"	SNGLJUN							
226	4060101	405010000	407000000	0.0	0.0	0.0	1000			
227	4060201	1	0.0	0.0	0.0					
228	*									
229	4070000	"PORV"	BRANCH							
230	4070001	0								

231	4070101	0.0716	0.451	0.0	0.0	0.0	0.0	1.33E-4	0.0	00
232	4070200	2	2349.7	1.0	0.0	0.0	0.0			
233	*									
234	4080000	"PORV"	SNGLJUN							
235	4080101	407010000	409000000	0.0	0.0	0.0	1000			
236	4080201	1	0.0	0.0	0.0					
237	*									
238	4090000	"PORV"	PIPE							
239	4090001	26								
240	4090101	0.0716	1							
241	4090102	0.03757	22							
242	4090103	0.03388	23							
243	4090104	0.02650	24							
244	4090105	0.01912	25							
245	4090106	0.01175	26							
246	4090301	0.53	1							
247	4090302	.30	2							
248	4090303	0.493	10							
249	4090304	0.55	14							
250	4090305	0.510	22							
251	4090306	0.255	26							
252	4090401	0.0	26							
253	4090601	0.0	26							
254	4090801	1.33E-4	0.0	1						
255	4090802	1.53E-4	0.0	26						
256	4090901	0.0	0.0	13						
257	4090902	0.585	0.585	14						
258	4090903	0.0	0.0	25						
259	4091001	00	26							
260	4091102	1000	25							
261	4091201	2	2349.7	1.0	0.0	0.0	17			
262	4091202	2	2349.7	0.0	0.0	0.0	26			
263	4091300	1								
264	4091301	0.0	0.0	0.0	25					
265	*									
266	4100000	"PORV151"	VALVE							
267	4100101	409010000	411000000	0.00808	0.0	0.0	0100			
268	4100201	1	0.0	0.0	0.0					
269	4100300	MTRVLV								
270	4100301	501	502	1.0	0.0					
271	*									
272	5080000	"PORV"	SNGLJUN							
273	5080101	407010000	509000000	0.0	0.2172	0.2172	1000			
274	5080201	1	0.0	0.0	0.0					
275	*									
276	5090000	"PORV"	PIPE							
277	5090001	12								
278	5090101	0.03757	8							
279	5090102	0.03388	9							
280	5090103	0.02650	10							
281	5090104	0.01912	11							
282	5090105	0.01175	12							
283	5090301	0.4089	2							
284	5090302	0.5078	8							
285	5090303	0.2539	12							
286	5090401	0.0	12							
287	5090601	0.0	12							
288	5090801	1.53E-4	0.0	12						

289	5090901	0.0	0.0	1					
290	5090902	0.2172		0.2172	2				
291	5090903	0.0		0.0	11				
292	5091001	00		12					
293	5091101	1000		11					
294	5091201	2	2349.7	1.0	0.0	0.0	0.0	3	
295	5091202	2	2349.7	0.0	0.0	0.0	0.0	12	
296	5091300	1							
297	5091301	0.0	0.0	0.0				11	
298	*								
299	5100000	"PORV152"	VALVE						
300	5100101	509010000	511000000	0.00806	0.0	0.0	0.0	0100	
301	5100201	1	0.0	0.0	0.0				
302	5100300	MTRVLV							
303	5100301	501	502	1.0	0.0				
304	*								
305	6080000	"PORV"	SNGLJUN						
306	6080101	403010000	609000000	0.0	0.1836	0.1836	1000		
307	6080201	1	0.0	0.0	0.0				
308	*								
309	6090000	"PORV"	PIPE						
310	6090001	11							
311	6090101	0.03757		7					
312	6090102	0.03388		8					
313	6090103	0.02650		9					
314	6090104	0.01912		10					
315	6090105	0.01175		11					
316	6090301	0.4089		2					
317	6090302	0.5699		7					
318	6090303	.2850		11					
319	6090401	0.0		11					
320	6090601	0.0		11					
321	6090801	1.53E-4		0.0	11				
322	6090901	0.0	0.0	1					
323	6090902	0.2172		0.2172	2				
324	6090903	0.0		0.0	10				
325	6091001	00		11					
326	6091101	1000		10					
327	6091201	2	2349.7	1.0	0.0	0.0	0.0	4	
328	6091202	2	2349.7	0.0	0.0	0.0	0.0	11	
329	6091300	1							
330	6091301	0.0	0.0	0.0				10	
331	*								
332	6100000	"PORV153"	VALVE						
333	6100101	609010000	611000000	0.00806	0.0	0.0	0.0	0100	
334	6100201	1	0.0	0.0	0.0				
335	6100300	MTRVLV							
336	6100301	501	502	1.0	0.0				
337	*****								
338	*								
339	*	VALVE	DOWNSTREAM	PIPING					
340	1070000	"DWNSTRM#1"	PIPE						
341	1070001	33							
342	*								
343	1070101	0.20069		33					
344	*								
345	1070301	0.5261		4					
346	1070302	0.9943		15					

347	1070303	0.9132		21
348	1070304	0.8472		30
349	1070305	1.085		33
350	*			
351	1070401	0.0		33
352	*			
353	1070601	0.0		4
354	1070602	-90.		15
355	1070603	0.0		33
358	*			
357	1070801	1.52-4	0.	33
358	1070901	0.0	0.0	3
359	1070902	0.18	0.18	4
360	1070903	0.0	0.0	14
361	1070904	0.18	0.18	15
362	1070905	0.0	0.0	32
363	*			
364	1071001	00		33
365	1071101	1000		32
366	*			
367	1071201	4	17.7 120.	0.8284 0. 33
368	*			
369	1071300	1		
370	1071301	0.0	0.0 0.0	32
371	*			
372	*			
373	*			
374	*			
375	*****			
376	*			
377	+	VALVE DOWNSTREAM PIPING		
378	2070000	"DWNSTRM#2"	PIPE	
379	*			
380	2070001			26
381	2070101	0.20069		26
382	*			
383	2070301	0.5261		4
384	2070302	0.9271		14
385	2070303	0.8852		23
388	2070304	1.085		28
387	*			
388	2070401	0.0		26
389	*			
390	2070601	0.0		4
391	2070602	-90.		14
392	2070603	0.0		28
393	*			
394	2070801	1.52-4	0.	28
395	*			
396	2070901	0.0	0.0	3
397	2070902	0.18	0.18	4
398	2070903	0.0	0.0	13
399	2070904	0.18	0.18	14
400	2070905	0.0	0.0	25
401	*			
402	2071001	00		28
403	*			
404	2071101	1000		25



405 *
 406 2071201 4 17.7 120. 0.9284 0. 28
 407 *
 408 2071300 1
 409 2071301 0.0 0.0 0.0 25
 410 *
 411 *

414 * VALVE DOWNSTREAM PIPING

415 3070000 "DWNSTRM#3" PIPE

416 3070001 18

417 *
418 3070101 0.20069 18

419 *
420 3070301 0.5261 4

421 3070302 1.0339 12

422 3070303 0.801 15

423 3070304 1.085 18

424 *
425 3070401 0.0 18

426 *
427 3070601 0.0 4

428 3070602 -90. 12

429 3070603 0.0 18

430 *
431 3070801 1.52-4 0. 18

432 *
433 3070901 0.0 0.0 3

434 3070902 0.18 0.18 4

435 3070903 0.0 0.0 11

438 3070904 0.18 0.18 12

437 3070905 0.0 0.0 17

438 *
439 3071001 00 18

440 3071101 1000 17

441 *
442 3071201 4 17.7 120. 0.9284 0. 18

443 *
444 3071300 1

445 3071301 0.0 0.0 0.0 17

446 *
447 *

448 *****

449 * PORV DISCHARGE SECTION

450 *****

451 *****

452 *****

453 *****

454 * PORV NRV-151 DISCHARGE LINE ARC "A"

455 *****

456 *
457 *

458 4110000 "PORV1" PIPE

459 4110001 18

460 *
461 4110101 0.05132 17

462 4110102 0.20069 19

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463	*								
464	4110301	0.3724	4						
465	4110302	0.3802	8						
466	4110303	0.561	17						
467	4110304	0.349	19						
468	*								
469	4110401	0.0	19						
470	*								
471	4110601	0.0	4						
472	4110602	-90.	8						
473	4110603	0.0	19						
474	*								
475	4110801	1.53-4	0 17						
476	4110802	1.52-4	0 19						
477	*								
478	4110901	0.0	0.0	3					
479	4110902	0.2088	0.2088	4					
480	4110903	0.0	0.0	7					
481	4110904	0.2088	0.2088	8					
482	4110905	0.0	0.0	18					
483	4110906	0.3784	0.1565	17					
484	4110907	0.0	0.0	18					
485	*								
486	4111001	00	19						
487	4111101	1000	18						
488	*								
489	4111201	4	17.7	120.	0.9284	0.0	19		
490	*								
491	4111300	1							
492	4111301	0.0	0.0	0.0	18				
493	*								
494	4120000	"ENTERMAIN"	SNGLJUN						
495	4120101	411010000	701000000	0.0	0.1800	0.1800	1100		
496	4120201	1	0.0	0.0	0.0				
497	*								
498	*								
499	*****								
500	*	PORV NRV-153 DISCHARGE LINE ARC "B"	*						
501	*****								
502	*								
503	*								
504	*								
505	5110000	"PORV2LINE"	PIPE						
506	5110001	19							
507	*								
508	5110101	0.05132	18						
509	5110102	0.08840	19						
510	*								
511	5110301	0.4303	3						
512	5110302	0.3620	7						
513	5110303	0.3529	9						
514	5110304	0.6058	18						
515	5110305	0.371	19						
516	*								
517	5110401	0.0	19						
518	*								
519	5110601	0.0	3						
520	5110602	-90.	7						

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TELEDYNE
ENGINEERING SERVICES




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579 5151001 00 12
580 *
581 5151101 1000 11
582 *
583 5151201 4 17.7 120. 0.9284 0.0 12
584 *
585 5151300 1
586 5151301 0.0 0.0 0.0 11
587 *
588 5160000 "ENTERMAIN" SNGLJUN
589 5160101 515010000 701000000 0.0 0.0 0.0 1000
590 5160201 1 0.0 0.0 0.0
591 *
592 *
593 *****
594 * PORV NRV-152 DISCHARGE LINE ARC "C" *
595 *****
596 *
597 *
598 *
599 6110000 "PORVDISC3" PIPE
600 6110001 8
601 *
602 6110101 0.05132 8
603 *
604 6110301 0.3723 4
605 6110302 0.3648 8
606 *
607 6110401 0.0 8
608 *
609 6110601 0.0 4
610 6110602 -90. 8
611 *
612 6110801 1.53-4 .0 8
613 *
614 6110901 0.0 0.0 3
615 6110902 0.211 0.211 4
616 6110903 0.0 0.0 7
617 *
618 6111001 00 8
619 6111101 1000 7
620 *
621 6111201 4 17.7 120. 0.9284 0.0 8
622 *
623 6111300 1
624 6111301 0.0 0.0 0.0 7
625 *
626 6120000 "PORVLINE" SNGLJUN
627 6120101 611010000 513000000 0.0 0.0 0.0 1000
628 6120201 1 0.0 0.0 0.0
629 *
630 *****
631 * MAIN DISCHARGE LINE SECTION *
632 *****
633 *
634 *
635 * MAIN DISCHARGE LINE
636 7010000 "ENTERMAIN" BRANCH

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TELEDYNE
ENGINEERING SERVICES

637	7010001	0									
638	7010101	0.20069	0.7035	0.0	0.0	0.0	0.0	1.52-4	0.0	00	
639	7010200	4	17.7	120.	0.9284	0.0	0.0				
640	*										
641	7020000	"MAINLINE"	SNGLUUN								
642	7020101	701010000	703000000	0.0	0.0	0.0	1000				
643	7020201	1	0.0	0.0	0.0						
644	*										
645	7030000	"MAINLINE"	PIPE								
646	*										
647	7030001	14									
648	*										
649	7030101	0.20069	12								
650	7030102	0.77708	14	* 12 IN LINE STARTS HERE							
651	*										
652	7030301	0.7035	1								
653	7030302	1.0076	12								
654	7030303	0.5834	14	* 12 IN LINE STARTS HERE							
655	*										
656	7030401	0.0	14								
657	*										
658	7030601	0.0	1								
659	7030602	-90.	14								
660	*										
661	7030801	1.52-4	0.	12							
662	7030802	1.69-4	0.	14							
663	*										
664	7030901	0.180	0.180	1							
665	7030902	0.0	0.0	11							
666	7030903	0.493	0.2045	12							
667	7030904	0.0	0.0	13							
668	*										
669	7031001	00	14								
670	7031101	1000	13								
671	*										
672	7031201	4	17.7	120.	0.9284	0.0	14				
673	*										
674	7031300	1									
675	7031301	0.0	0.0	0.0	13						
676	*										
677	*										
678	7040000	"MAINLINE"	SNGLUUN								
678	7040101	703010000	801000000	0.0	0.0	0.0	1000				
680	7040201	1	0.0	0.0	0.0						
681	*										
682	3080000	"CON.1"	SNGLUUN								
683	3080101	307010000	801000000	0.0	0.1560	0.1560	1000				
684	3080201	1	0.0	0.0	0.0						
685	*										
686	*										
687	*										
688	*										
689	*										
690	*	CONNECTION TO MAIN LINE AT ELEV. 672'-6"									
691	*										
692	*										
693	8010000	"12-BRANC1"	BRANCH								
694	8010001	0									

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695	8010101	0.77708	0.8334	0.0	0.0	-90.	-0.8334	1.69-4	0.0	00
696	8010200	4	17.7	120.	0.9284	0.0	0.0			
697	*									
698	8020000	"MAINLINE"	SNGLJUN							
699	8020101	801010000	803000000	0.0	0.0	0.0	1000			
700	8020201	1	0.0	0.0	0.0					
701	*									
702	8030000	"MAINLINE"	SNGLVOL							
703	8030101	0.77708	0.8334	0.0	0.0	-90.	-0.8334	1.69-4	0.0	00
704	8030200	4	17.7	120.	0.9284	0.0	0.0			
705	*									
706	*	CONNECTION TO MAIN LINE AT ELEV. 670'-10"								
707	*									
708	*									
709	8040000	"MAINLINE"	SNGLJUN							
710	8040101	803010000	805000000	0.0	0.0	0.0	1000			
711	8040201	1	0.0	0.0	0.0					
712	*									
713	2080000	"CON.2"	SNGLJUN							
714	2080101	207010000	805000000	0.0	0.1560	0.1560	1000			
715	2080201	1	0.0	0.0	0.0					
716	*									
717	8050000	"MAINBR.3"	BRANCH							
718	8050001	0								
719	8050101	0.77708	0.8334	0.0	0.0	-90.	-0.8334	1.69-4	0.0	00
720	8050200	4	17.7	120.	0.9284	0.0	0.0			
721	*									
722	8060000	"MAINLINE"	SNGLJUN							
723	8060101	805010000	807000000	0.0	0.0	0.0	1000			
724	8060201	1	0.0	0.0	0.0					
725	*									
726	8070000	"MAINLINE"	SNGLVOL							
727	8070101	0.77708	0.8334	0.0	0.0	-90.	-0.8334	1.69-4	0.0	00
728	8070200	4	17.7	120.	0.9284	0.0	0.0			
729	*									
730	*									
731	*	CONNECTION TO MAIN LINE AT ELEV. 669'-2"								
732	*									
733	*									
734	*									
735	8080000	"MAINLINE"	SNGLJUN							
736	8080101	807010000	809000000	0.0	0.0	0.0	1000			
737	8080201	1	0.0	0.0	0.0					
738	*									
739	1080000	"CON.3"	SNGLJUN							
740	1080101	107010000	809000000	0.0	0.1560	0.1560	1000			
741	1080201	1	0.0	0.0	0.0					
742	*									
743	8090000	"MAINBR4"	BRANCH							
744	8090001	0								
745	8090101	0.77708	0.8334	0.0	0.0	-90.	-0.8334	1.69-4	0.0	00
746	8090200	4	17.7	120.	0.9284	0.0	0.0			
747	*									
748	8100000	"MAINLINE"	SNGLJUN							
749	8100101	809010000	811000000	0.0	0.0	0.0	1000			
750	8100201	1	0.0	0.0	0.0					
751	*									
752	*									

753	8110000	"MAINLINE"	PIPE		
754	*				
755	8110001		97		
756	*				
757	8110101	0.77708	97		
758	*				
759	8110301	1.0149	14		
760	8110302	0.5303	18		
761	8110303	0.5	22		
762	8110304	0.5303	26		
763	8110305	0.9908	56		
764	8110306	0.5	64		
765	8110307	0.8750	72		
766	8110308	0.5104	80		
767	8110309	0.5000	88		
768	8110310	1.0558	97		
769	*				
770	8110401	0.0	97		
771	*				
772	8110601	-90.	14		
773	8110602	-45.	18		
774	8110603	-90.	22		
775	8110604	-45.	26		
776	8110605	-90.	56		
777	8110606	0.0	80		
778	8110607	-90.	88		
779	8110608	0.0	97		
780	*				
781	8110801	1.69-4	0. 97		
782	*				
783	8110901	0.0	0.0	13	
784	8110902	0.078	0.078	14	
785	8110903	0.0	0.0	17	
786	8110904	0.078	0.078	18	
787	8110905	0.0	0.0	21	
788	8110906	0.078	0.078	22	
789	8110907	0.0	0.0	25	
790	8110908	0.078	0.078	26	
791	8110909	0.0	0.0	55	
792	8110910	0.158	0.158	56	
793	8110911	0.0	0.0	63	
794	8110912	0.028	0.028	64	
795	8110913	0.0	0.0	71	
796	8110914	0.13	0.13	72	
797	8110915	0.0	0.0	79	
798	8110916	0.158	0.158	80	
799	8110917	0.0	0.0	87	
800	8110918	0.158	0.158	88	
801	8110919	0.0	0.0	96	
802	*				
803	8111001	00	97		
804	*				
805	8111101	1000	96		
806	*				
807	8111201	4 17.7 120.	0.9298 0.0	97	
808	*				
809	8111300	1			
810	8111301	0.0 0.0 0.0	96		



811	*									
812	*									
813	8120000	"MAINDISC"	SINGLJUN							
814	8120101	811010000	813000000	0.0	0.158	0.158	1000			
815	8120201	1	0.0	0.0	0.0					
816	*									
817	8130000	"MAINLINE"	PIPE							
818	*									
819	8130001		26							
820	*									
821	8130101	0.77708	26							
822	*									
823	8130301	1.0	14							
824	8130302	0.5	24							
825	8130303	1.20833	28							
826	*									
827	8130401	0.0	28							
828	*									
829	8130601	0.0	24							
830	8130602	-90.	26							
831	*									
832	8130801	1.89-4	0. 28							
833	*									
834	8130901	0.0	0.0	13						
835	8130902	0.158	0.158	14						
836	8130903	0.0	0.0	23						
837	8130904	0.158	0.158	24						
838	8130905	0.0	0.0	25						
839	*									
840	8131001	00	28							
841	*									
842	8131101	1000	25							
843	*									
844	8131201	4	17.7	120.	0.9284	0.0	28			
845	*									
846	8131300	1								
847	8131301	0.0	0.0	0.0	25					
848	*									
849	*									
850	*									
851	*	*****								
852	*	QUENCH TANK	*							
853	*	*****								
854	*									
855	*									
856	*									
857	9770000	"QTANK-IN"	SINGLJUN							
858	9770101	813010000	978000000	0.	0.	0.	1000			
859	9770201	1	0.	0.	0.					
860	*									
861	*	SPARGER	12 IN SCH40	PIPE						
862	*									
863	9780000	"SPARGER"	PIPE							
864	*	NO OF VOLUMES								
865	9780001	18								
866	*	FLOW AREA								
867	9780101	0.7773	18							
868	*	VOL. LENGTHS								

Faint, illegible markings at the top left of the page, possibly bleed-through from the reverse side.



869	9780301	1.125	2							
870	9780302	1.1333	7							
871	9780303	1.0	18							
872	*	VOL. VOLS.								
873	9780401	0.0	18							
874	*									
875	*	VERTICAL ANGLES								
876	9780601	-90.	7							
877	9780602	0.0	18							
878	*	PIPE ROUGHNESS								
879	9780801	1.69-4	0.0	18						
880	*	JUNCTION LOSS COEFF.								
881	9780901	0.0	0.0	8						
882	9780902	0.156	0.158	7						
883	9780903	0.0	0.0	17						
884	*	VOL. CONTROL FLAG								
885	9781001	00	18							
886	*	JUN. CONTROL FLAG								
887	9781101	1000	17							
888	*	INITIAL COND.								
889	9781201	4	17.7	120.	0.9284	0.	2			
890	9781202	3	17.7	120.	0.0	0.	18			
891	*	JUN. INITIAL COND.								
892	9781300	1								
893	9781301	0.0	0.0	0.0	17					
894	*	SPARGER EXIT								
895	9790000	"EXIT" SNGLJUN								
896	9790101	978010000	980000000	0.0	1.0	1.0	1100			
897	9790201	1	0.	0.						
898	*	QUENCH TANK								
899	*									
900	*	WATER VOL.								
901	9800000	"QT. WATER" SNGLVOL								
902	9800101	260.4706	5.6667	0.0	0.0	90.	5.6667	0.003	0.0	01
903	9800200	3	17.7	120.						
904	*	INTERFACE								
905	9810000	"INTERFACE" SNGLJUN								
906	9810101	980010000	982000000	0.0	0.0	0.0	1000			
907	9810201	1	0.0	0.0	0.0					
908	*	AIR VOLUME								
909	9820000	"QT. AIR" SNGLVOL								
910	9820101	260.4706	1.2439	0.0	0.0	90.	1.2439	0.003	0.0	01
911	9820200	4	17.7	120.	0.9284					
912	*									
913	*	RUPTURE DISC								
914	9830000	"RUP. DISC" VALVE								
915	9830101	982010000	998000000	1.77	0.	0.	1100			
916	9830201	1	0.	0.	0.					
917	9830300	TRPVLV								
918	9830301	515	*	VALVE OPENING TRIP						
919	*									
920	*									
921	*	*****								
922	*	PIPE OUTSIDE ENVIROMENT								
923	*	*****								
924	*									
925	*									
926	9990000	"ATMOSPHERE" TMDPVOL								

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 The logo for Teledyne Engineering Services, featuring a stylized starburst or leaf-like symbol to the left of the text "TELEDYNE ENGINEERING SERVICES" which is arranged in two lines.

927	9990101	10000.	10000.	0.0	0.0	0.0	0.0	0.00001	0.0	11
928	9990200	4								
929	9990201	0.0	17.7	120.	0.9284					
930	*									
931	*									
932	*****									
933	* PLOT CARDS									
934	*****									
935	*									
936	*									
937	*									
938	20300100	MFLOWJ	410000000							
939	20300200	MFLOWJ	510000000							
940	20300300	MFLOWJ	610000000							
941	20300400	MFLOWJ	402000000							
942	20300500	MFLOWJ	811140000							
943	20300600	MFLOWJ	811570000							
944	20300700	MFLOWJ	308000000							
945	20300800	MFLOWJ	208000000							
946	20300900	MFLOWJ	108000000							
947	*									
948	20301000	QUALS	411010000							
949	20301100	QUALS	511010000							
950	20301200	QUALS	611010000							
951	20301300	QUALS	409240000							
952	20301400	QUALS	509100000							
953	20301500	QUALS	609090000							
954	20301600	QUALS	401280000							
955	20301700	QUALS	811140000							
956	20301800	QUALS	811570000							
957	20301900	QUALS	307010000							
958	20302000	QUALS	307180000							
959	20302100	QUALS	207010000							
960	20302200	QUALS	207260000							
961	20302300	QUALS	107010000							
962	20302400	QUALS	107330000							
963	*									
964	20302500	P	411010000							
965	20302600	P	511010000							
966	20302700	P	611010000							
967	20302800	P	409240000							
968	20302900	P	509100000							
969	20303000	P	609090000							
970	20303100	P	401280000							
971	20303200	P	811140000							
972	20303200	P	811570000							
	CARD ABOVE IS REPLACEMENT CARD.									
973	20303400	P	307010000							
974	20303500	P	307180000							
975	20303600	P	207010000							
976	20303700	P	207260000							
977	20303800	P	107010000							
978	20303900	P	107330000							
979	*									
980	*									
981	*									
982	*									
983	END OF CASE									

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10/10/20



Technical Report
TR-5364-1
Revision 0

4-439

 **TELEDYNE**
ENGINEERING SERVICES

4.9.2 Condensate/Steam Restart

LISTING OF INPUT DATA FOR CASE 1

```

1 =THIS RESTARTS RELAP,3PORVS OPENING ON LOOPSEALS UP/DWN 2 ARCS
2 *
3 100 RESTART TRANSNT
4 101 RUN
5 *
6 103 1102
7 104 NOACTION
8 201 0.600 1.-7 2.-4 11001 5 50 250
9 *
10 * MINOR EDITS
11 *
12 301 MFLOWJ 41000000
13 302 MFLOWJ 51000000
14 303 MFLOWJ 61000000
15 304 MFLOWJ 40200000
16 305 MFLOWJ 811140000
17 306 MFLOWJ 811570000
18 307 MFLOWJ 308000000
19 308 MFLOWJ 208000000
20 309 MFLOWJ 108000000
21 *
22 310 QUALS 411010000
23 311 QUALS 511010000
24 312 QUALS 611010000
25 313 QUALS 409260000
26 314 QUALS 509120000
27 315 QUALS 609110000
28 316 QUALS 401280000
29 317 QUALS 811140000
30 318 QUALS 811570000
31 319 QUALS 307010000
32 320 QUALS 307180000
33 321 QUALS 207010000
34 322 QUALS 207260000
35 323 QUALS 107010000
36 324 QUALS 107330000
37 *
38 325 P 411010000
39 326 P 511010000
40 327 P 611010000
41 328 P 409260000
42 329 P 509120000
43 330 P 609110000
44 331 P 401280000
45 332 P 811140000
46 333 P 811570000
47 334 P 307010000
48 335 P 307180000
49 336 P 207010000
50 337 P 207260000
51 338 P 107010000
52 339 P 107330000
53 *
54 *
55 *
56 400000 "PORV" SNGLJUN

```

BY CUM DATE 4-14-83

CHKD. BY JRM DATE 4-20-83

Technical Report
TR-5364-1
Revision 0

4-440

TELEDYNE
ENGINEERING SERVICES




```

57 4000101 399000000 401000000 0.0 0.0 0.0 1100
58 4000201 1 0.0 0.0 0.0
59 *****
60 * FORCE CARDS FOR REPIPE *
61 *****
62 *
63 *****
64 * THIS RELAP RUN INCLUDES ENTIRE ARCS 1 AND 3, PORV UPSTREAM AND
65 * DOWN AS WELL AS THE MAIN HEADER AND SOME DISCHARGE PIPING
66 *****
67 *
68 *
69 *****ARC-1*****
70 *
71 *
72 2001 5,247,509110000,509120000,609100000,107040000
73 2002 107050000,107060000,107070000,107080000,107090000
74 2003 107100000,107110000,107120000,107130000,107140000
75 2004 107150000,107160000,107170000,107180000,107190000
76 2005 107200000,107210000,107220000,107230000,107240000
77 2006 107250000,107260000,107270000,107280000,107290000
78 2007 107300000,107310000,107320000,107330000
79 *
80 *
81 *****ARC-2*****
82 *
83 *
84 *
85 *
86 *****ARC-3*****
87 *
88 *
89 2014 609110000,409250000,409260000,307040000
90 2015 307050000,307060000,307070000,307080000,307090000
91 2016 307100000,307110000,307120000,307130000,307140000
92 2017 307150000,307160000,307170000,307180000
93 *
94 *
95 *
96 *
97 *** PORV'S DOWNSTREAM ***
98 *
99 *
100 *
101 2046 611010000,611020000,611030000,611040000,611050000
102 2047 611060000,611070000,611080000,611090000,611100000
103 2048 611110000,611120000,611130000,611140000,611150000
104 2049 611160000,611170000,611180000,611190000,611200000
105 2050 611210000,611220000,611230000,611240000,611250000
106 2051 611260000,611270000,611280000,611290000,611300000
107 2052 611310000,611320000,611330000,611340000,611350000
108 2053 611360000,611370000,611380000,611390000,611400000
109 2054 611410000,611420000,611430000,611440000,611450000
110 2055 611460000,611470000,611480000,611490000,611500000
111 2056 611510000,611520000,611530000,611540000,611550000
112 2057 611560000,611570000,611580000,611590000,611600000
113 2058 703010000
114 *

```



```

115 *
116 *****MAIN DISCHARGE LINE*****
117 *
118 *
119 2018 703020000,703030000,703040000,703050000,703060000
120 2019 703070000,703080000,703090000,703100000,703110000
121 2020 703120000,703130000,703140000,801010000,803010000
122 2021 805010000,807010000
123 2022 809010000,811010000,811020000,811030000,811040000
124 2023 811050000,811060000,811070000,811080000,811090000
125 2024 811100000,811110000,811120000,811130000,811140000
126 2025 811150000,811160000,811170000,811180000,811190000
127 2026 811200000,811210000,811220000,811230000,811240000
128 2027 811250000,811260000,811270000

```

129 *

130 *

131 *** PORV UPSTREAM ***

132 *

133 *

134 2028 399010000,401010000,401020000,401030000,401040000

135 2029 401050000,401060000,401070000,401080000,401090000

136 2030 401100000,401110000,401120000,401130000,401140000

137 2031 401150000,401160000,401170000,401180000,401190000

138 2032 401200000,401210000,401220000,401230000,401240000

139 2033 401250000,401260000,401270000,401280000,403010000

140 2034 405010000,405020000,405030000,405040000,405050000

141 2035 405060000,405070000,405080000,405090000,405100000

142 2036 405110000,405120000,405130000,405140000,405150000

143 2037 405160000,407010000,409010000,409020000,409030000

144 2038 409040000,409050000,409060000,409070000,409080000

145 2039 409090000,409100000,409110000,409120000,409130000

146 2040 409140000,409150000,409160000,409170000,409180000

147 2041 409190000,409200000,409210000,409220000,409230000

148 2042 409240000,609010000,609020000,609030000,609040000

149 2043 609050000,609060000,609070000,609080000,609090000

150 2044 509010000,509020000,509030000,509040000,509050000

151 2045 509060000,509070000,509080000,509090000,509100000

152 *

153 *

154 *****

155 * PLOT CARDS *

156 *****

157 *

158 *

159 *

160 20300100 MFLOWJ 410000000

161 20300200 MFLOWJ 510000000

162 20300300 MFLOWJ 610000000

163 20300400 MFLOWJ 402000000

164 20300500 MFLOWJ 811140000

165 20300600 MFLOWJ 811570000

166 20300700 MFLOWJ 308000000

167 20300800 MFLOWJ 208000000

168 20300900 MFLOWJ 108000000

169 *

170 20301000 QUALS 411010000

171 20301100 QUALS 511010000

172 20301200 QUALS 811010000

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173	20301300	QUALS	409240000
174	20301400	QUALS	509100000
175	20301500	QUALS	609090000
176	20301600	QUALS	401280000
177	20301700	QUALS	811140000
178	20301800	QUALS	811570000
179	20301900	QUALS	307010000
180	20302000	QUALS	307180000
181	20302100	QUALS	207010000
182	20302200	QUALS	207260000
183	20302300	QUALS	107010000
184	20302400	QUALS	107330000
185	*		
188	20302500	P	411010000
187	20302600	P	511010000
188	20302700	P	811010000
189	20302800	P	409240000
190	20302900	P	509100000
191	20303000	P	609090000
192	20303100	P	401280000
193	20303200	P	811140000
194	20303300	P	811570000
195	20303400	P	307010000
198	20303500	P	307180000
197	20303600	P	207010000
198	20303700	P	207260000
199	20303800	P	107010000
200	20303900	P	107330000
201	↑		
202	*		
203	↑		
204	*		
205	↑		

END OF CASE



LISTING OF INPUT DATA FOR CASE 1

```

1  =THIS RESTARTS RELAP,3PORVS OPENING ON LOOPSEALS UP/DWN 2 ARCS
2  *
3  100 RESTART TRANSNT
4  101 RUN
5  *
6  103 3791
7  104 NOACTION
8  201 1.0 1.-7 2.-4 11001 5 50 250
9  *
10 * MINOR EDITS
11 *
12 301 MFLOWJ 41000000
13 302 MFLOWJ 51000000
14 303 MFLOWJ 61000000
15 304 MFLOWJ 40200000
16 305 MFLOWJ 811140000
17 306 MFLOWJ 811570000
18 307 MFLOWJ 308000000
19 308 MFLOWJ 208000000
20 309 MFLOWJ 108000000
21 *
22 310 QUALS 411010000
23 311 QUALS 511010000
24 312 QUALS 611010000
25 313 QUALS 409260000
26 314 QUALS 509120000
27 315 QUALS 609110000
28 316 QUALS 401280000
29 317 QUALS 811140000
30 318 QUALS 811570000
31 319 QUALS 307010000
32 320 QUALS 307180000
33 321 QUALS 207010000
34 322 QUALS 207260000
35 323 QUALS 107010000
36 324 QUALS 107330000
37 *
38 325 P 411010000
39 326 P 511010000
40 327 P 611010000
41 328 P 409260000
42 329 P 509120000
43 330 P 609110000
44 331 P 401280000
45 332 P 811140000
46 333 P 811570000
47 334 P 307010000
48 335 P 307180000
49 336 P 207010000
50 337 P 207260000
51 338 P 107010000
52 339 P 107330000
53 *
54 *
55 *
56 4000000 "PORV" SNGLJUN

```

BY CMY DATE 4-14-83CHKD. BY JRM DATE 4-20-83

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57 4000101 399000000 401000000 0.0 0.0 0.0 1100

58 4000201 1.0 0.0 0.0 0.0

59 *****

60 * FORCE CARDS FOR REPIPE *

61 *****

62 *

63 *****

64 * THIS RELAP RUN INCLUDES ENTIRE ARCS 1 AND 3, PORV UPSTREAM AND

65 * DOWN AS WELL AS THE MAIN HEADER AND SOME DISCHARGE PIPING

66 *****

67 *

68 *

69 *****ARC-1*****

70 *

71 *

72 2001 5,247,509110000,509120000,609100000,107040000

73 2002 107050000,107060000,107070000,107080000,107090000

74 2003 107100000,107110000,107120000,107130000,107140000

75 2004 107150000,107160000,107170000,107180000,107190000

76 2005 107200000,107210000,107220000,107230000,107240000

77 2006 107250000,107260000,107270000,107280000,107290000

78 2007 107300000,107310000,107320000,107330000

79 *****

80 *

81 *****ARC-2*****

82 *

83 *

84 *

85 *

86 *****ARC-3*****

87 *

88 *

89 2014 609110000,409250000,409260000,307040000

90 2015 307050000,307060000,307070000,307080000,307090000

91 2016 307100000,307110000,307120000,307130000,307140000

92 2017 307150000,307160000,307170000,307180000

93 *****

94 *

95 *

96 *

97 *** PORV'S DOWNSTREAM ***

98 *

99 *

100 *

101 2046 611010000,611020000,611030000,611040000,611050000

102 2047 611060000,611070000,611080000,611090000,611100000

103 2048 611110000,611120000,611130000,611140000,611150000

104 2049 611160000,611170000,611180000,611190000,611200000

105 2050 611210000,611220000,611230000,611240000,611250000

106 2051 611260000,611270000,611280000,611290000,611300000

107 2052 611310000,611320000,611330000,611340000,611350000

108 2053 611360000,611370000,611380000,611390000,611400000

109 2054 611410000,611420000,611430000,611440000,611450000

110 2055 611460000,611470000,611480000,611490000,611500000

111 2056 611510000,611520000,611530000,611540000,611550000

112 2057 611560000,611570000,611580000,611590000,701010000

113 2058 703010000

114 *

115	*								
116	*****	MAIN DISCHARGE LINE	*****						
117	*								
118	*								
119	2018	703020000	703030000	703040000	703050000	703060000			
120	2019	703070000	703080000	703090000	703100000	703110000			
121	2020	703120000	703130000	703140000	801010000	803010000			
122	2021	805010000	807010000						
123	2022	809010000	811010000	811020000	811030000	811040000			
124	2023	811050000	811060000	811070000	811080000	811090000			
125	2024	811100000	811110000	811120000	811130000	811140000			
126	2025	811150000	811160000	811170000	811180000	811190000			
127	2026	811200000	811210000	811220000	811230000	811240000			
128	2027	811250000	811260000	811270000					
129	*								
130	*								
131	***	PORV UPSTREAM	***						
132	*								
133	*								
134	2028	399010000	401010000	401020000	401030000	401040000			
135	2029	401050000	401060000	401070000	401080000	401090000			
136	2030	401100000	401110000	401120000	401130000	401140000			
137	2031	401150000	401160000	401170000	401180000	401190000			
138	2032	401200000	401210000	401220000	401230000	401240000			
139	2033	401250000	401260000	401270000	401280000	403010000			
140	2034	405010000	405020000	405030000	405040000	405050000			
141	2035	405060000	405070000	405080000	405090000	405100000			
142	2036	405110000	405120000	405130000	405140000	405150000			
143	2037	405160000	407010000	409010000	409020000	409030000			
144	2038	409040000	409050000	409060000	409070000	409080000			
145	2039	409090000	409100000	409110000	409120000	409130000			
146	2040	409140000	409150000	409160000	409170000	409180000			
147	2041	409190000	409200000	409210000	409220000	409230000			
148	2042	409240000	609010000	609020000	609030000	609040000			
149	2043	609050000	609060000	609070000	609080000	609090000			
150	2044	509010000	509020000	509030000	509040000	509050000			
151	2045	509060000	509070000	509080000	509090000	509100000			
152	*								
153	*								
154	*****								
155	*	PLOT CARDS							
156	*****								
157	*								
158	*								
159	*								
160	20300100	MFLOWJ	410000000						
161	20300200	MFLOWJ	510000000						
162	20300300	MFLOWJ	610000000						
163	20300400	MFLOWJ	402000000						
164	20300500	MFLOWJ	811140000						
165	20300600	MFLOWJ	811570000						
166	20300700	MFLOWJ	308000000						
167	20300800	MFLOWJ	208000000						
168	20300900	MFLOWJ	108000000						
169	*								
170	20301000	QUALS	411010000						
171	20301100	QUALS	511010000						
172	20301200	QUALS	811010000						

173	20301300	QUALS	409240000
174	20301400	QUALS	509100000
175	20301500	QUALS	609090000
176	20301600	QUALS	401280000
177	20301700	QUALS	811140000
178	20301800	QUALS	811570000
179	20301900	QUALS	307010000
180	20302000	QUALS	307180000
181	20302100	QUALS	207010000
182	20302200	QUALS	207260000
183	20302300	QUALS	107010000
184	20302400	QUALS	107330000
185	*		
186	20302500	P	411010000
187	20302600	P	511010000
188	20302700	P	611010000
189	20302800	P	409240000
190	20302900	P	509100000
191	20303000	P	609090000
192	20303100	P	401280000
193	20303200	P	811140000
194	20303300	P	811570000
195	20303400	P	307010000
196	20303500	P	307180000
197	20303600	P	207010000
198	20303700	P	207260000
199	20303800	P	107010000
200	20303900	P	107330000
201	*		
202	*		
203	*		
204	*		
205	. END OF CASE		

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Technical Report
TR-5364-1
Revision 0

4.9.3 PORV Solid 400^o Liquid



LISTING OF INPUT DATA FOR CASE 1

```

1  =D.C.COOK UNIT1 PORV OPEN
2  *
3  * DISCHARGE PIPING
4  * THIS IS THE NUMBERING SYSTEM FOR UNIT1'S RELAP MODEL
5  * WHERE COMPONENTS NUMBERED IN THE:
6  *   100'S ARE VALVE SV-45C AND ARC 1 LEVEL 669'-2"
7  *   200'S ARE VALVE SV-45B AND ARC 2 LEVEL 670'-10"
8  *   300'S ARE VALVE SV-45A AND ARC 3 LEVEL 672'-8"
9  *   400'S ARE PORV NRV-151 AND ARC "A"
10 *   500'S ARE PORV NRV-153 AND ARC "B"
11 *   600'S ARE PORV NRV-152 AND ARC "C"
12 *   700'S AND 800'S ARE 6" AND 12" MAIN DISCHARGE PIPING
13 *   900'S QUENCH TANK PORTION
14 *   999 ATMOSPHERE
15 *
16 *
17 *
18 100 NEW TRANSNT
19 101 RUN
20 102 BRITISH BRITISH
21 104 NOACTION
22 *
23 *****
24 * TIME STEP CONTROL *
25 *****
26 *
27 201 0.200,1.-7,2.-4,11001,5,50,250
28 *
29 *
30 *****
31 * MINOR EDITS *
32 *****
33 *
34 301 MFLOWJ 41000000
35 302 MFLOWJ 51000000
36 303 MFLOWJ 61000000
37 304 MFLOWJ 40200000
38 305 MFLOWJ 811140000
39 306 MFLOWJ 811570000
40 307 MFLOWJ 308000000
41 308 MFLOWJ 208000000
42 309 MFLOWJ 108000000
43 *
44 310 QUALS 411010000
45 311 QUALS 511010000
46 312 QUALS 611010000
47 313 QUALS 409260000
48 314 QUALS 509120000
49 315 QUALS 609110000
50 316 QUALS 401280000
51 317 QUALS 811140000
52 318 QUALS 811570000
53 319 QUALS 307010000
54 320 QUALS 307180000
55 321 QUALS 207010000
56 322 QUALS 207260000

```

BY CMM DATE 4-21-83
 CHECKED BY KJG DATE 5-20-83

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57	323	QUALS	107010000
58	324	QUALS	107330000
59	*		
60	325	P	411010000
61	326	P	511010000
62	327	P	611010000
63	328	P	409260000
64	329	P	509120000
65	330	P	609110000
66	331	P	401280000
67	332	P	811140000
68	333	P	811570000
69	334	P	307010000
70	335	P	307180000
71	336	P	207010000
72	337	P	207260000
73	338	P	107010000
74	339	P	107330000
75	*		
76	*		
77	*		

78 * FORCE CARDS FOR REPIPE *

79 *****

80 *

81 *****

82 * THIS RELAP RUN INCLUDES ENTIRE ARCS 1 AND 3, PORV UPSTREAM AND

83 * DOWN AS WELL AS THE MAIN HEADER AND SOME DISCHARGE PIPING

84 *****

85 *

86 *

87 *****ARC-1*****

88 *

89 *

90 2001 5,247,509110000,509120000,609100000,107040000

91 2002 107050000,107060000,107070000,107080000,107090000

92 2003 107100000,107110000,107120000,107130000,107140000

93 2004 107150000,107160000,107170000,107180000,107190000

94 2005 107200000,107210000,107220000,107230000,107240000

95 2006 107250000,107260000,107270000,107280000,107290000

96 2007 107300000,107310000,107320000,107330000

97 *

98 *

99 *****ARC-2*****

100 *

101 *

102 *

103 *

104 *****ARC-3*****

105 *

106 *

107 2014 809110000,409250000,409260000,307040000

108 2015 307050000,307060000,307070000,307080000,307090000

109 2016 307100000,307110000,307120000,307130000,307140000

110 2017 307150000,307160000,307170000,307180000

111 *

112 *

113 *

114 *

115	***	PORV'S	DOWNSTREAM	***		
116	*					
117	*					
118	*					
119	2046	611010000	611020000	611030000	611040000	611050000
120	2047	611060000	611070000	611080000	611090000	611100000
121	2048	611110000	611120000	611130000	611140000	611150000
122	2049	611160000	611170000	611180000	611190000	611200000
123	2050	611210000	611220000	611230000	611240000	611250000
124	2051	611260000	611270000	611280000	611290000	611300000
125	2052	611310000	611320000	611330000	611340000	611350000
126	2053	611360000	611370000	611380000	611390000	611400000
127	2054	611410000	611420000	611430000	611440000	611450000
128	2055	611460000	611470000	611480000	611490000	611500000
129	2056	611510000	611520000	611530000	611540000	611550000
130	2057	611560000	611570000	611580000	611590000	611600000
131	2058	703010000				
132	*					
133	*					
134	*****	MAIN DISCHARGE LINE	*****			
135	*					
136	*					
137	2018	703020000	703030000	703040000	703050000	703060000
138	2019	703070000	703080000	703090000	703100000	703110000
139	2020	703120000	703130000	703140000	801010000	803010000
140	2021	805010000	807010000			
141	2022	809010000	811010000	811020000	811030000	811040000
142	2023	811050000	811060000	811070000	811080000	811090000
143	2024	811100000	811110000	811120000	811130000	811140000
144	2025	811150000	811160000	811170000	811180000	811190000
145	2026	811200000	811210000	811220000	811230000	811240000
146	2027	811250000	811260000	811270000		
147	*					
148	*					
149	***	PORV UPSTREAM	***			
150	*					
151	*					
152	2028	399010000	401010000	401020000	401030000	401040000
153	2029	401050000	401060000	401070000	401080000	401090000
154	2030	401100000	401110000	401120000	401130000	401140000
155	2031	401150000	401160000	401170000	401180000	401190000
156	2032	401200000	401210000	401220000	401230000	401240000
157	2033	401250000	401260000	401270000	401280000	403010000
158	2034	405010000	405020000	405030000	405040000	405050000
159	2035	405060000	405070000	405080000	405090000	405100000
160	2036	405110000	405120000	405130000	405140000	405150000
161	2037	405160000	407010000	409010000	409020000	409030000
162	2038	409040000	409050000	409060000	409070000	409080000
163	2039	409090000	409100000	409110000	409120000	409130000
164	2040	409140000	409150000	409160000	409170000	409180000
165	2041	409190000	409200000	409210000	409220000	409230000
166	2042	409240000	609010000	609020000	609030000	609040000
167	2043	609050000	609060000	609070000	609080000	609090000
168	2044	509010000	509020000	509030000	509040000	509050000
169	2045	509060000	509070000	509080000	509090000	509100000
170	*					
171	*					
172	*****					

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```

173 * TRIPS *
174 *****
175 *
176 *
177 501 TIME 0 GE NULL 0 0.0 L * VALVE OPENING TRIP
178 502 TIME 0 GE NULL 0 5.0 L * JOB TERMINATION TRIP
179 515 P 982010000 GE NULL 0 114.7 L * QUENCH TANK RUPTURE PRESS.
180 600 502
181 *

```

```

182 *****
183 *
184 * HYDRODYNAMIC COMPONENTS *
185 * *****
186 *****
187 *

```

```

188 *
189 * PRESSURIZER COMPONENT
190 3990000 "PRESS" TMDPVOL
191 3990101 0.0 20.0 500.0 0.0 0.0 0.0 0.00005 0.0 11
192 3990200 3
193 3990201 0.0 2349.7 400.0 0.8 2420.0 400.0 1.2 2498.7 400.0
194 *

```

```

195 4000000 "PORV" SNGLJUN
196 4000101 399000000 401000000 0.0 0.0 0.0 1100
197 4000201 1 0.0 0.0 0.0
198 *

```

```

199 4010000 "PORV" PIPE
200 4010001 28
201 4010101 0.1465 28
202 4010301 .4375 4
203 4010302 .5104 12
204 4010303 .5 19
205 4010304 .5 27
206 4010305 0.72 28
207 4010401 0.0 28
208 4010601 45 4
209 4010602 90 12
210 4010603 0.0 19
211 4010604 90 27
212 4010605 0.0 28
213 4010801 1.51E-4 0.0 28
214 4010901 0.0 0.0 3
215 4010902 .092 .092 4
216 4010903 0.0 0.0 11
217 4010904 .1836 .1836 12
218 4010905 0.0 0.0 18
219 4010906 .1836 .1836 19
220 4010907 0.0 0.0 28
221 4010908 0.1836 0.1836 27
222 4011001 00 28
223 4011101 1000 27
224 4011201 3 2349.7 400.0 0.0 0.0 28
225 4011300 1
226 4011301 0.0 0.0 0.0 27
227 *

```

```

228 4020000 "PORV" SNGLJUN
229 4020101 401010000 403000000 0.0 0.0 0.0 1000
230 4020201 1 0.0 0.0 0.0

```

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231	*										
232	4030000	"PORV" BRANCH									
233	4030001	0									
234	4030101	0.1465 0.5 0.0 0.0 0.0 0.0 1.51E-4 0.0 00									
235	4030200	3 2349.7 400.0 0.0 0.0 0.0									
236	*										
237	4040000	"PORV" SNGLJUN									
238	4040101	403010000 405000000 0.1465 0.0 0.0 1000									
239	4040201	1 0.0 0.0 0.0									
240	*										
241	4050000	"PORV" PIPE									
242	4050001	16									
243	4050101	0.1465 1									
244	4050102	0.0718 16									
245	4050301	0.698 1									
246	4050302	0.471 7									
247	4050303	0.451 16									
248	4050401	0.0 16									
249	4050601	0.0 16									
250	4050801	1.51E-4 0.0 1									
251	4050802	1.33E-4 0.0 16									
252	4050901	0.0577 0.0981 1									
253	4050902	0.0 0.0 15									
254	4051001	00 16									
255	4051101	1000 15									
256	4051201	3 2349.7 400.0 0.0 0.0 16									
257	4051300	1									
258	4051301	0.0 0.0 0.0 15									
259	*										
260	4060000	"PORV" SNGLJUN									
261	4060101	405010000 407000000 0.0 0.0 0.0 1000									
262	4060201	1 0.0 0.0 0.0									
263	*										
264	4070000	"PORV" BRANCH									
265	4070001	0									
266	4070101	0.0718 0.451 0.0 0.0 0.0 0.0 1.33E-4 0.0 00									
267	4070200	3 2349.7 400.0 0.0 0.0 0.0									
268	*										
269	4080000	"PORV" SNGLJUN									
270	4080101	407010000 409000000 0.0 0.0 0.0 1000									
271	4080201	1 0.0 0.0 0.0									
272	*										
273	4090000	"PORV" PIPE									
274	4090001	28									
275	4090101	0.0718 1									
276	4090102	0.03757 22									
277	4090103	0.03388 23									
278	4090104	0.02650 24									
279	4090105	0.01912 25									
280	4090106	0.01175 26									
281	4090301	0.53 1									
282	4090302	.30 2									
283	4090303	0.493 10									
284	4090304	0.55 14									
285	4090305	0.510 22									
286	4090306	0.255 26									
287	4090401	0.0 28									
288	4090601	0.0 28									



289	4090801	1.33E-4	0.0	1				
290	4090802	1.53E-4	0.0	26				
291	4090901	0.0	0.0	13				
292	4090902	0.585	0.585	14				
293	4090903	0.0	0.0	25				
294	4091001	00	28					
295	4091102	1000	25					
298	4091201	3	2349.7	400.0	0.0	0.0	28	
297	4091300	1						
298	4091301	0.0	0.0	0.0	25			
299	*							
300	4100000	"PORV151"	VALVE					
301	4100101	409010000	411000000	0.00806	0.0	0.0	0100	
302	4100201	1	0.0	0.0	0.0			
303	4100300	MTRVLV						
304	4100301	501	502	1.0	0.0			
305	*							
308	5080000	"PORV"	SNGLJUN					
307	5080101	407010000	509000000	0.0	0.2172	0.2172	1000	
308	5080201	1	0.0	0.0	0.0			
309	*							
310	5090000	"PORV"	PIPE					
311	5090001	12						
312	5090101	0.03757	8					
313	5090102	0.03388	9					
314	5090103	0.02650	10					
315	5090104	0.01912	11					
316	5090105	0.01175	12					
317	5090301	0.4089	2					
318	5090302	0.5078	8					
319	5090303	0.2539	12					
320	5090401	0.0	12					
321	5090601	0.0	12					
322	5090801	1.53E-4	0.0	12				
323	5090901	0.0	0.0	1				
324	5090902	0.2172	0.2172	2				
325	5090903	0.0	0.0	11				
326	5091001	00	12					
327	5091101	1000	11					
328	5091201	3	2349.7	400.0	0.0	0.0	12	
329	5091300	1						
330	5091301	0.0	0.0	0.0	11			
331	*							
332	5100000	"PORV152"	VALVE					
333	5100101	509010000	511000000	0.00806	0.0	0.0	0100	
334	5100201	1	0.0	0.0	0.0			
335	5100300	MTRVLV						
336	5100301	501	502	1.0	0.0			
337	*							
338	6080000	"PORV"	SNGLJUN					
339	6080101	403010000	609000000	0.0	0.1838	0.1838	1000	
340	6080201	1	0.0	0.0	0.0			
341	*							
342	6090000	"PORV"	PIPE					
343	6090001	11						
344	6090101	0.03757	7					
345	6090102	0.03388	8					
346	6090103	0.02650	9					

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TELEDYNE
ENGINEERING SERVICES



347	6090104	0.01912	10						
348	6090105	0.01175	11						
349	8090301	0.4089	2						
350	6090302	0.5699	7						
351	6090303	.2850	11						
352	6090401	0.0	11						
353	8090601	0.0	11						
354	6090801	1.53E-4	0.0	11					
355	6090901	0.0	0.0	1					
356	6090902	0.2172	0.2172	2					
357	6090903	0.0	0.0	10					
358	6091001	00	11						
359	6091101	1000	10						
360	6091201	3	2349.7	400.0	0.0	0.0	11		
361	6091300	1							
362	6091301	0.0	0.0	0.0	10				
363	*								
364	6100000	"PORV153"	VALVE						
365	6100101	609010000	611000000	0.00808	0.0	0.0	0100		
366	6100201	1	0.0	0.0	0.0				
367	6100300	MTRVLV							
368	6100301	501	502	1.0	0.0				
369	*								
370	*								
371	*	VALVE	DOWNSTREAM	PIPING					
372	1070000	"DWNSTRM#1"	PIPE						
373	1070001	33							
374	*								
375	1070101	0.20069	33						
376	*								
377	1070301	0.5281	4						
378	1070302	0.9943	15						
379	1070303	0.9132	21						
380	1070304	0.8472	30						
381	1070305	1.085	33						
382	*								
383	1070401	0.0	33						
384	*								
385	1070601	0.0	4						
386	1070602	-90	15						
387	1070603	0.0	33						
388	*								
389	1070801	1.52-4	0.	33					
390	1070901	0.0	0.0	3					
391	1070902	0.18	0.18	4					
392	1070903	0.0	0.0	14					
393	1070904	0.18	0.18	15					
394	1070905	0.0	0.0	32					
395	*								
396	1071001	00	33						
397	1071101	1000	32						
398	*								
399	1071201	4	17.7	120.	0.9284	0.	33		
400	*								
401	1071300	1							
402	1071301	0.0	0.0	0.0	32				
403	*								
404	*								



405	*								
406	*								
407	*								
408	*								
409	*	VALVE DOWNSTREAM PIPING							
410	*	207000	"DNSTRM#2"	PIPE					
411	*								
412	*	207001			28				
413	*	2070101	0.20069		28				
414	*								
415	*	2070301	0.5261		4				
416	*	2070302	0.9271		14				
417	*	2070303	0.8852		23				
418	*	2070304	1.085		28				
419	*								
420	*	2070401	0.0		26				
421	*								
422	*	2070601	0.0		4				
423	*	2070602	-90.		14				
424	*	2070603	0.0		26				
425	*								
426	*	2070801	1.52-4	0.	26				
427	*								
428	*	2070901	0.0	0.0	3				
429	*	2070902	0.18	0.18	4				
430	*	2070903	0.0	0.0	13				
431	*	2070904	0.18	0.18	14				
432	*	2070905	0.0	0.0	25				
433	*								
434	*	2071001	00		26				
435	*								
436	*	2071101	1000		25				
437	*								
438	*	2071201	4	17.7	120.	0.9284	0.	26	
439	*								
440	*	2071300	1						
441	*	2071301	0.0	0.0	0.0	25			
442	*								
443	*								
444	*								
445	*								
446	*								
447	*	VALVE DOWNSTREAM PIPING							
448	*	3070000	"DNSTRM#3"	PIPE					
449	*	3070001	18						
450	*	3070101	0.20069		18				
451	*								
452	*	3070301	0.5261		4				
453	*	3070302	1.0339		12				
454	*	3070303	0.801		15				
455	*	3070304	1.085		18				
456	*								
457	*	3070401	0.0		18				
458	*								
459	*	3070601	0.0		4				
460	*	3070602	-90.		12				
461	*	3070603	0.0		18				
462	*								

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463	3070801	1.52-4	0.	18			
464	*						
465	3070901	0.0	0.0	3			
466	3070902	0.18	0.18	4			
467	3070903	0.0	0.0	11			
468	3070904	0.18	0.18	12			
469	3070905	0.0	0.0	17			
470	*						
471	3071001	00	18				
472	3071101	1000	17				
473	*						
474	3071201	4	17.7	120.	0.9284	0.	18
475	*						
476	3071300	1					
477	3071301	0.0	0.0	0.0			17
478	*						
479	*						
480	*****						
481	* PORV DISCHARGE SECTION *						
482	*****						
483	*						
484	*						
485	*****						
486	* PORV NRV-151 DISCHARGE LINE ARC "A" *						
487	*****						
488	*						
489	*						
490	4110000	"PORV1"	PIPE				
491	4110001	19					
492	*						
493	4110101	0.05132	17				
494	4110102	0.20069	19				
495	*						
496	4110301	0.3724	4				
497	4110302	0.3802	8				
498	4110303	0.581	17				
499	4110304	0.349	19				
500	*						
501	4110401	0.0	19				
502	*						
503	4110601	0.0	4				
504	4110602	-90.	8				
505	4110603	0.0	19				
506	*						
507	4110801	1.53-4	0	17			
508	4110802	1.52-4	0	19			
509	*						
510	4110901	0.0	0.0	3			
511	4110902	0.2088	0.2088	4			
512	4110903	0.0	0.0	7			
513	4110904	0.2088	0.2088	8			
514	4110905	0.0	0.0	16			
515	4110906	0.3784	0.1565	17			
516	4110907	0.0	0.0	18			
517	*						
518	4111001	00	19				
519	4111101	1000	18				
520	*						

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521	4111201	4	17.7	120.	0.9284	0.0	19
522	*						
523	4111300	1					
524	4111301	0.0	0.0	0.0	18		
525	*						
526	4120000	"ENTERMAIN"	SNGLJUN				
527	4120101	411010000	701000000	0.0	0.1800	0.1800	1100
528	4120201	1	0.0	0.0	0.0		
529	*						
530	*						
531	*****						
532	*	PORV NRV-153 DISCHARGE LINE ARC "B"					*
533	*****						
534	*						
535	*						
536	*						
537	5110000	"PORV2LINE"	PIPE				
538	5110001		19				
539	*						
540	5110101	0.05132	18				
541	5110102	0.08840	19				
542	*						
543	5110301	0.4303	3				
544	5110302	0.3620	7				
545	5110303	0.3529	9				
546	5110304	0.6058	18				
547	5110305	0.371	19				
548	*						
549	5110401	0.0	19				
550	*						
551	5110601	0.0	3				
552	5110602	-90.	7				
553	5110603	0.0	19				
554	*						
555	5110801	1.53-4	0 18				
556	5110802	1.34-4	0 19				
557	*						
558	5110901	0.0	0.0	2			
559	5110902	0.2088	0.2088	3			
560	5110903	0.0	0.0	8			
561	5110904	0.2088	0.2088	7			
562	5110905	0.0	0.0	17			
563	5110906	0.0544	0.0399	18			
564	*						
565	5111001	00	19				
566	*						
567	5111101	1000	18				
568	*						
569	5111201	4	17.7	120.	0.9284	0.0	19
570	*						
571	5111300	1					
572	5111301	0.0	0.0	0.0	18		
573	*						
574	5120000	"JUNC."	SNGLJUN				
575	5120101	511010000	513000000	0.0	0.0	0.0	1000
576	5120201	1	0.0	0.0	0.0		
577	*						
578	*						



579	*										
580	5130000	"4X4X3TEE"	BRANCH								
581	5130001	0									
582	5130101	0.08840	0.3524	0.0	0.0	0.0	0.0	1.34-4	0.0	00	
583	5130200	4	17.7	120.	0.9284	0.0	0.0				
584	*										
585	*										
586	5140000	"4IN JUNC"	SNGLJUN								
587	5140101	513010000	515000000	0.0	0.0	0.0	0.0	1000			
588	5140201	1	0.0	0.0	0.0						
589	*										
590	5150000	"4INSCH40"	PIPE								
591	5150001		12								
592	*										
593	5150101	0.0884	10								
594	5150102	0.20069	12								
595	*										
596	5150301	0.3524	1								
597	5150302	0.6963	10								
598	5150303	0.349	12								
599	*										
600	5150401	0.0	12								
601	*										
602	5150601	0.0	12								
603	*										
604	5150801	1.34-4	0.0	10							
605	5150802	1.52-4	0.0	12							
606	*										
607	5150901	0.0	0.0	9							
608	5150902	0.1483	0.0815	10							
609	5150903	0.0	0.0	11							
610	*										
611	5151001	00	12								
612	*										
613	5151101	1000	11								
614	*										
615	5151201	4	17.7	120.	0.9284	0.0	12				
616	*										
617	5151300	1									
618	5151301	0.0	0.0	0.0	11						
619	*										
620	5160000	"ENTERMAIN"	SNGLJUN								
621	5160101	515010000	701000000	0.0	0.0	0.0	1000				
622	5160201	1	0.0	0.0	0.0						
623	*										
624	*										
625	*****										
626	*	PORV NRV-152 DISCHARGE LINE ARC "C"								*	
627	*****										
628	*										
629	*										
630	*										
631	6110000	"PORVDISC3"	PIPE								
632	6110001		8								
633	*										
634	6110101	0.05132	8								
635	*										
636	6110301	0.3723	4								

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637	6110302	0.3846	8						
638	*								
639	6110401	0.0	8						
640	*								
641	6110601	0.0	4						
642	6110602	-90.	8						
643	*								
644	6110801	1.53-4	0.8						
645	*								
646	6110901	0.0	0.0	3					
647	6110902	0.211	0.211	4					
648	6110903	0.0	0.0	7					
649	*								
650	6111001	00	8						
651	6111101	1000	7						
652	*								
653	6111201	4	17.7	120.	0.9284	0.0	8		
654	*								
655	6111300	1							
656	6111301	0.0	0.0	0.0	7				
657	*								
658	6120000	"PORVLINE"	SNGLJUN						
659	6120101	611010000	513000000	0.0	0.0	0.0	1000		
660	6120201	1	0.0	0.0	0.0				
661	*								
662	*****								
663	* MAIN DISCHARGE LINE SECTION								
664	*****								
665	*								
666	*								
667	* MAIN DISCHARGE LINE								
668	7010000	"ENTERMAIN"	BRANCH						
669	7010001	0							
670	7010101	0.20069	0.7035	0.0	0.0	0.0	0.0	1.52-4	0.0
671	7010200	4	17.7	120.	0.9284	0.0	0.0		
672	*								
673	7020000	"MAINLINE"	SNGLJUN						
674	7020101	701010000	703000000	0.0	0.0	0.0	1000		
675	7020201	1	0.0	0.0	0.0				
676	*								
677	7030000	"MAINLINE"	PIPE						
678	*								
679	7030001	14							
680	*								
681	7030101	0.20069	12						
682	7030102	0.77708	14						* 12 IN LINE STARTS HERE
683	*								
684	7030301	0.7035	1						
685	7030302	1.0076	12						
686	7030303	0.5834	14						* 12 IN LINE STARTS HERE
687	*								
688	7030401	0.0	14						
689	*								
690	7030501	0.0	1						
691	7030602	-90.	14						
692	*								
693	7030801	1.52-4	0.	12					
694	7030802	1.69-4	0.	14					

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695	*									
696	7030901	0.180	0.180	1						
697	7030902	0.0	0.0	11						
698	7030903	0.493	0.2045	12						
699	7030904	0.0	0.0	13						
700	*									
701	7031001	00	14							
702	7031101	1000	13							
703	*									
704	7031201	4	17.7	120.	0.9284	0.0	14			
705	*									
706	7031300	1								
707	7031301	0.0	0.0	0.0	13					
708	*									
709	*									
710	7040000	"MAINLINE"	SNGLJUN							
711	7040101	703010000	801000000	0.0	0.0	0.0	1000			
712	7040201	1	0.0	0.0	0.0					
713	*									
714	3080000	"CON.1"	SNGLJUN							
715	3080101	307010000	801000000	0.0	0.1560	0.1560	1000			
716	3080201	1	0.0	0.0	0.0					
717	*									
718	*									
719	*									
720	*									
721	*									
722	*	CONNECTION TO MAIN LINE AT ELEV. 672'-8"								
723	*									
724	*									
725	8010000	"12-BRANC1"	BRANCH							
726	8010001	0								
727	8010101	0.77708	0.8334	0.0	0.0	-90.	-0.8334	1.69-4	0.0	00
728	8010200	4	17.7	120.	0.9284	0.0	0.0			
729	*									
730	8020000	"MAINLINE"	SNGLJUN							
731	8020101	801010000	803000000	0.0	0.0	0.0	1000			
732	8020201	1	0.0	0.0	0.0					
733	*									
734	8030000	"MAINLINE"	SNGLVOL							
735	8030101	0.77708	0.8334	0.0	0.0	-90.	-0.8334	1.69-4	0.0	00
736	8030200	4	17.7	120.	0.9284	0.0	0.0			
737	*									
738	*	CONNECTION TO MAIN LINE AT ELEV. 670'-10"								
739	*									
740	*									
741	8040000	"MAINLINE"	SNGLJUN							
742	8040101	803010000	805000000	0.0	0.0	0.0	1000			
743	8040201	1	0.0	0.0	0.0					
744	*									
745	2080000	"CON.2"	SNGLJUN							
746	2080101	207010000	805000000	0.0	0.1560	0.1560	1000			
747	2080201	1	0.0	0.0	0.0					
748	*									
749	8050000	"MAINBR.3"	BRANCH							
750	8050001	0								
751	8050101	0.77708	0.8334	0.0	0.0	-90.	-0.8334	1.69-4	0.0	00
752	8050200	4	17.7	120.	0.9284	0.0	0.0			

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753	*																			
754	8060000	"MAINLINE"	SNGLJUN																	
755	8060101	805010000	807000000	0.0	0.0	0.0	1000													
756	8060201	1	0.0	0.0	0.0															
757	*																			
758	8070000	"MAINLINE"	SNGLVOL																	
759	8070101	0.77708	0.8334	0.0	0.0	-90.	-0.8334	1.69-4	0.0	00										
760	8070200	4	17.7	120.	0.9284	0.0	0.0													
761	*																			
762	*																			
763	*	CONNECTION TO MAIN LINE AT ELEV. 669'-2"																		
764	*																			
765	*																			
766	*																			
767	8080000	"MAINLINE"	SNGLJUN																	
768	8080101	807010000	809000000	0.0	0.0	0.0	1000													
769	8080201	1	0.0	0.0	0.0															
770	*																			
771	1080000	"CON.3"	SNGLJUN																	
772	1080101	107010000	809000000	0.0	0.1560	0.1560	1000													
773	1080201	1	0.0	0.0	0.0															
774	*																			
775	8090000	"MAINBR4"	BRANCH																	
776	8090001	0																		
777	8090101	0.77708	0.8334	0.0	0.0	-90.	-0.8334	1.69-4	0.0	00										
778	8090200	4	17.7	120.	0.9284	0.0	0.0													
779	*																			
780	8100000	"MAINLINE"	SNGLJUN																	
781	8100101	809010000	811000000	0.0	0.0	0.0	1000													
782	8100201	1	0.0	0.0	0.0															
783	*																			
784	*																			
785	8110000	"MAINLINE"	PIPE																	
786	*																			
787	8110001		97																	
788	*																			
789	8110101	0.77708	97																	
790	*																			
791	8110301	1.0149	14																	
792	8110302	0.5303	18																	
793	8110303	0.5	22																	
794	8110304	0.5303	26																	
795	8110305	0.9908	56																	
796	8110306	0.5	64																	
797	8110307	0.8750	72																	
798	8110308	0.5104	80																	
799	8110309	0.5000	88																	
800	8110310	1.0556	97																	
801	*																			
802	8110401	0.0	97																	
803	*																			
804	8110601	-90.	14																	
805	8110602	-45.	18																	
806	8110603	-90.	22																	
807	8110604	-45.	26																	
808	8110605	-90.	56																	
809	8110606	0.0	80																	
810	8110607	-90.	88																	

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811	8110608	0.0	97						
812	*								
813	8110801	1.69-4	0. 97						
814	*								
815	8110901	0.0	0.0	13					
816	8110902	0.078	0.078	14					
817	8110903	0.0	0.0	17					
818	8110904	0.078	0.078	18					
819	8110905	0.0	0.0	21					
820	8110908	0.078	0.078	22					
821	8110907	0.0	0.0	25					
822	8110908	0.078	0.078	26					
823	8110909	0.0	0.0	55					
824	8110910	0.156	0.156	56					
825	8110911	0.0	0.0	63					
826	8110912	0.026	0.026	64					
827	8110913	0.0	0.0	71					
828	8110914	0.13	0.13	72					
829	8110915	0.0	0.0	79					
830	8110916	0.156	0.156	80					
831	8110917	0.0	0.0	87					
832	8110918	0.156	0.156	88					
833	8110919	0.0	0.0	96					
834	*								
835	8111001	00	97						
836	*								
837	8111101	1000	86						
838	*								
839	8111201	4	17.7 120. 0.9288 0.0	97					
840	*								
841	8111300	1							
842	8111301	0.0 0.0 0.0	98						
843	*								
844	*								
845	8120000	"MAINDISC"	SNGLJUN						
846	8120101	811010000	813000000 0.0 0.156 0.156	1000					
847	8120201	1 0.0 0.0 0.0							
848	*								
849	8130000	"MAINLINE"	PIPE						
850	*								
851	8130001		26						
852	*								
853	8130101	0.77708	26						
854	*								
855	8130301	1.0	14						
856	8130302	0.5	24						
857	8130303	1.20833	26						
858	*								
859	8130401	0.0	26						
860	*								
861	8130601	0.0	24						
862	8130602	-90.	26						
863	*								
864	8130801	1.69-4	0. 26						
865	*								
866	8130901	0.0	0.0	13					
867	8130902	0.156	0.156	14					
868	8130903	0.0	0.0	23					

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869	8130904	0.158	0.158	24				
870	8130905	0.0	0.0	25				
871	*							
872	8131001	00	26					
873	*							
874	8131101	1000	25					
875	*							
876	8131201	4	17.7	120.	0.9284	0.0	28	
877	*							
878	8131300	1						
879	8131301	0.0	0.0	0.0			25	
880	*							
881	*							
882	*							
883	*****							
884	* QUENCH TANK *							
885	*****							
886	*							
887	*							
888	*							
889	9770000	"QTANK-IN"	SNGLJUN					
890	9770101	813010000	978000000	0.	0.	0.	1000	
891	9770201	1	0.	0.	0.			
892	*							
893	* SPARGER 12 IN SCH40 PIPE							
894	*							
895	9780000	"SPARGER"	PIPE					
896	* NO OF VOLUMES							
897	9780001	18						
898	* FLOW AREA							
899	9780101	0.7773	18					
900	* VOL. LENGTHS							
901	9780301	1.125	2					
902	9780302	1.1333	7					
903	9780303	1.0	18					
904	* VOL. VOLS.							
905	9780401	0.0	18					
906	*							
907	* VERTICAL ANGLES							
908	9780601	-90.	7					
909	9780602	0.0	18					
910	* PIPE ROUGHNESS							
911	9780801	1.69-4	0.0	18				
912	* JUNCTION LOSS COEFF.							
913	9780901	0.0	0.0	6				
914	9780902	0.158	0.158	7				
915	9780903	0.0	0.0	17				
916	* VOL. CONTROL FLAG							
917	9781001	00	18					
918	* JUN. CONTROL FLAG							
919	9781101	1000	17					
920	* INITIAL COND.							
921	9781201	4	17.7	120.	0.9284	0.	2	
922	9781202	3	17.7	120.	0.0	0.	18	
923	* JUN. INITIAL COND.							
924	9781300	1						
925	9781301	0.0	0.0	0.0			17	
926	* SPARGER EXIT							



```

927 9790000 "EXIT" SNGLJUN
928 9790101 978010000 980000000 0.0 1.0 1.0 1100
929 9790201 1 0. 0. 0.
930 * QUENCH TANK
931 *
932 * WATER VOL.
933 9800000 "QT. WATER" SNGLVOL
934 9800101 260.4708 5.6667 0.0 0.0 90. 5.6687 0.003 0.0 01
935 9800200 3 17.7 120.
936 * INTERFACE
937 9810000 "INTERFACE" SNGLJUN
938 9810101 980010000 982000000 0.0 0.0 0.0 1000
939 9810201 1 0.0 0.0 0.0
940 * AIR VOLUME
941 9820000 "QT. AIR" SNGLVOL
942 9820101 260.4708 1.2439 0.0 0.0 90. 1.2439 0.003 0.0 01
943 9820200 4 17.7 120. 0.9284
944 *
945 * RUPTURE DISC
946 9830000 "RUP. DISC" VALVE
947 9830101 982010000 999000000 1.77 0. 0. 1100
948 9830201 1 0. 0. 0.
949 9830300 TRPVLV
950 9830301 515 * VALVE OPENING TRIP
951 *
952 *
953 *****
954 * PIPE OUTSIDE ENVIROMENT *
955 *****
956 *
957 *
958 9990000 "ATMOSPHERE" TMDPVOL
959 9990101 10000. 10000. 0.0 0.0 0.0 0.0 .00001 0.0 11
960 9990200 4
961 9990201 0.0 17.7 120. 0.9284
962 *
963 *
964 *****
965 * PLOT CARDS *
966 *****
967 *
968 *
969 *
970 20300100 MFLOWJ 410000000
971 20300200 MFLOWJ 510000000
972 20300300 MFLOWJ 610000000
973 20300400 MFLOWJ 402000000
974 20300500 MFLOWJ 811140000
975 20300600 MFLOWJ 811570000
976 20300700 MFLOWJ 308000000
977 20300800 MFLOWJ 208000000
978 20300900 MFLOWJ 108000000
979 *
980 20301000 QUALS 411010000
981 20301100 QUALS 511010000
982 20301200 QUALS 611010000
983 20301300 QUALS 409240000
984 20301400 QUALS 509100000

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985	20301500	QUALS	609090000
988	20301600	QUALS	401280000
987	20301700	QUALS	811140000
988	20301800	QUALS	811570000
989	20301900	QUALS	307010000
990	20302000	QUALS	307180000
991	20302100	QUALS	207010000
992	20302200	QUALS	207260000
993	20302300	QUALS	107010000
994	20302400	QUALS	107330000

995	*		
998	20302500	P	411010000
997	20302600	P	511010000
998	20302700	P	811010000
999	20302800	P	409240000
1000	20302900	P	509100000
1001	20303000	P	609090000
1002	20303100	P	401280000
1003	20303200	P	811140000
1004	20303200	P	811570000

CARD ABOVE IS REPLACEMENT CARD.

1005	20303400	P	307010000
1008	20303500	P	307180000
1007	20303600	P	207010000
1008	20303700	P	207260000
1009	20303800	P	107010000
1010	20303900	P	107330000

1011	*		
1012	*		
1013	*		
1014	*		

1015 END OF CASE

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Technical Report
TR-5364-1
Revision 0

4-467

 **TELEDYNE
ENGINEERING SERVICES**

4.9.4 PORV Solid 400^o Liquid Restart

LISTING OF INPUT DATA FOR CASE 1

```

1  * THIS RESTARTS RELAP, PORVS OPENING ON LOOPSEALS UP/DWN 2 ARCS
2  *
3  100 RESTART TRANSNT
4  101 RUN
5  *
6  103 1010
7  104 NOACTION
8  201 0.600 1.-7 2.-4 11001 5 50 250
9  *
10 * MINOR EDITS
11 *
12 301 MFLOWJ 41000000
13 302 MFLOWJ 51000000
14 303 MFLOWJ 61000000
15 304 MFLOWJ 40200000
16 305 MFLOWJ 81114000
17 306 MFLOWJ 81157000
18 307 MFLOWJ 30800000
19 308 MFLOWJ 20800000
20 309 MFLOWJ 10800000
21 *
22 310 QUALS 411010000
23 311 QUALS 511010000
24 312 QUALS 811010000
25 313 QUALS 409260000
26 314 QUALS 509120000
27 315 QUALS 609110000
28 316 QUALS 401280000
29 317 QUALS 811140000
30 318 QUALS 811570000
31 319 QUALS 307010000
32 320 QUALS 307180000
33 321 QUALS 207010000
34 322 QUALS 207260000
35 323 QUALS 107010000
36 324 QUALS 107330000
37 *
38 325 P 411010000
39 326 P 511010000
40 327 P 611010000
41 328 P 409260000
42 329 P 509120000
43 330 P 609110000
44 331 P 401280000
45 332 P 811140000
46 333 P 811570000
47 334 P 307010000
48 335 P 307180000
49 336 P 207010000
50 337 P 207260000
51 338 P 107010000
52 339 P 107330000
53 *
54 *
55 *
56 4000000 "PORV" SNGLJUN

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BY CMM DATE 5-13-83
 CHKD. BY KTG DATE 5-13-83

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57 4000101 399000000 401000000 0.0 0.0 0.0 1100
58 4000201 1 0.0 0.0 0.0
59 *****
60 * FORCE CARDS FOR REPIPE *
61 *****
62 *
63 *****
64 * THIS RELAP RUN INCLUDES ENTIRE ARCS 1 AND 3, PORV UPSTREAM AND
65 * DOWN AS WELL AS THE MAIN HEADER AND SOME DISCHARGE PIPING
66 *****
67 *
68 *
69 *****ARC-1*****
70 *
71 *
72 2001 5,247,509110000,509120000,609100000,107040000
73 2002 107050000,107060000,107070000,107080000,107090000
74 2003 107100000,107110000,107120000,107130000,107140000
75 2004 107150000,107160000,107170000,107180000,107190000
76 2005 107200000,107210000,107220000,107230000,107240000
77 2006 107250000,107260000,107270000,107280000,107290000
78 2007 107300000,107310000,107320000,107330000
79 *
80 *
81 *****ARC-2*****
82 *
83 *
84 *
85 *
86 *****ARC-3*****
87 *
88 *
89 2014 609110000,409250000,409260000,307040000
90 2015 307050000,307060000,307070000,307080000,307090000
91 2016 307100000,307110000,307120000,307130000,307140000
92 2017 307150000,307160000,307170000,307180000
93 *
94 *
95 *
96 *
97 *** PORV'S DOWNSTREAM ***
98 *
99 *
100 *
101 2046 611010000,611020000,611030000,611040000,611050000
102 2047 611060000,611070000,611080000,611090000,611100000
103 2048 611100000,611110000,611120000,611130000,611140000
104 2049 611150000,611160000,611170000,611180000,611190000
105 2050 611200000,611210000,611220000,611230000,611240000
106 2051 611250000,611260000,611270000,611280000,611290000
107 2052 611300000,611310000,611320000,611330000,611340000
108 2053 611350000,611360000,611370000,611380000,611390000
109 2054 611400000,611410000,611420000,611430000,611440000
110 2055 611450000,611460000,611470000,611480000,611490000
111 2056 611500000,611510000,611520000,611530000,611540000
112 2057 611550000,611560000,611570000,611580000,611590000
113 2058 703010000
114 *

```



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```

115 *
116 *****MAIN DISCHARGE LINE*****
117 *
118 *
119 2018 703020000,703030000,703040000,703050000,703060000
120 2019 703070000,703080000,703090000,703100000,703110000
121 2020 703120000,703130000,703140000,801010000,803010000
122 2021 805010000,807010000
123 2022 809010000,811010000,811020000,811030000,811040000
124 2023 811050000,811060000,811070000,811080000,811090000
125 2024 811100000,811110000,811120000,811130000,811140000
126 2025 811150000,811160000,811170000,811180000,811190000
127 2026 811200000,811210000,811220000,811230000,811240000
128 2027 811250000,811260000,811270000
129 *
130 *
131 *** PORV UPSTREAM ***
132 *
133 *
134 2028 399010000,401010000,401020000,401030000,401040000
135 2029 401050000,401060000,401070000,401080000,401090000
136 2030 401100000,401110000,401120000,401130000,401140000
137 2031 401150000,401160000,401170000,401180000,401190000
138 2032 401200000,401210000,401220000,401230000,401240000
139 2033 401250000,401260000,401270000,401280000,403010000
140 2034 405010000,405020000,405030000,405040000,405050000
141 2035 405080000,405070000,405080000,405090000,405100000
142 2036 405110000,405120000,405130000,405140000,405150000
143 2037 405180000,407010000,409010000,409020000,409030000
144 2038 409040000,409050000,409060000,409070000,409080000
145 2039 409090000,409100000,409110000,409120000,409130000
146 2040 409140000,409150000,409160000,409170000,409180000
147 2041 409190000,409200000,409210000,409220000,409230000
148 2042 409240000,809010000,809020000,809030000,809040000
149 2043 809050000,809060000,809070000,809080000,809090000
150 2044 509010000,509020000,509030000,509040000,509050000
151 2045 509060000,509070000,509080000,509090000,509100000
152 *
153 *
154 *****
155 * PLOT CARDS *
156 *****
157 *
158 *
159 *
160 20300100 MFLOWJ 410000000
161 20300200 MFLOWJ 510000000
162 20300300 MFLOWJ 610000000
163 20300400 MFLOWJ 402000000
164 20300500 MFLOWJ 811140000
165 20300600 MFLOWJ 811570000
166 20300700 MFLOWJ 308000000
167 20300800 MFLOWJ 208000000
168 20300900 MFLOWJ 108000000
169 *
170 20301000 QUALS 411010000
171 20301100 QUALS 511010000
172 20301200 QUALS 611010000
  
```

173	20301300	QUALS	409240000
174	20301400	QUALS	509100000
175	20301500	QUALS	609090000
178	20301600	QUALS	401280000
177	20301700	QUALS	811140000
178	20301800	QUALS	811570000
179	20301900	QUALS	307010000
180	20302000	QUALS	307180000
181	20302100	QUALS	207010000
182	20302200	QUALS	207280000
183	20302300	QUALS	107010000
184	20302400	QUALS	107330000
185	*		
186	20302500	P	411010000
187	20302600	P	511010000
188	20302700	P	611010000
189	20302800	P	409240000
190	20302900	P	509100000
191	20303000	P	609090000
192	20303100	P	401280000
193	20303200	P	811140000
194	20303300	P	811570000
195	20303400	P	307010000
196	20303500	P	307180000
197	20303600	P	207010000
198	20303700	P	207260000
199	20303800	P	107010000
200	20303900	P	107330000
201	*		
202	*		
203	*		
204	*		
205	END OF CASE		



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4.9.5 SV Cold Loop Seal (Quarter Model)



LISTING OF INPUT DATA FOR CASE 1

```

1 =AEP UNIT2 1 LINE RELAP5
2 100 NEW TRANSNT
3 101 RUN
4 102 BRITISH BRITISH
5 104 NOACTION
6 * TIME STEP CONTROL
7 *
8 201 0.6000 1.0-7 2.0-4 11001 5 25 250
9 * MINOR EDITS
10 *
11 301 QUALS 007010000
12 302 QUALS 005200000
13 303 QUALS 013200000
14 304 P 005200000
15 305 P 007010000
16 308 P 007380000
17 307 MFLOWJ 006000000
18 308 MFLOWJ 005070000
19 309 MFLOWJ 014000000
20 310 P 007140000
21 311 P 011560000
22 312 P 013300000
23 313 MFLOWJ 007140000
24 314 MFLOWJ 007380000
25 315 MFLOWJ 011560000
26 *
27 *
28 2001 5, 192, 001010000, 003010000, 005010000
29 2002 005020000, 005030000, 005040000, 005050000, 005080000
30 2003 005070000, 005080000, 005090000, 005100000, 005110000
31 2004 005120000, 005130000, 005140000, 005150000, 005160000
32 2005 005170000, 005180000, 005190000, 005200000, 007010000
33 2006 007020000, 007030000, 007040000, 007050000, 007080000, 007070000
34 2007 007080000, 007090000, 007100000, 007110000, 007120000
35 2008 007130000, 007140000, 007150000, 007160000, 007170000
36 2009 007180000, 007190000, 007200000, 007210000, 007220000
37 2010 007230000, 007240000, 007250000, 007260000, 007270000
38 2011 007280000, 007290000, 007300000, 007310000, 007320000
39 2012 007330000, 007340000, 007350000, 007360000, 007370000
40 2013 007380000, 007390000, 009010000, 011010000, 011020000
41 2014 011030000, 011040000, 011050000, 011060000, 011070000
42 2015 011080000, 011090000, 011100000, 011110000, 011120000
43 2016 011130000, 011140000, 011150000, 011160000, 011170000
44 2017 011180000, 011190000, 011200000, 011210000, 011220000
45 2018 011230000, 011240000, 011250000, 011260000, 011270000
46 2019 011280000, 011290000, 011300000, 011310000, 011320000
47 2020 011330000, 011340000, 011350000, 011360000, 011370000
48 2021 011380000, 011390000, 011400000, 011410000, 011420000
49 2022 011430000, 011440000, 011450000, 011460000, 011470000
50 2023 011480000, 011490000, 011500000, 011510000, 011520000
51 2024 011530000, 011540000, 011550000, 011560000, 011570000
52 2025 011580000, 011590000, 011600000, 011610000, 011620000
53 2026 011630000, 011640000, 011650000, 011660000, 011670000
54 2027 011680000, 011690000, 011700000, 011710000, 011720000
55 2028 011730000, 011740000, 011750000, 011760000, 011770000
56 2029 011780000, 011790000, 011800000, 011810000, 011820000

```

BY CMH DATE 2-9-83
 CHKD. BY LGS DATE 2-9-83

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```

57 2030 011830000,011840000,011850000,011860000,011870000
58 2031 011880000,011890000,011900000,011910000,011920000
59 2032 011930000,011940000,011950000,011960000,011970000
60 2033 011980000,011990000,013010000,013020000,013030000
61 2034 013040000,013050000,013060000,013070000,013080000
62 2035 013090000,013100000,013110000,013120000,013130000
63 2036 013140000,013150000,013160000,013170000,013180000
64 2037 013190000,013200000,013210000,013220000,013230000
65 2038 013240000,013250000,013260000,013270000,013280000
66 2039 013290000,013300000,015010000
67 *
68 *TRIPS
69 *
70 502 TIME 0 GT NULL 0 1.500 L * JOB TERMINATION TRIP
71 503 TIME 0 GE NULL 0 0.0 L * VALVE OPEN
72 504 TIME 0 GE NULL 0 5.0 L * VALVE CLOSED
73 600 502
74 *
75 * HYDRODYNAMIC COMPONENTS
76 *
77 *
78 * PRESSURIZER
79 *
80 0010000 "PRESS1" TMDPVOL
81 0010101 0.0 20.0 500.0 0.0 0.0 0.0 0.0005 0.0 11
82 0010200 2
83 0010201 0.0 2500.0 1.0 0.1 2514.0 1.0 0.3 2555.0 1.0 0.5 2600.0 1.0
84 0010202 0.7 2687.0 1.0 0.9 2700.0 1.0 1.1 2740.0 1.0 1.3 2745.0 1.0
85 0010203 1.5 2747.0 1.0 1.7 2748.0 1.0 1.9 2750.0 1.0 2.0 2750.0 1.0
86 0010204 2.5 2750.0 1.0
87 *
88 * LOOP SEAL GEOMETRY
89 *
90 0020000 "LPSL" SNGLJUN
91 0020101 001000000 003000000 0.0 0.0 0.0 1000 * THIS IS A SHORT RADIUS ELBOW LEAVING
92 0020201 1 0.0 0.0 0.0
93 *
94 0030000 "LPSL" SNGLVOL
95 0030101 0.1485 1.0 0.0 90.0 0.0 0.0 0.000151 0.0 00
96 0030200 2 2500.0 1.0
97 *
98 0040000 "LPSL" SNGLJUN
99 0040101 003010000 005000000 0.0 0.1838 0.1838 1000
100 0040201 1 0.0 0.0 0.0
101 *
102 0050000 "LPSL" PIPE
103 0050001 20
104 0050101 0.1485 20
105 0050301 0.50 10
106 0050302 0.574 20
107 0050401 0.0 20
108 0050601 -90.0 7
109 0050602 0.0 10
110 0050603 90.0 20
111 0050801 0.000151 0.0 20
112 0050901 0.0 0.0 8
113 0050902 0.1838 0.1838 7
114 0050803 0.0 0.0 9

```

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115	0050904	0.1836	0.1838	10					
116	0050905	0.0	0.0	19					
117	0051001	00	20						
118	0051101	1000	19						
119	0051201	3	2500.0	584.4	0.0	0.0	1		
120	0051202	3	2500.0	451.1	0.0	0.0	2		
121	0051203	3	2500.0	352.1	0.0	0.0	3		
122	0051204	3	2500.0	278.8	0.0	0.0	4		
123	0051205	3	2500.0	218.1	0.0	0.0	5		
124	0051206	3	2500.0	169.3	0.0	0.0	6		
125	0051207	3	2500.0	141.1	0.0	0.0	20		
126	0051300	1							
127	0051301	0.0	0.0	0.0	19				
128	*								
129	*****								
130	* VALVE 6M6 CROSBY SAFETY								
131	*****								
132	0060000 "SRV" VALVE								
133	0080101 005010000 007000000	0.022	0.0	0.0	0100				
134	0060201	1	0.0	0.0	0.0				
135	0060300 MTRVLV								
136	0060301 503 504	100.0	0.0	*	CROSBY 6M6 OPENING IN 10 MSEC				
137	*								
138	* DISCHARGE PIPING								
139	0070000 "DISCHA1" PIPE								
140	0070001	39							
141	0070101	0.20069	39						
142	0070301	0.526	4						
143	0070302	1.094	14						
144	* ARC STARTS HERE LEVEL 669-2"								
145	0070303	0.84187	17						
146	0070304	0.942	20						
147	0070305	0.8425	23						
148	0070306	0.844	26						
149	0070307	0.8433	29						
150	0070308	0.8333	32						
151	0070309	0.8333	35						
152	* ARC ENDS								
153	0070310	0.91750	39						
154	0070401	0.0	39						
155	0070601	0.0	4						
156	0070602	-90.0	14						
157	0070603	0.0	39						
158	0070801	0.000152	0.0	39					
159	0070901	0.0	0.0	3					
160	0070902	0.1800	0.1800	4					
161	0070903	0.0	0.0	13					
162	0070904	0.1800	0.1800	14					
163	0070905	0.0	0.0	38					
164	0071001	00	39						
165	0071101	1000	38						
166	0071201	4	14.7	120.0	0.9284	0.0	39		
167	0071300	1							
168	0071301	0.0	0.0	0.0	38				
169	*								
170	0080000 "DISCHA1" SINGLJUN								
171	0080101 007010000 009000000	0.0	0.1560	0.1560	1000	*LOSSES FOR A 12 IN ELBOW			
172	0080201	1	0.0	0.0	0.0				

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```

173 *
174 * INPUT A BRANCH HERE FOR A COMPLETE MODEL
175 *
176 0090000 "DISCHA1" SNGLVOL
177 0090101 0.7771 0.5 0.0 0.0 -90.0 -0.5 0.000169 0.0 00
178 0090200 4 14.7 120.0 0.9284
179 *
180 0100000 "DISCHA1" SNGLJUN
181 0100101 009010000 011000000 0.0 0.0 0.0 1000
182 0100201 1 0.0 0.0 0.0
183 *
184 0110000 "DISCHA1" PIPE
185 0110001 99
186 0110101 0.7771 99
187 0110301 1.039 14
188 0110302 0.53025 18
189 0110303 0.5 22
190 0110304 0.53025 28
191 0110305 0.9875 58
192 0110308 0.475 68
193 0110307 0.49359 79
194 0110308 0.46875 87
195 0110309 0.51172 95
196 0110310 0.95 99
197 0110401 0.0 98
198 0110601 -90.0 14
199 0110602 -45.0 18
200 0110603 -90.0 22
201 0110604 -45.0 28
202 0110605 -90.0 58
203 0110606 0.0 87
204 0110607 -90.0 95
205 0110608 0.0 99
206 0110801 0.000169 0.0 99
207 0110901 0.0 0.0 13
208 0110902 0.078 0.078 14
209 0110903 0.0 0.0 17
210 0110904 0.078 0.078 18
211 0110905 0.0 0.0 21
212 0110908 0.078 0.078 22
213 0110907 0.0 0.0 25
214 0110908 0.078 0.078 26
215 0110909 0.0 0.0 55
216 0110910 0.158 0.158 58
217 0110911 0.0 0.0 65
218 0110912 0.158 0.158 68
219 0110913 0.0 0.0 78
220 0110914 0.158 0.158 78
221 0110915 0.0 0.0 86
222 0110918 0.158 0.158 87
223 0110917 0.0 0.0 94
224 0110918 0.158 0.158 95
225 0110919 0.0 0.0 98
226 0111001 00 99
227 0111101 1000 98
228 0111201 4 14.7 120.0 0.9284 0.0 99
229 0111300 1
230 0111301 0.0 0.0 0.0 98

```

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```

231 *
232 0120000 "DISCHA1" SNGLJUN
233 0120101 011010000 013000000 0.0 0.0 0.0 1000
234 0120201 1 0.0 0.0 0.0
235 *
236 0130000 "DISCHA1" PIPE
237 0130001 30
238 0130101 0.7771 30
239 0130301 0.95 8
240 0130302 1.0 20
241 0130303 0.5 30
242 0130401 0.0 30
243 0130501 0.0 30
244 0130801 0.000169 0.0 30
245 0130901 0.0 0.0 5
246 0130902 0.156 0.156 8
247 0130903 0.0 0.0 19
248 0130904 0.156 0.156 20
249 0130905 0.0 0.0 29
250 0131001 00 30
251 0131101 1000 29
252 0131201 4 14.7 120.0 0.9284 0.0 30
253 0131300 1
254 0131301 0.0 0.0 0.0 29
255 *
256 0140000 "DISCH1A" SNGLJUN
257 0140101 013010000 015000000 0.0 0.0 0.0 0100
258 0140201 1 0.0 0.0 0.0
259 *
260 0150000 "ATMOS" TMDPVOL
261 0150101 10000.0 10000.0 0.0 0.0 0.0 0.0 0.00001 0.0 11
262 0150200 4
263 0150201 0.0 14.7 120.0 0.9284
264 *
265 * PLOT CARDS
266 *
267 20300100 QUALS 007010000
268 20300200 QUALS 005200000
269 20300300 QUALS 013200000
270 20300400 P 005200000
271 20300500 P 007010000
272 20300600 P 007380000
273 20300700 MFLOWJ 008000000
274 20300800 MFLOWJ 005070000
275 20300900 MFLOWJ 014000000
276 20301000 P 007140000
277 20301100 P 011560000
278 20301200 P 013300000
279 20301300 MFLOWJ 007140000
280 20301400 MFLOWJ 007380000
281 20301500 MFLOWJ 011560000
282 .END OF CASE

```

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4.10 REPIPE Input.

These are input listings of Control Data Corporation's RELAP post-processor, REPIPE. Each set represents direction cosines of the RELAP model as well as structural node assignments. On the Unit 1 PORV model, it was necessary to break up the model in two sections because of REPIPE's size limitations.

<u>Input Set</u>	<u>Model Section</u>	<u>Unit</u>
4.10.1	A	1
4.10.2	B	1
4.10.3	-	2 (Quarter Model)

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4.10.1 Unit 1 - Model Section A



\$PIPES
 INLINE=10,KBLOCK=280,KPIPE=10,KPLOT(1)=1,KWAVE=1,
 KPRINT=-1,KPNV=1,KSTEP=3,
 NDROPV=399010000,811270000,307040000,107040000,805010000,811010000,
 511010000,411010000,609110000,509120000,409260000\$

112	107040000	0.	-1.0	0./
112	107050000	0.	-1.0	0./
112	107060000	0.	-1.0	0./
112	107070000	0.	-1.0	0./
112	107080000	0.	-1.0	0./
112	107090000	0.	-1.0	0./
112	107100000	0.	-1.0	0./
112	107110000	0.	-1.0	0./
112	107120000	0.	-1.0	0./
112	107130000	0.	-1.0	0./
112	107140000	0.	-1.0	0./
108	-107050000	0.	-1.0	0./
108	-107060000	0.	-1.0	0./
108	-107070000	0.	-1.0	0./
108	-107080000	0.	-1.0	0./
108	-107090000	0.	-1.0	0./
108	-107100000	0.	-1.0	0./
108	-107110000	0.	-1.0	0./
108	-107120000	0.	-1.0	0./
108	-107130000	0.	-1.0	0./
108	-107140000	0.	-1.0	0./
108	-107150000	0.	-1.0	0./
104	107150000	0.7723	0.	0.6353/
104	107160000	0.7723	0.	0.6353/
104	107170000	0.7723	0.	0.6353/
10301	-107160000	0.7723	0.	0.6353/
10301	-107170000	0.7723	0.	0.6353/
10301	-107180000	0.7723	0.	0.6353/
10302	107180000	0.9948	0.	0.1018/
10302	107190000	0.9948	0.	0.1018/
10302	107200000	0.9948	0.	0.1018/
10201	-107190000	0.9948	0.	0.1018/
10201	-107200000	0.9948	0.	0.1018/
10201	-107210000	0.9948	0.	0.1018/
10202	107210000	0.8945	0.	-0.4470/
10202	107220000	0.8945	0.	-0.4470/
10202	107230000	0.8945	0.	-0.4470/
10001	-107220000	0.8945	0.	-0.4470/
10001	-107230000	0.8945	0.	-0.4470/
10001	-107240000	0.8945	0.	-0.4470/
10002	107240000	0.8454	0.	-0.5342/
10002	107250000	0.8454	0.	-0.5342/
10002	107260000	0.8454	0.	-0.5342/
9901	-107250000	0.8454	0.	-0.5342/
9901	-107260000	0.8454	0.	-0.5342/
9901	-107270000	0.8454	0.	-0.5342/
9902	107270000	0.0195	0.	-0.9998/
9902	107280000	0.0195	0.	-0.9998/
9902	107290000	0.0195	0.	-0.9998/
9801	-107280000	0.0195	0.	-0.9998/
9801	-107290000	0.0195	0.	-0.9998/
9801	-107300000	0.0195	0.	-0.9998/
9802	107300000	-0.2497	0.	-0.9683/
9802	107310000	-0.2497	0.	-0.9683/
9802	107320000	-0.2497	0.	-0.9683/

BY CHM DATE 4-26-83
 CHKD. BY M/R DATE 4-26-83



97	-107310000	-0.2497	0.	-0.9683/
97	-107320000	-0.2497	0.	-0.9683/
97	-108000000	-0.2497	0.	-0.9683/
222	307040000	0.	-1.0	0./
222	307050000	0.	-1.0	0./
222	307060000	0.	-1.0	0./
222	307070000	0.	-1.0	0./
222	307080000	0.	-1.0	0./
222	307090000	0.	-1.0	0./
222	307100000	0.	-1.0	0./
222	307110000	0.	-1.0	0./
218	-307050000	0.	-1.0	0./
218	-307060000	0.	-1.0	0./
218	-307070000	0.	-1.0	0./
218	-307080000	0.	-1.0	0./
218	-307090000	0.	-1.0	0./
216	-307100000	0.	-1.0	0./
216	-307110000	0.	-1.0	0./
216	-307120000	0.	-1.0	0./
214	307120000	0.0047	0.	-0.99999/
214	307130000	0.0047	0.	-0.99999/
214	307140000	0.0047	0.	-0.99999/
20801	-307130000	0.0047	0.	-0.99999/
20801	-307140000	0.0047	0.	-0.99999/
20801	-307150000	0.0047	0.	-0.99999/
20802	307150000	-0.2497	0.	-0.9683/
20802	307160000	-0.2497	0.	-0.9683/
20802	307170000	-0.2497	0.	-0.9683/
208	-307160000	-0.2497	0.	-0.9683/
208	-307170000	-0.2497	0.	-0.9683/
208	-308000000	-0.2497	0.	-0.9683/
285	703010000	0.	-1.0	0./
285	703020000	0.	-1.0	0./
285	703030000	0.	-1.0	0./
285	703040000	0.	-1.0	0./
285	703050000	0.	-1.0	0./
285	703060000	0.	-1.0	0./
285	703070000	0.	-1.0	0./
285	703080000	0.	-1.0	0./
285	703090000	0.	-1.0	0./
285	703100000	0.	-1.0	0./
285	703110000	0.	-1.0	0./
260	703120000	0.	-1.0	0./
260	703130000	0.	-1.0	0./
260	704000000	0.	-1.0	0./
260	802000000	0.	-1.0	0./
260	804000000	0.0	-1.0	0.0/
280	806000000	0.0	-1.0	0.0/
260	808000000	0.	-1.0	0./
260	810000000	0.	-1.0	0./
260	811010000	0.	-1.0	0./
260	811020000	0.	-1.0	0./
260	811030000	0.	-1.0	0./
260	811040000	0.	-1.0	0./
260	811050000	0.	-1.0	0./
260	811060000	0.	-1.0	0./
260	811070000	0.	-1.0	0./
260	811080000	0.	-1.0	0./
260	811090000	0.	-1.0	0./
260	811100000	0.	-1.0	0./



750	401010000	0.6890	0.7071	-0.1591/
750	401020000	0.6890	0.7071	-0.1591/
750	401030000	0.6890	0.7071	-0.1591/
725	-401010000	0.6890	0.7071	-0.1591/
725	-401020000	0.6890	0.7071	-0.1591/
725	-401030000	0.6890	0.7071	-0.1591/
725	-401040000	0.6890	0.7071	-0.1591/
720	401040000	0.0	1.0	0.0/
720	401050000	0.0	1.0	0.0/
720	401060000	0.0	1.0	0.0/
720	401070000	0.0	1.0	0.0/
720	401080000	0.0	1.0	0.0/
720	401090000	0.0	1.0	0.0/
720	401100000	0.0	1.0	0.0/
720	401110000	0.0	1.0	0.0/
715	-401050000	0.0	1.0	0.0/
715	-401060000	0.0	1.0	0.0/
715	-401070000	0.0	1.0	0.0/
715	-401080000	0.0	1.0	0.0/
715	-401090000	0.0	1.0	0.0/
715	-401100000	0.0	1.0	0.0/
715	-401110000	0.0	1.0	0.0/
715	-401120000	0.0	1.0	0.0/
710	401120000	1.0	0.0	0.0/
710	401130000	1.0	0.0	0.0/
710	401140000	1.0	0.0	0.0/
710	401150000	1.0	0.0	0.0/
710	401160000	1.0	0.0	0.0/
710	401170000	1.0	0.0	0.0/
710	401180000	1.0	0.0	0.0/
700	-401130000	1.0	0.0	0.0/
700	-401140000	1.0	0.0	0.0/
700	-401150000	1.0	0.0	0.0/
700	-401160000	1.0	0.0	0.0/
700	-401170000	1.0	0.0	0.0/
700	-401180000	1.0	0.0	0.0/
700	-401190000	1.0	0.0	0.0/
690	401190000	0.0	1.0	0.0/
690	401200000	0.0	1.0	0.0/
690	401210000	0.0	1.0	0.0/
690	401220000	0.0	1.0	0.0/
690	401230000	0.0	1.0	0.0/
690	401240000	0.0	1.0	0.0/
690	401250000	0.0	1.0	0.0/
690	401260000	0.0	1.0	0.0/
675	-401200000	0.0	1.0	0.0/
675	-401210000	0.0	1.0	0.0/
675	-401220000	0.0	1.0	0.0/
675	-401230000	0.0	1.0	0.0/
675	-401240000	0.0	1.0	0.0/
675	-401250000	0.0	1.0	0.0/
675	-401260000	0.0	1.0	0.0/
675	-401270000	0.0	1.0	0.0/
670	401270000	-0.935	0.0	-0.3581/
670	402000000	-0.935	0.0	-0.3581/
670	404000000	-0.935	0.0	-0.3581/
595	-402000000	-0.935	0.0	-0.3581/
595	-404000000	-0.935	0.0	-0.3581/
595	-405010000	-0.935	0.0	-0.3581/
595	405010000	-0.994	0.0	-0.0341/

260	811110000	0.	-1.0	0./
260	811120000	0.	-1.0	0./
260	811130000	0.	-1.0	0./
2601	-703020000	0.	-1.0	0./
2601	-703030000	0.	-1.0	0./
2601	-703040000	0.	-1.0	0./
2801	-703050000	0.	-1.0	0./
2801	-703060000	0.	-1.0	0./
2801	-703070000	0.	-1.0	0./
2801	-703080000	0.	-1.0	0./
2601	-703090000	0.	-1.0	0./
2801	-703100000	0.	-1.0	0./
2801	-703110000	0.	-1.0	0./
2801	-703120000	0.	-1.0	0./
90	-703130000	0.	-1.0	0./
90	-704000000	0.	-1.0	0./
90	-802000000	0.	-1.0	0./
90	-804000000	0.0	-1.0	0.0/
90	-806000000	0.0	-1.0	0.0/
90	-808000000	0.	-1.0	0./
90	-810000000	0.	-1.0	0./
90	-811010000	0.	-1.0	0./
90	-811020000	0.	-1.0	0./
90	-811030000	0.	-1.0	0./
90	-811040000	0.	-1.0	0./
90	-811050000	0.	-1.0	0./
90	-811060000	0.	-1.0	0./
90	-811070000	0.	-1.0	0./
90	-811080000	0.	-1.0	0./
90	-811090000	0.	-1.0	0./
90	-811100000	0.	-1.0	0./
90	-811110000	0.	-1.0	0./
90	-811120000	0.	-1.0	0./
90	-811130000	0.	-1.0	0./
90	-811140000	0.	-1.0	0./
88	811140000	-0.6667	-0.7071	0.2356/
88	811150000	-0.6667	-0.7071	0.2356/
88	811160000	-0.6667	-0.7071	0.2356/
88	811170000	-0.6667	-0.7071	0.2356/
88	-811150000	-0.6667	-0.7071	0.2356/
88	-811160000	-0.6667	-0.7071	0.2356/
88	-811170000	-0.6667	-0.7071	0.2356/
88	-811180000	-0.6667	-0.7071	0.2356/
84	811180000	0.	-1.0	0./
84	811190000	0.	-1.0	0./
84	811200000	0.	-1.0	0./
84	811210000	0.	-1.0	0./
82	-811190000	0.	-1.0	0./
82	-811200000	0.	-1.0	0./
82	-811210000	0.	-1.0	0./
82	-811220000	0.	-1.0	0./
80	811220000	-0.2356	-0.7071	-0.6667/
80	811230000	-0.2356	-0.7071	-0.6667/
80	811240000	-0.2356	-0.7071	-0.6667/
80	811250000	-0.2356	-0.7071	-0.6667/
78	-811230000	-0.2356	-0.7071	-0.6667/
78	-811240000	-0.2356	-0.7071	-0.6667/
78	-811250000	-0.2356	-0.7071	-0.6667/
78	-811260000	-0.2356	-0.7071	-0.6667/
750	400000000	0.6890	0.7071	-0.1591/

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5951	405020000	-.9994	0.0	-.0341/
5951	405030000	-.9994	0.0	-.0341/
590	-405020000	-.9994	0.0	-.0341/
590	-405030000	-.9994	0.0	-.0341/
590	-405040000	-.9994	0.0	-.0341/
5901	405040000	-.9703	0.0	.2420/
5901	405050000	-.9703	0.0	.2420/
5901	405060000	-.9703	0.0	.2420/
585	-405050000	-.9703	0.0	.2420/
585	-405060000	-.9703	0.0	.2420/
585	-405070000	-.9703	0.0	.2420/
5851	405070000	-.8217	0.0	.570/
5851	405080000	-.8217	0.0	.570/
5851	405090000	-.8217	0.0	.570/
5851	405100000	-.8217	0.0	.570/
5851	405110000	-.8217	0.0	.570/
575	-405080000	-.8217	0.0	.570/
575	-405090000	-.8217	0.0	.570/
575	-405100000	-.8217	0.0	.570/
575	-405110000	-.8217	0.0	.570/
575	-405120000	-.8217	0.0	.570/
5751	405120000	-.4962	0.0	.8682/
5751	405130000	-.4962	0.0	.8682/
5751	405140000	-.4962	0.0	.8682/
5751	405150000	-.4962	0.0	.8682/
5751	406000000	-.4962	0.0	.8682/
435	-405130000	-.4962	0.0	.8682/
435	-405140000	-.4962	0.0	.8682/
435	-405150000	-.4962	0.0	.8682/
435	-406000000	-.4962	0.0	.8682/
435	-408000000	-.4962	0.0	.8682/
4351	408000000	-.24165	0.0	.97036/
440	-409010000	-.24165	0.0	.97036/
4401	409010000	-.1623	0.0	.9867/
450	-409020000	-.1623	0.0	.9867/
4501	409020000	.0623	0.0	.9981/
4501	409030000	.0623	0.0	.9981/
4501	409040000	.0623	0.0	.9981/
4501	409050000	.0623	0.0	.9981/
480	-409030000	.0623	0.0	.9981/
480	-409040000	.0623	0.0	.9981/
480	-409050000	.0623	0.0	.9981/
460	-409060000	.0623	0.0	.9981/
4601	409060000	.4362	0.0	.8999/
4601	409070000	.4362	0.0	.8999/
4801	409080000	.4362	0.0	.8999/
4001	409090000	.4362	0.0	.8999/
465	-409070000	.4362	0.0	.8999/
465	-409080000	.4362	0.0	.8999/
465	-409090000	.4362	0.0	.8999/
465	-409100000	.4362	0.0	.8999/
4851	409100000	.76	0.0	.6500/
4651	409110000	.76	0.0	.6500/
4651	409120000	.76	0.0	.6500/
4651	409130000	.76	0.0	.6500/
475	-409110000	.76	0.0	.6500/
475	-409120000	.76	0.0	.6500/
475	-409130000	.76	0.0	.6500/
475	-409140000	.76	0.0	.6500/
480	409140000	0.9263	-0.044	-.3742/

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480	409150000	0.9263	-0.044	-.3742/	
480	409160000	0.9263	-0.044	-.3742/	
480	409170000	0.9263	-0.044	-.3742/	
480	409180000	0.9263	-0.044	-.3742/	
480	409190000	0.9263	-0.044	-.3742/	
480	409200000	0.9263	-0.044	-.3742/	
480	409210000	0.9263	-0.044	-.3742/	
480	409220000	0.9263	-0.044	-.3742/	
480	409230000	0.9263	-0.044	-.3742/	
480	409240000	0.9263	-0.044	-.3742/	
525	411010000	0.9263	-0.044	-.3742/	
525	411020000	0.9283	-0.044	-.3742/	
525	411030000	0.9263	-0.044	-.3742/	
510	-409150000	0.9263	-0.044	-.3742/	
510	-409160000	0.9263	-0.044	-.3742/	
510	-409170000	0.9263	-0.044	-.3742/	
510	-409180000	0.9263	-0.044	-.3742/	
510	-409190000	0.9263	-0.044	-.3742/	
510	-409200000	0.9263	-0.044	-.3742/	
510	-409210000	0.9263	-0.044	-.3742/	
510	-409220000	0.9263	-0.044	-.3742/	
510	-409230000	0.9263	-0.044	-.3742/	
510	-409240000	0.9263	-0.044	-.3742/	
510	-409250000	0.9263	-0.044	-.3742/	
530	-411020000	0.9263	-0.044	-.3742/	
530	-411030000	0.9263	-0.044	-.3742/	
530	-411040000	0.9283	-0.044	-.3742/	
600	608000000	-0.292	-0.0464	0.9563/	
600	609010000	-0.292	-0.0464	0.9563/	
665	-609010000	-0.292	-0.0464	0.9563/	
665	-609020000	-0.292	-0.0464	0.9563/	
660	609020000	-0.9262	-0.0464	0.3742/	
660	609030000	-0.9262	-0.0464	0.3742/	
660	609040000	-0.9262	-0.0464	0.3742/	
660	609050000	-0.9262	-0.0464	0.3742/	
660	609060000	-0.9262	-0.0464	0.3742/	
660	609070000	-0.9262	-0.0464	0.3742/	
660	609080000	-0.9262	-0.0464	0.3742/	
660	609090000	-0.9262	-0.0464	0.3742/	
625	811010000	-0.9262	-0.0464	0.3742/	
625	811020000	-0.9262	-0.0464	0.3742/	
625	811030000	-0.9262	-0.0464	0.3742/	
635	-609030000	-0.9262	-0.0464	0.3742/	
635	-609040000	-0.9262	-0.0464	0.3742/	
635	-609050000	-0.9262	-0.0464	0.3742/	
635	-609060000	-0.9262	-0.0464	0.3742/	
635	-609070000	-0.9262	-0.0464	0.3742/	
635	-609080000	-0.9262	-0.0464	0.3742/	
635	-609090000	-0.9262	-0.0464	0.3742/	
635	-609100000	-0.9262	-0.0464	0.3742/	
615	-611020000	-0.9262	-0.0464	0.3742/	
615	-611030000	-0.9262	-0.0464	0.3742/	
615	-611040000	-0.9262	-0.0464	0.3742/	
435	508000000	0.9670	-0.2548	0.0/	
435	509010000	0.9670	-0.2548	0.0/	
430	-509010000	0.9670	-0.2548	0.0/	
430	-509020000	0.9670	-0.2548	0.0/	
429	509020000	0.3745	-0.0292	0.9268/	
429	509030000	0.3745	-0.0292	0.9268/	
429	509040000	0.3745	-0.0292	0.9268/	

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429	509050000	0.3745	-0.0292	0.9268/
429	509060000	0.3745	-0.0292	0.9268/
429	509070000	0.3745	-0.0292	0.9268/
429	509080000	0.3745	-0.0292	0.9268/
429	509090000	0.3745	-0.0292	0.9268/
429	509100000	0.3745	-0.0292	0.9268/
385	511010000	0.3745	-0.0292	0.9268/
385	511020000	0.3745	-0.0292	0.9268/
400	-509030000	0.3745	-0.0292	0.9268/
400	-509040000	0.3745	-0.0292	0.9268/
400	-509050000	0.3745	-0.0292	0.9268/
400	-509060000	0.3745	-0.0292	0.9268/
400	-509070000	0.3745	-0.0292	0.9268/
400	-509080000	0.3745	-0.0292	0.9268/
400	-509090000	0.3745	-0.0292	0.9268/
400	-509100000	0.3745	-0.0292	0.9268/
400	-509110000	0.3745	-0.0292	0.9268/
380	-511020000	0.3745	-0.0292	0.9268/
380	-511030000	0.3745	-0.0292	0.9268/
810	611040000	0.0	-1.0	0.0/
810	611050000	0.0	-1.0	0.0/
810	611060000	0.0	-1.0	0.0/
810	611070000	0.0	-1.0	0.0/
335	-811050000	0.0	-1.0	0.0/
335	-811060000	0.0	-1.0	0.0/
335	-811070000	0.0	-1.0	0.0/
335	-812000000	0.0	-1.0	0.0/
535	411040000	0.0	-1.0	0.0/
535	411050000	0.0	-1.0	0.0/
535	411060000	0.0	-1.0	0.0/
535	411070000	0.0	-1.0	0.0/
540	-411050000	0.0	-1.0	0.0/
540	-411060000	0.0	-1.0	0.0/
540	-411070000	0.0	-1.0	0.0/
540	-411080000	0.0	-1.0	0.0/
545	411080000	.285	0.0	-.9585/
545	411090000	.285	0.0	-.9585/
545	411100000	.285	0.0	-.9585/
55001	-411090000	.285	0.0	-.9585/
55001	-411100000	.285	0.0	-.9585/
55001	-411110000	.285	0.0	-.9585/
55002	411110000	-.107	0.0	-.9943/
55002	411120000	-.107	0.0	-.9943/
55002	411130000	-.107	0.0	-.9943/
55501	-411120000	-.107	0.0	-.9943/
55501	-411130000	-.107	0.0	-.9943/
55501	-411140000	-.107	0.0	-.9943/
55502	411140000	-.483	0.0	-.876/
55502	411150000	-.483	0.0	-.876/
55502	411160000	-.483	0.0	-.876/
56001	-411150000	-.483	0.0	-.876/
56001	-411160000	-.483	0.0	-.876/
56001	-411170000	-.483	0.0	-.876/
56002	411170000	-.7064	0.0	-.7078/
56002	411180000	-.7064	0.0	-.7078/
285	-411180000	-.7064	0.0	-.7078/
295	-412000000	-.7064	0.0	-.7078/
375	511030000	0.0	-1.0	0.0/
375	511040000	0.0	-1.0	0.0/
375	511050000	0.0	-1.0	0.0/

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375	511060000	0.0	-1.0	0.0/
370	-511040000	0.0	-1.0	0.0/
370	-511050000	0.0	-1.0	0.0/
370	-511060000	0.0	-1.0	0.0/
370	-511070000	0.0	-1.0	0.0/
365	511070000	-.826	0.0	-.563/
365	511080000	-.826	0.0	-.563/
36001	-511080000	-.826	0.0	-.563/
36001	-511090000	-.826	0.0	-.563/
38002	511090000	-.633	0.0	-.7745/
38002	511100000	-.633	0.0	-.7745/
38002	511110000	-.633	0.0	-.7745/
35501	-511100000	-.633	0.0	-.7745/
35501	-511110000	-.633	0.0	-.7745/
35501	-511120000	-.633	0.0	-.7745/
35502	511120000	-.264	0.0	-.967/
35502	511130000	-.264	0.0	-.967/
35502	511140000	-.264	0.0	-.967/
35001	-511130000	-.264	0.0	-.967/
35001	-511140000	-.264	0.0	-.967/
35001	-511150000	-.264	0.0	-.967/
35002	511150000	.169	0.0	-.9858/
35002	511160000	.169	0.0	-.9858/
35002	511170000	.169	0.0	-.9858/
34001	-511160000	.169	0.0	-.9858/
34001	-511170000	.169	0.0	-.9858/
34001	-511180000	.169	0.0	-.9858/
34002	511180000	.415	0.0	-.9099/
33501	-512000000	.415	0.0	-.9099/
33502	512000000	.525	0.0	-.851/
33502	612000000	0.525	0.0	-.851/
33502	514000000	.525	0.0	-.851/
32501	-514000000	.525	0.0	-.851/
32501	-515010000	.525	0.0	-.851/
32502	515010000	.773	0.0	-.635/
32502	515020000	.773	0.0	-.635/
32502	515030000	.773	0.0	-.635/
32001	-515020000	.773	0.0	-.635/
32001	-515030000	.773	0.0	-.635/
32001	-515040000	.773	0.0	-.635/
32002	515040000	.981	0.0	-.195/
32002	515050000	.981	0.0	-.195/
32002	515060000	.981	0.0	-.195/
31001	-515050000	.981	0.0	-.195/
31001	-515060000	.981	0.0	-.195/
31001	-515070000	.981	0.0	-.195/
31002	515070000	.957	0.0	.290/
31002	515080000	.957	0.0	.290/
31002	515090000	.957	0.0	.290/
30001	-515080000	.957	0.0	.290/
30001	-515090000	.957	0.0	.290/
30001	-515100000	.957	0.0	.290/
30002	515100000	.812	0.0	.583/
30002	515110000	.812	0.0	.583/
295	-515110000	.812	0.0	.583/
295	-516000000	.812	0.0	.583/
2951	516000000	-0.648	0.0	-.761/
2951	412000000	-0.648	0.0	-.761/
2951	702000000	-0.648	0.0	-.761/
280	-702000000	-0.648	0.0	-.761/

290 -703010000 -0.648 0.0 -.781/
99999/
\$STEPS TSTEP(1)=0.001,1.0\$

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TR-5364-1
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 **TELEDYNE
ENGINEERING SERVICES**

4.10.2 Unit 1 - Model Section B

\$PIPES
INLINE=3,KBLOCK=200,KPIPE=10,KPLOT(1)=1,KWAVE=1,
KPRINT=-1,KPNV=1,KSTEP=3,
NDROPV=811260000,307050000,107050000,703010000,811150000,
307180000,107330000,811260000,978080000\$

115	105000000	0.3498	0.	0.9368/
115	107010000	0.3498	0.	0.9368/
115	107020000	0.3498	0.	0.9368/
115	107030000	0.3498	0.	0.9368/
114	-107010000	0.3498	0.	0.9368/
114	-107020000	0.3498	0.	0.9368/
114	-107030000	0.3498	0.	0.9368/
114	-107040000	0.3498	0.	0.9368/
164	206000000	0.9966	0.	0.0819/
164	207010000	0.9966	0.	0.0819/
164	207020000	0.9966	0.	0.0819/
164	207030000	0.9966	0.	0.0819/
162	-207010000	0.9966	0.	0.0819/
182	-207020000	0.9966	0.	0.0819/
182	-207030000	0.9966	0.	0.0819/
182	-207040000	0.9966	0.	0.0819/
160	207040000	0.	-1.0	0./
160	207050000	0.	-1.0	0./
160	207060000	0.	-1.0	0./
160	207070000	0.	-1.0	0./
160	207080000	0.	-1.0	0./
160	207090000	0.	-1.0	0./
160	207100000	0.	-1.0	0./
160	207110000	0.	-1.0	0./
180	207120000	0.	-1.0	0./
160	207130000	0.	-1.0	0./
152	-207050000	0.	-1.0	0./
152	-207060000	0.	-1.0	0./
152	-207070000	0.	-1.0	0./
152	-207080000	0.	-1.0	0./
152	-207090000	0.	-1.0	0./
152	-207100000	0.	-1.0	0./
152	-207110000	0.	-1.0	0./
152	-207120000	0.	-1.0	0./
152	-207130000	0.	-1.0	0./
152	-207140000	0.	-1.0	0./
150	207140000	0.9202	0.	-0.3915/
150	207150000	0.9202	0.	-0.3915/
150	207160000	0.9202	0.	-0.3915/
14801	-207150000	0.9202	0.	-0.3915/
14801	-207160000	0.9202	0.	-0.3915/
14801	-207170000	0.9202	0.	-0.3915/
14802	207170000	0.5647	0.	-0.8253/
14802	207180000	0.5647	0.	-0.8253/
14802	207190000	0.5647	0.	-0.8253/
14601	-207180000	0.5647	0.	-0.8253/
14601	-207190000	0.5647	0.	-0.8253/
14601	-207200000	0.5647	0.	-0.8253/
14602	207200000	0.0318	0.	-0.9995/
14602	207210000	0.0318	0.	-0.9995/
14602	207220000	0.0318	0.	-0.9995/
14401	-207210000	0.0318	0.	-0.9995/
14401	-207220000	0.0318	0.	-0.9995/
14401	-207230000	0.0318	0.	-0.9995/
14402	207230000	-0.2497	0.	-0.9683/

BY CMM DATE 4-26-83
CHKD. BY M/L DATE 4-26-83

14402	207240000	-0.2497	0.	-0.9683/
14402	207250000	-0.2497	0.	-0.9683/
142	-207240000	-0.2497	0.	-0.9683/
142	-207250000	-0.2497	0.	-0.9683/
142	-208000000	-0.2497	0.	-0.9683/
224	306000000	-0.4621	0.	-0.8868/
224	307010000	-0.4621	0.	-0.8868/
224	307020000	-0.4621	0.	-0.8868/
224	307030000	-0.4621	0.	-0.8868/
223	-307010000	-0.4621	0.	-0.8868/
223	-307020000	-0.4621	0.	-0.8868/
223	-307030000	-0.4621	0.	-0.8868/
223	-307040000	-0.4621	0.	-0.8868/
285	703010000	0.	-1.0	0./
285	703020000	0.	-1.0	0./
285	703030000	0.	-1.0	0./
285	703040000	0.	-1.0	0./
285	703050000	0.	-1.0	0./
285	703060000	0.	-1.0	0./
285	703070000	0.	-1.0	0./
285	703080000	0.	-1.0	0./
285	703090000	0.	-1.0	0./
285	703100000	0.	-1.0	0./
285	703110000	0.	-1.0	0./
285	703120000	0.	-1.0	0./
285	703130000	0.	-1.0	0./
285	704000000	0.	-1.0	0./
285	308000000	0.0	-1.0	0.0/
285	802000000	0.	-1.0	0./
285	804000000	0.	-1.0	0./
285	208000000	0.0	-1.0	0.0/
285	806000000	0.	-1.0	0./
285	808000000	0.	-1.0	0./
285	108000000	0.0	-1.0	0.0/
285	810000000	0.	-1.0	0./
285	811010000	0.	-1.0	0./
285	811020000	0.	-1.0	0./
285	811030000	0.	-1.0	0./
285	811040000	0.	-1.0	0./
285	811050000	0.	-1.0	0./
285	811060000	0.	-1.0	0./
285	811070000	0.	-1.0	0./
285	811080000	0.	-1.0	0./
285	811090000	0.	-1.0	0./
285	811100000	0.	-1.0	0./
285	811110000	0.	-1.0	0./
285	811120000	0.	-1.0	0./
285	811130000	0.	-1.0	0./
90	-703020000	0.	-1.0	0./
90	-703030000	0.	-1.0	0./
90	-703040000	0.	-1.0	0./
90	-703050000	0.	-1.0	0./
90	-703060000	0.	-1.0	0./
90	-703070000	0.	-1.0	0./
90	-703080000	0.	-1.0	0./
90	-703090000	0.	-1.0	0./
90	-703100000	0.	-1.0	0./
90	-703110000	0.	-1.0	0./
90	-703120000	0.	-1.0	0./
90	-703130000	0.	-1.0	0./

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90	-704000000	0.	-1.0	0./
90	-802000000	0.	-1.0	0./
90	-804000000	0.	-1.0	0./
90	-806000000	0.	-1.0	0./
90	-808000000	0.	-1.0	0./
90	-810000000	0.	-1.0	0./
90	-811010000	0.	-1.0	0./
90	-811020000	0.	-1.0	0./
90	-811030000	0.	-1.0	0./
90	-811040000	0.	-1.0	0./
90	-811050000	0.	-1.0	0./
90	-811060000	0.	-1.0	0./
90	-811070000	0.	-1.0	0./
90	-811080000	0.	-1.0	0./
90	-811090000	0.	-1.0	0./
90	-811100000	0.	-1.0	0./
90	-811110000	0.	-1.0	0./
90	-811120000	0.	-1.0	0./
90	-811130000	0.	-1.0	0./
90	-811140000	0.	-1.0	0./
74	811260000	0.0	-1.0	0.0/
74	811270000	0.0	-1.0	0.0/
74	811280000	0.0	-1.0	0.0/
74	811290000	0.0	-1.0	0.0/
74	811300000	0.0	-1.0	0.0/
74	811310000	0.0	-1.0	0.0/
74	811320000	0.0	-1.0	0.0/
74	811330000	0.0	-1.0	0.0/
74	811340000	0.0	-1.0	0.0/
74	811350000	0.0	-1.0	0.0/
74	811360000	0.0	-1.0	0.0/
74	811370000	0.0	-1.0	0.0/
74	811380000	0.0	-1.0	0.0/
74	811390000	0.0	-1.0	0.0/
74	811400000	0.0	-1.0	0.0/
74	811410000	0.0	-1.0	0.0/
74	811420000	0.0	-1.0	0.0/
74	811430000	0.0	-1.0	0.0/
74	811440000	0.0	-1.0	0.0/
74	811450000	0.0	-1.0	0.0/
74	811460000	0.0	-1.0	0.0/
74	811470000	0.0	-1.0	0.0/
74	811480000	0.0	-1.0	0.0/
74	811490000	0.0	-1.0	0.0/
74	811500000	0.0	-1.0	0.0/
74	811510000	0.0	-1.0	0.0/
74	811520000	0.0	-1.0	0.0/
74	811530000	0.0	-1.0	0.0/
74	811540000	0.0	-1.0	0.0/
74	811550000	0.0	-1.0	0.0/
82	-811270000	0.0	-1.0	0.0/
82	-811280000	0.0	-1.0	0.0/
82	-811290000	0.0	-1.0	0.0/
82	-811300000	0.0	-1.0	0.0/
82	-811310000	0.0	-1.0	0.0/
82	-811320000	0.0	-1.0	0.0/
82	-811330000	0.0	-1.0	0.0/
82	-811340000	0.0	-1.0	0.0/
82	-811350000	0.0	-1.0	0.0/
82	-811360000	0.0	-1.0	0.0/

62	-811370000	0.0	-1.0	0.0/
62	-811380000	0.0	-1.0	0.0/
62	-811390000	0.0	-1.0	0.0/
62	-811400000	0.0	-1.0	0.0/
62	-811410000	0.0	-1.0	0.0/
62	-811420000	0.0	-1.0	0.0/
62	-811430000	0.0	-1.0	0.0/
62	-811440000	0.0	-1.0	0.0/
62	-811450000	0.0	-1.0	0.0/
62	-811460000	0.0	-1.0	0.0/
62	-811470000	0.0	-1.0	0.0/
62	-811480000	0.0	-1.0	0.0/
62	-811490000	0.0	-1.0	0.0/
62	-811500000	0.0	-1.0	0.0/
62	-811510000	0.0	-1.0	0.0/
62	-811520000	0.0	-1.0	0.0/
62	-811530000	0.0	-1.0	0.0/
62	-811540000	0.0	-1.0	0.0/
62	-811550000	0.0	-1.0	0.0/
62	-811560000	0.0	-1.0	0.0/
60	811560000	0.0	0.0	-1.0/
60	811570000	0.0	0.0	-1.0/
60	811580000	0.0	0.0	-1.0/
60	811590000	0.0	0.0	-1.0/
60	811600000	0.0	0.0	-1.0/
60	811610000	0.0	0.0	-1.0/
60	811620000	0.0	0.0	-1.0/
60	811630000	0.0	0.0	-1.0/
58	-811570000	0.0	0.0	-1.0/
58	-811580000	0.0	0.0	-1.0/
58	-811590000	0.0	0.0	-1.0/
58	-811600000	0.0	0.0	-1.0/
58	-811610000	0.0	0.0	-1.0/
58	-811620000	0.0	0.0	-1.0/
58	-811630000	0.0	0.0	-1.0/
58	-811640000	0.0	0.0	-1.0/
58	811640000	-.259	0.0	-.966/
58	811650000	-.259	0.0	-.966/
58	811660000	-.259	0.0	-.966/
58	811670000	-.259	0.0	-.966/
58	811680000	-.259	0.0	-.966/
58	811690000	-.259	0.0	-.966/
58	811700000	-.259	0.0	-.966/
58	811710000	-.259	0.0	-.966/
52	-811650000	-.259	0.0	-.966/
52	-811660000	-.259	0.0	-.966/
52	-811670000	-.259	0.0	-.966/
52	-811680000	-.259	0.0	-.966/
52	-811690000	-.259	0.0	-.966/
52	-811700000	-.259	0.0	-.966/
52	-811710000	-.259	0.0	-.966/
52	-811720000	-.259	0.0	-.966/
50	811720000	-1.0	0.0	0.0/
50	811730000	-1.0	0.0	0.0/
50	811740000	-1.0	0.0	0.0/
50	811750000	-1.0	0.0	0.0/
50	811760000	-1.0	0.0	0.0/
50	811770000	-1.0	0.0	0.0/
50	811780000	-1.0	0.0	0.0/
50	811790000	-1.0	0.0	0.0/

46	-811730000	-1.0	0.0	0.0/
46	-811740000	-1.0	0.0	0.0/
46	-811750000	-1.0	0.0	0.0/
46	-811760000	-1.0	0.0	0.0/
46	-811770000	-1.0	0.0	0.0/
46	-811780000	-1.0	0.0	0.0/
46	-811790000	-1.0	0.0	0.0/
46	-811800000	-1.0	0.0	0.0/
44	811800000	0.0	-1.0	0.0/
44	811810000	0.0	-1.0	0.0/
44	811820000	0.0	-1.0	0.0/
44	811830000	0.0	-1.0	0.0/
44	811840000	0.0	-1.0	0.0/
44	811850000	0.0	-1.0	0.0/
44	811860000	0.0	-1.0	0.0/
44	811870000	0.0	-1.0	0.0/
40	-811810000	0.0	-1.0	0.0/
40	-811820000	0.0	-1.0	0.0/
40	-811830000	0.0	-1.0	0.0/
40	-811840000	0.0	-1.0	0.0/
40	-811850000	0.0	-1.0	0.0/
40	-811860000	0.0	-1.0	0.0/
40	-811870000	0.0	-1.0	0.0/
40	-811880000	0.0	-1.0	0.0/
38	811880000	-1.0	0.0	0.0/
38	811890000	-1.0	0.0	0.0/
38	811900000	-1.0	0.0	0.0/
38	811910000	-1.0	0.0	0.0/
38	811920000	-1.0	0.0	0.0/
38	811930000	-1.0	0.0	0.0/
38	811940000	-1.0	0.0	0.0/
38	811950000	-1.0	0.0	0.0/
38	811960000	-1.0	0.0	0.0/
32	-811890000	-1.0	0.0	0.0/
32	-811900000	-1.0	0.0	0.0/
32	-811910000	-1.0	0.0	0.0/
32	-811920000	-1.0	0.0	0.0/
32	-811930000	-1.0	0.0	0.0/
32	-811940000	-1.0	0.0	0.0/
32	-811950000	-1.0	0.0	0.0/
32	-811960000	-1.0	0.0	0.0/
32	-812000000	-1.0	0.0	0.0/
30	812000000	0.0	0.0	1.0/
30	813010000	0.0	0.0	1.0/
30	813020000	0.0	0.0	1.0/
30	813030000	0.0	0.0	1.0/
30	813040000	0.0	0.0	1.0/
30	813050000	0.0	0.0	1.0/
30	813060000	0.0	0.0	1.0/
30	813070000	0.0	0.0	1.0/
30	813080000	0.0	0.0	1.0/
30	813090000	0.0	0.0	1.0/
30	813100000	0.0	0.0	1.0/
30	813110000	0.0	0.0	1.0/
30	813120000	0.0	0.0	1.0/
30	813130000	0.0	0.0	1.0/
12	-813010000	0.0	0.0	1.0/
12	-813020000	0.0	0.0	1.0/
12	-813030000	0.0	0.0	1.0/
12	-813040000	0.0	0.0	1.0/

12	-813050000	0.0	0.0	1.0/
12	-813060000	0.0	0.0	1.0/
12	-813070000	0.0	0.0	1.0/
12	-813080000	0.0	0.0	1.0/
12	-813090000	0.0	0.0	1.0/
12	-813100000	0.0	0.0	1.0/
12	-813110000	0.0	0.0	1.0/
12	-813120000	0.0	0.0	1.0/
12	-813130000	0.0	0.0	1.0/
12	-813140000	0.0	0.0	1.0/
10	813140000	1.0	0.0	0.0/
10	813150000	1.0	0.0	0.0/
10	813160000	1.0	0.0	0.0/
10	813170000	1.0	0.0	0.0/
10	813180000	1.0	0.0	0.0/
10	813190000	1.0	0.0	0.0/
10	813200000	1.0	0.0	0.0/
10	813210000	1.0	0.0	0.0/
10	813220000	1.0	0.0	0.0/
10	813230000	1.0	0.0	0.0/
8	-813150000	1.0	0.0	0.0/
8	-813160000	1.0	0.0	0.0/
8	-813170000	1.0	0.0	0.0/
8	-813180000	1.0	0.0	0.0/
8	-813190000	1.0	0.0	0.0/
8	-813200000	1.0	0.0	0.0/
8	-813210000	1.0	0.0	0.0/
8	-813220000	1.0	0.0	0.0/
8	-813230000	1.0	0.0	0.0/
8	-813240000	1.0	0.0	0.0/
4	813240000	0.0	-1.0	0.0/
4	813250000	0.0	-1.0	0.0/
4	977000000	0.0	-1.0	0.0/
4	978010000	0.0	-1.0	0.0/
4	978020000	0.0	-1.0	0.0/
4	978030000	0.0	-1.0	0.0/
4	978040000	0.0	-1.0	0.0/
4	978050000	0.0	-1.0	0.0/
4	978060000	0.0	-1.0	0.0/
1	-813250000	0.0	-1.0	0.0/
1	-877000000	0.0	-1.0	0.0/
1	-978010000	0.0	-1.0	0.0/
1	-978020000	0.0	-1.0	0.0/
1	-978030000	0.0	-1.0	0.0/
1	-978040000	0.0	-1.0	0.0/
1	-978050000	0.0	-1.0	0.0/
1	-978060000	0.0	-1.0	0.0/
1	-978070000	0.0	-1.0	0.0/

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99999/
 \$STEPS TSTEP(1)=0.001,1.0\$



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TR-5364-1
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4.10.3 Unit 2 - (Quarter Model)

\$PIPES

INLINE=3,KBLOCK=601,KPIPE=0,KPLOT(1)=1,KWAVE=1,
KPRINT=-1,KPNV=1,KSTEP=3,NOROPV=1010000,15010000\$

1	002000000	-1.0	0.0	0.0/
2	-004000000	-1.0	0.0	0.0/
3	004000000	0.0	-1.0	0.0/
3	005010000	0.0	-1.0	0.0/
3	005020000	0.0	-1.0	0.0/
3	005040000	0.0	-1.0	0.0/
3	005050000	0.0	-1.0	0.0/
3	005060000	0.0	-1.0	0.0/
4	-005010000	0.0	-1.0	0.0/
4	-005020000	0.0	-1.0	0.0/
4	-005030000	0.0	-1.0	0.0/
4	-005040000	0.0	-1.0	0.0/
4	-005050000	0.0	-1.0	0.0/
4	-005060000	0.0	-1.0	0.0/
4	-005070000	0.0	-1.0	0.0/
5	005070000	-1.0	0.0	0.0/
5	005080000	-1.0	0.0	0.0/
5	005090000	-1.0	0.0	0.0/
6	-005080000	-1.0	0.0	0.0/
6	-005090000	-1.0	0.0	0.0/
6	-005100000	-1.0	0.0	0.0/
7	005100000	0.0	1.0	0.0/
7	005110000	0.0	1.0	0.0/
7	005120000	0.0	1.0	0.0/
7	005130000	0.0	1.0	0.0/
7	005140000	0.0	1.0	0.0/
7	005150000	0.0	1.0	0.0/
7	005160000	0.0	1.0	0.0/
7	005170000	0.0	1.0	0.0/
7	005180000	0.0	1.0	0.0/
7	005190000	0.0	1.0	0.0/
8	-005110000	0.0	1.0	0.0/
8	-005120000	0.0	1.0	0.0/
8	-005130000	0.0	1.0	0.0/
8	-005140000	0.0	1.0	0.0/
8	-005150000	0.0	1.0	0.0/
8	-005160000	0.0	1.0	0.0/
8	-005170000	0.0	1.0	0.0/
8	-005180000	0.0	1.0	0.0/
8	-005190000	0.0	1.0	0.0/
8	-008000000	0.0	1.0	0.0/
9	008000000	-1.0	0.0	0.0/
9	007010000	-1.0	0.0	0.0/
9	007020000	-1.0	0.0	0.0/
9	007030000	-1.0	0.0	0.0/
10	-007010000	-1.0	0.0	0.0/
10	-007020000	-1.0	0.0	0.0/
10	-007030000	-1.0	0.0	0.0/
10	-007040000	-1.0	0.0	0.0/
11	007040000	0.0	-1.0	0.0/
11	007050000	0.0	-1.0	0.0/
11	007080000	0.0	-1.0	0.0/
11	007070000	0.0	-1.0	0.0/
11	007080000	0.0	-1.0	0.0/
11	007090000	0.0	-1.0	0.0/
11	007100000	0.0	-1.0	0.0/
11	007110000	0.0	-1.0	0.0/

BY CHM DATE 2-9-83
CHKD. BY LOS DATE 2-9-83



11	007120000	0.0	-1.0	0.0/
11	007130000	0.0	-1.0	0.0/
12	-007050000	0.0	-1.0	0.0/
12	-007060000	0.0	-1.0	0.0/
12	-007070000	0.0	-1.0	0.0/
12	-007080000	0.0	-1.0	0.0/
12	-007090000	0.0	-1.0	0.0/
12	-007100000	0.0	-1.0	0.0/
12	-007110000	0.0	-1.0	0.0/
12	-007120000	0.0	-1.0	0.0/
12	-007130000	0.0	-1.0	0.0/
12	-007140000	0.0	-1.0	0.0/
14	007140000	-.258	0.0	-.966/
14	007150000	-.258	0.0	-.966/
14	007160000	-.258	0.0	-.966/
15	-007150000	-.258	0.0	-.966/
15	-007160000	-.258	0.0	-.966/
15	-007170000	-.258	0.0	-.966/
16	007170000	.337	0.0	-.942/
16	007180000	.337	0.0	-.942/
16	007190000	.337	0.0	-.942/
17	-007180000	.337	0.0	-.942/
17	-007190000	.337	0.0	-.942/
17	-007200000	.337	0.0	-.942/
18	007200000	.793	0.0	-.609/
18	007210000	.793	0.0	-.609/
18	007220000	.793	0.0	-.609/
19	-007210000	.793	0.0	-.609/
19	-007220000	.793	0.0	-.609/
19	-007230000	.793	0.0	-.609/
20	007230000	.994	0.0	-.1132/
20	007240000	.994	0.0	-.1132/
20	007250000	.994	0.0	-.1132/
21	-007240000	.994	0.0	-.1132/
21	-007250000	.994	0.0	-.1132/
21	-007260000	.994	0.0	-.1132/
22	007260000	.910	0.0	.415/
22	007270000	.910	0.0	.415/
22	007280000	.910	0.0	.415/
23	-007270000	.910	0.0	.415/
23	-007280000	.910	0.0	.415/
23	-007290000	.910	0.0	.415/
24	007290000	.555	0.0	.8321/
24	007300000	.555	0.0	.8321/
24	007310000	.555	0.0	.8321/
25	-007300000	.555	0.0	.8321/
25	-007310000	.555	0.0	.8321/
25	-007320000	.555	0.0	.8321/
26	007320000	.0183	0.0	.9998/
26	007330000	.0183	0.0	.9998/
26	007340000	.0183	0.0	.9998/
27	-007330000	.0183	0.0	.9998/
27	-007340000	.0183	0.0	.9998/
27	-007350000	.0183	0.0	.9998/
28	007350000	-.264	0.0	.965/
28	007360000	-.264	0.0	.965/
28	007370000	-.264	0.0	.965/
28	007380000	-.264	0.0	.965/
28	-007360000	-.264	0.0	.965/
28	-007370000	-.264	0.0	.965/

29	-007380000	-.284	0.0	.965/
29	-008000000	-.264	0.0	.965/
30	008000000	0.0	-1.0	0.0/
30	010000000	0.0	-1.0	0.0/
30	011010000	0.0	-1.0	0.0/
30	011020000	0.0	-1.0	0.0/
30	011030000	0.0	-1.0	0.0/
30	011040000	0.0	-1.0	0.0/
30	011050000	0.0	-1.0	0.0/
30	011060000	0.0	-1.0	0.0/
30	011070000	0.0	-1.0	0.0/
30	011080000	0.0	-1.0	0.0/
30	011090000	0.0	-1.0	0.0/
30	011100000	0.0	-1.0	0.0/
30	011110000	0.0	-1.0	0.0/
30	011120000	0.0	-1.0	0.0/
30	011130000	0.0	-1.0	0.0/
31	-010000000	0.0	-1.0	0.0/
31	-011010000	0.0	-1.0	0.0/
31	-011020000	0.0	-1.0	0.0/
31	-011030000	0.0	-1.0	0.0/
31	-011040000	0.0	-1.0	0.0/
31	-011050000	0.0	-1.0	0.0/
31	-011060000	0.0	-1.0	0.0/
31	-011070000	0.0	-1.0	0.0/
31	-011080000	0.0	-1.0	0.0/
31	-011090000	0.0	-1.0	0.0/
31	-011100000	0.0	-1.0	0.0/
31	-011110000	0.0	-1.0	0.0/
31	-011120000	0.0	-1.0	0.0/
31	-011130000	0.0	-1.0	0.0/
31	-011140000	0.0	-1.0	0.0/
32	011140000	.316	-.707	-.948/
32	011150000	.316	-.707	-.948/
32	011160000	.316	-.707	-.948/
32	011170000	.316	-.707	-.948/
33	-011150000	.316	-.707	-.948/
33	-011160000	.316	-.707	-.948/
33	-011170000	.316	-.707	-.948/
33	-011180000	.316	-.707	-.948/
34	011180000	0.0	-1.0	0.0/
34	011190000	0.0	-1.0	0.0/
34	011200000	0.0	-1.0	0.0/
34	011210000	0.0	-1.0	0.0/
35	-011200000	0.0	-1.0	0.0/
35	-011210000	0.0	-1.0	0.0/
35	-011220000	0.0	-1.0	0.0/
36	011220000	-.316	-.707	.948/
36	011230000	-.316	-.707	.948/
36	011240000	-.316	-.707	.948/
36	011250000	-.316	-.707	.948/
37	-011230000	-.316	-.707	.948/
37	-011240000	-.316	-.707	.948/
37	-011250000	-.316	-.707	.948/
37	-011260000	-.316	-.707	.948/
38	011260000	0.0	-1.0	0.0/
38	011270000	0.0	-1.0	0.0/
38	011280000	0.0	-1.0	0.0/
38	011290000	0.0	-1.0	0.0/
38	011300000	0.0	-1.0	0.0/

38	011310000	0.0	-1.0	0.0/
38	011320000	0.0	-1.0	0.0/
38	011330000	0.0	-1.0	0.0/
38	011340000	0.0	-1.0	0.0/
38	011350000	0.0	-1.0	0.0/
38	011360000	0.0	-1.0	0.0/
38	011370000	0.0	-1.0	0.0/
38	011380000	0.0	-1.0	0.0/
38	011390000	0.0	-1.0	0.0/
38	011400000	0.0	-1.0	0.0/
38	011410000	0.0	-1.0	0.0/
38	011420000	0.0	-1.0	0.0/
38	011430000	0.0	-1.0	0.0/
38	011440000	0.0	-1.0	0.0/
38	011450000	0.0	-1.0	0.0/
38	011460000	0.0	-1.0	0.0/
38	011470000	0.0	-1.0	0.0/
38	011480000	0.0	-1.0	0.0/
38	011490000	0.0	-1.0	0.0/
38	011500000	0.0	-1.0	0.0/
38	011510000	0.0	-1.0	0.0/
38	011520000	0.0	-1.0	0.0/
38	011530000	0.0	-1.0	0.0/
38	011540000	0.0	-1.0	0.0/
38	011550000	0.0	-1.0	0.0/
39	-011270000	0.0	-1.0	0.0/
39	-011280000	0.0	-1.0	0.0/
39	-011290000	0.0	-1.0	0.0/
39	-011300000	0.0	-1.0	0.0/
39	-011310000	0.0	-1.0	0.0/
39	-011320000	0.0	-1.0	0.0/
39	-011330000	0.0	-1.0	0.0/
39	-011340000	0.0	-1.0	0.0/
39	-011350000	0.0	-1.0	0.0/
39	-011360000	0.0	-1.0	0.0/
39	-011370000	0.0	-1.0	0.0/
39	-011380000	0.0	-1.0	0.0/
39	-011390000	0.0	-1.0	0.0/
39	-011400000	0.0	-1.0	0.0/
39	-011410000	0.0	-1.0	0.0/
39	-011420000	0.0	-1.0	0.0/
39	-011430000	0.0	-1.0	0.0/
39	-011440000	0.0	-1.0	0.0/
39	-011450000	0.0	-1.0	0.0/
39	-011460000	0.0	-1.0	0.0/
39	-011470000	0.0	-1.0	0.0/
39	-011480000	0.0	-1.0	0.0/
39	-011490000	0.0	-1.0	0.0/
39	-011500000	0.0	-1.0	0.0/
39	-011510000	0.0	-1.0	0.0/
39	-011520000	0.0	-1.0	0.0/
39	-011530000	0.0	-1.0	0.0/
39	-011540000	0.0	-1.0	0.0/
39	-011550000	0.0	-1.0	0.0/
39	-011560000	0.0	-1.0	0.0/
40	011560000	0.0	0.0	-1.0/
40	011570000	0.0	0.0	-1.0/
40	011580000	0.0	0.0	-1.0/
40	011590000	0.0	0.0	-1.0/
40	011600000	0.0	0.0	-1.0/

40	011610000	0.0	0.0	-1.0/
40	011620000	0.0	0.0	-1.0/
40	011630000	0.0	0.0	-1.0/
40	011640000	0.0	0.0	-1.0/
40	011650000	0.0	0.0	-1.0/
41	-011570000	0.0	0.0	-1.0/
41	-011580000	0.0	0.0	-1.0/
41	-011590000	0.0	0.0	-1.0/
41	-011600000	0.0	0.0	-1.0/
41	-011610000	0.0	0.0	-1.0/
41	-011620000	0.0	0.0	-1.0/
41	-011630000	0.0	0.0	-1.0/
41	-011640000	0.0	0.0	-1.0/
41	-011650000	0.0	0.0	-1.0/
41	-011660000	0.0	0.0	-1.0/
42	011660000	-.259	0.0	.966/
42	011670000	-.259	0.0	.966/
42	011680000	-.259	0.0	.966/
42	011690000	-.259	0.0	.966/
42	011700000	-.259	0.0	.966/
42	011710000	-.259	0.0	.966/
42	011720000	-.259	0.0	.966/
42	011730000	-.259	0.0	.966/
42	011740000	-.259	0.0	.966/
42	011750000	-.259	0.0	.966/
42	011760000	-.259	0.0	.966/
42	011770000	-.259	0.0	.966/
42	011780000	-.259	0.0	.966/
43	-011670000	-.259	0.0	.966/
43	-011680000	-.259	0.0	.966/
43	-011690000	-.259	0.0	.966/
43	-011700000	-.259	0.0	.966/
43	-011710000	-.259	0.0	.966/
43	-011720000	-.259	0.0	.966/
43	-011730000	-.259	0.0	.966/
43	-011740000	-.259	0.0	.966/
43	-011750000	-.259	0.0	.966/
43	-011760000	-.259	0.0	.966/
43	-011770000	-.259	0.0	.966/
43	-011780000	-.259	0.0	.966/
43	-011790000	-.259	0.0	.966/
44	011790000	-1.0	0.0	0.0/
44	011800000	-1.0	0.0	0.0/
44	011810000	-1.0	0.0	0.0/
44	011820000	-1.0	0.0	0.0/
44	011830000	-1.0	0.0	0.0/
44	011840000	-1.0	0.0	0.0/
44	011850000	-1.0	0.0	0.0/
44	011860000	-1.0	0.0	0.0/
45	-011800000	-1.0	0.0	0.0/
45	-011810000	-1.0	0.0	0.0/
45	-011820000	-1.0	0.0	0.0/
45	-011830000	-1.0	0.0	0.0/
45	-011840000	-1.0	0.0	0.0/
45	-011850000	-1.0	0.0	0.0/
45	-011860000	-1.0	0.0	0.0/
45	-011870000	-1.0	0.0	0.0/
46	011870000	0.0	-1.0	0.0/
46	011880000	0.0	-1.0	0.0/
46	011890000	0.0	-1.0	0.0/

48	011900000	0.0	-1.0	0.0/
48	011910000	0.0	-1.0	0.0/
48	011920000	0.0	-1.0	0.0/
48	011930000	0.0	-1.0	0.0/
48	011940000	0.0	-1.0	0.0/
47	-011880000	0.0	-1.0	0.0/
47	-011890000	0.0	-1.0	0.0/
47	-011900000	0.0	-1.0	0.0/
47	-011910000	0.0	-1.0	0.0/
47	-011920000	0.0	-1.0	0.0/
47	-011830000	0.0	-1.0	0.0/
47	-011940000	0.0	-1.0	0.0/
47	-011950000	0.0	-1.0	0.0/
48	011950000	-1.0	0.0	0.0/
48	011960000	-1.0	0.0	0.0/
48	011970000	-1.0	0.0	0.0/
48	011980000	-1.0	0.0	0.0/
48	011990000	-1.0	0.0	0.0/
48	012000000	-1.0	0.0	0.0/
48	013010000	-1.0	0.0	0.0/
48	013020000	-1.0	0.0	0.0/
48	013030000	-1.0	0.0	0.0/
48	013040000	-1.0	0.0	0.0/
48	013050000	-1.0	0.0	0.0/
49	-011960000	-1.0	0.0	0.0/
49	-011970000	-1.0	0.0	0.0/
49	-011980000	-1.0	0.0	0.0/
49	-011990000	-1.0	0.0	0.0/
49	-012000000	-1.0	0.0	0.0/
49	-013010000	-1.0	0.0	0.0/
49	-013020000	-1.0	0.0	0.0/
49	-013030000	-1.0	0.0	0.0/
49	-013040000	-1.0	0.0	0.0/
49	-013050000	-1.0	0.0	0.0/
49	-013060000	-1.0	0.0	0.0/
50	013060000	0.0	0.0	-1.0/
50	013070000	0.0	0.0	-1.0/
50	013080000	0.0	0.0	-1.0/
50	013090000	0.0	0.0	-1.0/
50	013100000	0.0	0.0	-1.0/
50	013110000	0.0	0.0	-1.0/
50	013120000	0.0	0.0	-1.0/
50	013130000	0.0	0.0	-1.0/
50	013140000	0.0	0.0	-1.0/
50	013150000	0.0	0.0	-1.0/
50	013160000	0.0	0.0	-1.0/
50	013170000	0.0	0.0	-1.0/
50	013180000	0.0	0.0	-1.0/
50	013190000	0.0	0.0	-1.0/
51	-013070000	0.0	0.0	-1.0/
51	-013080000	0.0	0.0	-1.0/
51	-013090000	0.0	0.0	-1.0/
51	-013100000	0.0	0.0	-1.0/
51	-013110000	0.0	0.0	-1.0/
51	-013120000	0.0	0.0	-1.0/
51	-013130000	0.0	0.0	-1.0/
51	-013140000	0.0	0.0	-1.0/
51	-013150000	0.0	0.0	-1.0/
51	-013160000	0.0	0.0	-1.0/
51	-013170000	0.0	0.0	-1.0/



51	-013180000	0.0	0.0	-1.0/
51	-013190000	0.0	0.0	-1.0/
51	-013200000	0.0	0.0	-1.0/
52	013200000	1.0	0.0	0.0/
52	013210000	1.0	0.0	0.0/
52	013220000	1.0	0.0	0.0/
52	013230000	1.0	0.0	0.0/
52	013240000	1.0	0.0	0.0/
52	013250000	1.0	0.0	0.0/
52	013260000	1.0	0.0	0.0/
52	013270000	1.0	0.0	0.0/
52	013280000	1.0	0.0	0.0/
52	013290000	1.0	0.0	0.0/
53	-013210000	1.0	0.0	0.0/
53	-013220000	1.0	0.0	0.0/
53	-013230000	1.0	0.0	0.0/
53	-013240000	1.0	0.0	0.0/
53	-013250000	1.0	0.0	0.0/
53	-013260000	1.0	0.0	0.0/
53	-013270000	1.0	0.0	0.0/
53	-013280000	1.0	0.0	0.0/
53	-013290000	1.0	0.0	0.0/
53	-014000000	1.0	0.0	0.0/

99999/
\$STEPS TSTEP(I)=0.001,0.600\$

Technical Report
TR-5364-1
Revision 0

4-504

 **TELEDYNE
ENGINEERING SERVICES**

4.11 APPENDIX A

BY JM DATE 8-24-82
 CHKD. BY SGC DATE 8-25-82
JK 6-1-85

AMERICAN ELECTRIC POWER
 D.C. COOK UNITS 1 & 2
 PIPE PROPERTIES

SHEET NO. 1 OF 1
 PROJ. NO. 5364

PIPE PROPERTIES

SIZE	SCHEDULE	I.D. (in.)	FLOW AREA (ft ²)	FRICION FACTOR f	ϵ/d	ROUGHNESS ϵ (ft)	* K _{ELBOW} 125
3"	40	3.068	.05132	.0174	.0006	1.53×10^{-4}	.2088
3"	160	2.624	.03757	.0181	.0007	1.53×10^{-4}	.2172
4"	40	4.026	.08840	.0161	.0004	1.34×10^{-4}	.1932
4"	120	3.624	.07160	.0162	.00044	1.33×10^{-4}	.1944
6"	40	6.065	.20069	.015	.0003	1.52×10^{-4}	.1800
6"	160	5.189	.14653	.0153	.00035	1.51×10^{-4}	.1836
12"	40	11.938	.77708	.013	.00017	1.69×10^{-4}	.1560

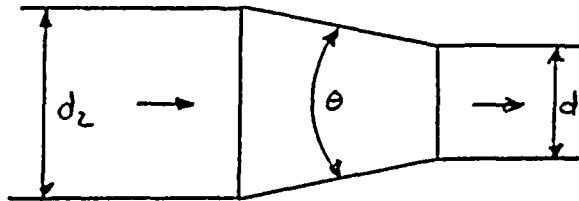
* RESISTANCE DUE TO BEND ONLY FOR 1.5d BENDS

REF: CRANE TECHNICAL PAPER No. 410

BY JBM DATE 12-8-82
 CHKD. BY J.E.Y. DATE 12-8-82
287 6-1-83

AMERICAN ELECTRIC POWER
 D.C. COOK UNITS 1 & 2
 LOSSES IN REDUCERS

SHEET NO. 1 OF 1
 PROJ. NO. 5364



$$\beta = \frac{d_1}{d_2}$$

IF: $\theta \leq 45^\circ$

FORWARD LOSS COEFFICIENTS

$$K = 0.8 \left(\sin \frac{\theta}{2} \right) (1 - \beta^2)$$

REVERSE LOSS COEFFICIENTS

$$K = 2.0 \left(\sin \frac{\theta}{2} \right) (1 - \beta^2)^2$$

SIZE	d_1	d_2	β	θ	$K, \text{ FORWARD}$	$K, \text{ REVERSE}$
17" SCH 40 x 6" SCH 40S	6.065"	11.938"	.5080	40.3°	.2045	.4930
6" SCH 40S x 4" SCH 40S	4.026"	6.065"	.6638	21°	.0815	.1483
4" SCH 40S x 3" SCH 40	3.068"	4.026"	.7620	13.66°	.0399	.0544
3" SCH 160 x 4" SCH 120	2.624"	3.624"	.7241	14.25°	.0472	.0730
4" SCH 120 x 6" SCH 160	3.624"	5.189"	.6984	16.19°	.0577	.0961
6" SCH 40S x 3" SCH 40	3.068"	6.065"	.5059	30.48°	.1565	.3784

REFERENCE: CRANE TECHNICAL PAPER 410 p. A-26

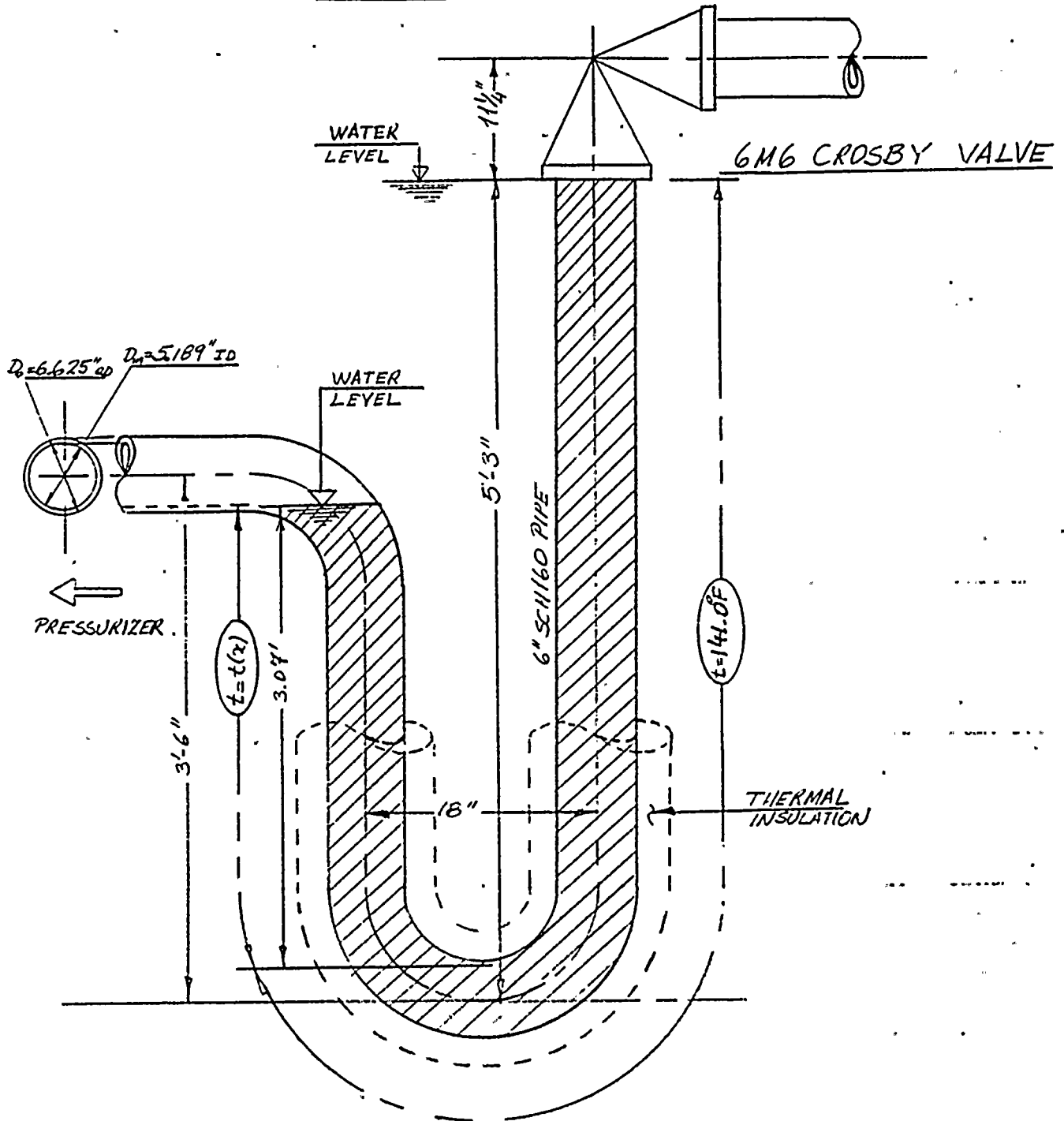
K IS TAKEN WITH RESPECT TO THE SMALLER DIAMETER PIPE.




BY BAT DATE 12-17-82
CHKD. BY JMM DATE 1-3-84

AEP D.C. COOK UNIT 1
SV LINE LOOP SEAL TEMP DISTRIBUTION

SHEET NO. 1 OF 12
PROJ. NO. 5364



 INDICATES TEMPERATURE VARIATIONS IN LOOP SEAL (REF. TEXT)

D.C. COOK UNIT 1
SAFETY VALVE LINE-LOOP SEAL
GEOMETRY

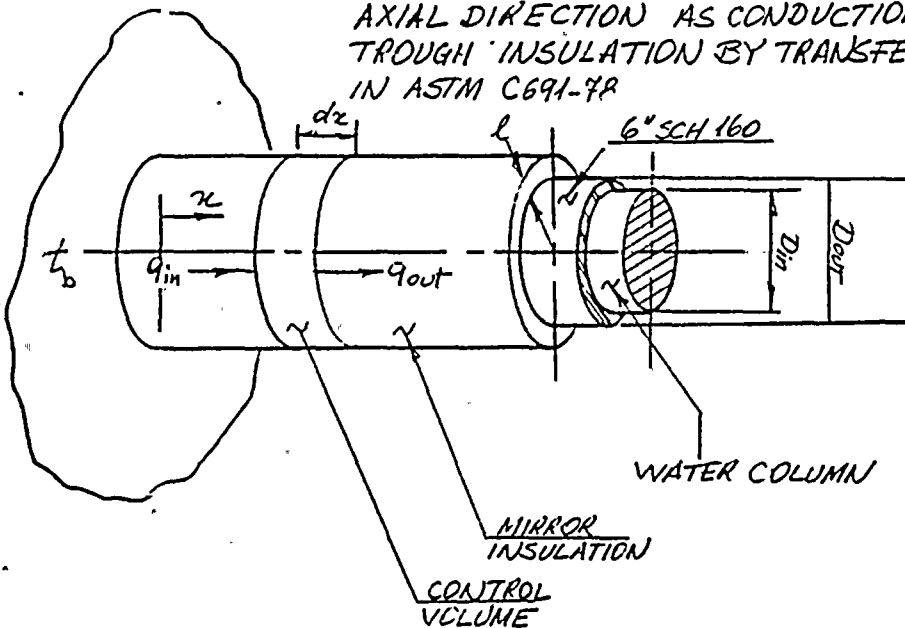
BY BAI DATE 12-17-88
 CHKD. BY CMU DATE 1-7-83

AEP D.C. COOK UNIT 1
 SV LINE LOOP SEAL TEMP. DISTRIBUTION

SHEET NO. 2 OF 12
 PROJ. NO. 5364

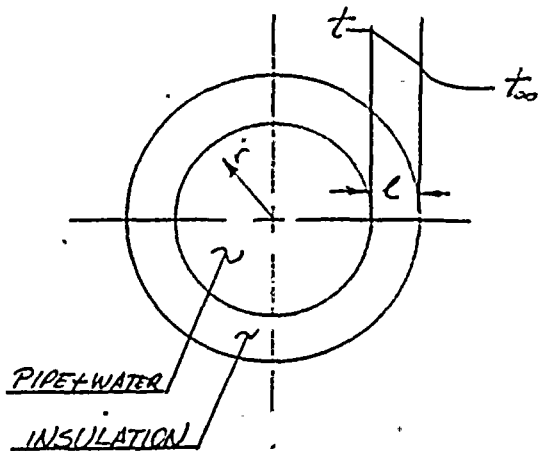
DERIVATION OF ENERGY EQUATION

ASSUMPTION 1: LOOP SEAL PIPING IS MODELED AS STRAIGHT PIPE WITH FINITE LENGTH WITH BOUNDARY CONDITIONS DESCRIBED BELOW. HEAT IS TRANSFERRED BOTH IN AXIAL DIRECTION AS CONDUCTION AND IN RADIAL DIRECTION THROUGH INSULATION BY TRANSFERENCE EQUATION AS DESCRIBED IN ASTM C691-78



PIPE MODEL

ASSUMPTION 2: TEMPERATURE ACROSS CROSS-SECTION OF THE PIPE INCLUDING WATER AND WALL IS CONSTANT.



$$q_{in} \text{ (CONDUCTED INTO ELEMENT)} = [(KA)_{PIPE} + (KA)_{WATER}] \frac{dt}{dx}$$

$$q_{in} = -(KA)_{eff} \frac{dt}{dx} \quad \text{WHERE } (KA)_{eff} = (KA)_{PIPE} + (KA)_{WATER}$$

$$q_{out} \text{ (CONDUCTED OUT OF ELEMENT)} = q_{in} + \Delta q$$

$$q_{out} = \left[-(KA)_{eff} \frac{dt}{dx} + \frac{d}{dx} \left(-(KA)_{eff} \frac{dt}{dx} \right) dx \right]$$

TEMPERATURE DISTRIBUTION ACROSS THE CROSS-SECTION OF PIPE

BY BAT DATE 12-14-82
CHKD. BY MM DATE 1-7-83

AEP D.C. COOK UNIT 1
SV LINE LOOP SEAL TEMP. DISTRIBUTION

SHEET NO. 3 OF 12
PROJ. NO. 5364

$(KA)_{eff}$ = EQUIVALENT THERMAL CONDUCTANCE OF PIPE IN AXIAL DIRECTION
 t = TEMPERATURE AS A FUNCTION OF x
 q_s (TRANSFERRED OUT OF SURFACE OF THE PIPE) = $T_r A_s (t_{in} - t_{\infty})$

(REF: ASTM C691-78)

WHERE: A_s = SURFACE AREA OF PIPE (ft^2) = $\pi D_o dx$
 t_{in} = TEMPERATURE OF PIPE & WATER (ASSUMED EQUAL)
 t_{∞} = PIPE ENVIRONMENT TEMPERATURE = $120^\circ F$
 T_r = THERMAL TRANSFERENCE $\frac{Btu}{hr-ft^2-F}$

ENERGY EQUATION FOR THE CONTROL VOLUME

$$q_{in} = q_{out} + q_s$$

$$-(KA)_{eff} \frac{dt}{dx} = \left\{ -(KA)_{eff} \frac{dt}{dx} + \frac{d}{dx} \left[-(KA)_{eff} \frac{dt}{dx} \right] dx \right\} + T_r \pi D_o dx (t - t_{\infty})$$

$$(KA)_{eff} \frac{d^2 t}{dx^2} = T_r \pi D_o (t - t_{\infty})$$

LET $\theta = t - t_{\infty}$ THEN $\frac{d\theta}{dx} = \frac{dt}{dx}$ AND $\frac{d^2\theta}{dx^2} = \frac{d^2t}{dx^2}$

LET $m^2 = \frac{T_r \pi D_o}{(KA)_{eff}}$

THEREFORE:

$$\frac{d^2\theta}{dx^2} = m^2 \theta$$

$$\theta = C_1 e^{mx} + C_2 e^{-mx}$$

$$t = C_1 e^{mx} + C_2 e^{-mx} + 120$$

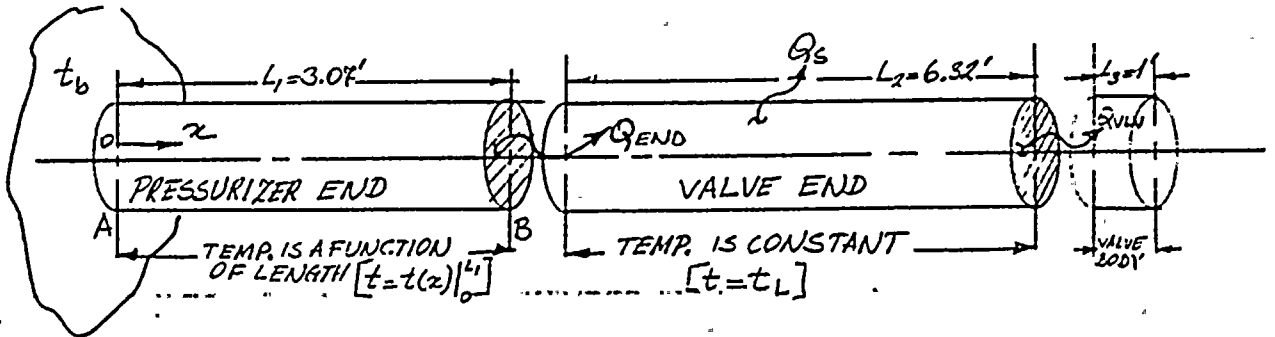
EQUATION-①
GENERAL TEMPERATURE
DISTRIBUTION EQN.

BY BAT DATE 12-20-82
 CHKD. BY MH DATE 1-7-83

AEP D. C. COOK UNIT 1
 S.V. LINE LOOP SEAL TEMP. DISTRIBUTION

SHEET NO. 4 OF 12
 PROJ. NO. 5364

ASSUMPTION 3. TEMPERATURE VARIES ONLY IN THE PRESSURIZER END OF THE LOOP SEAL AND REMAINS CONSTANT AT THE VALVE END OF THE LOOP SEAL. THIS IS DUE TO THE CIRCULATION OF WATER IN THE VALVE END OF LOOP SEAL BECAUSE OF NATURAL CONVECTION (REF. PAGE 1 OF THIS ANALYSIS)



LOOP SEAL MODEL

BOUNDARY CONDITIONS FOR EQN 1

- 1- $x = 0 \quad t = t_b = 668^\circ\text{F}$ (SAT. STEAM TEMP. @ 2500 psia)
- 2- $x = 3.07 \text{ ft} \quad -(kA)_{\text{eff}} \left. \frac{dt}{dx} \right|_{x=3.07} = Q_{\text{END}}$

$$-(kA)_{\text{eff}} [mC_1 e^{mx} - mC_2 e^{-mx}] = Q_{\text{END}} \quad \text{EQU. (2)}$$

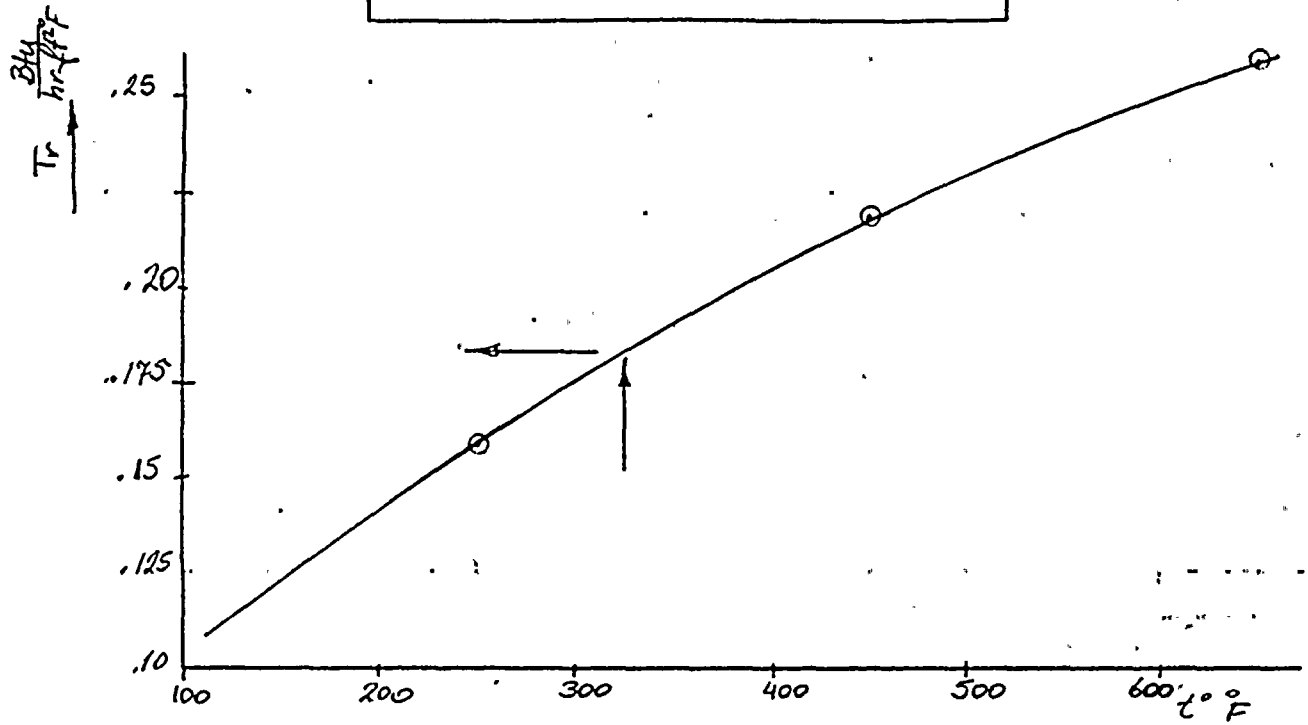
C₁ AND C₂ ARE FOUND FROM EQN. 1 AND EQN. 2
 T_r (TRANSMISSIVITY) IS A FUNCTION OF TEMPERATURE AND FROM THE TELECON BETWEEN "TES" AND "DIAMOND POWER" DATED (12-16-82)

$T_r \frac{\text{Btu}}{\text{hr ft}^2 \text{ }^\circ\text{F}}$	TEMP $^\circ\text{F}$
0.259	650
0.219	450
0.158	250

BY BAI DATE 12-20-82
 CHKD. BY CMM DATE 1-7-83

AEP D.C. COOK UNIT 1
 S.V. LINE LOOP SEAL TEMP. DISTRIBUTION

SHEET NO. 5 OF 12
 PROJ. NO. 5364



PLOT OF TRANSMISSIVITY VS TEMPERATURE FROM DATA ON TELECON BETWEEN "TES" AND "DIAMOND POWER" DATED (12-16-82).

ASSUMED AVERAGE FLUID TEMPERATURE = 325 °F
 FROM PLOT $T_r = 0.182 \frac{\text{Btu}}{\text{hr-ft}^2 \cdot \text{F}}$ @ $t = 325 \text{ °F}$

$$(KA)_{\text{eff}} = (KA)_{\text{PIPE}} + (KA)_{\text{WATER}}$$

$$A_{\text{PIPE}} = 13.22 \text{ in}^2$$

$$A_{\text{WATER}} = 21.1 \text{ in}^2$$

ESTIMATED AVERAGE VALUES

$$K_{\text{PIPE}} \approx 7.9 \frac{\text{Btu}}{\text{hr-ft}^2 \cdot \text{F}} \quad (\text{REF: PIPE MAT. SPECT DCCPM104QCS PROVIDED BY AEP AND ASME III BOILER \& PRESSURE VESSEL CODE})$$

$$K_{\text{WATER}} = 0.38 \frac{\text{Btu}}{\text{hr-ft}^2 \cdot \text{F}} \quad (\text{REF: HEAT TRANSFER; J. P. HOLMAN Fig 1.5})$$

FIRST EDITION

$$(KA)_{\text{eff}} = 0.48 \frac{\text{Btu-ft}}{\text{hr-F}}$$

(*NOTE: PIPE IS MADE OF ASTM A-376 GRADE TP316 SEAMLESS AUSTENITIC STEEL)

14



BY BAI DATE 12-21-82
CHKD. BY CMM DATE 1-7-83

AEP D.C. COOK UNIT 1
S.V. LINE LOOPSEAL TEMP. DISTRIBUTION

SHEET NO. 6 OF 12
PROJ. NO. 5364

ASSUME $t = 145^{\circ}\text{F}$ AT VALVE END OF LOOPSEAL

$$Q_{\text{END}} = Q_s + Q_{\text{VLV}}$$

Q_s = HEAT LOSS ACROSS INSULATION FROM VALVE END OF LOOP-SEAL

$$Q_s = T_r A_s (t_L - t_{\infty})$$

WHERE $A_s = D_o \pi L_2$ SURFACE AREA OF VALVE END OF LOOPSEAL

$$T_r = 0.120 \frac{\text{Btu}}{\text{ft}^2 \cdot \text{hr} \cdot \text{F}} \quad @ \quad 145^{\circ}\text{F} \quad (\text{FROM PLOT AT PAGES OF THIS ANALYSIS})$$

(NOTE: DIFFERENT T_r IS USED IN EQN. 1 AND Q_s SINCE MEAN TEMPERATURES ARE DIFFERENT)

$$Q_s = (0.120)(0.55 \times \pi \times 6.32)[145 - 120]$$

$$Q_s = 32.76 \frac{\text{Btu}}{\text{hr}}$$

VALVE END HEAT LOSS IS ASSUMED AS HEAT FLOWING THROUGH A SOLID VALVE BODY WITH $L_3 = 1'$ EQUIVALENT LENGTH AND D_o DIAMETER.

$$Q_{\text{VLV}} = (kA)_{\text{steel}} \frac{t_L - t_{\infty}}{L_3}$$

$$Q_{\text{VLV}} = (7.9)(0.24) \frac{145 - 120}{1.0}$$

$$Q_{\text{VLV}} = 47.28 \frac{\text{Btu}}{\text{hr}}$$

$$Q_{\text{END}} = Q_s + Q_{\text{VLV}}$$

$$Q_{\text{END}} = 80.04 \frac{\text{Btu}}{\text{hr}}$$

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BY BAT DATE 12-21-82
 CHKD. BY CHM DATE 1-7-83

A EP D.C. COOK UNIT 1
 S.V LINE LOOP SEAL TEMP. DISTRIBUTION

SHEET NO. 7 OF 12
 PROJ. NO. 5364

TEMPERATURE DISTRIBUTION EQUATION @ $0 < x < L_1 = 3.07$

$$t = C_1 e^{mx} + C_2 e^{-mx} + 120$$

SOLVE FOR C_1 AND C_2 USING BOUNDARY CONDITIONS:

$$x = 0 \quad t = t_b = 668 \text{ }^\circ\text{F} \quad \text{BOUNDARY CON. 1}$$

$$-(kA)_{\text{eff}} \left. \frac{dt}{dx} \right|_{x=L_1} = Q_{\text{END}} \quad \text{BOUNDARY CON. 2}$$

$$-m \times 0.78 [C_1 e^{mL_1} - C_2 e^{-mL_1}] = 80.04$$

$$m = \left[\frac{T_r \pi D_o}{(kA)_{\text{eff}}} \right]^{1/2}$$

$$m = \left[\frac{0.182 \pi \cdot 0.55}{0.78} \right]^{1/2}$$

$$m = 0.64$$

SUBSTITUTING BOUNDARY CONDITIONS:

$$\text{FROM B.C. 1} \quad C_1 e^{0.64(0)} + C_2 e^{-0.64(0)} = 548 \quad \text{EQN. (2)}$$

$$\text{FROM B.C. 2} \quad -C_1 e^{0.64L_1} + C_2 e^{-0.64L_1} = (1.) [Q_s + Q_{\text{vuv}}] \quad \text{EQN. (3)}$$

AFTER SUBSTITUTING

$$C_1 + C_2 = 548$$

$$-7.13 C_1 + 0.14 C_2 = 160.08$$

TWO EQUATIONS WITH TWO UNKNOWN. AFTER SOLVING

$$C_1 = -11.5 \quad \text{AND} \quad C_2 = 559.50$$

1948

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BY BAT DATE 12-21-82
 CHKD. BY LMM DATE 1-7-83

AEP D. C. COOK UNIT 1
 S-V. LINE LOOP SEAL TEMP. DISTRIBUTION

SHEET NO. 8 OF 12
 PROJ. NO. 5364

TEMPERATURE DISTRIBUTION EQUATION BECOMES

$$t = -11.5 e^{0.64x} + 559.5 e^{-0.64x} + 120 \quad @ \quad 0 < x < 3.07$$

CHECKING ASSUMED $t = t_L = 145^\circ$ @ $x = 3.07$

PROCEDURE: FIND $A(t)$ BY SUBSTITUTING $x = 3.07$ AND COMPARE THIS (t) BY ASSUMED $t = 145^\circ F$

$$t = -11.5 e^{(0.64)(3.07)} + 559.5 e^{-(0.64)(3.07)} + 120$$

$$t_{\text{FOUND}} = 116.44^\circ F < t_{\text{ass}} = 145^\circ F$$

... ASSUME: $t = t_L = 135^\circ F$...

EQNS (2) AND (3) BECOMES :

$$\begin{cases} C_1 + C_2 = 54.8 \\ -7.13 C_1 + 0.14 C_2 = 96.20 \end{cases}$$

$Q_{NLV} = 28.44 \text{ Btu/hr}$
 $Q_S = 19.66 \text{ Btu/hr}$
 $Q_{END} = 48.10$

AFTER SOLVING

.. $C_1 = -2.68$..
 $C_2 = 550.68$ AND TEMP. DISTRIBUTION:

$$t = -2.68 e^{0.64x} + 550.68 e^{-0.64x} + 120$$

@ $x = 3.07$ $t_{\text{FOUND}} = 178.08^\circ F > t_{\text{ass}} = 135^\circ F$

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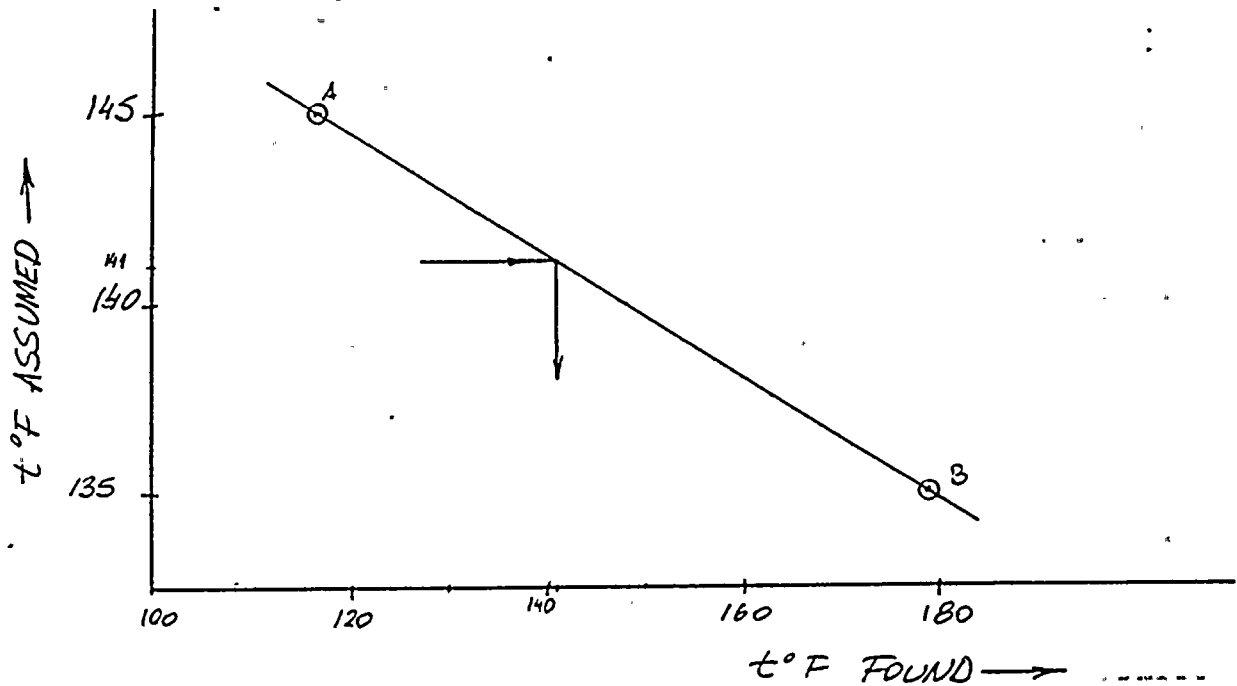
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BY BAI DATE 12-21-82
 CHKD. BY PLM DATE 1-7-83

A EP D.C. COOK UNIT 1
 S.V. LINE LOOP SEAL TEMP. DISTRIBUTION

SHEET NO. 9 OF 12
 PROJ. NO. 5364



AFTER PLOTTING t_{ass} VS. t_{found} AND BY VISUAL INTERPOLATION
 (PROCEDURE: FIND $t_{ass} = t_{found}$ ON LINE A-B)
 NEW $t_{ass} = 141^\circ F$

SUBSTITUTING $t_{ass} = 141^\circ F$, INTO EQN (2) AND EQN (3)

$$Q_s = 27.52 \frac{\text{Btu}}{\text{hr}}$$

$$Q_{VLV} = 39.82 \frac{\text{Btu}}{\text{hr}}$$

$$Q_{END} = 67.34 \text{ Btu/hr}$$

$$\begin{cases} C_1 + C_2 = 548 \\ -7.13C_1 + 0.14C_2 = 134.67 \end{cases}$$

$$C_1 = -7.97$$

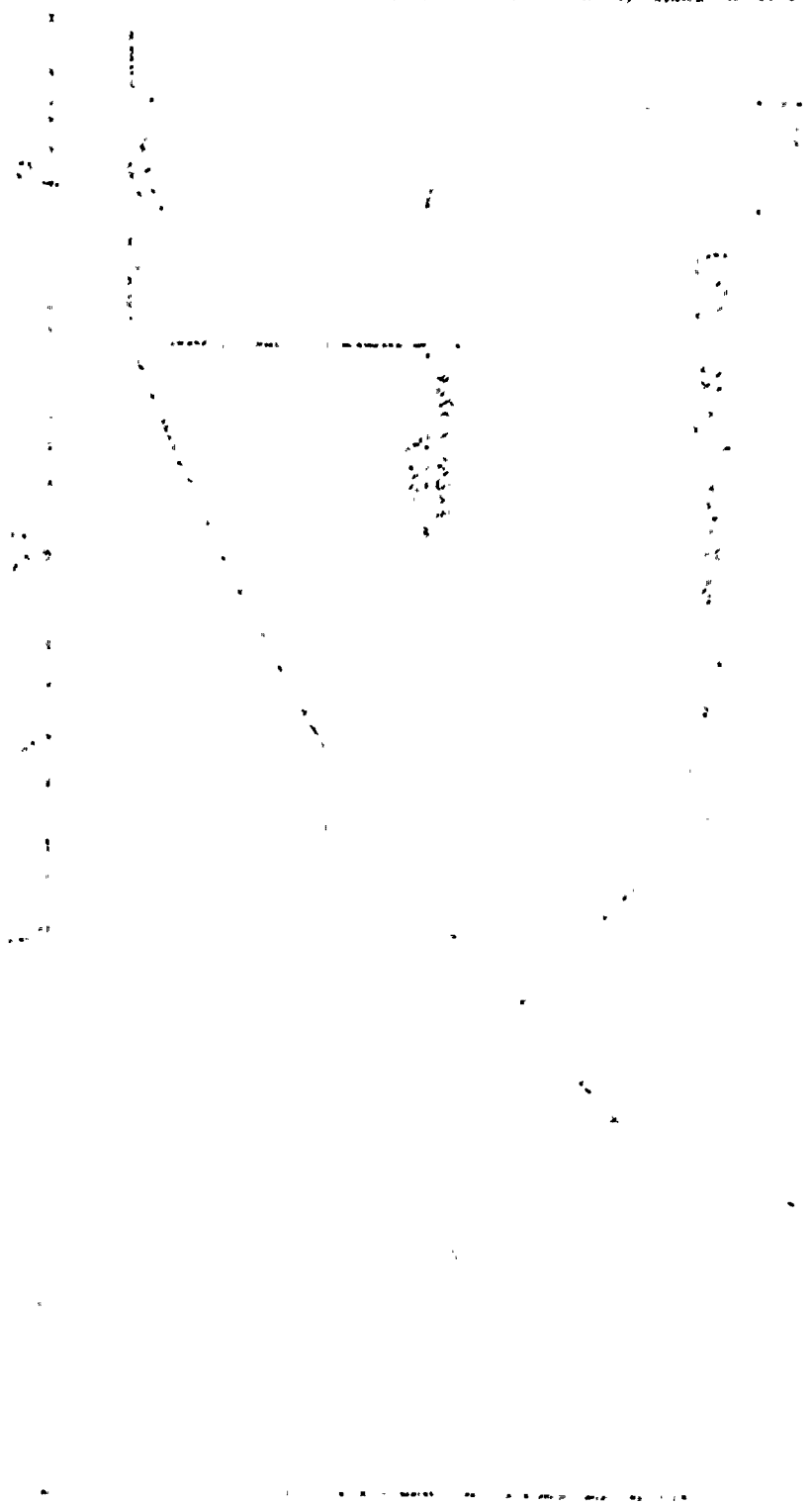
$$C_2 = 555.97$$

$$t = -7.97 e^{0.64x} + 555.97 e^{-0.64x} + 120$$

$$\text{@ } x = 3.07; \quad t_{\text{FOUND}} = 141.08^\circ F \approx t_{ass} = 141.00$$

BY THE BOARD OF TRUSTEES
OF THE UNIVERSITY OF CHICAGO

RESOLUTION
APPROVED BY THE BOARD OF TRUSTEES
ON MAY 12, 1950



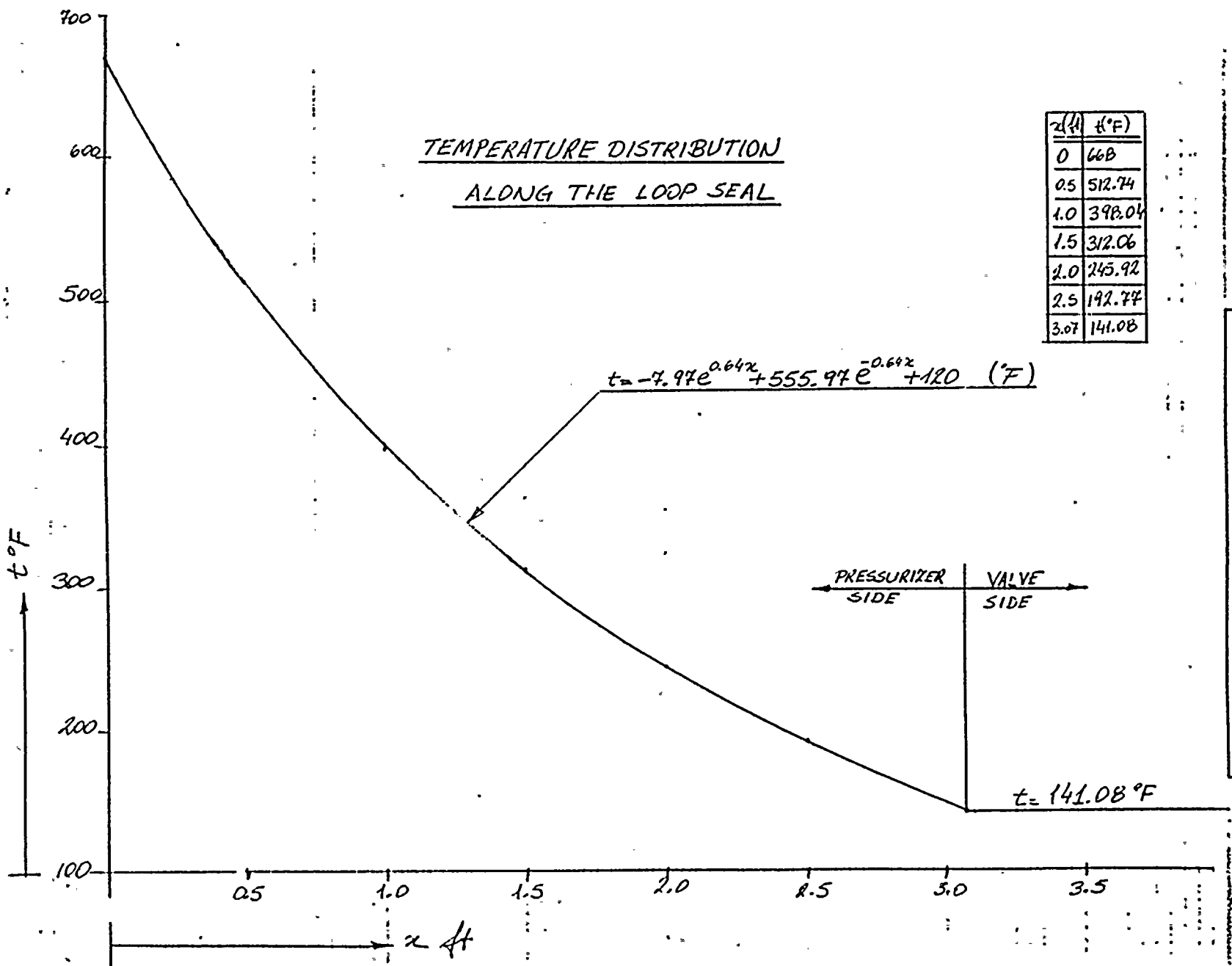
BY BAT DATE 12-21-83
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A E P D. C. COOK
 S. V. LINE LOOP SEAL TEMP DISTRIBUTION

SHEET NO. 10 OF 12
 PROJ. NO. 5364

x (ft)	t (°F)
0	668
0.5	512.74
1.0	398.04
1.5	312.06
2.0	245.92
2.5	192.77
3.07	141.08

TEMPERATURE DISTRIBUTION
ALONG THE LOOP SEAL



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BY BAT DATE 12-21-82
CHKD. BY CLM DATE 1-7-83

AEP D.C. COOK UNIT 1
S.V. LINE LOOP SEAL TEMP. DISTRIBUTION

SHEET NO. 11 OF 12
PROJ. NO. 5364

CHECKING $T_r = 0.182 \frac{\text{Btu}}{\text{hr ft}^2 \text{F}}$ FOR $T_{\text{AVE}} = 325^\circ\text{F}$ (PAGE 5)

AREA UNDER $t = t(x)$ CURVE @ $0 < x < L, = 3.07'$

$$\text{AREA} = \int_0^L t(x) dx$$

$$= \int_0^L [-7.97 e^{(0.64)x} + 555.97 e^{-(.64)x} + 120] dx$$

$$= -\frac{7.97}{0.64} e^{0.64x} \Big|_{x=0}^{3.07} - \frac{555.97}{0.64} e^{-(.64)x} \Big|_{x=0}^{3.07} + 120x \Big|_{x=0}^{3.07}$$

$$= (-88.83 + 12.45) - (121.78 - 868.70) + (368.4)$$

$$\text{AREA} = 1038.94 \text{ F ft}$$

$$t_{\text{AVE}} = \frac{1038.94}{3.07}$$

$$t_{\text{AVE}} = 338.42^\circ\text{F}$$

4% DIFFERENCE FROM THE ASSUMED $t_{\text{AVE}} = 325^\circ\text{F}$

WHICH IS ACCEPTABLE

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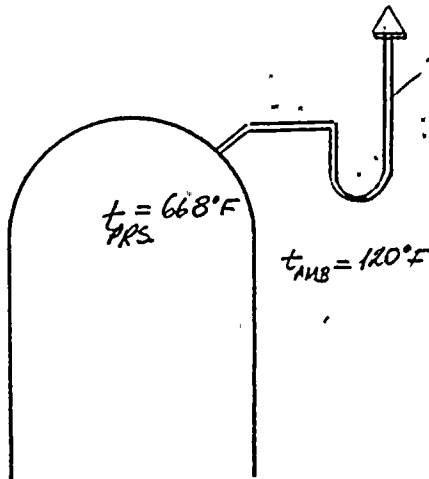
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BY BAI DATE 12-22-82
 CHKD. BY MM DATE 1-7-83

AEP D.C. COOK UNIT 1
 S.V. LINE LOOP SEAL TEMP. DISTRIBUTION

SHEET NO. 12 OF 12
 PROJ. NO. 5364

CHECKING THE RADIATION EFFECTS ON LOOP SEAL BY
TAKING CONSERVATIVE VALUES FOR THE WORST CASE



ASSUME THE LOOP SEAL AS LUMPED VOL.
 AVERAGE TEMPERATURE OF LOOP SEAL

$$t_{AVE} = \frac{C_p A L_1 (338.42) + C_p A L_2 (141.08)}{C_p A (L_1 + L_2)} = 205.6$$

WHERE = ρ : DENSITY
 A : CROSS-SECTIONAL AREA
 C_p : HEAT CAPACITY

$t_{AVE} = 205.60^\circ F = 665.60^\circ R$ $L_1 = 3.0'$
 $L_2 = 6.32'$

FROM PAGE 5 $T_r = .145 \frac{Btu}{hr ft^2 F}$ @ $t = 212.71^\circ F$

$$\frac{q}{A} = (.145)(205.6 - 120) = 12.41 \frac{Btu}{hr ft^2}$$

T_s - SURFACE TEMP. OF LOOP SEAL
 USING NEWTON'S LAW OF
 COOLING : $h = 5 \frac{Btu}{hr F ft^2}$

$$12.41 = 5(T_s - 120)$$

$$T_s = 122.48^\circ F$$

PRESSURIZER :

MAX. HEAT LOSS FROM PRESSURIZER $\frac{q}{A} = 80 \frac{Btu}{ft^2 F hr}$ (REF: METALLIC INSULATION AEP SPEC. NO. DCCSG102RCS)

t_p SURFACE TEMP. OF PRESSURIZER $80 = 5(t_p - 120)$
 $t_p = 136^\circ$

ASSUMING : RADIATION SHAPE FACTORS = 0.5
 EMISSIVITY $\epsilon \cong 0.03$ (SINCE SURFACES ARE MIRROR)
 (REF: MARKS MECH. ENG. HANDBOOK 6th EDITION)

STEFAN-BOLTZMANN CONST. $\sigma = 0.1714 \times 10^{-8} \frac{Btu}{hr ft^2 R^4}$

$$\frac{q}{A}_{RAD} = \epsilon F_{12} (T_p^4 - T_s^4) = (0.03)(0.5)(.1714 \times 10^{-8}) [596^4 - 582^4]$$

$$\frac{q}{A}_{RAD} = 0.294 \frac{Btu}{hr ft^2}$$

RADIATION HEAT TRANSFER HAS NEGLIGIBLE EFFECT ON LOOP SEAL TEMP. DISTRIBUTION

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BY CHM DATE 1-11-82
 CHKD. BY KV DATE 5-24-83

TEMPERATURE DISTRIBUTION
 DETERMINATION - UNIT 2

SHEET NO. 1 OF 1
 PROJ. NO. 5364

USING THE EQUATION:

$$t = -7.97e^{0.64x} + 355.97e^{-0.64x} + 120 \text{ (}^\circ\text{F)}$$

WHERE x = AXIAL DISTANCE AWAY FROM
 PRESSURIZER ALONG LOOP SEAL

ACCURATE $0 \leq x \leq 3.07$ (FT)

FOR VALUES $x > 3.07$ $t = 141.08$ °F

REF: SA3 HAND CALC 12-22-82

CONTROL VOLUME	x VALUE (FT)	t (DETERMINED) (°F)
501	0.25	584.4
502	0.75	451.1
503	1.25	352.1
504	1.75	276.8
505	2.25	218.1
506	2.75	169.3
507	3.25	141.1
↓		↓
520	VALVE	↓

MEMORANDUM FOR THE DIRECTOR

DATE: 10/10/54

TO: DIRECTOR

FROM: SAC, NEW YORK

RE: [Illegible]

[Illegible]

[Illegible]

[Illegible]

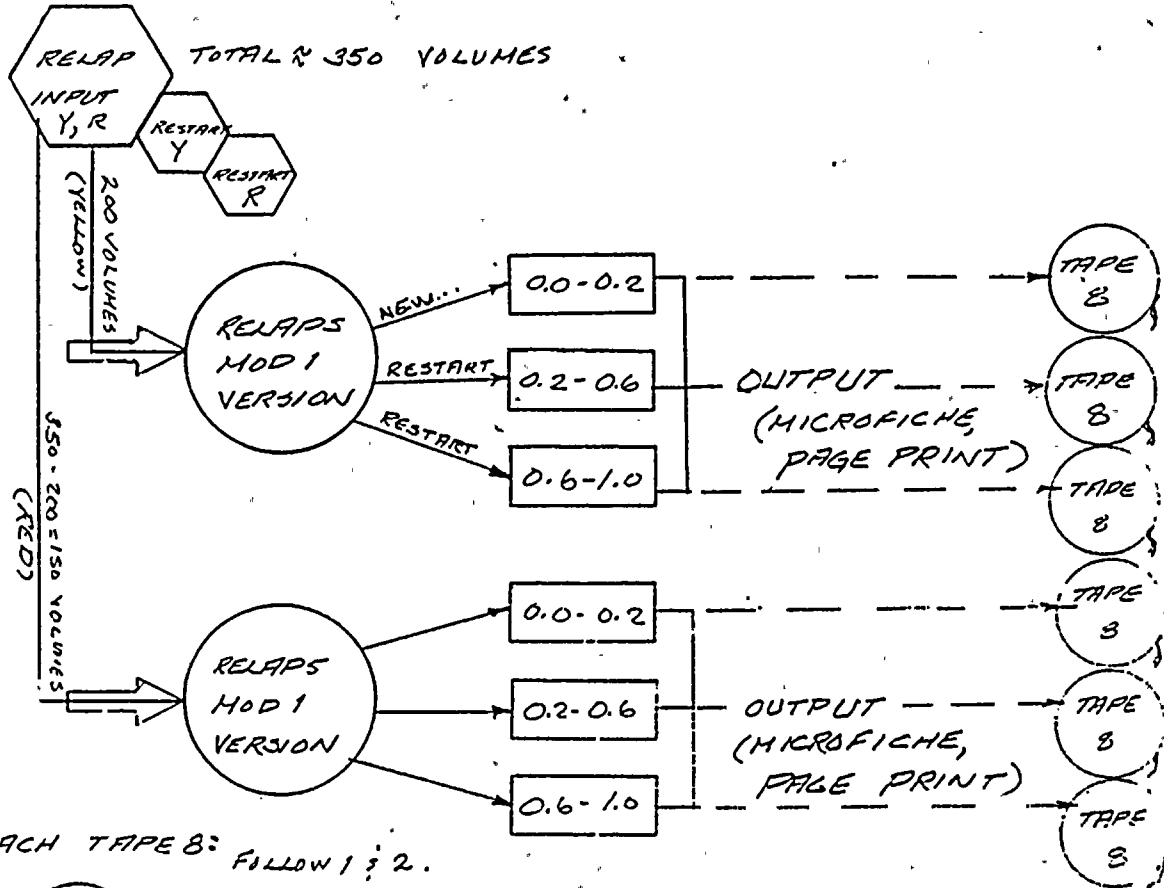
BY CHM DATE 5-4-83
 CHKD. BY KY DATE 5-24-83

COMPUTER USAGE FOR
 THERMAL ANALYSIS

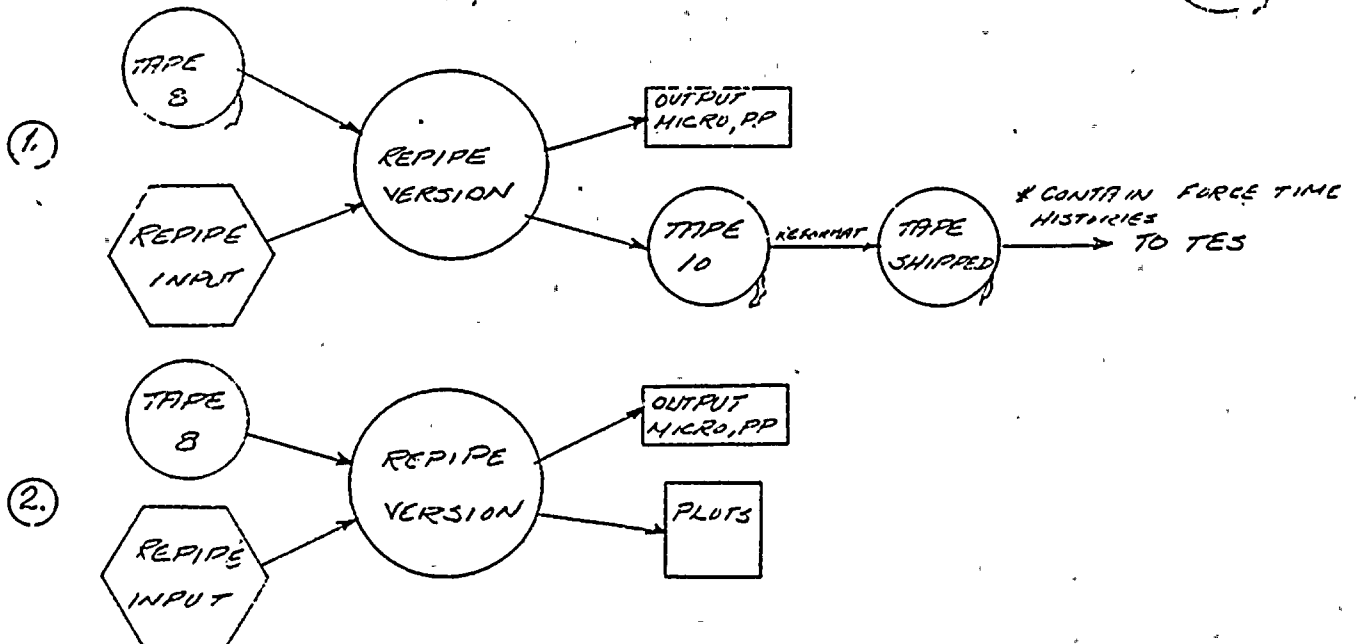
SHEET NO. 1 OF 2
 PROJ. NO. 5364

TRANSIENTS:

1. LOOPSEAL (SATURATED) STEAM CASE @ CDC
2. SOLID 400° WATER CASE



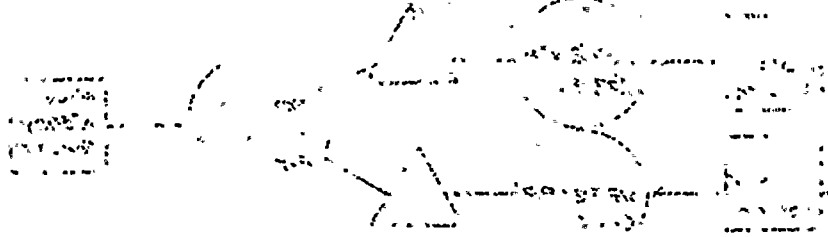
FOR EACH TAPE 8: FOLLOW 1 & 2.



TELEPHONE ENGINEERING SERVICES

ORDER NO. _____
DATE _____

NAME _____
ADDRESS _____
CITY _____



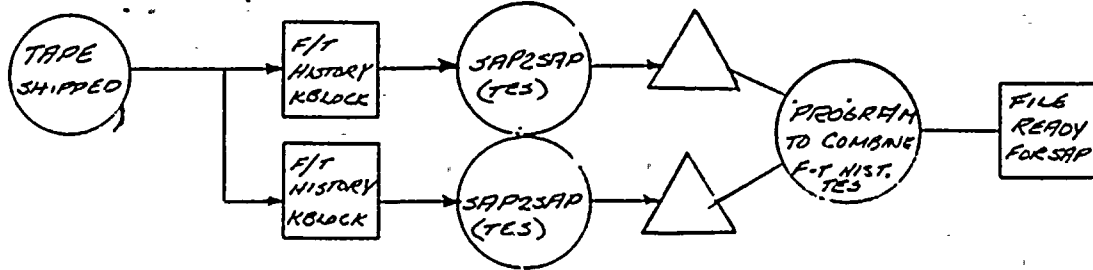
DESCRIPTION OF WORK _____

TERMS AND CONDITIONS _____

BY CHM DATE 5-4-83
CHKD. BY KJG DATE 5-24-83

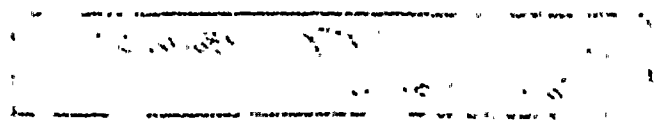
COMPUTER USAGE FOR
THERMAL ANALYSIS.

SHEET NO. 2 OF 2
PROJ. NO. 5364



TELETYPE ENGINEERING SERVICES

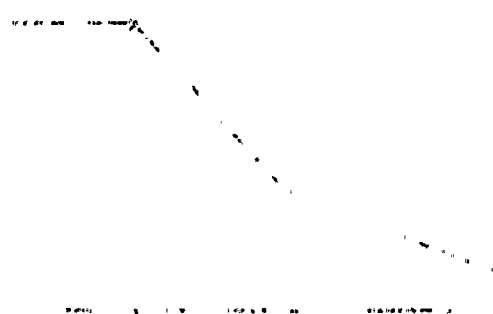
TELETYPE ENGINEERING SERVICES
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BY CMM DATE 3-28-83
CHKD. BY KY DATE 5-9-83

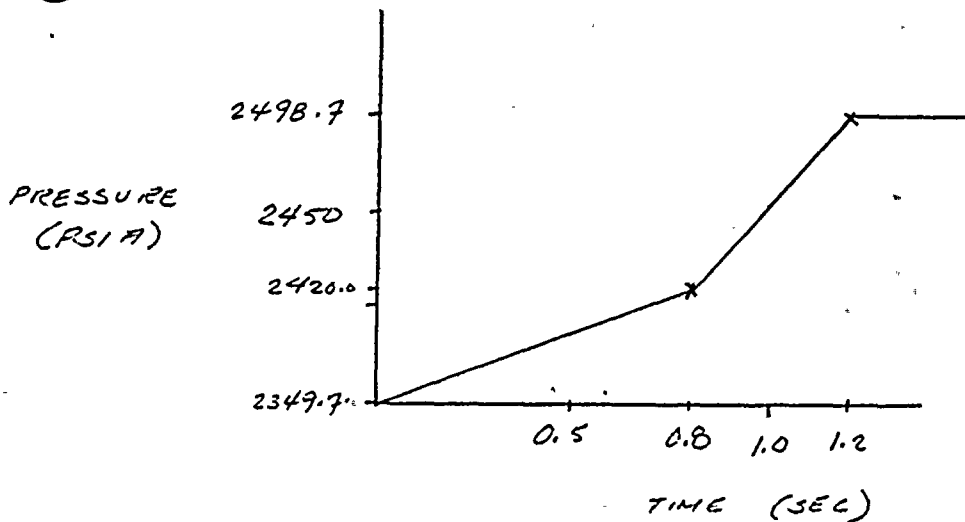
PORV UNIT BOUNDARY
CONDITIONS

SHEET NO. 1 OF 1
PROJ. NO. 5364

① VALVE OPENING TIME, PORV : 1.0 SEC
MASON EILAN : REF:

(TIME) REF: TABLE 4.5.2-1 PG 4-50 EPR1 SAFETY & RELIEF VALVE TEST REPORT (RP-V102)

② PRESSURIZER CONDITIONS:



REF: REP LETTER TO LBS 11-29-82 / CURVE PG 6 OF 7

③ VALVE FLOW AREA CALCULATED KNOWING F3ME
FLOW RATE = 199,000 lbm/HR. REF: PG 4-53 EPR1 SAFETY AND RELIEF VALVE TEST REPORT (RP-V102)
AND RUN BAICDRD AREA = 0.00806 FT²

④ QUALITY USED IN UPSTREAM PIPING TO SIMULATE CONDENSATE SEE N1G CALC

THE ENGINEERING SERVICES

MEMORANDUM FOR THE DIRECTOR
SUBJECT: [Illegible]

[Illegible text]

[Illegible text]

[Illegible text]

[Illegible text]

[Illegible text]

BY CHM DATE 5-21-83
CHKD. BY KV DATE 5-26-83

NON-CONDENSIBLE GAS QUALITY
CALCULATION FOR INITIAL COND.
UNITS 1 3 2

SHEET NO. 1 OF 1
PROJ. NO. 5364

FOR INITIAL CONDITIONS OF:

$$P_T = 17.7 \text{ PSIA}$$

$$T = 120^\circ \text{ F}$$

$$P_v = 1.6924 \text{ PSIA}$$

SPECIFIC HUMIDITY

$$\gamma = \frac{M_w}{M_a} = \frac{\text{MASS OF WATER VAPOR}}{\text{MASS OF AIR}} = \frac{V_w}{V_a}$$

$$\gamma = \frac{R_a T / P_a}{R_w T / P_w} = 0.622 \frac{P_w}{P_a}$$

$$\gamma = 0.622 \frac{1.6924 \text{ PSIA}}{16.008 \text{ PSIA}}$$

$$\gamma = 0.06576$$

$$\text{NONCONDENSIBLE GAS (AIR) QUALITY} = 1 - \gamma = 0.93424$$

Docket # 50-215
Control # 8608060048
Date 07.30.86 of Document

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m

TECHNICAL REPORT TR-5364-1
REVISION 0

BOOK 3 OF 15

DONALD C. COOK NUCLEAR GENERATING PLANT

ANALYSIS OF PRESSURIZER SAFETY/RELIEF VALVES
DISCHARGE PIPING SYSTEM PER NUREG 0737, I.D.1,
UNIT 1

JUNE 6, 1983

16 FEB 9 1954
3 11 10

MEMORANDUM FOR THE DIRECTOR
FROM THE CHIEF OF BUREAU OF AERONAUTICS
SUBJECT: [Illegible]

1. [Illegible]

2. [Illegible]

3. [Illegible]

4. [Illegible]

5. [Illegible]

6. [Illegible]

7. [Illegible]

AMERICAN ELECTRIC POWER SERVICE CORPORATION
2 BROADWAY
NEW YORK, NEW YORK 10004

TECHNICAL REPORT TR-5364-1
REVISION 0

BOOK 3 OF 15

DONALD C. COOK NUCLEAR GENERATING STATION

ANALYSIS OF PRESSURIZER SAFETY/RELIEF VALVES
DISCHARGE PIPING SYSTEM PER NUREG 0737, II. D.1,
UNIT 1

FOR REFERENCE ONLY
UNCONTROLLED COPY

JUNE 6, 1983

TELEDYNE ENGINEERING SERVICES
130 SECOND AVENUE
WALTHAM, MASSACHUSETTS 02254
617-890-3350

SERVICES

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1978

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5.0 STRUCTURAL ANALYSIS

Deadweight, thermal, seismic and force/time history analyses were performed for the pressurizer safety and relief valve discharge piping using the TMRSAP computer program; a modified version of SAPIV. The computer model used was based on TES isometric drawing E-5763, Revision 2 which is shown in Section 7.0. In general, the structural analysis was done in accordance with AEP letter dated November 29, 1982 from Mr. Sam Ulan of AEP to Mr. L. B. Semprucci of TES (Reference 2) and AEP letter dated March 15, 1983 from Mr. Sam Ulan of AEP to Mr. Pat Harrison of TES (Reference 3). Section 6.0 contains all of the results for the analyses performed.

Only the piping shown on drawing E-5763 was included in the analysis. Branch lines not in the scope of work were decoupled in accordance with the procedure outlined in TES letter 5364-21 dated February 2, 1983 (Reference 8); that is if the moment of inertia of the main run of pipe is greater than or equal to 40 times the moment of inertia of the branch, the branch line was decoupled.

Valve drawing 88405-1 listed the weight of valves NMO-151, 152 and 153 as being 352 pounds and this value was used by TES in the deadweight and seismic analyses. However, per Reference 7, TES was informed by AEP that the valve weight was actually 400 pounds. TES immediately reran the deadweight and seismic analyses and observed a minor increase in seismic results, which were offset by a decrease in deadweight results. The decrease in deadweight results, in the opinion of TES, indicates the constant force supports near the valves are over supporting the pipe. The net result of the valve weight change was considered negligible and since pipe stresses and support loads had already been extracted and calculated based on the 352 pound valve weight, it was decided not to revise the deadweight and seismic analyses. The valve weight was changed to 400 pounds prior to executing the force/time history analysis.

SERVICES

1. The first part of the report is a description of the work done during the period covered by the report.

2. The second part of the report is a description of the results of the work done during the period covered by the report.

3. The third part of the report is a description of the conclusions reached during the period covered by the report.

4. The fourth part of the report is a description of the recommendations made during the period covered by the report.

5. The fifth part of the report is a description of the work done during the period covered by the report.

5.1 Deadweight Analysis

The effects of pipe weight, water weight and insulation weight were considered in the deadweight analysis. In addition, concentrated weights were located wherever branch lines were decoupled, at flanges, and at valve cg's. The weights used for decoupled branch lines were calculated in accordance with the procedure defined in TES letter 5364-25, dated February 14, 1983 (Reference 9). Per Reference 3, only the normal operation deadweight case was analyzed.

A summary of the weights and forces applied in the deadweight analysis are shown in Table 5-1.

5.2 Thermal Analysis

Two thermal cases were analyzed; normal operation and PORV operation. Temperature distributions for the PORV case were obtained from the RELAP5 output. Throughout this report, thermal case 1 refers to normal operation and thermal case 2 refers to PORV operation.

Boundary displacements were calculated for the quench tank nozzle, pressurizer nozzles and support 1-GRC-R-616, which connects to the pressurizer, for both thermal conditions analyzed. These calculations are shown in Section 6.6.

5.3 Seismic Analysis

Seismic analysis was performed for both the operating basis earthquake (OBE) and design basis earthquake (DBE). For each of these conditions, two analyses were made; one considering response spectra applied in the X and Y directions and one considering response spectra applied in the Y and Z directions. The results in Section 6 will be based on the greater of these two analyses for all values reported.

DATE 1/10/52
PAGE 1/10/52
NO. OF

RESTAURANT WATER

W I
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RESTAURANT WATER

WEIGHT LOSS
100

WEIGHT LOSS

WEIGHT LOSS

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TELEDYNE ENGINEERING SERVICES

PROJECT: 5364 6 JUNE 1983
 D. C. COOK UNIT 1
 DEADWEIGHT DATA TABLE 5-1

BY DMD DATE 6/6/83
 CHKD POA DATE 6/6/83
 SHEET NO. _____ OF _____

MAIN RISER

NODES	PIPE SIZE	DIST. WEIGHT LBS/IN	CONTENTS PIPE/INSULATION/WATER
1	12" SCH. 40	34.748 *	(P) I W
4 THRU 206	12" SCH. 40	4.458	(P) I W
260 THRU 295	6" SCH. 40S	1.582	(P) I W

* FLANGE WEIGHT DISTRIBUTED OVER 2.042' ADDED TO PIPE WEIGHT.

APPLIED FORCES

NODE	FORCE LBS.
48	426
70	1200

CONCENTRATED WEIGHTS

NODE	WEIGHT LBS.
1000	122
1001	20

NOTE: APPLIED FORCES REPRESENT THE SETTINGS OF CONSTANT FORCE SUPPORTS AT THE NODES INDICATED. ALL FORCES ARE APPLIED IN THE +Y GLOBAL DIRECTION.

SRV LOOP C (REFERS TO SRV LOOP CONTAINING VALVE SV-45C, THIS NOTATION IS TYPICAL OF LOOPS B AND A ALSO.)

NODES	PIPE SIZE	DIST. WEIGHT LBS/IN	CONTENTS PIPE/INSULATION/WATER
97 THRU 109	6" SCH. 40S	1.582	(P) I W
110 THRU 115	6" SCH. 40S	2.632	(P) (I) W
120 THRU 130	6" SCH. 160	5.575	(P) (I) (W)
132 THRU 138	6" SCH. 160	4.904	(P) (I) W

APPLIED FORCES

NODE	FORCE LBS.
101	142
111	1067

CONCENTRATED WEIGHTS

NODE	WEIGHT LBS.
116	81
1170	685
118	164

Служба
Служба

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TELEDYNE ENGINEERING SERVICES



PROJECT: 5364
 D. C. COOK UNIT 1
 DEADWEIGHT DATA Table 5-1 (Cont)

BY Dms DATE 6/6/83
 CHKD POH DATE 6/6/83
 SHEET NO. _____ OF _____

SRV LOOP B

NODES	PIPE SIZE	DIST. WEIGHT LBS/IN	CONTENTS PIPE/INSULATION/WATER		
142 THRU 157	6" SCH. 40S	1,582	(F)	I	W
158 THRU 165	6" SCH. 40S	2,632	(F)	(I)	W
170 THRU 180	6" SCH. 160	5,575	(F)	(I)	(W)
181 THRU 185	6" SCH. 160	4,904	(F)	(I)	W

APPLIED FORCES

NODE	FORCE LBS.
159	1074

CONCENTRATED WEIGHTS

NODE	WEIGHT LBS.
164	81
1660	685
168	164

SRV LOOP A

NODES	PIPE SIZE	DIST. WEIGHT LBS/IN	CONTENTS PIPE/INSULATION/WATER		
206 THRU 216	6" SCH. 40S	1,582	(P)	I	W
220 THRU 225	6" SCH. 40S	2,632	(P)	(I)	W
229 THRU 237	6" SCH. 160	5,575	(P)	(I)	(W)
238 THRU 244	6" SCH. 160	4,904	(P)	(I)	W

APPLIED FORCES

NODE	FORCE LBS.
221	1025

CONCENTRATED WEIGHTS

NODE	WEIGHT LBS.
224	81
2260	685
228	164

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TELEDYNE ENGINEERING SERVICES



PROJECT: 5364
 D. C. COOK UNIT 1
 DEADWEIGHT DATA Table 5-1 (Cont)

6 JUNE 1983

BY Smd DATE 6/6/83
 CHKD PDH DATE 6/6/83
 SHEET NO. _____ OF _____

PORV LOOP 153 (REFERS TO PORV LOOP CONTAINING VALVES NMO-153 AND NRV-153; THIS NOTATION IS TYPICAL OF LOOPS 152 AND 151 ALSO.)

NODES	PIPE SIZE	DIST. WEIGHT LBS/IN	CONTENTS PIPE/INSULATION/WATER		
295	6" SCH. 40S	1.58	P	I	W
560 THRU 534	3" SCH. 40S	.632	(P)	I	W
533 THRU 525	3" SCH. 40S	1.190	(P)	(I)	W
510 THRU 480	3" SCH. 160	1.948	(P)	(I)	(W)
475 THRU 450	3" SCH. 160	1.753	(P)	(I)	W
440 THRU 590	4" SCH. 120	2.200	(P)	(I)	W
595 THRU 750	6" SCH. 160	4.825	(P)	(I)	W

APPLIED FORCES

NODE	FORCE LBS.
529	658
485	811
668	1159

CONCENTRATED WEIGHTS

NODE	WEIGHT LBS.
516	480
496	352
1002	14
1003	14

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TELEDYNE ENGINEERING SERVICES



PROJECT: 5364 6 JUNE 1983
 D. C. COOK UNIT 1
 DEADWEIGHT DATA Table 5-1 (Cont)

BY DMD DATE 6/6/83
 CHKD PDT DATE 6/6/83
 SHEET NO. _____ OF _____

PORV LOOP 152

NODES	PIPE SIZE	DIST. WEIGHT LBS/IN	CONTENTS PIPE/INSULATION/WATER		
300 THRU 335	4" SCH. 40S	.899	(F)	I	W
340 THRU 370	3" SCH. 40S	.632	(F)	I	W
375 THRU 385	3" SCH. 40S	1.190	(F)	(I)	W
400 THRU 435	3" SCH. 160	1.948	(F)	(I)	(W)

APPLIED FORCES

NODE	FORCE LBS.
382	638
431	930

CONCENTRATED WEIGHTS

NODE	WEIGHT LBS.
391	480
411	352

PORV LOOP 151

NODES	PIPE SIZE	DIST. WEIGHT LBS/IN	CONTENTS PIPE/INSULATION/WATER		
335	3" SCH. 40S	.632	(F)	I	W
610 THRU 625	3" SCH. 40S	1.190	(F)	(I)	W
635 THRU 660	3" SCH. 160	1.948	(F)	(I)	(W)

APPLIED FORCES

NODE	FORCE LBS.
620	783

CONCENTRATED WEIGHTS

NODE	WEIGHT LBS.
631	480
651	352

NOTE: THE VALUE WEIGHTS OF 352 LBS. LISTED FOR THE THREE PORV LOOPS I KNOWN TO BE INCORRECT. PER AMENDED INFORMATION, THESE WEIGHTS WERE CHANGED TO 400 LBS. THE 48 LB. DIFFERENCE WAS, HOWEVER, DETERMINED TO HAVE NEGLIGIBLE AFFECT ON THE ANALYSIS. (SEE SECTION 5)

REVISED

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For the OBE analysis, the horizontal spectra was obtained by enveloping Containment Crane Wall Figures for elevations 651'-3", 663'-4", 675'-4" and 687'-6". The figures used were based on .5% equipment damping and 2% structural damping. Prior to enveloping the figures, the peaks of each curve were broadened +/-15%, in accordance with NRC Regulatory Guide 1.122.

For the vertical direction Containment Base Slab, elevation 597'6" was used with .5% equipment damping and 2% structural damping. The peaks of this curve were also broadened +/-15% and two-thirds of the value obtained from the figure was used in the spectra.

For the DBE analysis, the spectra were obtained for the horizontal and vertical directions in the same manner as for the horizontal direction; except that 5% structural damping was used rather than 2%.

The procedures described above are in accordance with the November 29, 1982 letter from AEP (Reference 2) and TES letter 5364-33, dated April 8, 1983 (Reference 10).

The peak broadened figures used and spectra obtained are detailed in Section 6.6.

5.4 Force/Time History Analysis

5.4.1 PORV Transient

Two potential PORV transients exist, condensate and solid water. Based on a preliminary analysis by TES, it was determined that the solid water case was the dominating condition throughout the piping system. Based on these results, only the solid water case was analyzed.

The solid water analysis was performed at one millisecond intervals for a length of one second. All loads peaked previous to one second, indicating that the analysis was performed for a sufficient length of time.

5.4.2 SV Transient

The SV transient condition was not analyzed for Unit 1 based on the quarter model SV transient analysis performed for Unit 2. That analysis, which considered the opening of only one SV valve, resulted in catastrophic failure of the piping system. Due to the similarity of the Unit 1 and Unit 2 piping systems, it was considered not justifiable economically to analyze the SV transient for Unit 1 until the system was modified. The results of the 1/4 model SV analysis are given in TES Technical Report TR-5364-2, Revision 0 (Reference 6).

6.0 ANALYTICAL RESULTS

6.1 Stress Summary

Stress calculations were based on the 1967 Edition of the ANSI B31.1 Code (Reference 11), the AEP letter dated November 29, 1982 (Reference 2), and the AEP letter dated March 15, 1983 (Reference 3). The stress combinations performed were:

- A1 normal pressure stress + deadweight stress $< S_h$
- A2 normal thermal stress range $< (1.25 S_c + .25 S_h)$
- B1 normal pressure stress + deadweight stress + OBE stress $< 1.2 S_h$
- B2 PORV transient pressure stress + deadweight stress + $\left[(\text{OBE stress})^2 + (\text{PORV transient shock stress})^2 \right]^{1/2} < 1.2 S_h$
- B3 PORV transient thermal stress range $< (1.25 S_c + .25 S_h)$
- C1 normal pressure stress + deadweight stress + DBE stress $< 1.8 S_h$

Stresses were not calculated for equation A3 since all node points passed the equation A2 stress criteria. The equation C2 stresses were not calculated since the SV transient shock analysis was not performed, based on the Unit 2 Quarter model analysis (see Section 5.4.2). Equation C3 stresses do not exist since TES did not analyze for the SV transient thermal condition, see Section 5.2.

The TMRPASS computer program was used, when possible, to aid in the stress calculations. The program; however, does not allow for intensification factors to be omitted in the torsional direction as does the B31.1 code. Therefore, the stresses presented consider, at any intensified nodes, all moments

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to be intensified. For equation B2, three nodes, (540, 533 and 435B), originally failed this more conservative method. In order to not exceed the stress criteria at these nodes, the intensification factor was removed, by hand calculations, in the torsional direction for as many of the loading conditions as necessary. The revised stress values are presented in the appropriate Table.

Allowable stresses were obtained by using the maximum temperature the piping experienced during any loading case to determine Sh. The value of Sc was based on 70°F per Reference 2. A summary of the allowable stresses is given in Table 6.1-1.

Section 119.6.1 of the B31.1 code indicates that the thermal stress range stress calculations shall be based on the range between the minimum and maximum temperature. Neither equation A2 or B3 allows for this criteria, however, the worst thermal moments due to both conditons analyzed, plus the case of no expansion, was analyzed and found to be satisfactory.

Stresses were calculated as follows:

Pressure

$$\frac{pd^2}{D^2-d^2}$$

Deadweight

$$\frac{.75i M_A}{Z}$$

Thermal

$$\frac{i M_C}{Z}$$

277



Seismic

$$\frac{.75i M_B}{Z}$$

Force/Time History

$$\frac{.75i M_D}{Z}$$

where:

- d = inside diameter of pipe
- D = outside diameter of pipe
- i = intensification factor
- M_A = resultant moment due to deadweight loadings
- M_B = resultant moment due to seismic loadings
- M_C = range of resultant moments due to thermal loadings
- M_D = resultant moment due to force/time history analysis

100
100



TELEDYNE ENGINEERING SERVICES

PROJECT: 5364 28 MAY 1983
 D. C. COOK UNIT 1
 SUMMARY OF ALLOWABLES

BY *DMB* DATE *5-28-83*

CHKD *SMD* DATE *5/29/83*

SHEET NO. _____ OF _____

TABLE 6.1-1

MAIN RISER

NODES	MATERIAL	TEMPERATURE (F)	SH (PSI)
1 THRU 30	SA-308-316 CL 1	400	15210
32 THRU 32	.	324	13744
56 THRU 72	.	337	14378
74 THRU 93	.	354	14576
97 THRU 204	.	348	14612
260	SA-312-304	340	15262
280 THRU 295	.	390	15070
299 THRU 295	.	410	14698

SRV LOOPS

NODES LOOP C	NODES LOOP B	NODES LOOP A	MATERIAL	TEMPERATURE (F)	SH (PSI)
99 THRU 100	144 THRU 146	200	SA-312-304	340	15252 *
102 THRU 109	148 THRU 155	214 THRU 216	.	350	15150
110 THRU 112	157 THRU 160	220 THRU 222	.	430	14830
114 THRU 1140	162 THRU 163	223 THRU 2230	.	460	14710
115	165	225	.	460	11740 *
120	170	227	SA-376-316	353	11600 *
122 THRU 138	172 THRU 185	233 THRU 244	SA-376-316	353	13000

NOTE: LOOP C REFERS TO THE SRV LOOP CONTAINING VALVE 6V-45C THIS NOTATION IS TYPICAL OF LOOPS B AND A ALSO.
 * ALLOWABLE AS PER NOTE (6), TABLE A-1 OF 5-31.1.0, 1967 CODE.



TELEDYNE ENGINEERING SERVICES

PROJECT: 5364 28 MAY 1983
 D. C. COOK UNIT 1
 SUMMARY OF ALLOWABLES

BY *JMB* DATE *5-28-83*
 CHKD *Emd* DATE *5/28/83*
 SHEET NO. _____ OF _____

TABLE 6.1-1 (cont.)

FORV LOOP 153

NODES	MATERIAL	TEMPERATURE (F)	Sh (PSI)
560 THRU 555	SA-312-304	413	14898
550 THRU 529	'	480	14630
525 THRU 515	'	653	14300
510 THRU 450	SA-376-304	653	14300
440 THRU 750	SA-376-316	653	16000

FORV LOOP 152

NODES	MATERIAL	TEMPERATURE (F)	Sh (PSI)
500 THRU 382	SA-312-304	413	14898
505 THRU 390	SA-312-304	653	14300
400 THRU 431	SA-376-304	653	14300

FORV LOOP 151

NODES	MATERIAL	TEMPERATURE (F)	Sh (PSI)
310 THRU 320	SA-312-304	480	14630
325 THRU 330	SA-312-304	653	14300
325 THRU 365	SA-376-304	653	14300

NOTE: FORV LOOP 151 REFERS TO THE FORV LOOP CONTAINING VALVES VMO-151 AND NRV-151. THIS IS TYPICAL OF LOOPS 152 AND 153.

6.1.1 Equation A-1 Stresses



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 **TELEDYNE
ENGINEERING SERVICES**

DONALD C. COOK
UNIT #1
PROJECT 5364

BY: AMB DATE: 5-3-83

CHECKED BY: DmD DATE: 5/3/83

STRESS SUMMARY - EQUATION A1

NODE #	PRESSURE STRESS (KSI)	DEADWEIGHT STRESS (KSI)	EQUATION A1 STRESS (KSI)	ALLOWABLE STRESS (KSI)
1	0	.1	.1	16.2
4		.9	.9	
6		.3	.3	
7		.2	.2	
8		.1	.1	
10		.2	.2	
12		.5	.5	
18		.4	.4	
30		.4	.4	↓
32		.7	.7	16.7
33		.4	.4	
34		.4	.4	
36		.5	.5	
38		.2	.2	
40		.2	.2	
42		.1	.1	
44		.2	.2	
46		.2	.2	
48		.1	.1	
50	↓	.2	.2	↓

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**TELEDYNE
 ENGINEERING SERVICES**

DONALD C. COOK
 UNIT #1
 PROJECT 5364

BY: AMB DATE: 5-3-83

CHECKED BY: SMB DATE: 5/3/83

STRESS SUMMARY - EQUATION A1

NODE #	PRESSURE STRESS (KSI)	DEADWEIGHT STRESS (KSI)	EQUATION A1 STRESS (KSI)	ALLOWABLE STRESS (KSI)
52	0	.3	.3	16.7
56		.4	.4	
58		.4	.4	
60		.3	.3	
62		.4	.4	
66		.2	.2	
68		.2	.2	
70		.2	.2	
72		.1	.1	✓
74		.3	.3	16.6
76		.2	.2	
80		.3	.3	
82		.5	.5	
83		.2	.2	
84		.5	.5	
86		.3	.3	
88		.3	.3	
90		.5	.5	
93		.4	.4	✓
97R	✓	.8	.8	16.6

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DONALD C. COOK
 UNIT #1
 PROJECT 5364

BY: DMB DATE: 5-3-83

CHECKED BY: DMB DATE: 5/3/83

STRESS SUMMARY - EQUATION A1

NODE #	PRESSURE STRESS (KSI)	DEADWEIGHT STRESS (KSI)	EQUATION A1 STRESS (KSI)	ALLOWABLE STRESS (KSI)
97R	0	.7	.7	16.6
195		.5	.5	
142R		.7	.7	
142R		.6	.6	
200		.4	.4	
206R		.3	.3	
206R		.3	.3	↓
260		1.0	1.0	15.3
280		1.5	1.5	15.1
285		4.5	4.5	15.1
290		5.3	5.3	14.9
295B		3.7	3.7	↓
97B		.7	.7	15.3
98		.8	.8	
99		.7	.7	
100		.4	.4	↓
102		.3	.3	15.1
103		.3	.3	
104		.8	.8	
106	↓	1.0	1.0	↓



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 **TELEDYNE
ENGINEERING SERVICES**

DONALD C. COOK
UNIT #1
PROJECT 5364

BY: DWB DATE: 5-3-83

CHECKED BY: DMB DATE: 5/3/83

STRESS SUMMARY - EQUATION A1

NODE #	PRESSURE STRESS (KSI)	DEADWEIGHT STRESS (KSI)	EQUATION A1 STRESS (KSI)	ALLOWABLE STRESS (KSI)
108	0	.6	.6	15.1
109		.9	.9	15.1
110		1.2	1.2	14.8
112		.5	.5	14.8
114		1.2	1.2	14.7
1140		.7	.7	14.7
115	∇	.7	.7	11.7
120	3.5	0.9	4.4	11.6
122		1.1	4.6	16.0
124		.9	4.4	
126		.9	4.4	
128		.7	4.2	
130		.6	4.1	
132		.9	4.4	
134		1.0	4.5	
136		1.2	4.7	
138	∇	1.3	4.8	∇
142E	0	.6	.6	15.3
144		.4	.4	
146	∇	.2	.2	∇



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 **TELEDYNE
ENGINEERING SERVICES**

DONALD C. COOK
UNIT #1
PROJECT 5364

BY: AKC DATE: 5-3-83

CHECKED BY: Dmb DATE: 5/3/83

STRESS SUMMARY - EQUATION A1

NODE #	PRESSURE STRESS (KSI)	DEADWEIGHT STRESS (KSI)	EQUATION A1 STRESS (KSI)	ALLOWABLE STRESS (KSI)
148	0	.3	.3	15.1
150		1.0	1.0	
152		1.4	1.4	
156		.8	.8	<u>∇</u>
157		1.1	1.1	14.8
158		1.3	1.3	
160		.7	.7	<u>∇</u>
162		1.2	1.2	14.7
163		.7	.7	14.7
165	<u>∇</u>	.7	.7	11.7
170	3.5	.9	4.4	11.6
172		1.0	4.5	16.0
174		.8	4.3	
176		.8	4.3	
178		.5	4.0	
180		.5	4.0	
181		.8	4.3	
182		.9	4.4	
184		1.1	4.6	
185	<u>∇</u>	1.2	4.7	<u>∇</u>



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 **TELEDYNE
ENGINEERING SERVICES**

DONALD C. COOK
UNIT #1
PROJECT 5364

BY: DMD DATE: 5-3-83

CHECKED BY: DMD DATE: 5/3/83

STRESS SUMMARY - EQUATION A1

NODE #	PRESSURE STRESS (KSI)	DEADWEIGHT STRESS (KSI)	EQUATION A1 STRESS (KSI)	ALLOWABLE STRESS (KSI)
206B	0	1.1	1.1	15.3
208		.3	.3	15.3
214		1.0	1.0	15.1
216		1.5	1.5	15.1
220		1.3	1.3	14.8
222		.6	.6	14.8
223		1.0	1.0	14.7
2230		.6	.6	14.7
225	∇	.6	.6	11.7
229	3.5	.7	4.2	11.6
233		.8	4.3	16.0
234		.5	4.0	
235		.5	4.0	
236		.3	3.8	
237		.2	3.7	
238		.7	4.2	
240		.8	4.3	
242		1.1	4.6	
244	∇	1.1	4.6	∇
295R	0	3.2	3.2	14.9

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DONALD C. COOK
 UNIT #1
 PROJECT 5364

BY: AKB DATE: 5-3-83
 CHECKED BY: DMS DATE: 5/3/83

STRESS SUMMARY - EQUATION A1

NODE #	PRESSURE STRESS (KSI)	DEADWEIGHT STRESS (KSI)	EQUATION A1 STRESS (KSI)	ALLOWABLE STRESS (KSI)
560	0	9.9	9.9	14.9
555		5.6	5.6	14.9
550		3.5	3.5	14.6
545		3.7	3.7	
540		3.8	3.8	
536		3.7	3.7	
535		4.1	4.1	
534		4.7	4.7	
533		5.6	5.6	
530		6.4	6.4	
529		4.2	4.2	↓
525	↓	4.6	4.6	14.3
510	2.9	3.0	5.9	
505		2.5	5.4	
490		1.7	4.6	
485		2.8	5.7	
480		2.7	5.6	
475		2.5	5.4	
465		4.2	7.1	
460	↓	2.7	5.6	↓



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**TELEDYNE
 ENGINEERING SERVICES**

DONALD C. COOK
 UNIT #1
 PROJECT 5364

BY: JMB DATE: 5-3-83

CHECKED BY: DMD DATE: 5/3/83

STRESS SUMMARY - EQUATION A1

NODE #	PRESSURE STRESS (KSI)	DEADWEIGHT STRESS (KSI)	EQUATION A1 STRESS (KSI)	ALLOWABLE STRESS (KSI)
450	2.9	5.0	7.9	14.3
440	4.1	5.4	9.5	14.3
435R		3.4	7.5	16.0
435R		1.1	5.2	16.0
575		3.5	7.6	16.0
585		5.5	9.6	
590		6.3	10.4	
595	↓	7.0	11.1	
600R	3.5	2.1	5.6	
600R	3.5	2.5	6.0	
668	3.5	2.6	6.1	
670		2.6	6.1	
675		2.9	6.4	
680		2.9	6.4	
690		2.6	6.1	
700		2.1	5.6	
710		1.1	4.6	
715		.8	4.3	
717		.5	4.0	
720	↓	.4	3.9	↓



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DONALD C. COOK
 UNIT #1
 PROJECT 5364

BY: AMB DATE: 5-3-83

CHECKED BY: SMD DATE: 5/3/83

STRESS SUMMARY - EQUATION A1

NODE #	PRESSURE STRESS (KSI)	DEADWEIGHT STRESS (KSI)	EQUATION A1 STRESS (KSI)	ALLOWABLE STRESS (KSI)
725	3.5	.4	3.9	16.0
750	3.5	.3	3.8	16.0
295R	0	2.7	2.7	14.9
300		5.2	5.2	
310		4.1	4.1	
320		2.8	2.8	
325		1.6	1.6	
335R		1.2	1.2	
335R		2.9	2.9	✓
340		4.7	4.7	14.6
350		2.8	2.8	
355		1.0	1.0	
360		1.9	1.9	
365		3.1	3.1	
370		3.7	3.7	
375		3.6	3.6	
380		3.4	3.4	
382		2.4	2.4	✓
385	✓	2.5	2.5	14.3
400	2.9	1.7	4.6	14.3



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DONALD C. COOK
 UNIT #1
 PROJECT 5364

BY: DMB DATE: 5-3-83

CHECKED BY: SMD DATE: 5/3/83

STRESS SUMMARY - EQUATION A1

NODE #	PRESSURE STRESS (KSI)	DEADWEIGHT STRESS (KSI)	EQUATION A1 STRESS (KSI)	ALLOWABLE STRESS (KSI)
405	2.9	2.1	5.0	14.3
420		2.6	5.5	
429		4.1	7.0	
430		4.6	7.5	
431		4.7	7.6	
435B	<u>∇</u>	5.0	7.9	<u>∇</u>
335B	0	3.0	3.0	14.9
610		3.6	3.6	14.6
615		3.5	3.5	
620		2.6	2.6	<u>∇</u>
625	<u>∇</u>	2.8	2.8	14.3
635	2.9	2.9	5.8	
645		3.7	6.6	
657		3.8	6.7	
660		3.2	6.1	
665		3.0	5.9	
600B	<u>∇</u>	3.0	5.9	<u>∇</u>

6.1.2 Equation A-2 Stresses



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TELEDYNE
ENGINEERING SERVICES

DONALD C. COOK
UNIT #1
PROJECT 5364

BY: AMB DATE: 5-3-83

CHECKED BY: JMD DATE: 5/3/83

STRESS SUMMARY - EQUATION A2

NODE #	NORMAL THERMAL STRESS (KSI)	ALLOWABLE STRESS (KSI)
1	.7	27.5
4	7.6	
6	6.8	
7	2.5	
8	2.5	
10	7.0	
12	7.6	
18	3.1	
30	9.5	↓
32	8.8	27.6
33	3.3	
34	3.1	
36	3.0	
38	4.6	
40	6.9	
42	2.7	
44	7.2	
46	9.5	
48	3.8	
50	11.2	↓



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 **TELEDYNE
ENGINEERING SERVICES**

DONALD C. COOK
UNIT #1
PROJECT 5364

BY: AMB DATE: 5-3-83

CHECKED BY: DMD DATE: 5/3/83

STRESS SUMMARY - EQUATION A2

NODE #	NORMAL THERMAL STRESS (KSI)	ALLOWABLE STRESS (KSI)
52	11.7	27.6
56	11.0	
58	11.3	
60	13.0	
62	12.8	
66	2.5	
68	2.4	
70	2.3	
72	1.2	
74	2.1	
76	2.1	
80	2.3	
82	2.5	
83	.9	
84	2.4	
86	2.2	
88	2.4	
90	2.9	
93	1.4	
97R	3.5	↓

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TELEDYNE
ENGINEERING SERVICES

DONALD C. COOK
UNIT #1
PROJECT 5364

BY: AMS DATE: 5-3-83
CHECKED BY: SMS DATE: 5/3/83

STRESS SUMMARY - EQUATION A2

NODE #	NORMAL THERMAL STRESS (KSI)	ALLOWABLE STRESS (KSI)
97 R	2.1	27.6
195	1.1	
142 R	2.8	
142 R	1.7	
200	.8	
206 R	2.2	
206 R	2.8	↓
260	6.0	27.3
280	3.6	27.2
285	8.9	
290	8.3	
295 B	5.8	↓
97 B	7.5	27.3
98	3.1	
99	2.0	
100	1.9	↓
102	2.4	27.2
103	3.0	
104	7.4	
106	7.1	↓



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 **TELEDYNE
ENGINEERING SERVICES**

DONALD C. COOK
UNIT #1
PROJECT 5364

BY: DJB DATE: 5-3-83

CHECKED BY: DMD DATE: 5/3/83

STRESS SUMMARY - EQUATION A2

NODE #	NORMAL THERMAL STRESS (KSI)	ALLOWABLE STRESS (KSI)
108	3.1	27.2
109	1.0	27.2
110	1.3	27.1
112	4.7	
114	5.3	
1140	2.3	↓
115	2.3	26.4
120	.8	26.3
122	.8	27.4
124	1.2	
126	1.2	
128	1.4	
130	1.3	
132	1.4	
134	1.4	
136	1.4	
138	1.3	↓
142B	9.8	27.3
144	3.6	↓
146	2.3	↓



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DONALD C. COOK
UNIT #1
PROJECT 5364

BY: AMB DATE: 5-3-83

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STRESS SUMMARY - EQUATION A2

NODE #	NORMAL THERMAL STRESS (KSI)	ALLOWABLE STRESS (KSI)
148	2.7	27.2
150	8.1	
152	8.3	
156	3.5	↓
157	.6	27.1
158	2.1	
160	5.6	
162	5.6	
163	2.4	↓
165	2.4	26.4
170	.8	26.3
172	1.6	27.4
174	2.2	
176	2.2	
178	2.4	
180	2.0	
181	1.9	
182	1.9	
184	2.0	
185	1.8	↓



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TELEDYNE
ENGINEERING SERVICES

DONALD C. COOK
UNIT #1
PROJECT 5364

BY: JMB DATE: 5-3-83

CHECKED BY: EMD DATE: 5/3/83

STRESS SUMMARY - EQUATION A2

NODE #	NORMAL THERMAL STRESS (KSI)	ALLOWABLE STRESS (KSI)
206 B	17.6	27.3
208	4.0	27.3
214	4.6	27.2
216	6.6	27.2
220	2.4	27.1
222	7.5	
223	5.1	
2230	2.2	↓
225	2.2	26.4
229	1.7	26.3
233	3.3	27.4
234	4.5	
235	4.5	
236	5.2	
237	4.6	
238	4.1	
240	4.1	
242	4.2	
244	3.8	↓
295 R	2.9	27.2

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TELEDYNE
ENGINEERING SERVICES

DONALD C. COOK
UNIT #1
PROJECT 5364

BY: DWB DATE: 5-3-83

CHECKED BY: DMD DATE: 5/3/83

STRESS SUMMARY - EQUATION A2

NODE #	NORMAL THERMAL STRESS (KSI)	ALLOWABLE STRESS (KSI)
560	7.0	27.2
555	3.8	27.2
550	1.8	27.1
545	4.3	
540	4.6	
536	2.5	
535	2.5	
534	2.6	
533	4.6	
530	5.2	
529	2.9	↓
525	2.9	27.0
510	1.7	
505	1.7	
490	1.7	
485	1.8	
480	1.9	
475	1.7	
465	2.0	
460	1.6	↓

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 **TELEDYNE
ENGINEERING SERVICES**

DONALD C. COOK
UNIT #1
PROJECT 5364

BY: DWB DATE: 5-3-83

CHECKED BY: DMS DATE: 5/3/83

STRESS SUMMARY - EQUATION A2

NODE #	NORMAL THERMAL STRESS (KSI)	ALLOWABLE STRESS (KSI)
450	2.0	27.0
440	2.1	27.0
435R	1.2	27.4
435R	2.7	
575	2.1	
585	.8	
590	.7	
595	.5	
600R	.1	
600R	1.8	
668	1.8	
670	2.0	
675	1.9	
680	1.7	
690	1.5	
700	1.7	
710	2.0	
715	2.6	
717	3.5	
720	4.2	*



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**TELEDYNE
ENGINEERING SERVICES**

DONALD C. COOK
UNIT #1
PROJECT 5364

BY: DWB DATE: 5-3-83

CHECKED BY: DMD DATE: 5/3/83

STRESS SUMMARY - EQUATION A2

NODE #	NORMAL THERMAL STRESS (KSI)	ALLOWABLE STRESS (KSI)
725	4.5	27.4
750	4.4	27.4
295 R	4.6	27.2
300	6.1	
310	3.2	
320	2.3	
325	5.5	
335 R	10.0	
335 R	1.7	↓
340	2.1	27.1
350	2.5	
355	2.8	
360	2.9	
365	5.4	
370	4.8	
375	3.0	
380	2.3	
382	1.1	
385	.9	
400	.2	↓



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TELEDYNE
ENGINEERING SERVICES

DONALD C. COOK
UNIT #1
PROJECT 5364

BY: DMB DATE: 5-3-83

CHECKED BY: DMS DATE: 5/3/83

STRESS SUMMARY - EQUATION A2

NODE #	NORMAL THERMAL STRESS (KSI)	ALLOWABLE STRESS (KSI)
405	.7	27.0
420	1.2	
429	1.8	
430	2.1	
431	2.2	
435B	3.0	↓
335B	15.1	27.2
610	16.3	27.1
615	12.7	
620	6.7	↓
625	5.0	27.0
635	2.0	
645	4.1	
657	6.5	
660	9.1	
665	10.0	
600B	13.0	
		↓



6.1.3 Equation B-1 Stresses



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TELEDYNE
ENGINEERING SERVICES

DONALD C. COOK
 UNIT #1
 PROJECT 5364

BY: DMC DATE: 5-3-83

CHECKED BY: DMC DATE: 5/3/83

STRESS SUMMARY - EQUATION B1

NODE #	PRESSURE STRESS (KSI)	DEADWEIGHT STRESS (KSI)	OBE STRESS (KSI)	EQUATION B1-STRESS (KSI)	ALLOWABLE STRESS (KSI)
1	0	.1	.1	.2 (YZ)	19.5
4		.9	.8	1.7 YZ	
6		.3	.5	.8 YZ	
7		.2	.2	.4 YZ	
8		.1	.1	.2 YZ	
10		.2	.2	.4 YZ	
12		.5	.4	.9 YZ	
18		.4	.1	.5 YZ	
30		.4	.2	.6 YZ	↓
32		.7	.2	.9 YZ	20.1
33		.4	.1	.5 YZ	
34		.4	.2	.6 YZ	
36		.5	.1	.6 YZ	
38		.2	.3	.5 YZ	
40		.2	.2	.4 YZ	
42		.1	.1	.2 YZ	
44		.2	.2	.4 YZ	
46		.2	.2	.4 YZ	
48		.1	.1	.2 YZ	
50	↓	.2	.2	.4 YZ	↓

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**TELEDYNE
 ENGINEERING SERVICES**

DONALD C. COOK
 UNIT #1
 PROJECT 5364

BY: AKK DATE: 5-3-83

CHECKED BY: DJD DATE: 5/3/83

STRESS SUMMARY - EQUATION B1

NODE #	PRESSURE STRESS (KSI)	DEADWEIGHT STRESS (KSI)	OBE STRESS (KSI)	EQUATION B1-STRESS (KSI)	ALLOWABLE STRESS (KSI)
52	0	.3	.3	.6 YZ	20.1
56		.4	.2	.6 XY	20.0
58		.4	.2	.6 XY	
60		.3	.2	.5 YZ	
62		.4	.2	.6 XY	
66		.2	.3	.5 YZ	
68		.2	.2	.4 YZ	
70		.2	.2	.4 YZ	
72		.1	.4	.5 YE	↓
74		.3	.1	.4 XY	19.9
76		.2	.2	.4 XY	
80		.3	.2	.5 XY	
82		.5	.2	.7 XY	
83		.2	.2	.4 XY	
84		.5	.2	.7 XY	
86		.3	.2	.5 XY	
88		.3	.2	.5 XY	
90		.5	.2	.7 XY	
93		.4	.2	.6 XY	↓
97B	↓	.8	.4	1.2 XY	19.9

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DONALD C. COOK
 UNIT #1
 PROJECT 5364

BY: DMB DATE: 5-3-83

CHECKED BY: DMB DATE: 5/3/83

STRESS SUMMARY - EQUATION B1

NODE #	PRESSURE STRESS (KSI)	DEADWEIGHT STRESS (KSI)	OBE STRESS (KSI)	EQUATION B1-STRESS (KSI)	ALLOWABLE STRESS (KSI)
97R	0	.7	.4	1.1 XY	19.9
195		.5	.3	.8 XY	
142R		.7	.4	1.1 XY	
142R		.6	.4	1.0 XY	
200		.4	.2	.6 XY	
206R		.3	.4	.7 XY	
206R		.3	.3	.6 XY	↓
260		1.0	.8	1.8 XY	18.3
280		1.5	2.1	3.6 XY	18.1
285		4.5	1.5	6.0 XY	18.1
290		5.3	2.0	7.3 XY	17.9
295B		3.7	1.7	5.4 XY	17.9
97B		.7	1.1	1.8 XY	18.3
98		.8	.3	1.1 XY	
99		.7	.4	1.1 XY	
100		.4	.7	1.1 XY	↓
102		.3	.8	1.1 XY	18.2
103		.3	1.0	1.3 XY	
104		.8	1.8	2.6 XY	
106	↓	1.0	1.9	2.9 XY	↓

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DONALD C. COOK
 UNIT #1
 PROJECT 5364

BY: JMB DATE: 5-3-83

CHECKED BY: SMS DATE: 5/3/83

STRESS SUMMARY - EQUATION B1

NODE #	PRESSURE STRESS (KSI)	DEADWEIGHT STRESS (KSI)	OBE STRESS (KSI)	EQUATION B1-STRESS (KSI)	ALLOWABLE STRESS (KSI)
108	0	.6	1.1	1.7 XY	18.2
109		.9	1.2	2.1 XY	18.2
110		1.2	1.3	2.5 XY	17.8
112		.5	2.4	2.9 XY	17.8
114		1.2	2.6	3.8 XY	17.7
1140		.7	1.5	2.2 XY	17.7
115	↓	.7	1.5	2.2 XY	14.1
120	3.5	.9	.4	4.8 YZ	13.9
122		1.1	2.5	7.1 XY	19.2
124		.9	2.9	7.3 XY	
126		.9	2.9	7.3 XY	
128		.7	2.6	6.8 XY	
130		.6	1.6	5.7 XY	
132		.9	1.3	5.7 YZ	
134		1.0	1.4	5.9 YZ	
136		1.2	1.7	6.4 YZ	
138	↓	1.3	1.6	6.4 YZ	↓
142B	0	.6	.7	1.3 YZ	18.3
144		.4	.4	.8 XY	
146	↓	.2	.7	.9 YZ	↓

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DONALD C. COOK
 UNIT #1
 PROJECT 5364

BY: DMB DATE: 5-3-83

CHECKED BY: DMD DATE: 5/3/83

STRESS SUMMARY - EQUATION B1

NODE #	PRESSURE STRESS (KSI)	DEADWEIGHT STRESS (KSI)	OBE STRESS (KSI)	EQUATION B1-STRESS (KSI)	ALLOWABLE STRESS (KSI)
148	0	.3	1.0	1.3 YE	18.2
150		1.0	2.1	3.1 YE	
152		1.4	2.2	3.6 YE	
156		.8	1.4	2.2 YE	↓
157		1.1	1.2	2.3 YE	17.8
158		1.3	1.2	2.5 YE	
160		.7	2.0	2.7 YE	↓
162		1.2	2.1	3.3 YE	17.7
163		.7	1.3	2.0 YE	17.7
165	↓	.7	1.3	2.0 YE	14.1
170	3.5	.9	.3	4.7 XY	13.9
172		1.0	2.3	6.8 YE	19.2
174		.8	2.7	7.0 YE	
176		.8	2.7	7.0 YE	
178		.5	2.4	6.4 YE	
180		.5	1.5	5.5 YE	
181		.8	1.1	5.4 XY YE	
182		.9	1.2	5.6 XY	
184		1.1	1.5	6.1 XY	
185	↓	1.2	1.4	6.1 XY	↓



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**TELEDYNE
 ENGINEERING SERVICES**

DONALD C. COOK
 UNIT #1
 PROJECT 5364

BY: AWB DATE: 5-3-83

CHECKED BY: Smd DATE: 5/3/83

STRESS SUMMARY - EQUATION B1

NODE #	PRESSURE STRESS (KSI)	DEADWEIGHT STRESS (KSI)	OBE STRESS (KSI)	EQUATION B1-STRESS (KSI)	ALLOWABLE STRESS (KSI)
206B	0	1.1	1.3	2.4 XY	18.3
208		.3	1.0	1.3 XY	18.3
214		1.0	2.1	3.1 XY	18.2
216		1.5	2.2	3.7 XY	18.2
220		1.3	.8	2.1 XY	17.8
222		.6	1.3	1.9 XY	17.8
223		1.0	1.4	2.4 XY	17.7
2230		.6	.8	1.4 XY	17.7
225	↓	.6	.8	1.4 XY	14.1
229	3.5	.7	.4	4.6 XY	13.9
233		.8	2.0	6.3 XY	19.2
234		.5	2.2	6.2 XY	
235		.5	2.2	6.2 XY	
236		.3	1.8	5.6 XY	
237		.2	1.3	5.0 XY	
238		.7	1.1	5.3 XY	
240		.8	1.1	5.4 XY	
242		1.1	1.3	5.9 YE	
244	↓	1.1	1.3	5.9 YE	↓
295R	0	3.2	1.5	4.7 YE	17.9



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**TELEDYNE
 ENGINEERING SERVICES**

DONALD C. COOK
 UNIT #1
 PROJECT 5364

BY: DMS DATE: 5-3-83

CHECKED BY: DMS DATE: 5/3/83

STRESS SUMMARY - EQUATION B1

NODE #	PRESSURE STRESS (KSI)	DEADWEIGHT STRESS (KSI)	OBE STRESS (KSI)	EQUATION B1-STRESS (KSI)	ALLOWABLE STRESS (KSI)
560	0	9.9	4.1	14.0 YE	17.9
555		5.6	1.9	7.5 YE	17.9
550		3.5	4.8	8.3 YE	17.6
545		3.7	9.9	13.6 YE	17.6
540		3.8	11.4	15.2 YE	
536		3.7	8.6	12.3 YE	
535		4.1	8.0	12.1 YE	
534		4.7	7.2	11.9 YE	
533		5.6	9.6	15.2 YE	
530		6.4	8.2	14.6 YE	
529		4.2	6.2	10.4 YE	↓
525	↓	4.6	6.3	10.9 YE	17.2
510	2.9	3.0	3.6	9.5 XY	
505		2.5	4.0	9.4 XY	
490		1.7	4.5	9.1 YE	
485		2.8	4.2	9.9 YE	
480		2.7	4.2	9.8 YE	
475		2.5	4.2	9.6 YE	
465		4.2	4.1	11.2 YE	
460	↓	2.7	4.7	10.3 YE	↓

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**TELEDYNE
 ENGINEERING SERVICES**

DONALD C. COOK
 UNIT #1
 PROJECT 5364

BY: AMB DATE: 5-3-83

CHECKED BY: SMD DATE: 5/3/83

STRESS SUMMARY - EQUATION B1

NODE #	PRESSURE STRESS (KSI)	DEADWEIGHT STRESS (KSI)	OBE STRESS (KSI)	EQUATION B1-STRESS (KSI)	ALLOWABLE STRESS (KSI)
450	2.9	5.0	5.9	13.8 YZ	17.2
440	4.1	5.4	5.8	15.3 YZ	17.2
435R		3.4	3.3	10.8 YZ	19.2
435R		1.1	6.0	11.2 YZ	
575		3.5	3.9	11.5 YZ	
585		5.5	5.0	14.6 YZ	
590		6.3	4.2	14.6 YZ	
595	↓	7.0	4.5	15.6 YZ	
600R	3.5	2.1	1.5	7.1 YZ	
600R	3.5	2.5	1.7	7.7 YZ	
668		2.6	1.7	7.8 YZ	
670		2.6	1.8	7.9 YZ	
675		2.9	1.6	8.0 YZ	
680		2.9	1.6	8.0 YZ	
690		2.6	1.3	7.4 XY	
700		2.1	1.2	6.8 XY	
710		1.1	1.4	6.0 XY	
715		.8	1.5	5.8 XY	
717		.5	1.8	5.8 XY	
720	↓	.4	1.9	5.8 XY	↓



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**TELEDYNE
 ENGINEERING SERVICES**

DONALD C. COOK
 UNIT #1
 PROJECT 5364

BY: DWB DATE: 5-3-83

CHECKED BY: S.H.B. DATE: 5/3/83

STRESS SUMMARY - EQUATION B1

NODE #	PRESSURE STRESS (KSI)	DEADWEIGHT STRESS (KSI)	OBE STRESS (KSI)	EQUATION B1-STRESS (KSI)	ALLOWABLE STRESS (KSI)
725	3.5	.4	2.0	5.9 XY	19.2
750	3.5	.3	2.7	6.5 XY	19.2
295R	0	2.7	2.1	4.8 YZ	17.9
300		5.2	4.1	9.3 YZ	
310		4.1	3.7	7.8 YZ	
320		2.8	3.8	6.6 YZ	
325		1.6	4.1	5.7 YZ	
335R		1.2	4.4	5.6 YZ	
335R		2.9	5.3	8.1 YZ	↓
340		4.7	8.4	13.1 YZ	17.6
350		2.8	6.5	9.3 YZ	
355		1.0	4.6	5.6 YZ	
360		1.9	3.4	5.3 YZ	
365		3.1	4.1	7.2 YZ	
370		3.7	2.8	6.5 YZ	
375		3.6	2.0	5.6 YZ	
380		3.4	3.3	6.7 YZ	
382		2.4	2.7	5.1 YZ	↓
385	↓	2.5	3.0	5.5 YZ	17.2
400	2.9	1.7	5.1	9.7 YZ	17.2



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TELEDYNE
ENGINEERING SERVICES

DONALD C. COOK
 UNIT #1
 PROJECT 5364

BY: DMS DATE: 5-3-83

CHECKED BY: DMS DATE: 5/3/83

STRESS SUMMARY - EQUATION B1

NODE #	PRESSURE STRESS (KSI)	DEADWEIGHT STRESS (KSI)	OBE STRESS (KSI)	EQUATION B1-STRESS (KSI)	ALLOWABLE STRESS (KSI)
405	2.9	2.1	5.3	10.3 YE	17.2
420		2.6	6.9	12.4 YE	
429		4.1	8.1	15.1 YE	
430		4.6	8.6	16.1 YE	
431		4.7	8.7	16.3 YE	↓
435 B	↓	5.0	10.5	18.4 YE	19.2
335 B	0	3.0	5.7	8.7 YE	17.9
610		3.6	5.7	9.3 YE	17.6
615		3.5	5.5	9.0 YE	
620		2.6	4.2	6.8 YE	↓
625	↓	2.8	4.3	7.1 YE	17.2
635	2.9	2.9	3.5	9.3 YE	
645		3.7	3.4	10.0 YE	
657		3.8	3.8	10.5 YE	
660		3.2	4.3	10.4 YE	
665		3.0	4.5	10.4 YE	↓
600 B	↓	3.0	5.7	11.6 YE	17.2



6.1.4 Equation B-2 Stresses

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DONALD C. COOK
 UNIT #1
 PROJECT 5364

BY: SMS DATE: 5/23/83

CHECKED BY: AMB DATE: 5-25-83

STRESS SUMMARY - EQUATION B2

NODE #	PRESSURE STRESS (KSI)	DEADWEIGHT STRESS (KSI)	OBE STRESS (KSI)	PORV TRANSIENT SHOCK STRESS (KSI)	EQUATION B2 STRESS (KSI)	ALLOWABLE STRESS (KSI)
1	.6	.1	.1	0	.8	19.5
4		.9	.8	.3	2.4	
6		.3	.5	2.2	3.2	
7		.2	.2	.1	1.0	
8		.1	.1	.1	.8	
10		.2	.2	.1	1.0	
12		.5	.4	.2	1.5	
18		.4	.1	.1	1.1	
30	<u>↓</u>	.4	.2	.2	1.3	<u>↓</u>
32	.7	.7	.2	.2	1.7	20.1
33		.4	.1	.1	1.2	
34		.4	.2	.1	1.3	
36		.5	.1	.1	1.3	
38		.2	.3	.5	1.5	
40		.2	.2	.3	1.3	
42		.1	.1	.1	.9	
44		.2	.2	.3	1.3	
46		.2	.2	.2	1.2	
48		.1	.1	.1	.9	
50	<u>↓</u>	.2	.2	.2	1.2	<u>↓</u>



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**TELEDYNE
 ENGINEERING SERVICES**

DONALD C. COOK
 UNIT #1
 PROJECT 5364

BY: DMD DATE: May 23, 1983

CHECKED BY: AMB DATE: 5-25-83

STRESS SUMMARY - EQUATION B2

NODE #	PRESSURE STRESS (KSI)	DEADWEIGHT STRESS (KSI)	OBE STRESS (KSI)	PORV TRANSIENT SHOCK STRESS(KSI)	EQUATION B2 STRESS (KSI)	ALLOWABLE STRESS (KSI)
52	.7	.3	.3	.3	1.4	20.1
56		.4	.2	.3	1.5	20.0
58		.4	.2	.3	1.5	
60		.3	.2	.4	1.4	
62		.4	.2	.3	1.5	
66		.2	.3	.5	1.5	
68		.2	.2	.4	1.3	
70		.2	.2	.4	1.3	
72		.1	.4	.5	1.4	↓
74		.3	.1	.3	1.3	19.9
76		.2	.2	.2	1.2	
80		.3	.2	.3	1.4	
82		.5	.2	.5	1.7	
83		.2	.2	.2	1.2	
84		.5	.2	.4	1.6	
86		.3	.2	.2	1.4	
88		.3	.2	.3	1.4	
90		.5	.2	.4	1.6	
93	↓	.4	.2	.4	1.5	
9TR	.9	.8	.4	.4	2.3	↓



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TELEDYNE
ENGINEERING SERVICES

DONALD C. COOK
 UNIT #1
 PROJECT 5364

BY: SMD DATE: 5/23/83

CHECKED BY: AMB DATE: 5-25-83

STRESS SUMMARY - EQUATION B2

NODE #	PRESSURE STRESS (KSI)	DEADWEIGHT STRESS (KSI)	OBE STRESS (KSI)	PORV TRANSIENT SHOCK STRESS(KSI)	EQUATION B2 STRESS (KSI)	ALLOWABLE STRESS (KSI)
97R	.9	.7	.4	.4	2.2	19.9
195		.5	.3	.3	1.8	
142R		.7	.4	.4	2.2	
142R		.6	.4	.4	2.1	
200		.4	.2	.2	1.6	
206R		.3	.4	.3	1.7	
206R		.3	.3	.3	1.6	↓
260	↓	1.0	.8	.8	3.0	18.3
280	1.0	1.5	2.1	2.1	5.5	18.1
285	1.0	4.5	1.5	1.1	7.4	18.1
290	1.5	5.3	2.0	1.6	9.4	17.9
295B	1.5	3.7	1.7	1.3	7.3	17.9
97B	.3	.7	1.1	.9	2.4	18.3
98		.8	.3	.3	1.5	
99		.7	.4	.5	1.6	
100		.4	.7	.6	1.6	↓
102		.3	.8	.5	1.5	18.2
103		.3	1.0	.2	1.6	
104		.8	1.8	.2	2.9	
106	↓	1.0	1.9	.3	3.2	↓

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**TELEDYNE
 ENGINEERING SERVICES**

DONALD C. COOK
 UNIT #1
 PROJECT 5364

BY: SMD DATE: 5/23/83

CHECKED BY: JMB DATE: 5-25-83

STRESS SUMMARY - EQUATION B2

NODE #	PRESSURE STRESS (KSI)	DEADWEIGHT STRESS (KSI)	OBE STRESS (KSI)	PORV TRANSIENT SHOCK STRESS (KSI)	EQUATION B2 STRESS (KSI)	ALLOWABLE STRESS (KSI)
108	.3	.6	1.1	.2	2.0	18.2
109		.9	1.2	.2	2.4	18.2
110		1.2	1.3	.2	2.8	17.8
112	↓	.5	2.4	.5	3.3	17.8
114	.1	1.2	2.6	.6	4.0	17.7
1140		.7	1.5	.3	2.3	17.7
115	↓	.7	1.5	.3	2.3	14.1
120	3.5	.9	.4	.1	4.8	13.9
122		1.1	2.5	.1	7.1	19.2
124		.9	2.9	.1	7.3	
126		.9	2.9	.1	7.3	
128		.7	2.6	.1	6.8	
130		.6	1.6	.1	5.7	
132		.9	1.3	.2	5.7	
134		1.0	1.4	.2	5.9	
136		1.2	1.7	.2	6.4	
138	↓	1.3	1.6	.2	6.4	↓
142 B	.7	.6	.7	.6	2.2	18.3
144	↓	.4	.4	.5	1.7	↓
146	↓	.2	.7	.3	1.7	↓

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TELEDYNE
ENGINEERING SERVICES

DONALD C. COOK
 UNIT #1
 PROJECT 5364

BY: SMD DATE: 5/23/83

CHECKED BY: AMB DATE: 5-25-83

STRESS SUMMARY - EQUATION B2

NODE #	PRESSURE STRESS (KSI)	DEADWEIGHT STRESS (KSI)	OBE STRESS (KSI)	PORV TRANSIENT SHOCK STRESS (KSI)	EQUATION B2 STRESS (KSI)	ALLOWABLE STRESS (KSI)
148	.3	.3	1.0	.1	1.6	18.2
150		1.0	2.1	.1	3.4	
152		1.4	2.2	.3	3.9	
156		.8	1.4	.2	2.5	↓
157		1.1	1.2	.1	2.6	17.8
158		1.3	1.2	.1	2.8	↓
160	↓	.7	2.0	.2	3.0	↓
162	.1	1.2	2.1	.2	3.4	17.7
163	↓	.7	1.3	.1	2.1	17.7
165	↓	.7	1.3	.1	2.1	14.1
170	3.5	.9	.3	.1	4.7	13.4
172		1.0	2.3	.1	6.8	19.2
174		.8	2.7	.1	7.0	
176		.8	2.7	.1	7.0	
178		.5	2.4	.1	6.4	
180		.5	1.5	.1	5.5	
181		.8	1.1	.1	5.4	
182		.9	1.2	.1	5.6	
184		1.1	1.5	.1	6.1	
185	↓	1.2	1.4	.1	6.1	↓

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DONALD C. COOK
 UNIT #1
 PROJECT 5364

BY: DMD DATE: 5/23/83

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STRESS SUMMARY - EQUATION B2

NODE #	PRESSURE STRESS (KSI)	DEADWEIGHT STRESS (KSI)	OBE STRESS (KSI)	PORV TRANSIENT SHOCK STRESS (KSI)	EQUATION B2 STRESS (KSI)	ALLOWABLE STRESS (KSI)
206B	.7	1.1	1.3	.7	3.3	18.3
208	.7	.3	1.0	.2	2.0	18.3
214	.3	1.0	2.1	.4	3.4	18.2
216	.3	1.5	2.2	.5	4.1	18.2
220	.3	1.3	.8	.2	2.4	17.8
222	.3	.6	1.3	.5	2.3	17.8
223	.1	1.0	1.4	.5	2.6	17.7
2230	.1	.6	.8	.3	1.6	17.7
225	.1	.6	.8	.3	1.6	14.1
229	3.5	.7	.4	.1	4.6	13.9
233		.8	2.0	.1	6.3	19.2
234		.5	2.2	.1	6.2	
235		.5	2.2	.1	6.2	
236		.3	1.8	.1	5.6	
237		.2	1.3	.1	5.0	
238		.7	1.1	.2	5.3	
240		.8	1.1	.2	5.4	
242		1.1	1.3	.2	5.9	
244		1.1	1.3	.2	5.9	
295R	1.5	3.2	1.5	.9	6.4	17.9

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TELEDYNE
ENGINEERING SERVICES

DONALD C. COOK
 UNIT #1
 PROJECT 5364

BY: DMD DATE: 5/23/83

CHECKED BY: AMB DATE: 5-25-83

STRESS SUMMARY - EQUATION B2

NODE #	PRESSURE STRESS (KSI)	DEADWEIGHT STRESS (KSI)	OBE STRESS (KSI)	PORV TRANSIENT SHOCK STRESS (KSI)	EQUATION B2 STRESS (KSI)	ALLOWABLE STRESS (KSI)
560	1.5	9.9	4.1	2.8	16.4	17.9
555	1.0	5.6	1.9	1.6	9.1	17.9
550	1.9	3.5	4.8	2.0	10.6	17.6
545		3.7	9.9	3.1	16.0	17.6
540		3.8	11.4	3.5	17.6	
536		3.7	8.6	2.6	14.6	
535		4.1	8.0	2.4	14.4	
534		4.7	7.2	2.3	14.2	
533		5.6	9.6	3.1	17.5	
530		6.4	8.2	3.0	17.0	
529		4.2	6.2	4.0	13.5	
525		4.6	6.3	5.8	15.1	17.2
510	2.9	3.0	3.6	4.0	11.3	
505		2.5	4.0	4.0	11.1	
490		1.7	4.5	4.6	11.0	
485		2.3	4.2	3.0	10.9	
480		2.7	4.2	3.0	10.8	
475		2.5	4.2	2.7	10.4	
465		4.2	4.1	3.3	12.4	
460		2.7	4.7	2.5	10.9	

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**TELEDYNE
 ENGINEERING SERVICES**

DONALD C. COOK
 UNIT #1
 PROJECT 5364

BY: JMD DATE: 5/23/83

CHECKED BY: AMB DATE: 5-25-83

STRESS SUMMARY - EQUATION B2

NODE #	PRESSURE STRESS (KSI)	DEADWEIGHT STRESS (KSI)	OBE STRESS (KSI)	PORV TRANSIENT SHOCK STRESS (KSI)	EQUATION B2 STRESS (KSI)	ALLOWABLE STRESS (KSI)
450	2.9	5.0	5.9	4.3	15.2	17.2
440	4.1	5.4	5.8	4.5	16.8	17.2
435R		3.4	3.3	2.8	11.8	19.2
436R		1.1	6.0	3.1	12.0	
575		3.5	3.9	1.8	11.9	
585		5.5	5.0	2.7	15.3	
590		6.3	4.2	2.0	15.1	
595		7.0	4.5	2.5	16.2	
600R	↓	2.1	1.5	.9	7.9	
600R	3.5	2.5	1.7	.9	7.9	
668		2.6	1.7	1.0	8.1	
670		2.6	1.8	1.1	8.2	
675		2.9	1.6	1.2	8.4	
680		2.9	1.6	1.2	8.4	
690		2.6	1.3	1.1	7.8	
700		2.1	1.2	1.4	7.4	
710		1.1	1.4	2.5	7.5	
715		.8	1.5	2.9	7.6	
717		.5	1.8	1.4	6.3	
720	↓	.4	1.9	2.0	6.7	↓



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**TELEDYNE
 ENGINEERING SERVICES**

DONALD C. COOK
 UNIT #1
 PROJECT 5364

BY: Dms DATE: 5/23/83

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STRESS SUMMARY - EQUATION B2

NODE #	PRESSURE STRESS (KSI)	DEADWEIGHT STRESS (KSI)	OBE STRESS (KSI)	PORV TRANSIENT SHOCK STRESS(KSI)	EQUATION B2 STRESS (KSI)	ALLOWABLE STRESS (KSI)
725	3.5	.4	2.0	2.7	7.3	19.2
750	3.5	.3	2.7	4.6	9.1	19.2
295R	1.5	2.7	2.1	1.3	6.7	17.9
300	1.5	5.2	4.1	2.1	11.3	
310	1.2	4.1	3.7	2.1	9.6	
320	1.2	2.8	3.8	2.9	8.8	
325	1.2	1.6	4.1	3.6	8.3	
335R	2.3	1.2	4.4	3.3	9.0	
335R	2.3	2.9	5.3	1.8	10.8	↓
340	2.3	4.7	8.4	2.7	15.8	17.6
350	1.9	2.8	6.5	2.0	11.5	
355		1.0	4.6	1.9	7.9	
360		1.9	3.4	1.8	7.6	
365		3.1	4.1	2.4	9.8	
370		3.7	2.8	2.3	9.2	
375		3.6	2.0	2.7	8.9	
380		3.4	3.3	3.5	10.1	
382		2.4	2.7	2.6	8.0	↓
385		2.5	3.0	2.6	8.4	17.2
400	2.9	1.7	5.1	4.2	11.2	17.2

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DONALD C. COOK
 UNIT #1
 PROJECT 5364

BY: SMD DATE: 5/23/83

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STRESS SUMMARY - EQUATION B2

NODE #	PRESSURE STRESS (KSI)	DEADWEIGHT STRESS (KSI)	OBE STRESS (KSI)	PORV TRANSIENT SHOCK STRESS (KSI)	EQUATION B2 STRESS (KSI)	ALLOWABLE STRESS (KSI)
405	2.9	2.1	5.3	4.0	11.6	17.2
420		2.6	6.9	3.2	13.1	
429		4.1	8.1	3.0	15.6	
430		4.6	8.6	3.1	16.6	
431		4.7	8.7	3.1	16.8	↓
435 B	↓	5.0	10.5	3.6	19.0	19.2
335 B	2.3	3.0	5.7	5.5	13.2	17.9
610	1.9	3.6	5.7	2.7	11.8	17.6
615	1.9	3.5	5.5	3.2	11.8	↓
620	1.9	2.6	4.2	2.5	9.4	↓
625	1.9	2.8	4.3	4.7	11.1	17.2
635	2.9	2.9	3.5	9.6	16.0	↓
645		3.7	3.4	5.4	13.0	↓
657		3.8	3.8	3.2	11.7	↓
660		3.2	4.3	2.2	10.9	↓
665		3.0	4.5	2.7	11.1	↓
600 B	↓	3.0	5.7	5.4	13.8	↓

6.1.5 Equation B-3 Stresses



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DONALD C. COOK
UNIT #1
PROJECT 5364

BY: DMD DATE: 5/25/83

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STRESS SUMMARY - EQUATION B3

NODE #	PORV TRANSIENT THERMAL STRESS RANGE (KSI)	ALLOWABLE STRESS (KSI)
1	.2	27.5
4	2.0	
6	2.0	
7	.8	
8	.8	
10	2.2	
12	2.3	
18	.9	
30	2.5	
32	2.5	27.6
33	.9	
34	.9	
36	.9	
38	1.4	
40	1.4	
42	.5	
44	1.4	
46	1.7	
48	.7	
50	2.0	



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DONALD C. COOK
UNIT #1
PROJECT 5364

BY: DMD DATE: 5/25/83

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STRESS SUMMARY - EQUATION B3

NODE #	PORV TRANSIENT THERMAL STRESS RANGE (KSI)	ALLOWABLE STRESS (KSI)
52	2.2	27.6
56	2.5	
58	2.5	
60	2.9	
62	3.3	
66	1.4	
68	1.3	
70	1.3	
72	.7	
74	.9	
76	.8	
80	.8	
82	.8	
83	1.3	
84	.8	
86	.7	
88	.7	
90	.8	
93	.4	
97R	1.2	



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DONALD C. COOK
UNIT #1
PROJECT 5364

BY: DMD DATE: 5/25/83

CHECKED BY: DMB DATE: 5-25-83

STRESS SUMMARY - EQUATION B3

NODE #	PORV TRANSIENT THERMAL STRESS RANGE (KSI)	ALLOWABLE STRESS (KSI)
97 R	1.6	27.6
195	.8	
142 R	1.6	
142 R	2.1	
200	.9	
206 R	1.8	
206 R	2.5	↓
260	4.3	27.3
280	9.7	27.2
285	6.0	
290	5.6	
295 B	4.7	↓
97 B	4.7	27.3
98	2.3	
99	1.7	
100	1.2	↓
102	1.0	27.2
103	1.2	
104	3.3	
106	3.3	↓

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DONALD C. COOK
UNIT #1
PROJECT 5364

BY: DMT DATE: 5/25/83

CHECKED BY: DMB DATE: 5-25-83

STRESS SUMMARY - EQUATION B3

NODE #	PORV TRANSIENT THERMAL STRESS RANGE (KSI)	ALLOWABLE STRESS (KSI)
108	1.5	27.2
109	.7	27.2
110	.5	27.1
112	1.7	27.1
114	1.4	27.1
1140	.6	27.1
115	.6	26.4
120	.2	26.3
122	.4	27.4
124	.6	
126	.6	
128	.7	
130	.5	
132	.5	
134	.5	
136	.5	
138	.5	
142 B	6.1	27.3
144	2.8	
146	1.8	

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DONALD C. COOK
UNIT #1
PROJECT 5364

BY: Smd DATE: 5/23/83

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STRESS SUMMARY - EQUATION B3

NODE #	PORV TRANSIENT THERMAL STRESS RANGE (KSI)	ALLOWABLE STRESS (KSI)
148	1.0	27.2
150	2.5	
152	2.9	
156	1.2	
157	.5	27.1
158	.3	
160	.7	
162	.4	
163	.2	
165	.2	26.4
170	.5	26.3
172	.8	27.4
174	1.0	
176	1.0	
178	1.2	
180	1.1	
181	.9	
182	.9	
184	.9	
185	.8	

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DONALD C. COOK
UNIT #1
PROJECT 5364

BY: SJD DATE: 5/25/83

CHECKED BY: JMB DATE: 5-25-83

STRESS SUMMARY - EQUATION B3

NODE #	PORV TRANSIENT THERMAL STRESS RANGE (KSI)	ALLOWABLE STRESS (KSI)
206B	12.1	27.3
208	3.9	27.3
214	4.5	27.2
216	3.7	27.2
220	.5	27.1
222	2.0	27.1
223	3.3	27.1
2230	1.5	27.1
225	1.5	26.4
229	1.5	26.3
233	1.6	27.4
234	2.2	
235	2.2	
236	2.7	
237	2.7	
238	2.6	
240	2.6	
242	2.5	
244	2.3	
295 R	6.3	27.2

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DONALD C. COOK
UNIT #1
PROJECT 5364

BY: SMD DATE: 5/25/83

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STRESS SUMMARY - EQUATION B3

NODE #	PORV TRANSIENT THERMAL STRESS RANGE (KSI)	ALLOWABLE STRESS (KSI)
560	13.3	27.2
555	4.1	27.2
550	2.1	27.1
545	5.0	
540	3.9	
536	2.5	
535	2.8	
534	3.3	
533	5.9	
530	7.1	
529	3.9	
525	3.8	27.0
510	2.0	
505	1.8	
490	1.7	
485	1.4	
480	1.4	
475	1.2	
465	2.2	
460	1.5	

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DONALD C. COOK
UNIT #1
PROJECT 5364

BY: SMD DATE: 5/25/83

CHECKED BY: AKB DATE: 5-25-83

STRESS SUMMARY - EQUATION B3

NODE #	PORV TRANSIENT THERMAL STRESS RANGE (KSI)	ALLOWABLE STRESS (KSI)
450	2.2	27.0
440	2.3	27.0
435 R	1.4	27.4
435 R	3.0	
575	2.9	
585	1.9	
590	2.7	
595	3.2	
600 R	.9	
600 R	1.5	
668	1.5	
670	1.7	
675	1.8	
680	1.6	
690	1.9	
700	1.9	
710	1.6	
715	1.7	
717	2.3	
720	2.7	<u>✓</u>

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DONALD C. COOK
UNIT #1
PROJECT 5364

BY: DMD DATE: 5/25/83

CHECKED BY: AMB DATE: 5-25-83

STRESS SUMMARY - EQUATION B3

NODE #	PORV TRANSIENT THERMAL STRESS RANGE (KSI)	ALLOWABLE STRESS (KSI)
725	2.9	27.4
750	2.9	27.4
295R	2.1	27.2
300	2.4	
310	.8	
320	2.1	
325	2.8	
335R	4.1	
335R	3.9	↓
340	4.7	27.1
350	3.1	
355	1.6	
360	1.9	
365	2.9	
370	1.6	
375	.6	
380	1.7	
382	1.0	
385	1.2	
400	1.1	↓



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DONALD C. COOK
UNIT #1
PROJECT 5364

BY: DMD DATE: 5/25/83

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STRESS SUMMARY - EQUATION B3

NODE #	PORV TRANSIENT THERMAL STRESS RANGE (KSI)	ALLOWABLE STRESS (KSI)
405	1.7	27.0
420	2.3	
429	2.9	
430	3.1	
431	3.1	
435 B	3.9	↓
335 B	2.6	27.2
610	6.1	27.1
615	6.8	↓
620	3.8	↓
625	3.7	27.0
635	2.2	
645	2.7	
657	3.2	
660	3.8	
665	3.9	
600 B	4.4	↓

6.1.6 Equation C-1 Stresses



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**TELEDYNE
 ENGINEERING SERVICES**

DONALD C. COOK
 UNIT #1
 PROJECT 5364

BY: DMB DATE: 5-3-83

CHECKED BY: DAD DATE: 5/3/83

STRESS SUMMARY - EQUATION C1

NODE #	PRESSURE STRESS (KSI)	DEADWEIGHT STRESS (KSI)	DBE STRESS (KSI)	EQUATION C1 STRESS (KSI)	ALLOWABLE STRESS (KSI)
1	0	.1	.2	.3 YE	29.2
4		.9	1.3	2.2 YE	
6		.3	.8	1.1 YE	
7		.2	.3	.5 YE	
8		.1	.2	.3 YE	
10		.2	.3	.5 YE	
12		.5	.7	1.2 YE	
18		.4	.2	.6 YE	
30		.4	.3	.7 YE	.4
32		.7	.4	1.1 YE	30.1
33		.4	.1	.5 YE	
34		.4	.2	.6 YE	
36		.5	.2	.7 YE	
38		.2	.5	.7 YE	
40		.2	.4	.6 YE	
42		.1	.2	.3 YE	
44		.2	.3	.5 YE	
46		.2	.3	.5 YE	
48		.1	.2	.3 YE	
50	.4	.2	.4	.6 YE	.4

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TELEDYNE
ENGINEERING SERVICES

DONALD C. COOK
 UNIT #1
 PROJECT 5364

BY: DWB DATE: 5-3-83

CHECKED BY: SMB DATE: 5/3/83

STRESS SUMMARY - EQUATION C1

NODE #	PRESSURE STRESS (KSI)	DEADWEIGHT STRESS (KSI)	DBE STRESS (KSI)	EQUATION C1 STRESS (KSI)	ALLOWABLE STRESS (KSI)
52	0.	.3	.5	.8 YZ	30.1
56		.4	.4	.8 XY	30.0
58		.4	.4	.8 XY	
60		.3	.4	.7 YZ	
62		.4	.3	.7 XY	
66		.2	.4	.6 YZ	
68		.2	.4	.6 YZ	
70		.2	.3	.5 YZ	
72		.1	.6	.7 YZ	↓
74		.3	.3	.6 XY	29.8
76		.2	.3	.5 XY	
80		.3	.3	.6 XY	
82		.5	.4	.9 XY	
83		.2	.3	.5 XY	
84		.5	.4	.9 XY	
86		.3	.3	.6 XY	
88		.3	.3	.6 XY	
90		.5	.4	.9 XY	
93		.4	.3	.7 XY	
97B	↓	.8	.6	1.4 XY	↓

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**TELEDYNE
 ENGINEERING SERVICES**

DONALD C. COOK
 UNIT #1
 PROJECT 5364

BY: DWC DATE: 5-3-83

CHECKED BY: SJD DATE: 5/3/83

STRESS SUMMARY - EQUATION C1

NODE #	PRESSURE STRESS (KSI)	DEADWEIGHT STRESS (KSI)	DBE STRESS (KSI)	EQUATION C1 STRESS (KSI)	ALLOWABLE STRESS (KSI)
97R	0	.7	.7	1.4 XY	29.9
195		.5	.4	.9 XY	
142R		.7	.6	1.3 XY	
142R		.6	.7	1.3 XY	
200		.4	.4	.8 XY	
206R		.3	.6	.9 XY	
206R		.3	.4	.7 XY	↓
260		1.0	1.3	2.3 XY	27.5
280		1.5	3.2	4.7 XY	27.1
285		4.5	2.2	6.7 XY	27.1
290		5.3	3.0	8.3 XY	26.8
295B		3.7	2.5	6.2 XY	26.8
97B		.7	1.8	2.5 XY	27.5
98		.8	.6	1.4 XY	
99		.7	.7	1.4 XY	
100		.4	1.1	1.5 XY	↓
102		.3	1.4	1.7 XY	27.2
103		.3	1.7	2.0 XY	
104		.8	3.1	3.9 XY	
106	↓	1.0	3.3	4.3 XY	↓

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TELEDYNE
ENGINEERING SERVICES

DONALD C. COOK
 UNIT #1
 PROJECT 5364

BY: AMB DATE: 5-3-83

CHECKED BY: Dmb DATE: 5/3/83

STRESS SUMMARY - EQUATION C1

NODE #	PRESSURE STRESS (KSI)	DEADWEIGHT STRESS (KSI)	DBE STRESS (KSI)	EQUATION C1 STRESS (KSI)	ALLOWABLE STRESS (KSI)
108	0	.6	2.0	2.6 XY	27.2
109		.9	2.0	2.9 XY	27.2
110		1.2	2.3	3.5 XY	26.7
112		.5	4.3	4.8 XY	26.7
114		1.2	4.5	5.7 XY	26.5
1140		.7	2.6	3.3 XY	26.5
115	↓	.7	2.7	3.4 XY	21.2
120	3.5	.9	.7	5.1 YZ	20.9
122		1.1	4.3	8.9 XY	28.8
124		.9	5.1	9.5 XY	
126		.9	5.1	9.5 XY	
128		.7	4.5	8.7 XY	
130		.6	2.8	6.9 XY	
132		.9	2.1	6.5 YZ	
134		1.0	2.3	6.8 YZ	
136		1.2	2.8	7.5 YZ	
138	↓	1.3	2.7	7.5 YZ	↓
142B	0	.6	1.2	1.8 YZ	27.5
144		.4	.7	1.1 YZ	
146	↓	.2	1.2	1.4 YZ	↓



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**TELEDYNE
 ENGINEERING SERVICES**

DONALD C. COOK
 UNIT #1
 PROJECT 5364

BY: AWB DATE: 5-3-83

CHECKED BY: SMB DATE: 5-3-83

STRESS SUMMARY - EQUATION C1

NODE #	PRESSURE STRESS (KSI)	DEADWEIGHT STRESS (KSI)	DBE STRESS (KSI)	EQUATION C1 STRESS (KSI)	ALLOWABLE STRESS (KSI)
148	0	.3	1.8	2.1 YZ	27.2
150		1.0	3.6	4.6 YZ	27.2
152		1.4	3.9	5.3 YZ	27.2
156		.8	2.3	3.1 YZ	27.2
157		1.1	2.0	3.1 YZ	26.7
158		1.3	2.0	3.3 YZ	26.7
160		.7	3.5	4.2 YZ	26.7
162		1.2	3.7	4.9 YZ	26.5
163		.7	2.2	2.9 YZ	26.5
165	↓	.7	2.2	2.9 YZ	21.1
170	3.5	.9	.6	5.0 XY	20.9
172		1.0	4.0	8.5 YZ	28.8
174		.8	4.7	9.0 YZ	28.8
176		.8	4.7	9.0 YZ	
178		.5	4.2	8.2 YZ	
180		.5	2.6	6.6 YZ	
181		.8	2.0	6.3 YZ	
182		.9	2.0	6.4 XY	
184		1.1	2.4	7.0 XY	
185	↓	1.2	2.4	7.1 XY	↓

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**TELEDYNE
 ENGINEERING SERVICES**

DONALD C. COOK
 UNIT #1
 PROJECT 5364

BY: JMB DATE: 5-3-83

CHECKED BY: Sms DATE: 5/4/83

STRESS SUMMARY - EQUATION C1

NODE #	PRESSURE STRESS (KSI)	DEADWEIGHT STRESS (KSI)	DBE STRESS (KSI)	EQUATION C1 STRESS (KSI)	ALLOWABLE STRESS (KSI)
206B	0	1.1	2.2	3.3 XY	27.5
208		.3	1.6	1.9 XY	27.5
214		1.0	3.5	4.5 XY	27.2
216		1.5	3.8	5.3 XY	27.2
220		1.3	1.4	2.7 XY	26.7
222		.6	2.3	2.9 XY	26.7
223		1.0	2.4	3.4 XY	26.5
2230		.6	1.4	2.0 XY	26.5
225	↓	.6	1.4	2.0 XY	21.1
229	3.5	.7	.7	4.9 XY	20.9
233		.8	3.4	7.7 XY	28.8
234		.5	3.7	7.7 XY	
235		.5	3.7	7.7 XY	
236		.3	3.1	6.9 XY	
237		.2	2.2	5.9 XY	
238		.7	1.8	6.0 XY	
240		.8	1.9	6.2 XY	
242		1.1	2.2	6.8 YZ	
244	↓	1.1	2.2	6.8 YZ	↓
295R	0	3.2	2.0	5.2 YZ	26.8



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**TELEDYNE
 ENGINEERING SERVICES**

DONALD C. COOK
 UNIT #1
 PROJECT 5364

BY: AMB DATE: 5-3-83

CHECKED BY: Dms DATE: 5/4/83

STRESS SUMMARY - EQUATION C1

NODE #	PRESSURE STRESS (KSI)	DEADWEIGHT STRESS (KSI)	DBE STRESS (KSI)	EQUATION C1 STRESS (KSI)	ALLOWABLE STRESS (KSI)
560	0	9.9	5.5	15.4 YZ	26.8
555		5.6	2.7	8.3 YZ	26.8
550		3.5	6.6	10.1 YZ	26.3
545		3.7	13.5	17.2 YZ	
540		3.8	15.5	19.3 YZ	
536		3.7	11.6	15.3 YZ	
535		4.1	10.8	14.9 YZ	
534		4.7	9.8	14.5 YZ	
533		5.6	13.0	18.6 YZ	
530		6.4	11.2	17.6 YZ	
529		4.2	8.4	12.6 YZ	↓
525	↓	4.6	8.5	13.1 YZ	25.7
510	2.9	3.0	5.6	11.5 XY	
505		2.5	6.0	11.4 XY	
490		1.7	6.6	11.2 XY	
485		2.8	5.8	11.5 YZ	
480		2.7	5.8	11.4 YZ	
475		2.5	5.8	11.2 YZ	
465		4.2	5.6	12.7 YZ	
460	↓	2.7	6.4	12.0 YZ	↓

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**TELEDYNE
 ENGINEERING SERVICES**

DONALD C. COOK
 UNIT #1
 PROJECT 5364

BY: DMB DATE: 5-3-83

CHECKED BY: DMB DATE: 5/4/83

STRESS SUMMARY - EQUATION C1

NODE #	PRESSURE STRESS (KSI)	DEADWEIGHT STRESS (KSI)	DBE STRESS (KSI)	EQUATION C1 STRESS (KSI)	ALLOWABLE STRESS (KSI)
450	2.9	5.0	8.2	16.1 YZ	25.7
440	4.1	5.4	8.1	17.6 YZ	25.7
435R		3.4	4.8	12.3 XY	28.8
435R		1.1	8.3	13.5 YZ	
575		3.5	5.4	13.0 YZ	
585		5.5	6.8	16.4 YZ	
590		6.3	5.7	16.1 YZ	
595	↓	7.0	6.3	17.4 YZ	
600R	3.5	2.1	2.0	7.6 YZ	
600R		2.5	2.4	8.4 YZ	
668		2.6	2.4	8.5 YZ	
670		2.6	2.4	8.5 YZ	
675		2.9	2.3	8.7 YZ	
680		2.9	2.3	8.7 YZ	
690		2.6	1.8	7.9 XY	
700		2.1	1.7	7.3 XY	
710		1.1	2.0	6.6 XY	
715		.8	2.3	6.6 XY	
717		.5	2.7	6.7 XY	
720	↓	.4	2.9	6.8 XY	↓

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**TELEDYNE
 ENGINEERING SERVICES**

DONALD C. COOK
 UNIT #1
 PROJECT 5364

BY: AMB DATE: 5-3-83

CHECKED BY: Dmb DATE: 5/4/83

STRESS SUMMARY - EQUATION C1

NODE #	PRESSURE STRESS (KSI)	DEADWEIGHT STRESS (KSI)	DBE STRESS (KSI)	EQUATION C1 STRESS (KSI)	ALLOWABLE STRESS (KSI)
725	3.5	.4	3.0	6.9 XY	28.8
750	3.5	.3	3.8	7.6 XY	28.8
295R	0	2.7	2.9	5.6 YZ	26.8
300		5.2	5.6	10.8 YZ	
310		4.1	5.0	9.1 YZ	
320		2.8	5.3	8.1 YZ	
325		1.6	5.9	7.5 YZ	
335R		1.2	6.3	7.5 YZ	
335R		2.9	7.3	10.2 YZ	↓
340		4.7	11.7	16.4 YZ	26.3
350		2.8	9.1	11.9 YZ	
355		1.0	6.6	7.6 YZ	
360		1.9	5.1	7.0 YZ	
365		3.1	6.1	9.2 YZ	
370		3.7	4.2	7.9 YZ	
375		3.6	3.1	6.7 YZ	
380		3.4	4.8	8.2 YZ	
382		2.4	4.0	6.4 YZ	↓
385	↓	2.5	4.4	6.9 YZ	25.7
400	2.9	1.7	7.7	12.3 YZ	25.7

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TELEDYNE
ENGINEERING SERVICES

DONALD C. COOK
 UNIT #1
 PROJECT 5364

BY: JMB DATE: 5-3-83

CHECKED BY: dmd DATE: 5/4/83

STRESS SUMMARY - EQUATION C1

NODE #	PRESSURE STRESS (KSI)	DEADWEIGHT STRESS (KSI)	DBE STRESS (KSI)	EQUATION C1 STRESS (KSI)	ALLOWABLE STRESS (KSI)
405	2.9	2.1	8.0	13.0 YE	25.7
420		2.6	10.2	15.7 YE	
429		4.1	11.8	18.8 YE	
430		4.6	12.5	20.0 YE	
431		4.7	12.6	20.2 YE	
435B	↓	5.0	15.1	23.0 YE	25.7
335B	0	3.0	9.0	12.0 YE	26.8
610		3.6	8.5	12.1 YE	26.3
615		3.5	8.2	11.7 YE	
620		2.6	6.2	8.8 YE	↓
625	↓	2.8	6.5	9.3 YE	25.7
635	2.9	2.9	5.5	11.3 YE	
645		3.7	5.1	11.7 YE	
657		3.8	5.9	12.6 YE	
660		3.2	6.7	12.8 YE	
665		3.2	6.8	12.9 YE	
600B	↓	3.0	8.8	14.7 YE	25.7

6.2 Support Loads

Support loads are given for each support on the pressurizer relief line piping. Support load combinations were calculated in accordance with Table II, Reference 2. Combination E2 was not considered since the SV analysis was not performed. Thermal-1 refers to the normal thermal operating case and thermal-2 refers to the PORV transient thermal loading.

The support load combinations considered are as follows:

D1 = deadweight + normal thermal +/- OBE

D2 = deadweight + PORV transient thermal +/- $\left[\frac{(\text{OBE})^2 + (\text{PORV transient shock})^2}{2} \right]^{1/2}$

E1 = deadweight + normal thermal +/- DBE

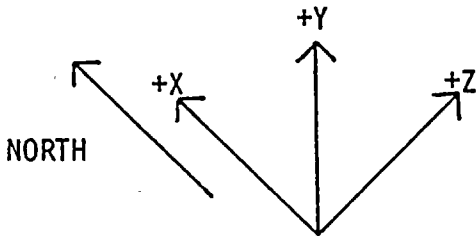
SUPPORT LOAD SUMMARY SHEET

DONALD C. COOK
 UNIT #1
 PROJECT 5364

BY: AKB DATE: 5-11-83

CHECKED BY: DMD DATE: 5/26/83

GLOBAL COORDINATE SYSTEM



MARK NUMBER 1-GRC-R-585

NODE NUMBER 33

	DESIGN LOADINGS								
	DISPLACEMENTS			FORCES			MOMENTS		
	X	Y	Z	FX	FY	FZ	MX	MY	MZ
DEADWEIGHT-1	0	.002	-.001	-60					
THERMAL-1	0	-.153	.069	2060					
THERMAL-2	0	-.045	-.393	-180					
SEISMIC-OBE	0	0	±.013	±221					
SEISMIC-DBE	0	±.001	±.021	±376					
BLOWDOWN-SRV									
BLOWDOWN-PORV	0	0	±.005	±423					

	TES COMBINED LOADS		
	FX	FY	FZ
NORMAL/UPSET	+2221 -717		
EMERGENCY	+2376 -436		

	SUPPORT DRAWING LOADS		
	FX	FY	FZ
DESIGN (+)	16613		
DESIGN (-)	15571		

UNITS: DISPLACEMENTS : INCHES
 FORCES : POUNDS
 MOMENTS : INCH-POUNDS

TES COMBINED LOADS ARE LESS
 THAN THE LOAD SHOWN
 ON THE SUPPORT DRAWING



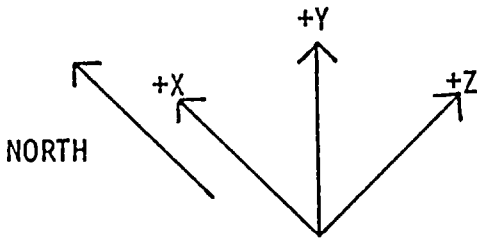
SUPPORT LOAD SUMMARY SHEET

DONALD C. COOK
 UNIT #1
 PROJECT 5364

BY: AMB DATE: 5-11-83

CHECKED BY: Smb DATE: 5/26/83

GLOBAL COORDINATE SYSTEM



MARK NUMBER 1-GRC-R-586

NODE NUMBER 36

DESIGN LOADINGS									
	DISPLACEMENTS			FORCES			MOMENTS		
	X	Y	Z	FX	FY	FZ	MX	MY	MZ
DEADWEIGHT-1	0	0	-0.001		-1020				
THERMAL-1	.002	0	.118		+2170				
THERMAL-2	.037	0	-.377		+370				
SEISMIC-OBE	0	0	±.013		±143				
SEISMIC-DBE	0	0	±.021		±254				
BLOWDOWN-SRV									
BLOWDOWN-PORV	0	0	±.006		±201				

	TES COMBINED LOADS		
	FX	FY	FZ
NORMAL/UPSET		+1293 -1163	
EMERGENCY		+1404 -1274	

	SUPPORT DRAWING LOADS		
	FX	FY	FZ
DESIGN (+)		7621	
DESIGN (-)		5856	

UNITS: DISPLACEMENTS : INCHES
 FORCES : POUNDS
 MOMENTS : INCH-POUNDS

TES COMBINED LOADS ARE LESS
 THAN THE LOAD SHOWN
 ON THE SUPPORT DRAWING



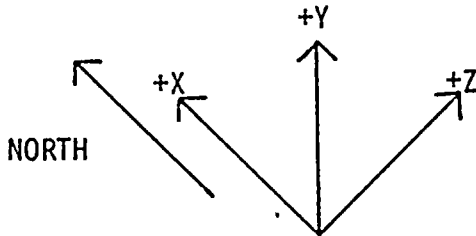
SUPPORT LOAD SUMMARY SHEET

DONALD C. COOK
 UNIT #1
 PROJECT 5364

BY: AKS DATE: 5-11-83

CHECKED BY: SMD DATE: 5/26/83

GLOBAL COORDINATE SYSTEM



MARK NUMBER 1-GRC-S-587

NODE NUMBER 42

	DESIGN LOADINGS								
	DISPLACEMENTS			FORCES			MOMENTS		
	X	Y	Z	FX	FY	FZ	MX	MY	MZ
DEADWEIGHT-1	.006	-.016	.003						
THERMAL-1	-.266	.855	.296						
THERMAL-2	.140	.329	-.326						
SEISMIC-OBE	±.004	0	±.011		±170				
SEISMIC-DBE	±.006	0	±.018		±281				
BLOWDOWN-SRV									
BLOWDOWN-PORV	±.008 -.006	0	±.014 -.010		±324				

	TES COMBINED LOADS		
	FX	FY	FZ
NORMAL/UPSET		+ 366 - 366	
EMERGENCY		+ 281 - 281	

	SUPPORT DRAWING LOADS		
	FX	FY	FZ
DESIGN (+)		12009	
DESIGN (-)		12009	

UNITS: DISPLACEMENTS : INCHES
 FORCES : POUNDS
 MOMENTS : INCH-POUNDS

TES COMBINED LOADS ARE LESS
 THAN THE LOAD SHOWN
 ON THE SUPPORT DRAWING



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TELEDYNE
ENGINEERING SERVICES

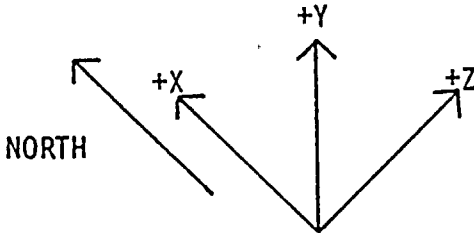
SUPPORT LOAD SUMMARY SHEET

DONALD C. COOK
 UNIT #1
 PROJECT 5364

BY: SMB DATE: 5-25-83

CHECKED BY: SMB DATE: 5/26/83

GLOBAL COORDINATE SYSTEM



MARK NUMBER 1-GRC-C-588

NODE NUMBER 48

	DESIGN LOADINGS								
	DISPLACEMENTS			FORCES			MOMENTS		
	X	Y	Z	FX	FY	FZ	MX	MY	MZ
DEADWEIGHT-1	.009	-.021	.004		426				
NORMAL-1	-.419	1.08	.218						
THERMAL-2	.151	.453	-.324						
SEISMIC-OBE	±.006	±.004	±.010						
SEISMIC-DBE	±.010	±.008	±.016						
BLOWDOWN-SRV									
BLOWDOWN-PORV	+ .013 - .011	+ .007 - .008	+ .016 - .010						

	TES COMBINED LOADS		
	FX	FY	FZ
NORMAL/UPSET		+426	
EMERGENCY		+426	

	SUPPORT DRAWING LOADS		
	FX	FY	FZ
DESIGN (+)		426	
DESIGN (-)			

UNITS: DISPLACEMENTS : INCHES
 FORCES : POUNDS
 MOMENTS : INCH-POUNDS

TES COMBINED LOADS ARE _____
 THAN THE LOAD SHOWN
 ON THE SUPPORT DRAWING

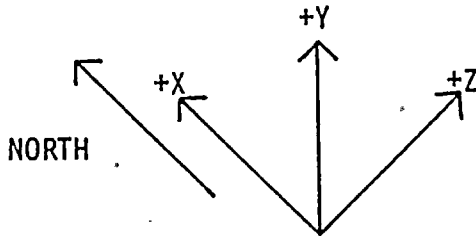
SUPPORT LOAD SUMMARY SHEET

DONALD C. COOK
UNIT #1
PROJECT 5364

BY: SWB DATE: 5-11-83

CHECKED BY: SWB DATE: 5/26/83

GLOBAL COORDINATE SYSTEM



MARK NUMBER 1-GRC-R-589

NODE NUMBER 66

	DESIGN LOADINGS								
	DISPLACEMENTS			FORCES			MOMENTS		
	X	Y	Z	FX	FY	FZ	MX	MY	MZ
DEADWEIGHT-1	0	-0.008	0	+70		+50			
THERMAL-1	0	2.26	0	-1360		-1119			
THERMAL-2	0	.964	0	+390		+100			
SEISMIC-OBE	0	±.002	0	±284		±384			
SEISMIC-DBE	0	±.004	0	±466		±637			
BLOWDOWN-SRV									
BLOWDOWN-PORV	0	+ .005 - .006	0	± 161		± 623			

	TES COMBINED LOADS		
	FX	FY	FZ
NORMAL/UPSET	+786 -1574		+882 -1453
EMERGENCY	+536 -1756		+487 -1706

	SUPPORT DRAWING LOADS		
	FX	FY	FZ
DESIGN (+)	4246		10089
DESIGN (-)	5595		10770

UNITS: DISPLACEMENTS : INCHES
FORCES : POUNDS
MOMENTS : INCH-POUNDS

TES COMBINED LOADS ARE LESS
THAN THE LOAD SHOWN
ON THE SUPPORT DRAWING



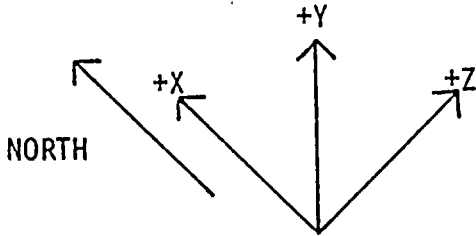
SUPPORT LOAD SUMMARY SHEET

DONALD C. COOK
 UNIT #1
 PROJECT 5364

BY: JMB DATE: 5-25-83

CHECKED BY: SMB DATE: 5/26/83

GLOBAL COORDINATE SYSTEM



MARK NUMBER 1-GRC-C-590

NODE NUMBER 70

	DESIGN LOADINGS								
	DISPLACEMENTS			FORCES			MOMENTS		
	X	Y	Z	FX	FY	FZ	MX	MY	MZ
DEADWEIGHT-1	0	-0.008	-0.001		1200				
THERMAL-1	-0.027	2.26	-0.022						
THERMAL-2	-0.018	1.03	-0.015						
SEISMIC-OBE	±.004	±.002	±.002						
SEISMIC-OBE	±.006	±.005	±.007						
BLOWDOWN-SRV									
BLOWDOWN-PORV	±.004	+0.005 -0.006	±.004 -0.006						

	TES COMBINED LOADS		
	FX	FY	FZ
NORMAL/UPSET		+1200	
EMERGENCY		+1200	

	SUPPORT DRAWING LOADS		
	FX	FY	FZ
DESIGN (+)		1200	
DESIGN (-)			

UNITS: DISPLACEMENTS : INCHES
 FORCES : POUNDS
 MOMENTS : INCH-POUNDS

TES COMBINED LOADS ARE _____
 THAN THE LOAD SHOWN
 ON THE SUPPORT DRAWING



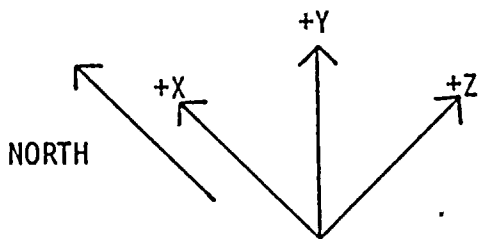
SUPPORT LOAD SUMMARY SHEET

DONALD C. COOK
 UNIT #1
 PROJECT 5364

BY: DMB DATE: 5-11-83

CHECKED BY: DMB DATE: 5/26/83

GLOBAL COORDINATE SYSTEM



MARK NUMBER 1-GRC-R-591

NODE NUMBER 83

DESIGN LOADINGS									
	DISPLACEMENTS			FORCES			MOMENTS		
	X	Y	Z	FX	FY	FZ	MX	MY	MZ
DEADWEIGHT-1	0	-0.007	0	-60		+50			
THERMAL-1	0	2.30	0	-210		-140			
THERMAL-2	0	1.74	0	-150		-10			
SEISMIC-OBE	0	±.002	0	±276		±218			
SEISMIC-DBE	0	±.003	0	±468		±364			
BLOWDOWN-SRV									
BLOWDOWN-PORV	0	+ .006 - .005	0	+ 354		+ 331			

	TES COMBINED LOADS		
	FX	FY	FZ
NORMAL/UPSET	+239 -659		+436 -356
EMERGENCY	+408 -738		+414 -454

	SUPPORT DRAWING LOADS		
	FX	FY	FZ
DESIGN (+)	2257		5339
DESIGN (-)	1935		5348

UNITS: DISPLACEMENTS : INCHES
 FORCES : POUNDS
 MOMENTS : INCH-POUNDS

TES COMBINED LOADS ARE LESS
 THAN THE LOAD SHOWN
 ON THE SUPPORT DRAWING



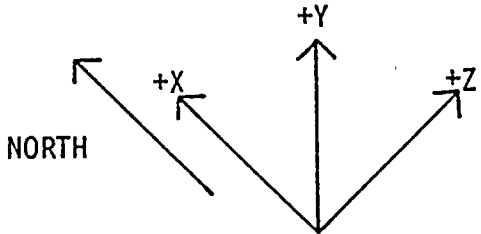
SUPPORT LOAD SUMMARY SHEET

DONALD C. COOK
 UNIT #1
 PROJECT 5364

BY: DWB DATE: 5-11-83

CHECKED BY: SMD DATE: 5/26/83

GLOBAL COORDINATE SYSTEM



MARK NUMBER 1-GRC-S-592

NODE NUMBER 1140

	DESIGN LOADINGS								
	DISPLACEMENTS			FORCES			MOMENTS		
	X	Y	Z	FX	FY	FZ	MX	MY	MZ
DEADWEIGHT-1	-0.034	.032	-0.076						
THERMAL-1	-0.185	2.82	.185						
THERMAL-2	-0.207	2.83	.161						
SEISMIC-OBE	±0.228	0	±0.055		±1280				
SEISMIC-DBE	±0.397	0	±0.091		±2122				
BLOWDOWN-SRV									
BLOWDOWN-PORV	±0.003 -0.002	0	±0.002		±142				

	TES COMBINED LOADS		
	FX	FY	FZ
NORMAL/UPSET		±1280	
EMERGENCY		±2122	

	SUPPORT DRAWING LOADS		
	FX	FY	FZ
DESIGN (+)		20531	
DESIGN (-)		20531	

UNITS: DISPLACEMENTS : INCHES
 FORCES : POUNDS
 MOMENTS : INCH-POUNDS

TES COMBINED LOADS ARE LESS
 THAN THE LOAD SHOWN
 ON THE SUPPORT DRAWING

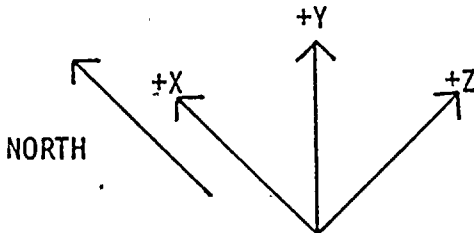


SUPPORT LOAD SUMMARY SHEET

DONALD C. COOK
 UNIT #1
 PROJECT 5364

BY: AMB DATE: 5-25-83
 CHECKED BY: SMB DATE: 5/26/83

GLOBAL COORDINATE SYSTEM



MARK NUMBER 1-GRC-C-593
 NODE NUMBER 111

	DESIGN LOADINGS								
	DISPLACEMENTS			FORCES			MOMENTS		
	X	Y	Z	FX	FY	FZ	MX	MY	MZ
DEADWEIGHT-1	-0.002	0.068	-0.036		1067				
THERMAL-1	-1.113	2.81	0.144						
THERMAL-2	-1.182	2.78	0.185						
SEISMIC-OBE	±.171	±.016	±.042						
SEISMIC-DBE	±.248	±.028	±.070						
BLOWDOWN-SRV									
BLOWDOWN-PORV	±.006	±.001	±.004 - .005						

	TES COMBINED LOADS		
	FX	FY	FZ
NORMAL/UPSET		+1067	
EMERGENCY		+1067	

	SUPPORT DRAWING LOADS		
	FX	FY	FZ
DESIGN (+)		1067	
DESIGN (-)			

UNITS: DISPLACEMENTS : INCHES
 FORCES : POUNDS
 MOMENTS : INCH-POUNDS

TES COMBINED LOADS ARE _____
 THAN THE LOAD SHOWN
 ON THE SUPPORT DRAWING

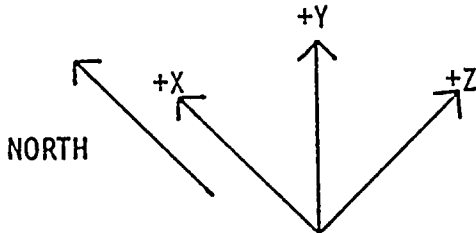
SUPPORT LOAD SUMMARY SHEET

DONALD C. COOK
 UNIT #1
 PROJECT 5364

BY: AWB DATE: 5-11-83

CHECKED BY: SMD DATE: 5/26/83

GLOBAL COORDINATE SYSTEM



MARK NUMBER 1-GRC-S-59A

NODE NUMBER 163

	DESIGN LOADINGS								
	DISPLACEMENTS			FORCES			MOMENTS		
	X	Y	Z	FX	FY	FZ	MX	MY	MZ
DEADWEIGHT-1	-0.076	.030	-0.006						
THERMAL-1	.178	2.78	.218						
THERMAL-2	.110	2.81	.249						
SEISMIC-OBE	±.056	0	±.202		±1131				
SEISMIC-DBE	±.097	0	±.350		±1872				
BLOWDOWN-SRV									
BLOWDOWN-PORV	±.001	0	±.002		±162				

	TES COMBINED LOADS		
	FX	FY	FZ
NORMAL/UPSET		±1143	
EMERGENCY		±1872	

	SUPPORT DRAWING LOADS		
	FX	FY	FZ
DESIGN (+)		19734	
DESIGN (-)		19734	

UNITS: DISPLACEMENTS : INCHES
 FORCES : POUNDS
 MOMENTS : INCH-POUNDS

TES COMBINED LOADS ARE LESS
 THAN THE LOAD SHOWN
 ON THE SUPPORT DRAWING



Technical Report
 TR-5364-1
 Revision 0

6-83

TELEDYNE
ENGINEERING SERVICES

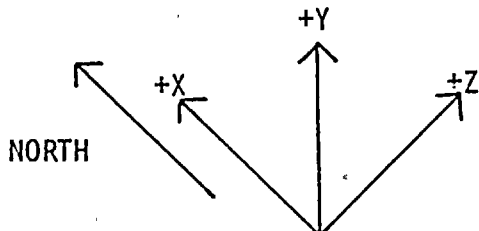
SUPPORT LOAD SUMMARY SHEET

DONALD C. COOK
 UNIT #1
 PROJECT 5364

BY: DMS DATE: 5-25-83

CHECKED BY: DMS DATE: 5/26/83

GLOBAL COORDINATE SYSTEM



MARK NUMBER 1-GRC-C-595

NODE NUMBER 159

	DESIGN LOADINGS								
	DISPLACEMENTS			FORCES			MOMENTS		
	X	Y	Z	FX	FY	FZ	MX	MY	MZ
DEADWEIGHT-1	.050	.062	.008		1074				
THERMAL-1	.167	2.76	.159						
THERMAL-2	.123	2.76	.241						
SEISMIC-OBE	±.046	±.014	±.175						
SEISMIC-DBE	±.079	±.023	±.303						
BLOWDOWN-SRV									
BLOWDOWN-PORV	±.001	±.001	±.003						

	TES COMBINED LOADS		
	FX	FY	FZ
NORMAL/UPSET		+1074	
EMERGENCY		+1074	

	SUPPORT DRAWING LOADS		
	FX	FY	FZ
DESIGN (+)		1074	
DESIGN (-)			

UNITS: DISPLACEMENTS : INCHES
 FORCES : POUNDS
 MOMENTS : INCH-POUNDS

TES COMBINED LOADS ARE
 THAN THE LOAD SHOWN
 ON THE SUPPORT DRAWING

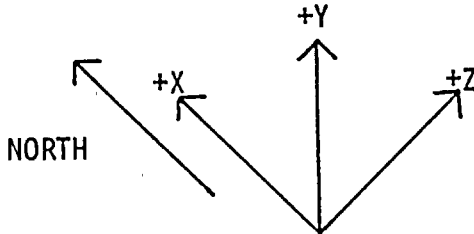
SUPPORT LOAD SUMMARY SHEET

DONALD C. COOK
UNIT #1
PROJECT 5364

BY: AKB DATE: 5-11-83

CHECKED BY: SMD DATE: 5/26/83

GLOBAL COORDINATE SYSTEM



MARK NUMBER 1-GRC-S-596

NODE NUMBER 2230

	DESIGN LOADINGS								
	DISPLACEMENTS			FORCES			MOMENTS		
	FX	FY	FZ	FX	FY	FZ	MX	MY	MZ
DEADWEIGHT-1	-0.009	.015	.05						
THERMAL-1	.391	2.66	-.271						
THERMAL-2	.323	2.75	-.105						
SEISMIC-OBE	±.127	0	±.099		±1052				
SEISMIC-DBE	±.217	0	±.168		±1734				
BLOWDOWN-SRV									
BLOWDOWN-PORV	±.003	0	±.003		± 206				

	TES COMBINED LOADS		
	FX	FY	FZ
NORMAL/UPSET		±1072	
EMERGENCY		±1734	

	SUPPORT DRAWING LOADS		
	FX	FY	FZ
DESIGN (+)		11811	
DESIGN (-)		11811	

UNITS: DISPLACEMENTS : INCHES
FORCES : POUNDS
MOMENTS : INCH-POUNDS

TES COMBINED LOADS ARE LESS
THAN THE LOAD SHOWN
ON THE SUPPORT DRAWING



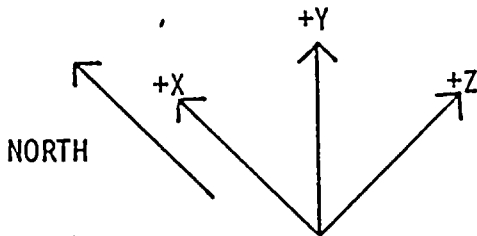
SUPPORT LOAD SUMMARY SHEET

DONALD C. COOK
 UNIT #1
 PROJECT 5364

BY: DMB DATE: 5-25-83

CHECKED BY: Dmb DATE: 5/26/83

GLOBAL COORDINATE SYSTEM



MARK NUMBER 1-GRC-C-597

NODE NUMBER 221

	DESIGN LOADINGS								
	DISPLACEMENTS			FORCES			MOMENTS		
	X	Y	Z	FX	FY	FZ	MX	MY	MZ
DEADWEIGHT-1	- .001	.036	.027		1025				
THERMAL-1	.283	2.57	-.216						
THERMAL-2	.253	2.63	-.078						
SEISMIC-OBE	±.094	±.013	±.071						
SEISMIC-DBE	±.160	±.022	±.122						
BLOWDOWN-SRV									
BLOWDOWN-PORV	+ .005 - .006	+ .002 - .002	+ .003 - .002						

	TES COMBINED LOADS		
	FX	FY	FZ
NORMAL/UPSET		+1025	
EMERGENCY		+1025	

	SUPPORT DRAWING LOADS		
	FX	FY	FZ
DESIGN (+)		1025	
DESIGN (-)			

UNITS: DISPLACEMENTS : INCHES
 FORCES : POUNDS
 MOMENTS : INCH-POUNDS

TES COMBINED LOADS ARE _____
 THAN THE LOAD SHOWN
 ON THE SUPPORT DRAWING

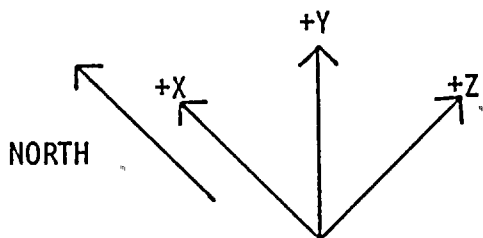
SUPPORT LOAD SUMMARY SHEET

DONALD C. COOK
 UNIT #1
 PROJECT 5364

BY: DMS DATE: 5-20-83

CHECKED BY: SMD DATE: 5/26/83

GLOBAL COORDINATE SYSTEM



MARK NUMBER 1-GRC-S-598

NODE NUMBER 108

	DESIGN LOADINGS								
	DISPLACEMENTS			FORCES			MOMENTS		
	X	Y	Z	FX	FY	FZ	MX	MY	MZ
DEADWEIGHT-1	.053	.049	.086						
THERMAL-1	.035	2.79	.105						
THERMAL-2	-.202	2.59	.193						
SEISMIC-OBE	±.021	±.006	±.017	± 37		± 46			
SEISMIC-DBE	±.034	±.010	±.027	± 61		± 76			
BLOWDOWN-SRV									
BLOWDOWN-PORV	±.022	±.001	±.017 -.018	± 58		± 72			

	TES COMBINED LOADS		
	FX	FY	FZ
NORMAL/UPSET	± 69		± 85
EMERGENCY	± 61		± 76

	SUPPORT DRAWING LOADS		
	FX	FY	FZ
DESIGN (+)	2763		4152
DESIGN (-)	2763		4152

UNITS: DISPLACEMENTS : INCHES
 FORCES : POUNDS
 MOMENTS : INCH-POUNDS

TES COMBINED LOADS ARE LESS
 THAN THE LOAD SHOWN
 ON THE SUPPORT DRAWING

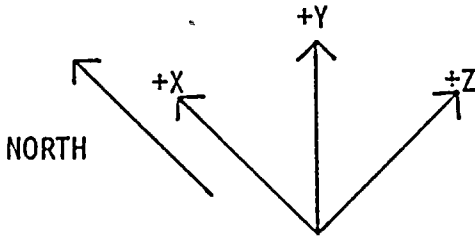
SUPPORT LOAD SUMMARY SHEET

DONALD C. COOK
 UNIT #1
 PROJECT 5364

BY: DMB DATE: 5-20-83

CHECKED BY: DMB DATE: 5/26/83

GLOBAL COORDINATE SYSTEM



MARK NUMBER 1-GRC-9-599

NODE NUMBER 156

	DESIGN LOADINGS								
	DISPLACEMENTS			FORCES			MOMENTS		
	X	Y	Z	FX	FY	FZ	MX	MY	MZ
DEADWEIGHT-1	.052	.045	.014						
THERMAL-1	.155	2.75	.066						
THERMAL-2	-.014	2.60	.274						
SEISMIC-OBE	±.001	±.009	±.008	± 97	± 17	± 12			
SEISMIC-DBE	±.002	±.016	±.015	± 166	± 29	± 20			
BLOWDOWN-SRV									
BLOWDOWN-PORV	±.001	0	±.007 -.008	± 97	± 17	± 12			

	TES COMBINED LOADS		
	FX	FY	FZ
NORMAL/UPSET	± 137	± 24	± 17
EMERGENCY	± 166	± 29	± 20

	SUPPORT DRAWING LOADS		
	FX	FY	FZ
DESIGN (+)	3610		545
DESIGN (-)	3610		545

UNITS: DISPLACEMENTS : INCHES
 FORCES : POUNDS
 MOMENTS : INCH-POUNDS

TES COMBINED LOADS ARE LESS
 THAN THE LOAD SHOWN
 ON THE SUPPORT DRAWING

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TELEDYNE
ENGINEERING SERVICES

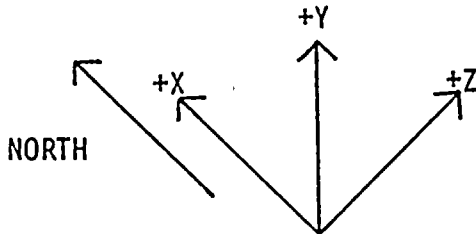
SUPPORT LOAD SUMMARY SHEET

DONALD C. COOK
 UNIT #1
 PROJECT 5364

BY: DMB DATE: 5-11-83

CHECKED BY: Dmd DATE: 5/26/83

GLOBAL COORDINATE SYSTEM



MARK NUMBER 1-GRC-R-600

NODE NUMBER 195

	DESIGN LOADINGS								
	DISPLACEMENTS			FORCES			MOMENTS		
	X	Y	Z	FX	FY	FZ	MX	MY	MZ
DEADWEIGHT-1	0	-0.003	0	+100		-120			
THERMAL-1	0	2.34	0	-1110		+1830			
THERMAL-2	0	2.30	0	-720		+1470			
SEISMIC-OBE	0	+0.001	0	+376		+269			
SEISMIC-DBE	0	+0.002	0	+599		+436			
BLOWDOWN-SRV									
BLOWDOWN-PORV	0	+0.002	0	+458		+718			

	TES COMBINED LOADS		
	FX	FY	FZ
NORMAL/UPSET	+476 -1386		+2117 -389
EMERGENCY	+699 -1609		+2146 -556

	SUPPORT DRAWING LOADS		
	FX	FY	FZ
DESIGN (+)	7047		19475
DESIGN (-)	6179		20488

UNITS: DISPLACEMENTS : INCHES
 FORCES : POUNDS
 MOMENTS : INCH-POUNDS

TES COMBINED LOADS ARE LESS
 THAN THE LOAD SHOWN
 ON THE SUPPORT DRAWING

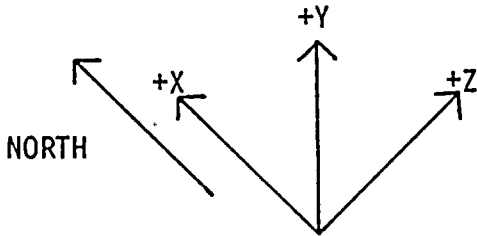
SUPPORT LOAD SUMMARY SHEET

DONALD C. COOK
 UNIT #1
 PROJECT 5364

BY: AKB DATE: 5-11-83

CHECKED BY: Dmd DATE: 5/26/83

GLOBAL COORDINATE SYSTEM



MARK NUMBER 1-GRC-R-601

NODE NUMBER 280

	DESIGN LOADINGS								
	DISPLACEMENTS			FORCES			MOMENTS		
	X	Y	Z	FX	FY	FZ	MX	MY	MZ
DEADWEIGHT-1	0	-0.003	0	-320		+720			
THERMAL-1	0	2.36	0	+300		-1050			
THERMAL-2	0	2.63	0	+1320		-2700			
SEISMIC-OBE	0	±.001	0	±642		±308			
SEISMIC-DBE	0	±.001	0	±983		±424			
BLOWDOWN-SRV									
BLOWDOWN-PORV	0	±.002	0	±698		±265			

	TES COMBINED LOADS		
	FX	FY	FZ
NORMAL/UPSET	+1948 -962		+1028 -2386
EMERGENCY	+963 -1303		+1144 -754

	SUPPORT DRAWING LOADS		
	FX	FY	FZ
DESIGN (+)	1223		1106
DESIGN (-)	8757		2740

UNITS: DISPLACEMENTS : INCHES
 FORCES : POUNDS
 MOMENTS : INCH-POUNDS

TES COMBINED LOADS ARE LESS *
 THAN THE LOAD SHOWN
 ON THE SUPPORT DRAWING

* EXCEPT +FX LOAD

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TELEDYNE
ENGINEERING SERVICES

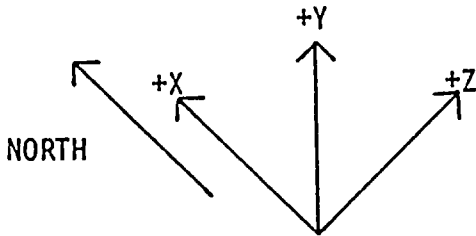
SUPPORT LOAD SUMMARY SHEET

DONALD C. COOK
 UNIT #1
 PROJECT 5364

BY: DMB DATE: 5-25-83

CHECKED BY: DMB DATE: 5/26/83

GLOBAL COORDINATE SYSTEM



MARK NUMBER 1-GRC-C-602

NODE NUMBER 668

	DESIGN LOADINGS								
	DISPLACEMENTS			FORCES			MOMENTS		
	X	Y	Z	FX	FY	FZ	MX	MY	MZ
DEADWEIGHT-1	.104	.001	-.043		1159				
THERMAL-1	.422	3.19	-.176						
THERMAL-2	.311	3.24	-.172						
SEISMIC-OBE	±.141	±.047	±.088						
SEISMIC-DBE	±.209	±.072	±.128						
BLOWDOWN-SRV									
BLOWDOWN-PORV	+ .099 - .127	+ .059 - .040	+ .085 - .062						

	TES COMBINED LOADS		
	FX	FY	FZ
NORMAL/UPSET		+1159	
EMERGENCY		+1159	

	SUPPORT DRAWING LOADS		
	FX	FY	FZ
DESIGN (+)		1159	
DESIGN (-)			

UNITS: DISPLACEMENTS : INCHES
 FORCES : POUNDS
 MOMENTS : INCH-POUNDS

TES COMBINED LOADS ARE _____
 THAN THE LOAD SHOWN
 ON THE SUPPORT DRAWING



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TELEDYNE
ENGINEERING SERVICES

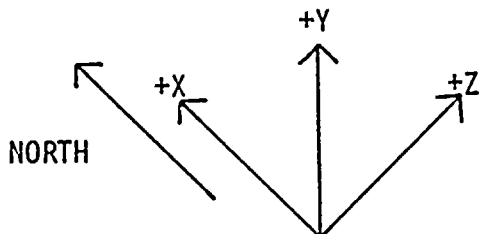
SUPPORT LOAD SUMMARY SHEET

DONALD C. COOK
 UNIT #1
 PROJECT 5364

BY: AMB DATE: 5-20-83

CHECKED BY: DMD DATE: 5/26/83

GLOBAL COORDINATE SYSTEM



MARK NUMBER 1-GRC-R-603

NODE NUMBER 585

	DESIGN LOADINGS								
	DISPLACEMENTS			FORCES			MOMENTS		
	X	Y	Z	FX	FY	FZ	MX	MY	MZ
DEADWEIGHT-1	.103	.211	-.042	-121		-298			
THERMAL-1	.163	3.33	-.067	-173		-428			
THERMAL-2	.056	3.37	-.023	-270		-650			
SEISMIC-OBE	±.141	±.077	±.057	±414		±1519			
SEISMIC-DBE	±.208	±.106	±.085	±855		±2117			
BLOWDOWN-SRV									
BLOWDOWN-PORV	+ .099 - .128	+ .045 - .044	+ .052 - .040	± 511		± 1266			

	TES COMBINED LOADS		
	FX	FY	FZ
NORMAL/UPSET	+493 -1190		+1221 -2925
EMERGENCY	+734 -1149		+1819 -2843

	SUPPORT DRAWING LOADS		
	FX	FY	FZ
DESIGN (+)	1833		4540
DESIGN (-)	1560		3863

UNITS: DISPLACEMENTS : INCHES
 FORCES : POUNDS
 MOMENTS : INCH-POUNDS

TES COMBINED LOADS ARE LESS
 THAN THE LOAD SHOWN
 ON THE SUPPORT DRAWING

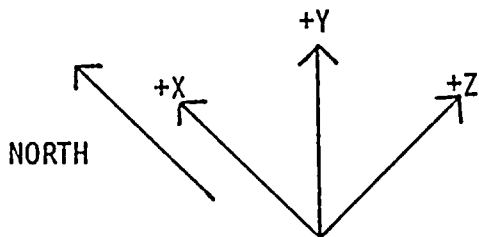
SUPPORT LOAD SUMMARY SHEET

DONALD C. COOK
 UNIT #1
 PROJECT 5364

BY: AKS DATE: 5-11-83

CHECKED BY: Smb DATE: 5/26/83

GLOBAL COORDINATE SYSTEM



MARK NUMBER 1-GRC-S-604

NODE NUMBER 450

	DESIGN LOADINGS								
	DISPLACEMENTS			FORCES			MOMENTS		
	X	Y	Z	FX	FY	FZ	MX	MY	MZ
DEADWEIGHT-1	.052	.816	-.075						
THERMAL-1	.120	3.36	.334						
THERMAL-2	.106	3.52	.445						
SEISMIC-OBE	±.093	0	±.202		±653				
SEISMIC-DBE	±.127	0	±.293		±952				
BLOWDOWN-SRV									
BLOWDOWN-PORV	+0.039 -0.058	0	+0.150 -0.147		±868				

	TES COMBINED LOADS		
	FX	FY	FZ
NORMAL/UPSET		±1086	
EMERGENCY		±952	

	SUPPORT DRAWING LOADS		
	FX	FY	FZ
DESIGN (+)		1629	
DESIGN (-)		1629	

UNITS: DISPLACEMENTS : INCHES
 FORCES : POUNDS
 MOMENTS : INCH-POUNDS

TES COMBINED LOADS ARE LESS
 THAN THE LOAD SHOWN
 ON THE SUPPORT DRAWING



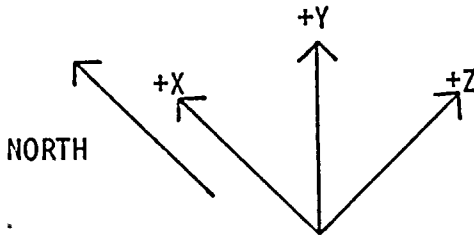
SUPPORT LOAD SUMMARY SHEET

DONALD C. COOK
UNIT #1
PROJECT 5364

BY: AMS DATE: 5-20-83

CHECKED BY: SMS DATE: 5/26/83

GLOBAL COORDINATE SYSTEM



MARK NUMBER 1-GRC-R-605

NODE NUMBER 465

	DESIGN LOADINGS								
	DISPLACEMENTS			FORCES			MOMENTS		
	X	Y	Z	FX	FY	FZ	MX	MY	MZ
DEADWEIGHT-1	-039	1.22	-053	+673		-507			
THERMAL-1	.402	3.20	.534	-414		+312			
THERMAL-2	.470	3.59	.630	-530		+400			
SEISMIC-OBE	±.138	±.362	±.182	±680		±512			
SEISMIC-DBE	±.199	±.487	±.263	±1021		±769			
BLOWDOWN-SRV									
BLOWDOWN-PORV	+ .100 - .105	+ .138 - .167	+ .132 - .137	+ 1217		+ 918			

	TES COMBINED LOADS		
	FX	FY	FZ
NORMAL/UPSET	+1537 -1251		+944 -1158
EMERGENCY	+1694 -762		+574 -1276

	SUPPORT DRAWING LOADS		
	FX	FY	FZ
DESIGN (+)	3150		1635
DESIGN (-)	2286		2337

UNITS: DISPLACEMENTS : INCHES
FORCES : POUNDS
MOMENTS : INCH-POUNDS

TES COMBINED LOADS ARE LESS
THAN THE LOAD SHOWN
ON THE SUPPORT DRAWING



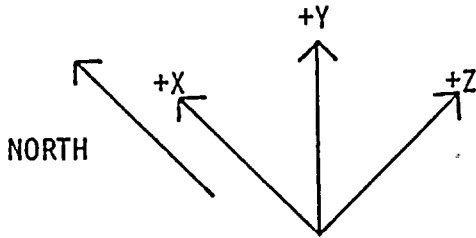
SUPPORT LOAD SUMMARY SHEET

DONALD C. COOK
 UNIT #1
 PROJECT 5364

BY: DWB DATE: 5-25-83

CHECKED BY: Smb DATE: 5/26/83

GLOBAL COORDINATE SYSTEM



MARK NUMBER 1-GRC-C-606

NODE NUMBER 485

DESIGN LOADINGS									
	DISPLACEMENTS			FORCES			MOMENTS		
	X	Y	Z	FX	FY	FZ	MX	MY	MZ
DEADWEIGHT-1	.043	1.25	-.050		811				
NORMAL-1	.608	3.02	.514						
THERMAL-2	.699	3.57	.571						
SEISMIC-OBE	±.167	±.523	±.160						
SEISMIC-DBE	±.243	±.704	±.216						
BLOWDOWN-SRV									
BLOWDOWN-PORV	+.123 -.131	+.194 -.231	+.101 -.104						

	TES COMBINED LOADS		
	FX	FY	FZ
NORMAL/UPSET		+811	
EMERGENCY		+811	

	SUPPORT DRAWING LOADS		
	FX	FY	FZ
DESIGN (+)		811	
DESIGN (-)			

UNITS: DISPLACEMENTS : INCHES
 FORCES : POUNDS
 MOMENTS : INCH-POUNDS

TES COMBINED LOADS ARE
 THAN THE LOAD SHOWN
 ON THE SUPPORT DRAWING

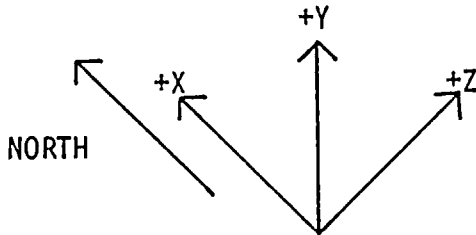
SUPPORT LOAD SUMMARY SHEET

DONALD C. COOK
 UNIT #1
 PROJECT 5364

BY: DMB DATE: 5-25-83

CHECKED BY: Dmb DATE: 5/26/83

GLOBAL COORDINATE SYSTEM



MARK NUMBER 1-GRC-C-607

NODE NUMBER 529

	DESIGN LOADINGS								
	DISPLACEMENTS			FORCES			MOMENTS		
	X	Y	Z	FX	FY	FZ	MX	MY	MZ
DEADWEIGHT-1	-0.065	.465	-.105		658				
THERMAL-1	.819	2.54	.039						
THERMAL-2	.879	3.28	.006						
SEISMIC-OBE	±.122	±.045	±.122						
SEISMIC-DBE	±.177	±.085	±.165						
BLOWDOWN-SRV									
BLOWDOWN-PORV	+0.085 -0.098	+0.028 -0.031	+0.025 -0.024						

	TES COMBINED LOADS		
	FX	FY	FZ
NORMAL/UPSET		+658	
EMERGENCY		+658	

	SUPPORT DRAWING LOADS		
	FX	FY	FZ
DESIGN (+)		658	
DESIGN (-)			

UNITS: DISPLACEMENTS : INCHES
 FORCES : POUNDS
 MOMENTS : INCH-POUNDS

TES COMBINED LOADS ARE _____
 THAN THE LOAD SHOWN
 ON THE SUPPORT DRAWING

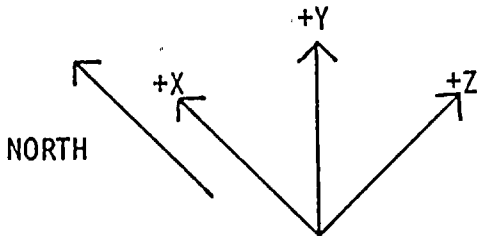
SUPPORT LOAD SUMMARY SHEET

DONALD C. COOK
 UNIT #1
 PROJECT 5364

BY: DMS DATE: 5-11-83

CHECKED BY: DMS DATE: 5/26/83

GLOBAL COORDINATE SYSTEM



MARK NUMBER 1-GRC-S-608

NODE NUMBER 534

	DESIGN LOADINGS								
	DISPLACEMENTS			FORCES			MOMENTS		
	X	Y	Z	FX	FY	FZ	MX	MY	MZ
DEADWEIGHT-1	-0.093	.373	-0.064						
THERMAL-1	.758	2.46	-0.010						
THERMAL-2	.863	3.21	-0.046						
SEISMIC-OBE	±.110	0	±.064		±639.				
SEISMIC-DBE	±.160	0	±.087		±876.				
BLOWDOWN-SRV									
BLOWDOWN-PORV	±.084 -0.087	0	±.018 -0.020		±1025				

	TES COMBINED LOADS		
	FX	FY	FZ
NORMAL/UPSET		±1208	
EMERGENCY		±876	

	SUPPORT DRAWING LOADS		
	FX	FY	FZ
DESIGN (+)		1288	
DESIGN (-)		1288	

UNITS: DISPLACEMENTS : INCHES
 FORCES : POUNDS
 MOMENTS : INCH-POUNDS

TES COMBINED LOADS ARE LESS
 THAN THE LOAD SHOWN
 ON THE SUPPORT DRAWING



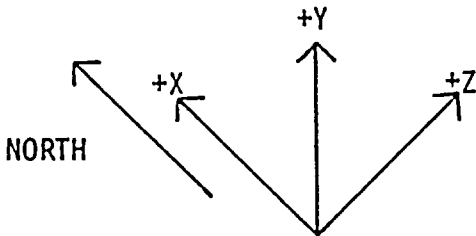
SUPPORT LOAD SUMMARY SHEET

DONALD C. COOK
 UNIT #1
 PROJECT 5364

BY: AKB DATE: 5-11-83

CHECKED BY: DMD DATE: 5/26/83

GLOBAL COORDINATE SYSTEM



MARK NUMBER 1-GRC-B-609

NODE NUMBER 536

	DESIGN LOADINGS								
	DISPLACEMENTS			FORCES			MOMENTS		
	X	Y	Z	FX	FY	FZ	MX	MY	MZ
DEADWEIGHT-1	-.129	.373	0			-280.			
THERMAL-1	.691	2.46	0			+ 10.			
THERMAL-2	.821	3.18	0			+ 900.			
SEISMIC-OBE	±.106	0	0			± 527.			
SEISMIC-DBE	±.154	0	0			± 711.			
BLOWDOWN-SRV									
BLOWDOWN-PORV	+ .087 - .079	+ .001 - .001	0			± 518			

	TES COMBINED LOADS		
	FX	FY	FZ
NORMAL/UPSET			+1359 - 307
EMERGENCY			+ 441 - 991

	SUPPORT DRAWING LOADS		
	FX	FY	FZ
DESIGN (+)			1916
DESIGN (-)			2543

UNITS: DISPLACEMENTS : INCHES
 FORCES : POUNDS
 MOMENTS : INCH-POUNDS

TES COMBINED LOADS ARE LESS
 THAN THE LOAD SHOWN
 ON THE SUPPORT DRAWING

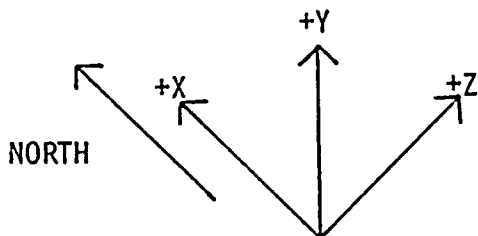
SUPPORT LOAD SUMMARY SHEET

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 PROJECT 5364

BY: DMB DATE: 5-25-83

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GLOBAL COORDINATE SYSTEM



MARK NUMBER 1-GRC-C-610

NODE NUMBER 620

	DESIGN LOADINGS								
	DISPLACEMENTS			FORCES			MOMENTS		
	X	Y	Z	FX	FY	FZ	MX	MY	MZ
DEADWEIGHT-1	.098	.404	-.057		783				
NORMAL-1	.258	3.08	.376						
THERMAL-2	.104	3.37	.310						
SEISMIC-OBE	±.055	±.027	±.151						
SEISMIC-DBE	±.088	±.041	±.219						
BLOWDOWN-SRV									
BLOWDOWN-PORV	+ .054 - .056	+ .023 - .029	+ .136 - .094						

	TES COMBINED LOADS		
	FX	FY	FZ
NORMAL/UPSET		+783	
EMERGENCY		+783	

	SUPPORT DRAWING LOADS		
	FX	FY	FZ
DESIGN (+)		783	
DESIGN (-)			

UNITS: DISPLACEMENTS : INCHES
 FORCES : POUNDS
 MOMENTS : INCH-POUNDS

TES COMBINED LOADS ARE _____
 THAN THE LOAD SHOWN
 ON THE SUPPORT DRAWING



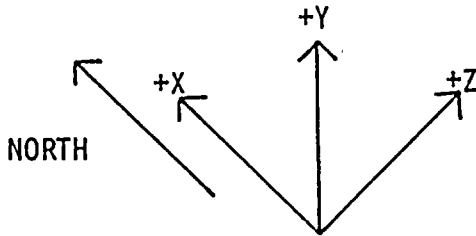
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 PROJECT 5364

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GLOBAL COORDINATE SYSTEM



MARK NUMBER 1-GFC-C-611

NODE NUMBER 431

	DESIGN LOADINGS								
	DISPLACEMENTS			FORCES			MOMENTS		
	X	Y	Z	FX	FY	FZ	MX	MY	MZ
DEADWEIGHT-1	.063	.693	-.066		930				
THERMAL-1	.137	3.34	.250						
THERMAL-2	.108	3.48	.344						
SEISMIC-OBE	±.081	±.017	±.173						
SEISMIC-OBE	±.111	±.027	±.251						
BLOWDOWN-SRV									
BLOWDOWN-PORV	+ .055 - .042	+ .015 - .017	+ .128 - .127						

	TES COMBINED LOADS		
	FX	FY	FZ
NORMAL/UPSET		+930	
EMERGENCY		+930	

	SUPPORT DRAWING LOADS		
	FX	FY	FZ
DESIGN (+)		930	
DESIGN (-)			

UNITS: DISPLACEMENTS : INCHES
 FORCES : POUNDS
 MOMENTS : INCH-POUNDS

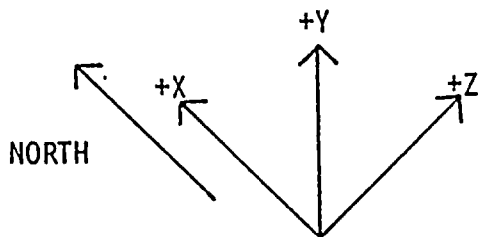
TES COMBINED LOADS ARE _____
 THAN THE LOAD SHOWN
 ON THE SUPPORT DRAWING

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GLOBAL COORDINATE SYSTEM



MARK NUMBER 1-GRC-C-612
 NODE NUMBER 382

	DESIGN LOADINGS								
	DISPLACEMENTS			FORCES			MOMENTS		
	X	Y	Z	FX	FY	FZ	MX	MY	MZ
DEADWEIGHT-1	.113	.918	-.085		638				
THERMAL-1	.569	3.08	.425						
THERMAL-2	.698	3.46	.455						
SEISMIC-OBE	±.219	±.650	±.119						
SEISMIC-DBE	±.316	±.874	±.172						
BLOWDOWN-SRV									
BLOWDOWN-PORV	+ .157 - .124	+ .125 - .093	+ .073 - .092						

	TES COMBINED LOADS		
	FX	FY	FZ
NORMAL/UPSET		+638	
EMERGENCY		+638	

	SUPPORT DRAWING LOADS		
	FX	FY	FZ
DESIGN (+)		638	
DESIGN (-)			

UNITS: DISPLACEMENTS : INCHES
 FORCES : POUNDS
 MOMENTS : INCH-POUNDS

TES COMBINED LOADS ARE _____
 THAN THE LOAD SHOWN
 ON THE SUPPORT DRAWING



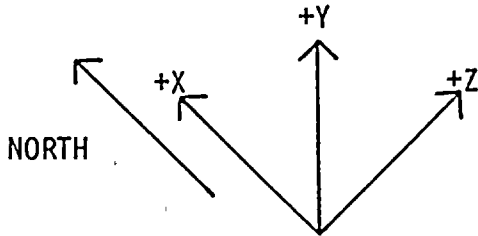
SUPPORT LOAD SUMMARY SHEET

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GLOBAL COORDINATE SYSTEM



MARK NUMBER 1-GRC-R-613

NODE NUMBER 360

	DESIGN LOADINGS								
	DISPLACEMENTS			FORCES			MOMENTS		
	X	Y	Z	FX	FY	FZ	MX	MY	MZ
DEADWEIGHT-1	.049	.928	.039	-136		+171			
THERMAL-1	.500	3.08	.397	-78		+97			
THERMAL-2	.638	3.40	.508	-220		+280			
SEISMIC-OBE	±.204	±.625	±.162	±276	"	±347			
SEISMIC-DBE	±.292	±.843	±.232	±407	"	±512			
BLOWDOWN-SRV									
BLOWDOWN-PORV	+ .152 - .123	+ .133 - .087	+ .120 - .048	+ 296 - 296		+ 372 - 372			

	TES COMBINED LOADS		
	FX	FY	FZ
NORMAL/UPSET	+140 -761		+960 -176
EMERGENCY	+271 -621		+780 -341

	SUPPORT DRAWING LOADS		
	FX	FY	FZ
DESIGN (+)	787		658
DESIGN (-)	772		670

UNITS: DISPLACEMENTS : INCHES
FORCES : POUNDS
MOMENTS : INCH-POUNDS

TES COMBINED LOADS ARE LESS *
THAN THE LOAD SHOWN
ON THE SUPPORT DRAWING

* EXCEPT + FZ LOAD

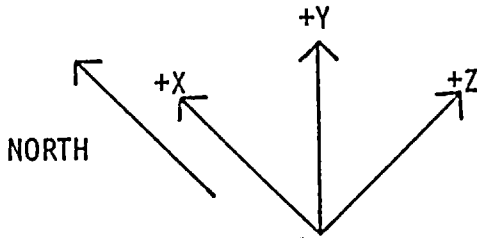
SUPPORT LOAD SUMMARY SHEET

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GLOBAL COORDINATE SYSTEM



MARK NUMBER 1-GRC-S-614

NODE NUMBER 325

	DESIGN LOADINGS								
	DISPLACEMENTS			FORCES			MOMENTS		
	X	Y	Z	FX	FY	FZ	MX	MY	MZ
DEADWEIGHT-1	.011	.380	.041						
THERMAL-1	.181	3.02	.423						
THERMAL-2	-.008	3.28	.341						
SEISMIC-OBE	±.027	±.041	±.192	± 99	± 368	± 73			
SEISMIC-DBE	±.045	±.058	±.277	± 156	± 580	± 115			
BLOWDOWN-SRV									
BLOWDOWN-PORV	+ .042 - .033	+ .026 - .030	+ .158 - .110	± 295	± 1101	± 218			

	TES COMBINED LOADS		
	FX	FY	FZ
NORMAL/UPSET	± 311	± 1161	± 230
EMERGENCY	± 156	± 580	± 115

	SUPPORT DRAWING LOADS		
	FX	FY	FZ
DESIGN (+)	288	953	104
DESIGN (-)	288	953	104

UNITS: DISPLACEMENTS : INCHES
 FORCES : POUNDS
 MOMENTS : INCH-POUNDS

TES COMBINED LOADS ARE GREATER *
 THAN THE LOAD SHOWN
 ON THE SUPPORT DRAWING

* EXCEPT - FX LOAD AND
 - FY LOAD

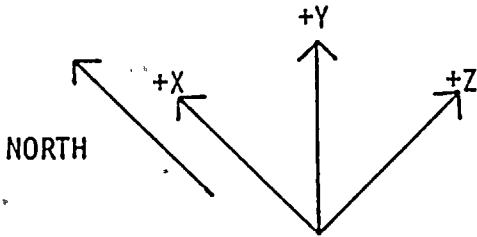
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GLOBAL COORDINATE SYSTEM



MARK NUMBER 1-GRC-C-615

NODE NUMBER 101

DESIGN LOADINGS									
	DISPLACEMENTS			FORCES			MOMENTS		
	X	Y	Z	FX	FY	FZ	MX	MY	MZ
DEADWEIGHT-1	.085	.065	.037		142				
NORMAL-1	.082	2.66	.036						
THERMAL-2	-.099	2.46	.277						
SEISMIC-OBE	±.018	±.023	±.004						
SEISMIC-DBE	±.029	±.038	±.007						
BLOWDOWN-SRV									
BLOWDOWN-PORV	±.015	±.010	±.004						

	TES COMBINED LOADS		
	FX	FY	FZ
NORMAL/UPSET		+142	
EMERGENCY		+142	

	SUPPORT DRAWING LOADS		
	FX	FY	FZ
DESIGN (+)		142	
DESIGN (-)			

UNITS: DISPLACEMENTS : INCHES
 FORCES : POUNDS
 MOMENTS : INCH-POUNDS

TES COMBINED LOADS ARE
 THAN THE LOAD SHOWN
 ON THE SUPPORT DRAWING



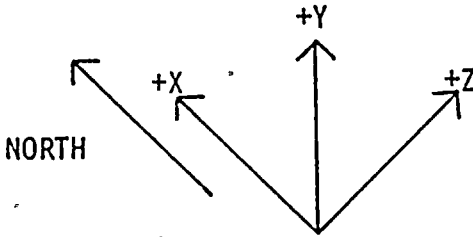
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GLOBAL COORDINATE SYSTEM



MARK NUMBER 1-GRC-R-616

NODE NUMBER 203

DESIGN LOADINGS									
	DISPLACEMENTS			FORCES			MOMENTS		
	X	Y	Z	FX	FY	FZ	MX	MY	MZ
DEADWEIGHT-1	.004	0	-.002		-1950.				
THERMAL-1	.013	2.35	-.003		+1451.				
THERMAL-2	-.016	2.35	.023		+1490.				
SEISMIC-OBE	±.003	0	±.002		±606.3				
SEISMIC-DBE	±.004	0	±.002		±946.9				
BLOWDOWN-SRV									
BLOWDOWN-PORV	±.003 -.004	0	±.002		±1070				

	TES COMBINED LOADS		
	FX	FY	FZ
NORMAL/UPSET		+ 770 - 2556	
EMERGENCY		+ 448 - 2897	

	SUPPORT DRAWING LOADS		
	FX	FY	FZ
DESIGN (+)		8315	
DESIGN (-)		3272	

UNITS: DISPLACEMENTS : INCHES
 FORCES : POUNDS
 MOMENTS : INCH-POUNDS

TES COMBINED LOADS ARE LESS
 THAN THE LOAD SHOWN
 ON THE SUPPORT DRAWING

6.3 Valve Accelerations

Valve accelerations were calculated for both the DBE seismic condition and the PORV transient shock condition. The horizontal allowable was taken as 3g and the vertical allowable as 2g based on the attachments to AEP letter dated September 16, 1982 from Mr. J. L. Williams of AEP to Mr. L. B. Semprucci of TES (Reference 12). For the seismic accelerations, the resultant horizontal acceleration was compared against the 3g allowable. Weights for valves NMO-151, 152 and 153 were taken as 352 pounds, in determining the seismic acceleration, since this is the value used in the seismic analysis, see Section 5.0.

For the PORV transient shock accelerations, the updated valve weight of 400 pounds was used in both the analysis and the acceleration calculations. It should be noted that valves NRV-151, NRV-152, NMO-151, NMO-152 and NMO-153 all fail the vertical acceleration criteria of 2g (see Section 2.0).



6.3.1 DBE Seismic Valve Accelerations

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BY: SMD DATE: 5/12/83

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VALVE NO.		NMJ-15			NMC-152			NMO-15-		
NODE NO.		651			411			415		
		ACCELERATION			ACCELERATION			ACCELERATION		
		A _x	A _y	A _z	A _x	A _y	A _z	A _x	A _y	A _z
SHOCK DIRECTION	X	.76	.41	.41	.73	.36	.56	.67	.73	.61
	Y	.17	.15	.15	.27	.25	.24	.24	.33	.34
	Z	.36	.27	.66	.70	.52	.69	.51	.67	.78
SRSS RESULTS	A _{xT}	.86 g			1.05 g			.89 g		
	A _{yT}	.51 g			.68 g			1.18 g		
	A _{zT}	.79 g			.92 g			1.05 g		
		ACCEL.	ALLOWABLE		ACCEL.	ALLOWABLE		ACCEL.	ALLOWABLE	
VERTICAL A _{vT}		.51 g	2 g		.68 g	2 g		1.18 g	2 g	
HORIZONTAL *		1.17 g	3 g		1.40 g	3 g		1.37 g	3 g	

* HORIZONTAL ACCELERATION = $\sqrt{(A_{xT})^2 + (A_{zT})^2}$

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VALVE NO.		SV-45A			SV-45B			SV-45C		
NODE NO.		2260			1660			1170		
		ACCELERATION			ACCELERATION			ACCELERATION		
		A _x	A _y	A _z	A _x	A _y	A _z	A _x	A _y	A _z
SHOCK DIRECTION	X	.99	.3	.33	.96	.16	.46	1.46	.10	.24
	Y	.05	.02	.05	.05	.02	.04	.04	.01	.04
	Z	.34	.15	.32	.51	.11	1.35	.29	.17	1.09
SRSS RESULTS	A _{xT}	1.30 g			1.09 g			1.49 g		
	A _{yT}	.20 g			.20 g			.20 g		
	A _{zT}	1.20 g			1.43 g			1.12 g		
		ACCEL.	ALLOWABLE		ACCEL.	ALLOWABLE		ACCEL.	ALLOWABLE	
VERTICAL A _{yT}		.20 g	2 g		.20 g	2 g		.20 g	2 g	
HORIZONTAL *		1.77 g	3 g		1.80 g	3 g		1.86 g	3 g	

* HORIZONTAL ACCELERATION = $\sqrt{(A_{xT})^2 + (A_{zT})^2}$

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VALVE NO.		NRV-15'			NRV-152			NRV-15'		
NODE NO.		631			391			516		
		ACCELERATION			ACCELERATION			ACCELERATION		
		A _x	A _y	A _z	A _x	A _y	A _z	A _x	A _y	A _z
SHOCK DIRECTION	X	.13	.32	.34	1.16	.60	.84	.97	.42	.67
	Y	.17	.14	.16	.46	.51	.35	.26	.14	.51
	Z	.54	.30	1.24	1.21	1.00	1.08	.51	.30	1.02
SRSS RESULTS	A _{xT}	1.09 g			1.74 g			1.13 g		
	A _{yT}	.46 g			1.27 g			.53 g		
	A ₋	1.30 g			1.41 g			1.32 g		
		ACCEL.	ALLOWABLE		ACCEL.	ALLOWABLE		ACCEL.	ALLOWABLE	
VERTICAL A _{yT}		.46 g	2 g		1.27 g	2 g		.53 g	2 g	
HORIZONTAL *		1.67 g	3 g		2.24 g	3 g		1.74 g	3 g	

* HORIZONTAL ACCELERATION = $\sqrt{(A_{xT})^2 + (A_{zT})^2}$

... 6.3.2. PORV Transient Shock Valve Accelerations



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VALVE ACCELERATIONS

VALVE	SV-45A			SV-45B		
NODE NUMBER	2260			1660		
VALVE WEIGHT	685 LBS			685 LBS		
DIRECTION	X	Y	Z	X	Y	Z
FORCE (LBS)	48	43	31	32	36	49
ACCELERATION	.07g	.06g	.05g	.05g	.05g	.07g
ALLOWABLE	3g	2g	3g	3g	2g	3g

VALVE	SV-45C					
NODE NUMBER	1170					
VALVE WEIGHT	685 LBS					
DIRECTION	X	Y	Z	X	Y	Z
FORCE (LBS)	47	33	41			
ACCELERATION	.07g	.05g	.06g			
ALLOWABLE	3g	2g	3g			



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VALVE ACCELERATIONS

VALVE	NMO-151			NMO-152		
NODE NUMBER	651			411		
VALVE WEIGHT	400 LBS			400 LBS		
DIRECTION	X	Y	Z	X	Y	Z
FORCE (LBS)	1116	999	835	783	960	899
ACCELERATION	2.79g	2.50g	2.09g	1.96g	2.40g	2.25g
ALLOWABLE	3g	2g	3g	3g	2g	3g

VALVE	NMO-153					
NODE NUMBER	496					
VALVE WEIGHT	400 LBS					
DIRECTION	X	Y	Z	X	Y	Z
FORCE (LBS)	1194	1083	399			
ACCELERATION	2.99g	2.71g	1.00g			
ALLOWABLE	3g	2g	3g			

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VALVE ACCELERATIONS

VALVE	NRV-151			NRV-152		
NODE NUMBER	631			391		
VALVE WEIGHT	480 LBS			480 LBS		
DIRECTION	X	Y	Z	X	Y	Z
FORCE (LBS)	658	1579	369	387	766	639
ACCELERATION	1.37g	3.29g	.77g	.81g	1.60g	1.33g
ALLOWABLE	3g	2g	3g	3g	2g	3g

VALVE	NRV-153					
NODE NUMBER	516					
VALVE WEIGHT	480 LBS					
DIRECTION	X	Y	Z	X	Y	Z
FORCE (LBS)	454	1269	307			
ACCELERATION	.95g	2.63g	.64g			
ALLOWABLE	3g	2g	3g			

6.4 Nozzle Loads

Forces and Moments for the four pressurizer nozzles and the quench tank nozzles are given in this section for each loading condition analyzed.

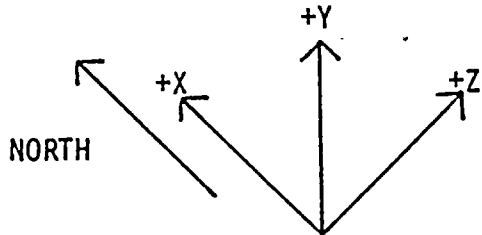
NOZZLE LOAD SUMMARY SHEET

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 PROJECT 5364

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GLOBAL COORDINATE SYSTEM



NODE NUMBER 1

	DESIGN LOADINGS								
	DISPLACEMENTS			FORCES			MOMENTS		
	X	Y	Z	FX	FY	FZ	MX	MY	MZ
DEADWEIGHT-1	—	—	—	0	-1000	-20	-1200	-870	20090
THERMAL-1	—	—	—	-450	340	1479	31540	62080	121840
THERMAL-2	—	—	—	-20	80	10	-8120	-9000	33650
SEISMIC-OBE	—	—	—	±50	±147	±510	±7676	±18535	±6030
SEISMIC-OBE	—	—	—	±94	±259	±340	±12681	±30537	±10427
BLOWDOWN-SRV									
BLOWDOWN-PORV	—	—	—	±495	±10369	±222	±3354	±1814	±8140

UNITS: DISPLACEMENTS : INCHES
 FORCES : POUNDS
 MOMENTS : INCH-POUNDS

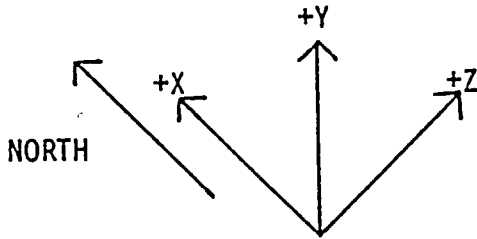
NOZZLE LOAD SUMMARY SHEET

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GLOBAL COORDINATE SYSTEM



NODE NUMBER 750

	DESIGN LOADINGS								
	DISPLACEMENTS			FORCES			MOMENTS		
	X	Y	Z	FX	FY	FZ	MX	MY	MZ
DEADWEIGHT-1	—	—	—	-100	470	250	9220	-1790	-3810
THERMAL-1	—	—	—	820	-579	170	17250	4720	-83830
THERMAL-2	—	—	—	390	-50	400	33520	9870	-45740
SEISMIC-OBE	—	—	—	±375	±500	±389	±19183	±26696	±34854
SEISMIC-DBE	—	—	—	±527	±806	±537	±26283	±39635	±52040
BLOWDOWN-SRV									
BLOWDOWN-PORV	—	—	—	±2083	±2803	± 886	±36134	± 37970	± 81181

UNITS: DISPLACEMENTS : INCHES
 FORCES : POUNDS
 MOMENTS : INCH-POUNDS

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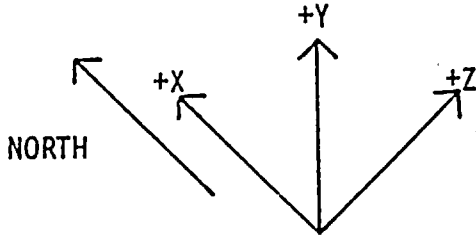
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GLOBAL COORDINATE SYSTEM



NODE NUMBER 244

	DESIGN LOADINGS								
	DISPLACEMENTS			FORCES			MOMENTS		
	X	Y	Z	FX	FY	FZ	MX	MY	MZ
DEADWEIGHT-1	-	-	-	20	-1040	60	18230	-950	-11150
THERMAL-1	-	-	-	-140	-2069	-690	-28480	26920	-64200
THERMAL-2	-	-	-	-260	-1180	-120	-19920	10250	-39240
SEISMIC-OBE	-	-	-	±611	±921	±501	±10864	±10964	±20444
SEISMIC-DBE	-	-	-	±1031	±1523	±852	±18491	±18177	±33944
BLOWDOWN-SRV									
BLOWDOWN-PORV	-	-	-	±94	±105	±130	±3725	±1966	±3188

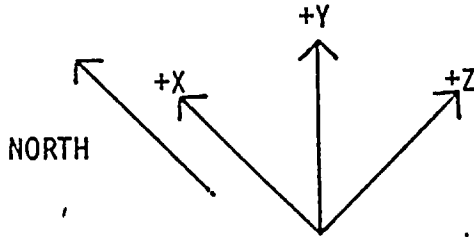
UNITS: DISPLACEMENTS : INCHES
 FORCES : POUNDS
 MOMENTS : INCH-POUNDS

NOZZLE LOAD SUMMARY SHEET

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NODE NUMBER 185

	DESIGN LOADINGS								
	DISPLACEMENTS			FORCES			MOMENTS		
	X	Y	Z	FX	FY	FZ	MX	MY	MZ
DEADWEIGHT-1	-	-	-	-50	-910	0	13930	440	16830
THERMAL-1	-	-	-	360	-820	-440	20890	22100	-17600
THERMAL-2	-	-	-	80	-430	-100	7080	5680	-12980
SEISMIC-OBE	-	-	-	±681	±1191	±810	±24668	±13523	±7006
SEISMIC-DBE	-	-	-	±1132	±1982	±1401	±40909	±22405	±12079
BLOWDOWN-SRV									
BLOWDOWN-PORV	-	-	-	±77	±113	±75	±2215	±1205	±2071

UNITS: DISPLACEMENTS : INCHES
 FORCES : POUNDS
 MOMENTS : INCH-POUNDS



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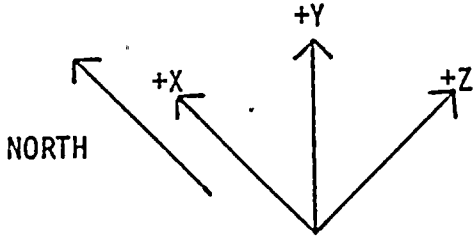
TELEDYNE
ENGINEERING SERVICES

NOZZLE LOAD SUMMARY SHEET

DONALD C. COOK
 UNIT #1
 PROJECT 5364

BY: Dmd DATE: 5/26/83
 CHECKED BY: AMB DATE: 5-26-83

GLOBAL COORDINATE SYSTEM



NODE NUMBER 138

DESIGN LOADINGS									
	DISPLACEMENTS			FORCES			MOMENTS		
	X	Y	Z	FX	FY	FZ	MX	MY	MZ
DEADWEIGHT-1	—	—	—	-20	-880	-60	-10330	850	21360
THERMAL-1	—	—	—	400	-430	-30	15060	15000	12520
THERMAL-2	—	—	—	150	-280	30	6850	4950	3270
SEISMIC-OBE	—	—	—	±920	±1350	±820	±16050	±15334	±23448
SEISMIC-OBE	—	—	—	±1600	±2241	±1361	±26601	±26287	±38971
BLOWDOWN-SRV	—	—	—						
BLOWDOWN-PORV	—	—	—	±127	±87	±50	±995	±1598	±2876

UNITS: DISPLACEMENTS : INCHES
 FORCES : POUNDS
 MOMENTS : INCH-POUNDS

6.5 Valve Loads

Section 6.5 gives the moments on each end of all valves in the piping system for each loading condition analyzed.

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VALVE END MOMENTS

DONALD C. COOK
UNIT #1
PROJECT 5364

BY: DMB DATE: 5-25-83

CHECKED BY: Dmd DATE: 5/27/83

VALVE NUMBER SV-45C

NODE NUMBER	115			120		
	MX	MY	MZ	MX	MY	MZ
DEADWEIGHT	5364	-2369	-1525	16095	-2363	-5536
THERMAL 1	-1913	-3627	-20154	-8605	-9858	-10136
THERMAL 2	2673	23	-4907	-2185	-2115	-514
SEISMIC OBE	± 2418	± 3067	± 12929	± 6421	± 1098	± 5189
SEISMIC DBE	± 4087	± 5324	± 22508	± 10645	± 1821	± 8610
BLOWDOWN PORV	± 1858	± 806	± 2466	± 1460	± 793	± 1894

VALVE NUMBER SV-45B

NODE NUMBER	165			170		
	MX	MY	MZ	MX	MY	MZ
DEADWEIGHT	2426	-1606	-5606	3252	-1550	-16289
THERMAL 1	-16818	-3639	-13166	-9819	-11254	6586
THERMAL 2	-246	-1464	596	1062	-3237	9045
SEISMIC OBE	± 10449	± 3248	± 2078	± 2403	± 1044	± 6396
SEISMIC DBE	± 18079	± 5616	± 3593	± 4037	± 1730	± 10582
BLOWDOWN PORV	± 1117	± 544	± 849	± 1046	± 706	± 911

UNITS: INCH-POUNDS

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VALVE END MOMENTS

DONALD C. COOK
UNIT #1
PROJECT 5364

BY: AMB DATE: 5-25-83
CHECKED BY: Smd DATE: 5/27/83

VALVE NUMBER SV-45A

NODE NUMBER	225			229		
	MX	MY	MZ	MX	MY	MZ
DEADWEIGHT	-2525	-909	-4675	-10304	-269	-7910
THERMAL 1	-17623	-4471	6022	24503	-11620	18857
THERMAL 2	3133	-3765	12510	22174	-8404	16514
SEISMIC OBE	±4649	±2775	±4870	±6046	±1853	±4509
SEISMIC DBE	±7941	±4736	±8259	±10129	±3152	±7664
BLOWDOWN PORV	±1064	±904	±2528	±672	±511	±1856

VALVE NUMBER _____

NODE NUMBER						
	MX	MY	MZ	MX	MY	MZ
DEADWEIGHT						
THERMAL 1						
THERMAL 2						
SEISMIC OBE						
SEISMIC DBE						
BLOWDOWN PORV						

UNITS: INCH-POUNDS

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VALVE END MOMENTS

DONALD C. COOK
UNIT #1
PROJECT 5364

BY: AMB DATE: 5-25-83

CHECKED BY: Dmd DATE: 5/27/83

VALVE NUMBER NRV-153

NODE NUMBER	525			510		
	MX	MY	MZ	MX	MY	MZ
DEADWEIGHT	-5959	3595	-4701	-6710	2225	-6561
THERMAL 1	2852	-4053	1999	2961	-3923	2271
THERMAL 2	3932	-3806	4366	3673	-3767	3725
SEISMIC OBE	±9951	±5546	±1702	±4646	±4981	±9759
SEISMIC DBE	±13438	±7551	±2527	±7165	±6806	±15305
BLOWDOWN PORV	±3998	±2113	±9683	±7039	±4021	±11669

VALVE NUMBER NMO-153

NODE NUMBER	505			490		
	MX	MY	MZ	MX	MY	MZ
DEADWEIGHT	-6204	562	-5309	-4760	-784	-2629
THERMAL 1	3094	-3766	2600	3202	-3636	2866
THERMAL 2	3358	-3723	2946	3105	-3682	2317
SEISMIC OBE	±4753	±5126	±10677	±8361	±7712	±9107
SEISMIC DBE	±7196	±7003	±16578	±9231	±6785	±17895
BLOWDOWN PORV	±8354	±6186	±12386	±4807	±6132	±13195

UNITS: INCH-POUNDS



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VALVE END MOMENTS

DONALD C. COOK
UNIT #1
PROJECT 5364

BY: AMB DATE: 5-25-83

CHECKED BY: Dmd DATE: 5/27/83

VALVE NUMBER NRV-152

NODE NUMBER	385			400		
	MX	MY	MZ	MX	MY	MZ
DEADWEIGHT	-347	595	-4480	1429	-1879	-5198
THERMAL 1	-400	1634	89	-704	-37	212
THERMAL 2	-1418	-1618	78	-1374	-3349	60
SEISMIC OBE	±4646	±2854	±1240	±9380	±4125	±2514
SEISMIC DBE	±6450	±4457	±1972	±14835	±6030	±18821
BLOWDOWN PORV	±4233	±1847	±3336	±11543	±3164	±12310

VALVE NUMBER NMO-152

NODE NUMBER	405			420		
	MX	MY	MZ	MX	MY	MZ
DEADWEIGHT	76	-4888	-4650	-2685	-7312	-3174
THERMAL 1	-1073	-2072	361	-1371	-3709	481
THERMAL 2	-1319	-5455	38	-1275	-7152	20
SEISMIC OBE	±70544	±4509	±13030	±14271	±6013	±16190
SEISMIC DBE	±16123	±6182	±19393	±21126	±8564	±23806
BLOWDOWN PORV	±10442	±5391	±11858	±10039	±4745	±9537

UNITS: INCH-POUNDS

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VALVE END MOMENTS

DONALD C. COOK
UNIT #1
PROJECT 5364

BY: DMB DATE: 5-25-83

CHECKED BY: SMD DATE: 5/27/83

VALVE NUMBER NRV-151

NODE NUMBER	625			635		
	MX	MY	MZ	MX	MY	MZ
DEADWEIGHT	5091	-575	670	7219	42	5939
THERMAL 1	7775	1660	4472	5328	-3428	-1588
THERMAL 2	5387	-3196	2717	4882	-5146	1466
SEISMIC OBE	± 5763	± 4843	± 2129	± 9577	± 4397	± 4585
SEISMIC DBE	± 8659	± 7323	± 3281	± 14592	± 6809	± 7333
BLOWDOWN PORV	± 3207	± 2431	± 8262	± 8007	± 4980	± 17493

VALVE NUMBER NM0-151

NODE NUMBER	645			657		
	MX	MY	MZ	MX	MY	MZ
DEADWEIGHT	8389	790	8832	8022	1396	9243
THERMAL 1	2349	-9618	-8955	-47	-14606	-14900
THERMAL 2	4267	-7517	-55	3772	-9431	-1283
SEISMIC OBE	± 9728	± 2722	± 3576	± 1289	± 3684	± 3669
SEISMIC DBE	± 14704	± 3880	± 5836	± 17293	± 5411	± 5967
BLOWDOWN PORV	± 9321	± 8307	± 15478	± 7523	± 7192	± 8935

UNITS: INCH-POUNDS

6.6 Miscellaneous Calculations

6.6.1 Thermal Boundary Displacements

11-11-11
11-11-11



BY DMD DATE 4/8/83
 CHKD. BY JLR DATE 7-15-83

THERMAL BOUNDARY DISPLACEMENT
 NORMAL THERMAL CONDITION

SHEET NO. 1 OF
 PROJ. NO. 5364

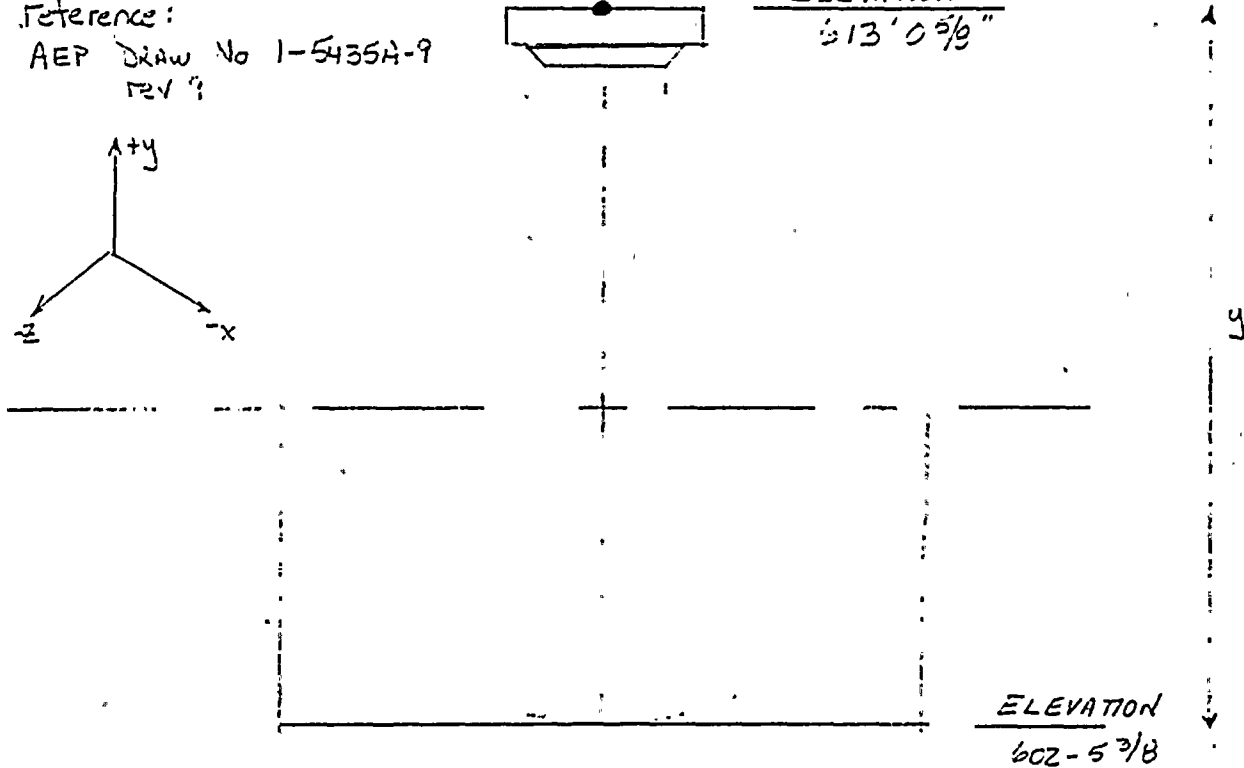
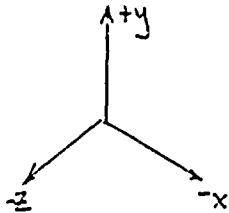
UNITS $1 \frac{1}{2}$

Temperature @ Quench Tank = 85°F (per AEP letter dated 11/29/82)

Reference:
 AEP Draw No 1-5435A-9
 REV ?



ELEVATION
 $513' - 0 \frac{5}{8}''$



Want displacements at point A

$$y = \frac{513' - 0 \frac{5}{8}'' - 602' - 5 \frac{3}{8}''}{10' - 7 \frac{1}{4}''} = 10.604'$$

x movement = z movement = 0 since nozzle is at ϕ of Q-tank

y movement = $\alpha \Delta t l$

$\alpha = 6.135 \times 10^{-6}$ in/in/°F (for ferritic carbon steel)

$\Delta t = 15^\circ\text{F}$ (85-70)

$l = 10.604' = 127.248''$

$\Delta y = 6.135 \times 10^{-6} \times 15 \times 127.248 = .0117''$

Summary $\Delta x = 0$ $\Delta y = +.0117''$ $\Delta z = 0$

10-10-10
10-10-10



6-129

BY DMD DATE 4/12/83
CHKD. BY [Signature] DATE 4-13-83

$\alpha, \Delta T$ Values Units $1/2$

SHEET NO. 1 OF
PROJ. NO. 5364

temperature $\Rightarrow 653^\circ F$

$$\Delta T = 653 - 70 = 583$$

for austenitic stainless steel $\alpha_{650} = 9.87 \times 10^{-6}$

$$\alpha_{700} = 9.93 \times 10^{-6}$$

$$\alpha_{700} - \alpha_{650} = 9.93 - 9.87 = .06$$

$$\frac{.06}{50^\circ} = \frac{x}{3^\circ} \quad x = .0036$$

$$\alpha_{653} = 9.87 + .0036 = 9.8736 \times 10^{-6}$$

temperature = 35°

$$\Delta T = 35 - 70 = 15^\circ$$

for austenitic stainless steel $\alpha_{70} = 9.11 \times 10^{-6}$

$$\alpha_{100} = 9.16 \times 10^{-6}$$

$$\alpha_{100} - \alpha_{70} = 9.16 - 9.11 = .05$$

$$\frac{.05}{30} = \frac{x}{15} \Rightarrow x = .025$$

$$\alpha_{35} = 9.11 + .025 = 9.135 \times 10^{-6}$$



BY DMD DATE 4/12/83
 CHKD. BY [Signature] DATE 4-12-83

Thermal Boundary Displacements
 Normal Thermal Condition

SHEET NO. 2 OF
 PROJ. NO. 5364

Temperature of Pressurizer = 653°F (per AEP letter dated 11/29/82)

References ① AEP DRAW No 1-5435-8 rev 8

② (W) DRAW No 1097 J56 sheet 1 of 2

③ AEP DRAW No 1-5436-7

per reference ② dimension from base of pressurizer to
 SRV & PORV nozzles is :

$$635.5 - (52.00 - 35.06) = 618.56''$$

Δy will be same for all four nozzles since the elevations are the same.

$\alpha_{583^\circ} = 7.3366 \times 10^{-6}$ in/in/°F for carbon steel @ 653°

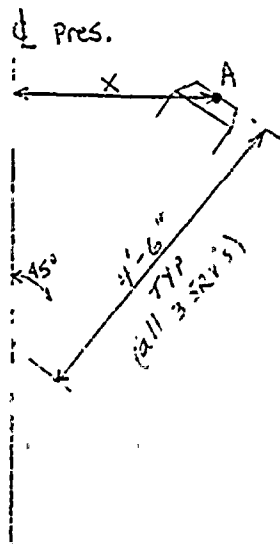
$$l = 618.56''$$

$$\Delta t = 653 - 70 = 583$$

$$\Delta y = + \alpha \Delta t l = 7.3366 \times 10^{-6} \times 618.56'' \times 583^\circ = 2.6457''$$

radial growth

per section "G-7" of ref 3



$$\frac{\sin 20}{4.5} = \frac{\sin 45}{x}$$

$$x = 3.142' = 38.1838''$$

note: this page of calculations is the same for both units since
 the pressurizer & nozzle dimensions are essentially identical



BY DMD DATE 4/12/83
 CHKD. BY ... DATE ...

Thermal Boundary Displacements
 NORMAL Thermal Condition

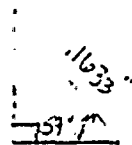
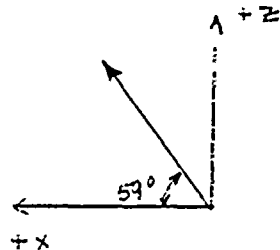
SHEET NO. 3 OF ...
 PROJ. NO. 5364

UNIT 1

radial $\Delta = 7.3366 \times 10^{-6} \times 583 \times 38.1838 = .1633''$

determine x & z components for radial Δ for each SRV value

Value SV-45A

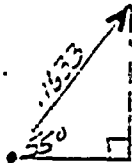
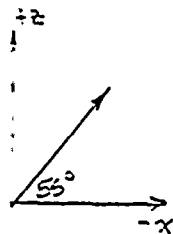


$$\frac{\sin 59}{.1633} = \frac{\sin 59}{+\Delta z} = \frac{\cos 59}{+\Delta x}$$

$$\Delta x = +.0841''$$

$$\Delta z = +.1400''$$

Value SV-45B

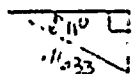
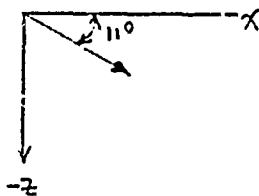


$$\frac{\sin 55}{.1633} = \frac{\sin 55}{-z} = \frac{\cos 55}{-x}$$

$$\Delta x = -.0937$$

$$\Delta z = -.1338$$

Value SV-45C



$$\frac{\sin 11}{.1633} = \frac{\sin 11}{-z} = \frac{\cos 11}{-x}$$

$$\Delta x = -.1603$$

$$\Delta z = -.0312$$

11

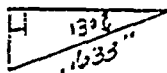
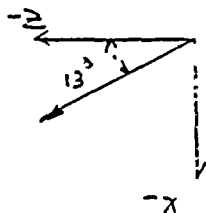


BY DMD DATE 4/12/83
 CHKD. BY JAC DATE 4-12-83

Thermal Boundary Displacements
 Normal Thermal Condition

SHEET NO. 4 OF
 PROJ. NO. 5364

UNIT 1
 PORV relief line



$$\frac{\sin 90}{.1633} = \frac{\sin 13}{-\Delta X} = \frac{\cos 13}{-\Delta Z}$$

$$\Delta X = -.0367''$$

$$\Delta Z = -.1591''$$

Summary, for the 4 pressurizer nozzles the following displacements will be inserted

node 138
 (SV-45C)
 $\Delta X = -.1603''$
 $\Delta y = +2.6457''$
 $\Delta z = -.10312''$

node 185
 (SV-45B)
 $\Delta X = -.0437''$
 $\Delta y = +2.6457''$
 $\Delta z = +.1338''$

node 244
 (SV-45A)
 $\Delta X = +.0841''$
 $\Delta y = +2.6457''$
 $\Delta z = +.1400''$

node 750
 (PORV relief)
 $\Delta X = -.0367''$
 $\Delta y = +2.6457''$
 $\Delta z = -.1591''$

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 **TELEDYNE
ENGINEERING SERVICES**

6.6.2 OBE Spectra

California
California





BY DMD DATE 4/8/83
 CHKD. BY SMB DATE 4/8/83

Response Spectra

SHEET NO. 1 OF
 PROJ. NO. 5364

OBE Analysis

For both Units 1 & 2 the attached spectra curves indicate that Containment CRANE WALL elevation 6E7'-6" governs for all frequencies. Therefore the horizontal (X & Z) response spectra for OBE analysis is

<i>f</i>	<i>g</i>
.5	.10
1.0	.30
1.2	.50
1.7	5.0
2.3	5.0
3.6	1.10
5.0	.70
10.0	.60
21.0	.42
50.0	.42

VERTICAL

The vertical OBE response, per the attached spectra, is:

<i>f</i>	<i>g</i>
.5	.04
1.0	.13
1.22	.20
1.70	1.33
2.30	1.33
3.10	1.62
5.00	1.62
10.0	.23
22.0	.12
50.0	.12

Q-21

Bill
The following information was obtained from the records of the
Department of the Interior, Bureau of Land Management, on
the subject of the above-captioned land.

12/1/57



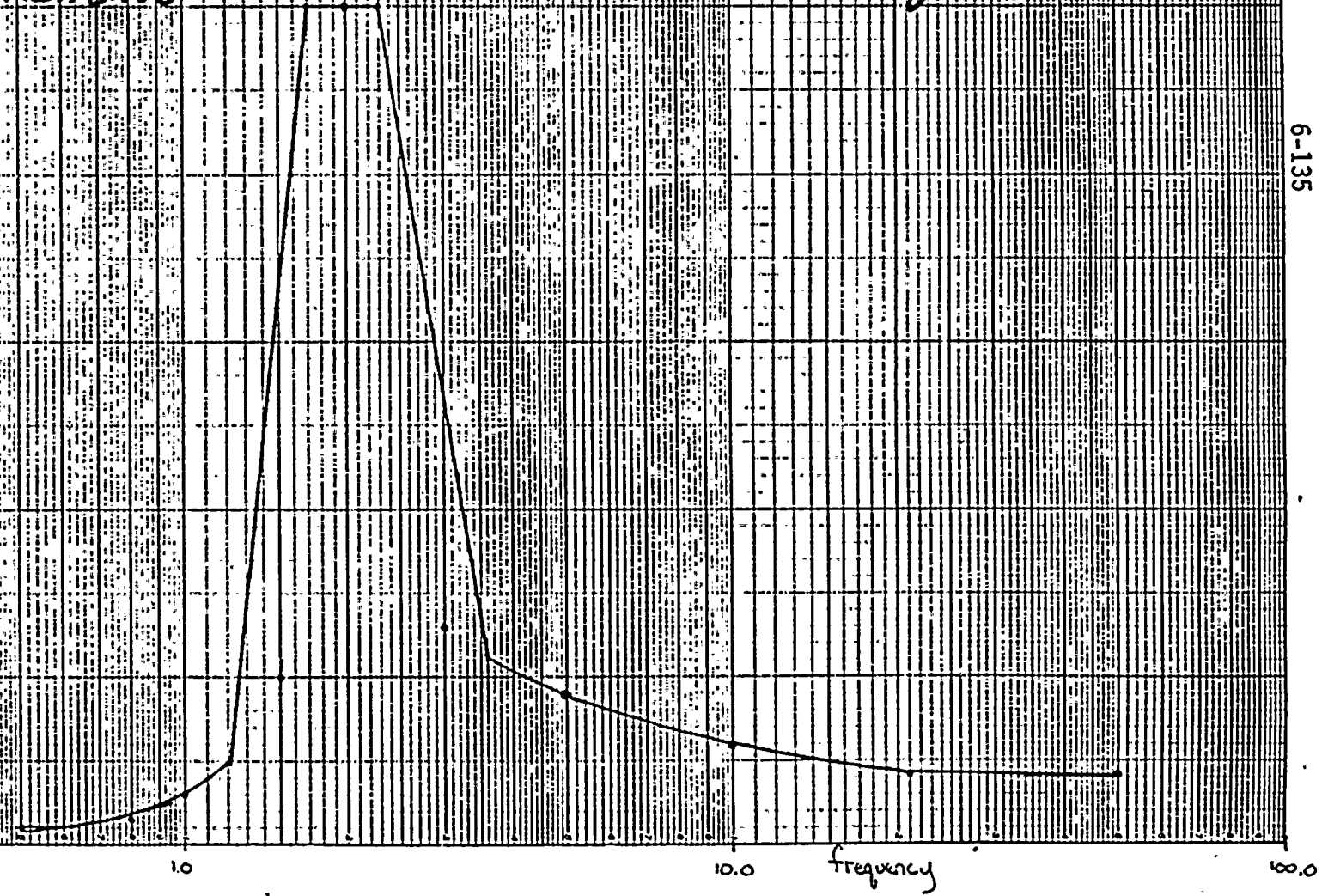
HORIZONTAL
5% EQUIPMENT DAMPING
2% STRUCTURAL DAMPING
CONTAINMENT CRANE WALL
ELEVATION 687'6"
OBE ANALYSIS
±15% PEAK SPREADING

PROJECT 5364
D.C. Cook

by SLD 4/8/83
checked by JMS 4/8/83

POINTS

11.5	1.9
1.5	1.3
1.0	1.5
1.2	5.0
1.7	5.0
2.3	1.2
3.6	9
5.0	6
10.0	42
21.0	42
50.0	42



0.001

0.0001

0.01

0.001



HORIZONTAL

5% EQUIPMENT DAMPING
2% STRUCTURAL DAMPING
CONTAINMENT CRANE WALL

ELEVATION 675' 4"
DBE ANALYSIS
± 15% PEAK SPREADING

PROJECT 5364

DC Cook

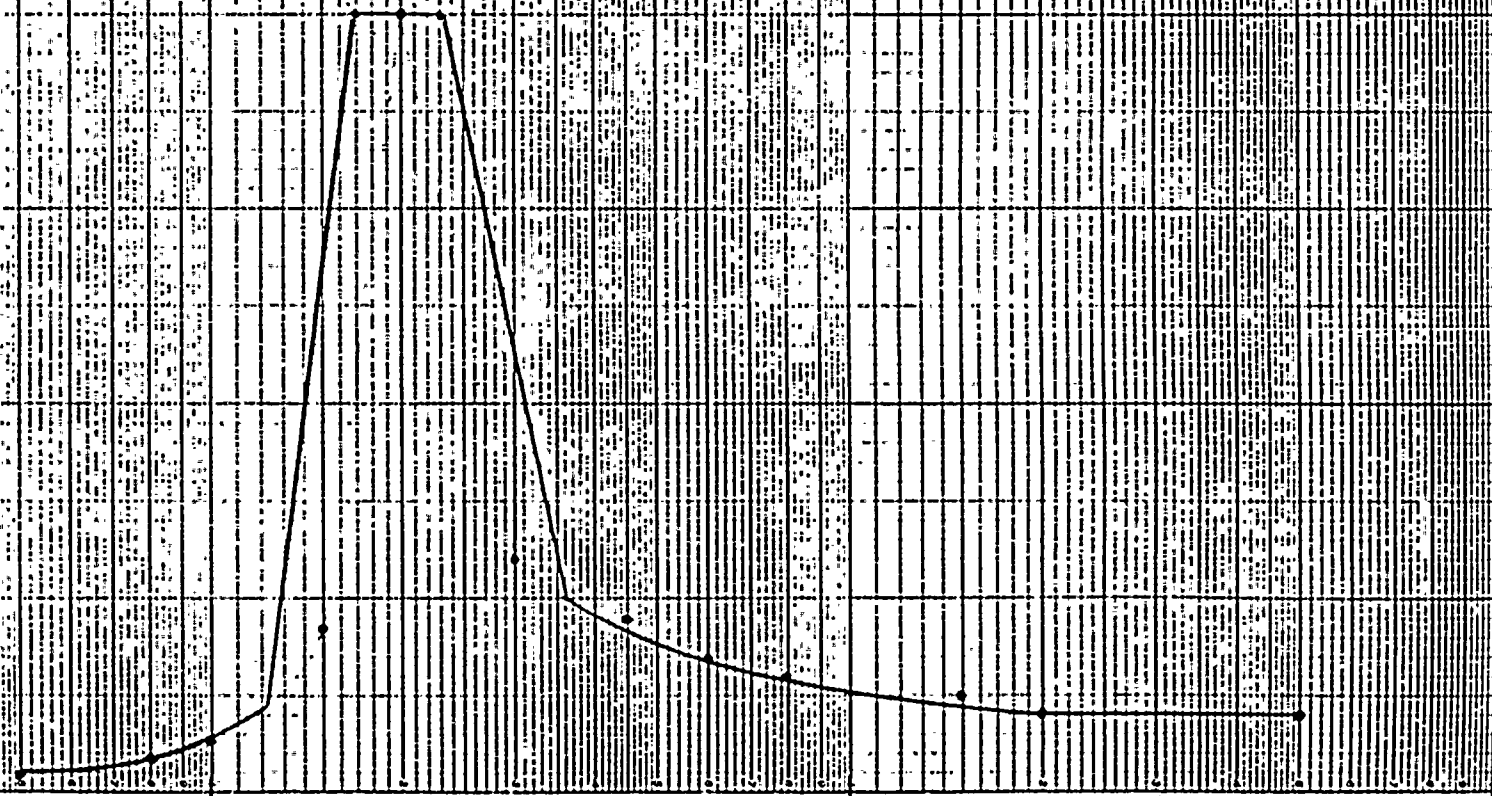
by: DMB 4/8/83

Checked by: JMK 4/8/83

9
5
4
3
2
1

Points

f	g
.5	.10
1.0	.28
1.2	.42
1.7	4.0
2.3	4.0
3.6	1.0
6.0	.7
10.0	.5
20.0	.4
50.0	.4



1.0 10.0 100.0
Frequency

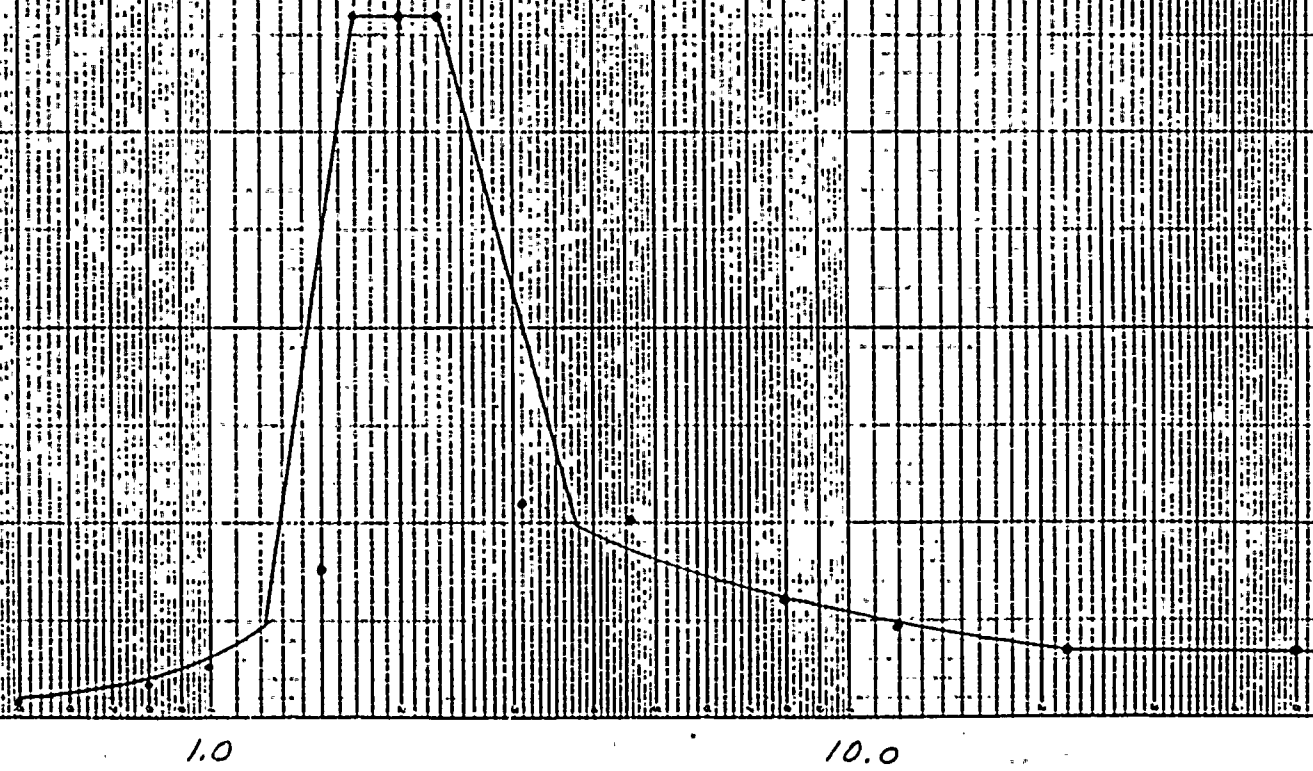
HORIZONTAL
5% EQUIPMENT DAMPING
2% STRUCTURAL DAMPING
CONFINEMENT CRANE WALL
ELEVATION 603' 4"
OBE ANALYSIS
± 15% PEAK SPREADING

Project 5364
D C Cook

by: DMD 4/8/83
checked by: ANB 4/8/83

Points

	<u>f</u>	<u>g</u>
4	.5	.70
	1.0	.30
3	1.21	.50
	1.70	3.60
	2.30	3.60
2	3.80	1.00
	8.0	.60
	12.0	.50
1	22.0	.35
	50.0	.35



0.001

1.000000

0.001

0.001



HORIZONTAL

1.5% EQUIPMENT DAMPING
2% STRUCTURAL DAMPING
CONTAINMENT CRANE WALL
ELEVATION 651' 3"
OBE ANALYSIS
± 15% PEAK SPREADING

PROJECT 5364

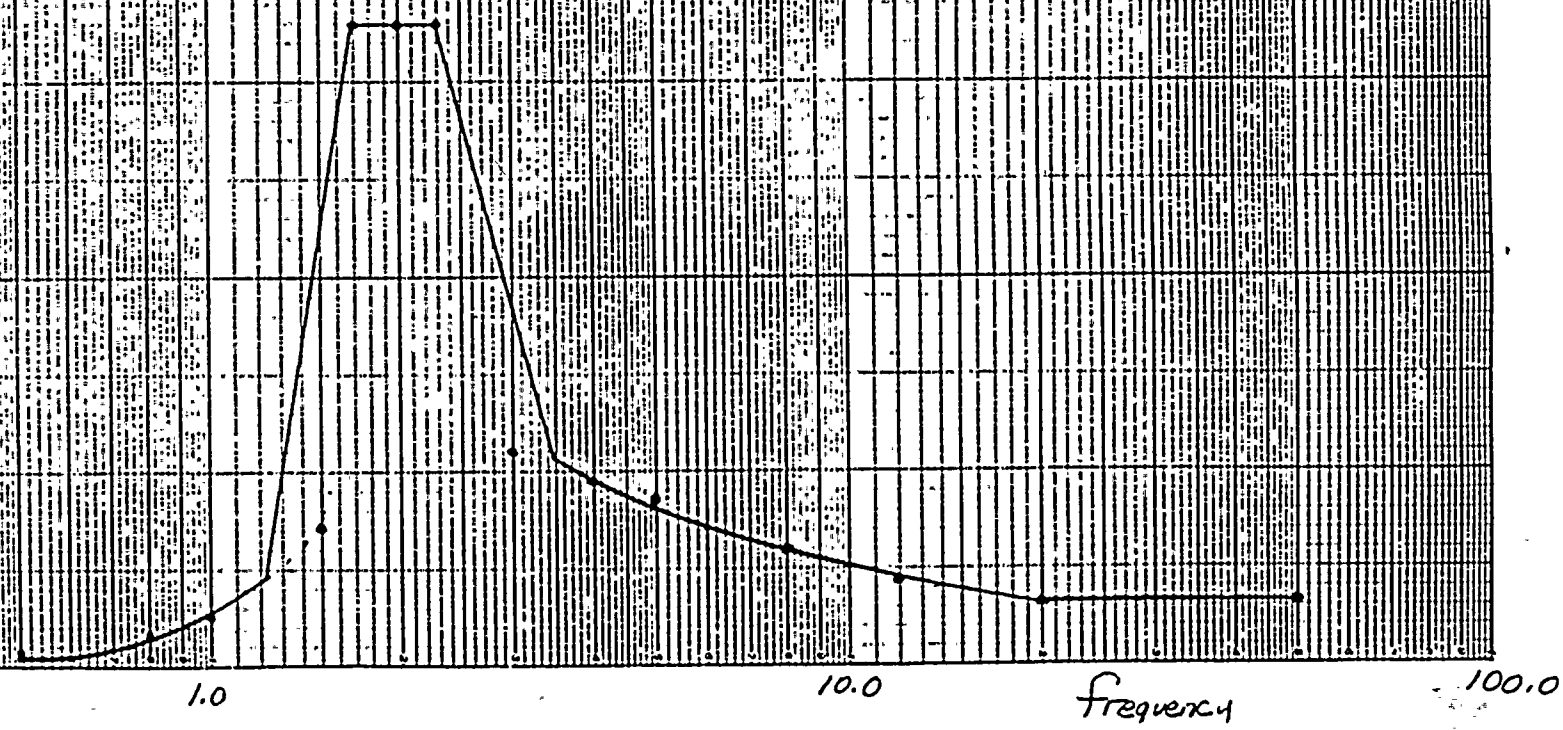
DC Cook

by: DMD 1/8/83

checked by: JMB 1/8/83

Points

f	g
.5	.09
1.0	.30
1.22	.45
1.7	3.3
2.3	3.3
3.45	1.05
5.0	.80
8.0	.60
15.0	.40
20.0	.32
50.0	.32



5.001

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AO



VERTICAL
 .5% EQUIPMENT DAMPING
 2% STRUCTURAL DAMPING
 CONTAINMENT BASE SLAB
 ELEVATION 597' 6"
 OBE ANALYSIS
 ± 15% PEAK SPREADING

Project 5364
 DC Cook

by: DMD 4/8/83
 checked by: JMB 4/8/83

Points

4

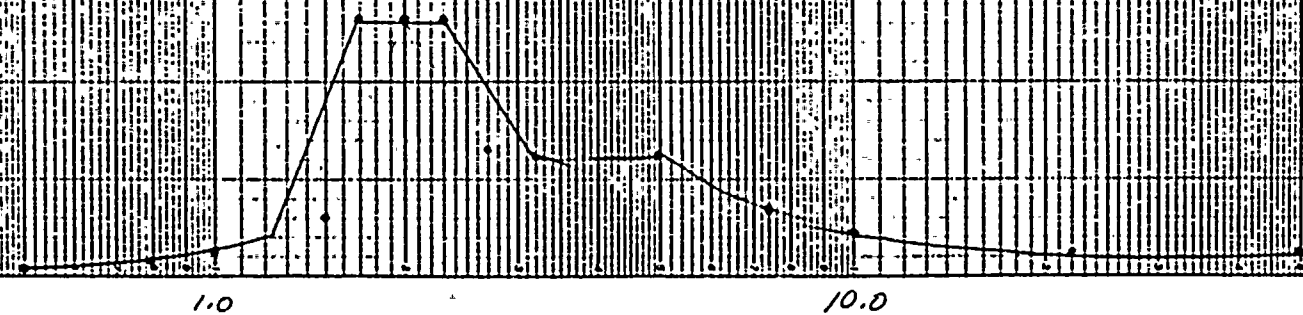
3

2

1

f	g
.5	.04
1.0	.13
1.22	.20
1.7	1.33
2.3	1.33
3.1	.62
5.0	.62
10.0	.23
22.0	.12
50.0	.12

Note: accelerations
 shown are 2/3
 of values from
 response spectra



6.6.3 DBE Spectra

11-11-11
11-11-11



BY SMD / DATE 4/11/83
 CHKD. BY SMK / DATE 4-13-83

RESPONSE SPECTRA

SHEET NO. 1 OF 1
 PROJ. NO. 5364

DBE Analysis

per the attached figures, enveloping CONTAINMENT CRANE WALL ELEVATIONS 651.3, 663.3, 675.3 & 687.5 results in the following DBE horizontal spectra for both Units 1 & 2

<u>fres</u>	<u>g</u>
.5	.19
1.0	.50
1.18	.70
1.7	5.2
2.3	5.2
3.15	2.6
3.65	1.46
6.0	1.40
7.0	1.15
10.0	1.0
17.0	.72
50.0	.72

VERTICAL

The vertical DBE response for Units 1 & 2, per the attached spectra, is:

<u>f</u>	<u>g</u>
.5	.11
1.0	.25
1.18	.33
1.70	1.40
2.30	1.40
3.42	.80
6.00	.80
10.0	.43
15.0	.28
25.0	.20
50.0	.20

0.001

1779958584

0.001

0.001

1779958584

1779958584

1779958584



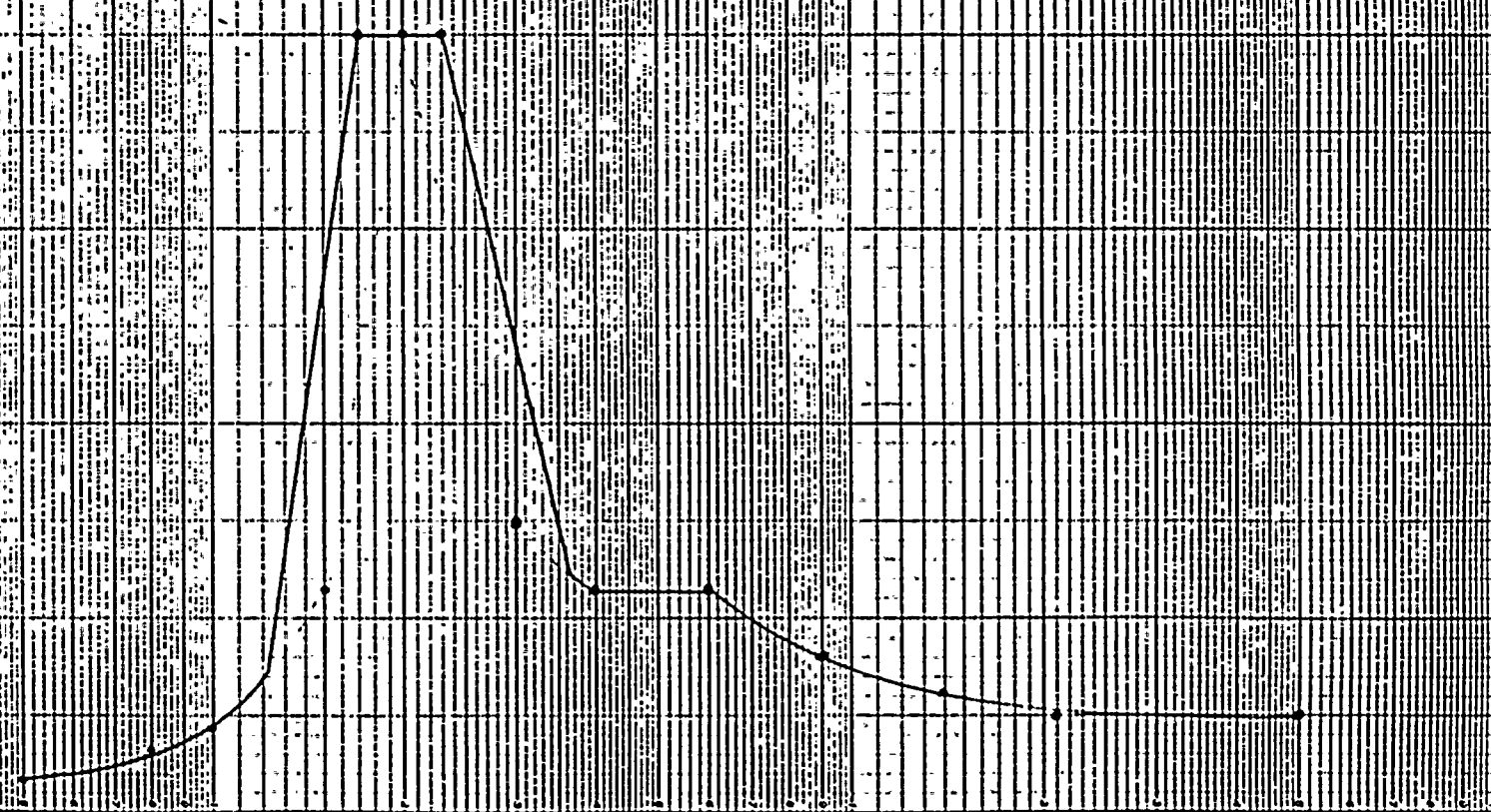
HORIZONTAL
 .5% EQUIPMENT DAMPING
 5% STRUCTURAL DAMPING
 CONTAINMENT CRANE WALL
 ELEVATION 651.3'
 NBE Analysis
 ±15% PEAK SPREADING

PROJECT 5364
 DC Cook

by: S.M. #11/83
 checked by: J.M.B. 4-13-83

Points

4	5	9
5	1.17	
1.0	.44	
3	1.21	1.72
1.70	4.0	
2.30	4.0	
2	3.60	1.22
4.00	1.25	
6.0	1.15	
1	9.0	.8
21.0	.5	
50.0	.5	



1.0 10.0 FREQUENCY 100.0

6.997

1997

0.01

0.01

Vertical text on the left side, possibly a list or index, including words like "1997", "0.01", and "0.01".

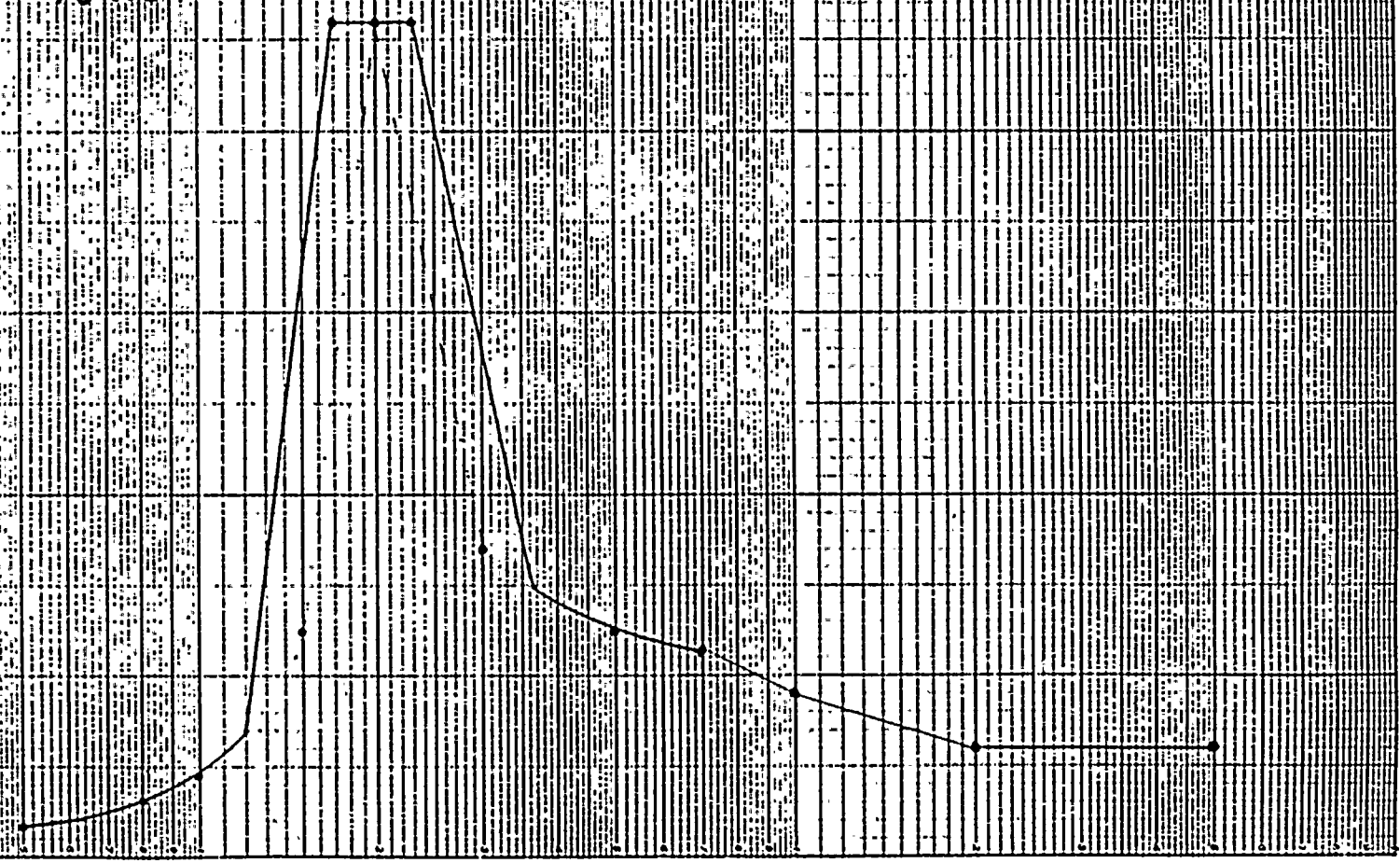
0.01



HORIZONTAL
590 EQUIPMENT DAMPING
590 STRUCTURAL DAMPING
CONTAINMENT CRANE WALL
ELEVATION 663.3
DOE Analysis
± 15% PEAK SPREADING

PROJECT 5364
DC Cook
by: DMB 4/11/83
checked by: JWB 4-13-83

Points	
f	g
.5	.18
1.0	.46
1.2	.70
1.7	.46
2.3	.46
3.65	1.48
5.0	1.25
7.0	1.15
10.0	.90
20.0	.60
50.0	.60



1.0 10.0 Frequency 100.0

0010

10/10/10

10/10/10

10/10/10

10/10/10



HORIZONTAL
5% EQUIPMENT DAMPING
5% STRUCTURAL DAMPING

CONTAINMENT CRANE WALL
ELEVATION 675.3'

DBE ANALYSIS

± 15% PEAK SPREADING

Points

F	g
---	---

.5	.19
----	-----

1.0	.50
-----	-----

1.21	.72
------	-----

1.7	5.0
-----	-----

2.3	5.0
-----	-----

3.15	2.6
------	-----

3.65	1.46
------	------

5.0	1.25
-----	------

6.0	1.0
-----	-----

10.0	.95
------	-----

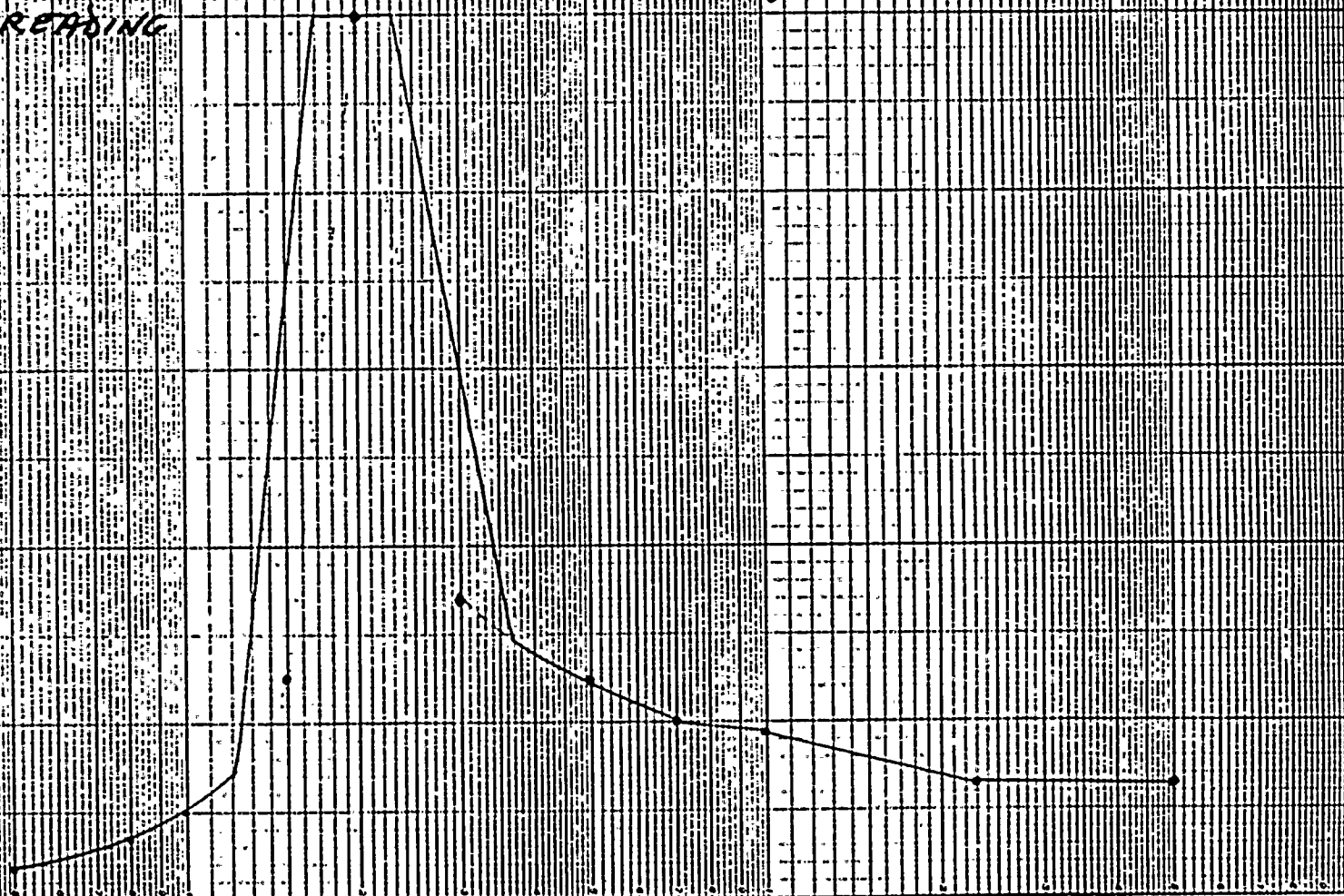
23.0	.65
------	-----

50.0	.65
------	-----

PROJECT 5364
DC Cook

by: DMD 4/11/83

checked by: FWS 4-13-83



1.0

10.0

frequency

100.0

HORIZONTAL
5% EQUIPMENT DAMPING
5% STRUCTURAL DAMPING
CONTAINMENT CRANE WALL
ELEVATION 687'-6"
DBE ANALYSIS
± 15% PEAK SPREADING

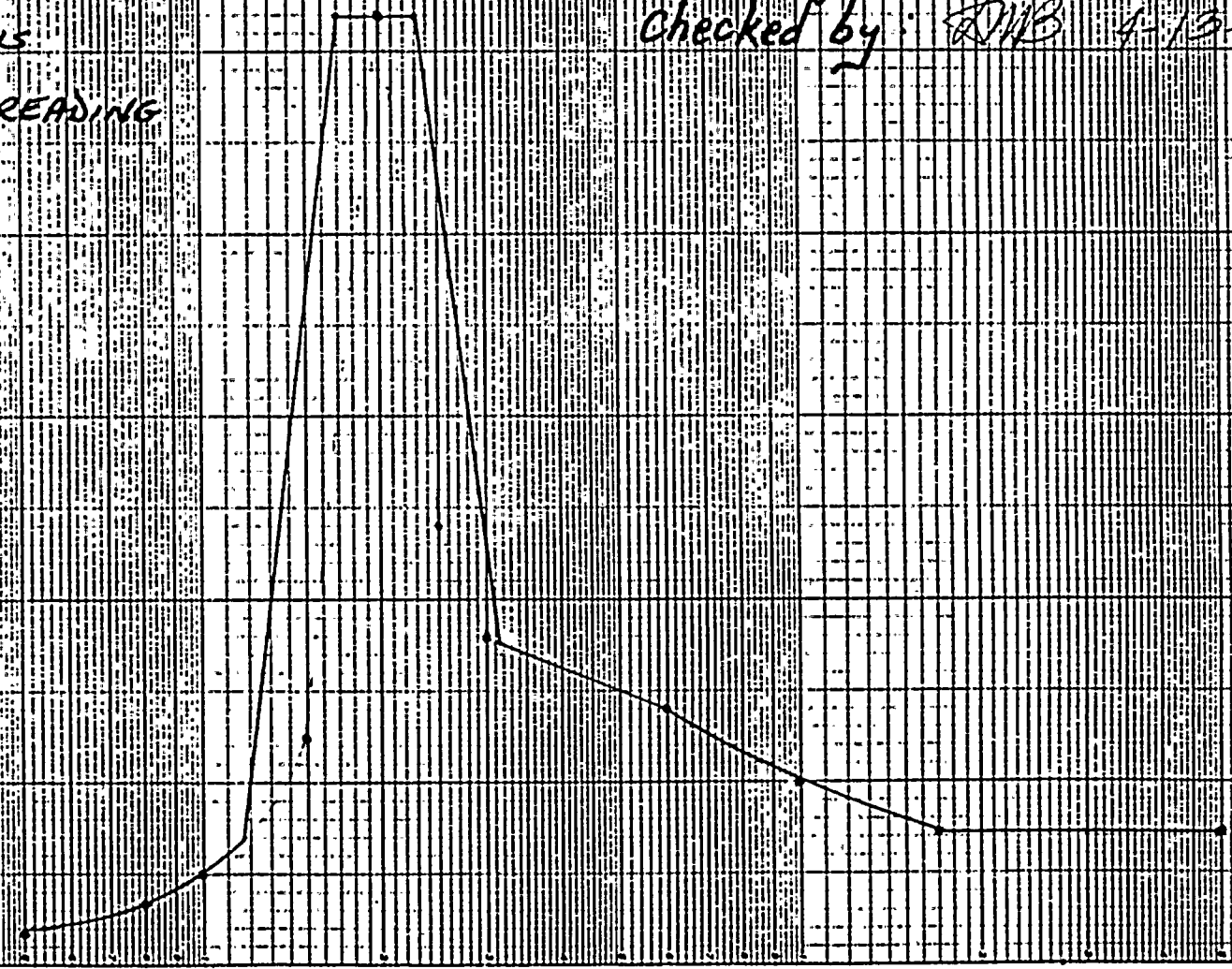
PROJECT 5364
D C Cook

by DMD 4/11/83

checked by: DMB 4-19-83

Points

freq	g
.5	.18
1.0	.50
1.18	.70
1.7	5.2
2.3	5.2
3.15	1.76
6.0	.14
10.0	.10
17.0	.72
50.0	.72



1000 0

1000000 00



VERTICAL
 5% EQUIPMENT DAMPING
 5% STRUCTURAL DAMPING
 CONTAINMENT BASE SLAB
 ELEVATION 597'-6"
 DBE Analysis
 ± 15% PEAK SPREADING

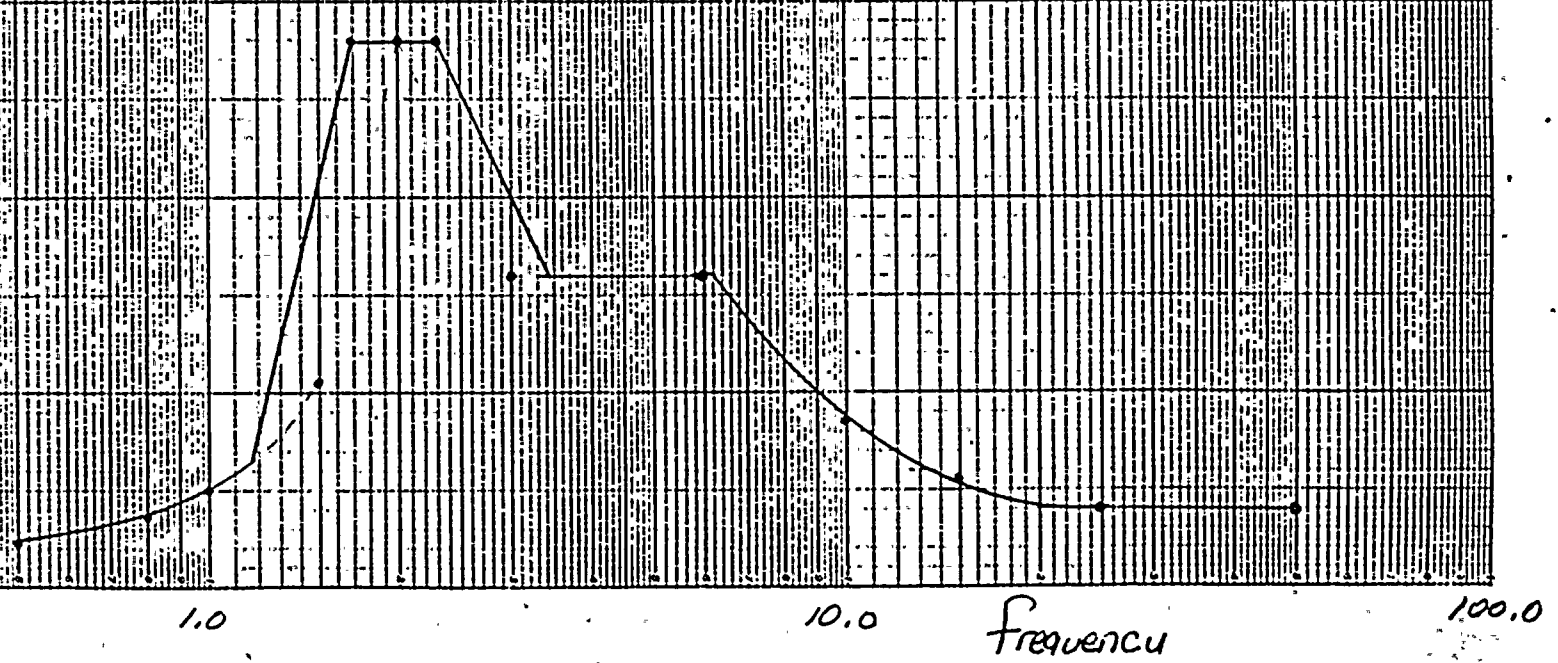
PROJECT 5364
 DC Cook

by DMB 4/11/83

checked by: DMB 4-13-83

Points

f	g
.5	.11
1.0	.25
1.8	.33
1.70	.40
2.30	.40
3.42	.80
6.0	.80
10.0	.43
15.0	.28
25.0	.20
50.0	.20



IN CASE OF

EMERGENCY



Technical Report
TR-5364-1
Revision 0

7-1

 **TELEDYNE
ENGINEERING SERVICES**

7.0 DRAWINGS

ENGINEERING

1. The first part of the report is a general introduction to the subject.

2. The second part is a detailed description of the experimental apparatus used.

3. The third part is a discussion of the results obtained from the experiments.

4. The fourth part is a conclusion and a list of references.

5. The fifth part is a list of figures and tables.

6. The sixth part is a list of symbols and abbreviations.

7. The seventh part is a list of footnotes.

8. The eighth part is a list of appendices.

9. The ninth part is a list of errata.

10. The tenth part is a list of acknowledgments.

8.0 REFERENCES

1. Teledyne Engineering Services Technical Proposal PR-5653, dated May 14, 1981.
2. Letter from Mr. S. Ulan of AEP to Mr. L.B. Semprucci of TES, dated November 29, 1983.
3. Letter from Mr. S. Ulan of AEP to Mr. P. D. Harrison of TES, dated March 15, 1983.
4. RELAP5 MOD1 - Version 2.11 - A five equation Thermal-Hydrodynamic Analysis computer program including non-condensibles.
5. TMRPIPE - A system of Computer Programs for the Complete Analysis of Nuclear Piping.
6. TES Technical Report TR-5364-2, Donald C. Cook Nuclear Generating Station, "Analysis of Pressurizer Safety Valves/Relief Valves Discharge Piping Systems per NUREG 0737, II.D.1, Unit 2.
7. Letter from Mr. S. Ulan of AEP to Mr. P. D. Harrison of TES, dated May 26, 1983.
8. TES letter 5364-21, dated February 2, 1983 from Mr. P. D. Harrison of TES to Mr. Sam Ulan of AEP.
9. TES letter 5364-25, dated February 14, 1983 from Mr. P. D. Harrison of TES to Mr. Sam Ulan of AEP.
10. TES letter 5364-33, dated April 8, 1983 from Mr. P. D. Harrison of TES to Mr. Sam Ulan of AEP.

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8.0 REFERENCES (Continued)

11. 1967 Edition of USAS B31.1 Power Piping Code.
12. Letter from Mr. J. L. Williams of AEP to Mr. L. B. Semprucci of TES dated September 16, 1982.
13. Crosby Valve Drawing and Gage Company Drawing No. H-51688, Revision A.
14. Masoneilan International, Inc. Control Valve Model No. 38-20721, Drawing No. CP1-18-55, Revision H.
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16. EPRI Safety and Relief Valve Test Report, Research Project V102 Interim Report, April 1982.
17. ASME Code NB7000, Section III.
18. ITI Report, "Evaluation of RELAP5/MOD1 for Calculation of Safety and Relief Valve Discharge Piping Hydrodynamic Loads," February 1982. Prepared by Intermountain Technologies.