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Docket No.: 50-315

U. S. Nuclear Regulatory Commission
ATTN: Document Control Desk
Washington, DC 20555-0001

Donald C. Cook Nuclear Plant Unit 1
CORE OPERATING LIMITS REPORT

Indiana Michigan Power Company, the licensee for Donald C. Cook Nuclear Plant Unit 1, is submitting the Core Operating Limits Report (COLR) for Unit 1 Cycle 28 in accordance with Technical Specification 5.6.5. Revision 0 of the Unit 1 Cycle 28 COLR is provided as an enclosure to this letter.

There are no new or revised commitments in this letter. Should you have any questions, please contact me at (269) 466-2649.

Sincerely,

Michael K. Scarpello
Regulatory Affairs Manager

DMB/mll

Enclosure: Donald C. Cook Nuclear Plant Unit 1 Cycle 28 Core Operating Limits Report, Revision 0

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A001
NRR

ENCLOSURE TO AEP-NRC-2017-58

Donald C. Cook Nuclear Plant Unit 1 Cycle 28

Core Operating Limits Report
Revision 0

Donald C. Cook Nuclear Plant
Unit 1 Cycle 28
Core Operating Limits Report

1.0 CORE OPERATING LIMITS REPORT

This Core Operating Limits Report (COLR) for Donald C. Cook Nuclear Plant Unit 1 Cycle 28 design has been prepared in accordance with the requirements of Technical Specification 5.6.5.

The analytical methods used to determine the core operating limits shall be those previously reviewed and approved by the NRC in:

a. WCAP-9272-P-A, Westinghouse Reload Safety Evaluation Methodology, July 1985

b. WCAP-8385, Power Distribution Control and Load Following Procedures – Topical Report, September 1974

c. WCAP-10216-P-A, Rev. 1A, Relaxation of Constant Axial Offset Control/F_Q Surveillance Technical Specification, February 1994

d. Plant-specific adaptation of WCAP-16009-P-A, Realistic Large Break LOCA Evaluation Methodology Using the Automated Statistical Treatment of Uncertainty Method (ASTRUM), as approved by NRC Safety Evaluation dated October 17, 2008

e. WCAP-12610-P-A, VANTAGE+ Fuel Assembly Reference Core Report, April 1995

f. WCAP-8745-P-A, Design Bases for the Thermal Overpower ΔT and Thermal Overtemperature ΔT Trip Functions, September 1986

g. WCAP-13749-P-A, Safety Evaluation Supporting the Conditional Exemption of the Most Negative EOL Moderator Temperature Coefficient Measurement, March 1997

h. WCAP-12610-P-A & CENPD-404-P-A, Addendum 1-A, Optimized ZIRLO™ July 2006.

The Technical Specifications affected by this report are listed below:

2.1.1	Reactor Core Safety Limits
3.1.1	SHUTDOWN MARGIN (SDM)
3.1.3	Moderator Temperature Coefficient (MTC)
3.1.5	Shutdown Bank Insertion Limits
3.1.6	Control Bank Insertion Limits
3.2.1	Heat Flux Hot Channel Factor ($\mathbf{F_Q(Z)}$)
3.2.2	Nuclear Enthalpy Rise Hot Channel Factor ($\mathbf{F^N_{\Delta H}}$)
3.2.3	AXIAL FLUX DIFFERENCE (AFD)
3.3.1	Reactor Trip System (RTS) Instrumentation
3.4.1	RCS Pressure, Temperature, and Flow Departure from Nucleate Boiling (DNB) Limits
3.9.1	Boron Concentration

2.0 OPERATING LIMITS

The cycle-specific parameter limits for the specifications listed in Section 1.0 are presented in the following subsections. These limits have been developed using the NRC-approved methodologies specified in Technical Specifications 5.6.5.

2.1 SAFETY LIMITS

2.1.1 Reactor Core Safety Limits (Specification 2.1.1)

In Modes 1 and 2, the combination of thermal power, pressurizer pressure, and the highest loop average temperature ($\mathbf{T_{avg}}$) shall not exceed the limits as shown in Figure 6 for 4 loop operation.

2.2 REACTIVITY CONTROL

2.2.1 SHUTDOWN MARGIN (SDM) (Specification 3.1.1)

Shutdown margin shall be greater than or equal to 1.3% Δk/k for $T_{avg} > 200°F$
Shutdown margin shall be greater than or equal to 1.0% Δk/k for $T_{avg} \leq 200°F$

2.2.2 Moderator Temperature Coefficient (MTC) (Specification 3.1.3)

a. The Moderator Temperature Coefficient (MTC) limits are:

The BOL/ARO-MTC shall be less positive or equal to the value given in Figure 1.

The EOL/ARO/RTP-MTC shall be less negative or equal to –4.54E-4 **Δk/k/°F**.

This limit is based on a $\mathbf{T_{avg}}$ program with HFP vessel $\mathbf{T_{avg}}$ of 569.0 to 573.0 °F.

Where: ARO stands for All Rods Out
BOL stands for Beginning of Cycle Life
EOL stands for End of Cycle Life
RTP stands for Rated Thermal Power
HFP stands for Hot Full Thermal Power

b. The MTC Surveillance limit is:
The 300 ppm/ARO/RTP-MTC should be less negative or equal to
–3.84E-4 **Δk/k/°F** at a HFP vessel $\mathbf{T_{avg}}$ of 569.0 to 573.0 °F.

c. The Revised Predicted near-EOL 300 ppm MTC shall be calculated using Figure 7 and the following algorithm:

Revised Predicted MTC = Predicted MTC + AFD Correction + Predicted Correction*

* Predicted Correction is -0.30E-4 **Δk/k/°F**.

If the Revised Predicted MTC is less negative than the SR 3.1.3.2 limit (COLR 2.2.2.b) and all of the benchmark data contained in the surveillance procedure are met, then a MTC measurement in accordance with SR 3.1.3.2 is not required.

d. The MTC Surveillance limit is:
The 60 ppm/ARO/RTP-MTC should be less negative or equal to
-4.41E-4 **Δk/k/°F** at a HFP vessel $\mathbf{T_{avg}}$ of 569.0 to 573.0 °F

2.2.3 Shutdown Bank Insertion Limits (Specification 3.1.5)

The shutdown rods shall be withdrawn to at least 228 steps.

2.2.4 Control Bank Insertion Limits (Specifications 3.1.6)

a. The control rod banks shall be limited in physical insertion as shown in Figure 2.

b. Successive Control Banks shall overlap by 100 steps. The sequence for Control Bank withdrawal shall be Control Bank A, Control Bank B, Control Bank C and Control Bank D.

2.3 POWER DISTRIBUTION LIMITS

2.3.1 AXIAL FLUX DIFFERENCE (AFD) (Specification 3.2.3)

a. The Allowable Operation Limits are provided in Figure 3.

b. The AFD target band is ±5% for a cycle average accumulated burnup ≥0.0 MWD/MTU.

2.3.2 Heat Flux Hot Channel Factor ($F_Q(Z)$) (Specification 3.2.1)

$$F_Q^C(Z) \le \frac{CF_Q}{P} * K(Z) \qquad for\ P > 0.5$$

$$F_Q^C(Z) \le 2 * CF_Q * K(Z) \qquad for\ P \le 0.5$$

$$F_Q^W(Z) \le \frac{CF_Q}{P} * K(Z) \qquad for\ P > 0.5$$

$$F_Q^W(Z) \le 2 * CF_Q * K(Z) \qquad for\ P \le 0.5$$

Where: $P = \frac{\text{THERMAL POWER}}{\text{RATED THERMAL POWER}}$

a. $\mathbf{CF_Q} = 2.09$

b. **K(Z)** is provided in Figure 4.

c. $\mathbf{F_Q^C(Z)}$ is the measured hot channel factor including a 3% manufacturing tolerance uncertainty and a 5% measurement uncertainty.

d. **W(Z)** is provided in Table 1 for ±5% AFD target band.

e. $\mathbf{F_Q^W(Z) = F_Q^C(Z)\ x\ W(Z)\ x\ F_P}$

The W(z) values are generated assuming that they will be used for a full power surveillance. When a part power surveillance is performed, the W(z) values should be multiplied by the factor 1/P, when P is > 0.5. When P is ≤ 0.5, the W(z) values should be multiplied by the factor 1/(0.5), or 2.0. This is consistent with the adjustment in the $F_Q(z)$ limit at part power conditions.

f. For Cycle 28, FP = 1.02 for all burnups associated with Note 2a of SR 3.2.1.2. When no penalty is required, FP = 1.00.

2.3.3 Nuclear Enthalpy Rise Hot Channel Factor ($\mathbf{F^N_{\Delta H}}$) (Specification 3.2.2)

$$\mathbf{F^N_{\Delta H}} \leq \mathbf{CF_{\Delta H}} * (1 + \mathbf{PF_{\Delta H}} * (1-P))$$

Where: $P = \frac{\text{THERMAL POWER}}{\text{RATED THERMAL POWER}}$

a. $\mathbf{CF_{\Delta H}} = 1.53$

b. $\mathbf{PF_{\Delta H}} = 0.3$

c. $\mathbf{F^N_{\Delta H}}$ is the measured Enthalpy Rise Hot Channel Factor including a 4% measurement uncertainty.

2.4 INSTRUMENTATION

2.4.1 Reactor Trip System (RTS) Instrumentation (Specification 3.3.1)

The Overtemperature **ΔT** and Overpower **ΔT** setpoints are as shown in Figure 5.

2.5 REACTOR COOLANT SYSTEM

2.5.1 RCS Pressure, Temperature, and Flow Departure from Nucleate Boiling (DNB) Limits (Specification 3.4.1)

a. Pressurizer Pressure shall be ≥ 2168 psig [+]

b. Reactor Coolant System T_{AVG} shall be ≤ 580.5°F [+]

c. Reactor Coolant System Total Flow Rate shall be ≥ 362,900 gpm

2.6 REFUELING OPERATIONS

2.6.1 Boron Concentration (Specification 3.9.1)

The boron concentration of all filled portions of the Reactor Coolant System, the refueling canal and the refueling cavity shall be greater than or equal to 2400 ppm[++].

[+] These are Safety Analysis values. With readability allowance, the corresponding values are 578.2°F for T_{avg}, and 2200 psig for Pressurizer Pressure.

[++] This concentration bounds the condition of $K_{eff} \leq 0.95$ which includes a 1% Δk/k conservative allowance for uncertainties. The boron concentration of 2400 ppm includes a 50 ppm conservative allowance for uncertainties.

FIGURE 1

MODERATOR TEMPERATURE COEFFICIENT (MTC) LIMITS

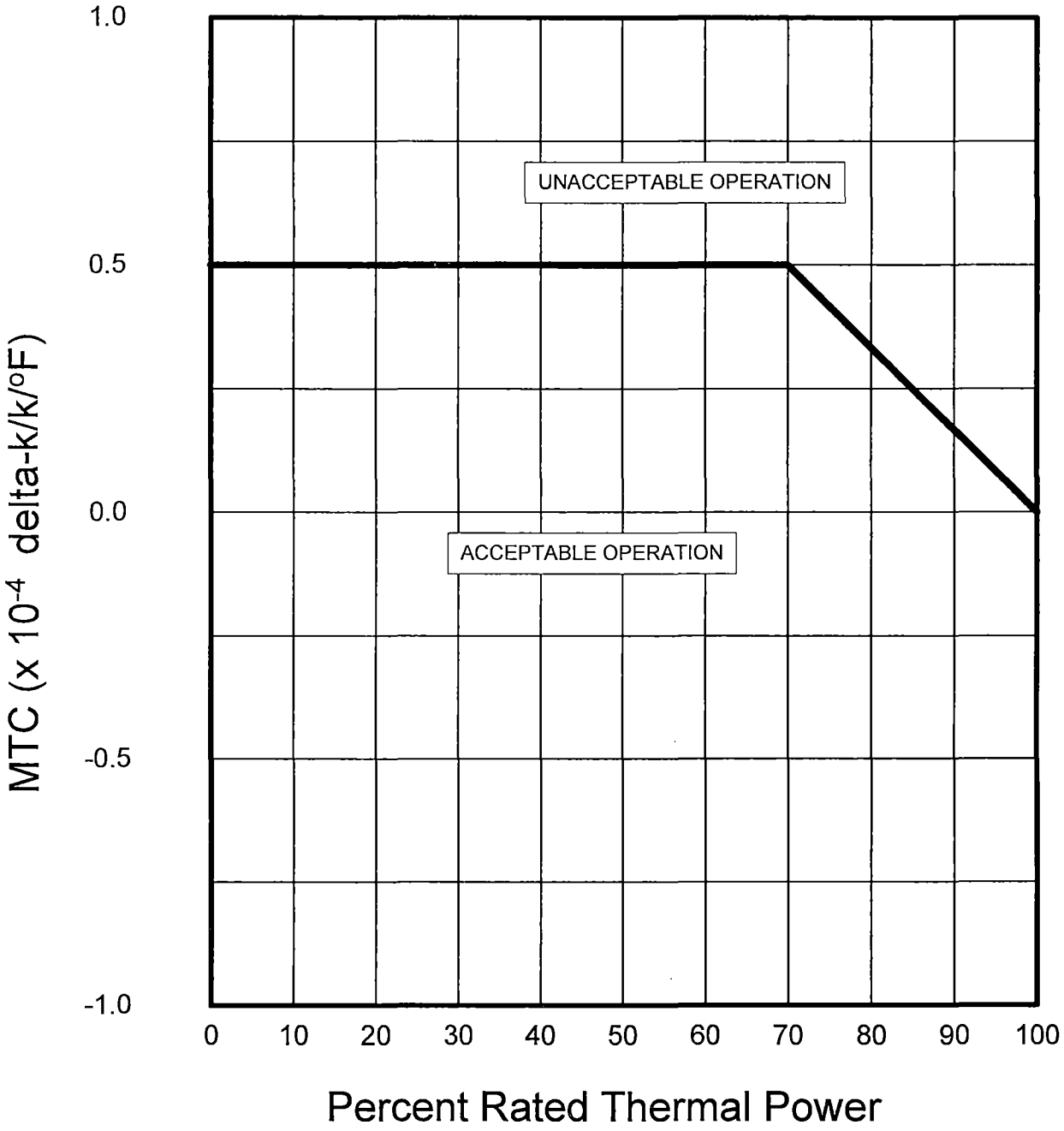


FIGURE 2

ROD BANK INSERTION LIMITS VERSUS THERMAL POWER

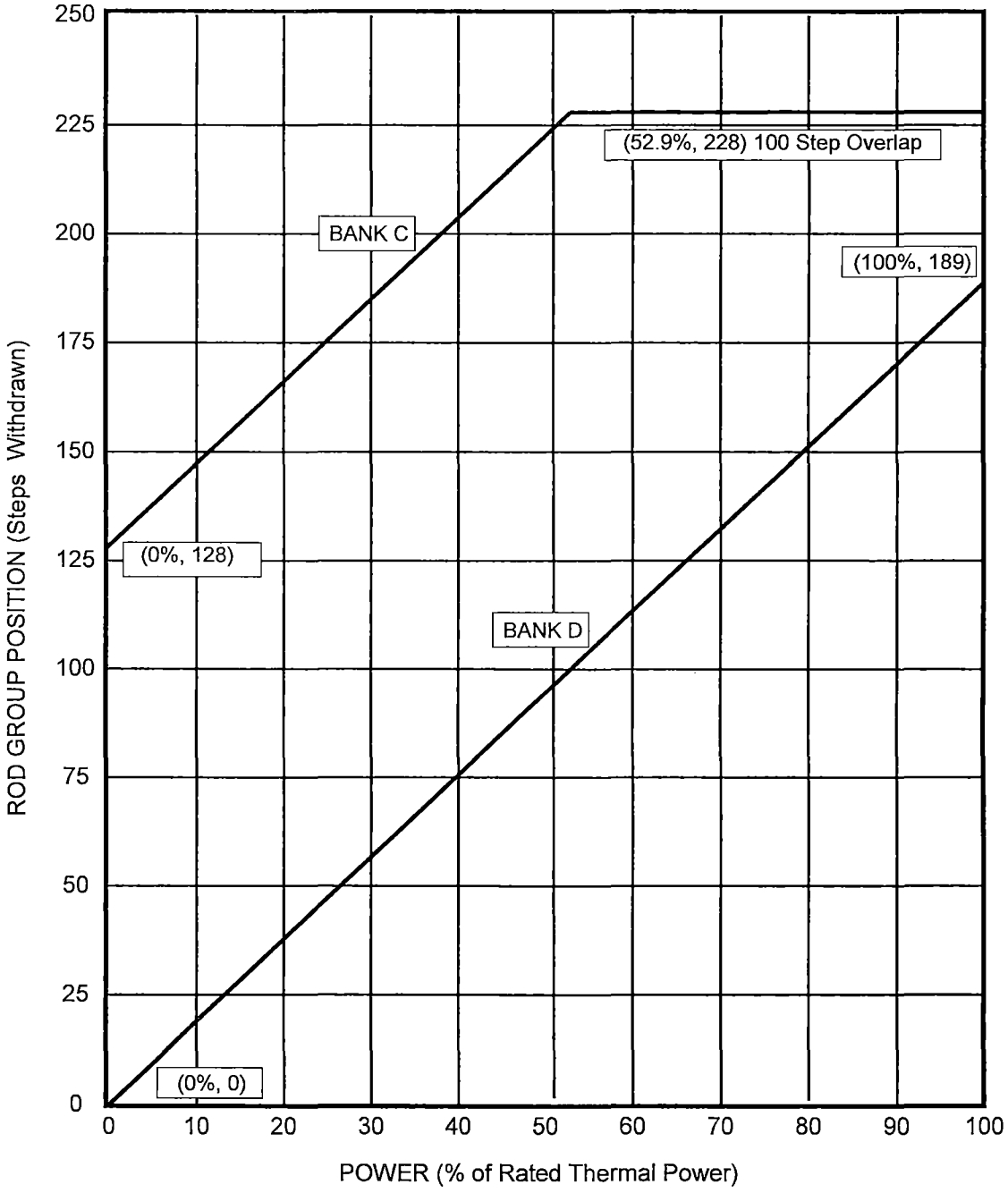


FIGURE 3

AXIAL FLUX DIFFERENCE LIMITS AS A FUNCTION OF RATED THERMAL POWER (RTP)

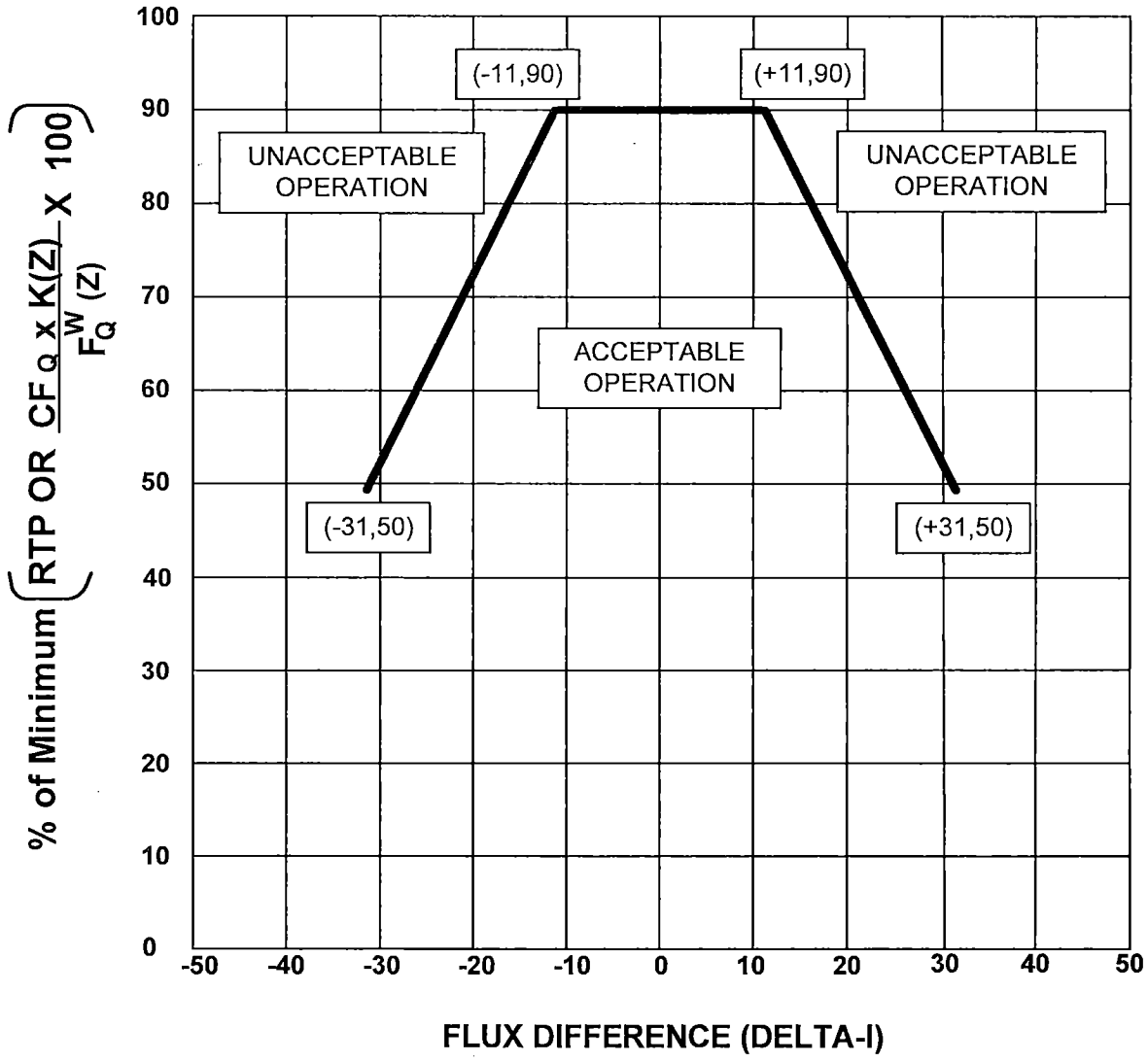


FIGURE 4

K(Z) – NORMALIZED $F_Q(Z)$ AS A FUNCTION OF CORE HEIGHT

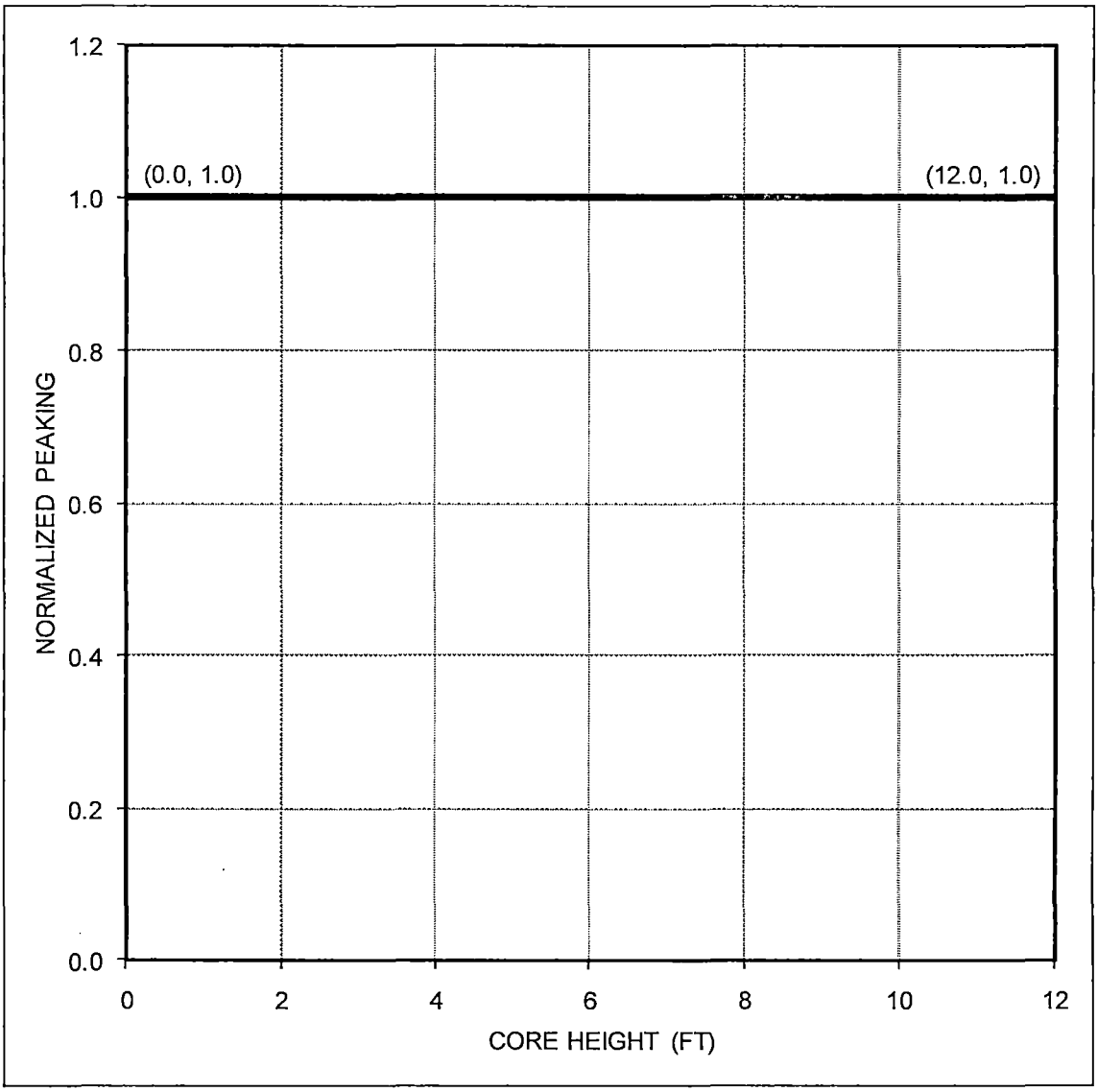


FIGURE 5
(Page 1 of 2)
Reactor Trip System Instrumentation Trip Setpoints
Overtemperature ΔT Trip Setpoint

Overtemperature $\Delta T \leq \Delta T_o \left[K_1 - K_2 \left[\frac{1+\tau_1 S}{1+\tau_2 S}\right] (T-T') + K_3 (P-P') - f_1(\Delta I)\right]$

Where:

	ΔT	=	Measured RCS ΔT, °F
	ΔT_o	=	Indicated ΔT at RATED THERMAL POWER, °F
	T	=	Average temperature, °F
	T'	=	Nominal T_{avg} at RATED THERMAL POWER (≤ 575.4 °F)
	P	=	Pressurizer pressure, psig
	P'	=	Nominal RCS operating pressure (2235 psig)
	$\frac{1+\tau_1 S}{1+\tau_2 S}$	=	The function generated by the lead-lag controller for T_{avg} dynamic compensation
	τ_1, τ_2	=	Time constants utilized in the lead-lag controller for T_{avg} $\tau_1 \geq 22$ secs. $\tau_2 \leq 4$ secs.
	S	=	Laplace transform operator, sec^{-1}
	K_1	≤	1.35 *
	K_2	≥	0.0230/°F
	K_3	≥	0.00110/psi
	$f_1(\Delta I)$	=	-0.33 {37% + (q_t - q_b)} when $q_t - q_b \leq$ -37% RTP 0% of RTP when -37% RTP < $q_t - q_b \leq$ 3% RTP +2.34 {($q_t - q_b$) – 3%} when $q_t - q_b >$ 3% RTP

where q_t and q_b are percent RATED THERMAL POWER in the upper and lower halves of the core respectively, and $q_t + q_b$ is total THERMAL POWER in percent RATED THERMAL POWER.

* This is a Safety Analysis value. Refer to Technical Requirements Manual for nominal value of this coefficient used in programming the trip setpoint.

FIGURE 5
(Page 2 of 2)
Overpower ΔT Trip Setpoint

Overpower $\Delta T \leq \Delta T_o \left[K_4 - K_5 \left[\frac{\tau_3 S}{1+\tau_3 S}\right] T - K_6 (T - T'') - f_2 (\Delta I)\right]$

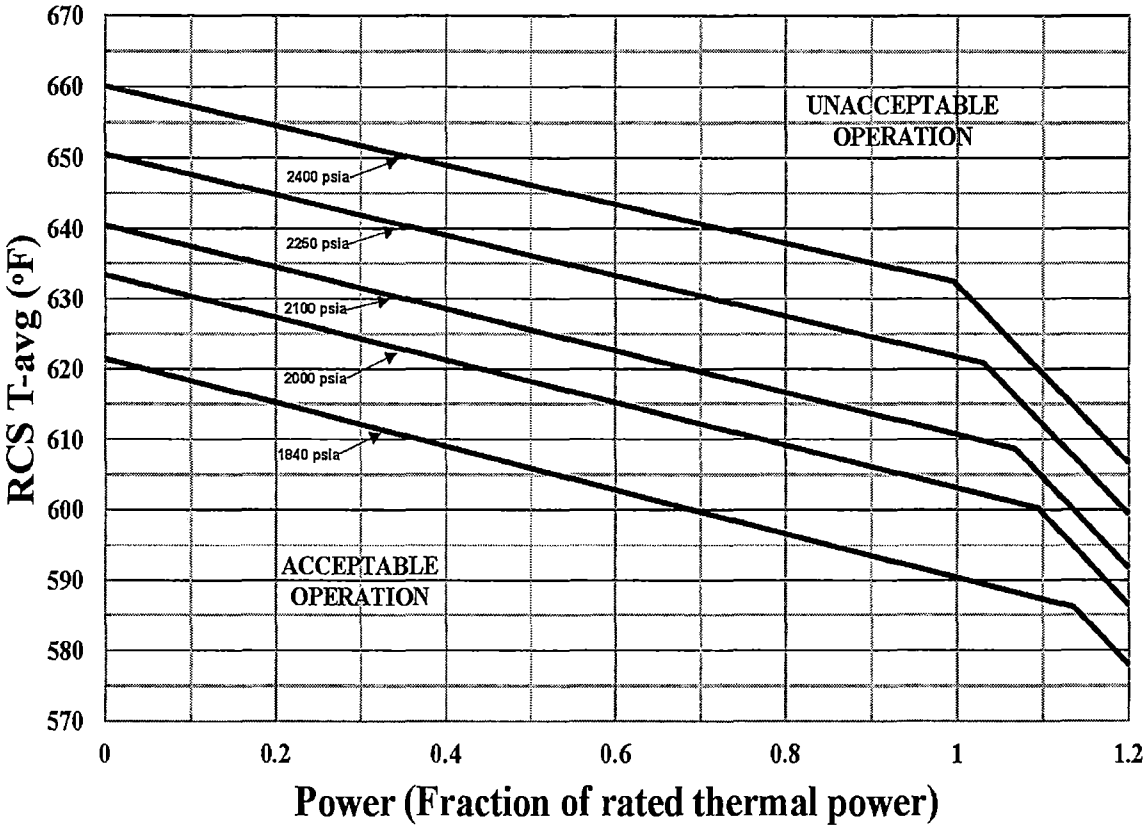
Where:

ΔT	=	Measured RCS ΔT, °F
ΔT_o	=	Indicated ΔT at RATED THERMAL POWER, °F
T	=	Average temperature, °F
T''	=	Nominal T_{avg} at RATED THERMAL POWER (≤ 575.4 °F)
K_4	≤	1.172 *
K_5	≥	0.0177/°F for increasing average temperature ; K_5 = 0 for decreasing average temperature
K_6	≥	0.0015/°F for T greater than T'' ; K_6 = 0 for T less than or equal to T''
$\frac{\tau_3 S}{1+\tau_3 S}$	=	The function generated by the rate lag controller for T_{avg} dynamic compensation
τ_3	=	Time constant utilized in the rate lag controller for T_{avg} $\tau_3 \geq$ 10 secs.
S	=	Laplace transform operator, sec^{-1}
$f_2(\Delta I)$	=	0.0

* This is a Safety Analysis value. Refer to Technical Requirements Manual for nominal value of this coefficient used in programming the trip setpoint.

FIGURE 6

Reactor Core Safety Limits



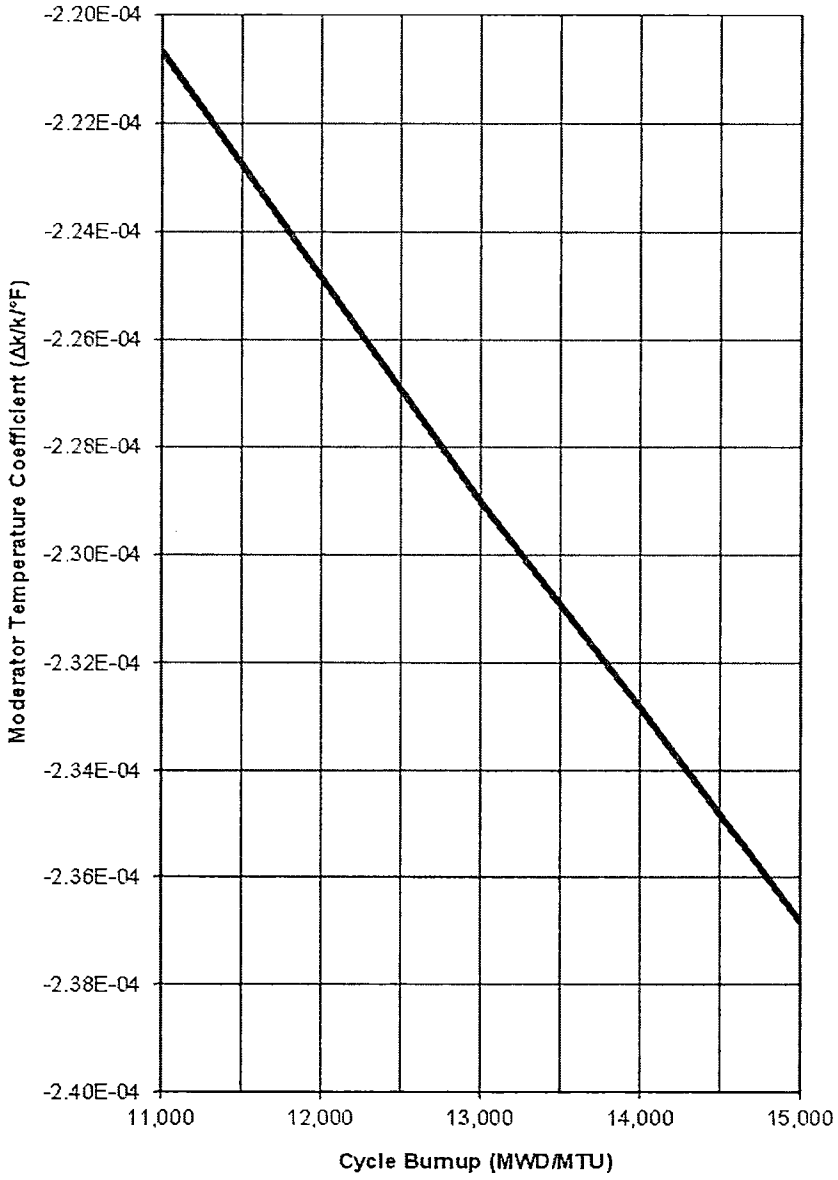
DESCRIPTION OF SAFETY LIMITS

Pressure (psia)	Power (frac)	Tavg (°F)	Power (frac)	Tavg (°F)	Power (frac)	Tavg (°F)	Power (frac)	Tavg (°F)
1840	0.0	621.48	0.02	620.86	1.136	586.17	1.2	577.94
2000	0.0	633.39	0.02	632.79	1.094	600.31	1.2	586.52
2100	0.0	640.44	0.02	639.85	1.068	608.72	1.2	591.77
2250	0.0	650.54	0.02	649.96	1.031	620.83	1.2	599.4
2400	0.0	660.08	0.02	659.52	0.996	632.42	1.2	606.63

UNIT 1 **Reactor Core Safety Limits**

FIGURE 7

Unit 1 Cycle 28 Predicted HFP ARO 300 PPM MTC Versus Burnup



Burnup (MWD/MTU)	MTC (pcm/°F)	MTC (Δk/k/°F)
11,000	-22.067	-2.2067E-04
12,000	-22.484	-2.2484E-04
13,000	-22.902	-2.2902E-04
14,000	-23.282	-2.3282E-04
15,000	-23.683	-2.3683E-04

TABLE 1

DONALD C. COOK UNIT 1 CYCLE 28
W(Z) FUNCTION

Node #	Height (ft)	Burnup (MWD/MTU) 150	1000	2000	4000	6000	8000
1	0.0	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000
2	0.2	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000
3	0.4	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000
4	0.6	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000
5	0.8	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000
6	1.0	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000
7	1.2	1.1004	1.0985	1.0971	1.0981	1.1026	1.1090
8	1.4	1.1005	1.0987	1.0975	1.0985	1.1028	1.1088
9	1.6	1.1003	1.0988	1.0977	1.0988	1.1027	1.1083
10	1.8	1.0999	1.0986	1.0977	1.0987	1.1024	1.1073
11	2.0	1.0992	1.0982	1.0974	1.0984	1.1016	1.1060
12	2.2	1.0984	1.0975	1.0970	1.0979	1.1006	1.1042
13	2.4	1.0973	1.0967	1.0963	1.0971	1.0993	1.1021
14	2.6	1.0960	1.0956	1.0955	1.0961	1.0977	1.0997
15	2.8	1.0945	1.0944	1.0944	1.0948	1.0958	1.0969
16	3.0	1.0926	1.0928	1.0929	1.0933	1.0936	1.0939
17	3.2	1.0907	1.0911	1.0914	1.0915	1.0912	1.0906
18	3.4	1.0895	1.0900	1.0903	1.0900	1.0888	1.0873
19	3.6	1.0891	1.0898	1.0902	1.0896	1.0876	1.0856
20	3.8	1.0887	1.0895	1.0900	1.0893	1.0871	1.0851
21	4.0	1.0882	1.0890	1.0896	1.0891	1.0875	1.0861
22	4.2	1.0875	1.0884	1.0891	1.0893	1.0885	1.0881
23	4.4	1.0868	1.0876	1.0884	1.0891	1.0893	1.0900
24	4.6	1.0859	1.0866	1.0873	1.0886	1.0898	1.0916
25	4.8	1.0848	1.0854	1.0862	1.0879	1.0901	1.0931
26	5.0	1.0836	1.0841	1.0849	1.0871	1.0902	1.0942
27	5.2	1.0825	1.0827	1.0834	1.0860	1.0899	1.0950
28	5.4	1.0811	1.0811	1.0815	1.0844	1.0893	1.0953
29	5.6	1.0795	1.0792	1.0795	1.0827	1.0883	1.0952
30	5.8	1.0775	1.0771	1.0775	1.0810	1.0871	1.0947

Top and bottom 10% of core excluded.

TABLE 1 (continued)
DONALD C. COOK UNIT 1 CYCLE 28
W(Z) FUNCTION

Node #	Height (ft)	Burnup (MWD/MTU) 150	1000	2000	4000	6000	8000
31	6.0	1.0754	1.0750	1.0753	1.0790	1.0856	1.0937
32	6.2	1.0738	1.0728	1.0726	1.0761	1.0832	1.0919
33	6.4	1.0725	1.0707	1.0697	1.0726	1.0800	1.0893
34	6.6	1.0708	1.0689	1.0677	1.0704	1.0776	1.0867
35	6.8	1.0688	1.0670	1.0660	1.0686	1.0751	1.0834
36	7.0	1.0669	1.0654	1.0646	1.0669	1.0728	1.0803
37	7.2	1.0652	1.0640	1.0633	1.0659	1.0718	1.0793
38	7.4	1.0646	1.0634	1.0629	1.0661	1.0731	1.0816
39	7.6	1.0683	1.0670	1.0665	1.0696	1.0763	1.0844
40	7.8	1.0734	1.0721	1.0715	1.0740	1.0798	1.0869
41	8.0	1.0777	1.0764	1.0756	1.0776	1.0827	1.0890
42	8.2	1.0819	1.0805	1.0796	1.0810	1.0853	1.0906
43	8.4	1.0858	1.0844	1.0833	1.0841	1.0874	1.0917
44	8.6	1.0894	1.0879	1.0866	1.0868	1.0892	1.0924
45	8.8	1.0927	1.0910	1.0896	1.0890	1.0905	1.0927
46	9.0	1.0956	1.0939	1.0923	1.0912	1.0917	1.0930
47	9.2	1.0981	1.0966	1.0952	1.0937	1.0933	1.0939
48	9.4	1.1001	1.0988	1.0977	1.0967	1.0970	1.0981
49	9.6	1.1020	1.1008	1.0997	1.0992	1.1003	1.1021
50	9.8	1.1036	1.1024	1.1014	1.1013	1.1031	1.1055
51	10.0	1.1052	1.1036	1.1023	1.1025	1.1050	1.1085
52	10.2	1.1059	1.1042	1.1030	1.1037	1.1070	1.1112
53	10.4	1.1061	1.1061	1.1063	1.1083	1.1115	1.1149
54	10.6	1.1136	1.1127	1.1120	1.1125	1.1145	1.1172
55	10.8	1.1120	1.1107	1.1099	1.1108	1.1142	1.1182
56	11.0	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000
57	11.2	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000
58	11.4	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000
59	11.6	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000
60	11.8	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000
61	12.0	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000

Top and bottom 10% of core excluded.

TABLE 1 (continued)
DONALD C. COOK UNIT 1 CYCLE 28
W(Z) FUNCTION

Node #	Height (ft)	Burnup (MWD/MTU) 10000	12000	14000	16000	16995
1	0.0	1.0000	1.0000	1.0000	1.0000	1.0000
2	0.2	1.0000	1.0000	1.0000	1.0000	1.0000
3	0.4	1.0000	1.0000	1.0000	1.0000	1.0000
4	0.6	1.0000	1.0000	1.0000	1.0000	1.0000
5	0.8	1.0000	1.0000	1.0000	1.0000	1.0000
6	1.0	1.0000	1.0000	1.0000	1.0000	1.0000
7	1.2	1.1160	1.1227	1.1298	1.1369	1.1403
8	1.4	1.1153	1.1215	1.1280	1.1345	1.1376
9	1.6	1.1142	1.1198	1.1256	1.1314	1.1343
10	1.8	1.1126	1.1175	1.1226	1.1277	1.1302
11	2.0	1.1105	1.1147	1.1189	1.1232	1.1253
12	2.2	1.1080	1.1114	1.1147	1.1181	1.1198
13	2.4	1.1050	1.1076	1.1100	1.1125	1.1138
14	2.6	1.1016	1.1033	1.1048	1.1064	1.1072
15	2.8	1.0979	1.0988	1.0995	1.1003	1.1007
16	3.0	1.0940	1.0939	1.0937	1.0936	1.0935
17	3.2	1.0898	1.0890	1.0881	1.0872	1.0868
18	3.4	1.0861	1.0853	1.0849	1.0844	1.0841
19	3.6	1.0845	1.0852	1.0872	1.0888	1.0895
20	3.8	1.0846	1.0868	1.0909	1.0945	1.0962
21	4.0	1.0864	1.0898	1.0954	1.1004	1.1027
22	4.2	1.0894	1.0935	1.0997	1.1053	1.1079
23	4.4	1.0923	1.0971	1.1037	1.1099	1.1128
24	4.6	1.0949	1.1003	1.1074	1.1141	1.1172
25	4.8	1.0973	1.1032	1.1106	1.1176	1.1210
26	5.0	1.0993	1.1057	1.1133	1.1206	1.1241
27	5.2	1.1009	1.1077	1.1154	1.1229	1.1265
28	5.4	1.1020	1.1091	1.1168	1.1244	1.1281
29	5.6	1.1026	1.1099	1.1174	1.1250	1.1288
30	5.8	1.1025	1.1099	1.1173	1.1248	1.1285

Top and bottom 10% of core excluded.

TABLE 1 (continued)
DONALD C. COOK UNIT 1 CYCLE 28
W(Z) FUNCTION

Node #	Height (ft)	Burnup (MWD/MTU) 10000	12000	14000	16000	16995
31	6.0	1.1018	1.1092	1.1164	1.1237	1.1273
32	6.2	1.1004	1.1077	1.1145	1.1216	1.1251
33	6.4	1.0983	1.1055	1.1118	1.1185	1.1218
34	6.6	1.0954	1.1023	1.1082	1.1145	1.1177
35	6.8	1.0914	1.0976	1.1029	1.1086	1.1115
36	7.0	1.0876	1.0935	1.0989	1.1045	1.1074
37	7.2	1.0867	1.0929	1.0987	1.1047	1.1077
38	7.4	1.0895	1.0954	1.1003	1.1055	1.1082
39	7.6	1.0918	1.0971	1.1012	1.1057	1.1080
40	7.8	1.0934	1.0980	1.1014	1.1052	1.1071
41	8.0	1.0946	1.0984	1.1010	1.1040	1.1056
42	8.2	1.0953	1.0982	1.1001	1.1023	1.1034
43	8.4	1.0954	1.0975	1.0986	1.1001	1.1009
44	8.6	1.0951	1.0964	1.0969	1.0976	1.0980
45	8.8	1.0944	1.0948	1.0943	1.0941	1.0941
46	9.0	1.0942	1.0945	1.0945	1.0946	1.0946
47	9.2	1.0951	1.0968	1.0993	1.1015	1.1026
48	9.4	1.0996	1.1014	1.1037	1.1059	1.1069
49	9.6	1.1041	1.1059	1.1077	1.1095	1.1104
50	9.8	1.1080	1.1098	1.1113	1.1129	1.1137
51	10.0	1.1116	1.1134	1.1145	1.1159	1.1166
52	10.2	1.1148	1.1165	1.1171	1.1180	1.1185
53	10.4	1.1175	1.1186	1.1186	1.1189	1.1192
54	10.6	1.1197	1.1215	1.1230	1.1247	1.1255
55	10.8	1.1214	1.1226	1.1226	1.1230	1.1233
56	11.0	1.0000	1.0000	1.0000	1.0000	1.0000
57	11.2	1.0000	1.0000	1.0000	1.0000	1.0000
58	11.4	1.0000	1.0000	1.0000	1.0000	1.0000
59	11.6	1.0000	1.0000	1.0000	1.0000	1.0000
60	11.8	1.0000	1.0000	1.0000	1.0000	1.0000
61	12.0	1.0000	1.0000	1.0000	1.0000	1.0000

Top and bottom 10% of core excluded.