

November 10, 2017

NRC 2017-0056 TS 5.6.4

U.S. Nuclear Regulatory Commission ATTN: Document Control Desk Washington DC 20555

Point Beach Nuclear Plant Unit 1 Docket No. 50-266 Renewed License No. DPR-24

Core Operating Limits Report (COLR) Unit 1 Cycle 38 (U1C38)

In accordance with the requirements of Point Beach Nuclear Plant (PBNP) Technical Specification 5.6.4, enclosed is TRM 2.1, COLR, Unit 1, Cycle 38.

The Enclosure to this letter contains the PBNP U1C38 COLR that was issued on October 16, 2017.

This letter contains no new regulatory commitments and no revisions to existing commitments.

Sincerely,

NextEra Energy Point Beach, LLC

Eric Schultz

Licensing Manager

Enclosure

CC:

Administrator, Region III, USNRC

Project Manager, Point Beach Nuclear Plant, USNRC Resident Inspector, Point Beach Nuclear Plant, USNRC

PSCW

NextEra Energy Point Beach, LLC

ENCLOSURE

NEXTERA ENERGY POINT BEACH, LLC POINT BEACH NUCLEAR PLANT, UNIT 1

CORE OPERATING LIMITS REPORT (COLR)
UNIT 1 CYCLE 38 (U1C38)

REVISION 19

1.0 CORE OPERATING LIMITS REPORT

This Core Operating Limits Report (COLR) for Point Beach Nuclear Plant has been prepared in accordance with the requirements of Technical Specification (TS) 5.6.4.

A cross-reference between the COLR sections and the PBNP Technical Specifications affected by this report is given below:

COLR Section	PBNP TS	Description	
2.1	2.1.1	Reactor Core Safety Limits	
2.2	3.1.1	Shutdown Margin	
	3.1.4	Rod Group Alignment Limits	
	3.1.5	Shutdown Bank Insertion Limits	
	3.1.6	Control Bank Insertion Limits	
	3.1.8	Physics Test Exceptions	
2.3	3.1.3	Moderator Temperature Coefficient	
2.4	3.1.5	Shutdown Bank Insertion Limit	
2.5	3.1.6	Control Bank Insertion Limits	
2.6	3.2.1	Nuclear Heat Flux Hot Channel Factor (FQ(Z))	
2.7	3.2.2	Nuclear Enthalpy Rise Hot Channel Factor (F ^N _{ΔH})	
2.8	3.2.3	Axial Flux Difference (AFD)	
2.9	3.3.1	Overtemperature ΔT Setpoint	
2.10	3.3.1	Overpower ΔT Setpoint	
2.11	3.4.1	RCS Pressure, Temperature, and Flow Departure from Nucleate Boiling (DNB) Limits	
2.12	3.9.1	Refueling Boron Concentration	
Figure 1	2.1.1	Reactor Core Safety Limits Curve	
Figure 2	3.1.1	Required Shutdown Margin	
Figure 3	3.1.6	Control Bank Insertion Limits	
Figure 4	3.2.1	Hot Channel Factor Normalized Operating Envelope (K(Z))	
Figure 5	3.2.1	Summary of W(Z) as a Function of Core Height	
Figure 5A	3.2.1	BOC Part-Power Summary of W(Z) as a Function of Core Height	
Figure 6	3.2.3	Flux Difference Operating Envelope	
Table 1	5.6.4	NRC Approved Methodologies for COLR Parameters	

2.0 OPERATING LIMITS

The cycle-specific parameter limits for the specifications listed in Section 1.0 are presented in the following subsections. These limits have been developed using the NRC approved methodologies specified in Technical Specification 5.6.4.

2.1 Reactor Core Safety Limits (TS 2.1.1)

The combination of THERMAL POWER, Reactor Coolant System (RCS) highest loop average temperature, and pressurizer pressure shall not exceed the limits specified in Figure 1.

Applicability: MODES 1 and 2

- 2.2 Shutdown Margin (TS 3.1.1 and referenced in TS 3.1.4, 3.1.5, 3.1.6, and 3.1.8)
 - 2.2.1 SDM shall be \geq 2.0% Δ k/k (see Figure 2).

Applicability: MODES 1, 2, and 3

2.2.2 SDM shall be $\geq 1\% \Delta k/k$.

Applicability: MODES 4 and 5

- 2.3 <u>Moderator Temperature Coefficient (TS 3.1.3)</u>
 - 2.3.1 The upper MTC limits shall be maintained within the limits.
 - 2.3.2 The maximum upper MTC limits shall be:

≤5 pcm/°F for power levels ≤70% RTP ≤0 pcm/°F for power levels >70% RTP

Applicability: MODE 1 and MODE 2 with $k_{eff} \ge 1.0$.

- 2.4 Shutdown Bank Insertion Limit (TS 3.1.5)
 - NOTE: This limit is not applicable while performing SR 3.1.4.2.
 - 2.4.1 Each shutdown bank shall be fully withdrawn.
 - 2.4.2 Fully withdrawn is defined as \geq 225 steps.

Applicability: MODES 1 and 2

2.5 Control Bank Insertion Limits (TS 3.1.6)

NOTE: This limit is not applicable while performing SR 3.1.4.2.

The control banks shall be within the insertion, sequence and overlap limits specified in Figure 3.

Applicability: MODE 1 and MODE 2 with $k_{eff} \ge 1.0$

2.6 Nuclear Heat Flux Hot Channel Factor (FQ(Z)) (TS 3.2.1)

The Heat Flux Hot Channel Factor shall be within the following limits:

$$F_Q(Z) \leq CF_Q * K(Z) / P$$

$$F_Q(Z) \le CF_Q * K(Z) / 0.5$$

for
$$P \le 0.5$$

Where P is the fraction of Rated Power at which the core is operating.

 $F_Q(Z)$ is both:

Steady State

$$F_Q^C(Z) = F_Q(Z) * 1.08$$

Transient

$$F_Q^W(Z) = F_Q^C(Z) * W(Z) / P \text{ for } P > 0.5$$

$$F_Q^W(Z) = F_Q^C(Z) * W(Z) / 0.5 \text{ for } P \le 0.5$$

 $CF_{Q} = 2.60$

K(Z) is the function in Figure 4

W(Z) is the function in Figures 5 and 5A.

The following F_0 penalty factors are applicable to Cycle 38.

Cycle Burnup	F ^W _Q (Z) Penalty
(MWD/MTU)	Factors
BOL to EOL	1.02

Applicability: MODE 1

2.7 Nuclear Enthalpy Rise Hot Channel Factor (F^N_{AH}) (TS 3.2.2)

The Nuclear Enthalpy Rise Hot Channel Factor shall be within the following limit:

2.7.1
$$F_{\Delta H}^{N} \le 1.68 \times [1 + 0.3(1-P)]$$

where: P is the fraction of Rated Power at which the core is operating.

Applicability: MODE 1

2.8 <u>Axial Flux Difference (AFD) (TS 3.2.3)</u>

The AFD target band is $\pm 5\%$.

The AFD Acceptability Operation Limits are provided in Figure 6.

Applicability: MODE 1 with THERMAL POWER ≥15% RTP

2.9 Overtemperature ΔT Setpoint (TS 3.3.1, Table 3.3.1-1 note 1)

Overtemperature ΔT setpoint parameter values (for 1800 MWt core power):

 ΔT_0 = indicated ΔT at RTP, °F

T = indicated RCS average temperature, °F

T′ ≤ 576.0°F

P = pressurizer pressure, psig

 $P' \geq 2235 \text{ psig}$

 $K_1 \leq 1.170 (NTSP)^1$

 $K_1 \leq 1.183 (AV)^2$

 $K_2 \geq 0.016$

 $K_3 \geq 0.000811$

 τ_1 = 40 sec

 $\tau_2 = 8 \sec$

 $\tau_3 = 4 \sec$

 τ_4 = 2 sec

 $f(\Delta I)$ is a function of the indicated difference between top and bottom detectors of the power-range nuclear ion chambers; with gains to be selected based on measured instrument response during plant startup tests, where q_t and q_b are the percent power in the top and bottom halves of the core respectively, and $q_t + q_b$ is total core power in percent of RTP, such that:

- 2.9.1 For q_t q_b within -12, +6 percent, $f(\Delta I) = 0$.
- 2.9.2 For each percent that the magnitude of q_t q_b exceeds +6 percent, the ΔT trip setpoint shall be automatically reduced by an equivalent of 2.00 percent of Rated Power.
- 2.9.3 For each percent that the magnitude of q_t q_b exceeds -12 percent, the ΔT trip setpoint shall be automatically reduced by an equivalent of 2.69 percent of Rated Power.

Applicability: MODES 1 and 2

¹ Nominal Setpoint Value

² Allowable Value

2.10 Overpower ΔT Setpoint (TS 3.3.1, Table 3.3.1-1 note 2)

Overpower ΔT setpoint parameter values (for 1800 MWt core power):

 ΔT_{O} = indicated ΔT at RTP, °F Τ = indicated RCS average temperature, °F T' 576.0°F \leq K₄ 1.083 (NTSP)1 ≤ 1.096 (AV)² K_4 \leq 0.0 for increasing T K_5 ≥ K_5 = 0.0 for decreasing T Ka $0.00123 \text{ for } T \ge T'$ ≥ K_6 0.0 for T < T'0 sec ≥ τ5 = 4 sec τз 2 sec =

Applicability: MODES 1 and 2

2.11 RCS Pressure, Temperature, and Flow Departure from Nucleate Boiling (DNB) Limits (TS 3.4.1)

- 2.11.1 T_{avg} shall be $\leq 577^{\circ}F$.
- 2.11.2 Pressurizer pressure shall be maintained ≥2205 psig during operation.

NOTE: Pressurizer pressure limit does not apply during:

- 1) THERMAL POWER ramp >5% RTP per minute; or
- 2) THERMAL POWER step >10% RTP.
- 2.11.3 Reactor Coolant System raw measured Total Flow Rate shall be maintained ≥186,000 gpm.

Applicability: MODE 1

2.12 Refueling Boron Concentration (TS 3.9.1)

Boron concentrations of the Reactor Coolant System, the refueling canal, and the refueling cavity shall be maintained ≥2350 ppm.

Applicability: MODE 6

¹ Nominal Setpoint Value

² Allowable Value

FIGURE 1
REACTOR CORE SAFETY LIMITS CURVE

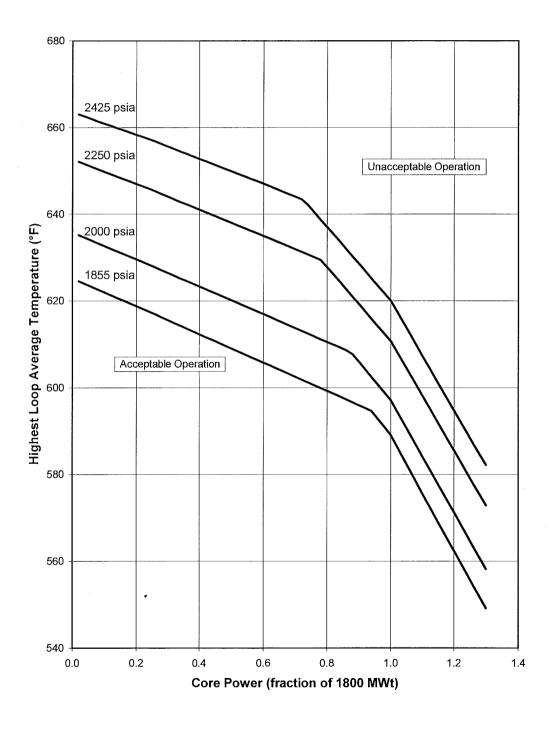
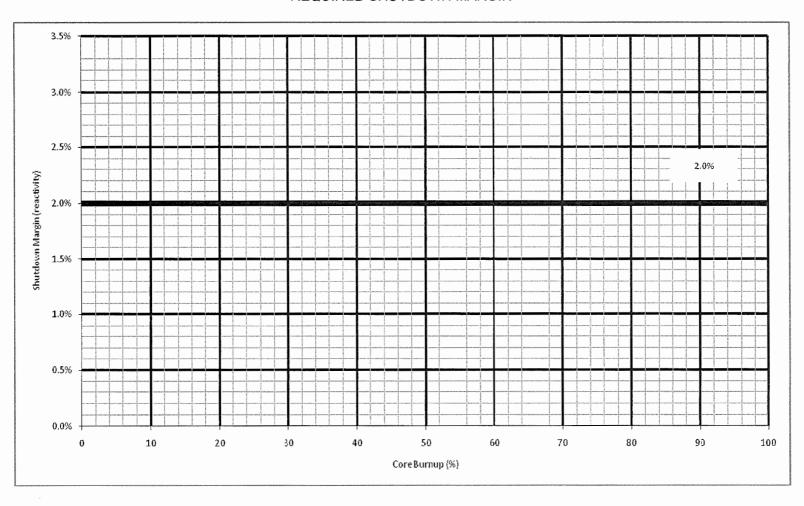
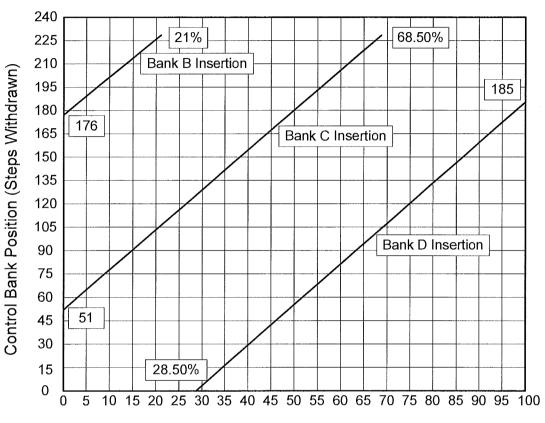


FIGURE 2 REQUIRED SHUTDOWN MARGIN



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FIGURE 3 CONTROL BANK INSERTION LIMITS



Power Level (% of Rated Power)

NOTE: The Figure is applicable for any fully withdrawn position of \geq 225 steps (Limits are always considered met when withdrawn position is \geq 225 steps).

FIGURE 4
HOT CHANNEL FACTOR NORMALIZED OPERATING ENVELOPE (K(Z))

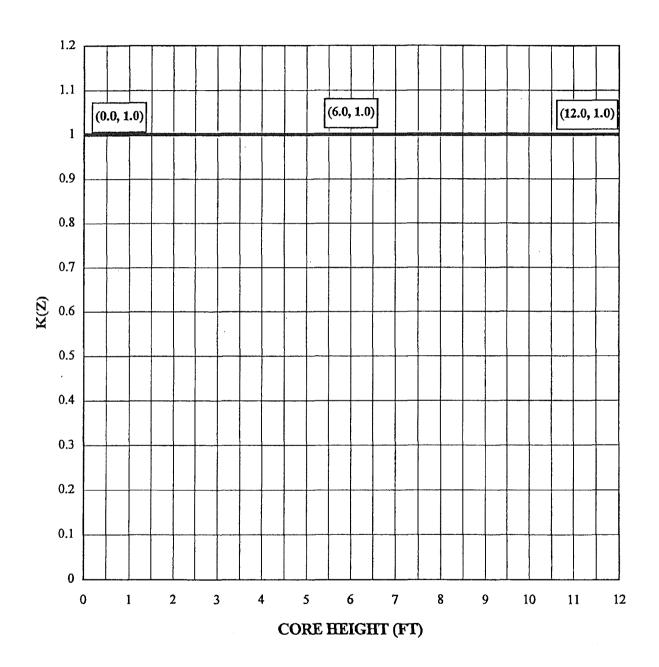


FIGURE 5
Summary of W(Z) as a Function of Core Height
(Top 15% and Bottom 12% Excluded)

	W(Z)			
Height (feet)	150 MWD/MTU	8000 MWD/MTU	16000 MWD/MTU	
0.0	1.0000	1.0000	1.0000	
0.2	1.0000	1.0000	1.0000	
0.4	1.0000	1.0000	1.0000	
0.6	1.0000	1.0000	1.0000	
0.8	1.0000	1.0000	1.0000	
1.0	1.0000	1.0000	1.0000	
1.2	1.0000	1.0000	1.0000	
1.4	1.0890	1.1025	1.1116	
1.6	1.0901	1.1027	1.1106	
1.8	1.0910	1.1025	1.1091	
2.0	1.0916	1.1018	1.1070	
2.2	1.0920	1.1007	1.1044	
2.4	1.0921	1.0992	1.1014	
2.6	1.0920	1.0973	1.0980	
2.8	1.0916	1.0951	1.0942	
3.0	1.0911	1.0926	1.0902	
3.2	1.0904	1.0897	1.0860	
3.4	1.0895	1.0867	1.0829	
3.6	1.0884	1.0838	1.0828	
3.8	1.0871	1.0819	1.0834	
4.0	1.0856	1.0812	1.0841	
4.2	1.0840	1.0811	1.0846	
4.4	1.0824	1.0809	1.0849	
4.6	1.0811	1.0806	1.0850	
4.8	1.0796	1.0802	1.0849	
5.0	1.0778	1.0795	1.0845	
5.2	1.0759	1.0787	1.0838	
5.4	1.0738	1.0776	1.0828	
5.6	1.0717	1.0763	1.0814	
5.8	1.0694	1.0749	1.0797	
6.0	1.0669	1.0737	1.0776	

FIGURE 5 (con't) Summary of W(Z) as a Function of Core Height (Top 15% and Bottom 12% Excluded)

	W(Z)			
Height (feet)	150 MWD/MTU	8000 MWD/MTU	16000 MWD/MTU	
6.2	1.0640	1.0722	1.0750	
6.4	1.0609	1.0704	1.0723	
6.6	1.0584	1.0682	1.0714	
6.8	1.0574	1.0647	1.0733	
7.0	1.0563	1.0651	1.0771	
7.2	1.0557	1.0696	1.0804	
7.4	1.0570	1.0736	1.0836	
7.6	1.0623	1.0775	1.0864	
7.8	1.0679	1.0811	1.0887	
8.0	1.0731	1.0844	1.0906	
8.2	1.0783	1.0874	1.0921	
8.4	1.0832	1.0901	1.0933	
8.6	1.0880	1.0925	1.0941	
8.8	1.0926	1.0946	1.0946	
9.0	1.0969	1.0965	1.0949	
9.2	1.1008	1.0985	1.0950	
9.4	1.1045	1.1001	1.0947	
9.6	1.1084	1.1014	1.0941	
9.8	1.1121	1.1023	1.0935	
10.0	1.1155	1.1031	1.0928	
10.2	1.1186	1.1033	1.0919	
10.4	1.0000	1.0000	1.0000	
10.6	1.0000	1.0000	1.0000	
10.8	1.0000	1.0000	1.0000	
11.0	1.0000	1.0000	1.0000	
11.2	1.0000	1.0000	1.0000	
11.4	1.0000	1.0000	1.0000	
11.6	1.0000	1.0000	1.0000	
11.8	1.0000	1.0000	1.0000	
12.0	1.0000	1.0000	1.0000	

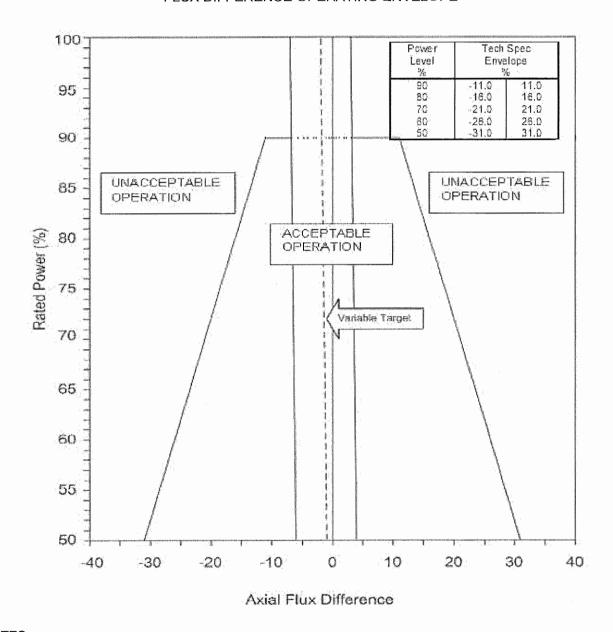
FIGURE 5A BOC Part-Power Summary of W(Z) as a Function of Core Height (D-Bank \leq 205 steps) (Top 15% and Bottom 12% Excluded)

Height (feet)	Part-Power W(Z) with Correction Factor (excluding power ratio)
0.0	75% Power
0.0	1,0000
0.2	1.0000
0.4	1.0000
0.6	1.0000
0.8	1.0000
1.0	1.0000
1.2	1.0000
1.4	1.1896
1.6	1.1870
1.8	1.1844
2.0	1.1807
2.2	1.1764
2.4	1.1720
2.6	1.1677
2.8	1.1630
3.0	1.1580
3.2	1.1529
3.4	1.1481
3.6	1.1431
3.8	1.1378
4.0	1,1323
4.2	1.1266
4.4	1.1208
4.6	1.1153
4.8	1.1096
5.0	1.1037
5.2	1.0976
5.4	1.0910
5.6	1.0843
5.8	1.0773
6.0	1.0702

FIGURE 5A (con't) BOC Part-Power Summary of W(Z) as a Function of Core Height (D-Bank \leq 205 steps) (Top 15% and Bottom 12% Excluded)

Height (feet)	Part-Power W(Z) with Correction Factor (excluding power ratio)	
	75% Power	
6.2	1.0626	
6.4	1.0548	
6.6	1.0476	
6.8	1.0420	
7.0	1.0363	
7.2	1.0310	
7.4	1.0275	
7.6	1.0277	
7.8	1.0282	
8.0	1.0285	
8.2	1.0287	
8.4	1.0284	
8.6	1.0279	
8.8	1.0274	
9.0	1.0269	
9.2	1.0263	
9.4	1.0254	
9.6	1.0248	
9.8	1.0244	
10.0	1.0245	
10.2	1.0251	
10.4	1.0000	
10.6	1.0000	
10.8	1.0000	
11.0	1.0000	
11.2	1.0000	
11.4	1.0000	
11.6	1.0000	
11.8	1.0000	
12.0	1.0000	

FIGURE 6
FLUX DIFFERENCE OPERATING ENVELOPE



NOTES:

- 1) This figure represents the Constant Axial Offset Control (CAOC) band used in safety analyses, it may be administratively tightened depending on in-core flux map results. Refer to Figure 2 of Reactor Operating Data (ROD) 1.2 for the administrative limit.
- 2) The AFD may deviate outside the target band with THERMAL POWER < 50% RTP.
- 3) The AFD target band is +/-5% for THERMAL POWER ≥15% RTP.

TABLE 1 NRC APPROVED METHODOLOGIES FOR COLR PARAMETERS

COLR Section	Parameter	NRC Approved Methodology
All	Reactor Thermal Output	Caldon, Inc., Engineering Report-80P, "TOPICAL REPORT: Improving Thermal Power Accuracy and Plant Safety While Increasing Operating Power Level Using the LEFMê System," Revision 0, Mar 1997.
		Caldon, Inc., Engineering Report-160P, "Supplement to Topical Report ER-80P: Basis for a Power Uprate With the LEFMê System," Revision 0, May 2000.
	Fuel Assembly	WCAP-12610-P-A, "VANTAGE+ Fuel Assembly Reference Core Report," April 1995.
		WCAP-12610-P-A & CENPD-404-P-A, Addendum 1- A, "Optimized ZIRLO TM ," July 2006.
2.1	Reactor Core Safety Limits	WCAP-9272-P-A, "Westinghouse Reload Safety Evaluation Methodology," July 1985.
2.2	Shutdown Margin	WCAP-9272-P-A, "Westinghouse Reload Safety Evaluation Methodology," July 1985.
2.3	Moderator Temperature Coefficient	WCAP-9272-P-A, "Westinghouse Reload Safety Evaluation Methodology," July 1985.
2.4	Shutdown Bank Insertion Limit	WCAP-9272-P-A, "Westinghouse Reload Safety Evaluation Methodology," July 1985.
2.5	Control Bank Insertion Limits	WCAP-9272-P-A, "Westinghouse Reload Safety Evaluation Methodology," July 1985.
2.6	Nuclear Heat Flux Hot Channel Factor (F _Q (Z))	WCAP-8403 (non-proprietary), "Power Distribution Control and Load Following Procedures," September 1974.
		WCAP-14449-P-A, "Application of Best Estimate Large Break LOCA Methodology to Westinghouse PWRs with Upper Plenum Injection," Revision 1, October 1999 (cores containing 422V + fuel).
		WCAP-16009-P-A, "Realistic Large-Break LOCA Evaluation Methodology Using the Automated Statistical Treatment of Uncertainty Method (ASTRUM)," January 2005.
		WCAP-10054-P-A, "Westinghouse Small Break ECCS Evaluation Model Using the NOTRUMP Code," August 1985.
		WCAP-10054-P-A, "Addendum to the Westinghouse Small Break ECCS Evaluation Model Using the NOTRUMP Code: Safety Injection into the Broken Loop and COSI Condensation Model," Addendum 2, Revision 1, July 1997.

COLR Section	Parameter	NRC Approved Methodology
2.7	Nuclear Enthalpy Rise Hot Channel Factor (F ^N _{ΔH})	WCAP-9272-P-A, "Westinghouse Reload Safety Evaluation Methodology," July 1985.
		WCAP-16259-P-A, "Westinghouse Methodology for Applications of 3-D Transient Neutronics to Non-LOCA Accident Analysis," August 2006.
2.8	Axial Flux Difference (AFD)	WCAP-8403 (non-proprietary), "Power Distribution Control and Load Following Procedures," September 1974.
		NS-TMA-2198, Westinghouse to NRC Letter Attachment: "Operation and Safety Analysis Aspects of an Improved Load Follow Package," January 31, 1980.
		NS-CE-687, Westinghouse to NRC Letter, "Power Distribution Control Analysis," July 16, 1975.
2.9	Overtemperature ΔT Setpoint	WCAP-8745-P-A, "Design Bases for the Thermal Overpower ∆T and Thermal Overtemperature ∆T Trip Functions," September 1986.
2.10	Overpower ΔT Setpoint	WCAP-8745-P-A, "Design Bases for the Thermal Overpower ∆T and Thermal Overtemperature ∆T Trip Functions," September 1986.
2.11	RCS Pressure, Temperature, and Flow Departure from Nucleate Boiling (DNB) Limits	WCAP-11397-P-A, "Revised Thermal Design Procedure," April 1989, for those events analyzed using RTDP.
		WCAP-14787-P, Rev. 3, "Westinghouse Revised Thermal Design Procedure Instrument Uncertainty Methodology for Point Beach Units 1 & 2 Power Uprate 1775 MWt Core Power with Feedwater Venturis, or 1800 MWt Core Power with LEFM on Feedwater Header)," February 2009.
		WCAP-9272-P-A, "Westinghouse Reload Safety Evaluation Methodology," July 1985 for those events not utilizing RTDP.
2.12	Refueling Boron Concentration	WCAP-9272-P-A, "Westinghouse Reload Safety Evaluation Methodology," July 1985.