### Thermal Loads for Spent Fuel Dry Casks

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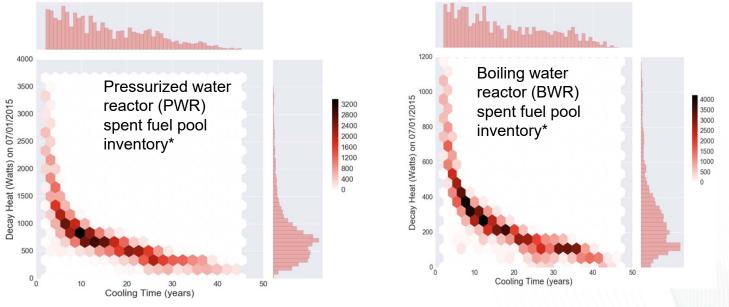
### Analysis tools and methods for thermal analyses are mature; accuracy is biased by how they are being applied

- Temperature analysis for dry storage systems is comprised of two primary models
  - Spent nuclear fuel (SNF) assembly decay heat generation rate
  - Heat transfer model
- Current design basis calculations bias the model results to be conservatively hotter
  - Input choices
  - Reverse engineer maximum allowable decay heat to achieve target component temperatures
- Overpredicting temperatures is undesirable when considering aging management
  - Stress corrosion cracking of canisters
  - Seeking the lowest temperatures during transportation after extended storage
- Need to calculate accurate temperatures as they change with time and apply uncertainty appropriately (in positive or negative direction) depending on application of interest



### **SNF** continues to produce decay heat after discharge from the reactor

- Recoverable energy released from the decay of radionuclides in fuel after its discharge from the reactor
- Driven by the isotopic composition in fuel at the end of irradiation
- Changes with decay time after discharge (cooling time)



\**Nuclear Fuel Data Survey Form GC-859*, Energy Information Administration (EIA), US Department of Energy. <u>http://www.eia.gov/survey/form/gc\_859/proposed/form.pdf</u>



### Thermal analyses for dry storage systems use a design basis approach to meet temperature criteria

- Decay heat from SNF is a limiting design boundary condition input for calculating component (e.g., cladding) temperatures for dry storage systems
- Decay heat removal effectiveness depends on system design
- Large margin exists between design basis limits and how casks are loaded

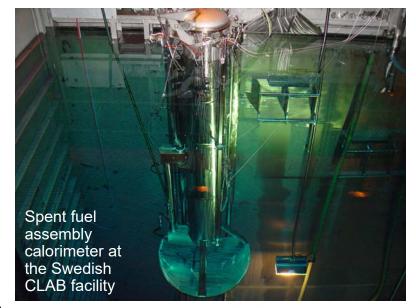
35-41	0	1	45	121	108	26	10	0		300	
w) 30-35	2	82	88	162	122	28	1	0			
COC Decay Heat Limit (kw) 10 10-15 15-20 20-25 25-30 30	5	39	19	0	0	0	0	0	Loaded Systems Count	240	
	55	181	339	122	0	0	0	0		180	
cay H 15-20	2	137	41	13	0	0	0	0	ystem		
10-15 De	5	48	0	0	0	0	0	0	ded S	120	
CO 5-10	8	1	0	0	0	0	0	0	Loa	60	
0-5	10	0	0	0	0	0	0	0		0	
	0-5 Deca	5-10 ay Hea	10-15 at Mar	15-20 gin (k		25-30 In-Se	30-35 ervice	35-40 Date		0	

Data extracted from Used Nuclear Fuel-Storage, Transportation & Disposal Analysis Resource and Data System (UNF-ST&DARDS).



# Experimental programs have measured SNF assembly decay heat for years (>160 assemblies measured\*)

- Calorimeters used to measure actual SNF assemblies
  - General Electric Morris Operation
  - Hanford Engineering Development Laboratory
  - Central Interim Storage Facility for Spent Fuel (CLAB) located in Sweden
- Measured assemblies include a wide range of assembly design types, enrichments, burnup, and cooling times



- CE 14 × 14, W 14 × 14, W 15 × 15, W 17 × 17, GE 7 × 7, ABB 8 × 8, SVEA 64 (8 × 8), ABB 9 × 9, SVEA 100 (10 × 10)
- Initial enrichment range (wt% <sup>235</sup>U): 2.09–3.40
- Burnup (GWd/MTU): 19.9–51.0
- Cooling time<sup>\*</sup>: 2–28 years

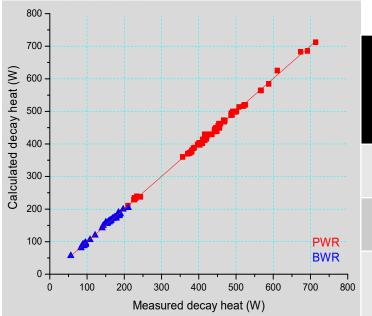
\*Small irradiated fuel samples have been used for cooling times less than 1 day and used to support development of decay heat standards for computer code validation (Information summarized from NUREG/CR-6999)



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### **Computational models have been validated using the decay heat measurements**

Excellent agreement between measured and calculated results when detailed assembly-specific operating history information is modeled



Summary of SCALE 6.1.3 code system validation results

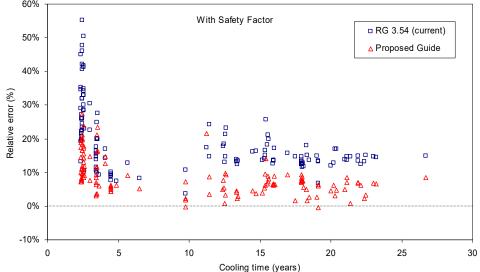
Data set	No. of measurements	C/	3	Residual (W)		
		mean	σ	mean	σ	
PWR	71	1.002	0.012	0.57	4.91	
BWR	50	0.997	0.024	-0.25	3.36	
PWR+ BWR	121	1.000	0.017	0.23	4.34	

Calculated vs measured decay heat



## Different methods are used to estimate assembly decay heat for dry storage loading

- Simplified approaches vs complex models and calculations
  - Regulatory Guide 3.54
  - ANSI/ANS-5.1
  - Branch technical position ASB 9-2
  - ORIGEN
  - Other software
- Trade precision and accuracy to simplify the method
  - Design limits have focused on bounding hot (one-sided tradeoff)
  - Applicability to aging management?



#### Comparison between measured decay heat values and the methodology in Reg. Guide 3.54 (current and proposed)\*

\*Safety factor used to account for bias and uncertainty; relative error is higher for shorter cooling times



### **Research is underway to reduce application** model bias and generate realistic temperature predictions

- High burnup spent fuel data project (EPRI 2014)
  - Integral experiment to validate temperature modeling predictions indirectly via thermocouple lances inserted into an SNF dry storage cask
- BWR cask simulator (SAND2015-10256)
  - Electrical heaters instrumented in a controlled environment
- Uncertainty analysis between application models and detailed models
  - Identification of key parameters that affect accuracy (short-cooled) versus long-cooled)
- Enhancement of methods to develop accurate results and apply uncertainty appropriately for the specific application (e.g., storage, transport, aging management) OAK RIDGE National Laboratory

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- NUREG/CR-6999. "Technical Basis for a Proposed Expansion of Regulatory Guide 3.54 –Decay Heat Generation in an Independent Spent Fuel Storage installation." ML100850213.
- Nuclear Technology, Special Issue on UNF-ST&DARDS, Vol. 199, September 2017.
- "Nuclear Fuel Data Survey Form GC-859," Energy Information Administration (EIA), U.S. Department of Energy. http://www.eia.gov/survey/form/gc\_859/proposed/form.pdf
- EPRI 2014. High Burnup Dry Storage Cask Research and Development Project: Final Test Plan





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