



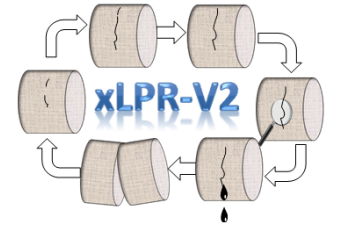
Extremely Low Probability of Rupture (xLPR) Project

xLPR Code Acceptance Criteria

David Rudland
USNRC

xLPR External Review Board Meeting
February 20, 2013

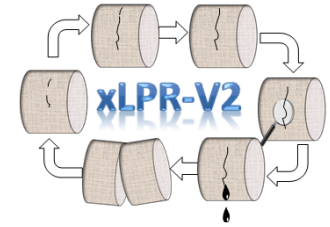
Acceptance Group Members



- **Bob Hardies - NRC**
- **David Rudland - NRC**
- **Tim Lupold - NRC**
- **Robin Dyle - EPRI**
- **Al Csontos - NRC**
- **Stephen Dinsmore - NRC**

Topics of on-going Discussion

Three Questions

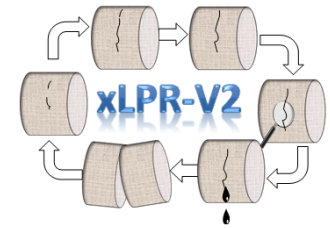


- **What constitutes acceptable inputs?**
 - Code model input, data, configuration
 - Technical basis for the code
 - Code structure

TODAY'S FOCUS

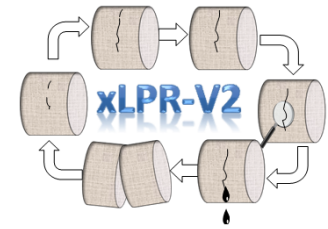
- **What constitutes acceptable results?**
 - Guidance on risk limits as an NRC regulatory position for LBB
 - In other than regulatory applications other criteria may apply
- **What constitutes an acceptable delivery vehicle for this information?**
 - Regulatory guide
 - Lead plant application

Initial Application is for LBB

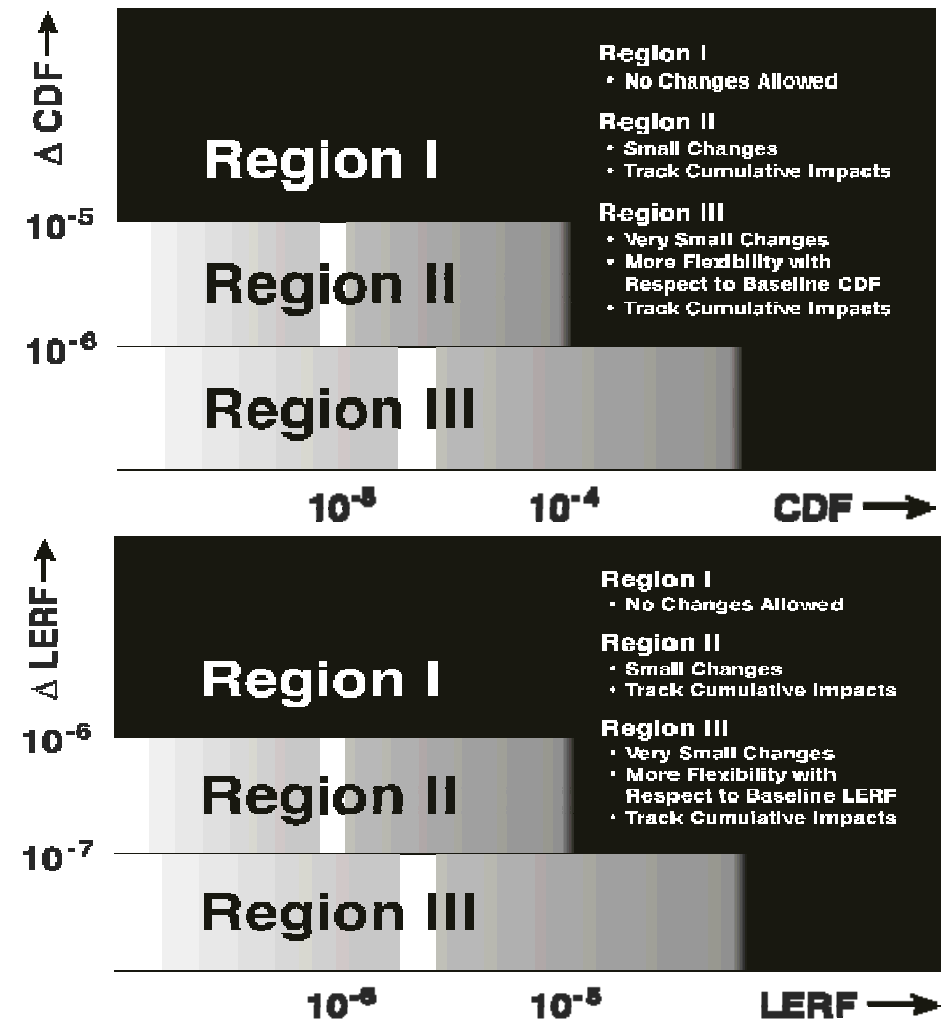


- **Acceptance Criteria Still Under Development**
 - Nascent ideas are presented here, still a work in progress
- **We expect that the xLPR project will evaluate changes in risk (Δ -Risk)**
 - Is stress corrosion cracking active (or not)
 - Changes in inspection periodicity
 - Mitigation activities
 - Repairs

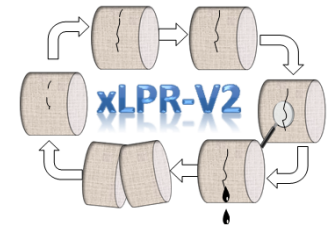
Acceptance Criteria being Considered



- Regulatory Guide 1.174 provides guidance on
 - Core Damage Frequency (CDF) and Δ CDF
 - Large Early Release Frequency (LERF) and Δ LERF
- Advantage
 - Criteria developed
 - NRC has experience with RG1.174 approach

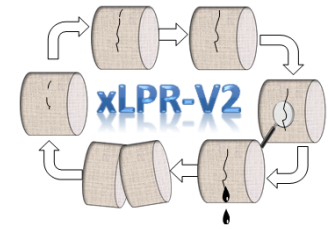


Thoughts on xLPR Outputs & Comparison to RG 1.174 Limits



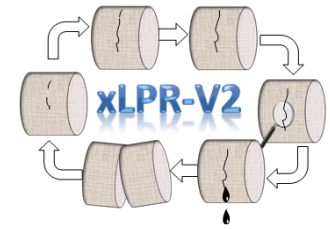
- xLPR output: failure probability/year
- Dependencies of interest
 - Effect of operational time
 - Effect of break size
- Quantiles
 - Mean values of failure probability used far from RG limits
 - Close to limits uncertainties need to be quantified (xLPR does this)
- Conversion of failure probability to CDF to compare with RG1.174 limits
 - Multiply failure probability by conditional core damage probability
 - Distinguish between different break sizes
 - e.g., $CDF_{total} = 10^{-2} * LBLOCA + 10^{-4} * MBLOCA + 10^{-3} * SBLOCA$
- LERF evaluation also needed
 - Conversion from CDF may be justified
 - e.g., $LERF = CDF \div X$
 - Magnitude of X depends on effect of pipe break on containment. As effect increases, so will X.

What Constitutes Failure?



- **Definition: Any LOCA is a failure**
- **Potential mitigating factors**
 - **Not all cracks progress rapidly to LOCA or rupture**
 - Some leak
 - Cracks that leak noticeably for a long time would be repaired before they rupture, so should not be counted as ruptures
 - **Crack has to leak noticeably**
 - Operators can reliably detect 10 GPM
 - **Cracks that leak >10 GPM get repaired if there is sufficient time between leak detection and rupture**

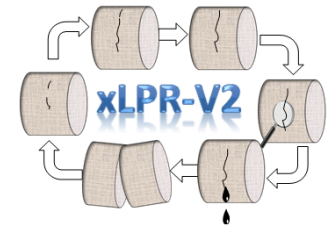
How Much Time Between Leak and Rupture?



Some definitions considered so far:

- If, at the next time step, a LOCA has occurred, then there was not enough time to notice the leak and shut down
- Define LOCA as a leak greater than charging pump capacity
 - Plant specific, but typically 55 GPM
 - Therefore recommend selecting 50 GPM
- If, at the next time step the leak rate $>50\text{GPM}$, then a LOCA has occurred

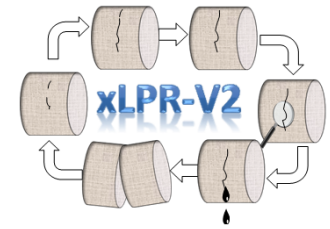
Failure Criteria



Some definitions considered so far:

- **One candidate**
 - Leak > 50 GPM AND
 - Leak at t-1 < 10 GPM
- **Another candidate**
 - Leak >50 GPM AND
 - Leak at t-2 < 10 GPM

Summary



- Ideas thus far
 - Use established guidelines of RG1.174 for CDF & LERF
 - Define failure as any LOCA
 - Define a LOCA as being a leak rate exceeding the capacity of a single charging pump
- Work is continuing