



GINNA STATION

PTLR
Revision 2

**RCS PRESSURE AND TEMPERATURE
LIMITS REPORT
(PTLR)**


Responsible Manager

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Effective Date

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R.E. Ginna Nuclear Power Plant
RCS Pressure and Temperature Limits Report

Revision 2

Note: This report is not part of the Technical Specifications. This report is referenced in the Technical Specifications.

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R.E. Ginna Nuclear Power Plant
Pressure and Temperature Limits Report

1.0 RCS Pressure and Temperature Limits Report (PTLR)

This Pressure and Temperature Limits Report (PTLR) for Ginna Station has been prepared in accordance with the requirements of Technical Specification 5.6.6. Revisions to the PTLR shall be provided to the NRC after issuance.

The Technical Specifications addressed in this report are listed below:

- 3.4.3 RCS Pressure and Temperature (P/T) Limits
- 3.4.6 RCS Loops - MODE 4
- 3.4.7 RCS Loops - MODE 5, Loops Filled
- 3.4.10 Pressurizer Safety Valves
- 3.4.12 Low Temperature Overpressure Protection (LTOP) System

2.0 OPERATING LIMITS

The cycle-specific parameter limits for the specifications listed in Section 1.0 are presented in the following subsections. All changes to these limits must be developed using the NRC approved methodologies specified in Technical Specification 5.6.6. These limits have been determined such that all applicable limits of the safety analysis are met. All items that appear in capitalized type are defined in Technical Specification 1.1, "Definitions."

2.1 RCS Pressure and Temperature Limits (LCO 3.4.3 and LCO 3.4.12) (Reference 1)

2.1.1 The RCS temperature rate-of-change limits are:

- a. A maximum heatup of 60°F per hour.
- b. A maximum cooldown of 100°F per hour.

2.1.2 The RCS P/T limits for heatup and cooldown are specified by Figures 1 and 2, respectively.

2.1.3 The minimum boltup temperature, using the methodology of Reference 4, Enclosure 2 is 60°F.

2.2 Low Temperature Overpressure Protection System Enable Temperature (LCOs 3.4.6, 3.4.7, 3.4.10 and 3.4.12) (Methodology of Reference 3, Attachment VI and Reference 6, as calculated in Reference 7).

2.2.1 The enable temperature for the Low Temperature Overpressure Protection System is 322°F.

2.3 Low Temperature Overpressure Protection System Setpoints (LCO 3.4.12)

2.3.1 Pressurizer Power Operated Relief Valve Lift Setting Limits (Methodology of Reference 3, Attachment VI and Reference 6, as calculated in Reference 3, Attachment VII).

The lift setting for the pressurizer Power Operated Relief Valves (PORVs) is ≤ 411 psig (includes instrument uncertainty).

3.0 REACTOR VESSEL MATERIAL SURVEILLANCE PROGRAM

The reactor vessel material irradiation surveillance specimens shall be removed and examined to determine changes in material properties. The removal schedule is provided in Table 1. The results of these examinations shall be used to update Figures 1 and 2.

The pressure vessel steel surveillance program (Ref. 5) is in compliance with Appendix H to 10 CFR 50, entitled, "Reactor Vessel Radiation Surveillance Program." The material test requirements and the acceptance standard utilize the reference nil-ductility temperature, RT_{NDT} , which is determined in accordance with ASTM E208. The empirical relationship between RT_{NDT} and the fracture toughness of the reactor vessel steel is developed in accordance with Appendix G, "Protection Against Non-Ductile Failure," to section III of the ASME Boiler and Pressure Vessel Code. The surveillance capsule removal schedule meets the requirements of ASTM E185-82.

As shown by Reference 1 (specifically its Reference 51), the reactor vessel material irradiation surveillance specimens indicate that the surveillance data meets the credibility discussion presented in Regulatory Guide 1.99 revision 2 where:

1. The capsule materials represent the limiting reactor vessel material.
2. Charpy energy vs. temperature plots scatter are small enough to permit determination of 30 ft-lb temperature and upper shelf energy unambiguously.
3. The scatter of ΔRT_{NDT} values are within the best fit scatter limits as shown on Table 2. The only exception is with respect to the Intermediate Shell which is not the limiting reactor vessel material.
4. The Charpy specimen irradiation temperature matches the reactor vessel surface interface temperature within $\pm 25^{\circ}\text{F}$.
5. The surveillance data falls within the scatter band of the material database.

4.0 SUPPLEMENTAL DATA INFORMATION AND DATA TABLES

4.1 The RT_{PTS} value for Ginna Station limiting beltline material is 256.6°F for 32 EFPY per Reference 1.

4.2 Tables

Table 2 contains a comparison of measured surveillance material 30 ft-lb transition temperature shifts and upper shelf energy decreases with Regulatory Guide 1.99, Revision 2 predictions.

Table 3 shows calculations of the surveillance material chemistry factors using surveillance capsule data.

Table 4 provides the reactor vessel toughness data.

Table 5 provides a summary of the fluence values used in the generation of the heatup and cooldown limit curves.

Table 6 shows example calculations of the ART values at 24 EFPY for the limiting reactor vessel material.

5.0 REFERENCES

1. WCAP-14684, "R.E. Ginna Heatup and Cooldown Limit Curves for Normal Operation," dated June 1996.
2. WCAP-14040-NP-A, "Methodology Used to Develop Cold Overpressure Mitigating System Setpoints and RCS Heatup and Cooldown Limit Curves," Revision 2, January 1996.
3. Letter from R.C. Mecredy, RG&E, to Guy S. Vissing, NRC, Subject: "Application for Amendment to Facility Operating License, Revision to Reactor Coolant System (RCS) Pressure and Temperature Limits Report (PTLR) Administrative Controls Requirements," dated September 29, 1997.
4. Letter from R.C. Mecredy, RG&E, to Guy S. Vissing, NRC, "Clarifications to Proposed Low Temperature Overpressure Protection System Technical Specification," dated June 3, 1997.
5. WCAP-7254, "Rochester Gas and Electric, Robert E. Ginna Unit No. 1 Reactor Vessel Radiation Surveillance Program," May 1969.
6. Letter from R.C. Mecredy, RG&E, to Guy S. Vissing, NRC, "Corrections to Proposed Low Temperature Overpressure Protection System Technical Specification," October 8, 1997.
7. RG&E Design Analysis DA-ME-97-031, "Evaluation of Ginna RCS Coolant Temperature to Support LTOPS Requirements," Revision 0.

MATERIAL PROPERTY BASIS

LIMITING MATERIAL: CIRCUMFERENTIAL WELD SA-847
LIMITING ART VALUES AT 24 EFPY: 1/4T, 232°F
 3/4T, 196°F

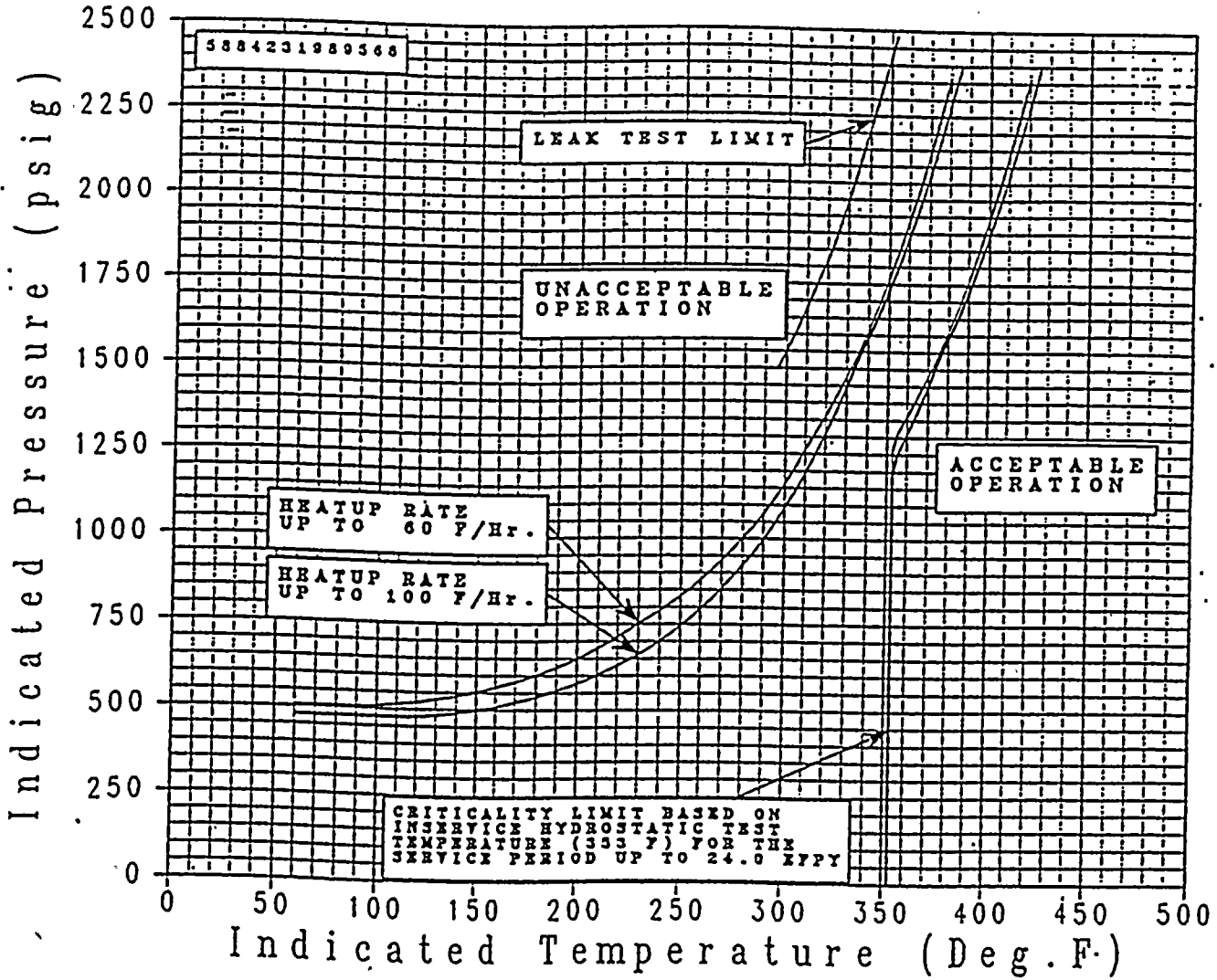


FIGURE 1

REACTOR VESSEL HEATUP LIMITATIONS
APPLICABLE FOR THE FIRST 24 EFPY
(WITHOUT MARGIN FOR INSTRUMENT ERRORS)

MATERIAL PROPERTY BASIS

LIMITING MATERIAL: CIRCUMFERENTIAL WELD SA-847

LIMITING ART VALUES AT 24 EPFY: 1/4T, 232°F

3/4T, 196°F

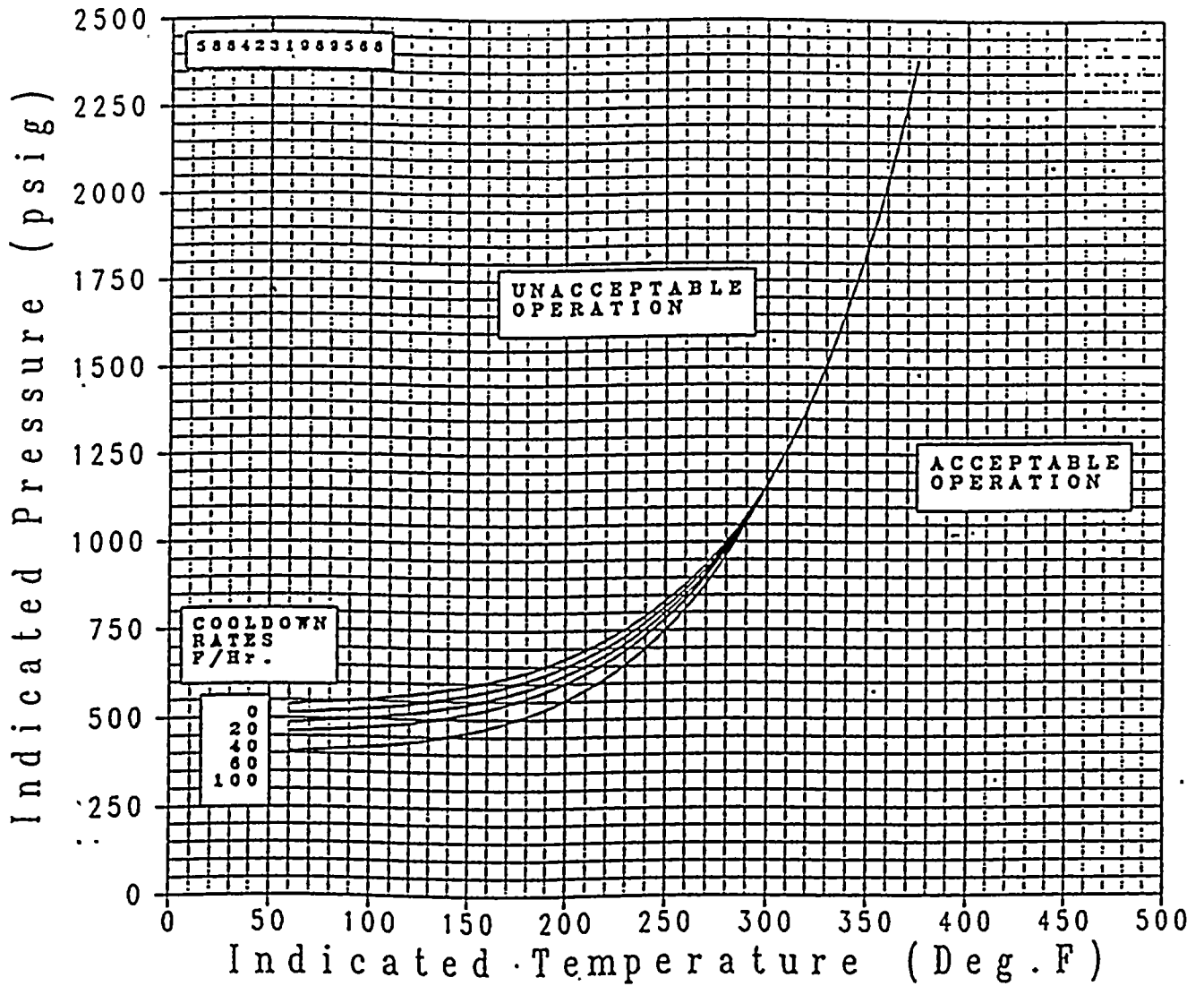


FIGURE 2

REACTOR VESSEL COOLDOWN LIMITATIONS
APPLICABLE FOR THE FIRST 24 EPFY
(WITHOUT MARGIN FOR INSTRUMENT ERRORS)

Table 1
Surveillance Capsule Removal Schedule

Capsule	Vessel Location (deg.)	Capsule Lead Factor	Removal Schedule ^(a)	Capsule Fluence E19(n/cm ²) ^(c)
V	77°	2.99	1.6 (removed)	.5028
R	257°	3.00	2.7 (removed)	1.105
T	67°	1.85	7 (removed)	1.864
S	57°	1.74	17 (removed)	3.746
N	237°	1.74	TBD ^(b)	TBD ^(b)
P	247°	1.9	Standby	N/A

NOTES:

- (a) Effective Full Power Years (EFPY).
- (b) To be determined, there is no current requirement for removal.
- (c) Reference 1.

TABLE 2 Surveillance Material 30 lb-ft Transition Temperature Shift					
Material	Capsule	Fluence ($\times 10^{19}$ n/cm ² , E > 1.0 MeV) ^(a)	30 lb-ft Transition Temperature Shift		
			Predicted ^(a) (°F)	Measured ^(a) (°F)	Δ (°F)
Lower Shell	V	.5028	26	25	1
	R	1.105	32	25	7
	T	1.864	37	30	7
	S	3.746	42	42	0
Intermediate Shell	V	.5028	37	0	37
	R	1.105	46	0	46
	T	1.864	52	0	52
	S	3.746	59	60	1
Weld Metal	V	.5028	135	140	5
	R	1.105	168	165	3
	T	1.864	191	150	41
	S	3.746	218	205	13
HAZ Metal	V	.5028	---	0	---
	R	1.105	---	90	---
	T	1.864	---	100	---
	S	3.746	---	95	---

(a) Reference 1 (including its Reference 51).

TABLE 3							
Calculation of Chemistry Factors Using Surveillance Capsule Data							
Material	Capsule	Fluence ($\times 10^{19}$ n/cm ² , E > 1.0 MeV) ^(a)	FF	ΔRT_{NDT} (°F) ^{(a)(b)}	FF* ΔRT_{NDT} (°F)	FF ²	
Intermediate Shell Forging 05 (Tangential)	V	.5028	.8081	25	20.2	.6530	
	R	1.105	1.0279	25	25.7	1.0566	
	T	1.864	1.1706	30	35.1	1.3703	
	S	3.746	1.3418	42	56.4	1.8004	
	Sum:					137.4	4.8803
	Chemistry Factor = 28.2°F						
Intermediate Shell	V	.5028	.8081	0	0	.6530	
	R	1.105	1.0279	0	0	1.0566	
	T	1.864	1.1706	0	0	1.3703	
	S	3.746	1.3418	60	80.5	1.8004	
	Sum:					80.5	4.8803
	Chemistry Factor = 16.5°F						
Weld Metal	V	.5028	.8081	149.7	121.0	.6530	
	R	1.105	1.0279	176.4	181.3	1.0566	
	T	1.864	1.1706	160.4	187.8	1.3703	
	S	3.746	1.3418	219.1	294.0	1.8004	
	Sum:					854.69	4.8803
	Chemistry Factor = 160.7°F						

NOTES:

(a) Reference 1.

(b) ΔRT_{NDT} for weld material is the adjusted value using the 1.069 ratioing factor per Reference 1 applied to the measured values of Table 2.

TABLE 4 Reactor Vessel Toughness Table (Unirradiated) ^(a)			
Material Description	Cu (%)	Ni(%)	Initial RT _{NDT} (°F)
Intermediate Shell	.07	.69	20
Lower Shell	.05	.69	40
Circumferential Weld	.25	.56	-4.8

(a) Per Reference 1.

TABLE 5 Reactor Vessel Surface Fluence Values at 19.5 and 32 EFPY ^(a) $\times 10^{19}$ (n/cm ² , E > 1.0 MeV)				
EFPY	0°	15°	30°	45°
19.5	2.32	1.47	1.05	.969
32	3.49	2.20	1.56	1.45

(a) Reference 1.



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TABLE 6		
Calculation of Adjusted Reference Temperatures at 24 EFPY for the Limiting Reactor Vessel Material		
Parameter	Values	
Operating Time	24 EFPY	
Material	Circ. Weld	Circ. Weld
Location	1/4-T	3/4-T
Chemistry Factor (CF), °F ^(b)	160.7	160.7
Fluence (f), 10 ¹⁹ n/cm ² (E > 1.0 MeV) ^(a)	1.85	.851
Fluence Factor (FF)	1.17	.955
$\Delta RT_{NDT} = CF \times FF$, °F	188	153.4
Initial RT_{NDT} (I), °F	-4.8	-4.8
Margin (M), °F ^(a)	48.3	48.3
$ART = I + (CF \times FF) + M$, °F ^{(a)(c)}	232	196.9

NOTES:

(a) Value calculated using Table 5 values.

(b) Values from Table 3.

(c) Reference 1.