NRC FORM 464 Part I
(03-2017)

U.S. NUCLEAR REGULATORY COMMISSION

RESPONSE TO FREEDOM OF INFORMATION ACT (FOIA) REQUEST

FOIA	RESPONSE NUMBER
2017-0633	1

RESPONSE TYPE ☐ INTERIM ☑ FINAL

REQUESTER: David Brownawell

DATE: AUG 0 9 2017

DESCRIPTION OF REQUESTED RECORDS:

Accession number 7811160005, Draft Reg Guide 1.XXX, "Atmospheric Dispersion Models for Potential Accident Consequence Assessments at Nuclear Power Plants," Date 1978

PART I. -- INFORMATION RELEASED

You have the right to seek assistance from the NRC's FOIA Public Liaison. Contact information for the NRC's FOIA Public Liaison is available at https://www.nrc.gov/reading-rm/foia/contact-foia.html

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☑ Agency records subject to the request are enclosed.

☐ Records subject to the request that contain information originated by or of interest to another Federal agency have been referred to that agency (see comments section) for a disclosure determination and direct response to you.

☐ We are continuing to process your request.

☑ See Comments.

PART I.A -- FEES

AMOUNT*
$0.00
*See Comments for details

☐ You will be billed by NRC for the amount listed.

☐ You will receive a refund for the amount listed.

☐ Fees waived.

NO FEES

☑ Minimum fee threshold not met.

☐ Due to our delayed response, you will not be charged fees.

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☐ We have withheld certain information pursuant to the FOIA exemptions described, and for the reasons stated, in Part II.

☐ Because this is an interim response to your request, you may not appeal at this time. We will notify you of your right to appeal any of the responses we have issued in response to your request when we issue our final determination.

☐ You may appeal this final determination within 90 calendar days of the date of this response by sending a letter or e-mail to the FOIA Officer, at U.S. Nuclear Regulatory Commission, Washington, D.C. 20555-0001, or FOIA.Resource@nrc.gov. Please be sure to include on your letter or email that it is a "FOIA Appeal." You have the right to seek dispute resolution services from the NRC's Public Liaison, or the Office of Government Information Services (OGIS). Contact information for OGIS is available at https://ogis.archives.gov/about-ogis/contact-information.htm

PART I.C COMMENTS (Use attached Comments continuation page if required)

Please find the requested record attached.

Signature - Freedom of Information Act Officer or Designee

Stephanie Blaney

OCT 2 6 1978

REGULATORY GUIDE 1.XXX

ATMOSPHERIC DISPERSION MODELS FOR POTENTIAL ACCIDENT CONSEQUENCE ASSESSMENTS AT NUCLEAR POWER PLANTS

OUTLINE

REGULATORY GUIDE 1.XXX

ATMOSPHERIC DISPERSION MODELS FOR POTENTIAL ACCIDENT CONSEQUENCE ASSESSMENTS AT NUCLEAR POWER PLANTS

A. INTRODUCTION

Section 100.10 of 10 CFR Part 100 states that meteorological conditions at the site and surrounding area should be considered in determining the acceptability of a site for a power or testing reactor. Section 50.34 of 10 CFR Part 50 requires that each applicant for a construction permit or operating license provide an analysis and evaluation of the design and performance of structures, systems and components of the facility with the objective of assessing the risk to public health and safety resulting from the operation of the facility. Section 50.34 of 10 CFR Part 50 also states that special attention should be directed to the site evaluation factors identified in 10 CFR Part 100 in the assessment of the site.

The Regulatory Position presented in this guide represents a substantial change from procedures previously used to determine relative concentrations for assessing the potential offsite radiological consequences for a range of postulated accidental releases of radiological material to the atmosphere. These procedures now include consideration of plume meander and of directional dependence of dispersion conditions, wind frequencies, exclusion area boundary distances, and low population zone (LPZ) boundary distances.

The direction-dependent approach was developed to provide an improved basis for the Part 100-related review of proposed reactor/site considerations.

Accordingly, this guide provides an acceptable methodology for determining site specific relative concentrations (χ/Q) and should be used in determining χ/Q values for the evaluations discussed in Regulatory Guide 1.3, Revision 2, "Assumptions Used for Evaluating the Potential Radiological Consequences of a Loss of Coolant Accident for Boiling Water Reactors," and Regulatory Guide 1.4, Revision 2, "Assumptions Used for Evaluating the Potential Radiological Consequences of a Loss of Coolant Accident for Pressurized Water Reactors." A number of other Regulatory Guides also include requirements for or refer to radiological analyses of potential accidents. The applicability of the specific criteria discussed herein to these other analyses will be considered on a case-by-case basis. Until such time as generic guidelines are developed for such analyses, the methodology provided in this guide is acceptable.

B. DISCUSSION

The atmospheric diffusion models described in this guide reflect review of recent experimental data on diffusion from releases at ground-level without buildings present and from releases at various locations on reactor facility buildings during stable atmospheric conditions with low wind speeds (Refs. 1-6). These tests verify the existence of effluent plume "meander" under light wind speed conditions and neutral (D) and stable (E, F and G) atmospheric stability conditions (as defined by the ΔT criteria in Regulatory Guide 1.23) (Ref. 7). Effluent concentrations measured over a period of one hour under such conditions have been shown to be substantially lower than would be predicted using the traditional curves (Ref. 8) of lateral and vertical plume spread which are functions of atmospheric stability and downwind distance.

The procedures in this guide also recognize that atmospheric dispersion conditions and wind frequencies are usually directionally dependent; that is, certain air flow directions can exhibit substantially more or less favorable diffusion conditions than others, and the wind can transport effluents in certain directions more frequently than in others. The procedures also allow evaluations of atmospheric dispersion for directionally variable distances such as a non-circular exclusion area boundary.

C. REGULATORY POSITION

This section identifies acceptable methods for 1) calculating atmospheric relative concentration (χ/Q) values, 2) determining χ/Q values on a directional basis, 3) determining χ/Q values on an overall site basis, and 4) choosing χ/Q values to be used in evaluations of the types of events described in Regulatory Guides 1.3 and 1.4.

Selection of conservative, less detailed site parameters for the evaluation may be sufficient to establish compliance with Regulatory guidelines.

C.1 Calculation of Atmospheric Relative Concentration (χ/Q) Values

Equations and parameters presented in this section should be used unless unusual siting, meteorological, or terrain conditions dictate the use of other models or considerations. High-quality, site-specific atmospheric diffusion tests may be used as a basis for modifying the equations and parameters.

C.1.1 Meteorological Data Input

The meterological data needed for χ/Q calculations include wind speed, wind direction, and atmospheric stability. These data should represent hourly averages as defined in Section C.6.a of Regulatory Guide 1.23 (Ref. 7).

Wind direction should be classed into 16 compass directions (22.5 degree sectors centered on true north, north-northeast, etc.)

Atmospheric stability should be determined by vertical temperature difference (ΔT) between the release height and the 10-meter level, or by other well-documented parameters that have been substantiated by diffusion data. Acceptable stability classes are given in Table 2 of Regulatory Guide 1.23 (Ref. 7).

Calms should be defined as hourly averaged wind speeds below the vane or anemometer starting speed, whichever is higher (to reflect limitations in instrumentation). If the instrumentation program conforms to the Regulatory Position in Regulatory Guide 1.23, calms should be assigned a wind speed equal to the vane or anemometer starting speed, whichever is higher. Otherwise, consideration of a conservative evaluation of calms, as indicated by the system, will be necessary. Wind directions during calm conditions should be assigned in proportion to the directional distribution of non-calm winds with speeds less than 1.5 meters per second.[1]

C.1.2 Determination of Distances for χ/Q Calculations

For each wind direction sector, χ/Q values for each significant release point should be calculated at an appropriate exclusion area

[1] Staff experience has shown that non-calm wind speeds below 1.5 meters per second provide a reasonable range for defining the distribution of wind direction during light winds.

boundary distance and outer low population zone (LPZ) boundary distance. The following procedure should be used to determine these distances. The procedure takes into consideration the possibility of curved airflow trajectories, plume segmentation (particularly in light wind, stable conditions), and the potential for wind speed and direction frequency shifts from year to year.

For each of the 16 sectors, the distance for exclusion area boundary or outer LPZ boundary χ/Q calculation should be the minimum distance to the exclusion area boundary or outer LPZ boundary within a 45 degree sector centered on the compass direction of interest.

For stack releases, the maximum ground level concentration in a sector may occur beyond the exclusion area boundary distance or outer LPZ boundary distance. Therefore, for stack releases, χ/Q calculations should be made in each sector at each boundary distance and at various distances beyond the exclusion area boundary distance to determine the maximum relative concentration for consideration in subsequent calculations.

C.1.3 Calculation of χ/Q Values at Exclusion Area Boundary Distances

Relative concentrations that can be assumed to apply at the exclusion area boundary for two hours immediately following an accident should be determined.[2] Calculations based on meteorological data averaged over a one-hour period should be assumed to apply for the entire two-hour period. This assumption is reasonably conservative considering the small variation of χ/Q values with averaging time (Ref. 9). If releases associated with a postulated event are estimated to occur in a period substantially

[2] See Section 100.11 of 10 CFR Part 100.

less than one hour (i.e., less than 20 minutes), the applicability of the models should be evaluated on a case-by-case basis.

Procedures for calculating "two-hour" χ/Q values depend on the mode of release. The procedures are described below.

C.1.3.1 <u>Releases Through Vents or Other Building Penetrations</u>

This class of release modes includes all release points or areas which are effectively lower than two and one-half times the height of adjacent solid structures (Ref. 10). Within this class, two sets of meteorological conditions are treated differently, as follows.

(1) During neutral (D) or stable (E, F, or G) atmospheric stability conditions when the wind speed at the 10-meter level is less than 6 meters per second, horizontal plume meander can be considered. χ/Q values may be determined through selective use of the following set of equations for ground-level relative concentrations at the plume centerline:

$$\chi/Q = \frac{1}{\overline{U}_{10}(\pi\sigma_y\sigma_z + A/2)} \qquad (1)$$

$$\chi/Q = \frac{1}{\overline{U}_{10}(3\pi\sigma_y\sigma_z)} \qquad (2)$$

$$\chi/Q = \frac{1}{\overline{U}_{10}\pi\Sigma_y\sigma_z} \qquad (3)$$

where χ/Q is relative concentration (sec/m^3),

π is 3.14159,

$\overline{U}_{10}$ is wind speed at 10 meters above plant grade[3] (m/sec),

[3] The 10-meter level is representative of the depth through which the plume is mixed with building wake effects.

σ_y is lateral plume spread (m), a function of atmospheric stability and distance (Figure 1),

σ_z is vertical plume spread (m), a function of atmospheric stability and distance (Figure 2),

Σ_y is lateral plume spread with meander and building wake effects (m), a function of atmospheric stability, wind speed $\overline{U}_{10}$, and distance [For distances of 800 meters or less, $\Sigma_y = M\sigma_y$, where M is determined from Figure 3. For distances greater than 800 meters, $\Sigma_y = (M - 1)\ \sigma_{y800m} + \sigma_y$.], and

A is the smallest vertical-plane cross-sectional area of the reactor building (m^2). (Other structures and/or a directional consideration may be justified when appropriate.)

χ/Q values should be calculated using Equations 1, 2, and 3. The values from Equations 1 and 2 should be compared and the <u>higher</u> selected. This value should be compared with the value from Equation 3, and the <u>lower</u> of these two should be selected as the appropriate χ/Q value. Examples and a detailed explanation of the rationale for determining the controlling conditions are given in Appendix A.

(2) During all other meteorological conditions [unstable (A, B, or C) atmospheric stability and/or 10-meter level wind speeds of 6 meters per second or more], plume meander should not be considered. The appropriate χ/Q value is the higher value calculated from Equation 1 or 2.

C.1.3.2 <u>Stack Releases</u>

This class of release modes includes all release points which are equal to or higher than two and one-half times the height of adjacent solid structures (Ref. 10). Non-fumigation and fumigation conditions are treated separately.

(1) For non-fumigation conditions, the equation for ground-level relative concentration at the plume centerline for stack releases is:

$$\chi/Q = \frac{1}{\pi \bar{U}_h \sigma_y \sigma_z} \exp \frac{-h_e^2}{2\sigma_z^2} \tag{4}$$

where $\bar{U}_h$ is wind speed representing conditions at the release height (m/sec),

h_e is effective stack height (m): $h_e = h_s - h_t$,

h_s is the initial height of the plume (usually the stack height) above plant grade (m),

h_t is the maximum terrain height above plant grade between the release point and the point for which the calculation is made (m); h_t cannot exceed h_s, and

the other parameters have been defined previously.

(2) For fumigation conditions, a "fumigation χ/Q" should be calculated for each sector as follows. The equation for ground-level relative concentration at the plume centerline for stack releases during fumigation conditions is:

$$\chi/Q = \frac{1}{(2\pi)^{1/2} \bar{U}_{h_e} \sigma_y h_e}, \; h_e > 0 \tag{5}$$

where $\bar{U}_{h_e}$ is wind speed representative of the layer of depth h_e (m/sec); in lieu of information to the contrary, the staff considers a value of 2 meters per second as a reasonably conservative assumption for h_e of about 100 meters,

σ_y is the lateral plume spread (m) which is representative of the layer at a given distance; a moderately stable (F) atmospheric stability condition is usually assumed, and

h_e is as defined for Equation 4.

Ground-level relative concentrations for fumigation conditions cannot be higher than those produced by non-fumigation stable atmospheric conditions. Therefore, if the χ/Q value from Equation 5 exceeds that from Equation 4 assuming F stability and a wind speed of 2 meters per second, use the value from Equation 4 as the fumigation χ/Q for the sector.

C.1.4 Calculation of χ/Q Values at Outer LPZ Boundary Distances

"Two-hour" χ/Q values should also be calculated at outer LPZ boundary distances. The procedures described above for exclusion area boundary distances (Section C.1.3) should be used.

An annual average (8760-hour) χ/Q should be calculated for each sector at the outer LPZ boundary distance for that sector, using the method described in Section C.1.c of Regulatory Guide 1.111 (Ref. 13). (For stack releases, h_e should be determined as described in Section C.1.3.2 of this Guide.)

These calculated "two-hour" and annual average values are used in Section C.2.2 to determine sector χ/Q values at outer LPZ boundary distances for various longer time periods.[4]

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[4] See Section 100.11 of 10 CFR Part 100.

C.2 Determination of Maximum Sector χ/Q Values

The χ/Q values calculated in Section C.1 are used to determine "sector χ/Q values" and "maximum sector χ/Q values" for the exclusion area boundary and the outer LPZ boundary as follows.

C.2.1 Exclusion Area Boundary

General Method: Using the χ/Q values calculated for each hour of data according to Section C.1.3, a cumulative probability distribution of χ/Q value should be constructed for each of the 16 sectors. Each distribution should be described in terms of probabilities of given χ/Q values being exceeded in that sector during the total time. A plot of χ/Q versus probability of being exceeded should be made for each sector and a curve should be drawn to form an upper bound of the data points. From each of the 16 curves, the χ/Q value which is exceeded 0.5% of the total time should be selected (Ref. 14). These are the sector χ/Q values. The highest of the 16 sector values is defined as the maximum sector χ/Q value.

Fumigation Conditions for Stack Releases: Section C.1.3.2 gave procedures for calculating a fumigation χ/Q for each sector. These sector fumigation values, along with the general (non-fumigation) sector values obtained above, are used to determine appropriate sector χ/Q's for fumigation conditions, based on conservative assumptions concerning the duration of fumigation. These assumptions differ for inland and coastal sites and certain modifications may be appropriate for specific sites.

Inland Sites: For stack releases at sites located 3200 meters or more from large bodies of water (e.g., oceans or Great Lakes), a fumigation condition should be assumed to exist at the time of the accident and continue for one-half hour (Ref. 11). For each sector, if the sector fumigation χ/Q exceeds the sector non-fumigation χ/Q, use the fumigation value for the 0 to 1/2-hour time period and the non-fumigation value for the 1/2 to 2-hour time period. Otherwise, use the non-fumigation sector value for the entire 0 to 2-hour time period. The 16 (sets of) values thus determined will be used in dose assessments requiring time-integrated concentration considerations.

Coastal Sites: For stack releases at sites located less than 3200 meters from large bodies of water, a fumigation condition should be assumed to exist at the exclusion area boundary at the time of the accident and continue for the entire two-hour period. For each sector, if the sector fumigation χ/Q exceeds the sector non-fumigation χ/Q, use the fumigation value for the two-hour period. Otherwise, use the non-fumigation value for the two-hour period. Of the 16 sector values thus determined, the highest is the maximum sector χ/Q value for fumigation.

Modifications: These conservative assumptions do not consider frequency and duration of fumigation conditions as a function of airflow direction. If information can be presented to substantiate the likely directional occurrence and duration of fumigation conditions at a site, the assumptions of fumigation in all appropriate directions and of duration of one-half hour and two hours for the exclusion area boundary may be modified. Then fumigation need only be considered for airflow directions in which fumigation has been determined to occur and of a duration determined from the study of site conditions.[5]

C.2.2 Outer LPZ Boundary

General Method: Sector χ/Q values for the outer LPZ boundary should be determined for various time periods throughout the course of the postulated accident.[6] The time periods should represent appropriate meteorological regimes, e.g. 8 and 16 hours and 3 and 26 days as presented in Section 2.3.4 of Regulatory Guide 1.70 (Ref. 12).

For a given sector, the average χ/Q values for the various time periods should be approximated by a logarithmic interpolation between the "two-hour"[7] sector χ/Q and the annual average (8760-hour) χ/Q for the same sector. The "two-hour" sector χ/Q for the outer LPZ boundary is determined using the general method given for the exclusion area boundary in Section C.2.1. The annual average χ/Q for a given sector is determined as in Section C.1.4.

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[5] For example, examination of site-specific information at a location in a pronounced river valley may indicate that fumigation conditions occur only during the down-valley "drainage flow" regime and persist for durations of about one-half hour. Therefore, in this case airflow directions other than the down-valley directions can be excluded from consideration of fumigation conditions, and the duration of fumigation would still be considered as one-half hour. On the other hand, data from sites in open terrain (non-coastal) may indicate no directional preference for fumigation conditions, but may indicate durations much less than one-half hour. In this case, fumigation should be considered for all directions, but with durations less than one-half hour.

[6] See Section 100.11 of 10 CFR Part 100.

[7] The χ/Q's are based on one-hour averaged data, but are assumed to apply for two hours.

The logarithmic interpolation procedure produces results which are consistent with studies of variations of average concentrations with time periods to 100 hours (Ref. 9). Alternative methods should also be consistent with these studies.

For each time period, the highest of the 16 sector χ/Q values should be identified. In most cases these highest values will occur in the same sector for all time periods. These are then the maximum sector χ/Q values. However, if the highest sector χ/Q's do not all occur in the same sector, the 16 (sets of) values will be used in dose assessments requiring time-integrated concentration considerations. The χ/Q values for the various time periods within that sector should be considered the maximum sector χ/Q values.

Fumigation Conditions for Stack Releases: Determination of sector χ/Q values for fumigation conditions at the outer LPZ boundary involves the following assumptions concerning the duration of fumigation for inland and coastal sites.

Inland Sites: For stack releases at sites located 3200 meters or more from large bodies of water, a fumigation condition should be assumed to exist at the outer LPZ boundary at the time of the accident and continue for one-half hour. Sector χ/Q values for fumigation should be determined as for the exclusion area boundary in Section C.2.1.

Coastal Sites: For stack releases at sites located less than 3200 meters from large bodies of water, a fumigation condition should be assumed to exist at the outer LPZ boundary following the arrival of the plume and continue for a four-hour period. Sector χ/Q values for fumigation should be determined as for the exclusion area boundary in Section C.2.1.

The modifications discussed in Section C.2.1 may also be considered for the outer LPZ boundary.

C.3 Determination of 5% Overall Site χ/Q Value

The χ/Q values which are exceeded no more than 5% of the total time around the exclusion area boundary and around the outer LPZ boundary should be determined as follows (Ref. 14).

Using the χ/Q values calculated according to Section C.1, an overall cumulative probability distribution for all directions combined should be constructed. A plot of χ/Q versus probability of being exceeded should be made, and an upper bound curve should be drawn. The two-hour χ/Q value which is exceeded 5% of the time should be selected from this curve as the dispersion condition indicative of the type of release being considered. In addition, for the outer LPZ boundary the maximum of the 16 annual average χ/Q values should be used along with the 5% two-hour χ/Q value to determine χ/Q values for the appropriate time periods by logarithmic interpolation.

C.4 Selection of χ/Q Values to be Used in Evaluations

The χ/Q value for exclusion area boundary or outer LPZ boundary evaluations should be the maximum sector χ/Q (Section C.2) or the 5% overall site χ/Q (Section C.3), whichever is higher. All direction-dependent sector values should be presented for consideration of the appropriateness of the exclusion area and outer LPZ boundaries, and the efficacy of evacuation routes and emergency plans. Where the basic meteorological data necessary for the analyses described herein substantially deviate from the Regulatory Position stated in Regulatory Guide 1.23 (Ref. 7), consideration should be given to the resulting uncertainties in dispersion estimates.

D. IMPLEMENTATION

This proposed guide has been released to encourage public participation in its development and is not intended to foreclose other options in siting evaluations. Except in those cases in which an applicant proposes an acceptable alternative method for complying with specified portions of the Commission's regulations, the method to be described in the active guide reflecting public comments will be used in the evaluation of applications for Construction Permits and Early Site Reviews tendered after the implementation date to be specified in the active guide. This implementation date will in no case be earlier than November 1, 1979.

For Construction Permit applications tendered before the implementation date and for Operating License applications whose construction permits preceed the active implementation date, either the proposed guide or the procedures described in Standard Review Plan Section 2.3.4 (1974) may be used. The staff will use both the procedures described in the guide and the Standard Review Plan Section 2.3.4 (1974) to judge the conservatism of an applicant's assessment of diffusion conditions. Except in the unlikely event that direction dependent evaluations reveal a significant bias of high relative concentrations in specific directions, the staff expects the results obtained using the SRP method to provide acceptably conservative estimates. The method described in the proposed guide will be considered for licensing actions concerning operating reactors on an individual case basis.

In all cases, selection of conservative, less detailed site parameters for the evaluation should be sufficient to establish compliance with Regulatory guidelines.

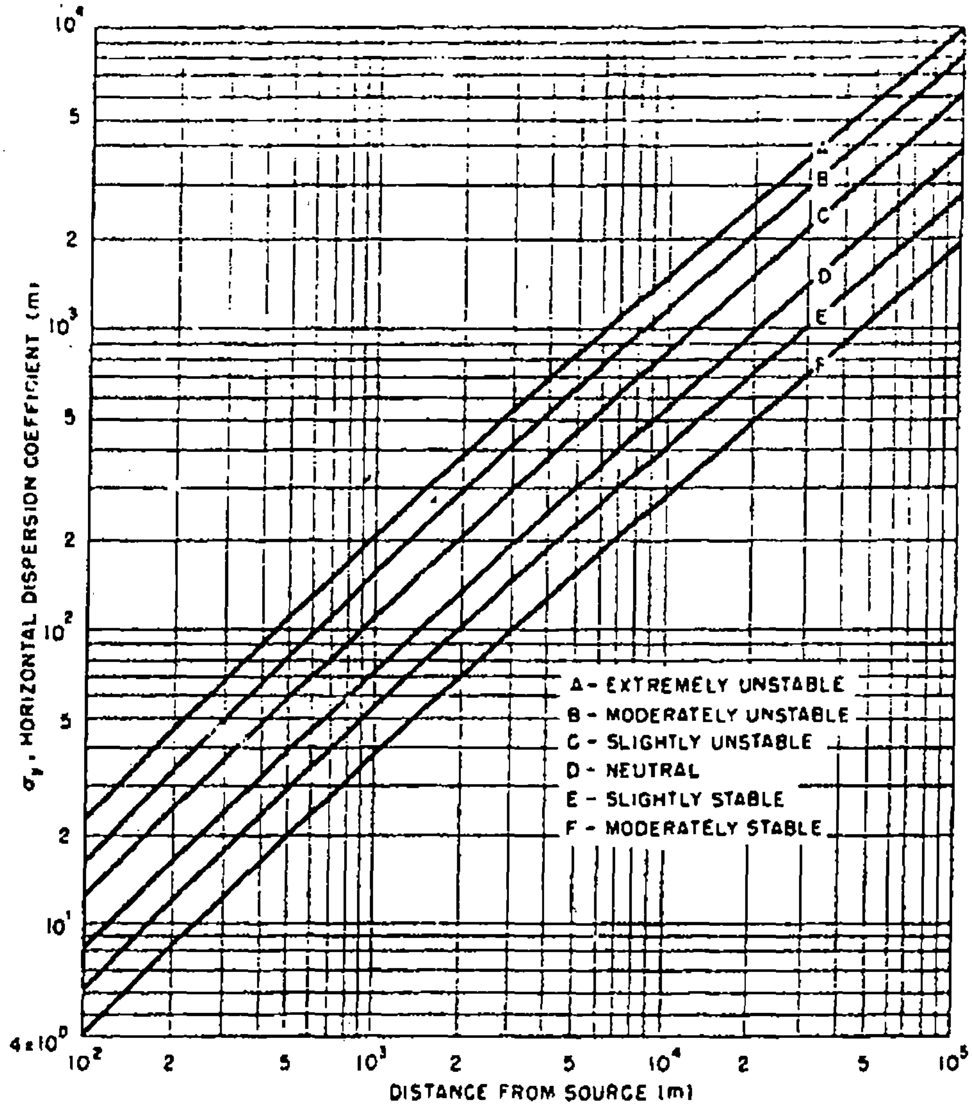


Figure 1. Lateral diffusion without meander and building wake effects, σ_y, vs. downwind distance from source for Pasquill's turbulence types (atmospheric stability) (Ref. 8).

For purposes of estimating σ_y during extremely stable (G) atmospheric stability conditions, without plume meander or other lateral enhancement, the following approximation is appropriate:

$$\sigma_y\ (G) = \frac{2}{3}\ \sigma_y\ (F)$$

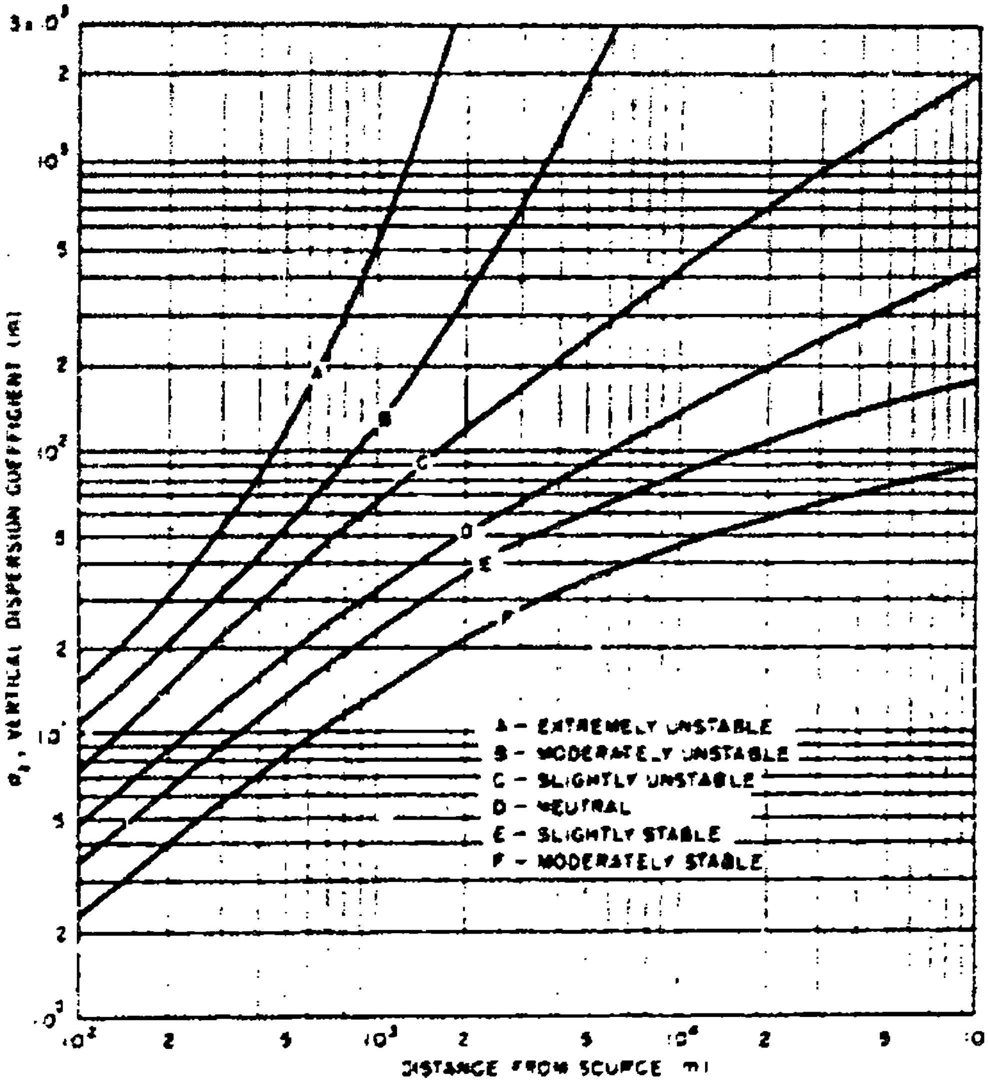


Figure 2. Vertical diffusion without meander and building wake effects, σ_z, vs. downwind distance from source for Pasquill's turbulence types (atmospheric stability) (Ref. 8).

For purposes of estimating σ_z during extremely stable (G) atmospheric stability conditions, the following approximation is appropriate:

$$\sigma_z(G) = \frac{3}{5}\,\sigma_z\,(F)$$

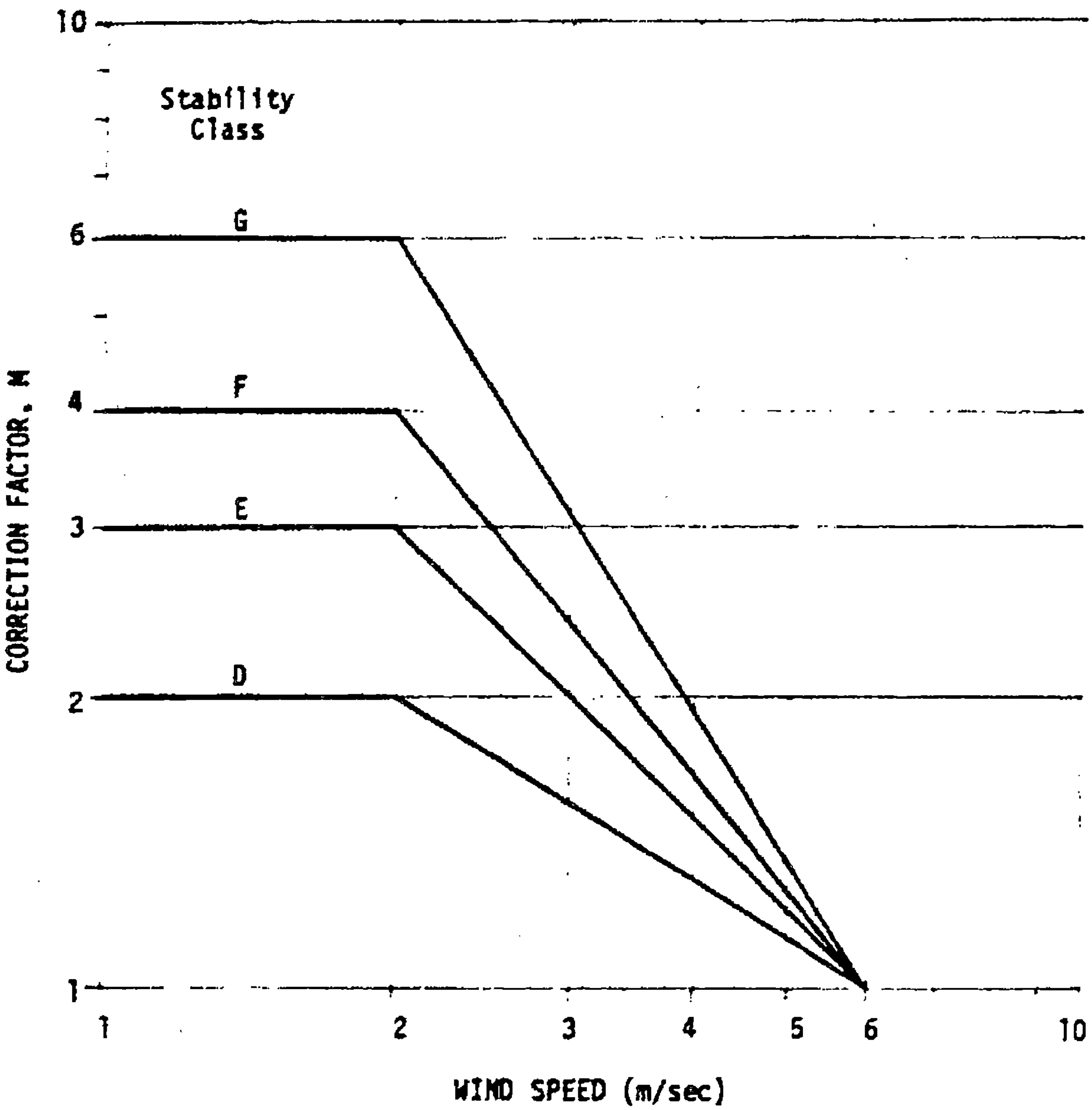


Figure 3. Correction factors for Pasquill-Gifford σ_y values by atmospheric stability class (see Appendix A)

APPENDIX A

ATMOSPHERIC DIFFUSION MODEL FOR RELEASES THROUGH VENTS AND BUILDING PENETRATIONS

Rationale

The effects of building wake mixing and ambient plume meander on atmospheric dispersion are expressed in this guide in terms of conditional use of Equations 1, 2, and 3.

Equations 1 and 2 are formulations which have been acceptable for evaluating nuclear power plant sites over a period of many years (Ref. 8 and Reg. Guides 1.3 and 1.4), but have been recently found to provide estimates of ground-level concentrations which are consistently too high during light wind and stable or neutral atmospheric conditions for one-hour release durations (Refs. 1-6).

Equation 3 is an empirical formulation based on staff analysis of atmospheric diffusion experiment results (Ref. 2). The staff examined values of lateral plume spread with meander and building wake effects (Σ_y) by atmospheric stability class (based on ΔT), calculated from measured ground-level concentrations from the experimental results. Plots of the computed Σ_y values by atmospheric stability class and downwind distance were analyzed conservatively, but within the scatter of the data points by virtually enveloping most test data. The resultant analysis is the basis for the correction factors applied to the Pasquill-Gifford σ_y values (see Figure 3). Thus, Equation 3 identifies conservatively the combined effects of increased plume meander and building wake on diffusion in the horizontal crosswind direction under light wind and stable or neutral atmospheric conditions, as quantified in Figure 3. These experiments also indicate that vertical building wake mixing is not as complete during light wind, stable conditions as during moderate wind, unstable conditions, although the results could not be quantified in a generic manner.

The conditional use of Equations 1, 2, and 3 is considered appropriate because 1) horizontal plume meander tends to dominate dispersion during light wind and stable or neutral conditions and 2) building wake mixing becomes more effective in dispersing effluents than meander effects as the wind speed increases and the atmosphere becomes less stable.

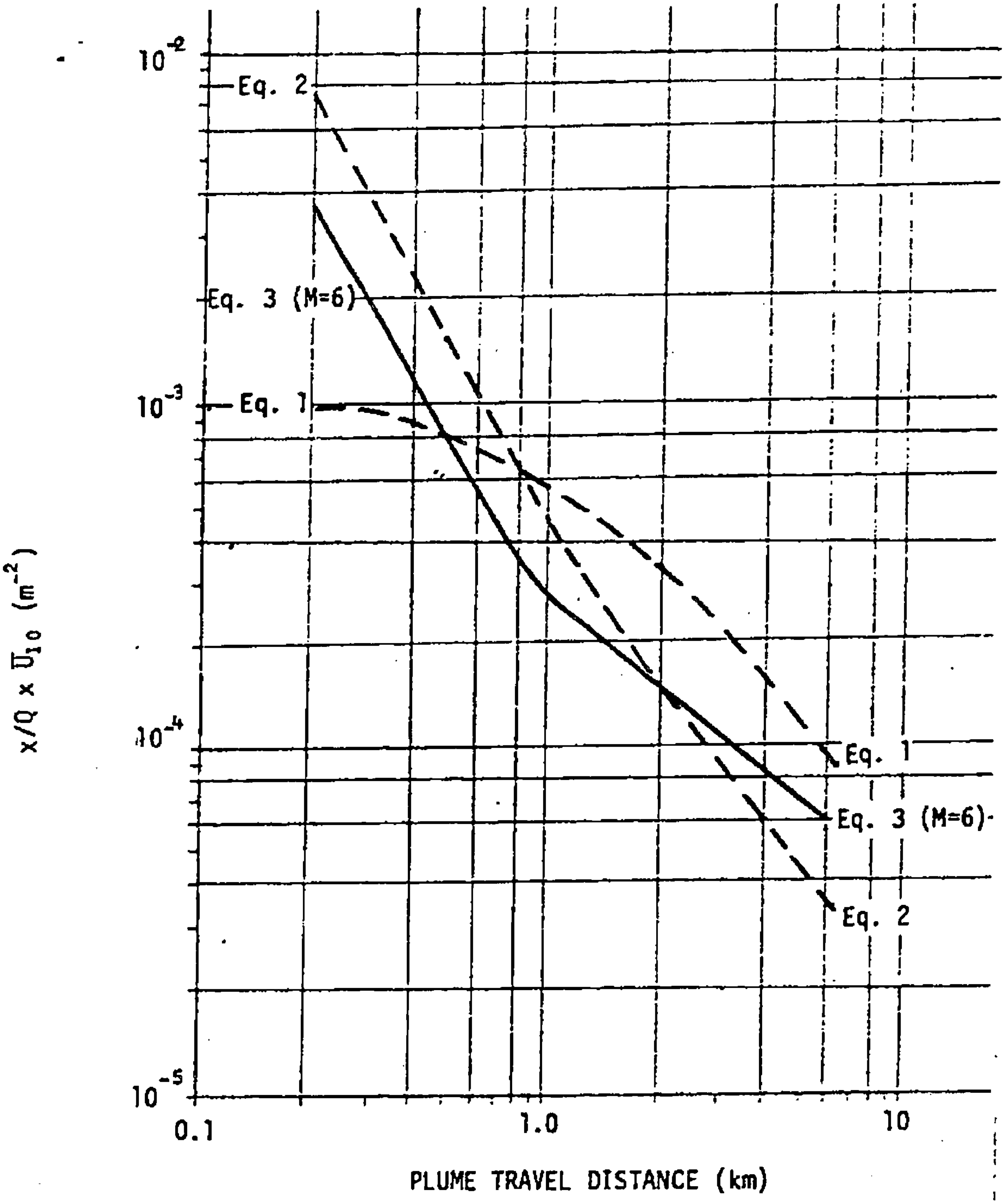
<u>Examples of Conditional Use of Diffusion Equations</u>

Figures A-1, A-2, and A-3 show plots of $\chi\overline{U}_{10}/Q$ (χ/Q multiplied by the wind speed $\overline{U}_{10}$) versus downwind distance based on the conditional use (as described in Section C.1.3.1) of Equations 1, 2, and 3 during atmospheric stability class G. The variable M for Equation 3 equals 6, 3, and 2 respectively in Figures A-1, A-2, and A-3 (M is as defined in Section C.1.3.1). The wind speed conditions are those appropriate for G stability and M = 6, 3, and 2.

In Figure A-1, the $\chi\overline{U}_{10}/Q$ from Equation 3 (M = 6) is less than the higher value from Equation 1 or 2 at all distances. Therefore, for M = 6, Equation 3 is used for all distances.

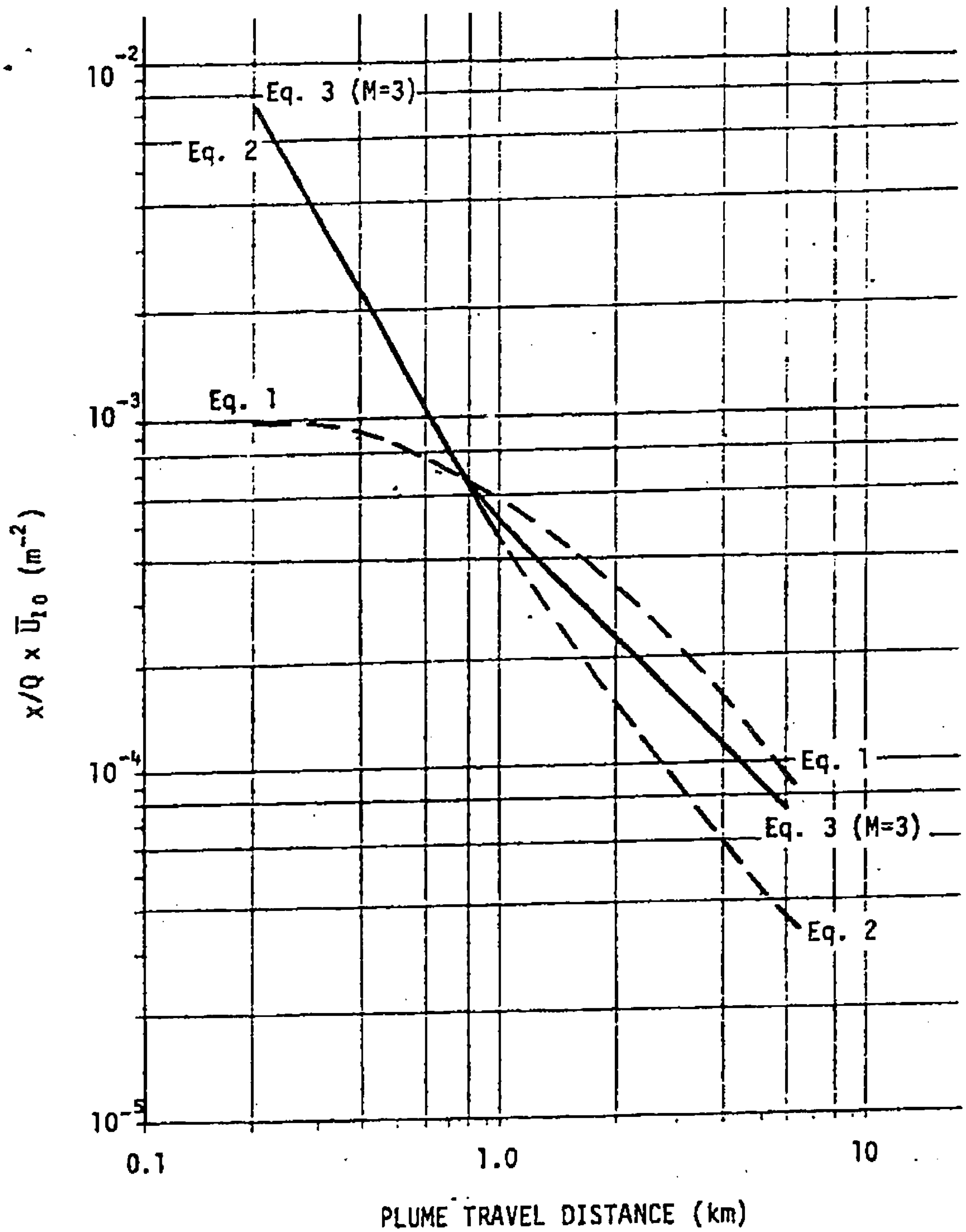
In Figure A-2, the $\chi\bar{U}_{10}/Q$ from Equation 3 (M = 3) is less than the higher value from Equation 1 or 2 beyond 0.8 km. Therefore, for M = 3, Equation 3 is used beyond 0.8 km. For distances less than 0.8 km, the value from Equation 3 equals that from Equation 2. Equation 2 is used in this case.

In Figure A-3, the $\chi\bar{U}_{10}/Q$ from Equation 3 (M = 2) is never less than the higher value from Equation 1 or 2. Therefore, for M = 3, Equation 3 is not used at all. Instead, Equation 2 is used up to 0.8 km and Equation 1 is used beyond 0.8 km.

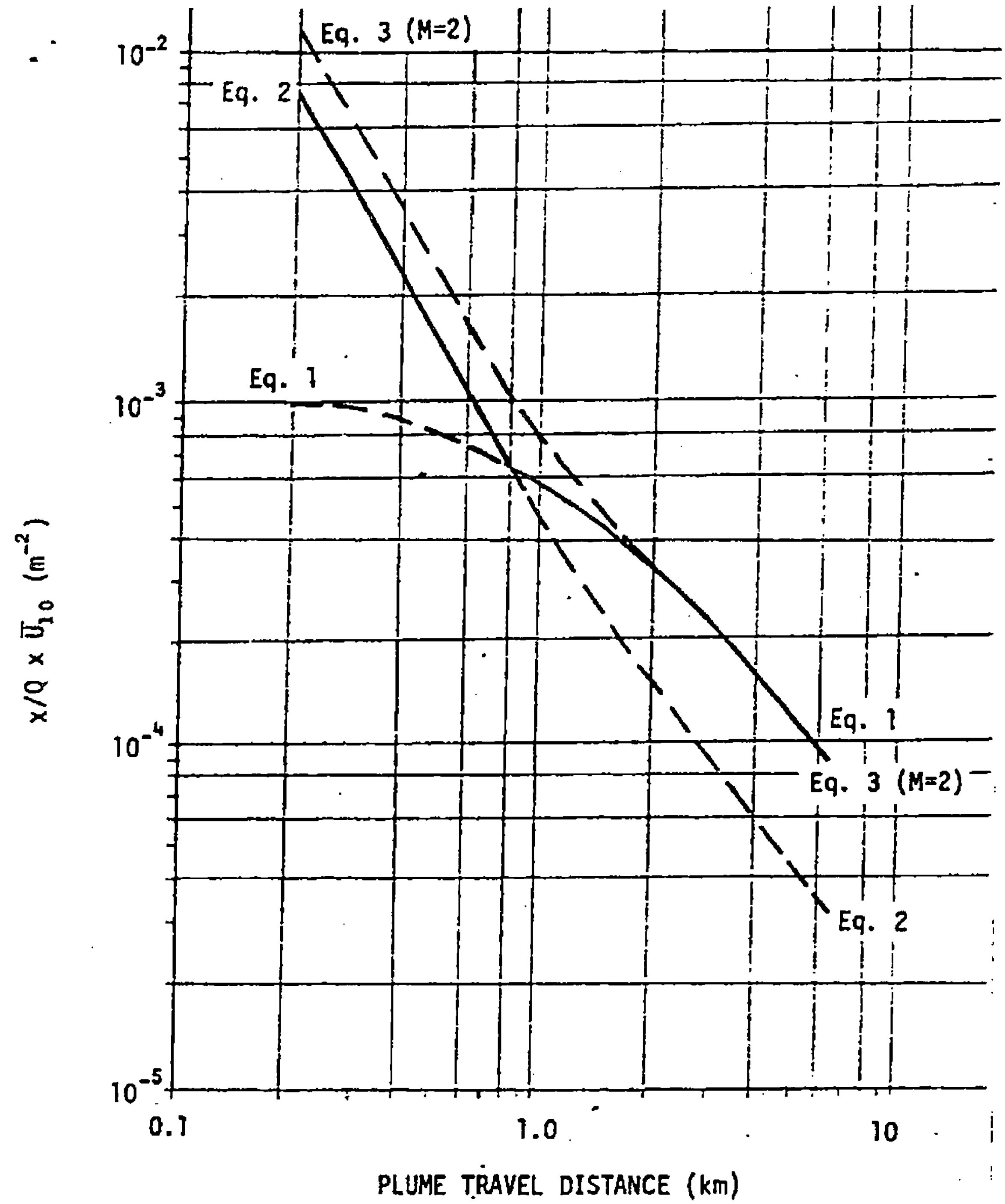


430 Figure A-1. $\chi\overline{U}_{10}/Q$ as a function of plume travel distance for G stability

431 condition using Equations 1, 2, and 3 (M = 6).



432 Figure A-2. $\chi\bar{U}_{10}/Q$ as a function of plume travel distance for G stability
433 using Equations 1, 2, and 3 (M = 3).



434 Figure A-3. $\chi\bar{U}_{10}/Q$ as a function of plume travel distance for G stability

435 condition using Equations 1, 2, and 3 (M = 2).

REFERENCES

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