## REGULATORY INFORMATION DISTRIBUTION STATEM (RIDS)

ACCESSION NBR:8408090096 DOC.DATE: 84/08/06 NOTARIZED: NO FACIL:50-389 St. Lucie Plant, Unit 2, Florida Power & Light Co.

DOCKET # 05000389

AUTH, NAME WILLIAMS, J.W.

AUTHOR AFFILIATION

RECIP NAME

Florida Power & Light Co. RECIPIENT AFFILIATION

MILLER, J.R. Operating Reactors Branch 3

SUBJECT: Forwards addl info re crack growth rates & westinghouse methodology for determining temps for calculating crack growth rates, in response to NRC 840409 request. Info will be included in next FSAR update.

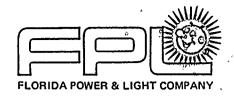
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L-84-198 August 6, 1984

Office of Nuclear Reactor Regulation

Attention:

Mr. James R. Miller, Chief

Operating Reactors Branch #3
Division of Licensing

U. S. Nuclear Regulatory Commission

Washington, D.C. 20555

Dear Mr. Miller:

Re: St. Lucie Unit No. 2 Docket No. 50-389 Turbine Disc Inspection

During NRC review of Florida Power & Light Company letter L-84-97, dated April 9, 1984, additional information was requested.

Attachment I provides the information requested concerning crack growth rates and reinspection intervals. This information will be included in the next update to the St. Lucie Unit 2 FSAR.

Attachment 2 provides the information requested concerning Westinghouse's methodology for determining temperatures for the purpose of calculating crack growth rate.

Should you require any further information, please call.

Very truly yours,

J. W. Williams, Jr. Group Vice President Nuclear Energy

JWW/RJS/cab

**Attachments** 

FEORLE ... SERVING PEOPLE

## FLORIDA POWER & LIGHT COMPANY

## ST. LUCIE UNIT 2

		TEMP				A <sub>CR</sub> ,		CRACK GROWTH RATE			REINSPECTION TIME MONTH			
		00	INLET	OUTLET	€,	Kıc	BORE	KEAMAA*	BORE INLET	BORE EXIT	KEYWAY	BORE INLET	BORE EXIT	KEYWAY
Rotor TN	8194													
Disc 1	GOV	84.3	438	324	116	246.6	7.458	4.002	.1618	.0496	.02527	DRY	75.2	79.2
Disc 2	GOV	88.0	280	263	126.2	185.8	3.883	1.904	.0370	.02935	.01496	52.4	66.2	63.6
Disc 1	GEN	84.3	438	324	111.0	173.8	3.705	1.800	.1377	.0422	.02151	DRY	43.9	41.8
Disc 2	GEN	88.0	280	·263	127.3	168.5	3.196	1.501	.0382	.0303	.01542	41.9	52.8	48.7
ROTOR TN	8195							<u>.</u>					•	
Disc 1	GOV	84.3	438	324	112.9	178.4	3.900	1.914	.1451	.04449	.02268	DRY	43.8	42.2
Disc 2	GOV	88.0	280	263	129.1	159.8	2.872	1.311	.04012	.03181	.01621	35.8	45.1	40.4
Disc 1	GEN	84.3	438	324	115.2	176.8	3.830	1.873	.1547	.04743	.02417	DRY .	40.4	38.8
Disc 2	GEN	88.0	280	263	131.5	169.0	3.212	1.511	.04289	.03401	.01733	37.4	47.2	43.59

$$A_{CR} = \frac{Q}{\Pi \times 1.21} \left\{ \frac{1.2K_{1c}}{C_0} \right\}^2$$

TIME (MONTHS) = 
$$\frac{1/2 (A_{CR} - \rho)}{da/dt \times 730}$$

Ln da/dt = 
$$\frac{-7302}{460 + \text{Temp}} + .0278 \sigma_y - \frac{3.531}{4.205}$$
 (BORE) (KEYWAY)

$$\rho$$
= KEYWAY RADIUS = 0.375

 $<sup>^{\</sup>star}A_{CR}$  for the Keyway has the radius subtracted from the calculated value.

ATTACHMENT 2



Westinghouse Electric Corporation **Power Generation** 

Steam Turbine Generator Division

The Quadrangle University Boulevard at Alafaya Trail Orlando Florida 32817

RECEIVED

JUL 3 1 1984

July 18, 1984

Nuclear Licensing

Mr. Stan Shepherd Florida Power & Light Company P.O. Box 529100 Miami, Florida 33152

Subject: St. Lucie Unit #2

Dear Mr. Shepherd:

This letter will document a Telecon in which S. Shepherd (FP&L), R. Stevens (FP&L), W. Hazelton (NRC), R. Sells (NRC) and M. Schlatter (Westinghouse) participated. The purpose of the call was to address concerns which were raised by J. Schiffens review of FP&L's recent FSAR which contained disc inspection interval calculations for the St. Lucie Unit #2.

At issue was the method for determing the appropriate temperatures at a shrunk on disc bore and keyway for the purpose of calculating crack growth rate. Westinghouse confirmed that we use the disc metal temperature at a point two inches from the disc outlet face to calculate keyway crack growth rate. Likewise, the temperature at a point two inches from the inlet face is used in the bore crack growth rate expression. These temperatures are determined on an individual unit basis using the relationships between local steam temperature and disc metal temperature as determined by two dimensional steady state heat transfer analysis.

This procedure is consistant with the convention used to establish the growth rate expressions; i.e., all actual keyway data points used in the regression analysis were assigned temperatures corresponding to that two inches from the exit face. The bore points were treated similarly.

The significance of selecting the locations two inches from the disc faces is that these represent the average temperatures of the local areas where cracking had been observed.

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There has been no change in the method of establishing these temperatures since the acceptance of the methodology described in MSTG-1-P "Criteria for Low Pressure Nuclear Turbine Disc Inspection" by the NRC in 1981.

Regards,

J. H. Sturges

Customer Project Management

Southeast Area

cc: W. Caperton

M. Schlatter

Miami 00610-PGS \*

Orlando 00707-205

JHS/ep