## TSD 14-014

## End State Surface Areas, Volumes, and Source Terms of Ancillary Buildings

## Revision 3



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Summary of Changes in this Revision:

- Rev. 2 - Added interior walls to Section A and E of the Main Steam Tunnels. Updated Figures 16, 17 and Tables 19, 20, 21, 25 and 60 with interior walls and a column in the Main Steam Tunnel Valve Houses.
- Rev. 3 - Added Buttress Pits


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## 1. PURPOSE

The purpose of this technical support document (TSD) is to calculate the end state surface areas, volumes and source terms of structures other than the Reactor Buildings and Auxiliary Building. The ancillary buildings encompass those whose substructures below the 588 foot elevation will remain in the end state and have the basement fill model applied but will not have significant source term remaining or have not yet been characterized because they are in use. The Spent Fuel Pool and Transfer Canal may have significant source term remaining but have not been characterized. The Waste Water Treatment Facility (WWTF) is also in use but source terms are expected to be minimal. Turbine Building and Crib House/Forebay characterization data indicate these structures have minimal contamination as well.

## 2. DISCUSSION

As discussed in the Reactor Building and Auxiliary Building technical support documents, (1) (2), the Exelon and ZionSolutions Asset Sale Agreement (3) requires all systems, structures, and components (SSCs) or "improvements" to be removed to 3 feet below finish grade of site (e.g., 588' elevation). Scoping and characterization surveys have been performed in all the substructures that will remain in the end state except for those in the Spent Fuel Building whose end state spent fuel pool and transfer canal substructures are inaccessible. The Unit 1 and 2 Reactor Buildings, Auxiliary Building and Spent Fuel Building end state structures are anticipated to contain the bulk of the end state radioactive source term and bound the potential future dose to the maximally exposed member of the critical group. The Containments and Auxiliary Building end state concrete has been characterized and the structures have separate detailed TSDs to estimate end state surface areas, volumes and source terms. The ancillary buildings addressed in this TSD are shown in yellow in Figure 1and consist of the Turbine Building, Crib House, Waste Water Treatment Facility (WWTF) and Spent Fuel Building. All other site buildings such as the Service Building and Diesel Generator Buildings will not have substructures below the 588 foot elevation remaining in the end state.

Scoping and characterization surveys indicate that the Turbine Building and WWTF contain detectable source terms at this time. The Turbine Building end state source term will consist of limited, localized embedded source term in the embedded piping in the concrete floor and source term in the floor drains. The floor drain characterization data and source term estimates are discussed in TSD 14-016 on end state embedded and buried pipe and penetrations. The equipment and floor drains in the 560 foot elevation slab will remain in the end state. The source term in the concrete floor has been characterized by scanning with a floor monitor and limited collection of concrete cores.

The WWTF is an operating facility required for National Pollutant Discharge Elimination System (NPDES) permit compliance. Therefore characterization has been limited to direct radiation and removable contamination surveys. Scoping surveys and cores in the Crib House have not detected radionuclides above background.


Figure 1- Ancillary Structures

## 3. CALCULATION

### 3.1. Turbine Building

### 3.1.1. End State Configuration

The turbine building end state will consist of the peripheral walls of the 560 foot elevation and associated Diesel Generator Building Oil Storage rooms, steam tunnels and discharge tunnels as shown in Figure 2 and Figure 3. It is possible that the walls between the Diesel Generator Oil storage rooms and the Turbine Building may be removed to create better access for commodity removal.


Figure 2 - Structures Evaluated as Part of Turbine Building Complex


Figure 3 - Unit 1 Turbine Building Side
The Turbine Building has large concrete structures that support the Condensers, Turbine and Generators that are solid past the 588' elevation. The Circulating Water Intake and Discharge pipes are embedded in concrete above the 560 elevation. The steam tunnels are at the 570 ' elevation and the Diesel Generator Oil Storage rooms are at the 567’ elevation. The Turbine Building sits on top of the Discharge Tunnels which also have multiple elevations as seen in Figure 4.


Figure 4 - Discharge Structure Side View
Thus, although all these areas are connected in the end state, the Turbine Building structure is complex.

### 3.1.2. Discharge Structure Surface Areas and Volumes

The Unit 1 and 2 Discharge Tunnels are identical. As seen in Figure 2and Figure 4 the Unit 1 and Unit 2 Discharge Tunnels run from under the Turbine Building Section A where two 12 foot diameter Circulating Water discharge pipes open to the tunnel from above, dip down under the Circulating Water Intake Pipe and then up again in Section B and then the section C portion to the

Valve House where it connects to the 14 foot diameter discharge pipe to the lake. The 14 foot diameter discharge pipe will be grouted closed at the valve house and is not considered part of the calculation. The details and dimensions of the discharge structure are provided in Drawings (DWG) B-100, B-38 and B-39 as a composite sketch in Figure 5.

DWG B-39
DWG B-38
DWG B-100


Figure 5-Composite of Discharge Tunnel Dimensions
Section A is located under the Turbine Building as shown in Figure 6. A side view is provided in Figure 7.


Figure 6 - Top View of Turbine Building Floor Over Section A of Discharge Tunnel


Figure 7 - Side View of Section A from B-100
A top view of the Section A tunnel floor is provided in Figure 8.


Figure 8 - Top View of Discharge Tunnel Section A Floor
The calculated surface areas of the floors, ceilings and walls are provided in Table 1.
Table 1 - Discharge Tunnel Wall Ceiling and Floor Surface Areas

| Section | Item | Length ft | Width ft | Surface <br> Area per <br> Item ft $^{2}$ | No <br> Items | Total <br> Surface <br> Area ft $^{2}$ |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: |
| A1 | Floor | 5.19 | 13.92 | 72.16 | 1 | 72.16 |
| A1 | Ceiling | 3.67 | 13.92 | 51.03 | 1 | 51.03 |
| A1 | N \& S Wall | 3.78 | 10.17 | 38.43 | 2 | 76.85 |
| A1 | West Wall | 13.00 | 8.33 | 108.33 | 1 | 108.33 |
| A2 | Floor \& Ceiling | 12.33 | 17.92 | 220.97 | 2 | 441.94 |
| A2 | N \& S Wall | 12.71 | 12.00 | 152.55 | 2 | 305.11 |
| A3 | Floor \& Ceiling | 18.50 | 21.00 | 388.50 | 2 | 777.00 |
| A3 | N \& S Wall | 18.50 | 12.00 | 222.00 | 2 | 444.00 |
| A4 | Floor | 13.12 | 21.00 | 275.61 | 1 | 275.61 |
| A4 | Ceiling | 12.50 | 21.00 | 262.50 | 1 | 262.50 |
| A4 | N \& S Wall | 12.50 | 14.00 | 125.00 | 2 | 250.00 |
|  |  |  |  |  |  |  |

The floor length of section A1the hypotenuse of a $3^{\prime} 8^{\prime \prime}$ by $3^{\prime} 8^{\prime \prime}$ triangle or the square root of 44 " squared plus $44^{\prime \prime}$ squared or 5.19 feet. The mid-point width of A1 floor is $13^{\prime} 11^{\prime \prime}$ resulting in a surface area of 5.19 feet times 13.92 feet or 72.16 square feet. The A1 ceiling is $3^{\prime} 8^{\prime \prime}$ by $13^{\prime} 11$ " or
51.03 square feet. The north and south wall lengths are the square root of $3^{\prime} 8^{\prime \prime}$ squared plus $11^{\prime \prime}$ squared or 3.78 feet. Their height is the mid-point of the $3^{\prime} 8^{\prime \prime}$ triangle plus the $8^{\prime} 4{ }^{\prime \prime}$ from the top of the slant or $10^{\prime} 2^{\prime \prime}$. Each walls surface rea is 3.78 feet times 10.17 feet or 38.43 square feet each. There is also a back west wall in Section A1 that is intersected by the 48 " stand pipe and the 48 " Service Water Return pipe. Assuming these are plugged closed, the resulting surface rea is the 13 ' width times the $8^{\prime} 4^{\prime \prime}$ height or 108.33 square feet. As seen in Figure 9 the Discharge Tunnel is surrounded by concrete which creates a void space in the $7^{\prime} 8^{\prime \prime}$ foot thick $560^{\prime}$ elevation floor and extends below it $12^{\prime} 10^{\prime \prime}$.


Figure 9-Discharge Structure Section A1-A3 Front View from B-91
As seen in Figure 7, the length of the Section A portion of the tunnel is $12^{\prime} 6^{\prime \prime}+34^{\prime} 6^{\prime \prime}+17^{\prime}$ or 64 feet long. As seen in Figure 9, $12^{\prime} 10^{\prime \prime}$ is below the $7^{\prime}$ thick 560 foot elevation floor slab. The volume uncorrected for void space is $49^{\prime} 6^{\prime \prime}+12^{\prime} 10^{\prime \prime}$ or $62^{\prime} 4^{\prime \prime}$ times the $12^{\prime} 10^{\prime \prime}$ height and the $64^{\prime}$ length which equals $51,196.44$ cubic feet (cf).

The void space of section A1 of the tunnel is that of the bottom 3' 8 " high slant at the start of the tunnel and the $8^{\prime} 4^{\prime \prime}$ by $3^{\prime} 8^{\prime \prime}$ thick wall portion above it. As seen in Figure 8 the width changes from 13 ' at the start to $14^{\prime} 10^{\prime \prime}$ at the junction with section A2. The slant volume is $3^{\prime} 8^{\prime \prime}$ by $13^{\prime} 11^{\prime \prime}$ by $1^{\prime} 10^{\prime \prime}$ (i.e. $1 / 2$ of $3^{\prime} 8^{\prime \prime}$ ) or 93.55 cf . All of this volume is below the $7^{\prime} 8^{\prime \prime}$ thick floor slab. The portion above the slant is $8^{\prime} 4^{\prime \prime}$ by $3^{\prime} 8^{\prime \prime}$ by $13^{\prime} 111^{\prime \prime}$ or 425.23 cf of which 297.667 cf is below the $7^{\prime} 8^{\prime \prime}$ thick floor slab. Section A2 void space is 12 feet high by $12^{\prime} 4^{\prime \prime}$ long with a width that tapers from $14^{\prime} 10^{\prime \prime}$ to $21^{\prime}$. The void space volume is $12^{\prime} 4^{\prime \prime}$ by $17^{\prime} 11^{\prime \prime}$ by $12^{\prime}$ or $2,651.67 \mathrm{cf}$ of which 1,289 is below the $7^{\prime} 8^{\prime \prime}$ thick slab. Section A3 is $18^{\prime} 6^{\prime \prime}$ long by 21 feet wide and 12 feet high or 4,662 cf of which $2,266.25 \mathrm{cf}$ is below the 7 ' 8 "' floor slab. Section A4 tapers downward $546^{\prime} 6^{\prime \prime}$ to $542^{\prime} 6^{\prime \prime}$ for a hypotenuse length of $133^{\prime} 1.5^{\prime \prime}$. The volume of A4 is $12^{\prime} 6^{\prime \prime}$ long by $21^{\prime}$ wide by an average of 14 ' high or $3,675 \mathrm{cf}$ of which $2,056.25 \mathrm{cf}$ is below the $7^{\prime} 8^{\prime \prime}$ floor slab. The Section A void space volumes are summarized in Table 2.

Table 2 - Section A of Discharge Tunnel Void Space Volumes

| Section | Item | Length ft | Width ft | Height ft | Total Volume per Item $\mathrm{ft}^{3}$ | Total <br> Vol in <br> 7'8" <br> Floor <br> $\mathbf{f t}^{3}$ | Total <br> Vol <br> Below7' <br> Floor <br> ft $^{3}$ <br> 93.55 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A1 | Slant | 13.92 | 3.67 | 1.83 | 93.55 | 0.00 | 93.55 |
| A1 | Above Slant | 13.92 | 3.67 | 8.33 | 425.23 | 127.57 | 297.66 |
| A2 |  | 17.92 | 12.33 | 12.00 | 2651.67 | 1362.66 | 1289.00 |
| A3 |  | 21.00 | 18.50 | 12.00 | 4662.00 | 2395.75 | 2266.25 |
| A4 |  | 21.00 | 12.50 | 14.00 | 3675.00 | 1618.75 | 2056.25 |
|  |  |  |  | Totals | 11507 | 5505 | 6003 |

The concrete volume corrected for void space is $45,193.73$ cubic feet.
As seen in Figure 5 Section B of the tunnel is outside the footprint of the Turbine Building and has three changes in elevation. The tunnel floor elevation drops by $5^{\prime} 6 "$ from $542^{\prime} 6 "$ to 537 '.


Figure 10 - Section B Side View from B-100 and B-38
The sloped ceiling of section B1 is the hypotenuse of $20^{\prime} 3$ in by 5 ' $6^{\prime \prime}$ triangle. It is the square root of $20^{\prime} 3^{\prime \prime}$ squared plus $5^{\prime} 6^{\prime \prime}$ squared or approximately 21 feet. Then there is a $2^{\prime} 3$ " horizontal section for a total ceiling length of 23.23 feet. At 21 feet wide this equals a ceiling surface area of 487.91 square feet. The sloped floor of B1 is the hypotenuse of a $22^{\prime} 6^{\prime \prime}$ by $5^{\prime} 6^{\prime \prime}$ triangle or 23.15 feet. At 21
feet wide the surface area is 486.41 square feet. The floor to ceiling height is 16 feet. The wall surface area is $22^{\prime} 6^{\prime \prime}$ by $16^{\prime}$ or 360 square feet per wall.
The ceiling length of section B2 is 5 feet plus $32^{\prime} 6^{\prime \prime}$ plus $13^{\prime} 33^{\prime \prime}$ minus $2^{\prime} 33^{\prime \prime}$ or $50^{\prime} 6^{\prime \prime}$. At 21 feet wide the floor and ceiling surface area is 2,121 square feet. At 16 feet high the north and south wall surface areas are 1,616 square feet.

Section B3 rises $22^{\prime} 7^{\prime \prime}$ from $537^{\prime}$ elevation to $559^{\prime} 7$ '. The B3 floor and ceiling length is hypotenuse of a $39^{\prime} 1.5^{\prime \prime}$ by $22^{\prime} 7^{\prime \prime}$ triangle or approximately $45^{\prime} 2$,"plus the $4^{\prime} 3.5^{\prime \prime}$ horizontal section or $49^{\prime} 5.5^{\prime \prime}$. At 21 feet wide this equals a total surface area of $2,077.60$ square feet. The walls are $49^{\prime} 5.5^{\prime \prime}$ by 16 feet high or 791.47 square feet each. The interior surface areas of section B are provided in Table 3.

Table 3 - Discharge Tunnel Section B Surface Areas

| Section | Item | Length ft | Width ft | Surface <br> Area per <br> Item ft | No Items | Total <br> Surface <br> Area ft $^{2}$ |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: |
| B1 | Ceiling | 23.23 | 21.00 | 487.91 | 1 | 487.91 |
| B1 | Floor | 23.16 | 21.00 | 486.41 | 1 | 486.41 |
| B1 | N \& S Wall | 22.50 | 16.00 | 360.00 | 2 | 720.00 |
| B2 | Ceiling \& Floor | 50.50 | 21.00 | 1060.50 | 2 | 2121.00 |
| B2 | N \& S Wall | 50.50 | 16.00 | 808.00 | 2 | 1616.00 |
| B3 | Ceiling \& Floor | 49.47 | 21.00 | 1038.80 | 2 | 2077.60 |
| B3 | N \& S Wall | 49.47 | 16.00 | 791.47 | 2 | 1582.93 |

Once again the entire interior volume of Section B is below the 579 foot elevation of the water table. The interior volume is the horizontal wall lengths of each section times the 21 foot width and 16 foot height. The interior volumes of each Section are provided in Table 4.

Table 4 - Discharge Tunnel Section B Interior Volumes

| Section | Item | Length ft | Width ft | Height ft | Total <br> Volume <br> per Item <br> $\mathbf{f t}^{3}$ |  |  |  |  |  |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| B1 | Downward Sloping | 22.50 | 21.00 | 16.00 | 7560.00 |  |  |  |  |  |
| B2 | Horizontal | 50.50 | 21.00 | 16.00 | 16968.00 |  |  |  |  |  |
| B3 | Upward Sloping | 49.47 | 21.00 | 16.00 | 16620.77 |  |  |  |  |  |
|  |  |  |  |  |  |  |  | Totals |  | $\mathbf{4 1 1 4 9}$ |

The wall and floor thicknesses vary over the length of Section B. In Section B the walls are 3'3" thick, adding 6'6" to the width or 27.5 feet wide. The Floor wall and ceiling concrete volumes are summarized in Table 5.

Table 5 - Discharge Tunnel Section B Floor Wall and Ceiling Concrete Volumes

| Section | Item | Length ft | Width ft | $\begin{gathered} \text { Thickness } \\ \mathrm{ft} \end{gathered}$ | Concrete Volume per Item $\mathbf{f t}^{3}$ | No Items | Total Concrete Volume per Item $\mathbf{f t}^{3}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| B1 | Ceiling | 22.50 | 27.50 | 4 | 2475.00 | 1 | 2475.00 |
| B1 | Floor | 22.50 | 27.50 | 7 | 4331.25 | 1 | 4331.25 |
| B1 | N \& S Wall | 22.50 | 16.00 | 3.25 | 1170.00 | 2 | 2340.00 |
| B2 | Ceiling | 50.50 | 27.50 | 2.5 | 3471.88 | 1 | 3471.88 |
| B2 | Floor | 50.50 | 27.50 | 4 | 5555.00 | 1 | 5555.00 |
| B2 | N \& S Wall | 50.50 | 16.00 | 3.25 | 2626.00 | 2 | 5252.00 |
| B3 | Ceiling | 49.47 | 27.50 | 3 | 4080.99 | 1 | 4080.99 |
| B3 | Floor | 49.47 | 27.50 | 3.5 | 4761.16 | 1 | 4761.16 |
| B3 | N \& S Wall | 49.47 | 16.00 | 3.25 | 2572.26 | 2 | 5144.52 |
|  |  |  |  | Total | 31043.54 | Total | 37411.80 |

Section C of the Discharge Tunnel is the horizontal run to the Valve House where it connects the 14 foot diameter discharge pipe. The 14 foot discharge pipe will be plugged in the end state to close off contact with the lake. As seen in Figure 11, the width of the tunnel transitions from 21 feet wide to 17 feet wide and the wall thickness from $3^{\prime} 3^{\prime \prime}$ thick to $2^{\prime} 6^{\prime \prime}$ thick in Section C of the tunnel.


Figure 11 - Discharge Tunnel Section C Transition Top View

Figure 12 shows the side view of Section C including the valve house. Section C1 before the taper from 21 feet with to 17 feet wide starts is 3 feet long by 16 feet high and 21 feet wide. The floor and ceiling of the 7 foot long tapered section of C2 has an average with of 19 feet with wall lengths that are the square root of 7 feet squared plus 2 feet squared or 7 ' 3.4 '. The length of the Section C3 ceiling and floor is the distance from the taper to the inner wall of the Valve House or 152 ' 7 '" plus the 2 ' 6 " width of the wall or $155^{\prime} 1{ }^{\prime \prime}$. The $155^{\prime} 1$ "' length times the 17 ' wide floor and ceiling is $2,636.42$ square feet each. The north and south walls surface areas are 155 ' 1 " times the 16 foot height or $2,481.33$ square feet. Sections C4 and C5 will have no ceilings since remaining top elevation in the end state is the 588 '. The only ceiling surface area will be the bottom of the wall in C 4 at the $575^{\prime}$ elevation which is 3 feet thick and 17 feet wide or 51 square feet. The floor of C 4 has a 6 feet long section that rises 2 feet from $559^{\prime} 7^{\prime \prime}$ to $561^{\prime} 7$ '". The hypotenuse floor length is 6.32 feet. The horizontal 3 foot section at the $561^{\prime} 7$ '' results in a 9.32 foot long C4 floor that is 158.52 square feet.


Figure 12 - Discharge Tunnel Section C Side View
The north and south walls of C4 include the 3 foot wide by 14 ' high portion under the wall which is 42 square feet and the mid-point height of $560^{\prime} 7^{\prime \prime}$ to the $588^{\prime}$ elevation or $27^{\prime} 5^{\prime \prime}$ by the 6 foot length which is 159 square feet. C4 also includes the east west walls above $575^{\prime} 7^{\prime \prime}$ which are $12^{\prime} 5^{\prime \prime}$ high by 21 ' wide or 260.75 square feet each.
Section C5 is 12 feet long by 23 feet wide per drawing B-39. The C5 floor is 12 feet by 23 feet or 276 square feet. The north and south walls are 12 wide feet by 27 ' 5 " high or 329 square feet each. The east wall of C5 with the $14^{\prime}$ diameter pipe plugged is $23^{\prime}$ wide by $27^{\prime} 5$ ' high or 630.58 square feet. The west wall is the same surface area with the $14^{\prime}$ by 17 ' opening from C4 subtracted or 392.58 square feet. The Section C surface areas are summarized in Table 6.

Table 6 - Discharge Tunnel Section C Interior Surface Areas

| Section | Item | Length ft | Width ft | Surface <br> Area per <br> Item ft $^{2}$ | No Items | Total <br> Surface <br> Area ft $^{2}$ |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: |
| C1 | Ceiling \& Floor | 3.00 | 21.00 | 63.00 | 2 | 126.00 |
| C1 | N \& S Wall | 3.00 | 16.00 | 48.00 | 2 | 96.00 |
| C2 | Ceiling \& Floor | 7.00 | 19.00 | 133.00 | 2 | 266.00 |
| C2 | N \& S Wall | 7.28 | 16.00 | 116.48 | 2 | 232.96 |
| C3 | Ceiling \& Floor | 155.08 | 17.00 | 2636.42 | 2 | 5272.83 |
| C3 | N \& S Wall | 155.08 | 16.00 | 2481.33 | 2 | 4962.67 |
| C4 | Ceiling | 3.00 | 17.00 | 51.00 | 1 | 51.00 |
| C4 | Floor | 9.32 | 17.00 | 158.52 | 1 | 158.52 |
| C4 | N \& S Wall | 3.00 | 14.00 | 42.00 | 2 | 84.00 |
| C4 | N \& S Wall | 6.00 | 27.42 | 164.50 | 2 | 329.00 |
| C4 | E \& W Wall | 12.42 | 21.00 | 260.75 | 2 | 521.50 |
| C5 | Floor | 12.00 | 23.00 | 276.00 | 1 | 276.00 |
| C5 | N \& S Wall | 12.00 | 27.42 | 329.00 | 2 | 658.00 |
| C5 | E Wall | 23.00 | 27.42 | 630.58 | 1 | 630.58 |
| C5 | W. Wall | 23.00 | 27.42 | 392.58 | 1 | 392.58 |
|  |  |  |  |  |  |  |

The void space below the water table ( $579^{\prime}$ level) of Section C1 through C3 is the floor surface areas times the 16 foot tunnel height.

| Section | Item | Surface Area ft2 | Height ft | Total Volume per Item $\mathbf{f t}^{3}$ |
| :---: | :---: | :---: | :---: | :---: |
| C1 | Pre Taper | 63.00 | 16.00 | 1008.00 |
| C2 | Taper | 133.00 | 16.00 | 2128.00 |
| C3 | Post Taper | 2636.42 | 16.00 | 42182.67 |
| Totals |  |  |  | 45319 |

The void space volume of Section C4 is half of the 6' by 17' by 2' high section below the 561 ' 7 '" elevation and the volume from the $561^{\prime} 7$ inch to $579^{\prime}$ elevation that is $17{ }^{\prime} 5^{\prime \prime}$ high by 6 feet long by 17 feet wide. There is also a volume under the wall between C4 and C5 that is 3 feet long by 17 feet wide and $15^{\prime}$ high. The void space volume in Section C5 is 12 feet long by 23 feet wide and $18^{\prime} 5^{\prime \prime}$ high.

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Table 8 - Void Space of Section C4 and C5

| Section | Item | Length ft | Width ft | Height ft | $\begin{array}{c}\text { Total } \\ \text { (olume } \\ \text { per Item } \\ \mathbf{f t}^{3}\end{array}$ |
| :--- | :--- | :---: | :---: | :---: | :---: |
| C4 | Bottom Triangle | 6 | 17 | 1 | 102 |
| C4 | Gap to 579' | 6 | 17 | 17.42 | 1777 |
| C4 | Under Wall | 3 | 17 | 14 | 714 |
| C5 | To 579' | 12 | 23 | 18.42 | 5083 |
|  |  |  |  |  | Totals |$] \mathbf{7 6 7 6}$.

The Section C concrete volumes of the end state floors, walls and ceilings are summarized in Table 9.

Table 9 - Discharge Tunnel Section C Estimated Floor, Ceiling and Wall Concrete Volumes

| Section | Item | Length ft | Width ft | Thickness ft | Surface <br> Area per <br> Item ft ${ }^{3}$ | No Items | Total Surface Area ft ${ }^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| C1 | Ceiling | 3.00 | 27.50 | 2.5 | 206.25 | 1 | 206.25 |
| C1 | Floor | 3.00 | 27.50 | 2.75 | 226.88 | 1 | 226.88 |
| C1 | N \& S Wall | 3.00 | 16.00 | 3.25 | 156.00 | 2 | 312.00 |
| C2 | Ceiling | 7.00 | 25.50 | 2.5 | 446.25 | 1 | 446.25 |
| C2 | Floor | 7.00 | 25.50 | 2.75 | 490.88 | 1 | 490.88 |
| C2 | N \& S Wall | 7.28 | 16.00 | 3.25 | 378.57 | 2 | 757.13 |
| C3 | Ceiling | 155.08 | 22.00 | 2.5 | 8529.58 | 1 | 8529.58 |
| C3 | Floor | 155.08 | 22.00 | 2.75 | 9382.54 | 1 | 9382.54 |
| C3 | N \& S Wall | 155.08 | 16.00 | 2.5 | 6203.33 | 2 | 12406.67 |
| C4 | Floor | 6.00 | 22.00 | 2.75 | 363.00 | 1 | 363.00 |
| C4 | Floor | 6.00 | 22.00 | 1 | 132.00 | 1 | 132.00 |
| C4 | N \& S Wall | 6.00 | 27.42 | 2.5 | 411.25 | 2 | 822.50 |
| C4 | W Wall | 17.00 | 9.92 | 2.5 | 421.46 | 1 | 421.46 |
| C4 | East Wall | 29.00 | 31.17 | 3 | 1997.50 | 1 | 1997.50 |
| C5 | Floor | 15.00 | 29.00 | 3.75 | 1631.25 | 1 | 1631.25 |
| C5 | N \& S Wall | 15.00 | 27.42 | 3 | 1233.75 | 2 | 2467.50 |
| C5 | E Wall | 23.00 | 27.42 | 3 | 1891.75 | 1 | 1891.75 |
|  |  |  |  | Total | 26020.27 | Total | 33253.17 |

The ceiling of Section C 1 is $2^{\prime} 6^{\prime \prime}$ thick by 3 feet long. The ceiling width is the 21 foot width of the tunnel interior plus the 3 ' $3^{\prime \prime}$ thick walls or $27^{\prime} 6^{\prime \prime}$ wide. The floor of C 1 is $2^{\prime} 9^{\prime \prime}$ thick, by 3 feet long and 27.5 feet wide when the 3 ' 3 " wall thicknesses are included. The C 1 north and south walls are 3 feet long by $3^{\prime} 3{ }^{\prime \prime}$ thick by 16 feet high. The C 2 tunnel ceiling is $2^{\prime} 6$ " thick by 7 feet long times an average width of 19 feet plus the $6^{\prime} 6^{\prime \prime}$ ' of the walls or 25.5 feet wide. The floor has the same dimensions but is $2^{\prime} 9^{\prime \prime}$ thick. The walls are 7.28 feet long by 16 feet high and 3.25 inches thick. The
ceiling of C3 is 2 ' 6 " thick by $155^{\prime} 1$ " long. The width is 17 feet plus the 5 feet from the $2^{\prime} 6^{\prime \prime}$ thick walls or 22 feet. The floor is the same dimensions but $2^{\prime} 9^{\prime \prime}$ thick. The north and south walls are $155^{\prime} 1$ " long by 16 feet high and $2^{\prime} 6$ " thick.
The floor of C4 is the $22\left(17+2.5^{*} 2\right)$ foot wide $2^{\prime} 9$ " thick by 6 foot long section plus the 6 foot by 22 foot with a 1 foot high mid-point of the sloped floor section on top of it. The horizontal portion of the floor under the east wall will be included in the concrete volume of the wall. The volume of the north and south walls is the mid-point height of $27^{\prime} 5$ " by the 6 foot length and the $2^{\prime} 6^{\prime \prime}$ wall thickness. That portion corresponding to the east wall will be calculated as part of the volume of the east wall. The west wall portion above the ceiling is 17 feet plus 5 feet for the $2^{\prime} 6^{\prime \prime}$ walls wide or 22 feet wide, $2^{\prime} 6$ inches thick and its height is from the top of the ceiling at $578^{\prime} 1$ " to the $588^{\prime}$ elevation or $9^{\prime} 11$ ". The east wall of C 4 is 3 feet thick, 29 feet wide (i.e., width of C 5 with the 3 foot wall thicknesses are included) and $31^{\prime} 2^{\prime \prime}$ high with a $14^{\prime}$ by 17 ' opening. The floor of C5 is 29 feet wide by 15 feet long and 3 ' $9 \prime$ ' thick. The north and south walls are 15 feet long 27'5" high by 3 feet thick. The east wall of C5 assumes the 14 foot diameter pipe that penetrates it is plugged with concrete or grout and is therefore 23 feet wide by 27 ' 5 " high and 3 feet thick.

The Discharge Tunnel calculated surface areas, void space below the water table and end state concrete volumes are summarized in Table 10.

Table 10 - Discharge Tunnel Calculated Surface Areas, Void Space and Concrete Volumes

| Section | Surface Area <br> $\mathbf{f t}^{\mathbf{2}}$ | Total Void <br> Below Space <br> $\mathbf{5 7 9}^{\prime} \mathbf{f t}^{\mathbf{3}}$ | Total End <br> State <br> ${\text { Concrete } \mathbf{f t}^{\mathbf{3}}}$ |
| :--- | :---: | :---: | :---: |
| A | 3065 | 11507 | 45193.73 |
| B | 9092 | 41149 | 37411.80 |
| C | 14058 | 52994 | 33253.17 |
| Total | $\mathbf{2 6 , 2 1 4}$ | $\mathbf{1 0 5 , 6 5 0}$ | $\mathbf{1 1 5 , 8 5 9}$ |

### 3.1.3. Unit 1 and 2 Surface Areas and Volumes

The Turbine Building basement is at the 560' elevation for the Unit 1 and 2 Areas and has the Common Area between them. The Unit basement areas consist of an area where the Condenser Pedestals are on the East Side of the Building, a Hallway, the Main Steam Tunnel and the Diesel Generator Oil Storage Area on the West side as shown in Figure 13. The Unit 1 and 2 areas are mirror images of each other. Since the next floor is the 592 foot elevation and the Main Steam Tunnels will be access from above, it is assumed there are no ceilings in the Turbine Building end state structure. In order to expedite material load out and commodity removals using large excavators it is also assumed the all interior walls such as those between tanks in the Diesel Generator Oil Storage Area and between the Common Area and Units 1 and 2 are removed. The only walls assumed to remain are those between the Diesel Generator Oil Storage Area and the West Hallway of the Turbine Building.
The Diesel Generator Oil Storage Area and West Hallway are relatively simple geometries for calculation of surface areas, void spaces and concrete volumes. The Diesel Generator Oil Storage Area floor is at the 567 '6" elevation making the walls 20 ' 6 ' high to the $588^{\prime}$ '. The West Hallway of the Turbine Building is at the $560^{\prime}$ elevation making the walls to the $588^{\prime}$ elevation 28 feet high.


Figure 13 - Turbine Building End State Unit 1 Area Example
The estimated floor and wall surface areas for the Diesel Generator Oil Storage Area and West Hallway of a single Unit are provided in Table 11.
Table 11 - Estimated Surface Areas for Diesel Generator Oil Storage Area and Turbine Building West Hallway

| Area | Length <br> $\mathbf{f t}$ | Width <br> $\mathbf{f t}$ | Surface <br> Area | No <br> Items | Total <br> Surface <br> Area ft $^{2}$ |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Diesel Oil Storage Room Floor | 80 | 39.75 | 3180 | 1 | 3180 |
| Diesel Oil Storage Room N\&S Wall | 41 | 20.5 | 840.5 | 2 | 1681 |
| Diesel Oil Storage Room E\&W Wall | 83 | 20.5 | 1701.5 | 2 | 3403 |
| West Hall Way Floor | 169.25 | 32.5 | 5500.63 | 1.00 | 5500.63 |
| West Hallway South Wall | 32.5 | 28 | 910 | 1 | 910 |
| West DG Wall | 82 | 28 | 2296 | 1 | 2296 |
| West Wall Below Main Steam Tunnel | 20 | 10 | 200 | 1 | 200 |

$\left.\begin{array}{|c|c|c|c|c|c|}\hline \text { Area } & & & & & \begin{array}{c}\text { Length } \\ \text { ft }\end{array}\end{array} \begin{array}{c}\text { Width } \\ \mathbf{f t}\end{array} \quad \begin{array}{c}\text { Surface } \\ \text { Area }\end{array} \quad \begin{array}{c}\text { Notal } \\ \text { Items }\end{array}\right\}$

The void space to the water table is the surface area of the floor times the distance to the $579^{\prime}$ elevation as seen in Table 12

Table 12 - Estimated Water Table Void Spaces for Diesel Generator Oil Storage Area and West Hallway

| Item | Length <br> ft | Width <br> ft | Height to <br> Water <br> Table ft | Total Volume <br> per Item ft $^{3}$ |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Diesel Oil Storage | 80.00 | 39.75 | 11.50 | 36570.00 |  |  |  |
| West Hallway Floor | 169.25 | 32.50 | 19.00 | 104511.88 |  |  |  |
|  |  |  |  |  |  | Totals | $\mathbf{1 4 1 0 8 2}$ |

The floor concrete volume calculations included the portion under the walls for the Diesel Generator Oil Storage Area. The wall volumes were from the floor elevation to the 588' end state elevation. Only the South wall of the West Hallway was considered for concrete volume since the West Wall was already included in the Auxiliary Building concrete volume estimates.

Table 13 - Estimated Floor and Wall Concrete Volumes for Diesel Generator Oil Storage Area and West Hallway

| Item |  |  |  | Concrete <br> Volume <br> per Item <br> $\mathbf{f t}^{3}$ | Total <br> No <br> Items | Cength <br> Colume <br> per Item <br> $\mathbf{f t}^{3}$ |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Diesel Oil Storage Room Floor | 85.00 | 44.25 | 7.67 | 28836.25 | 1 | 28836.25 |
| DG Oil Store South Wall | 39.75 | 20.50 | 3 | 2444.63 | 1 | 2444.63 |
| DG Oil Store North Wall | 39.75 | 20.50 | 2 | 1629.75 | 1 | 1629.75 |
| DG Oil Store East Wall | 83.50 | 28.00 | 1.5 | 3507.00 | 1 | 3507.00 |
| DG Oil Store West Wall | 85.00 | 20.50 | 3 | 5227.50 | 1 | 5227.50 |
| West Hallway Floor | 173.25 | 32.50 | 7.67 | 43168.13 | 1 | 43168.13 |
| West Hallway South Wall | 32.50 | 28.00 | 4 | 3640.00 | 1 | 3640.00 |
|  |  |  |  |  |  |  |
|  |  | Total | $\mathbf{8 8 4 5 3 . 2 5}$ | Total | $\mathbf{8 8 4 5 3 . 2 5}$ |  |

The Condenser Pedestal Area contains massive concrete buttresses that will remain in the end state. These consist of the North and South Circulating Water Intakes to the Condenser and the Circulating Water Discharge from the Condenser to the Discharge Tunnel in between them as shown in Figure 13. The South Condenser pedestal area extends past West Hallways southern wall and includes two large backfilled void spaces as shown in Figure 14 and Figure 15


Figure 14 - Top View of South Condenser Pedestal Area

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Figure 15 - Side View of South Condenser Pedestal Area from Drawing B-90
As seen in Figure 15 there is a $583^{\prime} 6^{\prime \prime}$ concrete floor above the backfilled void spaces that will form a solid slab up to and around the key way cut out at the $572^{\prime}$ elevation and the pit around the intake pipe on the 567 ' elevation. This is $76^{\prime} 2$ inches by $66^{\prime} 6^{\prime \prime}$ or 5,065 square feet minus the keyway surface area of $22^{\prime}$ by $9^{\prime}(128 \mathrm{sq} \mathrm{ft})$ and $16^{\prime}$ by $33^{\prime}(429 \mathrm{sq} \mathrm{ft})$ or $4,438.08$ square feet at the $583 \prime 6{ }^{\prime}$ '. The wall surface areas will be those accessible from the $560^{\prime}$ elevation and those associated with the keyway. The 560 ' floor area north of the pedestal is also include in the calculations.
The North Condenser Pedestal is very similar to the South Condenser Pedestal with the exception of not having the extended length from the backfilled areas as seen in Figure 13. All the dimensions are identical with the exception of the $34^{\prime} 6$ " West Wall length. The calculated surface areas for the South and North Condenser Pedestal Areas are provided in Table 14.

Table 14 - South Condenser Pedestal Surface Areas

| Area | Length <br> ft | Width ft | Surface <br> Area | No <br> Items | Total <br> Surface <br> Area ft $^{2}$ |
| :--- | :---: | :---: | :---: | :---: | :---: |
| South Condenser Pedestal 583'6" Floor | 76.17 | 66.5 | 4339.0833 | 1 | 4339.083 |
| S. Cond Ped KeyWay 572' Surface Area | 9 | 22 | 198 | 1 | 198 |
| S. Cond Ped Keyway 567' Surface Area | 16 | 33 | 528 | 1 | 528 |
| S. Cond Ped West Wall with Hallway | 33.25 | 23.5 | 781.375 | 1 | 781.375 |
| S. Cond Ped N. Wall Minus 572' Opening | 61.5 | 23.5 | 1192.25 | 1 | 1192.25 |
| S. Cond Ped E\&W 572' Access Walls | 9 | 11.5 | 103.5 | 2 | 207 |
| S. Cond Ped Interior 567' Key Way Walls Without 572' <br> Access Cut out | 98 | 16.5 | 1364 | 1 | 1364 |


| Area | Length <br> $\mathbf{f t}$ | Width ft | Surface <br> Area | No <br> Items | Total <br> Surface <br> Area ft $^{2}$ |
| :--- | :---: | :---: | :---: | :---: | :---: |
| North 560' Floor Area | 26 | 61.5 | 1599 | 1 | 1599 |
|  |  | Totals | $\mathbf{1 0 1 0 5 . 2 0 8}$ |  | $\mathbf{1 0 2 0 8 . 7 1}$ |
| North Condenser Pedestal 583'6' Floor | 34.50 | 66.5 | 1568.25 | 1 | 1568.25 |
| N. Cond Ped KeyWay 572' Surface Area | 9 | 22 | 198 | 1 | 198 |
| N. Cond Ped Keyway 567' Surface Area | 16 | 33 | 528 | 1 | 528 |
| N. Cond Ped West Wall with Hallway | 34.5 | 23.5 | 810.75 | 1 | 810.75 |
| N. Cond Ped S. Wall Minus 572' Opening | 61.5 | 23.5 | 1192.25 | 1 | 1192.25 |
| N. Cond Ped E\&W 572' Access Walls | 9 | 11.5 | 103.5 | 2 | 207 |
| N. Cond Ped Interior 567' Key Way Walls Without 572' <br> Access Cut out | 98 | 16.5 | 1364 | 1 | 1364 |
| South 560' Floor Area | 26 | 61.5 | 1599 | 1 | 1599 |
|  |  | Totals | $\mathbf{7 3 6 3 . 7 5}$ |  | $\mathbf{7 4 6 7 . 2 5}$ |

Most of the south Condenser pedestal is above the water table at $583^{\prime} 6{ }^{\prime}$ '. Only the keyway openings are below the $579^{\prime}$ elevation. The geometry is complicated and it is not known if the partially embedded pipe will be grouted and left below 567 ' elevation or not. For conservatism only, the volume above $572^{\prime}$ elevation in the keyway will be calculated. The void space above the 560 ' elevation floor area north of the pedestal is also included in the calculations. The North Condenser Pedestal has identical void spaces below the water table.

Table 15 - South Condenser Pedestal Void Space to Water Table

| Item | Length ft | Width <br> ft | Height <br> to <br> Water <br> Table ft | Total <br> Volume <br> eer Item <br> $\mathbf{f t}^{3}$ |
| :--- | :---: | :---: | :---: | :---: |
| S. Condenser Pedestal Above 572' | 9.00 | 22.00 | 7.00 | 1386.00 |
| S. Condenser Pedestal Above 572' | 16.00 | 33.00 | 7.00 | 3696.00 |
| S. Condenser Pedestal N 560' Floor | 26.00 | 61.50 | 19.00 | 30381.00 |
|  |  |  | Totals | $\mathbf{3 5 4 6 3}$ |
| N. Condenser Pedestal Above 572' | 9.00 | 22.00 | 7.00 | 1386.00 |
| N. Condenser Pedestal Above 572' | 16.00 | 33.00 | 7.00 | 3696.00 |
| N. Condenser Pedestal N 560' Floor | 26.00 | 61.50 | 19.00 | 30381.00 |
|  |  |  | Totals | $\mathbf{3 5 4 6 3}$ |

The concrete volume of the South Condenser pedestal is the overall pedestal volume including the 7' 8 " thick floor below the 560 ' elevation, minus the backfill volume and the keyway volume as shown in Table 16. The 7 ' $8^{\prime \prime}$ thick floor of the area north of the pedestal and its 5 foot thick east wall are included in the volume estimate. The configuration is the same for the North Condenser pedestal area with the exception of the shorter length and absence of backfilled areas.

Table 16 - South Condenser Pedestal and North Floor Area and Wall Concrete Volumes

| Item | Length <br> ft |  | Width <br> ft | Thickness <br> ft | Concrete <br> Volume <br> per Item <br> $\mathbf{f t}^{3}$ | Total <br> No <br> Items |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Concrete <br> Volume <br> per Item <br> $\mathbf{f t}^{3}$ |  |  |  |  |  |  |
| S. Condenser Pedestal | 76.17 | 66.50 | 30.75 | 155758.13 | 1 | 155758.13 |
| Small Backfill Volume | -12.50 | 38.00 | 20.17 | -9580.75 | 1 | -9580.75 |
| Large Backfill Volume | -24.75 | 50.50 | 22.17 | -27709.73 | 1 | -27709.73 |
| 572' EL Keyway | -9.00 | 22.00 | 11.5 | -2277.00 | 1 | -2277.00 |
| 567' EL Keyway | -16.00 | 33.00 | 16.5 | -8712.00 | 1 | -8712.00 |
| S. Cond Pedestal N 560; Floor | 26.00 | 66.50 | 7.67 | 13261.43 | 1 | 13261.43 |
| S. Con Ped N 560' Fl East <br> Wall | 26.00 | 28.00 | 5 | 3640.00 | 1 | 3640.00 |
|  | 34.60 | 66.50 | 30.75 | 70752.68 | 1 | 70752.68 |
| N. Condenser Pedestal | -9.00 | 22.00 | 11.5 | -2277.00 | 1 | -2277.00 |
| 572' EL Keyway | -16.00 | 33.00 | 16.5 | -8712.00 | 1 | -8712.00 |
| 567' EL Keyway | 26.00 | 66.50 | 7.67 | 13255.67 | 1 | 13255.67 |
| N. Cond Pedestal N 560; <br> Floor | 26.00 | 28.00 | 5.00 | 3640.00 | 1 | 3640.00 |
| N. Con Ped S 560' Fl East <br> Wall |  |  | Total | $\mathbf{7 6 6 5 9 . 3 4}$ | Total | $\mathbf{7 6 6 5 9 . 3 4}$ |

The remaining condenser pedestal area is the center Circulating Water Discharge Pedestal located over the Discharge Tunnel as shown in Figure 3, Figure 6, Figure 7, and Figure 13. As seen in Figure 6, the Discharge Pedestal is $49^{\prime} 6$ ' long by $66^{\prime} 6$ '" wide when the width of the $5^{\prime}$ thick east wall is included. The lowest elevation is $562^{\prime}$ which is $38^{\prime}$ by $49^{\prime} 6^{\prime \prime}$ minus the surface areas of the four $8^{\prime}$ by 7' pedestals. The calculated surface areas for the Center Discharge Condenser Support Pedestal are provided in Table 17.

Table 17 - Estimated Surface Areas for Center Discharge Area Condenser Pedestal

| Area | Length <br> ft | Width ft | Surface <br> Area | Notal <br> Items | Surface <br> Area <br> $\mathbf{f t}^{2}$ |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Center Discharge Pedestal 562' Floor | 49.50 | 38 | 1657 | 1 | 1657 |
| Center Discharge Pedestal 580' 3/8" Pedestals | 8.00 | 7 | 56 | 4 | 224 |
| West Pedestal 588' Surface Area | 49.50 | 14.00 | 693 | 1 | 693 |
| East Pedestal 588' Surface Area | 49.50 | 10.67 | 528 | 1 | 528 |
| West Hallway Wall | 49.50 | 28 | 1386 | 1 | 1386 |
| West Pedestal Interior Wall | 49.50 | 26 | 1287 | 1 | 1287 |
| Center Discharge Pedestal 580' 3/8" Pedestals N\&S <br> Walls | 8.00 | 26 | 208 | 8 | 1664 |
|  |  | Totals | $\mathbf{5 8 1 5}$ |  | $\mathbf{7 4 3 9}$ |

The void space below the water table includes the $562^{\prime}$ surface area only since the tops of the four $7^{\prime}$ by $8^{\prime}$ pedestal are above the $579^{\prime}$ elevation. This is the surface area of $49.5^{\prime}$ by $38^{\prime}$ minus the four $7^{\prime}$ by $8^{\prime}$ pedestals times the height to the water table of 17 feet which equals 28,169 cubic feet.
The volume of concrete in the floor area of the center Pedestal is $49^{\prime} 6$ " by the $66^{\prime} 6^{\prime \prime}$ width times the $9^{\prime} 8^{\prime \prime}$ thickness of the floor minus the 5,505 cubic feet of discharge tunnel void space in Table 2.

Table 18 - Center Condenser Discharge Support Pedestal Concrete Volumes

| Item | $\begin{gathered} \text { Length } \\ \mathrm{ft} \\ \hline \end{gathered}$ | $\begin{gathered} \text { Width } \\ \text { ft } \end{gathered}$ | $\begin{gathered} \text { Thickness } \\ \text { ft } \end{gathered}$ | Concrete Volume per Item $\mathbf{f t}^{3}$ | No Items | Total <br> Concrete <br> Volume <br> per Item <br> ft $^{3}$ <br> 263 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Center Discharge Pedestal 562' Floor | 49.50 | 66.50 | 9.67 | 26315.52 | 1 | 26315.52 |
| Center Discharge Pedestal 580' 3/8" Pedestals | 7.00 | 8.00 | 26.00 | 1456.00 | 4 | 5824.00 |
| West 588' Pedestal | 49.50 | 14.00 | 26.00 | 18018.00 | 1 | 18018.00 |
| East 588' Pedestal | 49.50 | 10.67 | 26.00 | 13728.00 | 1 | 13728.00 |
|  |  |  | Total | 59517.52 | Total | 63885.52 |

As shown in Figure 2, each unit has a Main Steam Tunnel that runs from the west end of the containments into the Turbine Building adjacent to the Diesel Generator Oil Storage Area at the 570 ' elevation. The feedwater, main steam and other piping will be removed by removing the ceiling to the wall at the $588^{\prime}$ elevation. The details of the western portion of the Unit 1 Main Steam Tunnel are provided in Figure 16.


Figure 16 - Western Portion of Unit 1 Main Steam Tunnel
The calculated surface areas of the Main Steam Tunnel floors and walls are provided in Table 19.
Table 19- Main Steam Tunnel Floor and Wall Surface Areas

| Area | Length <br> ft | Width ft | Surface <br> Areaft $^{2}$ | No <br> Ntems | Total <br> Surface <br> Area ft ${ }^{2}$ |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Section A Main Steam Floor | 33.83 | 26 | 879.67 | 1 | 879.67 |
| Section A Main Steam Walls | 33.83 | 18 | 609 | 2 | 1218 |
| W1 Sides | 7.00 | 18 | 126 | 2 | 252 |
| W1 Ends | 2.00 | 18 | 36 | 2 | 72 |
| W2 Sides | 9.50 | 18 | 171 | 2 | 342 |
| W2 End | 3.00 | 18 | 54 | 1 | 54 |
| W3 Sides | 9.50 | 18 | 171 | 2 | 342 |
| W3 End | 3.00 | 18 | 54 | 1 | 54 |
| W4 Beam Sides | 2.00 | 18 | 36 | 2 | 72 |
| Section B Main Steam Floor | 23.08 | 6 | 138.5 | 1 | 138.5 |
| Section B Main Steam Walls | 23.08 | 18 | 415.5 | 1 | 415.5 |


| Area | Length <br> $\mathbf{f t}$ | Width ft | Surface <br> Area ft $^{2}$ | No <br> Items | Total <br> Surface <br> Area ft $^{2}$ |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Section C Main Steam Floor | 23.00 | 12 | 276 | 1 | 276 |
| Section C Main Steam Walls | 23.00 | 18 | 414 | 2 | 828 |
| Section D Main Steam Floor | 196.00 | 12 | 2352 | 1 | 2352 |
| Section D Main Steam Walls | 196.00 | 18 | 3528 | 2 | 6840 |
| Section E Main Steam Floor | 33.83 | 26 | 879.67 | 1 | 879.67 |
| Section E Main Steam Walls | 33.83 | 18 | 609 | 2 | 1218 |
| W1 Sides | 7.00 | 18 | 126 | 2 | 252 |
| W1 Ends | 2.00 | 18 | 36 | 2 | 72 |
| W2 Sides | 9.50 | 18 | 171 | 2 | 342 |
| W2 End | 3.00 | 18 | 54 | 1 | 54 |
| W3 Sides | 9.50 | 18 | 171 | 2 | 342 |
| W3 End | 3.00 | 18 | 54 | 1 | 54 |
| W4 Beam Sides | 2.00 | 18 | 36 | 2 | 72 |
| Section F Main Steam Floor | 7.83 | 26 | 203.67 | 1 | 203.67 |
| Section F Main Steam Wall | 15.80 | 18 | 284.40 | 1 | 284.40 |
| Section G Main Steam Floor | 75.50 | 20 | 1510.00 | 1 | 1510.00 |
| Section G Main Steam Floor | 34.35 | 2.5 | 85.89 | 1 | 85.89 |
| Section G Main Steam Floor | 2.00 | 12 | 24.00 | 1 | 24.00 |
| Section G Main Steam West Wall | 33.15 | 18 | 596.63 | 1 | 596.63 |
| Section G East Main Steam Wall | 75.50 | 18 | 1359.00 | 1 | 1359.00 |
| Section H Main Steam Floor | 64.25 | 20 | 1285.00 | 1 | 1285.00 |
| Section H Main Steam West Wall | 20.00 | 18 | 360.00 | 1 | 360.00 |
| Section H Main Steam South Wall | 44.25 | 18 | 796.50 | 1 | 796.50 |
| Section H Main Steam North Wall | 64.25 | 18 | 1156.50 | 1 | 1156.50 |
|  |  | Totals | $\mathbf{1 9 0 5 8 . 9 1}$ |  | $\mathbf{2 5 0 8 2 . 9 1}$ |

As seen in Figure 16, Section A is $33^{\prime} 10^{\prime \prime}$ long by $26^{\prime}$ wide, with a $2^{\prime} 6^{\prime \prime}$ floor. Section B equals a rectangle surface area of $23^{\prime} 1^{\prime \prime}$ by 6 feet (e.g., half the width). The total length of Section D is 196 feet for the South wall and $196^{\prime}$ minus $12^{\prime}$ or $184^{\prime}$ for the North wall. The remaining Main Steam Tunnel configuration is shown in Figure 17.


Figure 17 - Unit 1 East Section of Main Steam Tunnel
The surface area of the Section F floor is equal to the surface area of 17 ' 10 " (half the $15^{\prime} 8^{\prime \prime}$ wall) by $26^{\prime}$ rectangle. Section G includes the $2^{\prime} 6^{\prime \prime}$ setback for the west wall and the 2 foot setback for the point at which Section D ends.
Since the entire tunnel is at the 570' elevation, the void space below the water table is the floor surface area times the 9 foot depth from the water table.

Table 20 - Unit 1 Main Steam Tunnel Void Space Below Water Table

|  | Length ft | Width <br> $\mathbf{f t}$ | Height <br> to <br> Water <br> Table $\mathbf{f t}$ | Total <br> Volume <br> per Item <br> $\mathbf{f t}^{3}$ |
| :--- | :---: | :---: | :---: | :---: |
| Section A Main Steam Floor | 33.83 | 26 | 9.00 | 7917.00 |
| W1 Interior Wall | 7.00 | 2.00 | 9.00 | -126.00 |
| W2 Interior Wall | 9.50 | 3.00 | 9.00 | -256.50 |
| W3 Interior Wall | 9.50 | 3.00 | 9.00 | -256.50 |

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| Item | Length ft | Width <br> ft | Height <br> to <br> Water <br> Table ft | Total <br> Volume <br> per Item <br> ft ${ }^{\mathbf{3}}$ |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| W4 Beam | 2.00 | 2.00 | 9.00 | -36.00 |  |  |  |  |  |
| Section B Main Steam Floor | 23.08 | 6 | 9.00 | 1246.50 |  |  |  |  |  |
| Section C Main Steam Floor | 23.00 | 12 | 9.00 | 2484.00 |  |  |  |  |  |
| Section D Main Steam Floor | 196.00 | 12 | 9.00 | 21168.00 |  |  |  |  |  |
| Section E Main Steam Floor | 33.83 | 26 | 9.00 | 7917.00 |  |  |  |  |  |
| W1 Interior Wall | 7.00 | 2.00 | 9.00 | -126.00 |  |  |  |  |  |
| W2 Interior Wall | 9.50 | 3.00 | 9.00 | -256.50 |  |  |  |  |  |
| W3 Interior Wall | 9.50 | 3.00 | 9.00 | -256.50 |  |  |  |  |  |
| W4 Beam | 2.00 | 2.00 | 9.00 | -36.00 |  |  |  |  |  |
| Section F Main Steam Floor | 7.83 | 26 | 9.00 | 1833.00 |  |  |  |  |  |
| Section G Main Steam Floor | 75.50 | 20 | 9.00 | 13590.00 |  |  |  |  |  |
| Section G Main Steam Floor | 34.35 | 2.5 | 9.00 | 772.97 |  |  |  |  |  |
| Section G Main Steam Floor | 2.00 | 12 | 9.00 | 216.00 |  |  |  |  |  |
| Section H Main Steam Floor | 64.25 | 20 | 9.00 | 11565.00 |  |  |  |  |  |
|  |  |  |  |  |  |  |  | Totals | $\mathbf{6 7 3 5 9}$ |

The calculated concrete volumes for the floors include the wall thicknesses. The East Wall of Section G and the South wall of section H concrete volumes were included in the Diesel Generator Oil Storage Area calculation. The north wall of Section H was included in the Auxiliary Building calculation.

The Section B floor is $1 / 2$ of the 12 ' plus $2^{\prime} 6^{\prime \prime}$ West wall thickness or 7.25 feet since the floor area under the East wall is included in the Section A width. The section B wall thickness is $2^{\prime} 6^{\prime \prime}$. The Section D North wall is the same as the South with the 12' gap created by Section 6 subtracted.

Table 21 - Calculated Main Steam Tunnel Floor and Wall Concrete Volumes

| Item | Length ft | Width ft | Thickness ft | Concrete Volume per Item $\mathrm{ft}^{3}$ | No Items | Total Concrete Volume per Item $\mathrm{ft}^{3}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Section A Main Steam Floor | 33.83 | 32 | 2.50 | 2706.67 | 1 | 2706.67 |
| Section A Main Steam Walls | 33.83 | 18 | 3.00 | 1827.00 | 2 | 3654.00 |
| W1 Interior Wall | 7.00 | 18 | 2.00 | 252.00 | 1 | 252.00 |
| W2 Interior Wall | 9.50 | 18 | 3.00 | 513.00 | 1 | 513.00 |
| W3 Interior Wall | 9.50 | 18 | 3.00 | 513.00 | 1 | 513.00 |
| W4 Beam | 2.00 | 18 | 2.00 | 72.00 | 1 | 72.00 |
| Section B Main Steam Floor | 23.08 | 7.25 | 2.50 | 418.39 | 1 | 418.39 |
| Section B Main Steam Walls | 23.08 | 18 | 2.50 | 1038.75 | 1 | 1038.75 |
| Section C Main Steam Floor | 23.00 | 12 | 2.50 | 690.00 | 1 | 690.00 |


| Item | $\begin{gathered} \text { Length } \\ \mathrm{ft} \end{gathered}$ | Width ft | Thickness ft | Concrete Volume per Item $\mathrm{ft}^{3}$ | No Items | Total <br> Concrete <br> Volume per Item $\mathrm{ft}^{3}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Section C Main Steam Walls | 23.00 | 18 | 2.00 | 828.00 | 2 | 1656.00 |
| Section D Main Steam Floor | 196.00 | 16 | 2.50 | 7840.00 | 1 | 7840.00 |
| Section D Main Steam Walls | 196.00 | 18 | 2.00 | 7056.00 | 2 | 13680.00 |
| Section E Main Steam Floor | 33.83 | 32 | 2.50 | 2706.67 | 1 | 2706.67 |
| Section E Main Steam Walls | 33.83 | 18 | 3.00 | 1827.00 | 2 | 3654.00 |
| W1 Interior Wall | 7.00 | 18 | 2.00 | 252.00 | 1 | 252.00 |
| W2 Interior Wall | 9.50 | 18 | 3.00 | 513.00 | 1 | 513.00 |
| W3 Interior Wall | 9.50 | 18 | 3.00 | 513.00 | 1 | 513.00 |
| W4 Beam | 2.00 | 18 | 2.00 | 72.00 | 1 | 72.00 |
| Section F Main Steam Floor | 7.83 | 32 | 3.00 | 752.00 | 1 | 752.00 |
| Section F Main Steam Wall | 15.80 | 18 | 3.00 | 853.20 | 1 | 853.20 |
| Section G Main Steam Floor | 75.50 | 23 | 2.00 | 3473.00 | 1 | 3473.00 |
| Section G Main Steam Floor | 34.35 | 2.5 | 2.00 | 171.77 | 1 | 171.77 |
| Section G Main Steam Floor | 2.00 | 12 | 2.00 | 48.00 | 1 | 48.00 |
| Section G Main Steam West Wall | 45.15 | 18 | 2.00 | 1625.25 | 1 | 1625.25 |
| Section H Main Steam Floor | 68.25 | 20 | 2.00 | 2730.00 | 1 | 2730.00 |
| Section H Main Steam Wall East | 20.00 | 18 | 4.60 | 1656.00 | 1 | 1656.00 |
|  |  |  | Total | 40947.69 | Total | 52053.69 |

The Common Area of the Turbine Building lies between each Unit 1 and 2. It contains a large sump as seen in Figure 18.

Table 22 - Common Area Floor and Wall Surface Areas

| Area | Length <br> ft | Width ft | Surface <br> Area | No <br> Items | Total <br> Surface <br> Area ft $^{2}$ |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Common Area Floor minus Fire Sump | 137.50 | 103.83 | 13818.08 | 1 | 13359.08 |
| Common Area West Wall | 137.50 | 28 | 3850.00 | 1 | 3850.00 |
| Common Area East Wall | 49.00 | 28 | 1372.00 | 2 | 2744.00 |
| Oil Room Floor | 47.60 | 38 | 1808.80 | 1 | 1808.80 |
| Oil Room North and South Walls | 34.00 | 28 | 952.00 | 2 | 1904.00 |
| Oil Room East Wall | 39.50 | 28 | 1106.00 | 1 | 1106.00 |
| Fire Sump Floor | 19.13 | 24 | 459.00 | 1 | 459.00 |
| Fire Sump Walls N\&S to 549'4" EL | 19.13 | 10.67 | 204.00 | 2 | 408.00 |
| Fire Sump Walls E\&W to 549'4" EL | 24.00 | 10.67 | 256.00 | 2 | 512.00 |
| Fire Sump Pump Area Walls Interior 549'4" EL | 4.00 | 10.67 | 42.67 | 3 | 128.00 |
| Fire Sump Pump Area Walls Exterior 549'4' EL | 5.00 | 10.67 | 53.33 | 2 | 106.67 |


| Area | Length <br> ft | Width ft | Surface <br> Area | No <br> Items | Total <br> Surface <br> Area ft $^{2}$ |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Fire Sump Pump Area Walls Exterior 549'4" EL | 6.00 | 10.67 | 64.00 | 1 | 64.00 |
| Fire Sump Walls N\&S to 540'4" EL | 7.00 | 9.00 | 63.00 | 2 | 126.00 |
| Fire Sump Walls E\&W to 540'4" EL | 7.00 | 9.00 | 63.00 | 2 | 126.00 |
|  |  | Totals | $\mathbf{2 4 1 1 1 . 8 8}$ |  | $\mathbf{2 6 7 0 1 . 5 5}$ |
|  |  |  |  |  |  |

The sump interior is $19^{\prime} 1.5^{\prime \prime}$ wide and $24^{\prime}$ long. There is a $7^{\prime}$ by $7^{\prime}$ opening below which the sump floor is at $540^{\prime} 4^{\prime \prime}$. The rest of the sump is at $549^{\prime} 4^{\prime \prime}$ and is covered by a $2^{\prime} 8^{\prime \prime}$ thick slab. It is assumed the slab will be removed in the end state to create access to the sump. There is a $4^{\prime}$ by $4^{\prime}$ portion of the sump enclosed by one foot thick walls. The surface areas for the elevator pit, valve pits and other sumps were not included in the estimated surface areas, void space or concrete volume calculations.


Figure 18 - Turbine Building Common Area and Oil Room
The void space to the water table included the fire sump volume and the volume taken up by the 29 2' by 4' by 2' support columns along the common wall with the Auxiliary Building and the Common Area South, East and North Walls was subtracted from the void space volume. For conservatism the void space volume of the elevator pit other valve pits and sumps were not included in the void space volume. The calculated void space volumes for the Common Area are provided in Table 23.

Table 23 - Common Area Void Space Volumes Below Water Table

| Item | Length ft | Width $\mathbf{f t}$ | $\begin{gathered} \text { Height } \\ \text { to } \\ \text { Water } \\ \text { Table ft } \\ \hline \end{gathered}$ | Total Volume per Item $\mathbf{f t}^{3}$ |
| :---: | :---: | :---: | :---: | :---: |
| Common Area | 137.50 | 103.83 | 19.00 | 271264.58 |
| Oil Room | 39.50 | 38 | 19.00 | 28519.00 |
| Fire Sump | 19.13 | 24 | 10.67 | 4896.00 |
| Fire Sump | 7.00 | 7 | 9.00 | 441.00 |
| 29 Columns On Interior Walls | -2.00 | 8 | 19.00 | -8816.00 |
|  |  |  | Totals | 305121 |

As seen in the upper sketch of Figure 3 the floor is thicker under the Common Area and under approximately 65.25 feet of the Unit 1 West Hallway along the 262 ' length of the Auxiliary Building wall. The floor also increases in thickness at the transition to the Auxiliary Building basement as seen in Figure 19.


Figure 19-Common Area Floor and Transition to Auxiliary Building Floor Thickness
This extends approximately 13 feet under the Common Area and West Hallway Area floors. An additional 4 feet is added to the length of the Common Area to account for portions of the floor
under the wall. The calculated concrete volumes of the Common Area floors and walls and of the increased slab thickness are summarized in Table 24.

Table 24 - Common Area Calculated Concrete Volumes

| Item | $\begin{gathered} \text { Length } \\ \text { ft } \end{gathered}$ | Width ft | Thickness ft | Concrete <br> Volume per <br> Item ft ${ }^{3}$ | No Items | Total Concrete Volume per Item $\mathbf{f t}^{3}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Common Area Floor | 137.50 | 107.83 | 14.67 | 217463.89 | 1 | 217463.89 |
| Common Area East Wall | 49.00 | 28 | 4.00 | 5488.00 | 2 | 10976.00 |
| Oil Room Floor | 47.50 | 38 | 14.67 | 26473.33 | 1 | 26473.33 |
| Oil Room North and South Walls | 34.00 | 28 | 4.00 | 3808.00 | 2 | 7616.00 |
| Oil Room East Wall | 39.50 | 28 | 4.00 | 4424.00 | 1 | 4424.00 |
| Fire Sump Floor Void | 19.13 | -24 | 10.67 | -4896.00 | 1 | -4896.00 |
| Fire Sump Floor Void | 7.00 | -7 | 9.00 | -441.00 | 2 | -882.00 |
| Fire Sump Pump Area Walls Exterior 549'4" EL | 4.00 | 4.00 | 1.00 | 16.00 | 2 | 32.00 |
| Fire Sump Pump Area Walls Exterior 549'4" EL | 6.00 | 4.00 | 1.00 | 24.00 | 2 | 48.00 |
| Total Columns On Interior Walls | 2.00 | 4 | 28.00 | 224.00 | 29 | 6496.00 |
| Slope Along Wall G | 262.79 | 10.85 | 4 | 11409.54 | 1 | 11409.54 |
| Five Foot Slab Along Wall G | 262.79 | 8.85 | 5 | 11634.01 | 1 | 11634.01 |
| Overlap Under Unit 1 | 62.65 | 32.50 | 7 | 14251.93 | 1 | 14251.93 |
|  |  |  | Total | 289879.69 | Total | 305046.69 |

The void space created by the Fire Sump was subtracted from the volume and the additional volume created by the twenty nine 2 ' by 4 foot columns that extend 28 feet from the $588^{\prime}$ to 560 ' were included in the concrete volume.

Table 25 - Summary of Turbine Building Surface Areas, Water Table Void Spaces and Concrete Volumes

| Item | Total Surface Area $\mathrm{ft}^{2}$ | Total Water Table Void Volume per Item $\mathrm{ft}^{3}$ | Total <br> Concrete Volume per Item $\mathrm{ft}^{3}$ |
| :---: | :---: | :---: | :---: |
| Unit 1 Discharge Tunnel | 26214 | 105650 | 115859 |
| Unit 1 Diesel Oil Storage | 8264 | 36570 | 41645 |
| Unit 1 West Hallway | 10790 | 104512 | 46808 |
| Unit 1 S. Condenser Pedestal | 10209 | 35463 | 124380 |
| Unit 1 N . Condenser Pedestal | 7467 | 35463 | 76659 |
| Unit 1 Center Discharge Pedestal | 7439 | 28169 | 63886 |
| Unit 1 Main Steam Tunnel | 25083 | 67359 | 53332 |
| Common Area | 26702 | 305121 | 305047 |
| Unit 2 Discharge Tunnel | 26214 | 105650 | 115859 |
| Unit 2 Diesel Oil Storage | 8264 | 36570 | 41645 |
| Unit 2 West Hallway Floor | 10790 | 104512 | 46808 |
| Unit 2 S. Condenser Pedestal | 10209 | 35463 | 124380 |
| Unit 2 N . Condenser Pedestal | 7467 | 35463 | 76659 |
| Unit 2 Center Discharge Pedestal | 7439 | 28169 | 63886 |
| Unit 2 Main Steam Tunnel | 25083 | 67359 | 53332 |
| Total TB Void Space | 2.18E+05 | 1.13E+06 | $1.35 \mathrm{E}+06$ |
| Without Discharge Tunnel | $1.65 \mathrm{E}+05$ | 9.20E+05 | $1.12 \mathrm{E}+06$ |

### 3.2. Crib House

The Crib House is located east of the Turbine Building and houses the Circulating Water Pumps and Service Water Pumps. As seen in Figure 20 and Figure 22, the lower elevation of the Crib House is open to the Forebay where the Unit 1 and Unit 2 Circulating Water Intake Pipes and the Ice Melting Lines are located.


Figure 20 - Crib House and Forebay Below Grade Side View
Since end state will require removal of all materials above the $588^{\prime}$ elevation and only structural materials and embedded piping and components can remain. The Service Water Pumps, Circulating Water Pumps and the associated interior structures will be removed. The overall layout is shown in Figure 20. The yellow highlighted walls are interior walls whose surface areas and volumes are calculated separately and then subtracted from the water table void space. As seen in Figure 21, there are flow splitters that also constitute interior walls highlighted in yellow.


Figure 21 - Overhead View of Crib House and Forebay Showing Flow Splitter Interior Walls
Figure 22 shows the hollowed out structure that will be used to calculate the surface area, concrete volume and void space of the overall shell with no interior floors or walls. Then the interior floor and wall surface areas, concrete volumes will be calculated and added to the shell totals. The concrete volumes below the water table will be subtracted from the void space.


Figure 22 - Crib House and Forebay Overhead View.
Pipes will be cut at the wall penetrations and those that are buried and will remain such as the Service Water Header and Circulating Water pipes will be plugged to prevent communication with the Forebay and end state structures such as the Discharge Tunnels, Turbine Building and Auxiliary Building. The top view dimensions are shown in Figure 23.


Figure 23 - Crib House and Forebay Top View Dimensions
The side view dimensions of the Forebay are provided in Figure 25. This shows a lower section with a floor at the 545 ' elevation that is 16 feet high. As seen in Figure 23 and Figure 24, 545, elevation consists of three fan shaped openings with flow splitting concrete structures in the middle of them. The calculated surface areas for the $545^{\prime}$ elevation of the Forebay intake structure are summarized in Table 26. As seen in Figure 24 the fan shaped floor areas surface area is equal to a $26^{\prime} 6^{\prime \prime}$ by 32 foot rectangle. The north and south walls of each fan are the square root of 32 ' squared and $10^{\prime} 6^{\prime \prime}$ squared or $33.68^{\prime}$. At a $16^{\prime}$ height each walls surface area is 538.86 square feet. There are two center points that extend four of the six north and south fan walls past the interior of side of the east wall of the Forebay. This additional wall length is the square root of $13^{\prime} 6^{\prime \prime}$ squared plus $3^{\prime} 9^{\prime \prime}$ squared or 14.01 feet when multiplied by the 16 foot height the surface area is 224.18 square feet for the additional length of each of these four sides.

There are two side and one center flow splitters. Each flow splitter consists of a rectangular center section and east and west triangular point. As seen in Figure 24, the wall between the triangular sections is 4 feet wide by 16 feet high. The length of the triangular walls are the square root of 7 ' squared plus 2.5 ' squared or 7.43 feet. This equals a surface area of 119.93 square feet for each side of the east and west points of the diamond. The walls between the triangular sections of the center flow splitter has center side $8^{\prime} 2.25^{\prime \prime}$ by 16 feet high for 131 square feet per side. The east and west points have the same 7 ' by $2.5^{\prime}$ dimensions as the points on the side flow splitters.


Figure 24 - Top View of Forebay 545' Elevation
The remaining interior surface areas consist of the $16^{\prime}$ by $16^{\prime}$ east wall of the fan that will be formed when the Circulating Water intake pipes are grouted closed and the $22^{\prime} 6^{\prime \prime}$ section on the north and south sides of the structure.

Table 26 - Forebay 545' Elevation Intake Structure Surface Areas

| Area | $\underset{\mathrm{ft}}{\text { Length }}$ | Width ft | Surface Area $\mathrm{ft}^{2}$ | No Items | Total Surface Area $\mathrm{ft}^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Side Intake Floor | 26.5 | 32 | 848 | 3 | 2544 |
| Intake Wall N\&S Walls | 33.68 | 16 | 538.86 | 6 | 3233.1 |
| Center Point | 14.01 | 16 | 224.18 | 4 | 896.7 |
| Side Flow Splitter | 4 | 16 | 64.00 | 4 | 256.0 |
| Side Flow Splitter Points | 7.43 | 16 | 118.93 | 8 | 951.4 |
| Center Flow Splitter | 8.19 | 16 | 131.00 | 2 | 262 |
| Center Flow Splitter Points | 7.43 | 16 | 118.93 | 4 | 475.7 |
| Intake East Wall Plugged Pipe | 16 | 16 | 256 | 3 | 768 |
| West Wall Interior | 22.5 | 16 | 360.00 | 2 | 720.0 |
|  |  | Totals | 2659.89 |  | 10107 |

The void space created by the fan shaped intakes is below the 579 ' water table. The volume taken up by the south, center and north flow splitters is subtracted from the fan shaped volume as seen in Table 27.

Table 27 - Forebay 545' Intake Structure Void Space Below 579' Water Table

| Item | $\begin{gathered} \text { Length } \\ \text { ft } \end{gathered}$ | Width ft | Height to Water Table ft | Total Volume per Item $\mathrm{ft}^{3}$ |
| :---: | :---: | :---: | :---: | :---: |
| Three Intake Areas | 26.50 | 32.00 | 16.00 | 40704.00 |
| South Flow Splitter | -5.00 | 11.00 | 16.00 | -880.00 |
| Center Flow Splitter | -5.00 | 15.19 | 16.00 | -1215.20 |
| North Flow Splitter | -5.00 | 11.00 | 16.00 | -880.00 |
|  |  |  | Totals | 37729 |



Figure 25 - Side View of Forebay with Dimensions

As seen in Figure 25, the floor under the $545^{\prime}$ intake structure is $9^{\prime}$ thick minus the $7^{\prime}$ by $3^{\prime}$ and $1.5^{\prime}$ | by 3 ' sections. The floor length and width, including the foot print under the walls is $179^{\prime}$ long by $21^{\prime}$ wide. The volume is $179^{\prime}$ by $21^{\prime}$ by $9^{\prime}$ minus the $179^{\prime}$ x 3 ' by $8.5^{\prime}$ area or $29,699.25$ cubic feet. The north and south walls of each fan shaped opening are 2 feet thick equaling $1,077.72$ cubic feet of concrete per wall. The volume of the center points of the two fans which extend past the interior wall 13 ' 6 " by 3 ' 9 " by 16 ' each. The volumes of the flow splitters were described above. The west portion of the interior wall is 4 feet thick and is split into 4 parts by the fan shaped openings. The south and north portions are $22.5^{\prime}$ by $4^{\prime}$ by $16^{\prime}$ high. There is an approximately $4^{\prime}$ by $5^{\prime}$ by $16^{\prime}$ section in each of the two center points on either side of the center fan shaped opening.

The east wall is 3 feet thick and has a north and south section 27 ' 5 inches long by $16^{\prime}$ high. There are two $23^{\prime} 3$ " long sections adjacent to the center fan shaped opening. There is also the $16^{\prime}$ by $16^{\prime}$ by 2 ' thick wall formed once the 16 ' diameter Circulating water pipes are sealed at the east side of each fan shaped opening. The calculated concrete volumes for the $545^{\prime}$ section of the Forebay intake structure are shown in Table 28.

Table 28 - Forebay 545’ Intake Structure Estimated Concrete Volumes without Interior Structures

| Item | Length <br> $\mathbf{f t}$ | Width <br> $\mathbf{f t}$ | Thickness <br> $\mathbf{f t}$ | Concrete <br> Volume <br> per Item <br> $\mathbf{f t}^{3}$ | No <br> Items | Total <br> Concrete <br> Volume <br> per Item ft |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Intake Area | 21.00 | 179.00 | 9.00 | 29669.25 | 1 | 29669.25 |
| N\&S Walls | 33.68 | 16.00 | 2 | 1077.72 | 6 | 6466.30 |
| Center Points | 13.50 | 16.00 | 3.75 | 810.00 | 2 | 1620.00 |
| South Flow Splitter | 5.00 | 11.00 | 16.00 | 880.00 | 2 | 1760.00 |
| Center Flow Splitter | 5.00 | 15.19 | 16.00 | 1215.20 | 4 | 4860.80 |
| North Flow Splitter | 5.00 | 11.00 | 16.00 | 880.00 | 1 | 880.00 |
| West Wall Interior | 22.50 | 16.00 | 4 | 1440.00 | 2 | 2880.00 |
| Center Point West Wall | 4.00 | 16.00 | 5 | 320.00 | 2 | 640.00 |
| East Wall Ends | 27.42 | 16.00 | 3 | 1316.00 | 2 | 2632.00 |
| East Wall Interior | 23.26 | 16.00 | 3 | 1116.40 | 2 | 2232.80 |
| Intake East Wall Plugged Pipe | 16 | 16 | 2 | 512.00 | 3 | 1536.00 |
|  |  |  |  |  |  |  |

As seen in Figure 25, there is a floor above the fan shaped intakes at the 562 ' elevation. This floor is $14^{\prime}$ by $171^{\prime}$ or 2394 square feet as seen in Table 29. The walls extend from $588^{\prime}$ to $562^{\prime}$ or $26^{\prime}$ and creates an interior void space below the 570 ' water table of $14^{\prime}$ by $171^{\prime}$ by $17{ }^{\prime}$ or 40,698 cubic feet as seen in Table 30. Twenty seven feet of the interior wall in the Forebay above the fan shaped openings was not included in the 545 ' elevation section which went to a height of 16 feet. The remaining surface area of the east Forebay interior wall is 171 ' by 27 ' or 4,617 cubic feet.

Table 29 - Forebay Intake Structure Surface Areas Above 562' Elevation without Interior Structures

| Area | $\underset{\mathrm{ft}}{\text { Length }}$ | Width ft | Surface Area | No Items | Total Surface Area $\mathbf{f t}^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Forebay Intake 562' Floor | 14 | 171 | 2394 | 1 | 2394 |
| Forebay Intake 562' Interior N\&S Walls | 14 | 26 | 364 | 2 | 728 |
| Forebay Intake 562' Interior E\&W Walls | 171 | 26 | 4446 | 2 | 8892 |
| Forebay Intake 562' Exterior W Wall | 171 | 27 | 4617 | 1 | 4617 |
|  |  | Totals | 11821 |  | 16631 |

Table 30 - Upper Forebay Intake Structure Void Space Below 579' Water Table without Interior Structures

|  |  |  | Height to <br> Water Table <br> It | Total Volume per <br> Item $\mathbf{f t}^{3}$ |
| :---: | :---: | :---: | :---: | :---: |
| Forebay Intake 562' | Length ft | Width ft | ( |  |

The concrete volume of the upper floor is $21^{\prime}$ wide by $179^{\prime}$ long and 3 feet thick equaling 11,277 cubic feet as seen in Table 31.

Table 31 - Forebay Upper Intake Structure Concrete Volumes without Interior Structures

| Item | $\underset{\mathrm{ft}}{\text { Length }}$ | $\underset{\mathbf{f t}}{\text { Width }}$ | Thickness ft | Concrete Volume per Item $\mathbf{f t}^{3}$ | No Items | Total Concrete Volume per Item $\mathrm{ft}^{3}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Forebay Intake 562' Floor | 21 | 179 | 3.00 | 11277 | 1 | 11277 |
| Forebay Intake 562' Interior N\&S Walls | 26 | 14 | 4.00 | 1456 | 2 | 2912 |
| Forebay Intake 562' E Wall | 26 | 179 | 3.00 | 13962 | 1 | 13962 |
| Forebay Intake 562' W Wall | 26 | 179 | 4.00 | 18616 | 1 | 18616 |
|  |  |  | Totals | 45311.0 |  | 46767.0 |

As seen in Figure 25, the Forebay floor drops 8 feet in elevation from the $545^{\prime}$ to the 537' elevation. The floor is 65 ' 11 inches long by $171^{\prime}$ wide for a surface area of $11,271.75$ square feet. The north and south walls extend from the $588^{\prime}$ to a mean elevation of $541^{\prime}$ or 47 ' such that each wall has a surface area of $3,078.5$ square feet. As seen in Figure 26 the floor of the Crib House extends 79'11" to the west wall, resulting in a $13,665.75$ square foot surface area. The north and south walls extend from $588^{\prime}$ to 537 ' or $51^{\prime}$ resulting in a surface area of $4,075.75$ square feet per wall. The west wall once all the penetrations are sealed will have a surface area of 51 ' by 171 ' or 8,721 square feet as seen in Table 32.

Table 32 - Forebay and Crib House End State Surface Areas without Interior Structures

| Area | Length <br> ft | Width <br> $\mathbf{f t}$ | Surface <br> Area | No <br> Items | Total <br> Surface <br> Area ft $^{2}$ |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Forebay Floor | 65.92 | 171 | 11271.75 | 1 | 11271.75 |  |  |  |  |  |
| Forebay South \& North Walls | 47 | 65.50 | 3078.50 | 2 | 6157.00 |  |  |  |  |  |
| Crib House Floor | 79.92 | 171 | 13665.75 | 1 | 13665.75 |  |  |  |  |  |
| Crib House South \& North Walls | 51 | 79.92 | 4075.75 | 2 | 8151.50 |  |  |  |  |  |
| Crib House West Wall | 51 | 171.00 | 8721.00 | 1 | 8721.00 |  |  |  |  |  |
|  |  |  |  |  |  |  | Totals | $\mathbf{4 0 8 1 2 . 7 5}$ |  | $\mathbf{4 7 9 6 7 . 0 0}$ |
|  |  |  |  |  |  |  |  |  |  |  |

The void space below the water table for the Forebay and Crib House are shown in Table 33.
Table 33 - Forebay and Crib House Void Space Below 579' Water Table without Interior Structures

|  |  |  | Height <br> to <br> Water <br> Table | Total <br> Volume <br> per Item <br> ftem |
| :--- | :---: | :---: | :---: | :---: |
| Forebay | 65.50 | 171 | 38 | 425619.00 |
| Crib House | 79.92 | 171 | 42 | 573961.50 |
|  |  | Width <br> ft | Totals | $\mathbf{9 9 9 5 8 1}$ |



Figure 26 - Crib House End State Side View
As seen in Figure 25, most of the sloped Forebay floor is $6^{\prime} 6^{\prime \prime}$ thick with the exception of a small section that is $9^{\prime}$ thick and $4^{\prime} 6^{\prime \prime}$ long near the Forebay intake structure. The bevel is $2^{\prime} 6^{\prime \prime}$ by $2^{\prime} 6^{\prime \prime}$ such that the additional volume of this small section equals $9^{\prime}$ minus $6^{\prime} 6^{\prime \prime}$ or $2^{\prime} 6^{\prime \prime}$ thick by $5^{\prime} 9^{\prime \prime}$ long and $179^{\prime}$ wide or 2,573 cubic feet. The Forebay floor is $65^{\prime} 11$ " long by $179^{\prime}$ wide and $6^{\prime} 6^{\prime \prime}$ thick or 73,266 cubic feet. The additional volume at the seam where the Forebay floor meets the Crib House floor is approximated by a rectangle $16^{\prime}$ by $179^{\prime}$ by $3^{\prime} 6^{\prime \prime}$ thick. The Crib House floor is 6 feet thick and the walls are 4 feet thick.

Table 34 - Forebay and Crib House End State Concrete Volumes without Interior Structures

| Item | Length <br> $\mathbf{f t}$ | Width <br> $\mathbf{f t}$ | Thickness <br> $\mathbf{f t}$ | Concrete <br> Volume <br> per Item <br> $\mathbf{f t}^{3}$ | Total <br> No <br> Items | Concrete <br> Volume <br> per Item <br> $\mathbf{f t}^{3}$ |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Additional Volume for Forebay 9' Thick Section | 5.75 | 179 | 2.50 | 2573 | 1 | 2573 |
| Forebay Floor | 65.92 | 179 | 6.50 | 76694 | 1 | 76694 |
| Additional Crib House Steam Volume | 16 | 179 | 3.50 | 10024 | 1 | 10024 |
| Forebay South \& North Walls | 47 | 65.50 | 4.00 | 12314 | 1 | 12314 |
| Crib House Floor | 83.92 | 179 | 6.00 | 90127 | 1 | 90127 |
| Crib House South \& North Walls | 51 | 83.92 | 4.00 | 17119 | 1 | 17119 |
| Crib House West Wall | 51 | 171.00 | 4.00 | 34884 | 1 | 34884 |

The Forebay and Crib House end state surface areas, void space below the water table and concrete volumes are summarized

Table 35 - Summary of Crib House \& Forebay Surface Areas, Water Table Void Space and Concrete Volumes without Interior Structures

$\left.$| Item | Total <br> Surface <br> Area ft $^{2}$ | Total Water <br> Table Void <br> Volume per <br> Item ft |
| :--- | :---: | :---: | :---: | | Total |
| :---: |
| Concrete |
| Volume |
| per Item ft | \right\rvert\,

The surface areas and concrete volumes of the interior walls and floors will be added to the Table 35 values. The surface area parameters and calculated surface areas of the internal walls and floors are provided in Table 36, concrete volumes are in Table 37. The calculation described below resulted in an additional $73,812.5$ square feet above the 74,705 square feet calculated for the area with no interior walls. This is a factor of 1.99 higher than the hollowed out structure.
As seen in Figure 26, the basket wall behind the stop log guide is 25 feet tall from the 588 foot to the 565 foot elevation. Figure 21 and Figure 23 show that it spans the entire 171 ' foot interior width of the forebay. This equals a 3,933 square foot surface area for each side or 7,866 square feet total. Fourteen feet is below the 570 foot elevation water table and the wall is 2 feet thick creating a void space of 4,788 cubic feet that will have to be subtracted from the overall void space volume if the wall remains in the end state. The overall concrete volume is 7,866 cubic feet of concrete.
As seen in Figure 22, there are also Circulating Water Pump intake flow splitters that have surface areas and volumes that need to be calculated if they remain in the end state. As seen in Figure 22Error! Reference source not found. there is a common splitter between Units 1 and 2 and each unit has three channels that are the same for Unit 1 and Unit 2. The details of the Unit 1 channel and flow splitter layout are provided in Figure 27.


Figure 27 - Top View Unit 1 Flow Splitters from B-46
The portions of the splitter walls past on the Forebay side (East Side) of the Stop Logs extend from the 537' floor elevation to the 565 foot elevation or 28 feet. As seen in the case of the Common splitter on the right of the figure, it extends 20 feet past the stop log guide resulting in a side surface area of 560 square feet per side. The top is 7 feet wide resulting in a surface area of 140 square feet and a concrete volume of 3920 cubic feet that must be subtracted from the void space below the water table.

There is a center flow splitter in each of the three channels whose height is at the 565 foot elevation. There are three per unit or 6 total. Each splitter is 13 feet long and 28 feet high equaling a surface area of 364 square feet per side or 4,368 square feet for all 12 sides. Each center flow splitter is 3 feet wide resulting in a top surface area of 39 square feet which is 234 square feet for all 6 center flow splitters. The concrete volume is 1,092 cubic feet per center flow splitter or 6,552 square feet for all 6 . This volume is subtracted from the volume below the water table.
There are two flow splitters per unit that are $15^{\prime} 113 / 8^{\prime \prime}$ ( 15.95 feet) long past the stop logs. At 28 feet high per side this equals 446.54 square feet per side or 3,572 square feet for both units. Drawing B-46 and B-47 show the tunnel flow splitters to be 3 feet thick for 47.84 square feet per top portion that is past the stop locks equaling 191.38 square feet for both units. This equals $1,339.63$ cubic feet per channel flow splitter or $5,358.5$ for all four. This volume will be subtracted from the overall void space if they are left in place.
The portions of the common and channel flow splitters inboard of the stop logs (West) to the Circ Water Pump tunnel intake at the slanted wall extend to the 588 foot elevation or 51 feet high. The distance from the stop logs to the pump intake tunnel is $36^{\prime} 6^{\prime \prime}$. This equals $1,861.5$ square feet per side for the common flow splitter and top surface area of 255.5 square feet. The concrete volume of the common flow splitter west of the stop logs is $13,030.50$ cubic feet or which 10,731 cubic feet is below the water table.

The two channel splitters per unit are 3 feet thick and extend the same distances and elevations on the west side of the stop log to the circulating pump intake tunnel, also equaling 1.861 .5 feet per side or 14,892 square feet for all 8 sides for both units. The channel splitters are 3 feet thick equaling a total top surface area of 438 square feet for all four. The volume of each is 5584.5 cubic feet or 22338 cubic feet for all four of which 18,648 is below the water table.

Each of the three channels has a slanted wall this 25 ’ 4 " wide. As seen in Figure 26, the slanted portion of the wall is from $579^{\prime} 3^{\prime \prime}$ to $552^{\prime} 3^{\prime \prime}$ or a 27 foot drop. The base of the triangle is 13 feet across as determined by dimensions on drawing B-53. The hypotenuse is 29.97 feet. The straight piece is 599 to $579^{\prime} 3^{\prime \prime}$ or 8.25 feet long. The surface area of the straight portion of each channel is 221.67 square feet per side with each of the 6 tunnel total have an interior and exterior surface this is 2,660 square feet for both units. Each slanted portion of the channel has a surface area of 759.16 square feet minus the 49.38 square feet of the $8^{\prime} 3 \prime$ ' by $6^{\prime}$ service water pump openings or 709.78 square feet for a total of $8,517.3$ square feet for all 12 sides of both units. Each wall is 2 feet thick resulting making the volume of the concrete 29.97 puss 8.75 or 38.72 feet by 25.33 feet by 2 feet minus 49.38 square feet by 2 feet for the opening which equals 1862.88 cubic feet per tunnel or $11,177.3$ cubic feet for all six tunnels. Nine feet of the wall is above the water table making the length below the water table 29.72 feet resulting in $9,626.42$ cubic feet below the water table.
The side walls and the back walls of the Service Pump areas also have surface areas requiring calculation. As seen in Figure 26, the sides of the Service Pump housing have rectangular section 13 feet deep by 8.75 feet or 113.75 square feet per side which is 1365 square feet for all 12 side areas. The concrete volume is an extra 2 feet wide on the front and 4 feet wide on the back. The four tunnel flow splitting walls are three feet thick. The rectangular side walls are 3 feet thick for a concrete volume of 840 cubic feet per wall or 3360 cubic feet for all four for both units. The Common splitter wall rectangular portion is 13 by 8.75 by 7 feet thick or 367.5 cubic feet of
concrete. Since the 8.75 feet goes to the $579^{\prime} 3 \prime \prime$ and the water table is at the $579^{\prime}$ none of this volume is in the water table.
As seen in Figure 26, the triangle section extends from approximately $579^{\prime} 3$ " to 553 ' 3 " or 26 feet. It has a 13 foot base, making the surface area $1 / 226$ by 13 feet or 169 square feet which is 2,028 for all twelve sides. The concrete volume of the two channel sides is $1 / 2$ of 19 feet by 26 feet by 3 feet thick or 741 cubic feet for one and 2964 cubic feet for all four. Since only three inches is above the water table it can all be considered below the water table. The Common splitter has the same dimensions but with a 7 foot thickness equaling a concrete volume of 1,729 cubic feet which is subtracted from the void space below the water table.

The back wall of each service pump area is 25 ' 4 " wide and from the 588 from elevation to approximately the $555^{\prime} 6^{\prime \prime}$ elevation or 823.33 square feet for each tunnel area resulting in 4,940 square feet for all 6 channel areas. The volume of the back walls is $25^{\prime} 4^{\prime \prime}$ by $32^{\prime} 6^{\prime \prime}$ by $4^{\prime}$ thick or 329.33 cubic feet per channel resulting in 19,760 cubic feet for all 7 channels. The amount below the water table is 23.5 by 25.33 by 4 feet for 6 channels or 14,288 cubic feet. The outer wall concrete volumes were included in the volume calculated for the shell.
The Circulating water intake tunnels extend from the $537^{\prime}$ to the $549^{\prime} 6^{\prime \prime}$ or $12^{\prime} 6^{\prime \prime}$. As seen in Figure 27, there is a slanted portion with $6^{\prime} 5^{\prime \prime}$ base and 14 height whose hypotenuse is 15.40 feet resulting in a surface area of 192.51 square feet per side or 2310.07 square feet for all 12 . The floor and ceiling surface areas of the funnel area are $12^{\prime} 6^{\prime \prime}$ plus the $3^{\prime} 2.5^{\prime \prime}$ with a midpoint of the $6^{\prime} 5^{\prime \prime}$ or 15.71 feet by 14 feet each. This equals 219.92 feet per floor surface which is 2369 square feet for all 12 floors and walls. The walls are 2 feet thick with the centers filled with sand. The concrete volume of each wall is 15.4 feet by 12.5 feet by 2 feet or 385.01 cubic feet per wall which is 4620.13 cubic feet for all 12 walls. There are two triangle shaped sand filled areas for each unit that are 12 ' 6 " high, by $6^{\prime} 5^{\prime \prime}$ "on a side wide by 14 feet. This results in a void space sand volume of $4,491.67$ cubic feet for all four areas. The common area is $7^{\prime} 11^{\prime \prime}$ by 14 feet of sand or 1385.42 cubic feet. The additional concrete on the outer walls is $6^{\prime} 5^{\prime \prime}$ by 14 by $12^{\prime} 6^{\prime \prime}$ or $1,129.55$ cubic feet.
There is also a rectangular portion of each intake tunnel which is where the pump veins are. There are two side walls that are $15^{\prime} 3^{\prime \prime}$ long by $12^{\prime} 6^{\prime \prime}$ high which is 190.63 square feet per wall or 2287.5 for all 12 . The side walls are also 2 feet thick with rest of the volume being filled with sand. The side walls are 381.25 cubic feet each or 4575 cubic feet for all 12 . The back walls are 2 feet thick on the interior surface of the cubicles as shown on B-56 Section TT. They have sump areas on the back side that range in bottom elevations from 556 to 532 bottom floor elevations. The interior walls of the circ water pump intake tunnels are $12^{\prime} 6^{\prime \prime}$ by $12^{\prime} 6^{\prime \prime}$ or 156.25 square feet or 937.5 square feet for all 6 . At two feet thick this equals 1875 cubic feet of concrete for all 6 .

The floors are $12^{\prime} 6$ " by 15 ' 3 " or 1143.75 square feet for all 6 . The concrete volume has already been calculated as part of the floor slab. The ceiling is a slab with 6 holes for the Circ Water Pumps that average $8^{\prime} 6^{\prime \prime}$ in diameter the bottom of the cone has an approximate radius of $7 \prime 3 \prime$ ". Each ceiling surface area is $12^{\prime} 6$ by $15^{\prime} 3^{\prime \prime}$ minus the $7^{\prime} 3^{\prime \prime}$ radius of the opening or 25.5 square feet per ceiling which is 152.97 square feet for all 6 ceilings.

The concrete floor of the tunnels run under is 171 feet wide by 29.25 feet wide with 6 circulating water pump shaft openings with an average radius of 4 ' 3 ". The slab is $558^{\prime}$ minus $549^{\prime} 6$ " or 8.5
feet thick. This is $39,634.48$ cubic feet when the cone shaped opening volume of the 6 pumps is subtracted.

As seen in B-44 and Figure 26, each sump area has a 3' by 3' hatch. There are 7 sump areas in all when the one behind the common splitter is included. The 552' elevation floor is $11^{\prime} 3^{\prime \prime}$ wide by 171 feet long equaling 1860.75 square feet when the hatches are subtracted. The surface area on the drop from the 558 elevation to the $552^{\prime} 3^{\prime \prime}$ elevation is 171 by 5.25 feet or 920.25 square feet.

B-56 Sump Area


Figure 28-532' 6" Sump Behind Common Intake Splitter
The 552 ' 3 " elevation floor slab is 2 feet thick by 171 feet long by 11 ' 3 " wide with $73^{\prime}$ by 3 ' hatch openings or 3271.5 cubic feet.
Six of the sump areas are approximately at elevation $636^{\prime} 5^{\prime \prime}$ with one at $632^{\prime} 6^{\prime \prime}$. The six sumps areas are $12^{\prime}$ by $12^{\prime} 6^{\prime \prime}$ inside minus the 3 foot by 3 foot hatch opening for 141 square feet each or 846 square feet for all 6 . The sump area floors are $12^{\prime}$ by 12 ' 6 " or 150 square feet each for 900
square feet for all 6 . The average depth of the 6 sumps is $636^{\prime} 5^{\prime \prime}$. The side walls are 13.88 feet deep. The surface area of each side wall is 12 feet by 13.88 feet or 166.6 square feet per wall or 1,666 square feet for the 10 side walls whose surface areas were not part of the hollowed out shells surface area down to the 537' elevation. The front walls and back walls are 13.88 feet high by 12 ' 6 " wide or 173.54 square feet each. This is $1,041.25$ square feet for the 6 front walls. The back walls surface area was already included in the calculation of the hollowed out shells surface area. The 7" lower depth adds $12^{\prime}$ by $12^{\prime} 6^{\prime \prime}$ by $0.58^{\prime}$ or 525 cubic feet for all 6 sumps. The added concrete volume consists of 8 interior walls, not counting the common sump walls $12^{\prime}$ by 2 feet by 13.88 feet high or 333.2 cubic feet per interior wall or 2665.60 cubic feet for all 8 . No credit will be taken for the extra 6.5 foot thickness on the side walls since it can't be verified on the drawings. The 532' 6 " common sump ceiling area is $15^{\prime} 10^{\prime \prime}$ by 12 feet minus the $3^{\prime}$ by $3^{\prime}$ hatch or 181 square feet. The floor is 15.8 by 12 feet or 190 square feet. The interior side walls are 17.75 feet by 12 feet or 213 square feet each or 426 square feet total. At two feet thick, this equals 426 cubic feet per wall or 852 cubic feet total. The additional void space below the water table is 958 cubic feet.

Void space volume taken up by 6 the rectangular sand filled areas is $21^{\prime} 9$ inches long by $11^{\prime} 10$ " wide to the 537 ' elevation or 2445 square feet each with 9780.25 square feet for all four. The common area rectangular sand is 15.25 feet long by 15.83 wide by 9.50 feet deep or 2293.85 cubic feet.

As seen in Table 36 the interior concrete was $73,812.5$ square feet in addition to the $7.47 \mathrm{E}+04$ square feet in Table 35 . This increased the estimated surface area to 148,518 square feet by a factor of 1.99 .

Table 36 - Parameters and Calculated Surface Areas for Interior Walls and Floors

| Area | Length ft | Width ft | Surface <br> Area | No <br> Items | Total <br> Surface <br> Area ft $^{2}$ |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Basket East Wall | 23 | 171 | 3933 | 2 | 7866 |
| Common Flow Splitter East of Stop <br> Logs Sides | 20 | 28 | 560 | 2 | 1120 |
| Center Common Flow Splitter East of <br> Stop Logs Top | 20 | 7 | 140 | 1 | 140 |
| Center Flow Splitter Sides | 13 | 28 | 364 | 12 | 4368 |
| Center Flow Splitter Top | 13 | 3 | 39 | 6 | 234 |
| Channel Flow Splitters Past Stop Logs | 15.95 | 28 | 446.54 | 8 | 3572.33 |
| Channel Flow Splitters Past Stop Logs | 15.95 | 3 | 47.84 | 4 | 191.38 |
| Common Flow Splitter West of Stop <br> Logs Sides | 36.5 | 51 | 1861.50 | 2 | 3723.00 |
| Common Flow Splitter West of Stop <br> Logs Top | 36.5 | 7 | 255.50 | 1 | 255.50 |
| Channel Flow Splitters Past West of <br> Stop Logs Sides | 36.5 | 51 | 1861.50 | 8 | 14892 |
| Channel Flow Splitters Past West of <br> Stop Logs Tops | 36.5 | 3 | 109.50 | 4 | 438 |
| Slanted Wall |  |  |  |  |  |
| Traveling Screen Slanted | 29.97 | 25.33 | 759.16 | 12 | 9109.9 |
| Traveling Screen Straight | 8.75 | 25.33 | 221.67 | 12 | 2660 |
| Service Water Opening | 8.23 | 6 | -49.38 | 12 | -592.56 |


| Area | Length ft | Width ft | Surface <br> Area | No <br> Items | Total <br> Surface <br> Area ft $^{2}$ |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Service Pump Sides Rectangle | 13 | 8.75 | 113.75 | 12 | 1365 |
| Service Pump Sides Triangle | 13 | 26 | 169 | 12 | 2028 |
| Service Pump Back Walls | 32.5 | 25.33 | 823.33 | 6 | 4940 |
| Circ Pump Intake Tunnel Slanted Walls | 12.5 | 15.40 | 192.51 | 12 | 2310.07 |
| Circ Pump Intake Funnel Floors and <br> Ceilings | 15.71 | 14.00 | 219.92 | 12 | 2639 |
| Circ Pump Intake Side Walls | 12.50 | 15.25 | 190.63 | 12 | 2287.5 |
| Back Wall Circ Water Pump Intake <br> Tunnels | 12.5 | 12.50 | 156.25 | 6 | 937.5 |
|  |  |  |  |  |  |
| Floor Circ Water Pump Intake Tunnels | 15.25 | 12.50 | 190.63 | 6 | 1143.75 |
| Intake Tunnel Ceiling | 15.25 | 12.50 | 25.50 | 6 | 152.97 |
| 552 Foot Elevation Floor | 11.25 | 171.00 | 1860.75 | 1 | 1860.75 |
| Wall 558 to 552 3" | 5.75 | 171.00 | 920.25 | 1 | 920.25 |
| Sump Area Ceilings | 12.5 | 12.00 | 141.00 | 6 | 846 |
| Sump Area Floors | 12.5 | 12.00 | 150.00 | 6 | 900 |
| Sump Side Walls | 13.88 | 12 | 166.6 | 10 | 1666 |
| Front and Back Sump Walls | 13.88 | 12.5 | 173.54 | 6 | 1041.25 |
| Common Sump Area Ceiling | 15.8 | 12.00 | 181 | 1 | 181 |
| Common Sump Area Floor | 15.8 | 12.00 | 190 | 1 | 190 |
| Common Sump Area Side Walls | 17.75 | 12 | 213 | 2 | 426 |
| Totals |  |  |  |  | $\mathbf{7 3 8 1 2 . 5}$ |
| Crib House Totals |  |  |  |  | 121779.55 |
| Overall Total |  |  |  |  | $\mathbf{1 4 8 5 1 8}$ |
| Increase |  |  |  |  | 1.99 |

As seen in Table 37 the interior concrete increased the estimated concrete volume by a factor of 1.46.

Table 37 - Interior Concrete Parameters and Calculated Volumes

| Item | $\begin{gathered} \text { Lengt } \\ \mathbf{h ~ f t} \end{gathered}$ | Widt <br> h ft | $\begin{array}{\|c} \begin{array}{c} \text { Thicknes } \\ \mathbf{s f t} \end{array} \\ \hline \end{array}$ | $\begin{gathered} \text { Concret } \\ \text { e } \\ \text { Volume } \\ \text { per } \\ \text { Item } \mathrm{ft}^{3} \\ \hline \end{gathered}$ | $\begin{gathered} \text { No } \\ \text { Items } \\ \hline \end{gathered}$ | Total Concrete Volume per Item ft $^{3}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Basket East Wall | 23.00 | $\begin{gathered} 171.0 \\ 0 \\ \hline \end{gathered}$ | 2.00 | 7866.00 | 1 | 7866.00 |
| Center Common Flow Splitter East of Stop | 20 | 7 | 28 | 3920.00 | 1 | 3920.00 |
| Center Flow Splitter | 13 | 28 | 3 | 1092.00 | 6 | 6552.00 |
| Channel Flow Splitters Past Stop Logs | 15.95 | 28 | 3 | 1339.63 | 4 | 5358.50 |
| Common Flow Splitter West of Stop Logs | 36.5 | 51 | 7 | $\begin{gathered} 13030.5 \\ 0 \end{gathered}$ | 1 | 13030.5 |
| Channel Flow Splitters Past West of Stop Logs | 36.5 | 51 | 3 | 5584.50 | 4 | 22338 |

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| Item | Lengt h ft | Widt h ft | $\begin{gathered} \text { Thicknes } \\ \mathrm{s} f \mathrm{ft} \end{gathered}$ | Concret <br> e Volume per Item $\mathrm{ft}^{3}$ | No Items | Total Concrete Volume per Item $\mathbf{f t}^{3}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Channel Tunnel Sloped and Straight Traveling Screen Wall | 38.72 | 25.33 | 2 | 1862.88 | 6 | $\begin{gathered} 11177.3010 \\ 3 \\ \hline \end{gathered}$ |
| Service Side Wall for Tunnel Splitters Rectangular | 19.00 | 8.75 | 3 | 840.00 | 4 | 3360.00 |
| Common Splitter Wall Rectangular of Service Pump Sides | 19.00 | 8.75 | 7 | 2346.75 | 1 | 2346.75 |
| Service Side Wall for Tunnel Splitters Triangular | 19.00 | 26 | 3 | 741.00 | 4 | 2964.00 |
| Common Splitter Wall Triangular of Service Pump Sides | 19.00 | 26 | 7 | 1729.00 | 1 | 1729.00 |
| Back Service Pump Area Concrete Volume | 32.50 | 25.33 | 4 | 3293.33 | 6 | 19760.00 |
| Triangle Sand Filled Areas | 14.00 | 12.50 | 6.42 | 1122.92 | 4 | 4491.67 |
| Outer Fan Shaped Walls Additional Concrete | 6.45 | 14 | 12.5 | 1129.55 | 1 | 1129.55 |
| Circ Pump Intake Side Walls | 12.50 | 15.25 | 2 | 381.25 | 12 | 4575.00 |
| Back Wall Circ Water Pump Intake Tunnels | 12.5 | 12.50 | 2 | 312.50 | 6 | 1875.00 |
| Ceiling Slab over Cir Pump Intake Tunnel | 29.25 | 8.5 | 171 | $\begin{gathered} 39634.4 \\ 8 \end{gathered}$ | 1 | 39634.48 |
| 552' 3" Floor Slab over Sumps | 11.25 | 171 | 2 | 3721.50 | 1 | 3721.50 |
| Interior Sump Walls | 12.00 | 13.88 | 2.00 | 333.20 | 8 | 2665.60 |
| Common Sump Area Side Walls | 17.75 | 12 | 2.00 | 426.00 | 2 | 852.00 |
| Totals |  |  |  |  |  | 159346.85 |
| Crib House Totals |  |  |  |  |  | 403081.51 |
| Overall Total |  |  |  |  |  | 505025.66 |
| Increase |  |  |  |  |  | 1.46 |

The void space below the water table decreased by a factor of 0.86 due to the concrete and sand volume below the water table shown in Table 38.

Table 38 - Parameters and Calculated Values of Void Space Volume below the Water Table with Interior Structures In Place

| Item | Length ft | $\begin{gathered} \text { Width } \\ \text { ft } \\ \hline \end{gathered}$ | Height <br> to <br> Water <br> Table ft | Total <br> Volume per Item ft ${ }^{3}$ | Total Volume per Item m ${ }^{3}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Basket East Wall | -171.00 | 2.00 | 14.00 | -4788.00 | -135.58 |
| Center Common Flow Splitter East of Stop Logs | -20 | 7 | 28 | -3920.00 | -111.00 |
| Center Flow Splitters (6) | 13 | 28 | 3 | -6552.00 | -185.53 |
| Channel Flow Splitters Past Stop Logs | 15.95 | 28 | 3 | -5358.5 | -151.74 |
| Common Flow Splitter West of Stop Logs | 36.5 | 7 | 42 | -10731 | -303.87 |
| Channel Flow Splitters Past West of Stop Logs | 36.5 | 3 | 42 | -18648 | -528.05 |

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| Item | Length ft | Width ft | $\begin{gathered} \text { Height } \\ \text { to } \\ \text { Water } \\ \text { Table ft } \\ \hline \end{gathered}$ | Total <br> Volume per Item ft ${ }^{3}$ | Total Volume per Item $\mathbf{m}^{3}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Channel Tunnel Sloped and Straight Traveling Screen Wall | 25.33 | 2 | 29.72 | -9626.42 | -272.59 |
| Service Side Wall for Tunnel Splitters Triangular | 19.00 | 3 | 26 | -2964 | -83.93 |
| Common Splitter Wall Triangular of Service Pump Sides | 19.00 | 7 | 26 | -1729 | -48.96 |
| Back Service Pump Area Concrete Volume | 25.33 | 4 | 23.5 | -14288 | -404.59 |
| Funnel shaped Walls | 14.00 | 12.50 | 6.42 | -4491.67 | -127.19 |
| Triangle Sand Filled Areas | 6.42 | 14 | 12.5 | -4491.67 | -127.19 |
| Common Triangle Sand Filled Area | 7.92 | 14 | 12.5 | -1385.42 | -39.23 |
| Outer Fan Shaped Walls Additional Concrete | 6.45 | 14 | 12.5 | -1129.55 | -31.99 |
| Circ Pump Intake Side Walls | 15.25 | 2 | 12.50 | -4575 | -129.55 |
| Back Wall Circ Water Pump Intake Tunnels | 12.50 | 2.00 | 12.50 | -1875 | -53.09 |
| Ceiling Slab over Cir Pump Intake Tunnel | 29.25 | 8.5 | 171 | -39634.48 | -1122.32 |
| 552' 3' Floor Slab over Sumps | 11.25 | 171 | 2 | -3973.50 | -112.52 |
| Sump Additional Void Space | 12.00 | 12.50 | 0.58 | 525.00 | 14.87 |
| Interior Sump Walls | 12.00 | 13.88 | 2.00 | -2665.60 | -75.48 |
| Common Sump Area Side Walls | 17.75 | 12.00 | 2.00 | -852.00 | -24.13 |
| Common Sump Area Additional Void Space | 17.75 | 12.00 | 4.50 | 958.50 | 27.14 |
| Rectangular sand areas | 21.75 | 11.83 | 9.50 | -9780.25 | -276.95 |
| Common Area Rectangular Sand | 15.25 | 15.83 | 9.50 | -2293.85 | -64.95 |
| Totals |  |  |  | -154269.40 | -4368.42 |
| Crib House Totals |  |  |  | 845311.10 | 23936.54 |
| Overall Total |  |  |  | 923737.897 | 26157.344 |
| Ratio |  |  |  | 0.86 | 0.86 |

### 3.3. Waste Water Treatment Facility (WWTF)

The Waste Water Treatment Facility (WWTF) end state consists of concrete settling and equalization tanks, clarifiers and floculant (floc) and sludge tanks with sloped bottoms as seen in the top view of the WWTF basement in Figure 29. Most of the end state concrete below the 588' elevation is above the 579' water table. The floors of the structures will be perforated to ensure they can equilibrate with the water table and will not overflow the structure at the 588' elevation.

Table 39 - WWTF Northwest Area Surface Area

| Area | $\underset{f t}{\text { Length }}$ | Width ft | Surface Area | No Items | Total Surface Area ft ${ }^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Electrical Area Floor | 23.5 | 11 | 258.5 | 1 | 258.5 |
| Electrical Area E\&W Walls | 23.50 | 0.5 | 11.75 | 2 | 23.5 |
| Electrical Area N\&S Walls | 11.00 | 0.5 | 5.50 | 2 | 11.0 |
| Filter Area Floor | 34 | 26 | 884.00 | 4 | 3536.0 |
| Filter Area Sump N\&S Walls | 3.00 | 4.75 | 14.25 | 2 | 28.5 |
| Filter Area Sump E\&W Walls | 5.00 | 4.75 | 23.75 | 2 | 47.5 |
| Filter Area N\&S Walls | 34.00 | 10 | 340.00 | 2 | 680 |
| Filter Area E\&W Walls | 26.00 | 10 | 260.00 | 2 | 520 |
|  |  | Totals | 1797.75 |  | 5105 |

The Electrical Room floor is $23^{\prime} 6^{\prime \prime}$ by $11^{\prime}$ and is at the $587^{\prime} 6^{\prime \prime}$ level such that it is above the water table and only six inches below the 588' end state. The Filter Tank area is $34^{\prime}$ by $26^{\prime}$ and is located at the $578^{\prime}$ elevation; it has a $3^{\prime}$ by $5^{\prime}$ sump at the $573^{\prime} 4$ ' elevation. This results in the surface areas shown in Table 39.


Figure 29 - Waste Water Treatment Facility Top View from Drawing B-1024
As seen in Figure 30 the Filter Area $34^{\prime}$ by 26' floor is slightly below the 579' water table at the $578^{\prime}$ elevation. The 3 ' by $5^{\prime}$ sump floor is 5.75 ' below the main floor at 573 '3'".


Figure 30 - Side View Northwest WWTF from B-1019
This results in a void space below the water table of 2,723 cubic feet as seen in Table 40.
Table 40 - WWTF Northwest Area Void Space Below 579' Water Table

| Item | Length <br> ft | Width <br> ft | Height <br> to <br> Water <br> Table ft | Total <br> Volume <br> per Item <br> $\mathbf{f t}^{3}$ |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Filter Area Floor | 34.00 | 26.00 | 1.00 | 884.00 |  |  |  |  |
| Filter Area Sump | 3.00 | 5.00 | 5.75 | 86.25 |  |  |  |  |
|  |  |  |  |  |  |  | Totals | $\mathbf{9 7 0}$ |

The Electrical Room floor is 8 inches thick as seen in Figure 30 with one foot thick walls as seen in Figure 29. The East wall concrete volume of the Electrical Room is included as part of the Filter Area concrete volume. The Filter Area floor is 1 ' 4 " thick. The walls are 1' thick as seen in Figure 29 and Figure 30. The concrete volumes of the Electrical Room and Filter Area are shown in Table 38.

Table 41 - Concrete Volumes for WWTF Electrical Room and Filter Area End States

| Item | Length ft | Width ft | Thickness ft | Concrete Volume per Item ft $^{3}$ | No Items | Total Concrete Volume per Item $\mathrm{ft}^{3}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Electrical Area Floor | 23.5 | 11 | 0.67 | 172.33 | 1 | 172.33 |
| Electrical Area N\&S Walls | 11.0 | 0.5 | 1 | 5.50 | 2 | 11.00 |
| Electrical Area West Wall | 23.5 | 0.5 | 1 | 11.75 | 1 | 11.75 |
| Filter Area Floor | 34 | 26 | 1.33 | 1178.67 | 1 | 1178.67 |
| Filter Area Sump N\&S Walls | 3.00 | 4.75 | 1.00 | 14.25 | 2 | 28.50 |
| Filter Area Sump E\&W Walls | 5.00 | 4.75 | 1.00 | 23.75 | 2 | 47.50 |
| Filter Area N\&S Walls | 34.00 | 10 | 1.00 | 340.00 | 2 | 680.00 |
| Filter Area E\&W Walls | 26.00 | 10 | 1.00 | 260.00 | 2 | 520.00 |
|  |  |  | Totals | 2006.25 |  | 2649.75 |

As seen in Figure 29 and Figure 31 the northeast portion of the WWTF contains two (north and south) Clarifiers and Floculant Tanks and a single Sludge Holding Tank. Each Clarifier consists of a mildly sloped floor that drops from the 585.54 ' elevation to $585.25^{\prime}$ elevation after $27.5^{\prime}$ ( $30^{\prime}-2^{\prime}$ -$2.5^{\prime}-3^{\prime}$ ) and is 8 wide. There is then a pit with angled east and west walls and a $2^{\prime} 6^{\prime \prime}$ wide floor. A 6 " opening in the East wall above the pit allows flow to the Floculant Tank. The sloped floor length is the square root of the 27.5 feet squared plus the $0.29^{\prime}$ drop squared or 27.502 feet resulting in a floor surface area of 220.01 square feet per clarifier. The surface area of the west wall of each clarifier is the $8^{\prime}$ width by the $588^{\prime}$ minus 585.54 ' height or 2.46 feet which equals 19.68 square feet per clarifier. The surface area of the north and south walls above the sloped floor are the $27^{\prime} 6$ " lengths by the average depth of 2.605 feet or 71.64 square feet per wall. The north and south walls above the Clarifier Pits are 7 ' 6 '" long with a 2.75 ' depth below the 588 ' elevation equaling 20.63 square feet per wall.


Figure 31 - Side View Northeast WWTF from B-1019

The East wall of the clarifier pit has a depth of the $588^{\prime}$ elevation to $585.67^{\prime}$ elevation with a 6 " opening for a depth of 1.83 feet, with an 8 foot width this equals 14.64 square feet. The west face of each Clarifier Pit slopes with a length equaling the square root of 2' squared plus 5.25 ' squared or 5.62 feet long. At an $8^{\prime}$ width this equals 44.94 square feet each. The east wall slopes from the 585.67 ' elevation to the $580^{\prime}$ elevation pit bottom. The length is the square root of 3 ' squared plus 5.67 ' squared 6.41 feet resulting in a surface area 51.32 square feet each. The Clarifier Pit floor is 2.5 by 8 feet or 20 square feet. The east and west walls of the pit are made up of two triangles and a rectangles as seen in Figure 31. The average width of the pit is 1 ' plus 2.5 ' plus 1.5 ' or 5 feet. The depth is 5.25 feet resulting in a surface area of 26.25 feet per wall. There is an additional surface area created by the 6 " opening to the Floc Tank. The top and bottom are $10 "$ by 8 ' and the sides are $6 "$ by 10 ". The north and south Clarifier Surface areas are summarized in Table 42.

Table 42 - East and West Clarifier Surface Areas

| Area | Length <br> $\mathbf{f t}$ | Width <br> $\mathbf{f t}$ | Surface <br> Area | No <br> Items | Total <br> Surface <br> Area <br> $\mathbf{f t}^{2}$ |  |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Clarifier 585' Floor | 27.502 | 8 | 220.01 | 2 | 440.02 |  |  |  |  |  |  |
| Clarifier W Wall | 8 | 2.46 | 19.68 | 2 | 39.36 |  |  |  |  |  |  |
| Clarifier N \& S Wall Above Floor | 27.50 | 2.605 | 71.64 | 4 | 286.55 |  |  |  |  |  |  |
| Clarifier N \& S Wall Above Pit | 7.50 | 2.75 | 20.63 | 4 | 82.5 |  |  |  |  |  |  |
| Clarifier E Wall | 8 | 1.83 | 14.64 | 2 | 29.28 |  |  |  |  |  |  |
| Clarifier Pit West Face | 5.62 | 8 | 44.94 | 2 | 89.9 |  |  |  |  |  |  |
| Clarifier Pit East Face | 6.41 | 8 | 51.32 | 2 | 102.6 |  |  |  |  |  |  |
| Clarifier Pit Floor | 2.50 | 8 | 20.00 | 2 | 40.0 |  |  |  |  |  |  |
| Clarifier Pit N\&S Walls | 5.00 | 5.25 | 26.25 | 4 | 105 |  |  |  |  |  |  |
| Top and Bottom Floc Tank Opening | 0.83 | 8 | 6.67 | 2 | 13.3 |  |  |  |  |  |  |
| Sides Floc Tank Opening | 0.50 | 0.833 | 0.42 | 2 | 0.8 |  |  |  |  |  |  |
|  |  |  |  |  |  |  | Totals |  | $\mathbf{4 9 6 . 1 9}$ |  | $\mathbf{1 2 2 9 . 4 1}$ |

Since the lowest Clarifier elevation is the $580^{\prime}$ elevation of the pit, there is no void space below the 579 ' water table. The concrete volume of the south wall of the south Clarifier is included in the Equalization Tank concrete volume, resulting in a two 8 foot wide floors and three 10 " wide wall thicknesses since the north wall has an additional 10 " outer layer making it $20^{\prime \prime}$ thick. This results in $18^{\prime} 6^{\prime \prime}$ width across both Clarifiers. The concrete volume under the sloped floor is 27.502 feet long by 18.5 feet wide and $1^{\prime}$ thick or 508.78 cubic feet. The calculated Clarifier concrete volumes are provided in Table 43.

Table 43 - North and South Clarifier End State Concrete Volumes

|  |  |  |  | Concrete <br> Volume <br> per Item <br> $\mathbf{f t}^{3}$ | Total <br> No <br> Items | Congrete <br> Volume <br> per Item <br> $\mathbf{f t}^{3}$ |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Clarifier 585' Floor | 27.50 | 18.50 | 1 | 508.78 | 1 | 508.78 |
| Clarifier W Wall | 18.50 | 2.46 | 1 | 45.51 | 1 | 45.51 |


| Item | $\underset{\mathrm{ft}}{\text { Length }}$ | Width ft | Thickness ft | Concrete Volume per Item $\mathbf{f t}^{3}$ | No Items | Total Concrete Volume per Item $\mathbf{f t}^{3}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Clarifier N \& S Wall Above Floor | 27.50 | 2.605 | 0.83 | 59.70 | 3 | 179.09 |
| Clarifier N \& S Wall Above Pit | 7.50 | 2.75 | 0.83 | 17.19 | 3 | 51.56 |
| Clarifier E Wall | 18.50 | 1.83 | 0.83 | 28.21 | 1 | 28.21 |
| Clarifier Pit West Face | 5.25 | 18.50 | 2 | 194.25 | 1 | 194.25 |
| Clarifier Pit East Face | 5.67 | 18.50 | 2.33 | 244.76 | 1 | 244.756 |
| Clarifier Pit Floor | 2.50 | 18.50 | 1 | 46.25 | 1 | 46.25 |
| Clarifier Pit N\&S Walls | 5.00 | 5.25 | 0.83 | 21.88 | 2 | 43.75 |
|  |  |  | Totals | 1166.52 |  | 1342.16 |

The volumes of the walls above the pit are as described in the surface area calculation with a foot thickness for the West wall and 20 " thicknesses for the north wall, and 10 " thickness for the south and east walls. As seen in Figure 31, the west wall of the Clarifier Pit has an average width of 2' with a depth of 5 '3" and this concrete spans the 18.5 ' width for a volume of 194.25 cubic feet. Similarly the East wall of the pit has an average width of 1 ' 6 " plus 10 " or 2.33 feet with a depth of 5.67 ' which with a $18.5^{\prime}$ ' width equals 244.76 cubic feet. Between the walls, the pit floor is 2.5 feet long by $18.5^{\prime}$ wide and $1^{\prime}$ thick. The north and south walls of the clarifier are 10 " thick the north wall has an additional 10" thick outer layer as seen in Figure 29.

The north and south Floc Tanks are 6 feet long by 8 feet wide and 1'6" deep. The west wall has a 6" opening and is only 1 feet deep. The Floc Tank Surface Areas are shown in Table 44.

Table 44 - North and South Floc Tank Surface Areas

| Area | Length <br> $\mathbf{f t}$ | Width <br> $\mathbf{f t}$ | Surface <br> Area | No <br> Items | Total <br> Surface <br> $\mathbf{A r e a ~ f t}^{2}$ |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Floc Tank Floor | 6.00 | 8 | 48.00 | 2 | 96.00 |  |  |  |  |
| Floc Tank W Wall | 8 | 1 | 8.00 | 2 | 16 |  |  |  |  |
| Floc Tank E Wall | 8 | 1.5 | 12.00 | 2 | 24 |  |  |  |  |
| Floc tank N \& S Wall | 6.00 | 1.5 | 9.00 | 4 | 36 |  |  |  |  |
| Totals |  |  |  |  |  |  | 77.00 |  | $\mathbf{1 7 2 . 0 0}$ |
|  |  |  |  |  |  |  |  |  |  |

Since the Floc tank bottoms are at the $586^{\prime} 6^{\prime \prime}$ elevation there is no void space below the 579 ' water table. As with the clarifiers the southernmost wall concrete volume is calculated as part of the Equalization Tank concrete volume. The length of the 10 " floor slab that is not included in the wall volumes is $6^{\prime} 10^{\prime \prime}$. The Floc Tank west wall volume was included in the Clarifier volume. The east wall volume is calculated as part of the Sludge Holding Tank volume. The Floc Tank north and south walls are 10 " thick and $6^{\prime}$ long by 1 ' 6 ' deep. The outer wall of the north wall includes an additional 10 " thick portion.

Table 45 - WWTF North and South Floc Tank End State Concrete Volumes

| Item | $\underset{f t}{\text { Length }}$ | Width ft | Thickness ft | Concrete Volume per Item $\mathrm{ft}^{3}$ | No <br> Items | Total <br> Concrete <br> Volume <br> per Item <br> ft $^{3}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Floc Tank Floor | 6.83 | 18.5 | 0.83 | 105.35 | 1 | 105.35 |
| Floc tank N \& S Wall | 6.00 | 1.5 | 0.83 | 7.50 | 3 | 22.50 |
|  |  |  | Totals | 112.85 |  | 127.85 |

The Sludge Holding Tank walls slope from the 587.5; to 583 ' as seen in Figure 29and Figure 31. The tank interior is $11^{\prime}$ by $16^{\prime} 10^{\prime \prime}$. The floor is $3^{\prime}$ by $5^{\prime}$ as seen on drawing B-1018. The west wall has a top width of $16^{\prime} 10^{\prime \prime}$ and a bottom width of $5^{\prime}$ for an average width of $16^{\prime} 10^{\prime \prime}$ minus 5 feet equals $11^{\prime} 10^{\prime \prime}$ half of which is $5^{\prime} 11^{\prime \prime}$ thus the average width is $5^{\prime}$ of the sump plus $5^{\prime} 11^{\prime \prime}$ on either side of it or $10^{\prime} 111^{\prime \prime}$. The top of the sloped walls are $4^{\prime} 6^{\prime \prime}$ above the $583^{\prime}$ floor at the $587^{\prime} 66^{\prime \prime}$ elevation and the wall extends $9^{\prime}$ to the sump floor. The length of the wall is the square root of 4.5 feet squared plus 9 feet squared or 9.18 feet. The surface area of the Sludge Holding Tank west wall is 100.2 square feet. The East wall also has an average width of $10^{\prime} 11^{\prime \prime}$ but is vertical with a height of $4^{\prime} 6^{\prime \prime}$ for a surface area of 49.13 inches. The East and West walls are $11^{\prime}$ at the top and 3 ' at the bottom for an average width of 7 '. The length of each wall is the square root of $5^{\prime} 11^{\prime \prime}$ squared plus $4^{\prime} 6^{\prime \prime}$ squared or 7.43 feet. There is also a 6 " band below the 588 ' that is above the top of sloped walls at 587' 6 '".

Table 46 - WWTF Sludge Holding Tank End State Surface Areas

| Area | Length <br> $\mathbf{f t}$ | Width <br> $\mathbf{f t}$ | Surface <br> Area | No Items | Total <br> Surface <br> Area <br> $\mathbf{f t}^{2}$ |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Sludge Holding Tank Floor | 3.00 | 5 | 15.00 | 1 | 15 |
| West Wall | 9.18 | 10.92 | 100.20 | 1 | 100.20 |
| East Wall | 4.5 | 10.92 | 49.13 | 1 | 49.13 |
| North and South Walls | 7.43 | 7.00 | 52.03 | 2 | 104.07 |
| East and West Walls Above 587'6" | 0.5 | 16.83 | 8.42 | 2 | 16.83 |
| North and South Walls Above 587'6" | 0.5 | 11.00 | 5.50 | 2 | 11.00 |

There is no void space below the water table associated with the sludge holding tank. The floor slab is $1^{\prime}$ thick and has a length that is the west wall thickness of $10^{\prime \prime}$ plus $11^{\prime}$ plus the east wall $1^{\prime} 4 "$ thickness or $13.17^{\prime}$ long. The slab width is the $16^{\prime} 10^{\prime \prime}$ tank interior plus the $20^{\prime \prime}$ thick north wall or $18.5^{\prime}$. The west wall has an $8^{\prime}$ length at the base, thus the average width across the $4{ }^{\prime} 6^{\prime \prime}$ height is 4 feet with an additional $10^{\prime \prime}$ for the west wall making the length $4^{\prime} 10^{\prime \prime}$. The average interior width is $10^{\prime} 11^{\prime \prime}$ as described above plus the additional $20^{\prime \prime}$ thickness of the north wall portion or 12.58'. With a 4 ' 6 ' height this equals a concrete volume of 273.69 cubic feet. The wall has an $11^{\prime}$ top and a $3^{\prime}$ bottom for an average length of 7 feet plus the $1^{\prime}$ thick east wall equals $8^{\prime}$. The height is $4^{\prime} 6^{\prime \prime}$ and the width is the $20^{\prime \prime}$ north wall thickness plus half the $5^{\prime} 11$ "base or an average width of 4.63 feet. The sloped south wall is the same as the north except that the $1^{\prime}$ thick portion of the south wall is
part of the Equalization Tank volume so the average width is half the $5^{\prime} 11^{\prime \prime}$ base or $2.96^{\prime}$. The east wall has the same average length as the west wall at $12.58^{\prime}$ with a $4^{\prime} 6{ }^{\prime \prime}$ height and $1^{\prime}$ thickness. There are also the remaining 6 " portions of the walls above the 587 ' 6 " top of the sloped walls. The end state concrete volumes for the WWTF Sludge Holding Tank are provided in Table 47.

Table 47 - WWTF Sludge Holding Tank End State Concrete Volumes

| Item | $\underset{f t}{\text { Length }}$ | $\underset{\mathbf{f t}}{\text { Width }}$ | Thickness $\mathbf{f t}$ | Concrete Volume per Item $\mathbf{f t}^{3}$ | No <br> Items | Total Concrete Volume per Item $\mathbf{f t}^{3}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Sludge Holding Tank Floor | 13.17 | 18.50 | 1.00 | 243.58 | 1 | 243.58 |
| Sloped West Wall | 4.50 | 12.58 | 4.83 | 273.69 | 1 | 273.69 |
| Sloped North Wall | 4.50 | 8.00 | 4.63 | 166.50 | 1 | 166.50 |
| Sloped South Wall | 4.50 | 8.00 | 2.96 | 106.50 | 1 | 106.50 |
| East Wall | 4.50 | 12.58 | 1.00 | 56.63 | 1 | 56.63 |
| East and West Walls Above 587'6" | 18.50 | 0.50 | 1.00 | 9.25 | 2 | 18.50 |
| North Wall Above 587'6" | 11.00 | 0.50 | 1.67 | 9.17 | 1 | 9.17 |
|  |  |  | Totals | 865.31 |  | 874.56 |

As seen in Figure 29, the southern half of the WWTF consists of the Equalization Tank Oil Skimming Area and the Equalization Tank. As seen in Figure 32, only western portion of the slab is above the 588' end state. The Oil Skimming Area is $21^{\prime}$ wide by 34 ' long and slopes from the $577.58^{\prime}$ elevation on the west end to the 577.33 ' elevation on the east end. This is a 3 " drop in elevation. The length of the floor area is the square root of 34 ' squared plus 0.25 ' squared or 34.001 feet. The average height of the north and south walls of the oil skimming area are 588' minus $577.455^{\prime}$ (e.g. 577.33' plus $0.125^{\prime}$ ) or $10.66^{\prime}$.


Figure 32- Side View Southwest WWTF End State from B-1019
The west wall is $21^{\prime}$ wide by $10.42^{\prime}$ high and the south wall is $21^{\prime}$ wide by 10.67 feet high. The Equalization Tank Oil Skimming Area end state surface areas are provided in Table 48.

Table 48 - WWTF Equalization Tank Oil Skimming Area End State Surface Areas

| Area | Length <br> $\mathbf{f t}$ | Width <br> $\mathbf{f t}$ | Surface <br> Area | Total <br> No <br> Items | Surface <br> Area <br> $\mathbf{f t}^{2}$ |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Oil Skimming Area Floor | 34 | 21 | 714.02 | 1 | 714.02 |
| Oil Skimming Area North and South Walls | 34 | 10.66 | 362.35 | 2 | 724.71 |
| Oil Skimming Area West Wall | 21 | 10.42 | 218.82 | 1 | 218.82 |
| Oil Skimming Area East Wall | 21 | 10.67 | 224.07 | 1 | 224.07 |
|  |  | Totals | $\mathbf{1 5 1 9 . 2 6}$ |  | $\mathbf{1 8 8 1 . 6 2}$ |

The bottom of the area is slightly below the $57{ }^{\prime}$ ' water table with an average bottom depth of $577.455^{\prime}$. The average depth 1.54 ' below the water table results in a $1,103.13$ cubic foot void space as seen in Table 49

Table 49 - WWTF Equalization Tank Oil Skimming Area End State Void Space Below 579' Water Table

| Item | Length <br> $\mathbf{f t}$ | Width <br> ft | Height <br> to <br> Water <br> Table ft | Total <br> Volume <br> per <br> Item ft |
| :---: | :---: | :---: | :---: | :---: |
| Equalization Tank Oil Skimming Area | 34.00 | 21.00 | 1.54 | 1103.13 |

The floor slab is 1 ' 4 " thick for most of the length, but transitions to 1 ' 10 " thick starting at 4 ' west of the east wall. The slab extend $1^{\prime}$ past the $1^{\prime}$ thick west wall making it 36 ' long. The north and south walls are $1^{\prime}$ thick making the slab $23^{\prime}$ wide. The average increase in thickness across the 4 feet at which the slab transitions from $1^{\prime} 4$ ' to $1^{\prime} 10^{\prime \prime}$ is 3 inches. The transition concrete volume to the east wall is $4^{\prime}$ by $23^{\prime}$ by $0.25^{\prime}$ or 23 cubic feet.

Table 50 - WWTF Equalization Tank Oil Skimming Area End State Concrete Volumes

| Item | $\underset{\mathrm{ft}}{\text { Length }}$ | Width ft | Thickness ft | Concrete Volume per Item $\mathrm{ft}^{3}$ | No <br> Items | Total Concrete Volume per Item ft $^{3}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Sludge Holding Tank Floor | 36.00 | 23.00 | 1.33 | 1104.00 | 1 | 1104.00 |
| Sludge Holding Tank Floor Transition | 4 | 23.00 | 0.25 | 23.00 | 1 | 23.00 |
| Oil Skimming Area North and South Walls | 34.00 | 10.66 | 1 | 362.35 | 2 | 724.71 |
| Oil Skimming Area West Wall | 21 | 10.42 | 1 | 218.82 | 1 | 218.82 |
| Oil Skimming Area East Wall | 21.00 | 10.67 | 1 | 224.07 | 1 | 224.07 |
|  |  |  | Totals | 1932.25 |  | 2294.60 |



Figure 33 - WWTF Equalization Tank End State Side View from B-1019

As seen in Figure 29 and Figure 33 the Equalization Tank floor slopes from 577.3' to the top of a $10^{\prime}$ by $4^{\prime}$ sump at 577'. The sloped floors can be broken up into geometries as shown in Figure 34.


Figure 34 - Sloped Floor Geometries for Calculation of Surface Areas
For G1a the surface area is equal to a rectangle with a width of 1.5 feet or half the 3 foot width. The length corrected for the equals the square root of the 0.3 inch slope is the square root of $28^{\prime} 2^{\prime \prime}$ square plus 0.3 feet squared or 2.817 feet. Using this methodology the surface of the Equalization Tank below the 588 foot was calculated as seen in Table 51.

Table 51 - Equalization Tank Surface Areas Below 588 Foot Elevation

| Area | Length <br> ft | Width <br> ft | Surface <br> Area | No Items | Total <br> Surface <br> Area <br> $\mathbf{f t}^{2}$ |  |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| G1a Equalization Tank W Sloped Floor | 28.17 | 1.5 | 42.25 | 1 | 42.25 |  |  |  |  |  |  |
| G1b Equalization Tank W Sloped Floor | 28.17 | 10 | 281.68 | 1 | 281.68 |  |  |  |  |  |  |
| G1c Equalization Tank W Sloped Floor | 28.17 | 8.25 | 232.39 | 1 | 232.39 |  |  |  |  |  |  |
| G2a Equalization Tank N Sloped Floor | 28.17 | 1.5 | 42.46 | 1 | 42.46 |  |  |  |  |  |  |
| G2b Equalization Tank N Sloped Floor | 3.01 | 4 | 12.06 | 1 | 12.06 |  |  |  |  |  |  |
| G2c Equalization Tank N Sloped Floor | 3.01 | 10.75 | 32.41 | 1 | 32.41 |  |  |  |  |  |  |
| G3a Equalization Tank E Sloped Floor | 21.50 | 1.5 | 32.25 | 1 | 32.25 |  |  |  |  |  |  |
| G3b Equalization Tank E Sloped Floor | 21.50 | 10 | 215.02 | 1 | 215.02 |  |  |  |  |  |  |
| G3c Equalization Tank E Sloped Floor | 21.50 | 8.25 | 177.39 | 1 | 177.39 |  |  |  |  |  |  |
| G4a Equalization Tank S Sloped Floor | 16.50 | 10.75 | 177.40 | 1 | 177.40 |  |  |  |  |  |  |
| G4b Equalization Tank S Sloped Floor | 16.50 | 4 | 66.01 | 1 | 66.01 |  |  |  |  |  |  |
| G4c Equalization Tank S Sloped Floor | 16.50 | 14.08 | 232.41 | 1 | 232.41 |  |  |  |  |  |  |
| G5 Equalization Tank Sump Floor | 4.00 | 10 | 40.00 | 1 | 40.00 |  |  |  |  |  |  |
| Sump N\&S Walls | 4.00 | 2 | 8.00 | 2 | 16.00 |  |  |  |  |  |  |
| Sump E\&W Walls | 10.00 | 2 | 20.00 | 2 | 40.00 |  |  |  |  |  |  |
| Equalization Tank N\&S Walls | 53.67 | 10.7 | 574.23 | 2 | 1148.47 |  |  |  |  |  |  |
| Equalization Tank E\&W Walls | 29.50 | 10.7 | 315.65 | 2 | 631.30 |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  | Totals | $\mathbf{2 5 0 1 . 6 3}$ |  | $\mathbf{3 4 1 9 . 5 2}$ |
|  |  |  |  |  | 1 |  |  |  |  |  |  |

The void space below the water table can be calculated by breaking the Equalization Tank into 3 parts. The rectangular volume from the top of the sloped floors at 577.3 ft to the water table at 579 foot elevation. The volume from the top of the sloped floor at 577.3 ft to the top of the sump at 577 ft . This is the same as the volume of a rectangular volume source with a height of 0.15 feet. The void space of the sump from the 575 foot bottom elevation to the 577 foot elevation, as seen in Table 52.

Table 52 - Equalization Tank Void Space to Water Table

| Item | Length <br> $\mathbf{f t}$ | Width <br> $\mathbf{f t}$ | Height to <br> Water <br> Table ft | Total <br> Volume <br> per Item <br> $\mathbf{f t}^{\mathbf{3}}$ |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Equalization Tank Above 577.3 ft EL | 53.67 | 29.50 | 1.70 | 2691.38 |  |  |  |  |  |
| Equalization Tank Sloped Floors | 53.67 | 29.50 | 0.15 | 237.48 |  |  |  |  |  |
| Equalization Tank Sump Void Space | 10.00 | 4.00 | 2 | 80.00 |  |  |  |  |  |
|  |  |  |  |  |  |  | Totals |  | $\mathbf{3 0 0 9}$ |

As seen in Figure 33, the floor slab under the tank is 1 foot 10 inches (i.e., 1.83 ft ) thick, except for the area surrounding and directly below the sump which is thicker. As seen in Figure 29 and Figure 33 , the walls are 1 foot thick.

Table 53- Equalization Tank Concrete Volumes

| Item | $\begin{gathered} \text { Length } \\ \mathrm{ft} \\ \hline \end{gathered}$ | Width $\mathrm{ft}$ | $\begin{array}{\|c} \hline \begin{array}{c} \text { Thickness } \\ \text { ft } \end{array} \\ \hline \end{array}$ | Concrete Volume per Item $\mathbf{f t}^{3}$ | No <br> Items | Total Concrete Volume per Item $\mathbf{f t}^{3}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Equalization Tank Main Floor Slab Floor | 55.67 | 31.50 | 1.83 | 3214.75 | 1 | 3214.75 |
| Main Floor Slab Sump Void Space | -4 | 10.00 | 1.83 | -73.33 | 1 | -73.33 |
| Sump Area Tapered E\&W | 2.33 | 3.50 | 10.00 | 81.67 | 1 | 81.67 |
| Sump Area Tapered N\&S | 2.33 | 3.50 | 9.00 | 73.50 | 1 | 73.50 |
| Sump Area Side E\&W | 2.33 | 2.50 | 10.00 | 58.33 | 2 | 116.67 |
| Sump Area Ends N\&S | 2.33 | 2.50 | 9.00 | 52.50 | 2 | 105.00 |
| Volume Directly Below Sump | 4.00 | 10.00 | 2.17 | 86.67 | 1 | 86.67 |
| Equalization Tank N\&S Walls | 53.67 | 10.7 | 1.00 | 574.23 | 2 | 1148.47 |
| Equalization Tank E\&W Walls | 29.50 | 10.7 | 1.00 | 315.65 | 2 | 631.30 |
|  |  |  | Totals | 4383.97 |  | 5384.68 |

The end state surface area, void space below the water table and concrete volumes for the WWTF are summarized in Table 54

Table 54 - Waste Water Treatment Facility (WWTF) Summary of Surface Areas, Water Table Void Space and Concrete Volumes

| Item | Total <br> Total <br> Surface <br> Area ft $^{\mathbf{2}}$ | Water <br> Table Void <br> Volume <br> per Item <br> $\mathbf{f t}^{3}$ | Total <br> Concrete <br> Volume <br> per Item <br> $\mathbf{f t}^{\mathbf{3}}$ |
| :--- | :---: | :---: | :---: |
| WWTF NW Electrical and Filter Area | 5105 | 970 | 2656 |
| WWTF NE Clarifiers | 1229 | 0 | 1342 |
| WWTF NE Floc Tanks | 172 | 0 | 128 |
| WWTF NE Sludge Holding Tank | 296 | 0 | 875 |
| WWTF SW Oil Skimming Area | 1882 | 1103 | 2295 |
| WWTF SE Equalization Tank | 3420 | 3009 | 5385 |
| WWTF Totals | $\mathbf{1 . 2 1 E}+\mathbf{0 4}$ | $\mathbf{5 . 0 8 E}+\mathbf{0 3}$ | $\mathbf{1 . 2 7 E + 0 4}$ |

The abstracted model for the WWTF assumes an overall elevation of 577' and a water table void space of 5082.24 cubic feet and a $47.35^{\prime}$ by $53.67^{\prime}$ length and width as seen in Figure 29.

Table 55 - Example of WWTF Abstracted Model Based on Water Table Void Space

| Description | Floor <br> Elev ft | $\begin{gathered} \text { Length } \\ \text { ft } \end{gathered}$ | Width ft | Area ft ${ }^{2}$ | $\begin{gathered} \text { Height } \\ \text { to } \\ \text { Water } \\ \text { Table ft } \\ \hline \end{gathered}$ | Void Space to WT $\mathrm{ft}^{3}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Waste Water Treatment Facility | 577 | 47.35 | 53.67 | 2541.12 | 2 | 5082.24 |

### 3.4. Spent Fuel Pool and Transfer Canal

The Spent Fuel Pool and Transfer Canal are the only end state structures below the 588 ' elevation in the Spent Fuel Building (SFB). The $3 / 16$ " stainless steel liner on the Transfer Canal and Spent Fuel Pool will be removed in the end state. The Transfer Canal is in communication with Units 1 and 2 Containments from the fuel transfer tubes at the $578^{\prime} 6^{\prime \prime}$ elevation as seen in Figure 35. The transfer chute between the canal and pool is at the 592' elevation. Since everything above the $588^{\prime}$ elevation will be removed in the end state the Transfer Canal will be isolated from the Spent Fuel Pool unless the 6 foot thick wall between them is perforated.

As seen in Figure 35 and Figure 36, the Transfer Canal and Spent Fuel Pool floors are at the 576 foot elevation. The Spent fuel pool walls are 6 feet thick.


Figure 35 - Spent Fuel Pool and Transfer Canal Overhead View
The east wall of the Transfer Canal is $5^{\prime} 3^{\prime \prime}$ thick. The cask pit has two walls extending into the pool that are 9 ' 3 " long and tapers from $1^{\prime} 6^{\prime \prime}$ thick to 4 ' thick. The surface areas for the walls and floors are shown in Table 56. The cask pit slanted walls lengths are 9.58 ft (the square root of 9.25 ft squared plus 2.5 ft squared) as seen in Figure 37.

Table 56 - Spent Fuel and Transfer Canal Surface Areas

| Area | Length <br> $\mathbf{f t}$ | Width <br> $\mathbf{f t}$ | Surface <br> Area | No <br> Items | Total <br> Surface <br> Area ft $^{\mathbf{2}}$ |
| :--- | :---: | :---: | :---: | :---: | :---: |
| West Wall | 59 | 12 | 708 | 1 | 708 |
| East Wall | 63 | 12 | 756 | 1 | 756 |
| South Wall | 33 | 12 | 396 | 1 | 396 |
| North Wall | 29 | 12 | 348 | 1 | 348 |
| Cask Pit Straight Wall | 9.25 | 12 | 111 | 2 | 222 |
| Cask Pit Ends | 1.5 | 12 | 18 | 2 | 36 |
| Cask Pit Slant | 9.58 | 12 | 114.98 | 2 | 229.97 |
| Pool Floor Covered by Cask Pit Walls | 9.25 | -5.5 | -50.88 | 1 | -50.88 |
| Pool Floor | 63 | 33 | 2079 | 1 | 2079 |
| Transfer Canal East and West Walls | 105.79 | 12 | 1269.5 | 2 | 2539 |
| Transfer Canal North and South Walls | 4 | 12 | 48 | 2 | 96 |
| Transfer Canal Floor | 4 | 105.79 | 423.17 | 1 | 423.17 |
|  |  |  |  |  |  |



Figure 36 - Spent Fuel Pool and Transfer Canal Side View
The West Wall and North Wall lengths are the 63 feet minus 4 feet and 33 feet minus 4 feet to account for the surface are covered by the cask pit walls. The area of the floor covered by the cask pit walls is $4^{\prime}+1^{\prime} 6^{\prime \prime}$ multiplied times $9^{\prime} 3^{\prime \prime}$ as seen in Figure 37


Figure 37 - Cask Pit Walls Floor Foot Print
The void space to the water table at $579^{\prime}$ is calculated using the pool and canal floor surface areas in Table 56 as shown in Table 57.

Table 57 - Spent Fuel Pool and Transfer Canal Void Spaces to Water Table

| Item | Floor Surface Area ft ${ }^{2}$ | Height to Water Table ft | Total Volume per Item $\mathbf{f t}^{\mathbf{3}}$ |
| :---: | :---: | :---: | :---: |
| Spent Fuel Pool | 2028.13 | 3.00 | 6084.38 |
| Transfer Canal | 423.17 | 3.00 | 1269.50 |
|  |  | Totals | 7353.88 |

As seen in Figure 36, the floor under most of the Spent Fuel Pool is 4 feet thick and increases to 6 feet thick near the Transfer Canal. The concrete volumes of the walls and floors are shown in Table 58.

Table 58 - Spent Fuel Pool and Transfer Canal Wall and Floor Concrete Volumes

| Item | $\begin{gathered} \text { Length } \\ \mathrm{ft} \end{gathered}$ | Width ft | $\begin{gathered} \text { Thickness } \\ \text { ft } \end{gathered}$ | Concrete Volume per Item $\mathbf{f t}^{3}$ | No Items | Total Concrete Volume per Item ft $^{3}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| West Wall | 63 | 12 | 6 | 4536 | 1 | 4536.00 |
| East Wall | 105.79 | 12 | 6 | 7617 | 1 | 7617.00 |
| South Wall | 39 | 12 | 6 | 2808 | 1 | 2808.00 |
| North Wall | 39 | 12 | 6 | 2808 | 1 | 2808.00 |
| Cask Pit Walls | 9.25 | 12 | 2.75 | 305.3 | 2 | 610.50 |
| Pool Floor | 51 | 33 | 4 | 6666 | 1 | 6666.00 |
| Pool Floor | 12.50 | 33 | 6 | 2475 | 1 | 2475.00 |
| Transfer Canal East Wall | 105.8 | 4 | 5.25 | 2222 | 1 | 2221.63 |
| Transfer Canal Floor | 105.8 | 15.25 | 6 | 9680 | 1 | 9679.94 |
|  |  |  | Totals | 39116.81 |  | 39422.06 |

The dimensions of a potential abstracted model of the Spent Fuel Building are provided in Table 59.

| Description | Floor Elev ft | $\begin{gathered} \text { Length } \\ \mathrm{ft} \\ \hline \end{gathered}$ | $\begin{gathered} \text { Width } \\ \text { ft } \end{gathered}$ | Floor Area $\mathbf{f t}^{2}$ | $\begin{gathered} \text { Height } \\ \text { to } \\ \text { Water } \\ \text { Table ft } \\ \hline \end{gathered}$ | Void Space to WT $\mathbf{f t}^{3}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Spent Fuel Building | 576 | 38.91 | 63 | 2451.29 | 3 | 7353.88 |

### 3.5. Containment Buttress Pits and Tendon Tunnel Access

There are 6 Tendon Buttress Pits equally spaced around each Containment (\#s TBP1-1 through TBP1-6 and TBP2-1 through TBP 2-6) as seen in Figure 38. The most westerly TBP associated with each containment structure (TBP \#1-1 \& TBP \#2-1) also provides access to the tendon tunnel at the west tendon tunnel sump. Access into the TBP is through 2 removable slabs in the concrete cap at the $592^{\prime}$ el. An access ladder extends down to the $565^{\prime}$ el provide access to the bottom of the TBP.


Figure 38 - Unit 1 and 2 Tendon Buttress Pits
The Tendon Buttress Pit below grade structures provide access to the containment horizontal tendons anchored in the buttresses. The structure consists of concrete walls from 591' 6 'elevation down to 565 'el floor. The end state walls will be from the 588 ' to the 565 ' elevation or 23 '. The inner vertical wall of the TBP is the outer radial wall of the containment which includes the tendon buttress which is $12^{\prime}$ wide and protrudes from the containment wall approximately $1^{\prime} 10^{\prime \prime}$. The $1^{\prime} 10$ " face at each end of the buttress has painted tendon end caps. The exterior containment wall and horizontal tendon buttresses continue above the 592'el to the top of the vertical exterior of the containment. The TBPs have a wall centered on the tendon buttress dividing the space into 2 chambers.


Figure 39 - Tendon Buttress Pits 2 through 6 Dimensions from B-249
A s seen in Figure 40, Tendon Buttress Pits 2 through 6 end states are 23 ' high on the exterior and interior. The rectangular box shaped space is divided by a 23 ' high vertical wall centered on the tendon buttress that extends out from the containment structure to the outer wall of the TBP forming 2 chambers.

The side walls are by $7^{\prime} 6^{\prime \prime}$ wide on the exterior and $6^{\prime} 1^{\prime \prime}$ interior that connect to the outer radius of the containment structure. The interior surface area of each side wall is $139.92 \mathrm{ft}^{2}$. The vertical side walls are 1' thick resulting a concrete volume of each wall is $139.92 \mathrm{ft}^{3}$. The outer wall is 30 feet wide on the exterior with two interior surface areas due to the 1 foot thick center divider wall. This results in a $6^{\prime} 6^{\prime \prime}+6^{\prime} 6^{\prime \prime}$ or 13 foot width for each of the back wall interior surfaces or $26^{\prime}$ overall for $600.5 \mathrm{ft}^{2}$. The concrete volume of the outer wall is 30 feet by 1 foot thick by 23 ' for a concrete volume of $690 \mathrm{ft}^{3}$. The width of the interior divider wall, as seen in Figure 39, is 5 ' $3^{\prime \prime}-1$ ' $73 / 16$ "$1 / 2$ " or 3.15 feet. This equals an interior surface area of one side of $72.47 \mathrm{ft}^{2}$.


Figure 40-Tendon Buttress Pit 2-6 Side View Section FF B-235
As seen in Figure 39, the divider wall abuts to within $1 / 2$ " of the Tendon Buttress. The Tendon Buttress has two angle sides that extend the full 23 in elevation. The width is the hypotenuse of a $1^{\prime}$
$73 / 16^{\prime \prime}+3$ " opposite and $29 / 16^{\prime \prime}$ base or $1.861^{\prime}$ equaling a surface area of $42.81 \mathrm{ft}^{2}$ per side or $85.62 \mathrm{ft}^{2}$ for both. The flat surface of the Tendon Buttress is 23 ' high by 12 ' for a surface area of $276 \mathrm{ft}^{2}$. The concrete volume of the two angled sides of the Tendon Buttress is $42.81 \mathrm{ft}^{2} \times 29 / 16^{\prime \prime}$ thickness or $9.1 \mathrm{ft}^{3}$. The Volume of the flat center portion of the Tendon Buttress is $12^{\prime}-219 / 16^{\prime \prime}-$ $2 " 9 / 16^{\prime \prime}$ or $23^{\prime} \times 11.57^{\prime} \times 1$ x $7 / 16^{\prime \prime}$ or $426 \mathrm{ft}^{3}$. As seen in Figure 39, there two wedges at either end of the center section approximately 2 " $\times 3$ ' created by the curvature of the Containment. This provides an additional volume of $23^{\prime} \times 2$ " $x 3^{\prime}$ resulting in an additional concrete volume of 11.5 $\mathrm{ft}^{3}$.

As seen in Figure 39, the Containment outer wall section between the Tendon Buttress and the Side Wall is 7 ' 6 '" $-29 / 16^{\prime \prime}$ or $7.28^{\prime}$. B-223 shows the radius to the outer surface of Containment to be 73 ' 6 ' making the circumference 461.81 '. The curved face of the containment between the Tendon Buttress and the Side Walls is a Circular Segment as seen in Figure 39 and Figure 41. The cord length is the hypotenuse of the 1 ' 1 " base and $7.28^{\prime}$ opposite or 7.37 '.


Area:
$A=\frac{1}{2} R^{2}(\alpha-\sin \alpha)$
Arc length:
$L=\alpha R$
Chord length:
$c=2 R \sin \frac{\alpha}{2}$
Segment height:
$h=R\left(1-\cos \frac{\alpha}{2}\right)$
Figure 41 - Circular Segment Equations
The angle of the curved face of the containment exterior wall between the Tendon Buttress and the Side Wall can be calculated using Equation 1 .
Equation 1 - Angle and Arc Length Circular Segment

$$
\begin{gathered}
c=2 R \sin \frac{\propto}{2} \\
\propto_{\text {radians }}=\operatorname{ASIN}\left(\frac{c}{R}\right)=\operatorname{ASIN}\left(\frac{7.37}{73.5}\right)=0.100394 \\
L=\propto R=0.100394 \times 73.5=7.38
\end{gathered}
$$

In this case the arc length is virtually the same as the cord length which is evident in Figure 39. The surface area of each section between the Tendon Buttress and the Side Wall is 7.38' x 23' or 169.7

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$\mathrm{ft}^{2}$. The volume of the Containment wall concrete is already calculated and included in TSD 13-005 (2).

The $565^{\prime}$ floor is $27^{\prime}$ long by $6^{\prime} 1^{\prime \prime}$ wide minus the Containment Wall Circular Segment and Tendon Buttress surface Areas as seen in Figure 42.


Figure 42 - B-249 Top Buttress Pit 565' Floor Surface Area Top Vies
The $27^{\prime}$ by $6^{\prime} 1^{\prime \prime}$ Surface Area is $164.25 \mathrm{ft}^{2}$. As seen in Equation 1, the angle for the $27{ }^{\prime}$ cord is

$$
\begin{gathered}
\propto_{\text {radians }}=\operatorname{ASIN}\left(\frac{c}{R}\right)=\operatorname{ASIN}\left(\frac{27}{73.5}\right)=0.376155 \\
\propto_{\text {degrees }}=0.376155\left(\frac{180}{\pi}\right)=21.55^{\circ}
\end{gathered}
$$

The area of the circular segment is shown in Equation 2.

## Equation 2 - Surface Area of Circular Segment

$$
A=\frac{1}{2} 73.5^{2}(0.3607-\sin 0.3607)=23.79 f t^{2}
$$

The Tendon Buttress surface area is $\left(12^{\prime}+29 / 16^{\prime \prime}\right) \times\left(1^{\prime} 73 / 16^{\prime \prime}+3 \prime\right)=22.58 \mathrm{ft}^{2}$. The divider wall is $3.15^{\prime} \times 1$ ' or $3.15 \mathrm{ft}^{2}$. The net surface area of the floor is $164.25 \mathrm{ft}^{2}-23.79 \mathrm{ft}^{2}-22.58 \mathrm{ft}^{2}-3.15 \mathrm{ft}^{2}$ or $114.73 \mathrm{ft}^{2}$. The calculated surface areas are summarized in Table 60.

Table 60 - Single Unit Tendon Buttress Pit Surface Areas 2 though 6

| Area | $\begin{gathered} \text { Length } \\ \mathrm{ft} \end{gathered}$ | $\underset{\mathrm{ft}}{\text { Width }}$ | Surface <br> Area | No Items | Total Surface Area $\mathbf{f t}^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Side Wall 1 | 23 | 6.08 | 139.92 | 2 | 279.83 |
| Outer Wall | 23 | 26 | 600.5 | 1 | 600.5 |
| Divider Wall | 23 | 3.15 | 72.47 | 2 | 144.95 |
| Divider Wall Facing CTMT | 23 | 1.00 | 25.5 | 1 | 25.5 |
| Tendon Buttress Sides | 23 | 1.861 | 42.81 | 2 | 85.62 |
| Tendon Buttress Center | 23 | 12 | 276 | 1 | 276 |
| CTMT Outer Buttress to Side Wall | 23 | 7.38 | 169.7 | 2 | 339.43 |
| Floor Over All | 27 | 6.08 | 164.25 | 1 | 164.25 |
| Circular Segment | 27 |  | -23.79 | 1 | -23.79 |
| Tendon Buttress | 12.21 | 1.85 | -22.58 | 1 | -22.58 |
| Divider Wall | 3.15 | 1.00 | -3.15 | 1 | -3.15 |
|  |  |  | Totals |  | 1866.56 |
|  | Totals 2 thu 6 |  |  | 5 | 9332.78 |



Figure 43 - Tendon Buttress Pit End Relative to Containment Foundation
As seen in Figure 43, a portion of the Buttress Pit floor rests on the Containment Foundation whose concrete volume is included in TSD 13-005 (2) with the ends overhanging it by about $4^{\prime} 6$ " at the ends as seen in Figure 43 and Figure 44. The area of the floor extending beyond the foundation is $4.6 \times 30$ minus or $135 \mathrm{ft}^{2}$ the area of the circular segments highlighted in yellow. B-223 shows the radius of the Containment foundation to be $78^{\prime} 6^{\prime \prime}$. The cord is 30 feet and the angle is 0.392139 radians.


Figure 44 - Containment Foundation Below Buttress Pit Floor
The circular segment area in $30.728 \mathrm{ft}^{2}$ making the portion that extends past the foundation for an area of $135 \mathrm{ft}^{2}-30,728 \mathrm{ft}^{2}$ or $104.27 \mathrm{ft}^{2}$. As seen in Figure 43, the floor under the Buttress Pit is 2 feet thick making the concrete volume $208.54 \mathrm{ft}^{3}$. The Buttress Pit concrete volumes are summarized in Table 61.

Table 61 - Calculated Concrete Volumes for Buttress Pits 2 thru 6 (Single Unit)

| Item |  |  |  | $\begin{array}{c}\text { Concrete } \\ \text { Volume } \\ \text { per Item } \\ \mathbf{f t}^{3}\end{array}$ | $\begin{array}{c}\text { Width } \\ \mathbf{f t}\end{array}$ | $\begin{array}{c}\text { Thickness } \\ \mathbf{f t}\end{array}$ |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| No |  |  |  |  |  |  |
| Items |  |  |  |  |  |  | \(\left.\begin{array}{c}Total <br>

Concrete <br>
Volume <br>
per Item <br>
\mathbf{f t}^{3}\end{array}\right]\)

The void space to the water table at the 579 ' elevation is $579-565$ or 14 ' multiplied by the floor surface area of $114.73 \mathrm{ft}^{2}$ or $1,606.17 \mathrm{ft}^{3}$ as seen in Table 62.

Table 62 - Tendon Buttress Pits 2 thu 6 Void Space Below Water Table

| Item | Floor <br> Surface <br> Area ft $^{2}$ | Height <br> to <br> Water <br> Table ft $^{2}$ | Total <br> Volume per <br> Item ft |
| :--- | :---: | :---: | :---: |
| Single Pit | 114.73 | 14.00 | 1606.17 |
| Pits 2 thu 6 for a Unit | Total | 5 | 8030.84 |

Unit 1 and Unit 2 Buttress Pits 1-1 and 2-1 have a different configuration than Pits 2 through 6 with an access to the Tendon Tunnel as seen in Figure 38.


Figure 45 - Buttress Pit 1 Top View
As seen in Figure 45, the Unit 1 1-1 and Unit 2 2-1 western most Buttress Pits include an access to the Tendon Tunnel from floor of the Tendon Buttress Pits at the $565^{\prime}$ elevation to the floor of the Tendon Tunnel at the $548^{\prime} 6^{\prime \prime}$. As seen in Figure 46, the roof is a $1^{\prime}$ thick concrete slab that extends
from the 592' elevation to the 591' elevation. The end state is 3 feet below that at the 588 ' elevation. Side 1 is $1^{\prime} 6^{\prime \prime}$ thick and extends from the $588^{\prime}$ to the 565 ' elevation or 23 feet as seen in Figure 47. The interior surface is $6^{\prime} 3$ " wide making the interior surface area $143.75 \mathrm{ft}^{2}$. The exterior wall is 7 ' $9^{\prime \prime}$ making the concrete volume is $267.38 \mathrm{ft}^{3}$. Outer Wall 1 is 13 feet long, $1^{\prime} 6^{\prime \prime}$ thick and 23 feet high for an interior surface area of $301.5 \mathrm{ft}^{2}$. The concrete volume of Outer Wall 1 is $1^{\prime} 6^{\prime \prime}$ thick to the $580^{\prime}$ elevation and 2 feet thick from the $580^{\prime}$ to the $565^{\prime}$ elevation. Resulting in the upper portion being $156 \mathrm{ft}^{3}$ and the lower portion being $390 \mathrm{ft}^{3}$. The second side wall is $10^{\prime} 6^{\prime \prime}$ $6^{\prime} 6^{\prime \prime}$ or 4 feet wide. The interior surface is $3^{\prime} 6^{\prime \prime}$ as seen in Figure 45 . The top section of the Side Wall 2 is $1^{\prime} 6^{\prime \prime}$ thick from the 588 ' to the 580 " and 2 feet thick from the $578^{\prime} 6^{\prime \prime}$ to the 565 '. The divider wall sides are $5^{\prime}-1^{\prime} 73 / 16^{\prime \prime}-1 / 2^{\prime \prime}$ or $2.9^{\prime}$ and extends from the $588^{\prime}$ to the $565^{\prime}$ elevation resulting is surface area of $66.72 \mathrm{ft}^{2}$ per side or $133.45 \mathrm{ft}^{2}$ total. The surface of the divider wall facing the containment wall is $2^{\prime}$ by 23 feet or $46 \mathrm{ft}^{2}$. The divider wall volume is $2.9^{\prime} \times 2^{\prime} \times 23^{\prime}$ or $133.45 \mathrm{ft}^{3}$. The divider wall surface facing the Containment is $23^{\prime}$ high by $2^{\prime}$ wide or 46 square feet.
Side wall 3 extends from the $588^{\prime}$ elevation to the $548^{\prime} 6^{\prime \prime}$ elevation or 40 ' as seen in Figure 46 . The walls is $1^{\prime} 6^{\prime \prime}$ thick to the 580 foot elevation resulting in 156 ft 3 , then is 2 feet thick from there to $548^{\prime} 6^{\prime \prime}$ resulting in. The wall interior width is $8^{\prime} 6^{\prime \prime}+1^{\prime} 3^{\prime \prime}$ or $9^{\prime} 9^{\prime \prime}$ to the $565^{\prime}$ elevation. After that it is about $4^{\prime} 9^{\prime \prime}$ wide to the $548^{\prime} 6^{\prime \prime}$. Side wall 4 from the $565^{\prime}$ to the $548^{\prime} 6^{\prime \prime}$ is $3^{\prime} 9^{\prime \prime}$ wide. Outer wall 2 surface area is $14^{\prime} 3^{\prime \prime}$ to the $565^{\prime}$ elevation and 7 feet from the $565^{\prime}$ to the $548^{\prime} 6^{\prime \prime}$. The tendon buttress sides and center are the same as Table 60. The face of the containment wall to the right of the buttress is $13^{\prime}-6^{\prime}-29 / 16^{\prime \prime}$ or $6.79^{\prime}$. The width is the square root of $6.79^{2}+1^{2}$ or $6.86^{\prime}$ making the surface rea to the $565^{\prime}$ elevation $157.8 \mathrm{ft}^{2}$. The left hand containment wall is $8^{\prime} 3^{\prime \prime}-29 / 16^{\prime \prime}$ or $8.04^{\prime}$ making the hypotenuse 8.10 feet long for a total surface area of $186.26 \mathrm{ft}^{2}$. The portion of the Containment forming a wall next to the ladder is the hypotenuse of $7^{\prime}$ and $1^{\prime}$ or 7.07 ' wide by $9^{\prime}$ long or $63.64 \mathrm{ft}^{2}$.
The floor area at $565^{\prime}$ is $13^{\prime}$ by $6^{\prime} 3^{\prime \prime}$ or $81.25 \mathrm{ft}^{2}$ and $12^{\prime} 9^{\prime \prime}$ by $9^{\prime} 9^{\prime \prime}$ or $121.31 \mathrm{ft}^{2}$. Minus the Circular segment with a cord of $14^{\prime} 9^{\prime \prime}$ and $13^{\prime}$ or $27^{\prime} 9^{\prime \prime}$ making the angle 0.38175 radians and the area of the circular segment $25.93 \mathrm{ft}^{2}$. The Tendon Buttress surface area is the same as in Table 60. The opening in the floor to the $548^{\prime} 6^{\prime \prime}$ elevation is $7^{\prime}$ by a $4^{\prime} 3^{\prime \prime}$ average width or $29.75 \mathrm{ft}^{2}$ making the net surface area $127.30 \mathrm{ft}^{2}$.


Figure 46 - Side View of Buttress Pit 1-1 and 2-1


Figure 47 - Tendon Buttress Pits 1-1 and 2-1 Front View

There is an access area to the tendon tunnel traveling over the sump at the $548^{\prime} 6^{\prime \prime}$. The ceiling formed by the foundation is $7^{\prime}$ wide by $2^{\prime}+3^{\prime}+2.5^{\prime}$ or $52.5 \mathrm{ft}^{2}$. The tendon tunnel access walls are $16^{\prime} 6^{\prime \prime}-9^{\prime} 7^{\prime} 6^{\prime \prime}$ high by $4^{\prime} 6+2+3+5+1$ or $15^{\prime} 6^{\prime \prime}$ for an area of $116.25 \mathrm{ft}^{2}$ per side. The floor area is $7^{\prime} \times 15^{\prime} 6^{\prime \prime}$ including the floor of the sump or $108.5 \mathrm{ft}^{2}$. The Sump Walls are 5' x 3' each for a total of $60 \mathrm{ft}^{2}$. The calculated surface areas for Tendon Buttress Pit 1-1 and 2-1 are provided in Table 63.

Table 63 - Calculated Surface Areas for Tendon Buttress Pits 1-1 and 2-1

| Area | Length <br> ft | Width <br> ft | Surface <br> Area | No Items | Total <br> Surface <br> Area <br> $\mathbf{f t}^{2}$ |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Side Wall 1 to 565' | 23 | 6.25 | 143.75 | 1 | 143.75 |
| Outer Wall 1 | 23 | 13 | 301.5 | 1 | 301.5 |
| Side Wall 2 to 565' | 23 | 3.50 | 80.50 | 1 | 80.50 |
| Divider Wall | 23 | 2.90 | 66.72 | 2 | 133.45 |
| Divider Wall Face | 23 | 2 | 46.00 | 1 | 46.00 |
| Side Wall 3 to 565' | 23 | 9.75 | 224.25 | 1 | 224.25 |
| Side Wall 3 565' to 548'6" | 16.5 | 4.75 | 78.38 | 1 | 78.38 |
| Side Wall 4 565' to 548'6" | 16.5 | 3.75 | 61.88 | 1 | 61.88 |
| Outer Wall 2 to 565' | 23 | 14.25 | 327.75 | 1 | 327.75 |
| Outer Wall 2 565' to 548'6" | 16.5 | 7 | 115.50 | 1 | 115.50 |
| Tendon Buttress Sides | 23 | 1.861 | 42.81 | 2 | 85.62 |
| Tendon Buttress Center | 23 | 12 | 276 | 1 | 276 |
| CTMT Outer Buttress to Side Wall Right | 23 | 6.86 | 157.8 | 1 | 157.77 |
| CTMT Outer Buttress to Side Wall Left | 23 | 8.10 | 186.3 | 1 | 186.26 |
| CTMT Foundation | 9 | 7.07 | 63.6 | 1 | 63.64 |
| Floor Right | 13 | 6.25 | 81.25 | 1 | 81.25 |
| Floor Left | 12.75 | 9.75 | 124.31 | 1 | 124.31 |
| Circular Segment | 27 |  | -25.93 | 1 | -25.93 |
| Tendon Buttress | 12.21 | 1.85 | -22.58 | 1 | -22.58 |
| Floor Opening to 548'6"' | 7 | 4.25 | -29.75 | 1 | -29.75 |
| Foundation Ceiling | 7 | 7.5 | 52.50 | 1 | 52.50 |
| Tunnel Access Walls | 7.5 | 15.5 | 116.25 | 2 | 232.50 |
| 548'6" Floor Area | 7 | 15.5 | 108.50 | 1 | 108.50 |
| Sump Walls | 5 | 3 | 15.00 | 4 | 60.00 |
|  | Totals |  |  |  | $\mathbf{2 8 6 3 . 0 4}$ |

The total surface area of the buttress pits is $9322.78+2863.04$ or $12,195.83 \mathrm{ft}^{2}$.
The concrete volume of the walls are calculated using the wall thicknesses and lengths and widths. The 565 ' floor rests mainly on the 9 ' thick Containment foundation. The concrete volume of the foundation is included in the Concrete volume calculations in TSD 13-005. (2) B-223 shows the radius of the Containment foundation to be $78^{\prime} 6^{\prime \prime}$. The Pit 1 cord is $27^{\prime} 9^{\prime \prime}$ and the angle is 0.361313
radians resulting in a circular segment surface area of $24.06 \mathrm{ft}^{2}$. As seen in Figure 45 , the distance from outer wall 2 to the containment foundation is interpolated at 4 ' 9 " feet. Making the left side floor surface area $4.75^{\prime} \times 7^{\prime}+1^{\prime} 3^{\prime \prime} 6^{\prime} 6^{\prime \prime}$ or $4.75 \times 14.75^{\prime}$ or $70.0625 \mathrm{ft}^{2}$ which at 2 feet thick makes the volume $140.125 \mathrm{ft}^{3}$. The right side is $8^{\prime} 6-5^{\prime}-11^{\prime} 6^{\prime \prime}$ or $2^{\prime}$ which makes the right side distance to Outer Wall $14.75^{\prime}-2^{\prime}$ or $2.75^{\prime}$. The width is $13^{\prime}$ making the surface area $35.75 \mathrm{ft}^{2}$. The surface rea outside the foundation is $70.0625 \mathrm{ft}^{2}+35.75 \mathrm{ft}^{2}-24.06 \mathrm{ft}^{2}$ and the $22.75 \mathrm{ft}^{2}$ of the floor opening to the $548^{\prime} 6^{\prime \prime}$ or $52 \mathrm{ft}^{2}$ net. At 2 feet thick this is a net concrete volume of $104 \mathrm{ft}^{3}$. The Tendon Tunnel Access side walls by the sump are $7^{\prime} 6^{\prime \prime}$ from the foundation down by $15^{\prime} 6$ ' by $2^{\prime}$ thick or 232.5 ft 3 per wall which is $465 \mathrm{ft}^{3}$ overall. The floor area including the sump is $7^{\prime} \times 15^{\prime} 6^{\prime \prime} \times 2^{\prime}$ or $217 \mathrm{ft}^{3}$. The wall sof eth sump are $5^{\prime} \times 3^{\prime} \times 2$ ' or $30 \mathrm{ft}^{3}$ each for a total of $120 \mathrm{ft}^{3}$. The estimated Buttress Pit 1-1 and 2-1 concrete volumes are summarized in Table 64.

Table 64 - Estimated Concrete Volumes for Buttress Pits 1-1 and 2-1

| Item | $\underset{\mathrm{ft}}{\text { Length }}$ | Width ft | Thickness $\mathbf{f t}$ | Concrete Volume per Item ft $^{3}$ | No Items | Total Concrete Volume per Item $\mathbf{f t}^{3}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Side Wall 1 | 23 | 7.75 | 1.5 | 267.38 | 1 | 267.38 |
| Outer Wall Top 1 | 8 | 13 | 1.5 | 156.00 | 1 | 156.00 |
| Outer Wall Bottom 1 | 15 | 13 | 2 | 390.00 | 1 | 390.00 |
| Side Wall 2 Top | 8 | 4 | 1.5 | 48.00 | 1 | 48.00 |
| Side Wall 2 Bottom | 15 | 4 | 2 | 120.00 | 1 | 120.00 |
| Divider Wall | 23 | 2.90 | 2 | 133.45 | 1 | 133.45 |
| Side Wall 3 Top | 8 | 13 | 1.5 | 156.00 | 1 | 156.00 |
| Side Wall 3 Bottom | 31.5 | 13 | 2 | 819.00 | 1 | 819.00 |
| Side Wall 4 | 16.5 | 3.75 | 2 | 123.75 | 1 | 123.75 |
| Outer Wall 2 to 565' | 23 | 14.25 | 2 | 655.5 | 1 | 655.50 |
| Outer Wall $2565{ }^{\prime}$ to 548'6" | 8 | 7 | 2 | 112 | 1 | 112.00 |
| 565' Floor Left | 4.75 | 14.75 | 70.0625 |  |  |  |
| 565' Right side | 2.75 | 13 | 35.75 |  |  |  |
| 565' Foundation Circular Segment |  |  | -24.06 |  |  |  |
| Floor Opening to 548'6" | 4.25 | 7 | -29.75 |  |  |  |
| Floor Area Concrete Outside Foundation |  |  | 2 | 104.00 | 1 | 104.00 |
| Tendon Buttress Sides | 23 | 1.861 | 0.21 | 9.1 | 1 | 9.14 |
| Tendon Buttress Center | 23 | 11.57 | 1.60 | 426 | 1 | 425.61 |
| Tendon Buttress Center End Wedges | 23 | 3 | 0.17 | 11.5 | 1 | 11.5 |
| Tunnel Access Walls | 7.5 | 15.5 | 2 | 232.5 | 2 | 465.00 |
| 548'6" Floor Area | 7 | 15.5 | 2 | 217 | 1 | 217.00 |
| Sump Walls | 5 | 3 | 2 | 30 | 4 | 120.00 |
| Totals |  |  |  |  |  | 4333.32 |

The total concrete volume for the buttress pits associated per unit is $8489.45 \mathrm{ft}^{3}$ for pits 2-6 and $433.32 \mathrm{ft}^{3}$ for pit 1 or $12,818,81 \mathrm{ft}^{3}$.
The void space below the $57{ }^{\prime}$ ' water table is Table 65.
Table 65 - Pit 1 Void Space Below Water Table at 579'

| Item | Floor <br> Surface <br> Area <br> $\mathbf{f t}^{2}$ | Height <br> to of <br> Void <br> ft | Total <br> Volume <br> per Item <br> $\mathbf{f t}^{3}$ |
| :--- | :---: | :---: | :---: |
| To 565' | 127.30 | 14.00 | 1782.22 |
| Opening Beside Foundation | 29.75 | 9 | 267.75 |
| Tunnel Access 548'6" | 108.50 | 7.5 | 813.75 |
| Tendon Tunnel Sump | 5 | 3 | 15.00 |
| Pit 1 Water Table Void Space | Total | 33.50 | 2878.72 |

The total void space below the water table per unit for buttress pits is $2878.72 \mathrm{ft}^{3}+8,0.30 .84 \mathrm{ft}^{3}$ or $10,909.56 \mathrm{ft}^{3}$.

## 4. CONCLUSION

As seen in Table 66, the ancillary buildings include structures with low contamination levels and large surface areas and void spaces. The Spent Fuel Pool, Transfer Canal and WWTF will require additional characterization when their use is discontinued.

Table 66 - Summary of Ancillary Building Surface Areas, Water Table Void Space, and Concrete Volumes

| Structure | Total Wall and Floor Surface Area $\mathrm{ft}^{2}$ below 588' Elevation | Total Water Table Void Volume to 579 ft per Item ft ${ }^{3}$ | Total Water Table Void Volume to 579 ft per Item $\mathbf{m}^{3}$ | Total <br> Concrete <br> Volume per Item ft ${ }^{3}$ |
| :---: | :---: | :---: | :---: | :---: |
| Unit 1 Containment Liner Only | $2.97 \mathrm{E}+04$ | 230,881 | 6,538 |  |
| Unit 2 Containment Liner Only | $2.97 \mathrm{E}+04$ | 230,881 | 6,538 |  |
| Auxiliary Building | $7.00 \mathrm{E}+04$ | 1,003,735 | 28,423 | $5.20 \mathrm{E}+05$ |
| Turbine Bld, Main Steam Tunnel, Diesel Oil | $1.65 \mathrm{E}+05$ | 920,193 | 26,057 | $1.12 \mathrm{E}+06$ |
| Unit 1 Discharge Tunnel | $2.62 \mathrm{E}+04$ | 105,650 | 2,992 | $1.16 \mathrm{E}+05$ |
| Unit 2 Discharge Tunnel | $2.62 \mathrm{E}+04$ | 105,650 | 2,992 | $1.16 \mathrm{E}+05$ |
| Crib House and Forebay | $1.49 \mathrm{E}+05$ | 923,738 | 26,157 | $5.05 \mathrm{E}+05$ |
| Waste Water Treatment Facility | $1.21 \mathrm{E}+04$ | 5,082 | 144 | $1.27 \mathrm{E}+04$ |
| Spent Fuel Building | $7.78 \mathrm{E}+03$ | 7,354 | 208 | 3.94E+04 |
| Buttress Pits | $1.22 \mathrm{E}+04$ | 10,910 | 309 | $1.28 \mathrm{E}+04$ |
| Totals | 3.98E+05 | $2.08 \mathrm{E}+06$ | $5.89 \mathrm{E}+04$ | $1.92 \mathrm{E}+06$ |

## 5. REFERENCES

1. TSD 14-013 Zion Auxiliary Building End Sate Estimated Concrete Volumes, Surface Areas, and Source Terms.
2. TSD 13-005 Unit 1 \&2 Reactor Building Estimated End State Concrete and Liner Volumes and Surface Areas.
3. Zion Nuclear Power Station, Units 1 And 2 Asset Sale Agreement, December 11, 2007.

## 6. ATTACHMENTS

None

