

TECHNICAL EVALUATION REPORT

**PRIMARY COOLANT SYSTEM
PRESSURE ISOLATION VALVES**

FLORIDA POWER & LIGHT COMPANY
ST. LUCIE UNIT 1

NRC DOCKET NO. 50-335

NRC TAC NO. 12887

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FRC PROJECT C5257

FRC TASK 221

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1.0 INTRODUCTION

The NRC has determined that certain isolation valve configurations in systems connecting the high-pressure Primary Coolant System (PCS) to lower-pressure systems extending outside containment are potentially significant contributors to an intersystem loss-of-coolant accident (LOCA). Such configurations have been found to represent a significant factor in the risk computed for core melt accidents.

The sequence of events leading to the core melt is initiated by the concurrent failure of two in-series check valves to function as a pressure isolation barrier between the high-pressure PCS and a lower-pressure system extending beyond containment. This failure can cause an overpressurization and rupture of the low-pressure system, resulting in a LOCA that bypasses containment.

The NRC has determined that the probability of failure of these check valves as a pressure isolation barrier can be significantly reduced if the pressure at each valve is continuously monitored, or if each valve is periodically inspected by leakage testing, ultrasonic examination, or radiographic inspection. The NRC has established a program to provide increased assurance that such multiple isolation barriers are in place in all operating Light Water Reactor plants designated by DOR Generic Implementation Activity B-45.

In a generic letter of February 23, 1980, the NRC requested all licensees to identify the following valve configurations which may exist in any of their plant systems communicating with the PCS: 1) two check valves in series or 2) two check valves in series with a motor-operated valve (MOV).

For plants in which valve configurations of concern are found to exist, licensees were further requested to indicate: 1) whether, to ensure integrity of the various pressure isolation check valves, continuous surveillance or periodic testing was currently being conducted, 2) whether any check valves of concern were known to lack integrity, and 3) whether plant procedures should be revised or plant modifications be made to increase reliability.

Franklin Research Center (FRC) was requested by the NRC to provide technical assistance to NRC's B-45 activity by reviewing each licensee's submittal

against criteria provided by the NRC and by verifying the licensee's reported findings from plant system drawings. This report documents FRC's technical review.

2.0 CRITERIA

2.1 Identification Criteria

For a piping system to have a valve configuration of concern, the following five items must be fulfilled:

- 1) The high-pressure system must be connected to the Primary Coolant System;
- 2) there must be a high-pressure/low-pressure interface present in the line;
- 3) this same piping must eventually lead outside containment;
- 4) the line must have one of the valve configurations shown in Figure 1; and
- 5) the pipe line must have a diameter greater than 1 inch.

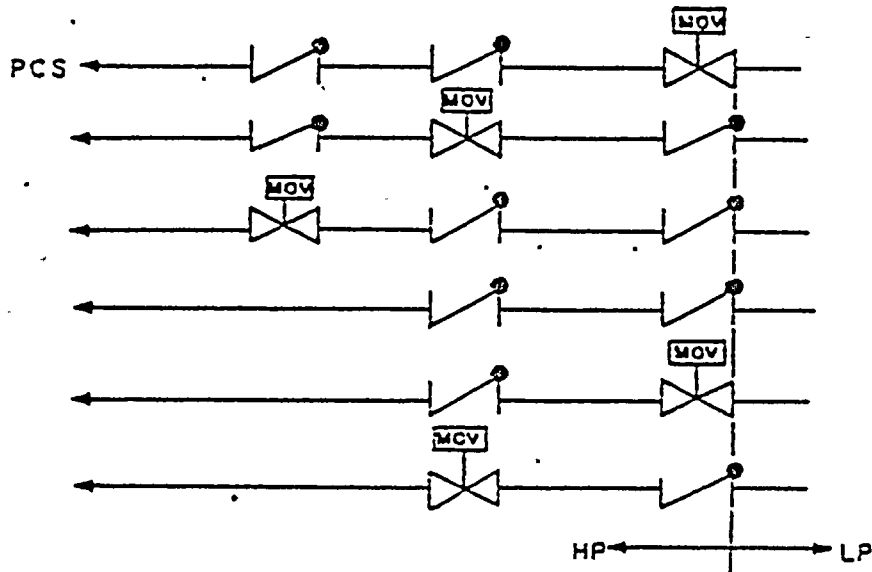


Figure 1. Valve Configurations Designated by the NRC To Be Included in This Technical Evaluation

2.2 Periodic Testing Criteria

For licensees whose plants have valve configurations of concern and choose to institute periodic valve leakage testing, the NRC has established criteria for frequency of testing, test conditions, and acceptable leakage rates. These criteria may be summarized as follows:

2.2.1 Frequency of Testing

Periodic hydrostatic leakage testing* on each check valve shall be accomplished every time the plant is placed in the cold shutdown condition for refueling, each time the plant is placed in a cold shutdown condition for 72 hours if testing has not been accomplished in the preceding 9 months, each time any check valve may have moved from the fully closed position (i.e., any time the differential pressure across the valve is less than 100 psig), and prior to returning the valve to service after maintenance, repair, or replacement work is performed.

2.2.2 Hydrostatic Pressure Criteria

Leakage tests involving pressure differentials lower than function pressure differentials are permitted in those types of valves in which service pressure will tend to diminish the overall leakage channel opening, as by pressing the disk into or onto the seat with greater force. Gate valves, check valves, and globe-type valves, having function pressure differential applied over the seat, are examples of valve applications satisfying this requirement. When leakage tests are made in such cases using pressures lower than function maximum pressure differential, the observed leakage shall be adjusted to function maximum pressure differential value. This adjustment shall be made by calculation appropriate to the test media and the ratio between test and function pressure differential, assuming leakage to be directly proportional to the pressure differential to the one-half power.

2.2.3 Acceptable Leakage Rates:

- Leakage rates less than or equal to 1.0 gpm are considered acceptable.
- Leakage rates greater than 1.0 gpm but less than or equal to 5.0 gpm are considered acceptable if the latest measured rate has not exceeded the rate determined by the previous test by an amount

*To satisfy ALARA requirements, leakage may be measured indirectly (as from the performance of pressure indicators) if accomplished in accordance with approved procedures and supported by computations showing that the method is capable of demonstrating valve compliance with the leakage criteria.

that reduces the margin between the measured leakage rate and the maximum permissible rate of 5.0 gpm by 50% or greater.

- Leakage rates greater than 1.0 gpm but less than or equal to 5.0 gpm are considered unacceptable if the latest measured rate exceeded the rate determined by the previous test by an amount that reduces the margin between measured leakage rate and the maximum permissible rate of 5.0 gpm by 50% or greater.
- Leakage rates greater than 5.0 gpm are considered unacceptable.

3.0 TECHNICAL EVALUATION

3.1 Licensee's Response to the Generic Letter

In response to the NRC's generic letter [Ref. 1], the Florida Power & Light Company (FPL) supplied in Reference 2 a simplified flow diagram showing the valve configuration of concern for St. Lucie Unit 1. This flow diagram basically outlined the High- and Low-Pressure Safety Injection Systems connected to the Primary Coolant System (PCS) piping.

The licensee further stated that instrumentation is provided to monitor the pressure on the low-pressure side of the check valves closest to the Primary Coolant System (V3217, V3227, V3237, and V3247). Also, plant procedures will be revised, according to FPL, during the current refueling outage to provide periodic surveillance testing for the remaining affected check valves:

- a) V3113 and V3114
- b) V3123 and V3124
- c) V3133 and V3134
- d) V3143 and V3144

It is FRC's understanding that, with FPL's concurrence, the NRC will direct FPL to change its Plant Technical Specifications as necessary to ensure that periodic leakage testing (or equivalent testing) is conducted in accordance with the criteria of Section 2.2.

3.2 FRC Review of Licensee's Response

FRC has reviewed the licensee's response against the plant-specific Piping and Instrumentation Diagrams (P&IDs) [Ref. 3] that might have the valve configurations of concern.

FRC has also reviewed the efficacy of instituting periodic testing for the check valves involved in this particular application with respect to the reduction of the probability of an intersystem LOCA in the the High- and Low-Pressure Safety Injection System pipe lines.

In its review of the P&IDs [Ref. 3] for St. Lucie Unit 1, FRC found the following two piping systems to be of concern:

The High- and Low-Pressure Safety Injection Systems are connected to the cold leg side of each of the four PCS loops by a single common piping line. Due to the outward branching of these four cold leg piping lines, both the High- and Low-Pressure Safety Injection Systems contain the dual check valve and a single motor-operated valve (MOV) in-series valve configuration of concern. The high-pressure/low-pressure interface is on the upstream side of the MOVs. The valves which comprise these configurations of concern are listed below for both systems.

High-Pressure Safety Injection

Loop 1A1, cold leg

high-pressure check valve, V3227
high-pressure check valve, V3123
high-pressure MOV, HCV 3626, normally closed (n.c.)

Loop 1A2, cold leg

high-pressure check valve, V3217
high-pressure check valve, V3113
high-pressure MOV, HCV 3616, n.c.

Loop 1B1, cold leg

high-pressure check valve, V3237
high-pressure check valve, V3133
high-pressure MOV, HCV 3636, n.c.

Loop 1B2, cold leg

high-pressure check valve, V3247
high-pressure check valve, V3143
high-pressure MOV, HCV 3647, n.c.

Low-Pressure Safety Injection

Loop 1A1, cold leg

high-pressure check valve, V3227
high-pressure check valve, V3124
high-pressure MOV, HCV 3625, n.c.

Loop 1A2, cold leg

high-pressure check valve, V3217
high-pressure check valve, V3114
high-pressure MOV, HCV 3615, n.c.

Loop 1B1, cold leg

high-pressure check valve, V3237
high-pressure check valve, V3134
high-pressure MOV, HCV 3635, n.c.

Loop 1B2, cold leg

high-pressure check valve, V3247
high-pressure check valve, V3144
high-pressure MOV, HCV 3645, n.c.

In accordance with the criteria of Section 2.0, FRC found no other valve configurations of concern existing in this plant. These findings confirm the licensee's response [Ref. 2].

FRC reviewed the effectiveness of instituting periodic leakage testing of the check valves in these lines as a means of reducing the probability of an intersystem LOCA occurring. FRC found that introducing a program of check valve leakage testing in accordance with the criteria summarized in Section 2.0 will be an effective measure in substantially reducing the probability of an intersystem LOCA occurring in these lines, and a means of increasing the probability that these lines will be able to perform their safety-related functions. It is also a step toward achieving a corresponding reduction in the plant probability of an intersystem LOCA in St. Lucie Unit 1.

4.0 CONCLUSION

St. Lucie Unit 1 has been determined to have valves in one of the configurations of concern in both the cold leg branches of the High- and Low-Pressure Safety Injection System.

If FPL modifies the Plant Technical Specifications for St. Lucie Unit 1 to incorporate periodic testing (as delineated in Section 2.2) for the check valves itemized in Table 1.0, then FRC considers this an acceptable means of achieving plant compliance with the NRC staff objectives of Reference 1.

Table 1.0

Primary Coolant System Pressure Isolation Valves

<u>System</u>	<u>Check Valve No.</u>	<u>Allowable Leakage*</u>
High-Pressure Safety Injection		
Loop 1A1, cold leg	V3227 V3123	
Loop 1A2, cold leg	V3217 V3113	
Loop 1B1, cold leg	V3237 V3133	
Loop 1B2, cold leg	V3247 V3143	
Low-Pressure Safety Injection		
Loop 1A1, cold leg	V3124	
Loop 1A2, cold leg	V3114	
Loop 1B1, cold leg	V3134	
Loop 1B2, cold leg	V3144	

*To be provided by the licensee at a future date in accordance with Section 2.2.3.

5.0 REFERENCES

1. Generic NRC letter, dated 2/23/80, from Mr. D. G. Eisenhut, Department of Operating Reactors (DOR), to Mr. R. E. Uhrig, Florida Power & Light Company (FPL).

2. Florida Power & Light Company's response to NRC's letter, dated 3/17/80, from Mr. R. E. Uhrig (FPL) to Mr. D. G. Eisenhut (DOR).
3. List of examined P&IDs:

FSAR Drawings of St. Lucie Unit 1:

Fig. 5.1-3

Fig. 6.3-1

Fig. 6.3-2

Fig. 9.3-2

Fig. 9.3-4

Fig. 9.3-5

Fig. 9.3-6