

Y1003J01A06
October 1980

SUPPLEMENTAL RELOAD LICENSING SUBMITTAL
FOR
DRESDEN NUCLEAR POWER STATION
UNIT 2 RELOAD 5

Prepared: *[Signature]*

for G. T. Kaminski
Licensing Engineer

Approved: *[Signature]*

R. E. Engel, Manager
Reload Fuel Licensing

NUCLEAR POWER SYSTEMS DIVISION • GENERAL ELECTRIC COMPANY
SAN JOSE, CALIFORNIA 95125

8110280270 811015
PDR ADOCK 05000237
P PDR

GENERAL  ELECTRIC

IMPORTANT NOTICE REGARDING

CONTENTS OF THIS REPORT

PLEASE READ CAREFULLY

This report was prepared by General Electric solely for Commonwealth Edison Company (CECo) for CECo's use with the U.S. Nuclear Regulatory Commission (USNRC) for amending CECo's operating license of the Dresden Nuclear Power Station Unit 2. The information contained in this report is believed by General Electric to be an accurate and true representation of the facts known, obtained or provided to General Electric at the time this report was prepared.

The only undertakings of the General Electric Company respecting information in this document are contained in the contract, as amended, between Commonwealth Edison Company and General Electric Company for nuclear fuel and related services for the nuclear system for Dresden Nuclear Power Station Units 2 and 3 and Quad Cities 1 and 2, dated December 13, 1965, and nothing contained in this document shall be construed as changing said contract. The use of this information except as defined by said contract, or for any purpose other than that for which it is intended, is not authorized; and with respect to any such unauthorized use, neither General Electric Company nor any of the contributors to this document makes any representation or warranty (express or implied) as to the completeness, accuracy or usefulness of the information contained in this document or that such use of such information may not infringe privately owned rights; nor do they assume any responsibility for liability or damage of any kind which may result from such use of such information.

4. CALCULATED CORE EFFECTIVE MULTIPLICATION AND CONTROL SYSTEM
WORTH - NO VOIDS, 20°C (3.3.2.1.1 AND 3.3.2.1.2)

BOC k_{eff}	
Uncontrolled	1.096
Fully Controlled	0.940
Strongest Control Rod Out	0.973
R, Max Increase in Cold Core Reactivity with Exposure Into Cycle, Δk	0.008

5. STANDBY LIQUID CONTROL SYSTEM SHUTDOWN CAPABILITY (3.3.2.1.3)

	Shutdown Margin (Δk) (20°C, Xenon Free)
ppm	
600	0.052

6. RELOAD-UNIQUE TRANSIENT ANALYSIS INPUTS (3.3.2.1.5 AND 5.2)

	<u>EOC 8</u>
Void Coefficient N/A*($\epsilon/\% R_g$)	-5.45/-6.82
Void Fraction (%)	34.48
Doppler Coefficient N/A ($\epsilon/^\circ F$)	-0.231/-0.219
Average Fuel Temperature ($^\circ F$)	1211
Scram Worth N/A ($\$$)	-37.94/-30.35
Scram Reactivity vs Time	Figure 2

7. RELOAD-UNIQUE GETAB TRANSIENT ANALYSIS INITIAL CONDITION
PARAMETERS (5.2)

	<u>EOC 8</u>			
<u>Exposure</u>	<u>7x7</u>	<u>8x8</u>	<u>8x8R</u>	<u>P8x8R</u>
Peaking Factors (local, radial and axial)	1.24 1.54 1.40	1.22 1.73 1.40	1.20 1.87 1.40	1.20 1.85 1.40
R-Factor	1.100	1.098	1.052	1.052
Bundle Power (MWt)	5.247	5.888	6.379	6.299
Bundle Flow (10^3 lb/hr)	111.5	107.2	105.7	106.2
Initial M CPR	1.23	1.25	1.25	1.27

*N=Nuclear Input Data, A=Used in Transient Analysis

1. PLANT-UNIQUE ITEMS (1.0)*

Items different from or not included in Reference 1.

- | | | |
|----|---|----------------|
| a. | Plant Parameter Changes | Appendix A |
| b. | Loading Error | Appendix A |
| c. | Densification Power Spiking | Appendix B |
| d. | Pressure Relief Setpoints | Reference 3 |
| e. | GETAB Initial Conditions - Inlet Enthalpy | Reference 4 |
| f. | ATWS RPT Setpoint of 1250 psig | Items 9 and 12 |

2. RELOAD FUEL BUNDLES (1.0, 2.0, 3.3.1 AND 4.0)

		<u>Fuel Type</u>	<u>Number</u>	<u>Number Drilled</u>
Irradiated	Reload 1	7DB230	4	0
	Reload 1	8DB250	48	0
	Reload 2	3DB250	28	0
	Reload 2	8DB262	68	0
	Reload 3	8DB250	192	0
	Reload 4	8DRB265L	160	160
	Reload 5	P8DRB265L	88	88
New	Reload 5	P8DRB265H	<u>136</u>	<u>136</u>
Total			724	384

3. REFERENCE CORE LOADING PATTERN (3.3.1)

Nominal previous cycle exposure: 18,751 MWd/t

Assumed reload cycle exposure: 17,481 MWd/t

Core loading pattern: Figure 1.

*() refers to areas of discussion in Reference 1.

8. SELECTED MARGIN IMPROVEMENT OPTIONS (5.2.2)

None

9. CORE WIDE TRANSIENT ANALYSIS RESULTS (5.2.1)

Transient	Exposure	Power (%)	Flow (%)	ϕ (%)	Q/A (%)	P _{sl} (psig)	P _v (psig)	ΔCPR			Plant Response	
								7x7	8x8	8x8R		
Load Rejection without Bypass	EOC 8	100	100	233	111	1209	1244	0.13	0.18	0.18	0.20	Figure 3
Loss of 145°F Feedwater Heating	--	100	100	121	119	994	1045	0.16	0.17	0.17	0.17	Figure 4
Feedwater Controller Failure	EOC 8	100	100	138	108	1112	1148	0.06	0.09	0.09	0.09	Figure 5

10. LOCAL ROD WITHDRAWAL ERROR (WITH LIMITING INSTRUMENT FAILURE) TRANSIENT SUMMARY (5.2.1)

Rod Block Reading (%)	Rod Position (Feet Withdrawn)	ΔCPR		LHGR***		Limiting Rod Pattern
		8x8*	8x8R/P8x8R	8x8	8x8R/P8x8R	
104	4.0	0.12	0.12	11.32	13.70	Figure 6
105	4.5	0.14	0.14	11.49	13.70	Figure 6
106	5.0	0.16	0.15	11.49	13.77	Figure 6
107**	5.5	0.18	0.17	11.49	13.82	Figure 6
108	6.0	0.19	0.19	11.49	13.88	Figure 6
109	7.5	0.23	0.23	11.49	13.88	Figure 6
110	9.0	0.26	0.26	11.60	16.06	Figure 6

* 7x7 bundles are all located in peripheral regions.

**Indicates setpoint selected.

***Includes 2.2% penalty due to fuel densification.

11. OPERATING MCPR LIMIT (5.2)BOC8 to EOC8

1.27	(P8x8R fuel)
1.25	(8x8R fuel)
1.25	(8x8 fuel)
1.23	(7x7 fuel)

12. OVERPRESSURIZATION ANALYSIS SUMMARY (5.3)

<u>Transient</u>	<u>Power (%)</u>	<u>Core Flow (%)</u>	<u>P_{sl} (psig)</u>	<u>P_v (psig)</u>	<u>Plant Response</u>
MSIV Closure (Flux Scram)	100	100	1293	1310	Figure 7.

13. STABILITY ANALYSIS RESULTS (5.4)

Decay Ratio: Figure 8

Reactor Core Stability: Decay Ratio, x_2/x_0 0.52
 (100% Rod Line - Natural
 Circulation Power)

Channel Hydrodynamic Performance

	<u>Decay Ratio, x_2/x_0 (100% Rod Line - Natural Circulation Power)</u>
P8x8R channel	0.17
8x8R channel	0.17
8x8 channel	0.24
7x7 channel	0.12

14. LOSS-OF-COOLANT ACCIDENT RESULTS (5.5.2)

Reference 2

15. LOADING ERROR RESULTS (5.5.4)

Limiting Event: Rotated Bundle (8x8R)

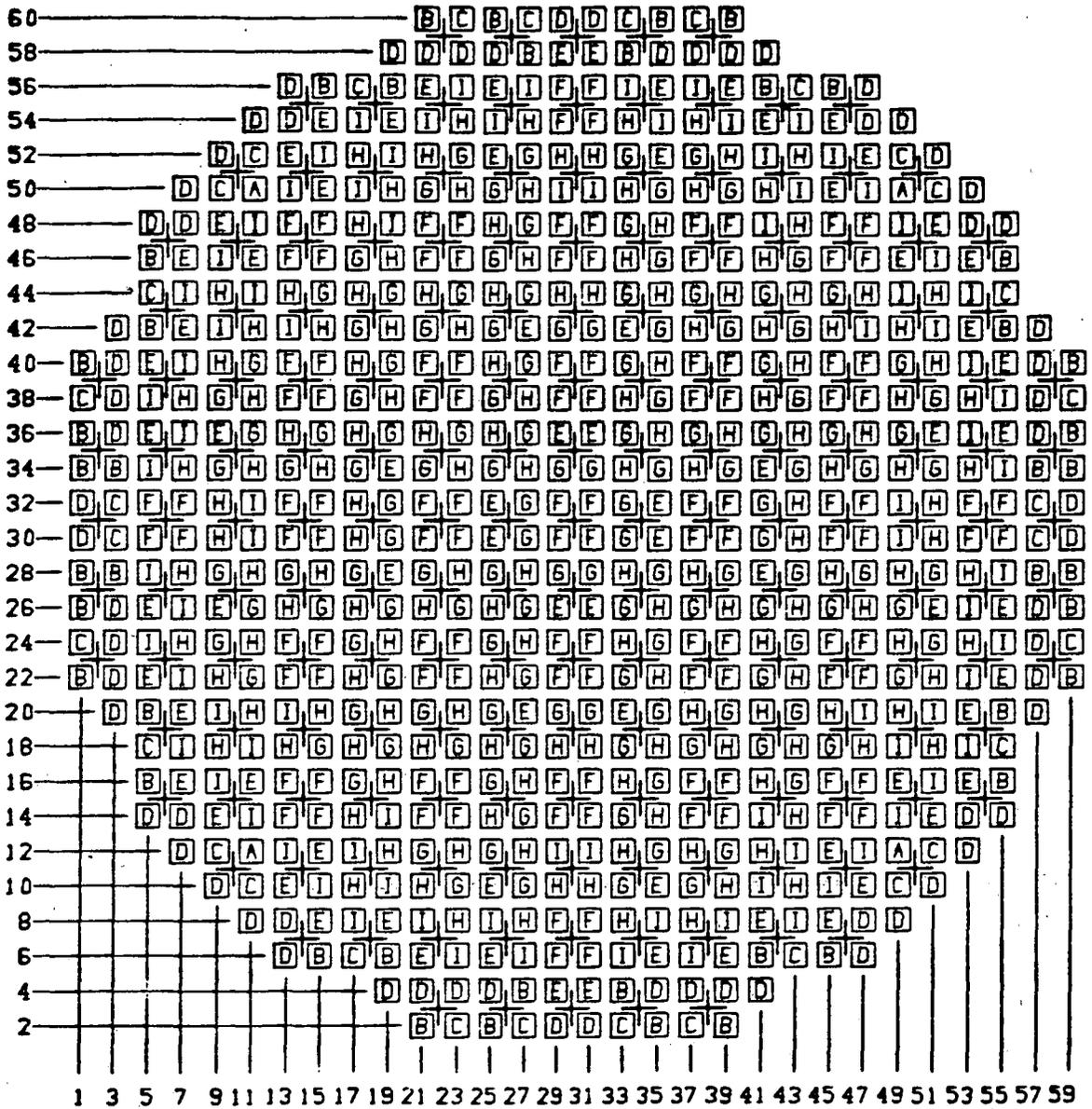
MCPR: 1.08

16. CONTROL ROD DROP ANALYSIS RESULTS (5.5.1)

Maximum incremental control rod worth: 0.465% ΔK

REFERENCES

1. "General Electric Boiling Water Reactor Generic Reload Fuel Application," July 1979 (NEDE-24011-P-1).
2. "Loss-of-Coolant Accident Analysis Report for Dresden Units 2, 3 and Quad Cities Units 1, 2 Nuclear Power Stations," NEDO-24146A, April 1979.
3. Attachment to letter No. MFN-048-80, R. E. Engel to T. A. Ippolito, "Categorization of Requested Reload Fuel Licensing Topical Report Revisions," February 27, 1980.
4. Attachment to letter, J. F. Quirk to Olan D. Parr, "General Electric Licensing Topical Report NEDE-24011-P-A-1, Generic Reload Fuel Application, Appendix D, Second Submittal," February 28, 1979.



FUEL TYPE			
A - 7DB230-GEN/B	BOC4	F - 8DB250	BOC6
B - 8DB250	BOC4	G - 8DB250	BOC8
C - 8DB250	BOC5	H - 8DB265L	BOC7
D - 8DB262	BOC5	I - 8DB265L	BOC8
E - 8DB250	BOC6		

Figure 1. Reference Core Loading Pattern

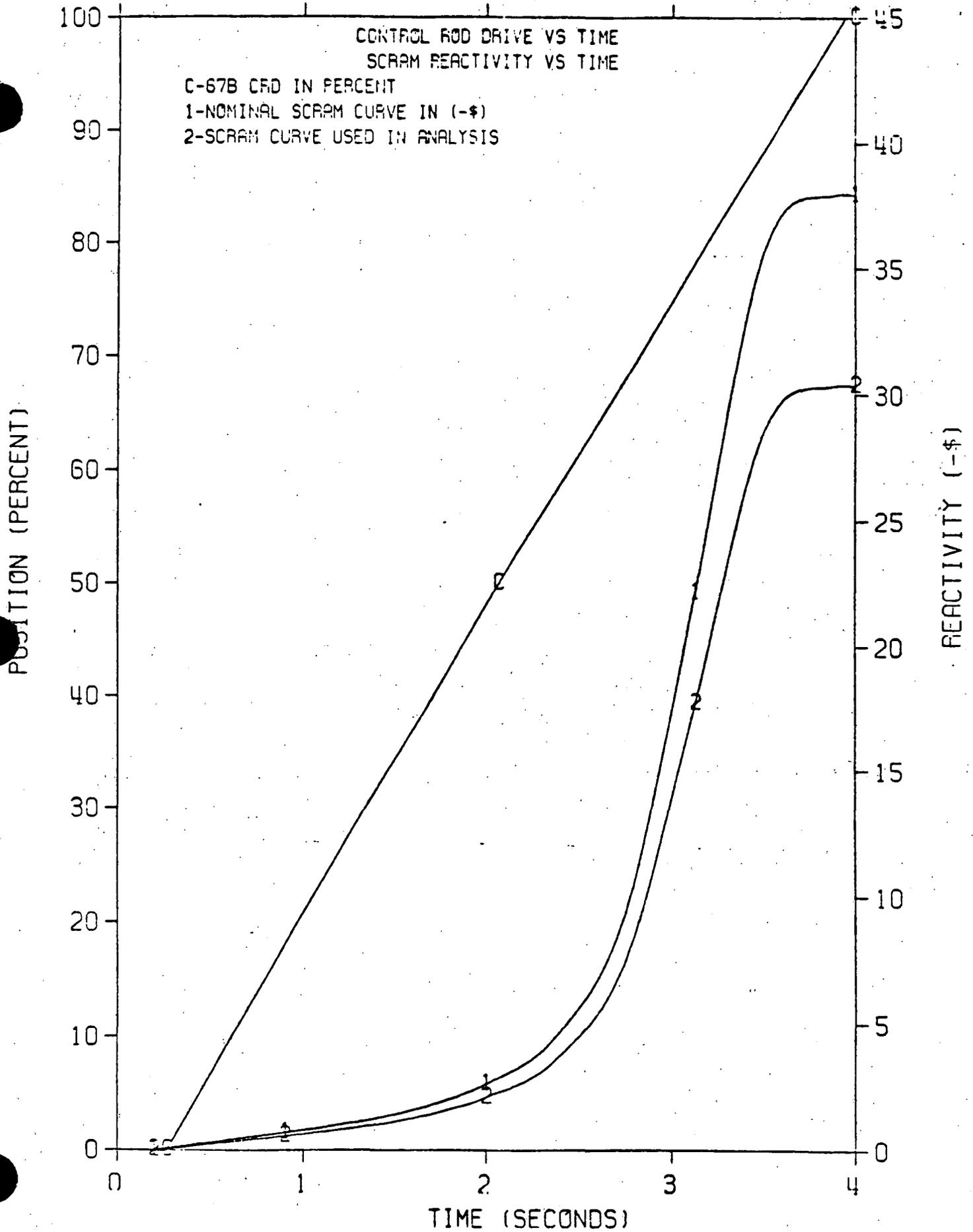


Figure 2. Scram Reactivity and Control Rod Drive Specification

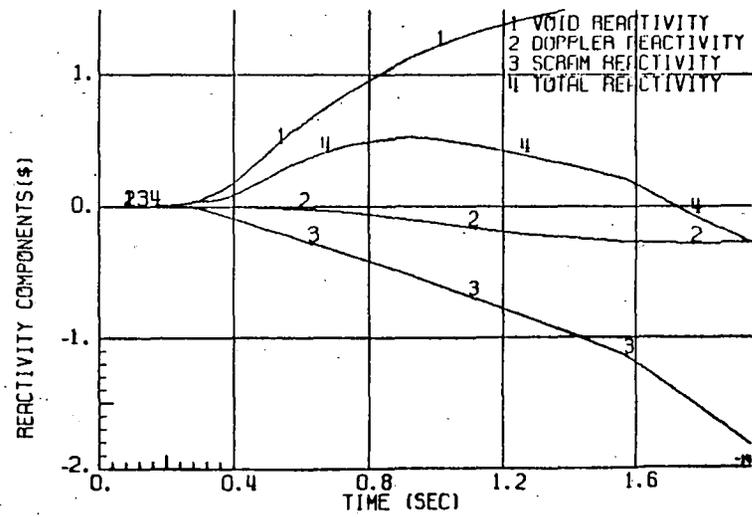
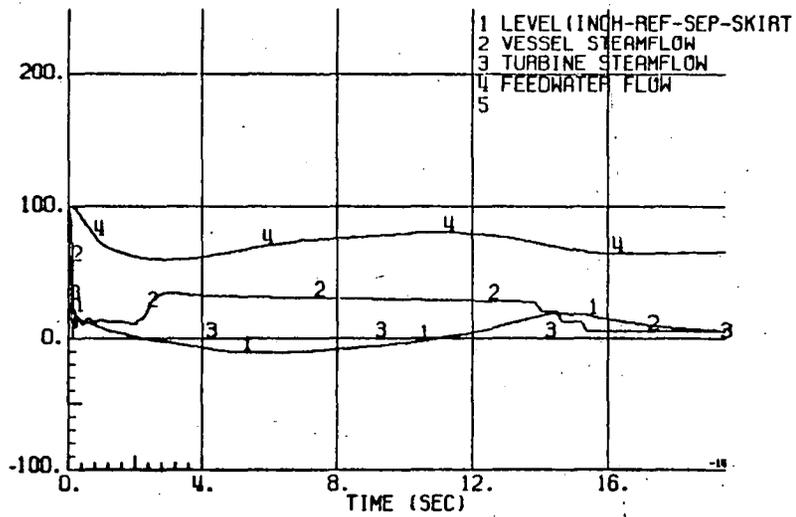
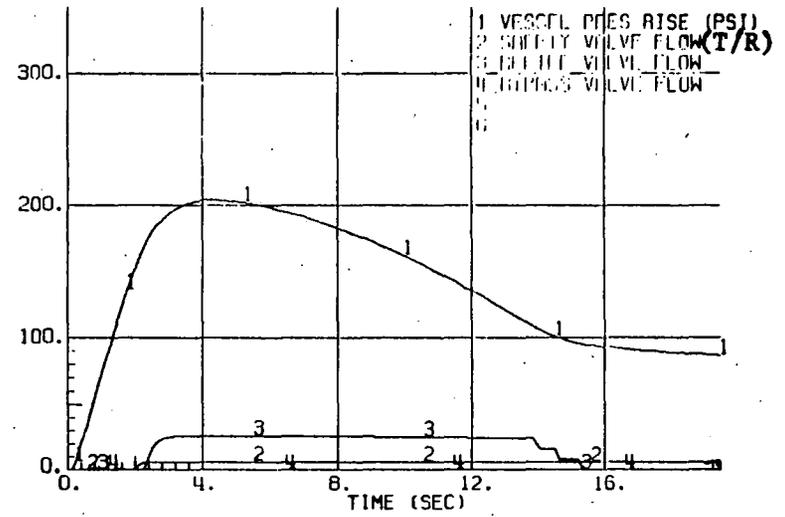
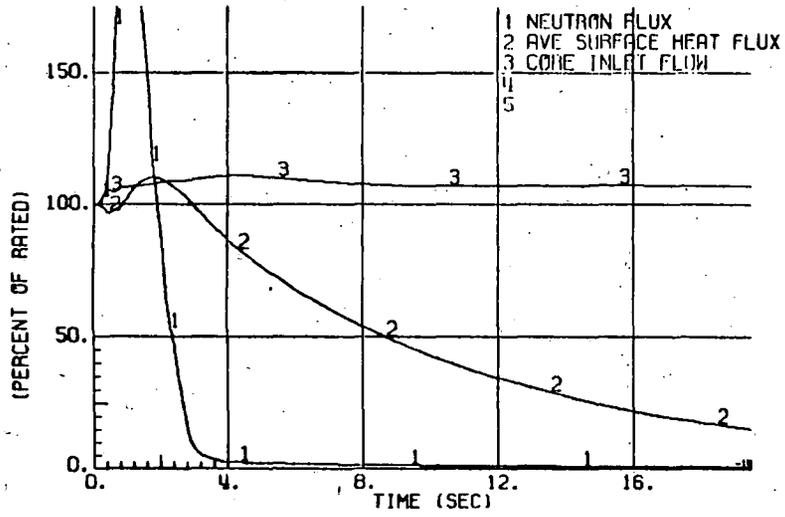


Figure 3. Plant Response to Load Rejection without Bypass

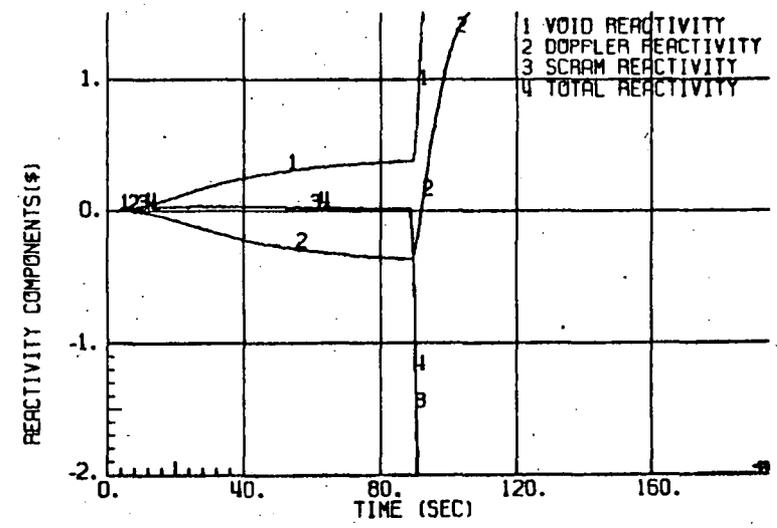
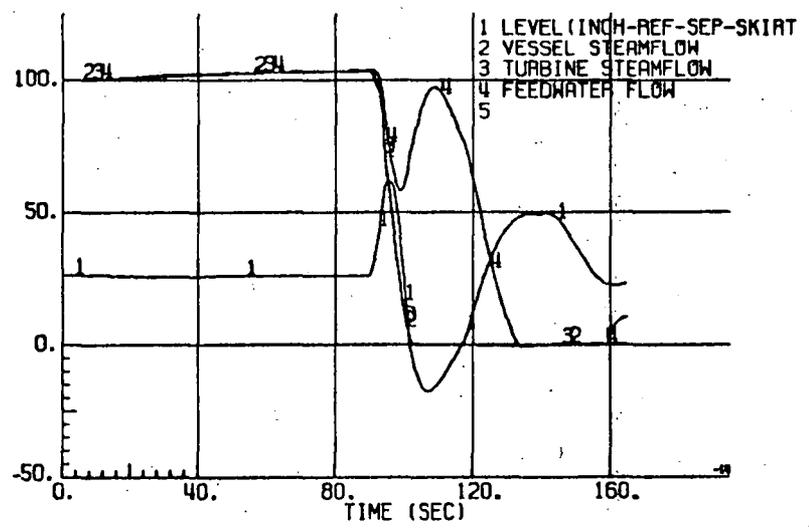
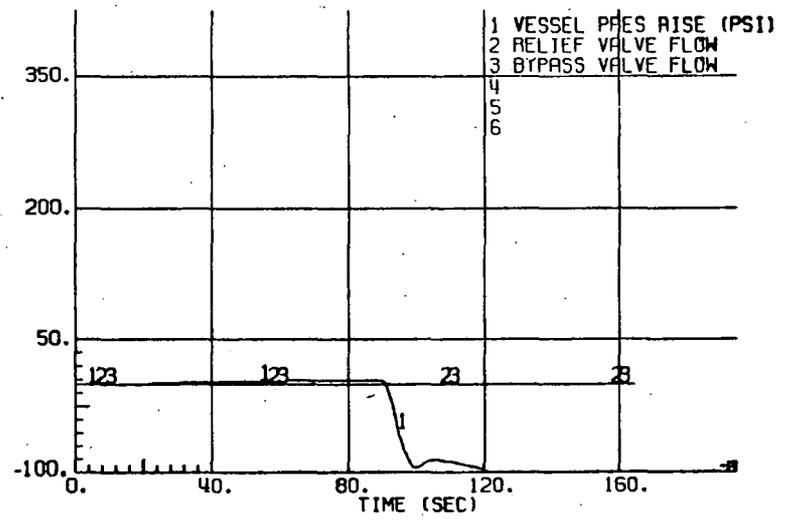
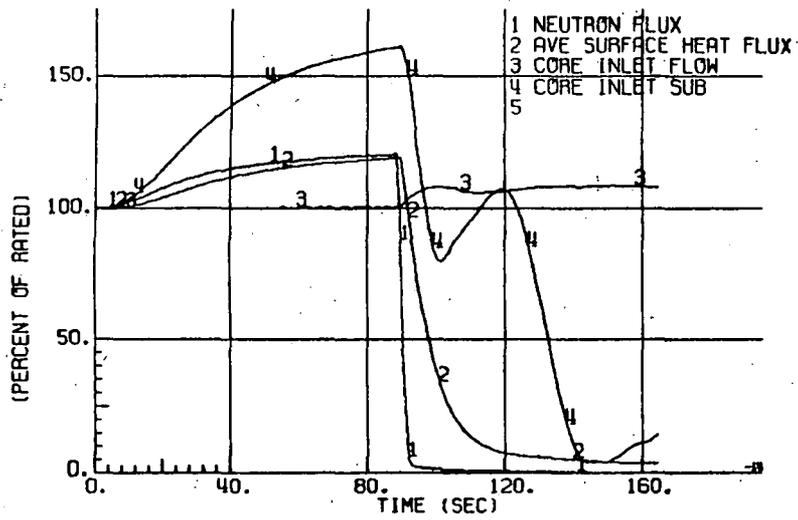


Figure 4. Plant Response to Loss of 145°F Feedwater Heating

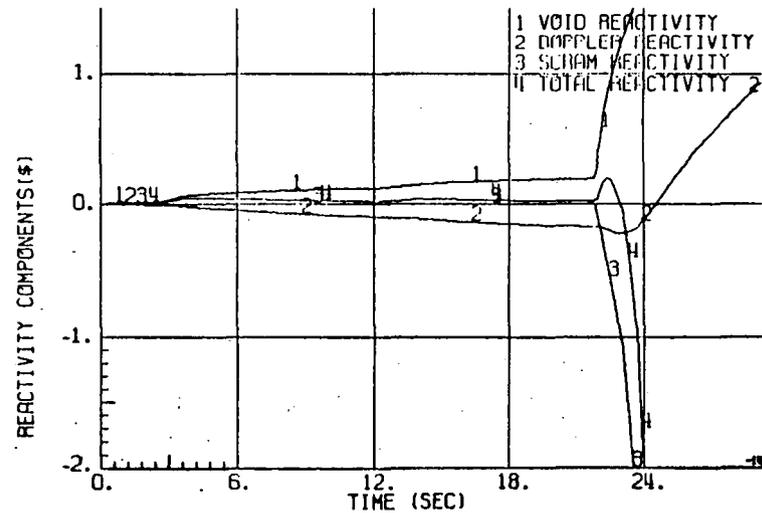
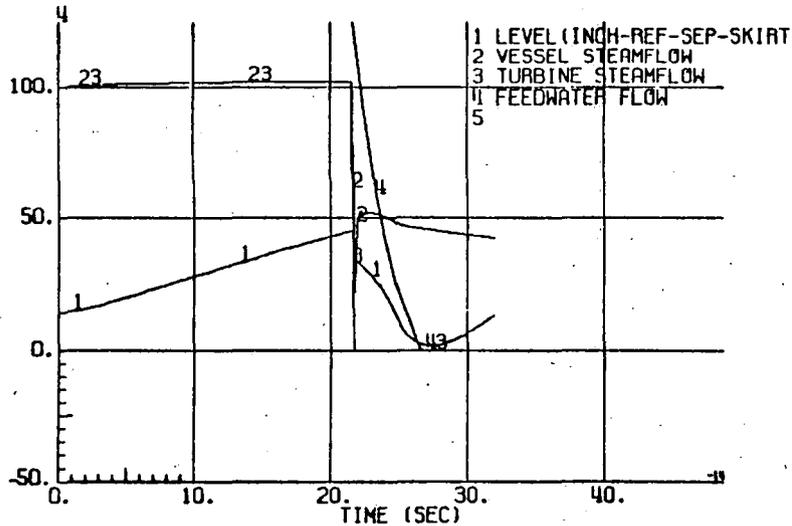
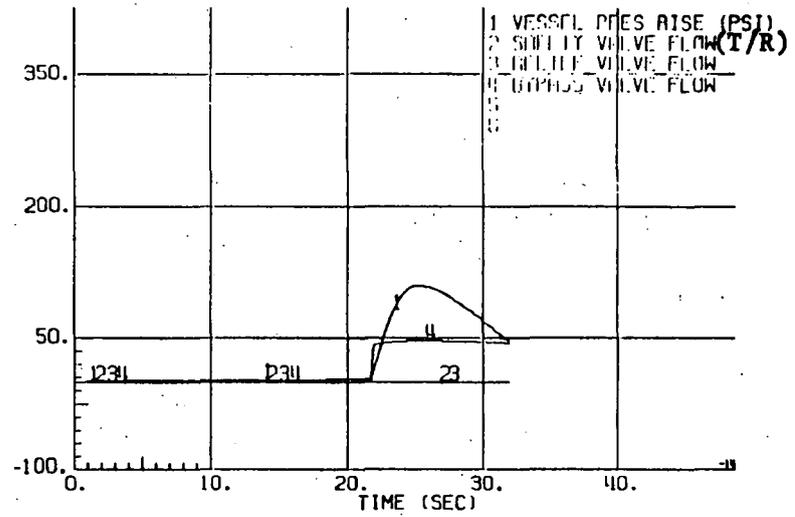
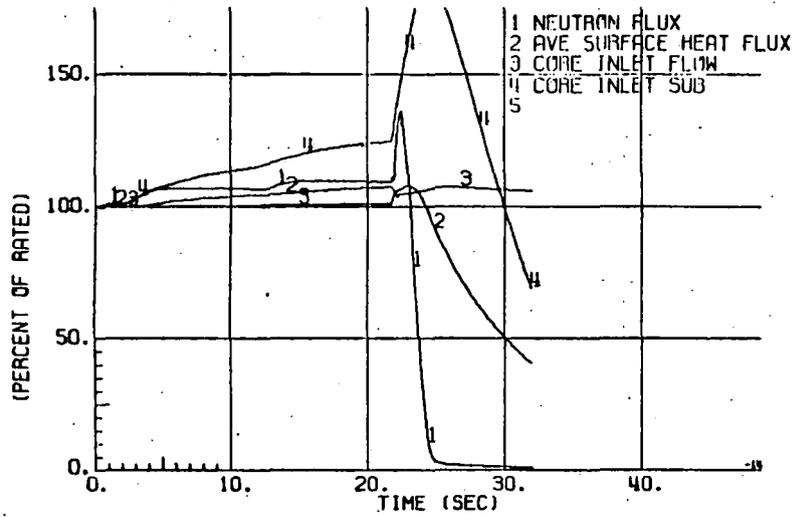


Figure 5. Plant Response to Feedwater Controller Failure

59						4		4									
55			36		38		36		38		36						
51		2		6		8		8		6		2					
47			36		44		44		44		36						
43		4		8		0		0		8		4					
39	36		38		46		46		46		38		36				
35	6	2		8		16		16		8		2		6			
31	36		36		40		40		40		36		36				
27	6	2		8		16		16		8		2		6			
23	36		38		46		46		46		38		36				
19		4		8		0		0		8		4					
15			36		44		44		44		36						
11		2		6		8		8		6		2					
7			36		38		36		38		36						
3						4		4									
	2	6	10	14	18	22	26	30	34	38	42	46	50	54	58		

NOTES:

1. No. indicates number of notches withdrawn out of 48. Blank is a withdrawn rod.
2. Error rod is (26, 43).

Figure 6. Limiting RWE Rod Pattern

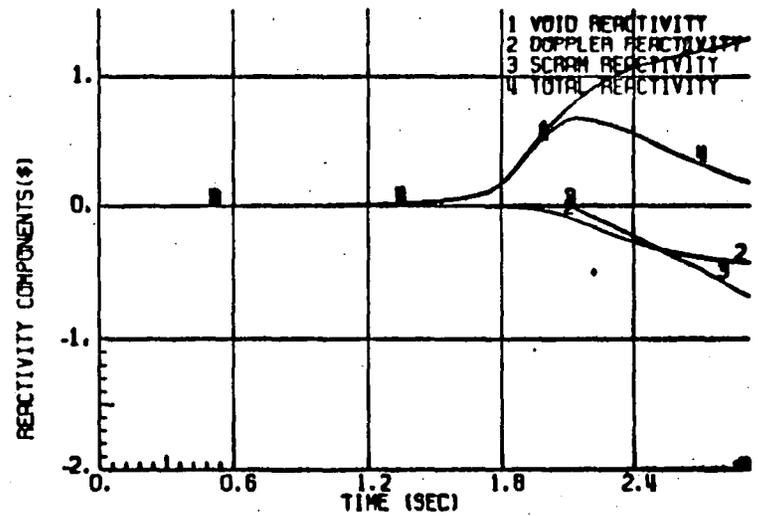
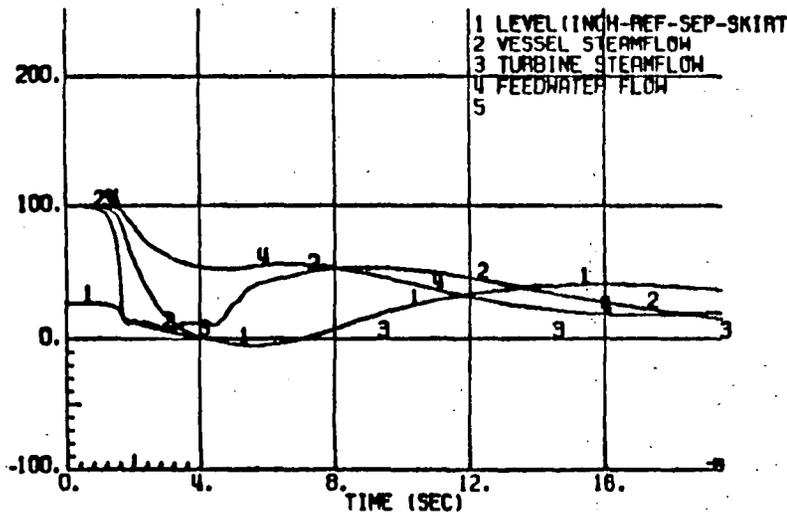
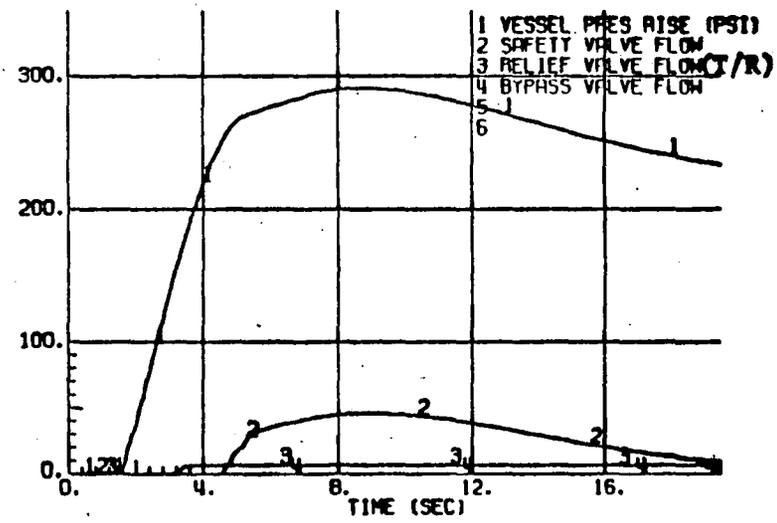
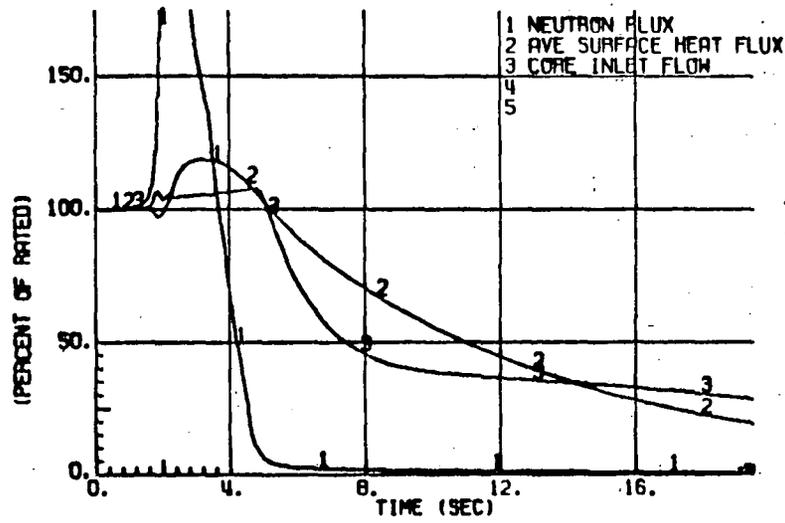


Figure 7. Plant Response to MSIV Closure

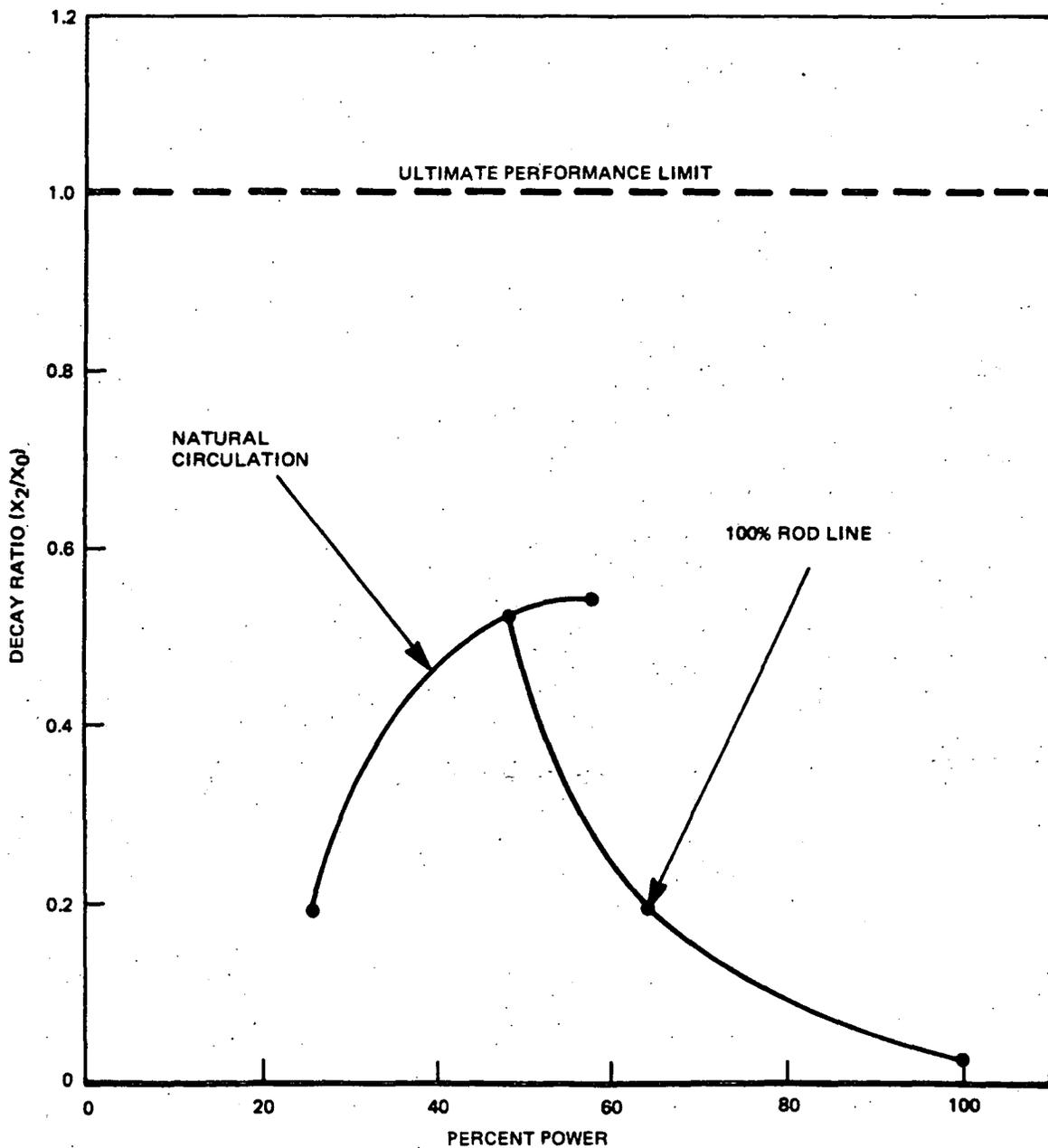


Figure 8. Decay Ratio

APPENDIX A

PLANT PARAMETER CHANGES

Pressure Relief Systems (Table 5-4, pg 5-62, NEDO-24011)

Safety/Relief Valve setpoint (psig)	1115 + 1%
Safety/Relief Valve capacity (% rated steam flow)	5/31.03
Safety Valve Capacity (% rated steam flow)	8/51.56

Transient Operating Parameters (Table 5-6, pg 5-64, NEDO-24011)

Turbine Pressure (psig)	950
-------------------------	-----

GETAB Initial Conditions

Reactor Core Pressure (psia)	1030
------------------------------	------

Stability Analysis

Natural Circulation/Extrapolated Rod Block Decay Ratio	0.54
--	------

Loading Error

Linear Heat Generation Rate (kW/ft):*

Rotated Bundle	16.84
Mislocated Bundle	16.85

*Includes 2.2% penalty due to fuel densification.

APPENDIX B
DENSIFICATION POWER SPIKING

Reference B-1 documents the NRC staff position that ". . . it (is) acceptable to remove the 8x8 and 8x8R spiking penalty factor from the plant Technical Specification for those operating BWR's for which it can be shown that the predicted worst case maximum transient LHGR's, when augmented by the power spike penalty, do not violate the exposure-dependent safety limit LHGR's".

The Dresden 2 Reload 5 submittal contains the required information to demonstrate that the stated criterion is met for Dresden 2 Reload 5, Section 10 (Rod Withdrawal Error) and Appendix A (Linear Heat Generation Rate for Bundle Loading Error) include the densification effect in the calculated LHGR of the 8x8 fuels.

REFERENCE

B-1 "Safety Evaluation of the General Electric Methods for the Consideration of Power Spiking Due to Densification Effects in BWR 8x8 Fuel Design and Performance," Reactor Safety Branch, DOR, May 1978.