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SUBJECT: Forwards responses to items from cont audit on 810819-20.

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THE UNIVERSITY OF CHICAGO
DEPARTMENT OF CHEMISTRY

RESEARCH REPORT
NO. 100

BY
J. H. GOLDSTEIN

PH.D. THESIS
SUBMITTED TO THE FACULTY OF THE DIVISION OF THE PHYSICAL SCIENCES
IN CANDIDACY FOR THE DEGREE OF DOCTOR OF PHILOSOPHY

DEPARTMENT OF CHEMISTRY
UNIVERSITY OF CHICAGO
CHICAGO, ILLINOIS

1955

ABSTRACT
The study of the structure of the nucleus of the atom of the element
is one of the most important problems in modern physics. The
present report is devoted to the study of the structure of the
nucleus of the element of the atomic number Z. The results of
the study are presented in the form of a series of tables and
figures. The tables give the values of the various quantities
which are calculated from the experimental data. The figures
show the dependence of these quantities on the atomic number Z.
The results of the study are compared with the results of
other workers in the field. It is shown that the present
results are in good agreement with the results of other
workers. The present results are also compared with the
theoretical predictions of the various theories of the nucleus.
It is shown that the present results are in good agreement
with the theoretical predictions of the various theories of
the nucleus.



Pennsylvania Power & Light Company

Two North Ninth Street • Allentown, PA 18101 • 215 / 770-5151

Docket Nos. 50-387
50-388

December 29, 1981

Mr. A. Schwencer, Chief
Licensing Branch No. 2
U. S. Nuclear Regulatory Commission
Washington, DC 20555

SUSQUEHANNA STEAM ELECTRIC STATION
NRC SQRT AUDIT OPEN ACTION ITEMS
ER 100450 FILE 148-01
PLA-988



Dear Mr. Schwencer:

Attached are the responses to the following items from the SQRT audit of August 19-20, 1981:

- IV(2) For the valves audited, provide confirmation that the acceleration 'g' values used in the qualification are correspondingly equal to or less than those obtained from the final as-built piping analysis (12/31/81).
- IV(3) For Control Panel (J05 A), provide clarification for the following:
 - (a) Dynamic relationship of the selected (reviewed) panel to the five panels tested and evaluated (12/31/81).
 - (b) Comparison of the maximum stress of the selected panel with the maximum stress of the five tested panels, and the basis for the evaluation (12/31/81).
- IV(4) For Containment Vacuum Relief Valve (M 149) provide clarification for the consideration of the loads at the free end of the downcomer during qualification (12/31/81).

If you have any questions, please contact us.

Very truly yours,

N. W. Curtis
Vice President - Engineering and Construction - Nuclear

Attachment

cc: R. Perch - NRC

*Bool
5/1/1*

8201040083 811229
PDR ADDOCK 05000387
A PDR



Faint, mostly illegible text in the upper right quadrant of the page, possibly representing a header or a list of items.

Several paragraphs of very faint, illegible text are scattered across the middle and lower middle sections of the page. The text is too light to transcribe accurately.

E317 010154557

RESPONSE TO NRC QUESTION ITEM #IV (2)Question:

For the valves audited, provide confirmation that the acceleration 'g' values used in the qualification are correspondingly equal to or less than those obtained from the final as-built piping analysis (12/31/81).

Response:

The valves audited were:

- (1) P-12BC - Motor Operated

Qty = 4 F073A, B; F075A, B

- (2) P-14BC - Motor Operated

Qty = 1 HV-12603

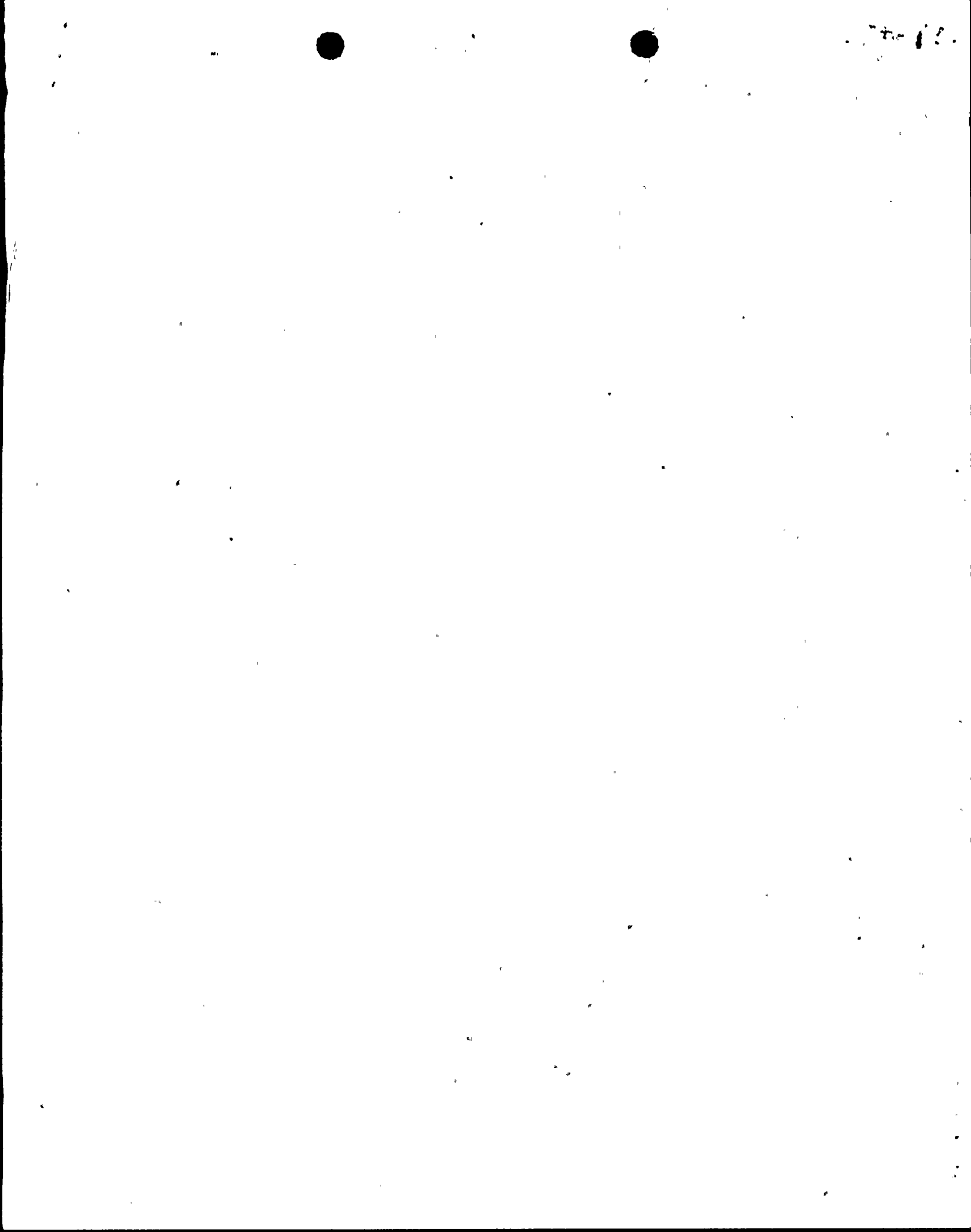
- (3) J-69 - Solenoid Valves

Qty = 4 F025, F026, F028m F029

- (4) M-159 - Relief Valves

Qty = 2 PSV-12643, PSV-12648

The following sheets 2 through 4 summarizes the desired confirmation in a tabular form.



ATTACHMENT - 1

SHT. 2 of 5

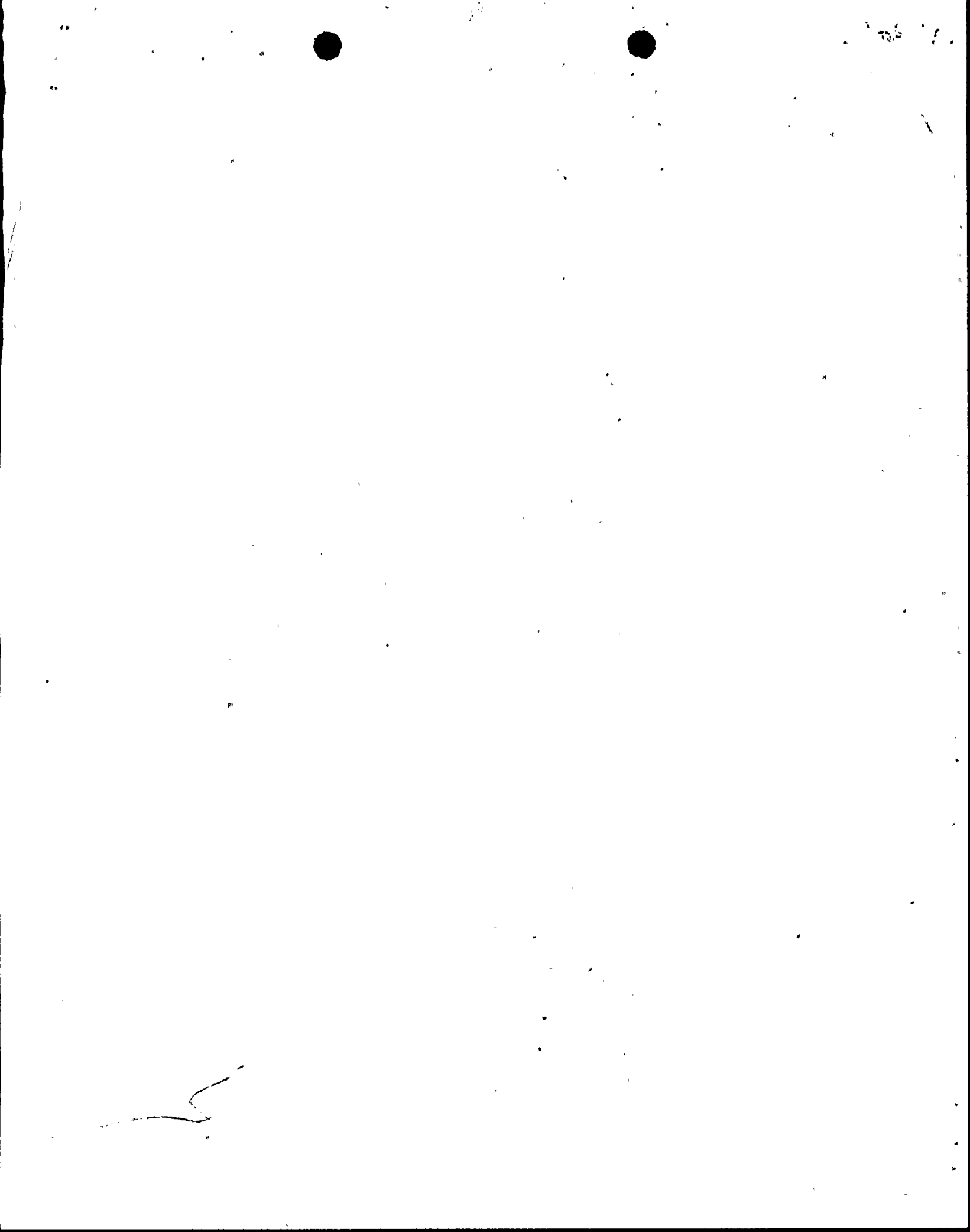
SUMMARY OF VALVE ACCELERATION

CALCULATION NUMBER : 887-1 Rev.1

DATA POINT	VALVE NUMBER	VALVE SIZE	VALVE DWG. NUMBER	SK-M NUMBER	LINE DESCRIPTION	MAX. VALUE ACCELERATION [#]	
						ACTUAL (g)	ALLOW. (g)
17	HV-1F0730	6"	8856-PI2AC-39-5	887/5	20" ARC-113	1.694	3.0
127	HV-1F0730	6"	8856-PI2AC-39-5	↓	6" ARC-113	2.937	5.07
147	HV-1F075B	6"	8856-PI2BC-47		6" GBB-119	3.181	7.33

* MAXIMUM IN ANY DIRECTION

ORIGINATOR: SMARTE, JUD DATE: 6-2-81 CALC. NO. 8856
PROJECT: SUSQUEHANNA UNIT - 1 CHECKED: SMR DATE: 6-5-81
SUBJECT: SUMMARY OF VALVE ACCELERATION SHEET NO. 5 of 30 Attachment # 1 Sht. 2 of 5



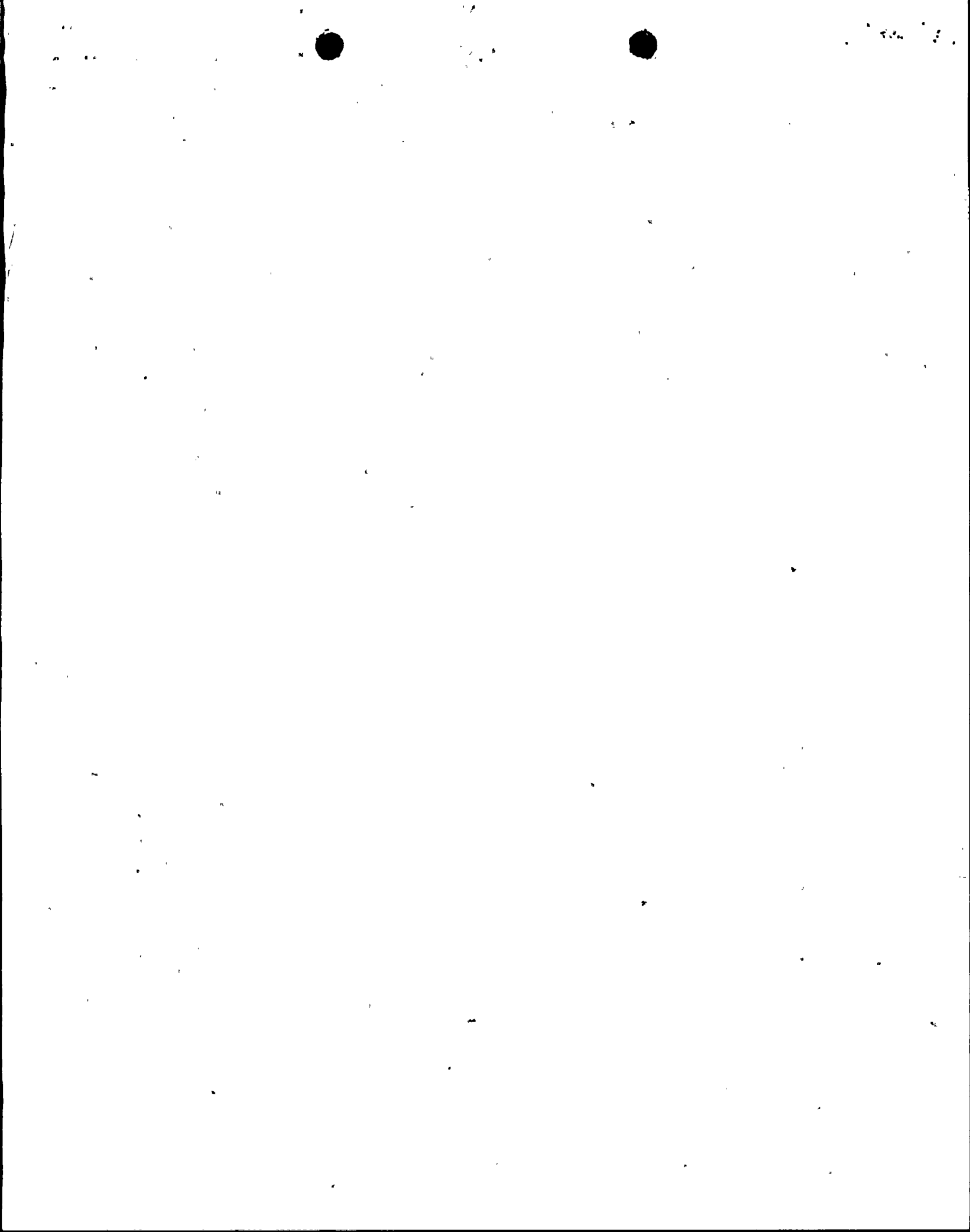
SUMMARY OF VALVE ACCELERATION

CALCULATION NUMBER : 893-1 Rev.1

DATA POINT	VALVE NUMBER	VALVE SIZE	VALVE DWG. NUMBER	SK-M NUMBER Rev No.	LINE DESCRIPTION	MAX. VALVE ACCELERATION		
						ACTUAL (g)	ALLOW. (g)	
117	HV-11210A	8"	8896-PI6-AC-8(r)-12	893/N	20" HRC-112	1.565	3.0	
127	HV-1F073A	6"	8896-PI2-BC-59-6	893/N	6" HRC-113	3.057	5.07	
147	HV-1F079A	6"	8896-PI2-BC-47-4	893/N	6" GBB-119	2.896	7.33	
	* MAXIMUM IN ANY DIRECTION							

Attachment # 1 Sheet 3 of 5

PROJECT SUSQUEHANNA UNIT - 1
 SUBJECT SUMMARY OF VALVE ACCELERATION SHEET NO. 4/34
 ORIGINATOR JE JUCON DATE 5-21-81 CHECKED 8856 REV. NO. 1
 CALC. N. 893-1 SHEET DATE 5-27-81



SUMMARY OF VALVE ACCELERATION

VALVE QUALIFICATION ACCELERATIONS (SQRT VALVES)

P& ID	VALVE NUMBER	VALVE SIZE	VALVE VENDOR I.D.	SK-M NUMBER	LINE DESCRIPTION	MAX. VALVE ACCELERATION	
						ACTUAL (g)	ALLOW. (g)
126	HV-12603	2"	P14 BC (MOTOR OPER.)	6071	HCB-129	X: 3.981 Y: 2.905 Z: 5.6	8
149	HV-E51-1F025	1"	J69 (SOLENOID)	5543	DBB-109	X: 4.853 Y: 4.919 Z: 1.404	6
149	HV-E51-1F026	1"	J69 "	5543	DBB-109	X: 4.853 Y: 4.919 Z: 1.404	6
155	HV-E41-1F028	1"	J69 "	5540	DBB-114	X: 4.853 Y: 4.919 Z: 1.404	6
155	HV-E41-1F029	1"	J69 "	5540	DBB-114	X: 4.853 Y: 4.919 Z: 1.404	6
126	PSV-12643	1"	M159 (SRV)	5471	HCC-140	X: 4.853 Y: 4.919 Z: 1.404	52
126	PSV-12648	1"	M159 (")	5428	HCC-139	X: 4.853 Y: 4.919 Z: 1.404	52

Attachment #1
Sheet 4 of 5

* PER SQRT DOCUMENTATION
** SEE ATTACHED GRAPH



CALCULATION SHEET

CALC. NO. _____

REV. NO. _____

ORIGINATOR: SHAIL CHORHAVASTIA DATE: 12/11/81

CHECKED: _____

DATE: _____

PROJECT: SUSQUEHANNA UNIT - 1

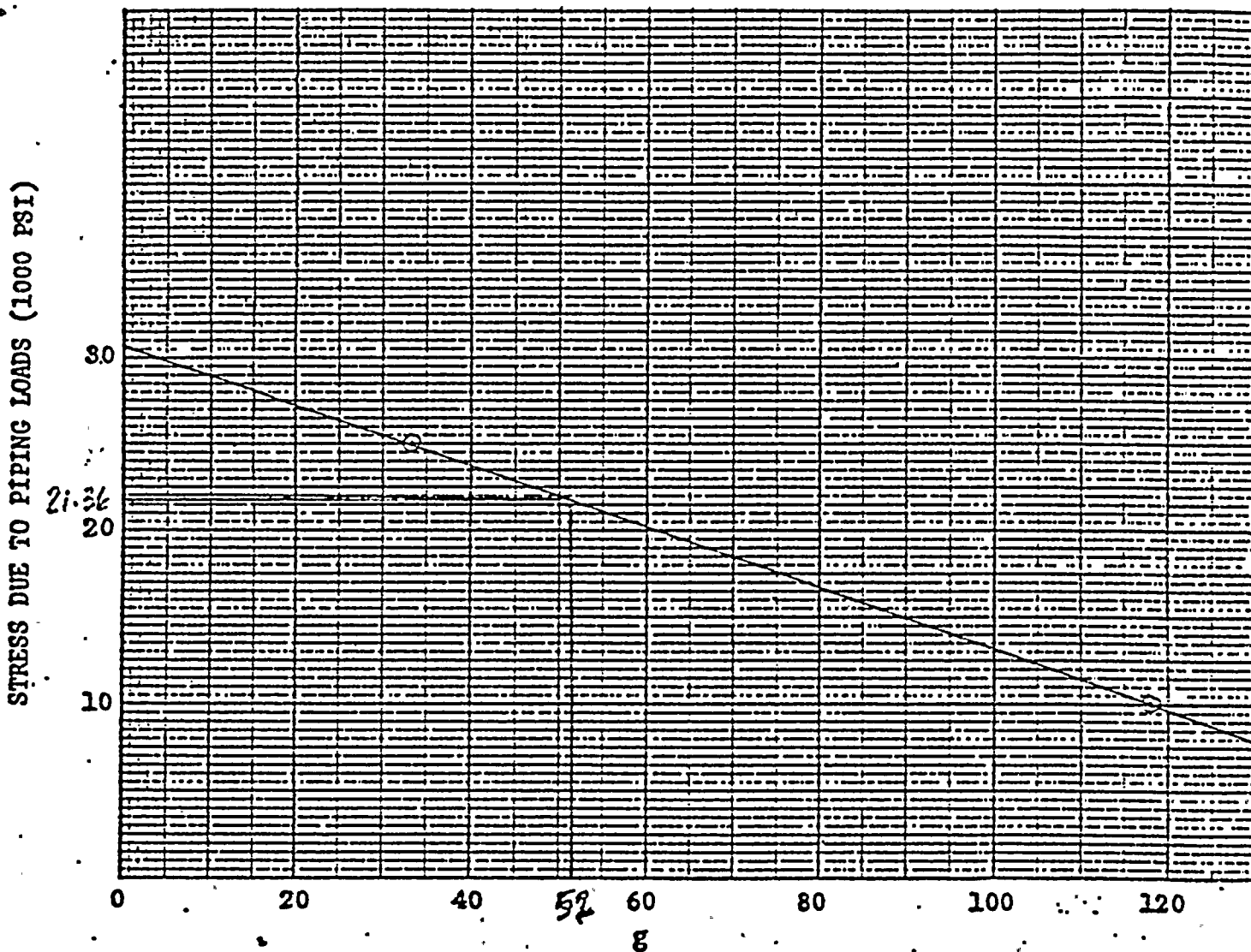
JOB NO. 8856

SUBJECT: SUMMARY OF VALVE ACCELERATION SHEET NO. _____



MANUFACTURERS OF SAFETY-RELIEF VALVES

SEISMIC CALCULATIONS



$Z = 2.75 \text{ IN}$

$S = .133 \text{ IN}^3$

PSV-12643
 PSV-12648

1X1

RESPONSE TO NRC QUESTION ITEM #IV (3)Question:

For Control Panel (J-05A), provide clarification for the following:

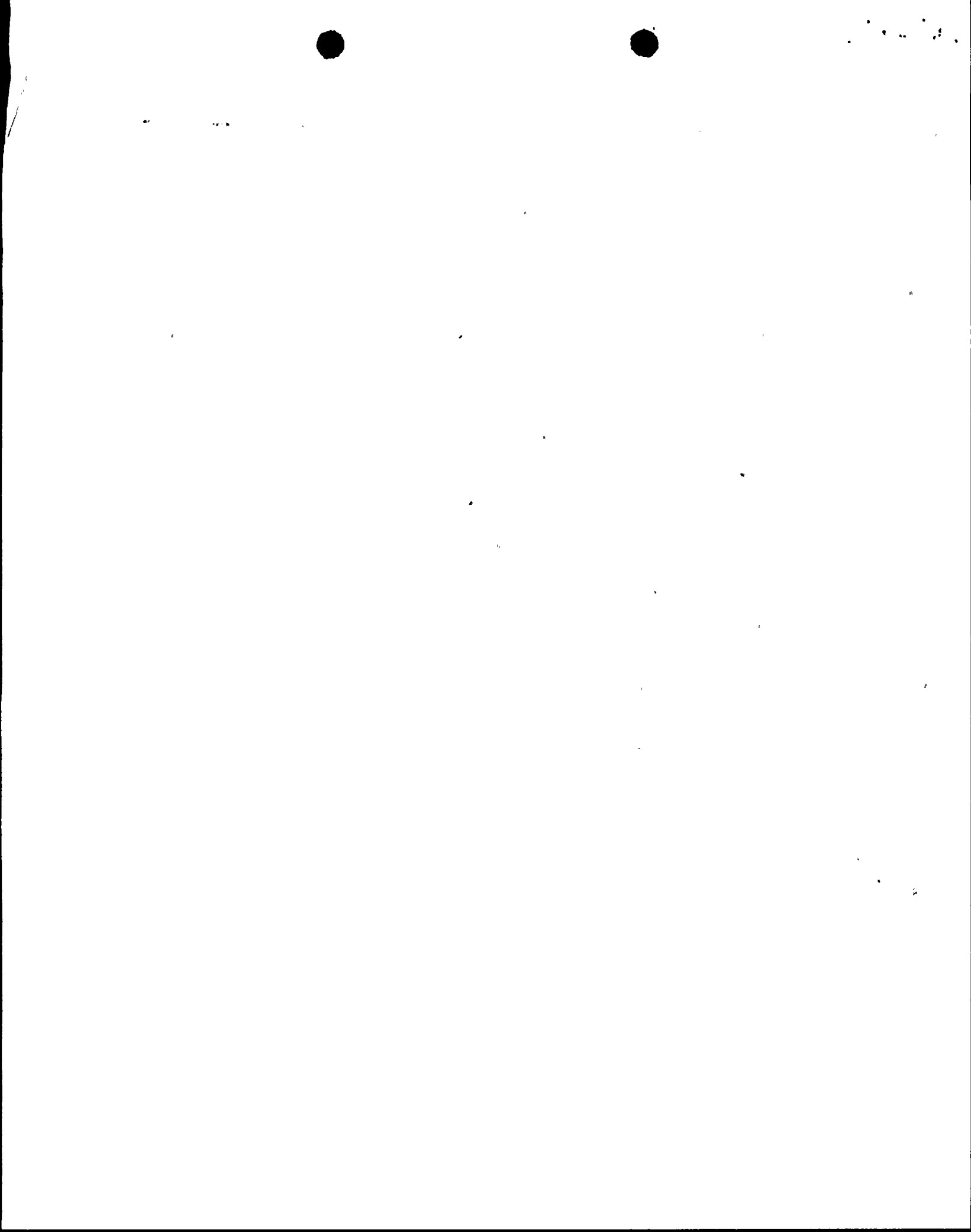
- (a) Dynamic relationship of the selected (reviewed) panel to the five panels tested and evaluated (12/31/81).
- (b) Comparison of the maximum stress of the selected panel with the maximum stress of the five tested panels, and the basis for the evaluation (12/31/81).

Response:

- (3a) Five panels were selected to get the best representation of the population of 49 panels.
- (1) To include the various elevation and the corresponding floor response spectra.
 - (2) To include the various sizes and the weights to get the highest weight per linear ft. to yield the highest response.
 - (3) To include the characteristics due to the mounting conditions at the base such as concrete floor support or the steel base mounting.
 - (4) To include the characteristics of the local mounting panels.

Analysis of these panels identified the necessity to do the following fixes to assure that the structural characteristics of the panels produce acceptable responses in terms of (a) structural integrity of the panels and (b) the response spectra for component qualifications.

1. Stiffen mounting panels.
2. Stiffen panel where instrument is directly mounted on the skin.
3. Stiffen center plate free edge.
4. Stiffen base channel.
5. Inspect and tighten anchor bolts and add anchor bolts as needed.



All the panels were inspected and field work for the above modifications is presently underway. These modifications will assure that the structural characteristics of all the panels be such that the responses are within that of the panels that have been analyzed.

(3b) Subsequent to the completion of engineering effort to extrapolate the results of analysis for five selected panels to the remainder 44 panels of P.O. J-05A, J-05B and M-334, two additional panels, namely 1C681 and 0C876A were selected and analyzed. This was done to:

- Verify the stresses and structural integrity of the panels actually not analyzed during initial (April, 1981) analysis. Panel 1C681 was specifically selected by the NRC audit team, for this purpose.
- Verify the representation achieved by the five panels selected initially.
- Verify the adequacy of the fixes.

A review of the results of this additional analysis (see sheet #3 for panel 1C681 and Sheet #4 for panel 0C876A) indicates that, as expected, the stresses in these panels are well below allowables. For ready reference the stresses in the initial five panels are given on sheet #5 through #9. The earlier conclusion that the panel qualification is satisfactory is hereby reaffirmed.

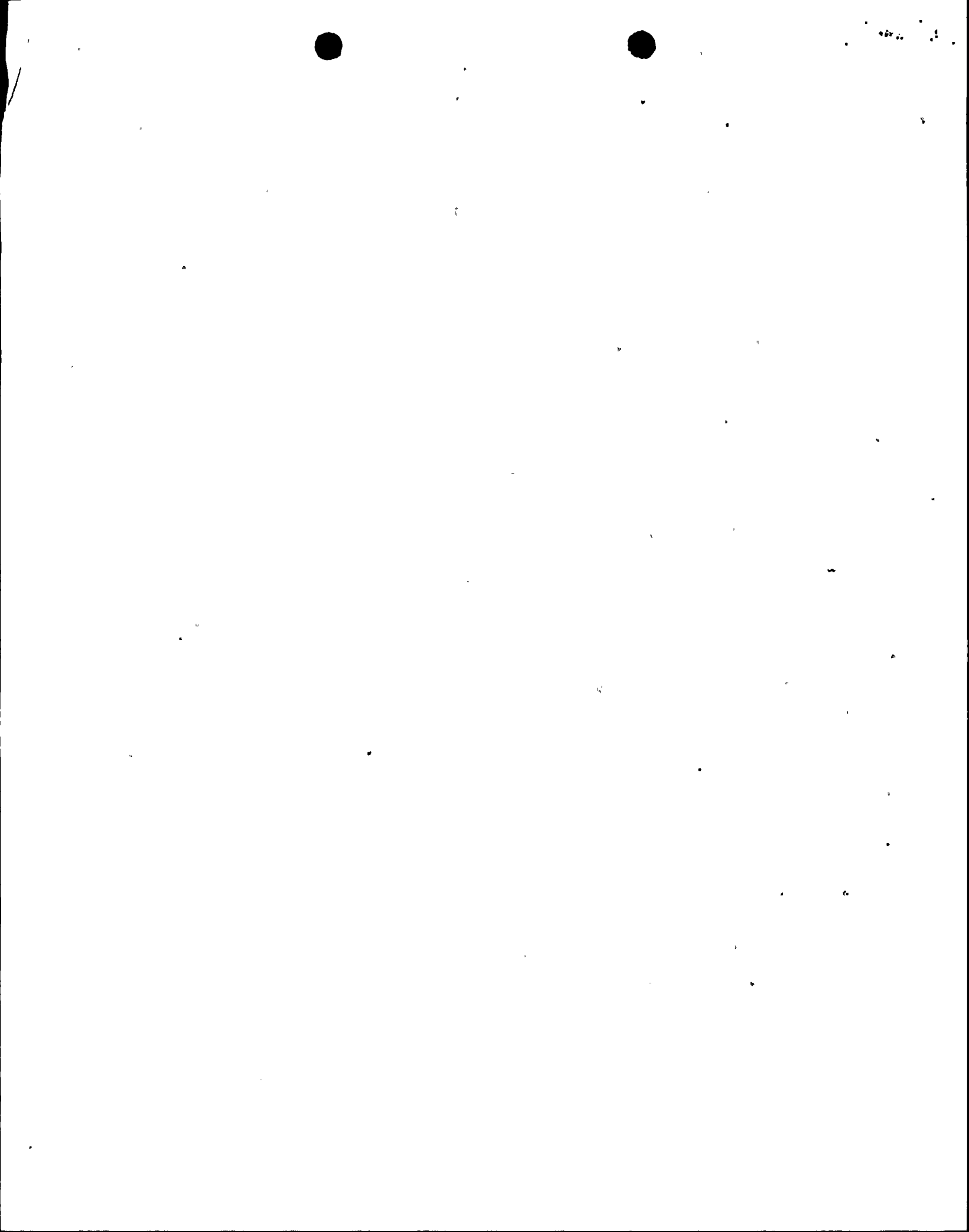
From: Bechtel v.p # 8856-J8-11-1
TABLE 9

SUMMARY OF MAXIMUM STRESSES IN PANEL 1C681

MAXIMUM DISPLACEMENT: .008 INCHES
 MAXIMUM ACCELERATION: 1.84g (HORIZONTAL)
 0.97g (VERTICAL)

154557

MAXIMUM STRESSES					
PANEL COMPONENT	STRESS TYPE	MAXIMUM VALUE	ALLOWABLE VALUE	MAXIMUM ALLOWABLE	
(a) <u>MOUNTING PLATES</u>	SHEAR	135	14400	.009	
	FLEXURE	150	27000	.006	
(b) <u>CABINET</u>	SIDES	SHEAR	112	13200	.008
		FLEXURE	156	14400	.01
	FRONT	SHEAR	331	27000	.01
(c) <u>WELDS</u>	SHEAR	1322	18000	.07	
(d) <u>ANCHOR BOLTS</u>	COMBINED SHEAR + TENSION	1476	1600	.92	
(e) <u>BRACINGS</u>	COMPRESSION	19	6480	.003	



From Bechtel V.P. 8856-J8-11-1

TABLE 10

SUMMARY OF MAXIMUM STRESSES IN PANEL OC876A

MAXIMUM DISPLACEMENT: .006 INCHES

MAXIMUM ACCELERATION: 0.91g (HORIZONTAL)
0.74g (VERTICAL)

MAXIMUM STRESSES					
PANEL COMPONENT	STRESS TYPE	MAXIMUM VALUE	ALLOWABLE VALUE	MAXIMUM ALLOWABLE	
(a) <u>MOUNTING PLATES</u>	SHEAR	38	14400	.003	
	FLEXURE	364	27000	.01	
(b) - <u>CABINET</u>	SIDES	75	13200	.006	
	DOOR JAMBS	SHEAR	58	13200	.004
		FLEXURE	1407	19800	.07
	ANGLE (H FRAME)	SHEAR	46	14400	.003
FLEXURE		1414	21600	.07	
(c) <u>WELDS</u>	SHEAR	802	18000	.04	
(d) <u>ANCHOR BOLTS</u>	COMBINED SHEAR + TENSION	648	16000	.41	
(e) <u>BRACINGS</u>	COMPRESSION	21	19900	.001	

MAXIMUM DISPLACEMENT: .073 INCHES

MAXIMUM ACCELERATION: 1.065g (VERTICAL)

0.837g (HORIZONTAL)

MAXIMUM STRESSES:				
PANEL COMPONENT	STRESS TYPE	MAXIMUM VALUE	ALLOWABLE VALUE	MAXIMUM ALLOWABLE
(a) <u>MOUNTING PLATES</u>	SHEAR	322	14400	.02
	FLEXURE	916	27000	.04
(b) <u>CABINET</u>	TOP	SHEAR 24	13200	.002
	SIDES	SHEAR 29	13200	.002
	DOOR JAMBS	SHEAR 99	13200	.008
		FLEXURE 4182	19800	.21
	HATCH JAMBS	SHEAR 223	13200	.02
		FLEXURE 488	19800	.03
	BOTTOM CHANNELS	SHEAR 13	14400	.001
		FLEXURE 263	21600	.012
ANGLE BRACKETS	SHEAR 157	14400	.01	
	FLEXURE 2739	21600	.13	
(c) <u>WELDS</u>	SHEAR	2732	18000	.15
		(WELD OF MOUNTING)		
(d) <u>ANCHOR BOLTS</u>	COMBINED SHEAR + TENSION	445	1200	0.37

TABLE 4.1 SUMMARY OF MAXIMUM STRESSES
IN PANEL OC883B

From Bechtel V.P. #8856-J8-4-2

MAXIMUM DISPLACEMENT: .057 inches

MAXIMUM ACCELERATION: 1.868g (horiz)

0.406g (vert)

MAXIMUM STRESSES:					
PANEL COMPONENT	STRESS TYPE	MAXIMUM VALUE	ALLOWABLE VALUE	MAXIMUM ALLOWABLE	
(a) Mounting Plates	Shear	510	13200	.04	
	Flexure	566	19800	.03	
(b) Cabinet	Sides Shear	143	13200	.011	
	Top Shear	1511	13200	.114	
	Corner Beams	Shear	194	13200	.015
		Flexure	3856	19800	.195
	Angle on Plate	Shear	53	14400	.004
		Flexure	2056	21600	.095
(c) Welds	Shear	6471 (side plates)	18000	.36	
(d) Anchor Bolts	Combined shear & Tension	917	2660	0.345	

TABLE 5.1 SUMMARY OF MAXIMUM STRESSES IN PANEL 2C661A2

From Bechtel V.P. #8856-J8-5-3
 MAXIMUM DISPLACEMENT: .060 inches

ATTACHMENT -2
 Sht 7 of 9

MAXIMUM ACCELERATION: 1.450 g (horz.)
 0.482 g (vert.)

MAXIMUM STRESSES					
PANEL COMPONENT	STRESS TYPE	MAXIMUM VALUE	ALLOWABLE VALUE	MAXIMUM ALLOWABLE	
(a) Mounting Plates	Shear	104	14400	0.007	
	Flexure	2011	27000	0.075	
(b) Cabinet	Top	Shear 90	13200	.007	
	Sides	Shear 186	13200	.014	
	Door Jamb	Shear	126	13200	.010
		Flexure	7707	19800	.389
	Stiffeners	Shear	154	13200	.012
		Flexure	42	19800	.002
	Separator Wall	Shear	140	13200	.011
(c) Welds	Shear	1131 (side plates)	18000	.063	
(d) Anchorage weld	Combined Shear & Tension	796 psi.	18000	0.044	

TABLE 4.1 SUMMARY OF MAXIMUM STRESSES IN PANEL 2C694

From Bechtel P #8856-J8-6-3

MAXIMUM DISPLACEMENT: .0116 inches

MAXIMUM ACCELERATION: 1.330g (horiz)
0.641 (vert)

MAXIMUM STRESSES: *

PANEL COMPONENT	STRESS TYPE	MAXIMUM VALUE	ALLOWABLE VALUE	MAXIMUM ALLOWANCE	
(a) Mounting Plates	Shear	240	14400	.017	
	Flexure	730	27000	.027	
(b) Cabinet	Sides Shear	35	13200	.003	
	Top Shear	23	13200	.002	
	Door Mullions	Shear	166	13200	.013
		Flexure	4478	19800	.226
	Tee Stiffeners	Shear	95	14400	.007
		Flexure	2624	21600	.122
	Channel Stiffeners	Shear	49	14400	.003
		Flexure	922	21600	.043
	Plate Stiffeners	Shear	84	14400	.006
		Flexure	1880	21600	.087
(c) Welds	Shear	2036 (mountings)	18000	.113	
(d) Anchor Bolts	Combined shear & tension	250	1200	0.21	

TABLE 5.1 Summary of Maximum Stresses in Panel 2C201B

* The stresses include the effects of LOCA loads. In fact this panel is not required to sustain LOCA loads.



From Bechtel VP # 8856-J8-7-3

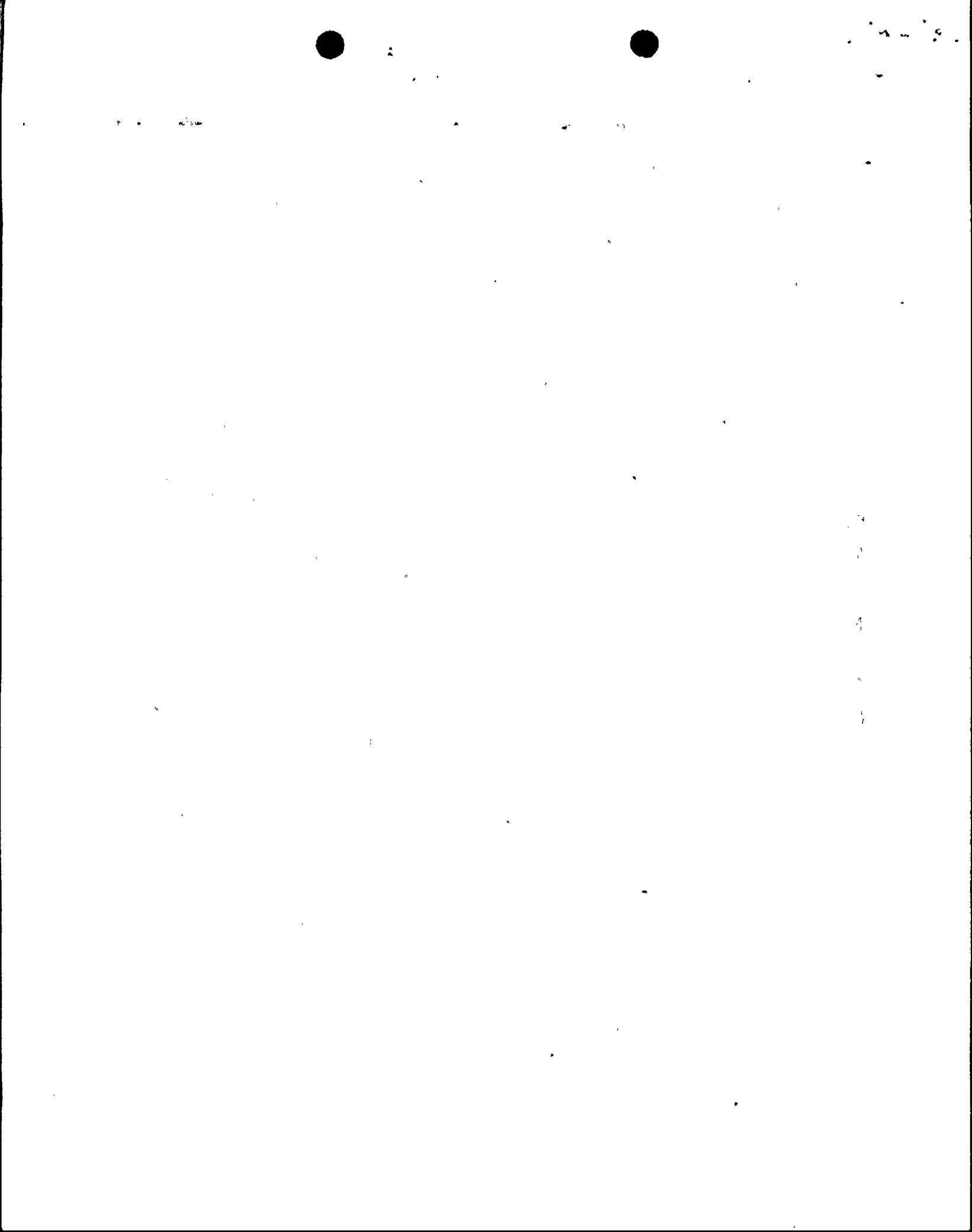
MAXIMUM DISPLACEMENT: .0044 inches

MAXIMUM ACCELERATION: .756g (vert)

.694g (horz)

MAXIMUM STRESSES:					
PANEL COMPONENT	STRESS TYPE	MAXIMUM VALUE lbs	ALLOWABLE VALUE lbs	MAXIMUM ALLOWABLE	
(a) Mounting Plates	Shear	513	13200	.039	
	Flexure	266	22000	.012	
(b) Cabinet Sides	Shear	77	13200	.006	
	Top Angles	Shear	220	14400	.015
		Flexure	5125	21600	.237
	Side Beams	Shear	124	13200	.009
		Flexure	10006	19800	.505
	Inner Stiffeners	Shear	117	13200	.009
		Flexure	481	19800	.024
	Added Angle Stiffeners	Shear	50	14400	.003
Flexure		676	21600	.031	
(c) Welds	Shear	2760 (mounting plate)	18000	.153	
(d) Anchor Bolts	Combined Shear & Tension	636 lbs.	1200	0.53	

TABLE 5.1 SUMMARY OF STRESS ANALYSIS IN PANEL 2C222



RESPONSE TO NRC QUESTION ITEM #IV (4)Question:

For Containment Vacuum Relief Valve (M-149) provide clarification for the consideration of the loads at the free end of the downcomer during qualification (12/31/81).

Response:

There are five pairs of vacuum relief valves in each unit. The valves are in series and bolted to T-flanges of the downcomer at one end and supported by a pair of diagonal bracing angles (4" x 4" x 3/8") on the outboard end. The model for the analysis of the valves includes the details of the valve components, the downcomer, the downcomer bracing system and the bracing angles as shown in the attached Figure 1.

In addition to the dead load and the pressure load (vacuum operating set pressure of 0.5 psi; positive design pressure of 53 psi), the following dynamic loads have been considered in qualifying the valve:

(1) Inertia Loads:

From seismic, SRV and LOCA applied at the diaphragm slab.

(2) Submerged Structure Loads:

(a) SRV: Pressure time history from KWU trace #76 applied laterally.

(b) LOCA: Pressure time history from KWU traces #303 and #306 applied laterally.

(3) Downcomer Tip Load due to LOCA (chugging):

The present configuration is such that the downcomer carrying the vacuum relief valves are capped at bottom ends. Hence, the direct tip load due to chugging is eliminated for these vents. However, the effect of the tip loads from the adjacent downcomers as transmitted through the bracing has been considered for a multiple vent discharge. This load consists of a 30 kip impulse applied as a half sine wave with a duration of 3 milliseconds. A multiple vent discharge factor of 0.25 is taken into account.

The total loads stresses and displacements are determined in the following manner:

- (i) the responses for the SRV inertia load and the SRV submerged structure load are added absolutely.
- (ii) the responses for LOCA inertia load, LOCA submerged structure load and the chugging tip load are added absolutely.
- (iii) the responses from the above (i & ii) SRV and LOCA and the responses from seismic loads are added by SRSS method.
- (iv) the total dynamic responses from (iii) are then added to the results of dead load and the pressure loads are added absolutely to obtain the final stresses and displacements.

The analysis of the valve show that there are adequate margins of safety in all the valve components and hence, it is concluded that the valve is satisfactorily qualified for hydrodynamic loads.

1010154557

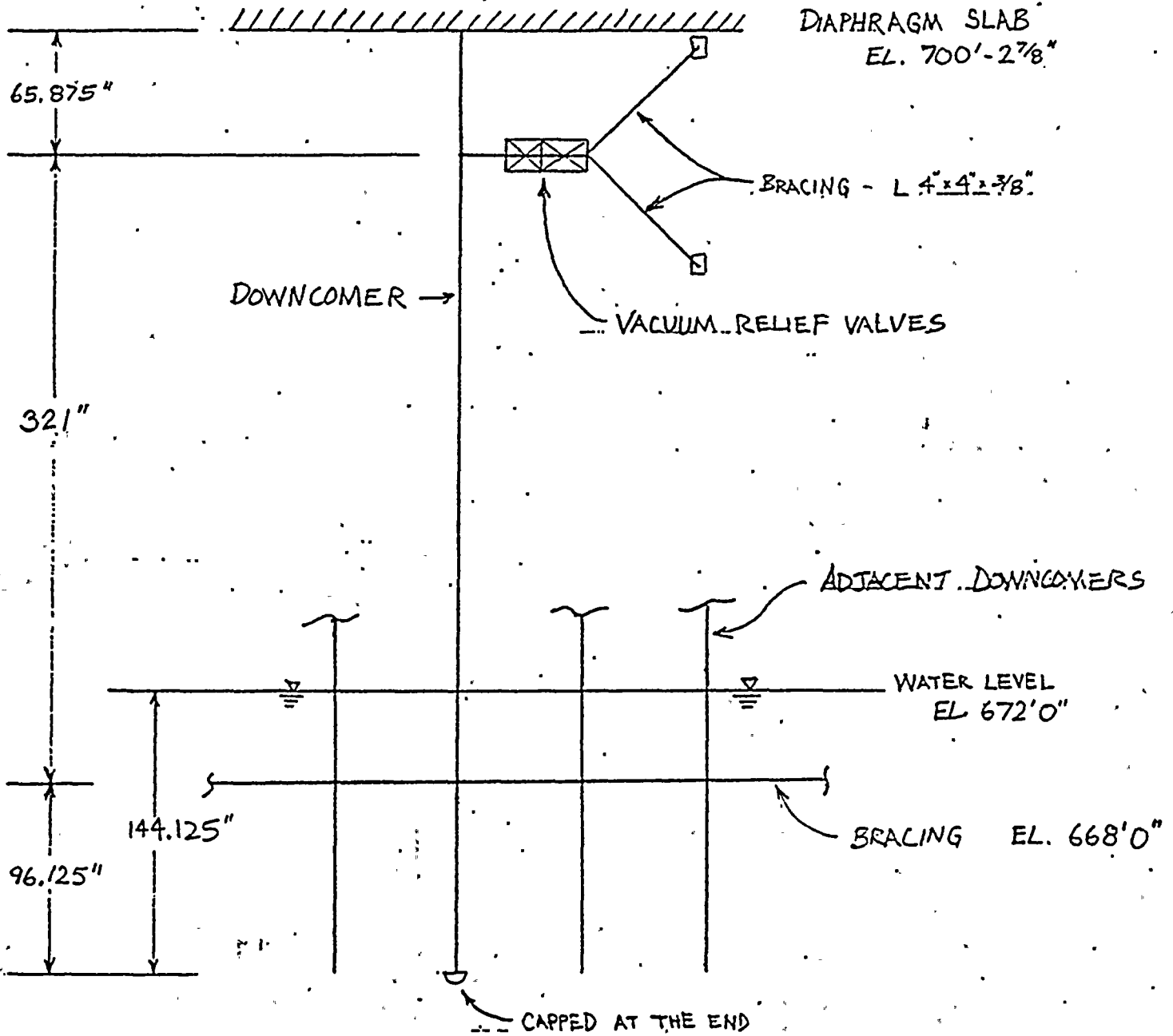


Figure - 1 : SCHEMATIC MODEL OF
DOWNCOMER WITH VACUUM
RELIEF VALVES

