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April 12, 1978

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 SERVICES UNIT

Mr. George E. Lear, Chief  
 Operating Reactors - Branch 3  
 Division of Operating Reactors  
 U.S. Nuclear Regulatory Commission  
 Washington, DC 20555

Subject: Dresden Station Units 2 and 3  
 Quad-Cities Station Units 1 and 2  
 Suppression Pool Temperature Transients  
NRC Docket Nos. 50-237/249 and 50-254/265

References (a): D. K. Davis letter to R. L. Bolger dated  
 December 12, 1977

(b): C. Reed letter to D. K. Davis dated  
 January 3, 1978

Dear Mr. Lear:

**REGULATORY DOCKET FILE COPY**

Commonwealth Edison has reviewed reference (a) and the Dresden Station and Quad-Cities Station Technical Specifications with General Electric in order to provide a technically justified basis upon which suppression pool temperature transient analyses could be performed. This review has generated proposed analysis cases with the initial conditions, event descriptions and assumptions defined. These proposed transient bases are being submitted to fulfill our commitment transmitted by Reference (b).

It is Commonwealth Edison's position that a commitment for the performance of the transient analyses is not currently justified. Although it is recognized that the available test data on suppression pool instability is limited, it is judged that sufficient experience exists in operating facilities to justify continued operation without the need for very costly analysis. This position is justified in the case of the Dresden and Quad-Cities units because of the particular plant unique parameters which contribute to the mitigation of the pool heating transients, e.g., large pool water volume and large pool cooling capacity.

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*Pool  
 5/1/60  
 APO  
 LEAR & TEWL  
 LOR  
 MOUINE*

Mr. George E. Lear:

- 2 -

April 12, 1978

Please address any additional questions on this matter to this office.

One (1) signed original and fifty-nine (59) copies of this letter are provided for your use.

Very truly yours,



Cordell Reed  
Assistant Vice-President

attachment

Suppression Pool Temperature Transient Bases  
Dresden Units 2 and 3  
Quad Cities Units 1 and 2

Attached are the initial conditions, event sequences, and assumptions that Commonwealth Edison proposes to use to analyze the transients which affect suppression pool temperature. It should be noted that the information provided is based upon the currently defined Technical Specifications for the subject units. It should also be noted that of the four events discussed, Event 2 (Stuck-open relief valve from isolated hot-standby) and Event 4 (Isolation and reactor depressurization) are judged to be trivial because they are non-limiting and would not challenge the bulk suppression pool temperature limit.

EVENT 1\* - STUCK-OPEN RELIEF VALVE FROM POWER OPERATION

Initial Conditions

1. Operation at Technical Specification safety analysis steam flow conditions. (QC = 105% rated).
2. Maximum RHR heat exchange service water temperature. (QC = 95°F).
3. Suppression pool temperature at normal power operation Technical Specification limit ( $T_{Op}$ ). (QC = 95°F).
4. Minimum Tech Spec suppression pool water volume. (QC = 112,200 cu. ft.)
5. Drywell air pressure at 1.1 psig or maximum of normal operating band.
6. Drywell air temperature at 135°F. or minimum of normal operating band.
7. Wetwell air pressure at -0.4 psig or maximum of normal operating band.
8. Recirculation pumps operating.

Event Sequence

<u>Time</u>	<u>Temp</u>	<u>Event Description</u>
# $t_a = 0.0$	$T_{Op}$	SRV fails open**. Pool temperature alarm at initial Condition 3. Initiate actions to turn RHR loops* on for pool cooling.
$t_a + 3$ minutes**		RHR loops* on for pool cooling.
$t_s$	$T_s$	Reactor Scram*** ( $T_s = 110^\circ\text{F.}$ for QC).
$t_s + 10.5$ seconds		Isolation (assuming mechanistic isolation on Lo-Lo level).
$t_s + 15$ minutes##		2-3 additional RV manually actuated as necessary.
### $t_b$	$T_b$	Drywell high pressure trip (QC = 2 psig). RHR automatically switched out of pool cooling mode.
$t_b + 30$ minutes		Operator vents drywell to Standby Gas Treatment System.

\* Corresponds to nonproprietary Question 1(a), two RHR loops available.

\*\* The operator can complete the actions necessary to turn the RHR loops on within three minutes.

\*\*\* Mode switch in Shutdown.

- \*\* Quad Cities has one Target Rock combination safety/relief valve (SRV), and 4 Electromatic relief valves. The Target Rock SRV, which has a higher capacity than an Electromatic RV, is assumed to be the relief valve which fails open.
- # The bulk suppression pool temperature is assumed to be 95°F rather than 120°F when SRV inadvertently fails open. Also, Section 3.7.A.1 in the QC tech specs specifies that the reactor shall be scrammed from any operating condition when the suppression pool temperature reaches 110°F.
- ## The operator can determine which valve is stuck open within ten minutes.
- ### Above operator action can prevent the drywell pressure from reaching 2 psig by using the torus spray.

Assumptions for Event 1

1. Maximum operating condensate storage water temperature.
2. Normal automatic operation of HPCI, RCIC - but manually controlled thereafter.
3. Both RHR loops available for pool cooling.
4. Vessel liquid mass adjusted to account for subcooled liquid in the RPV and piping.
5. Metal mass adjusted to account for lower temperature of some metal components.
6. Effect of steam void collapse included.
7. Trip volumes for makeup systems adjusted to account for relative elevations in the RPV.
8. RCIC and HPCI allowed to operate to 100 psia.
9. Duty of RHR heat exchangers based on 40 years of crud.
10. CRD flow maintained constant.
11. SRV capacities at 122.5% of ASME rated.
12. Licensed decay heat curve for containment analysis (adjusted to account for delay between scram and isolation).
13. On plants with motor-driven feedwater pumps (QC), the feedwater pumps operate continuously.
14. Event terminates in cold shutdown.

EVENT 2\* - STUCK-OPEN RELIEF VALVE FROM ISOLATED HOT STANDBY

Initial Conditions

1. Operation at Technical Specification safety analysis limit steam flow conditions before isolation. (QC = 105% rated).
2. Maximum RHR heat exchanger service water temperature. (QC = 95°F).
3. Suppression pool temperature at normal power operation Technical Specification limit ( $T_{op}$ ). (QC = 95°F).
4. Minimum Technical Specification suppression pool water volume. (QC = 112,200 cu. ft.).
5. Drywell air pressure at 1.1 psig or maximum of normal operating band.
6. Drywell air temperature at 135°F. or minimum of normal operating band.
7. Wetwell air pressure at -0.4 psig or maximum of normal operating band.
8. Recirculation pumps operating.
9. Reactor pressure when isolated is 920 psig.

Event Sequence

Time (Min.)	<u>Event Description</u>
$t_a = t_s = 0.0$	Pool temperature alarm reactor scram and isolation - Initial Condition 3. Initiate actions to turn RHR loop on for pool cooling.
$t_a + 3 \text{ minutes}^{**}$	RHR loop on for pool cooling.
$0 < t < 30$	Reactor pressure maintained using SRV.
$t_o$	Single SRV sticks open at 120°F.
$t_o + 10 \text{ minutes}^{***}$	2-3 additional SRV opened (by operator).
$\#t_b$	Drywell high pressure switch (QC = 2 psig). RHR automatically switched out of pool cooling mode.
$t_b + 30$	Operator vents drywell to Standby Gas Treatment System.

The number of SRV's to be manually actuated by the operator to be determined by the analysis.

\* Corresponds to nonproprietary Question 1(c). This event does not conform to the plant licensing basis because it requires a transient plus a single failure. Therefore, this event should not be analyzed.

- \*\* The operator can complete the actions necessary to turn the RHR loops on within three minutes.
- \*\*\* The operator can determine which valve is stuck open within ten minutes.
- # Above operator action can prevent the drywell pressure from reaching 2 psig by using the torus spray.

Assumptions for Event 2

1. Maximum operating condensate storage water temperature.
2. Normal automatic operation of HPCI, RCIC - but manually controlled thereafter.
3. Both RHR loops available for pool cooling.
4. Vessel liquid mass adjusted to account for subcooled liquid in the RPV and piping.
5. Metal mass adjusted to account for lower temperature of some metal components.
6. Effect of steam void collapse included.
7. Trip volumes for makeup systems adjusted to account for relative elevations in the RPV.
8. RCIC and HPCI allowed to operate to 100 psia.
9. Duty of RHR heat exchangers based on 40 years of crud.
10. CRD flow maintained constant.
11. SRV capacities at 122.5% of ASME rated.
12. Licensed decay heat curve for containment analysis (adjusted to account for delay between scram and isolation).
13. On plants with motor-driven feedwater pumps (QC), the feedwater pumps operate continuously.
14. Event terminates in cold shutdown.

EVENT 3\* - SMALL BREAK ACCIDENT WITH ADS

Initial Conditions

1. Operation at Technical Specification safety analysis limit steam flow conditions. (QC = 105% rated).
2. Maximum RHR heat exchanger service water temperature. (QC = 95°F).
3. Suppression pool temperature at normal power operation Technical Specification limit ( $T_{op}$ ). (QC = 95°F).
4. Minimum Technical Specification suppression pool water volume. (QC = 112,200 cu. ft.).
5. Recirculation pumps operating.

Event Sequence

<u>Time (Min.)</u>	<u>Event Description</u>
0.0	SBA occurs
	ADS blows down the plant**

No operator actions assumed, event runs to completion.

The suppression pool temperature versus discharge mass flux is determined by the analysis.

\* Corresponds to nonproprietary Question 1(d).

\*\* ADS valves out of service as allowed in Technical Specifications.

(QC) = 1 ADS valve allowed out of service.

Assumptions for Event 3

1. Maximum operating condensate storage water temperature.
2. HPCI failure, no credit taken for RCIC.
3. Both RHR loops available for pool cooling.
4. Vessel liquid mass adjusted to account for subcooled liquid in the RPV and piping.
5. Metal mass adjusted to account for lower temperature of some metal components.

6. Effect of steam void collapse included.
7. Trip volumes for makeup systems adjusted to account for relative elevations in the RPV.
8. Duty of RHR heat exchangers based on 40 years of crud.
9. No offsite power.
10. SRV capacities at 122.5% of ASME rated.
11. Licensed decay heat curve for containment analysis (adjusted to account for delay between scram and isolation).
12. On plants with motor-driven feedwater pumps (QC), the feedwater flow stops when the accident begins (see 9, above).
13. Event terminates in cold shutdown.
14. LPCI mode of RHR, LPCS, and ADS available.
15. Limiting small line break.
16. ADS valves out of service as allowed in Technical Specifications.

EVENT 4\* - ISOLATION AND REACTOR DEPRESSURIZATION

Initial Conditions

1. Operation at Technical Specification safety analysis limit steam flow conditions. (QC = 105% rated).
2. Maximum RHR heat exchanger service water temperature. (QC = 95°F).
3. Suppression pool temperature at normal power operation Technical Specification limit ( $T_{op}$ ). (QC = 95°F).
4. Minimum Technical Specification suppression pool water volume. (QC = 112,200 cu. ft.).
5. Recirculation pumps operating.

Event Sequence

<u>Time (Min.)</u>	<u>Event Description</u>
$t_a = t_s = 0.0$	Pool temperature alarm; reactor isolation and scram - Initial Condition 3. Initiate actions to turn RHR loops on for pool cooling.
$t_a + 3 \text{ minutes}^{**}$	Both RHR loops on for pool cooling.
$0 < t < t_c$	Reactor pressure maintained using SRV (intermittent operation).
$t_c$	Initiate cooldown at $\leq 100^\circ\text{F/hr.}$ using SRV and RV's at $120^\circ\text{F.}^{***}$
$t_b$	Drywell high pressure trip (QC = 2 psig). RHR automatically switched out of pool cooling mode.
$t_b + 30$	Operator vents drywell to Standby Gas Treatment System.

\* Corresponds to nonproprietary Question 1(e).

\*\* The operator can complete the actions necessary to turn the RHR loops on within three minutes.

\*\*\* If only one RHR loop is available, cooldown rate is not limited to  $100^\circ\text{F/hr.}$

Assumptions for Event 4

1. Maximum operating condensate storage water temperature.
2. Normal automatic operation of HPCI, RCIC - but manually controlled thereafter.

3. Both RHR loops available for pool cooling.
4. Vessel liquid mass adjusted to account for subcooled liquid in the RPV and piping.
5. Metal mass adjusted to account for lower temperature of some metal components.
6. Effect of steam void collapse included.
7. Trip volumes for makeup systems adjusted to account for relative elevations in the RPV.
8. RCIC and HPCI allowed to operate to 100 psia.
9. Duty of RHR heat exchangers based on 40 years of crud.
10. CRD flow maintained constant.
11. SRV capacities at 122.5% of ASME rated.
12. Licensed decay heat curve for containment analysis (adjusted to account for delay between scram and isolation).
13. On plants with motor-driven feedwater pumps (QC), the feedwater pumps operate continuously.
14. Event terminates in cold shutdown.

EVENT 1\* - STUCK-OPEN RELIEF VALVE FROM POWER OPERATION

Initial Conditions

1. Operation at Technical Specification safety analysis limit steam flow conditions. (D2/3 = 105% rated).
2. Maximum containment cooling heat exchanger service water temperature. (D2/3 = 95°F).
3. Suppression pool temperature at normal power operation Technical Specification limit ( $T_{op}$ ). (D2/3 = 95°F).
4. Minimum Tech Spec suppression pool water volume. (D2/3 = 112,000 cu. ft.).

Event Sequence

<u>Time</u>	<u>Temp</u>	<u>Event Description</u>
# $t_a = 0.0$	$T_{op}$	SRV fails open. Pool temperature at initial Condition 3. Initiate actions to turn containment cooling loops* on for pool cooling.
$t_a + 3$ minutes**		Containment cooling loops* on for pool cooling.
$t_s$	$T_s$	Reactor Scram*** ( $T_s = 110^\circ\text{F}$ . for D2/3).
$t_s + 10.5$ seconds		Isolation (assuming mechanistic isolation on low-low reactor water level).
$t_s + 1$ minutes		Manually initiate isolation condenser.
$t_s + 10$ minutes##		2-3 additional SRV manually actuated as necessary.
### $t_b$	$T_b$	Drywell high pressure trip (D2/3 = 2 psig). Containment cooling automatically switched out of pool cooling mode.
$t_b + 30$ minutes		Operator vents drywell to Standby Gas Treatment System.

\* Corresponds to nonproprietary Question 1(a), two containment cooling loops available.

\*\* The operator can complete the actions necessary to turn the containment cooling loops on within three minutes.

\*\*\* Mode switch in Shutdown.

- # The bulk suppression pool temperature is assumed to be 95°F rather than 120°F when an SRV inadvertently fails open. Also, Section 3.7.A.1 in the D2/3 tech specs specifies that the reactor shall be scrammed from any operating condition when the suppression pool temperature reaches 110°F.
- ## The operator can determine which valve is stuck open within ten minutes.
- ### The operator can prevent the drywell pressure from reaching 2 psig by using the torus spray.

Assumptions for Event 1

1. Maximum operating condensate storage water temperature.
2. Normal automatic operation of HPCI, but manually controlled thereafter.
3. Both containment cooling loops available for pool cooling.
4. Vessel liquid mass adjusted to account for subcooled liquid in the RPV and piping.
5. Metal mass adjusted to account for lower temperature of some metal components.
6. Effect of steam void collapse included.
7. Trip volumes for makeup systems adjusted to account for relative elevations in the RPV.
8. Duty of containment cooling heat exchangers based on 40 years of crud.
9. CRD flow maintained constant.
10. SRV capacities at 122.5% of ASME rated.
11. Licensed decay heat curve for containment analysis (adjusted to account for delay between scram and isolation).
12. Motor-drive feedwater pumps on continuously.
13. Event terminates in cold shutdown.

EVENT 2\* - STUCK-OPEN RELIEF VALVE FROM ISOLATED HOT STANDBY

Initial Conditions

1. Operation at Technical Specification safety analysis limit steam flow conditions before isolation. (D2/3 = 105% rated).
2. Maximum containment cooling heat exchanger service water temperature. (D2/3 = 95°F).
3. Suppression pool temperature at normal power operation Technical Specification limit ( $T_{op}$ ). (D2/3 = 95°F).
4. Minimum Technical Specification suppression pool water volume (D2/3 - 112,000 cu. ft.).
5. Reactor pressure when isolated is 920 psig.

Event Sequence

Time (Min.)	<u>Event Description</u>
$t_a = t_s = 0.0$	An abnormal operational transient has occurred, which resulted in reactor scram and isolation. The suppression pool temperature is $T_{op}$ (Initial Condition 4). The operator initiates actions to turn the containment cooling loop on for pool cooling.
$t_a + 3 \text{ minutes}^{**}$	Containment Cooling loop on for pool cooling.
$0 < t < 30$	Reactor pressure maintained using isolation condenser.
$t_o$	Single SRV fails open at 95°F.
$t_o + 10 \text{ minutes}^{***}$	2-3 additional SRV opened (by operator).
$\#t_b$	Drywell high pressure trip (D2/3 = 2 psig). Containment cooling automatically switched out of pool cooling mode.
$t_b + 30$	Operator vents drywell to Standby Gas Treatment System.

The number of SRV's to be manually actuated by the operator to be determined by the analysis.

\* Corresponds to nonproprietary Question 1(c). This event does not conform to the plant licensing basis because it requires a transient plus a single failure. In addition, due to the emergency condensers, relief valves are not used for cooldown in an isolated hot standby condition. Therefore, this event should not be analyzed.

- \*\* The operator can complete the actions necessary to turn the containment cooling loop on within three minutes.
- \*\*\* The operator can determine which valve is stuck open within ten minutes.
- # The operator can prevent the drywell pressure from reaching 2 psig by using the torus spray.

Assumptions for Event 2

1. Maximum operating condensate storage water temperature.
2. Normal automatic operation of HPCI, but manually controlled thereafter.
3. Both containment cooling loops available for pool cooling.
4. Vessel liquid mass adjusted to account for subcooled liquid in the RPV and piping.
5. Metal mass adjusted to account for lower temperature of some metal components.
6. Effect of steam void collapse included.
7. Trip volumes for makeup systems adjusted to account for relative elevations in the RPV.
8. Duty of containment cooling heat exchangers based on 40 years of crud.
9. CRD flow maintained constant.
10. SRV capacities at 122.5% of ASME rated.
11. Licensed delay heat curve for containment analysis (adjusted to account for delay between scram and isolation).
12. Motor-driven feedwater pumps on continuously.
13. Event terminates in cold shutdown.

EVENT 3\* - SMALL BREAK ACCIDENT WITH ADS

Initial Conditions

1. Operation at Technical Specification safety analysis limit steam flow conditions. (D2/3 = 105% rated).
2. Maximum containment cooling heat exchanger service water temperature. (D2/3 = 95°F).
3. Suppression pool temperature at normal power operation Technical Specification limit ( $T_{op}$ ). (D2/3 = 95°F).
4. Minimum Technical Specification suppression pool water volume. (D2/3 = 112,000 cu. ft.).

Event Sequence

<u>Time (Min.)</u>	<u>Event Description</u>
0.0	SBA occurs during normal power operation** ADS blows down the plant

No operator actions assumed, event runs to completion.

The maximum suppression pool temperature is determined by the analysis.

\* Corresponds to nonproprietary Question 1(d).

\*\* The bulk suppression pool temperature is assumed to be 95°F rather than 120°F when the SBA occurs. Also, Section 3.7.A.1 specifies that the reactor shall be scrammed from any operating condition when the suppression pool temperature reaches 110°F.

Assumptions for Event 3

1. Maximum operating condensate storage water temperature.
2. HPCI failure (ADS would not activate if HPCI was operative).
3. Both containment spray loops available for pool cooling.
4. Vessel liquid mass adjusted to account for subcooled liquid in the RPV and piping.
5. Metal mass adjusted to account for lower temperature of some metal components.

6. Effect of steam void collapse included.
7. Trip volumes for makeup systems adjusted to account for relative elevations in the RPV.
8. Duty of containment cooling heat exchangers based on 40 years of crud.
9. No offsite power.
10. SRV capacities at 122.5% of ASME rated.
11. Licensed decay heat curve for containment analysis (adjusted to account for delay between scram and isolation).
12. The feedwater flow stops when the accident begins (see 9, above).
13. Event terminates in cold shutdown.
14. LPCI, core spray, and ADS available.
15. Limiting small line break.
16. One ADS valve out of service as allowed in Technical Specifications.

EVENT 4\* - ISOLATION AND REACTOR DEPRESSURIZATION

Initial Conditions

1. Operation at Technical Specification safety analysis limit steam flow conditions. (D2/3 = 105% rated).
2. Maximum containment cooling heat exchanger service water temperature. (D2/3 = 95°F).
3. Suppression pool temperature at normal power operation Technical Specification limit ( $T_{op}$ ). (D2/3 = 95°F).
4. Minimum Technical Specification suppression pool water volume. (D2/3 = 112,000 cu. ft.).
5. Recirculation pumps operating.

Event Sequence

Dresden Units 2 and 3 are depressurized from an isolated condition using the emergency condenser. If a relief valve# inadvertently failed open, the event sequence would be the same as that for Event 2. Otherwise, D2/3 does not use relief valves for cooldown, and this event would not occur.

Assumptions for Event 4

None

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# or safety-relief valve