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Docket No. 50-237

Commonwealth Edison Company
ATTN: Mr. J. S. Abel
Nuclear Licensing Administrator
Boiling Water Reactors
Post Office Box 767
Chicago, Illinois 60690

Gentlemen:

Your letter and reload report of August 27, 1974 requested approval of a reload core consisting of 7 x 7 and 8 x 8 fuel assemblies. We have reviewed the report as supplemented by your submittal of October 10, 1974 and require the information listed in the attachment to continue our review. We also note that you made a commitment to propose technical specification changes for 8 x 8 and 7 x 7 MAPLHGR's by October 28, 1974. We have not received the proposed changes.

We request that the information in the Attachment be submitted by November 22, 1974 to enable us to maintain our review schedule.

Sincerely,

Original signed by
Dennis L. Ziemann

Dennis L. Ziemann, Chief
Operating Reactors Branch #2
Directorate of Licensing

Enclosure:
Attachment

cc w/enclosure:
John W. Rowe, Esquire
Isham, Lincoln & Beale
One First National Plaza
Chicago, Illinois 60670

Anthony Z. Roisman, Esquire
Berlin, Roisman and Kessler
1712 N Street, N. W.
Washington, D. C. 20036

Chairman, Board of Supervisors
of Grundy County
Morris, Illinois 60451

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SURNAME ➤	RSilver/tc	DLZiemann				
DATE ➤	11/ 8/74	11/11/74				

Form AEC-318 (Rev. 9-53) AECM 0240 GPO C43 16 81465-1 520-284

REQUEST FOR ADDITIONAL INFORMATION ON NEDO-20547

1. In Section 4.1. the thermal-hydraulic characteristics of the transition core are referenced to Table 4-3.3 in NEDO-20360. Provide a revised table of thermal-hydraulic characteristics which reflects the actual number of 8 x 8 reload fuel and the effects of the bypass flow modifications. Also include the peak LHGR used in the analyses for each of the fuel types and the bases for these values.

2. In Section 4.2 there is a summary discussion of increased bypass flow caused by channel distortion. Provide the following information with regard to the flow area between channel and lower tie plate.

   (1) Initial area at BOL
   (2) Anticipated area at the end of next cycle
   (3) Area with finger springs in place

3. Each assembly will have a different amount of channel distortion and differences in as fabricated dimensions. Define the uncertainty in assembly flow rate caused by these dimensional variations.

4. A variation in hot channel flow rate results in variations in hot channel power and thermal margin. How is the uncertainty in hot channel flow rate conservatively accounted for when calculating thermal margins with in-core data?

5. Define the MCHFR for each of the fuel types obtained in the rod withdrawal transient described in Section 6.3.3.2.

6. Justify using Dresden Station Special Report No. 29, Supplement B to demonstrate acceptable transient behavior in light of differences in assembly flow rates. Of particular concern is the pump seizure accident.