

CALCULATION COVER SHEET

NINE MILE POINT NUCLEAR STATION

Unit (1, 2 or 0=Both) : 1

Discipline : STRUCTURAL

Title LIMITED ANALYTICAL REVIEW OF CABLE TRAY SUPPORT	Calculation No. S0.0SQUGLAR1		
	(Sub)system(s) NA	Building RB	Floor Elev. 261

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Checker(s) / Approver(s) MOHAMMED ALVI

Rev	Description	Design Change No.	By	Date	Chk	Date	App	Date
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Ref No	Document No.	Doc Type	Index	Sheet	Rev
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- General Reference(s) :
- GENERIC IMPLIMENTATION PROCEDURE (GIP)
 - NMPC Letter to NRC, File Code NMP1L 1044, dated March 11, 1996

Remarks :
NONE

Confirmation Required (Yes / No) : No See Page(s) : _____	Final Issue Status (APP / FIO / VOI) : APP	File Location (Calc / Hold) : Calc	Operations Acceptance Required (Yes / No) : No
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Nine Mile Point Nuclear Station

Unit: 1

Disposition: ---

Originator/Date <u>B</u> / <u>7-9-97</u>	Checker/Date <u>M.A</u> / <u>7-9-97</u>	Calculation No. <u>S0.0SQUGLAR1</u>	Revision <u>00</u>
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Ref.

PURPOSE: Document the Limiting Analytical Review (LAR) evaluation for a typical Reactor Building cable tray support having a cast in-place cast iron insert as an anchor to the underside of the 281 foot elevation concrete slab.

This LAR has been prepared as part of the commitment to use the SQUG (GIP) methodology to document the seismic adequacy of cable tray supports.

CONCLUSION: This cable support meets the GIP requirements.

ATTACHMENTS

A. LAR for a cable tray support having cast iron inserts.



Nine Mile Point Nuclear Station

Unit: 1

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Originator/Date

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ATTACHMENT A

LIMITING ANALYTICAL REVIEW EVALUATION #1

<p>REVIEWED <i>ATTACHMENT A, LAR#1</i> NIAGARA MOHAWK POWER CORPORATION NUCLEAR ENGINEERING DEPARTMENT</p> <p>DISPOSITION OF SUBMITTAL</p> <p><input checked="" type="checkbox"/> ACCEPTED <input type="checkbox"/> ACCEPTED WITH CHANGES NOTED <input type="checkbox"/> NOT ACCEPTED <input type="checkbox"/> REVISE & RESUBMIT</p> <p>SIGNATURE: <u><i>[Signature]</i></u> DATE: <u>7-9-97</u></p> <p>DISCIPLINE: <u>STRUCTURAL</u> UNIT: <u>1</u></p>





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SUBJECT _____ JOB No. 93C2771 SHEET A1-2 OF 4

LAR # 1

REVISIONS	0	KC 01/06/94
		S.C. 1-11-94

EL 261'

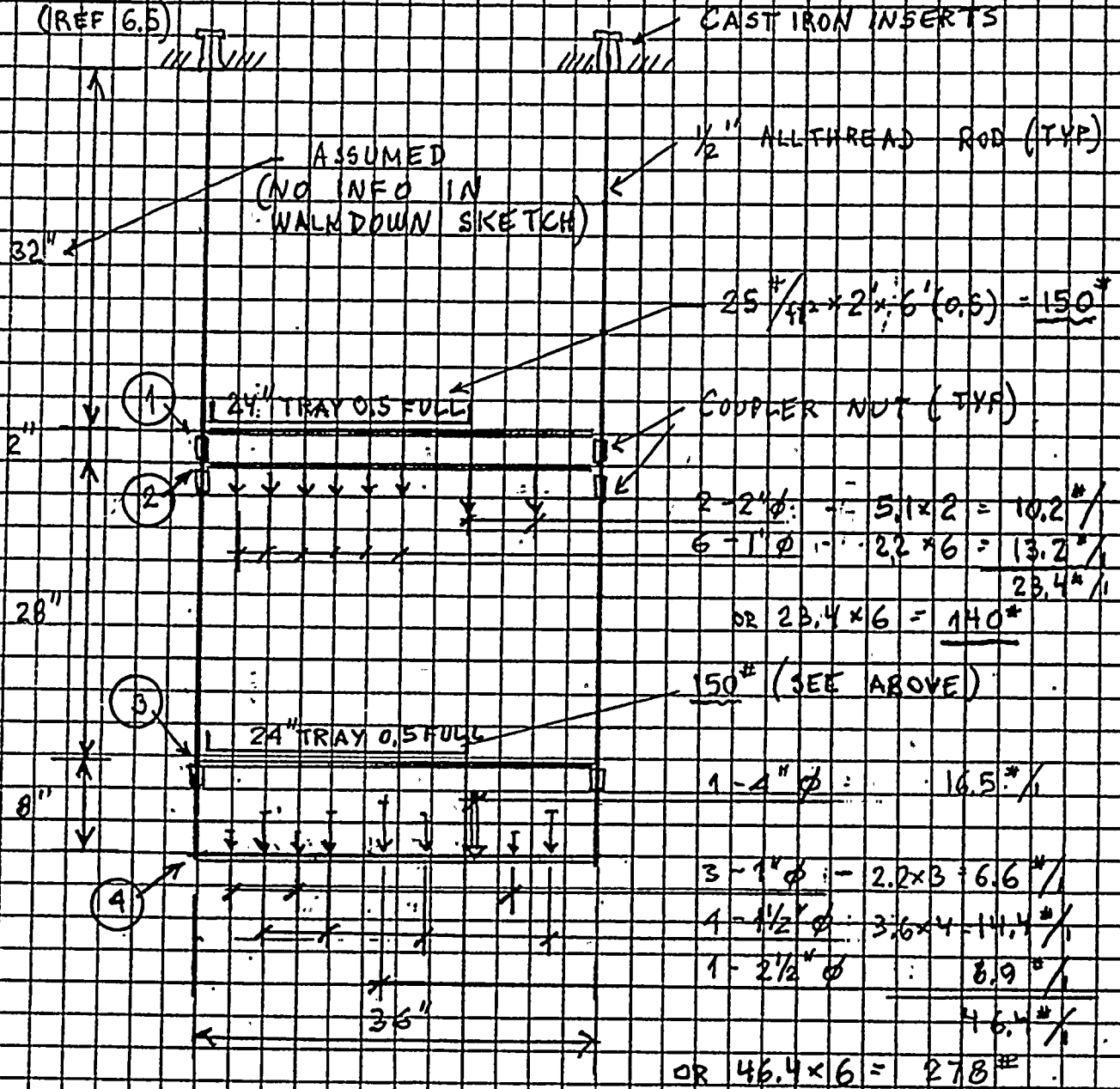
ATTACHMENT
CALC NO
REVISION
PAGE NO
5025041
A1

LOAD CALCULATION

LOCATION: RB NORTH COR.

TYP SUPPORT SPACING - 6'

EL 261'



ALL HORIZONTAL MEMBERS ARE F 1000;



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JOB NO. 91C2771

CALCULATION: C-006

Nine Mile Point Unit 1 Raceway Limited
Analytical Review

Sheet A1-3 of 4

Revision 0

By: KC 01/11/94

Check: S.C. 1-11-94

LAR #1

Dead Load Check

ATTACHMENT A
CALC NO SP.050901
REVISION 00
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Horizontal member

The worst case is member 4 - unistrut P1000.
For L=36" unistrut capacity = 1130 lb (Ref. 6.2, page 5)
1130 lb > 278 lb Hence the unistrut is OK.

Vertical member (1/2" threaded rod)

Load per one rod:
(150 + 140 + 150 + 278) x 0.50 = 718 x 0.5 = 360 lb
Max safe load = 7670 lb
7670 lb > 360 lb Hence the vertical member is OK.

Connection of treaded rod to concrete

Capacity of cast iron inserts = 1360 lb (Ref. 6.6, page 6)
1360 lb > 360 lb Hence the inserts are OK. SF = 1360 / 360 = 3.78

Vertical Capacity Check

Cast iron inserts

360 x 3 = 1080 lb < 1360 lb OK SF = 1360 / 1080 = 1.26

Ductility Check

This support is considered ductile (see Ref. 6.4, 8.3.3 for Rod Hanger Trapeze Supports).

Lateral Load Check

No lateral load check is required since the support is ductile (Ref. 6.4, 8.3.4).

Rod Hanger Fatigue Evaluation

Support resonant frequency (Ref. 6.4, 8.3.5):

$$f_{sup} = \frac{1}{2\pi} \sqrt{\frac{K_s}{M_s}} = \frac{1}{2\pi} \sqrt{\frac{514}{186}} = 0.84 \text{ Hz} \quad \text{where}$$

W = 360 x 2 = 720 lb (total dead weight on the pair of rod supports)

g = 386.4 in/sec²



<h1 style="margin: 0;">S&A</h1> <p style="margin: 0;">STEVENSON & ASSOCIATES a structural-mechanical consulting engineering firm</p>	JOB NO. 91C2771	Sheet R1-4 of 4
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	Nine Mile Point Unit 1 Raceway Limited Analytical Review	By: KC 01/11/94
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LAR #1

$E = 29 \times 10^6$ psi (elastic modulus of steel)

$I = 0.05 \times 0.406^4 = 136 \times 10^{-3} \text{ in}^4$ (moment of inertia of rod root section, $d = 0.406$ per page 4-147 of Ref. 6.1))

$L = 32$ " (length of rod above top tier)

$$K_s = 2 \frac{12EI}{L^3} + \frac{W}{L} = 2 \frac{12 \times 29 \times 10^6 \times 136 \times 10^{-3}}{32^3} + \frac{720}{32} = 514 \text{ lb/in}$$

$$M_s = \frac{720}{386.4} = 186 \text{ lb-sec}^2/\text{in}$$

ATTACHMENT A
CALC NO SO.050VHLAR1
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See attached comparison of Floor Response Spectra to Rod Fatigue Bounding Spectra (RB 281).

Use 0.5 g and go to Fig. 8-12 of Ref. 6.4.

At $L = 32$ " the maximum acceptable weight is > 2.2 k. This is far above 720 lb applied to both rods.

Hence fatigue capacity is OK.

Conclusion

This support meets the GIP requirements.



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		By TMT 1-20-94
		Chk. KC 01/24/94

ATTACHMENT A
CALC NO SO050201A1
REVISION 00
PAGE NO AS

6.0 References

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- 6.3. "Design Response Spectra for Nine Mile Point Unit 1, Reactor Building and Turbine Building", Stevenson & Associates, February 1992.
- 6.4. "Generic Implementation Plan Procedure (GIP), for Seismic Verification of Nuclear Plant Equipment", Revision 2A, March, 1993, Seismic Qualification Utility Group.
- 6.5. A-46 GIP Walkdown Notes, 1993.
- 6.6. "Development of Load Capacities of Cast Iron Inserts and Q-Decking at Nine Mile Point Unit 1", Stevenson & Associates, Project No. 92C2757, January 1993.
- 6.7. "Formulas for Natural Frequency and Mode Shape", R. D. Blevins, Van Nostrand Reinhold, 1979.
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