

# **ENCLOSURE 4**

## **SUPPLEMENT 1 NINE MILE POINT 1 SEISMIC ANALYSIS, CORE SHROUD REPAIR MODIFICATION**

**NON-PROPRIETARY VERSION**





**GE Nuclear  
Energy**

**GENE B13-01739-03  
Supplement 1  
Class III  
August 1996**

**~~—GE Proprietary Information—~~**

**Supplement 1  
Nine Mile Point 1  
Seismic Analysis, Core Shroud  
Repair Modification**

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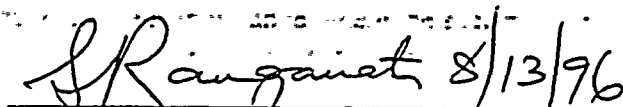
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REVISION STATUS SHEET

Revision	Approval	Date	Description
0	P. Walier	Dec. 1994	Initial issue.
Suppl. 1	S. Ranganath	August, 1996	Evaluate revised lower spring spacing.





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## 1. INTRODUCTION

The purpose of this supplement to the seismic analysis is to address the change in the spacing between lower spring on the shroud repair hardware. Lower springs located at  $90^\circ$  intervals have the same equivalent spring constant in any direction of the applied load. Spacing greater than  $90^\circ$  between two adjacent springs tends to decrease the equivalent spring constant for loads applied between the two. Spring spacing less than  $90^\circ$  tends to increase the equivalent spring constant for loads applied between the two. Relocating the  $270^\circ$  lower spring to the opposite side of the tie rod, along with changes made previously, result in the maximum spring spacing increasing to  $108^\circ$  and the minimum spacing between springs decreasing to  $76^\circ$ .

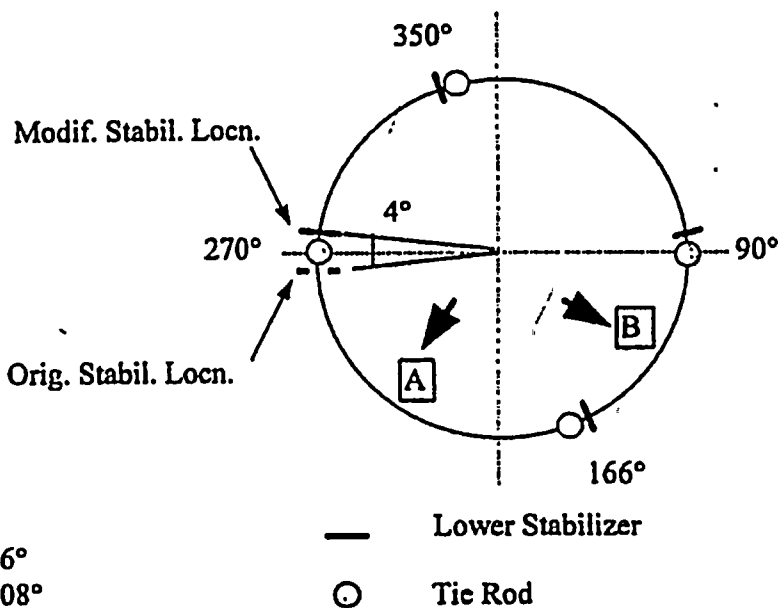
## 2. SUMMARY AND CONCLUSIONS



### 3. ANALYSIS

The as-built locations of the tie rods are at azimuths 90°, 166°, 270°, and 350°. The lower stabilizer is attached to one side of the tie rod assembly (consistent side) at all four tie rod locations. The lower stabilizer at the 270° tie rod location, however, was found to be contacting the RPV at the bend radius of the recirculation pipe nozzle, resulting in partial bearing against the RPV. In order to remedy this, the lower stabilizer spring at this tie rod location is proposed to be removed and re-attached to the 'other' side of the tie rod assembly. This would result in the lower stabilizers being apart as follows:

90° ~ 166°	= 76°
166° ~ 274°	= 108°
274° ~ 350°	= 76°
350° ~ 90°	= 100°



Minimum Angle Spread	=	76°
Maximum Angle Spread	=	108°

The nominal lower stabilizer stiffness used in seismic analysis is based on 90° spread. The minimum angle spread of 76° (Load direction B) results in upper bound net stabilizer stiffness and the maximum angle spread of 108° (Load direction A) results in lower bound net stabilizer stiffness. Analysis was performed to assess the impact of the variation of the lower stabilizer stiffness (bounded by these upper and lower bound stabilizer stiffnesses) on the hardware seismic loads and displacements.





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### 3.1 Lower Stabilizer Stiffness

## 4. RESULTS

The resulting hardware loads, displacements, loads in key internal components, and shroud frequencies are summarized in Table 1.

The displacements are within the allowables specified in the design specification (Reference 2). The hardware loads will be reconciled separately by comparing against the design loads/margins. The loads on key internal components are also summarized and are less than or equal to the loads based on uncracked, unmodified shroud. The shroud frequency shifts due to the stiffness changes are very small and moreover, they are in the frequency range where the spectral amplitudes are almost flat or mildly ramping, thus resulting in the above insignificant effects.



(ii)

**5. REFERENCES**

- 5.1. Nine Mile Point 1: Seismic Analysis -Core Shroud Repair Modification, Report Number GENE-B13-01739-03, Revision 0.
- 5.2. Design Specification - Shroud Repair, GE Document No. 25A5583.



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Table 1

NMP1 Shroud Repair : Seismic Analysis - Lower Stabilizer Stiffness Parametric Study

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