

REGULATORY INFORMATION DISTRIBUTION SYSTEM (RIDS)

ACCESSION NBR: 8709150217 DOC. DATE: 87/09/11 NOTARIZED: NO DOCKET #  
 FACIL: 50-410 Nine Mile Point Nuclear Station, Unit 2, Niagara Moha 05000410  
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 RANDALL, R. G. Niagara Mohawk Power Corp.  
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 RECIP. NAME RECIPIENT AFFILIATION

SUBJECT: LER 87-051-00: on 870813, shutdown cooling sys isolated during performance of electrical protection assemblies calibr surveillance procedure. Caused by procedural deficiency. Monitor reactor coolant temp per Tech Specs. W/870911 ltr.

DISTRIBUTION CODE: IE22D COPIES RECEIVED: LTR 1 ENCL 1 SIZE: 10  
 TITLE: 50.73 Licensee Event Report (LER), Incident Rpt, etc.

NOTES: 21

05000410

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	REG FILE 02	1 1	RES DEPY GI	1 1
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	RGN1 FILE 01	1 1		
EXTERNAL:	EG&G GROH, M	5 5	H ST LOBBY WARD	1 1
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LICENSEE EVENT REPORT (LER)

FACILITY NAME (1) <b>Nine Mile Point Unit 2</b>	DOCKET NUMBER (2) <b>0   5   0   0   0   410</b>	PAGE (3) <b>1 OF 08</b>
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TITLE (4) **Shutdown Cooling Isolation and LCO Exceeded due to Equipment Failure and Design Deficiency**

EVENT DATE (5)			LER NUMBER (6)			REPORT DATE (7)			OTHER FACILITIES INVOLVED (8)		
MONTH	DAY	YEAR	YEAR	SEQUENTIAL NUMBER	REVISION NUMBER	MONTH	DAY	YEAR	FACILITY NAMES		DOCKET NUMBER(S)
08	13	87	87	051	00	09	11	87	N/A		0   5   0   0   0
									N/A		0   5   0   0   0

OPERATING MODE (9) <b>4</b>	THIS REPORT IS SUBMITTED PURSUANT TO THE REQUIREMENTS OF 10 CFR §: (Check one or more of the following) (11)									
POWER LEVEL (10) <b>000</b>	<input type="checkbox"/> 20.402(b)	<input type="checkbox"/> 20.406(c)	<input checked="" type="checkbox"/> 50.73(e)(2)(iv)	<input type="checkbox"/> 73.71(b)						
	<input type="checkbox"/> 20.406(a)(1)(i)	<input type="checkbox"/> 50.38(c)(1)	<input type="checkbox"/> 50.73(e)(2)(v)	<input type="checkbox"/> 73.71(c)						
	<input type="checkbox"/> 20.406(a)(1)(ii)	<input type="checkbox"/> 50.38(c)(2)	<input type="checkbox"/> 50.73(e)(2)(vii)	OTHER (Specify in Abstract below and in Text, NRC Form 366A)						
	<input type="checkbox"/> 20.406(a)(1)(iii)	<input checked="" type="checkbox"/> 50.73(a)(2)(i)	<input type="checkbox"/> 50.73(a)(2)(viii)(A)							
	<input type="checkbox"/> 20.406(a)(1)(iv)	<input type="checkbox"/> 50.73(a)(2)(ii)	<input type="checkbox"/> 50.73(a)(2)(viii)(B)							
<input type="checkbox"/> 20.406(a)(1)(v)	<input type="checkbox"/> 50.73(a)(2)(iii)	<input type="checkbox"/> 50.73(a)(2)(ix)								

LICENSEE CONTACT FOR THIS LER (12)

NAME <b>Robert G. Randall, Supervisor Technical Support</b>	TELEPHONE NUMBER <b>315</b>	TELEPHONE NUMBER <b>349-2445</b>
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COMPLETE ONE LINE FOR EACH COMPONENT FAILURE DESCRIBED IN THIS REPORT (13)

CAUSE	SYSTEM	COMPONENT	MANUFACTURER	REPORTABLE TO NPDOS	CAUSE	SYSTEM	COMPONENT	MANUFACTURER	REPORTABLE TO NPDOS
X	ED	52	G080	N					

SUPPLEMENTAL REPORT EXPECTED (14)

YES (If yes, complete EXPECTED SUBMISSION DATE)  NO

EXPECTED SUBMISSION DATE (15)	MONTH	DAY	YEAR

ABSTRACT (Limit to 1400 spaces i.e. approximately fifteen single space typewritten lines) (16)

While in Mode 4 on August 13, 1987 at 0323 hours, the Shutdown Cooling (SDC) system isolated during performance of the Electrical Protection Assemblies (EPA) calibration surveillance procedure. When EPA 1A was tripped per the surveillance, the inboard SDC valve isolated and the running pump tripped. This was an unanticipated result, since tripping one divisional power supply normally would isolate either inboard (Division 2) or outboard (Division 1) valves. Upon attempting to reset EPA 1A, SDC could not be restored within the one hour limit per Technical Specifications. The causes of the event were equipment failure, procedural deficiency, lack of training and design deficiency.

Immediate corrective actions were to monitor coolant temperatures and to manually restore normal SDC by 0525 hours. Normal SDC was lost for approximately two hours, but coolant temperatures remained within the limit for cold shutdown. The EPA breaker was replaced, and the half scram condition and isolations were reset. Further corrective actions are procedural revisions, training for operators and an EPA modification.

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LICENSEE EVENT REPORT (LER) TEXT CONTINUATION

FACILITY NAME (1)  Nine Mile Point Unit 2	DOCKET NUMBER (2)  0   5   0   0   0   410	LER NUMBER (6)			PAGE (3)		
		YEAR	SEQUENTIAL NUMBER	REVISION NUMBER			
		87	051	00	02	OF	08

TEXT (If more space is required, use additional NRC Form 366A's) (17)

I. DESCRIPTION OF EVENT

On August 13, 1987 at 0323 hours the Shutdown Cooling (SDC) System isolated during performance of the Reactor Protection System (RPS) Electrical Protection Assemblies (EPA) calibration surveillance procedure. The normal SDC system could not be restored within the one hour limit established in Technical Specifications (TS). Thus, the Limiting Conditions of Operation (LCO) for the SDC system were exceeded, resulting in a violation of TS 3.4.9.2. Prior to the event, the unit was in cold shutdown (Mode 4), with SDC Loop B operating. Reactor vessel pressure was 0 psig and coolant temperature was 130°F.

Refer to Attachment 1 for the Residual Heat Removal System (RHR/RHS)-SDC subsystem configuration. Refer to Attachment 2 for RPS logic power supply configuration.

At 0322 hours, EPA 1A was tripped by NMPC Meter and Test (M&T) personnel in accordance with the surveillance procedure to perform the necessary channel calibrations. The expected Division 1 half scram and primary containment isolations (outboard containment isolation valves) were received. However, an unexpected result was the receipt of a Division 2 SDC isolation. Consequently, the inboard SDC suction isolation (2RHS\*MOV112) and SDC Loop B injection (2RHS\*MOV40B) valves closed. The other Division 2 SDC valves were already closed. Subsequently, the running SDC pump (2RHS\*PIB) tripped due to the suction valve closure, and normal SDC was interrupted at 0323 hours.

Prior to tripping the EPA, NMPC licensed control room operators and the Station Shift Supervisor (SSS) made a conscientious effort to take the necessary measures to prevent isolation of systems such as SDC, Reactor Water Cleanup (WCS) and normal reactor building ventilation (HVR). In addition, measures were taken to prevent auto initiation of Engineered Safety Features (ESF) systems such as Standby Gas Treatment (GTS). Except for the Main Steam Isolation Valves (MSIVs), the Nuclear Steam Supply Shutoff System (NS<sup>4</sup>) isolation circuits are designed to isolate one of the two isolation valves on a loss of either divisional power supply (i.e. Division 1 isolates outboards and Division 2 isolates inboards). However, the SDC isolation circuit is also an exception to this general design. A loss of any divisional power supply will result in a complete isolation of the SDC system (both inboard and outboard valves). The purpose for this unique design feature is to protect the SDC system from overpressurization. Due to procedural deficiencies and a lack of knowledge of this unique feature of the SDC isolation circuit, the operators' measures to prevent SDC isolations did not include preventing closure of 2RHS\*MOV112 or 40B. Thus, SDC isolated when the EPA was tripped.

Upon receiving the unexpected SDC isolation, the SSS instructed M&T personnel to reset the EPA output breaker so that power could be restored to the bus and measures taken to prevent SDC from isolating again. Plans were to proceed with the required calibration, once all necessary preventative measures were taken and normal SDC restored.



LICENSEE EVENT REPORT (LER) TEXT CONTINUATION

FACILITY NAME (1)  Nine Mile Point Unit 2	DOCKET NUMBER (2)  0   5   0   0   0   410	LER NUMBER (6)			PAGE (3)		
		YEAR	SEQUENTIAL NUMBER	REVISION NUMBER			
		87	— 051	— 00	03	OF	08

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However, upon attempting to reset the EPA output breaker, the breaker resetting mechanism failed. At this time the SSS allowed M&T personnel to troubleshoot the breaker in an attempt to correct the failure and reset it. At approximately 0400 hours, M&T personnel indicated that the breaker could not be fixed and that a replacement would be necessary. Consequently, the half scram condition and the NS<sup>4</sup> isolations could not be reset, and normal SDC could not be restored via remote operation.

Immediate corrective actions were to monitor reactor coolant temperatures per TS 3.4.9.2 and to re-establish normal SDC by manually opening 2RHS\*MOV112 and 40B and restarting the tripped SDC pump. In addition, an emergency work request was generated to replace the defective EPA output breaker. Operators also began raising reactor water level in an attempt to improve natural circulation.

An alternate decay heat removal method was in operation throughout the event via WCS system. However, an alternate coolant circulation method (i.e. forced circulation) could not be established within the one hour limit. Therefore, by 0423 hours the LCO for the SDC system was exceeded.

At 0525 hours, normal SDC was returned to service. Coolant temperature rose 15°F during the two-hour period but remained within the cold shutdown limits throughout the event.

Subsequently, the EPA breaker was replaced and reset and the half scram and NS<sup>4</sup> isolations were reset at 1508 hours.

II. CAUSE OF EVENT

The immediate cause of the event was the failed EPA output breaker resetting mechanism. The intermediate causes of the event were procedural deficiency and lack of training. The root cause was design deficiency.

The LCO for SDC capability would not have been exceeded if the EPA output breaker had not malfunctioned. Therefore, the immediate cause was equipment failure. The cause for the equipment failure has not been determined, and the investigation will continue.

The intermediate causes were procedural deficiency and lack of training. The EPA calibration surveillance procedure had an inadequate plant impact statement. Although the plant impact stated that the Residual Heat Removal System would isolate on a loss of an EPA, it did not specify that both divisional valves would isolate from a loss of a single division. This particular design feature was not discussed in training or any operating procedure. Thus, the operators relied on their knowledge and the plant impact statement in the procedure, in addition to reviewing drawings, to determine preventative measures to be taken. Therefore, better training and a more detailed plant impact statement were necessary to alert operators of this unique design feature not common to other systems.





LICENSEE EVENT REPORT (LER) TEXT CONTINUATION

FACILITY NAME (1)  Nine Mile Point Unit 2	DOCKET NUMBER (2)  0   5   0   0   0   410	LER NUMBER (8)			PAGE (3)	
		YEAR	SEQUENTIAL NUMBER	REVISION NUMBER		
		87	051	00	04	OF 08

TEXT (If more space is required, use additional NRC Form 366A's) (17)

The root cause of the event was design deficiency. Testing of these EPAs is a major operational event due to the loss of power to a single division of the RPS/NS<sup>4</sup> logic. A loss of power to a single division of the RPS/NS<sup>4</sup> logic results in a half scram and in numerous Engineered Safety Features (ESF) actuations such as primary containment isolation, secondary containment isolation and auto initiation of GTS. Because the EPAs cannot be tested without interrupting power, the operators took several hours assessing plant impact, reviewing prints, and taking preventative measures in order to prepare the plant for the EPA surveillance. This places an unnecessary burden upon Operations personnel when the EPA design could be improved to enable testing without power interruptions. Therefore, the EPA design should be modified to avoid unnecessary ESF actuations in the future.

III. ANALYSIS OF EVENT

This event had no adverse safety consequences. Normal SDC capability was lost and an alternate method of forced coolant circulation could not be established for approximately two hours. Coolant temperature rose 15°F during that period but remained within the limit for cold shutdown throughout the event. An alternate means of decay heat removal was available via the WCS system. The WCS heat exchangers were able to handle existing decay heat loads and maintain coolant temperatures within the TS limit. A loss of normal decay heat removal methods is a design basis condition mitigated by alternate decay heat removal methods described in FSAR Section 15.2.9, "Failure of RHR Shutdown Cooling", and in normal and emergency operation procedures.

The inadvertent failure of the EPA output breaker resetting mechanism or an unanticipated trip of an EPA has the potential to create a serious transient during power operation. The loss of power to Division 1 RPS/NS<sup>4</sup> logic has the following plant impact:

1. half scram via the RPS
2. secondary containment isolation
3. auto initiation of the emergency reactor building ventilation recirculation units and GTS
4. isolation of outboard primary containment isolation valves (Groups 2, 4, 6, 8 through 11 and main steam line drains) via NS<sup>4</sup>
5. isolation of inboard and outboard RHR-SDC system valves via NS<sup>4</sup>

The consequences of these events are previously analyzed events that are bounded by the "LOCA Inside Primary Containment" spectrum of events (FSAR 15.6.5) and "Inadvertent HPCS Startup" (FSAR 15.5.1).



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FACILITY NAME (1)  Nine Mile Point Unit 2	DOCKET NUMBER (2)  0   5   0   0   0   410	LER NUMBER (6)			PAGE (3)		
		YEAR	SEQUENTIAL NUMBER	REVISION NUMBER			
		87	051	00	05	OF	08

TEXT (If more space is required, use additional NRC Form 366A's) (17)

IV. CORRECTIVE ACTIONS

Immediate corrective actions were to monitor reactor coolant temperatures per TS 3.4.9.2 and to re-establish normal SDC by manually opening 2RHS\*MOV112 and 40B and restarting the tripped SDC pump. In addition, an emergency work request was generated to replace the defective EPA output breaker. At 0525 hours, normal SDC was returned to service. Subsequently, the EPA breaker was replaced and reset and the half scram and NS<sup>4</sup> isolations were reset at 1508 hours. Further corrective actions are as follows:

1. The plant impact statements in both the six month and eighteen month EPA surveillance procedures were revised to aid the SSS and control room operators in adequately assessing the plant impact for performance of these procedures.
2. The cause for the EPA output breaker resetting mechanism failure is unknown, and the investigation will continue. If the cause of the equipment failure results in additional corrective actions, a supplemental report will be issued.
3. A Training Modification Request (TMR) has been initiated to train Operations personnel on the unique design feature of the SDC isolation circuit to assist in preventing recurrence of this event.
4. The EPAs will be modified to allow testing without power interruptions. This modification will be completed during the 1988 midcycle outage.



LICENSEE EVENT REPORT (LER) TEXT CONTINUATION

FACILITY NAME (1)  Nine Mile Point Unit 2	DOCKET NUMBER (2)  0   5   0   0   0   410	LER NUMBER (6)			PAGE (3)	
		YEAR	SEQUENTIAL NUMBER	REVISION NUMBER		
		87	051	00	06	OF 08

TEXT (If more space is required, use additional NRC Form 366A's) (17)

V. ADDITIONAL INFORMATION

A. Components referred to in this LER

Component	IEEE 803 EIS Funct	IEEE 805 System ID
Electrical Protection Assemblies (EPA)	92	ED
Reactor Protection System	N/A	JC
Nuclear Steam Supply Shutoff System (NS <sup>4</sup> )	N/A	JM
Residual Heat Removal System (RHR/RHS)	N/A	BO
Shutdown Cooling System (SDC)	N/A	BO
Reactor Water Cleanup System (RWCU/WCS)	N/A	CE
Control Rod Drive System (CRD)	N/A	AA
Standby Gas Treatment System (GTS)	N/A	BH
Reactor Building Ventilation System (HVR)	N/A	VA
Pump	P	BO
Isolation Valve	ISV	JM
Circuit Breaker	52	ED

B. Previous Similar Events - None

C. Failed Components - General Electric Type TFJ-175A Molded Case Circuit Breaker; Part No. 184C4494P001



LICENSEE EVENT REPORT (LER) TEXT CONTINUATION

FACILITY NAME (1)

Nine Mile Point Unit 2

DOCKET NUMBER (2)

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LER NUMBER (8)

87-051-00

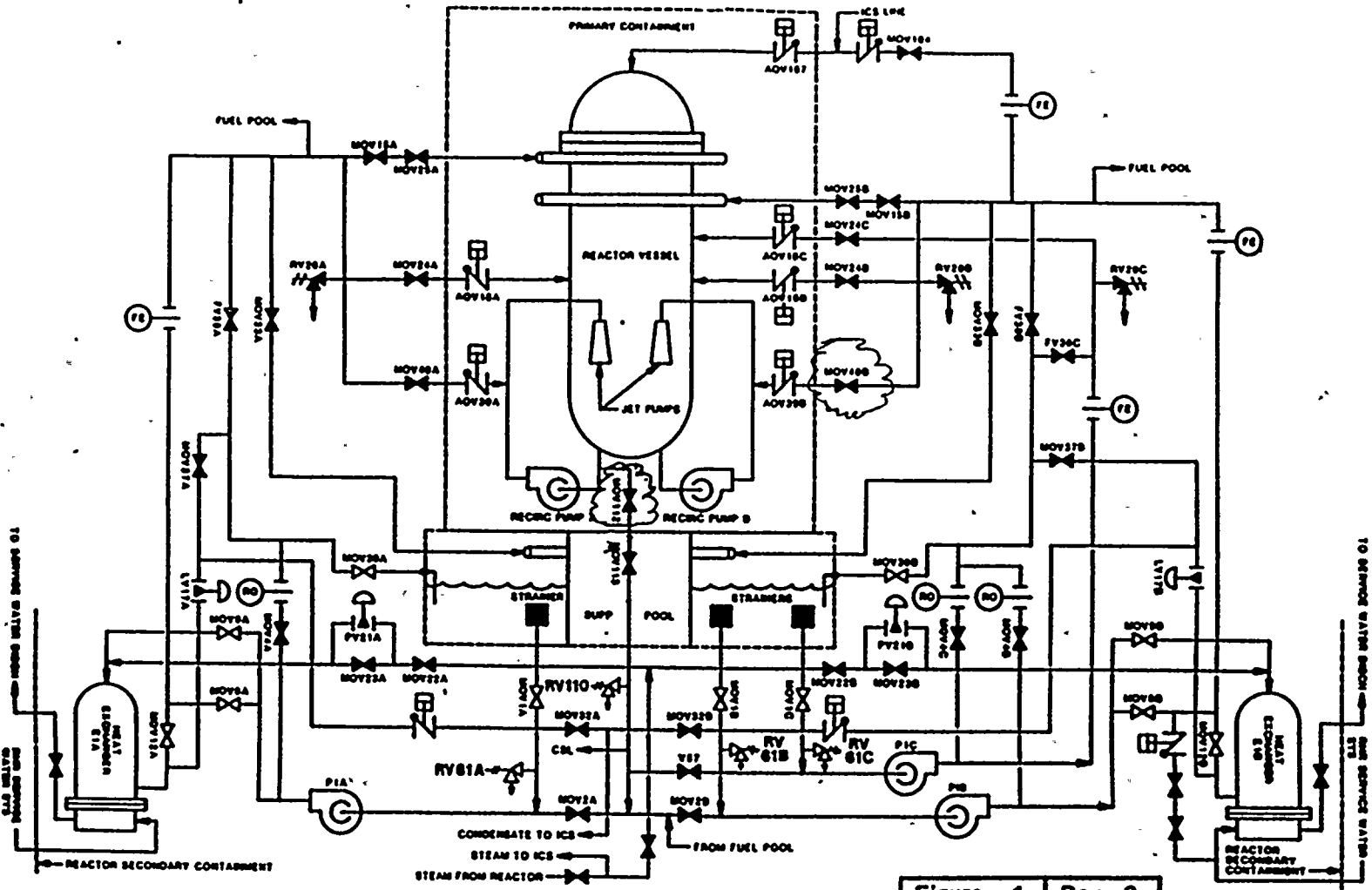
YEAR	SEQUENTIAL NUMBER	REVISION NUMBER
87	051	00

PAGE (3)

07 OF 08

TEXT (if more space is required, use additional NRC Form 366A/1/117)

ATTACHMENT 1



MOV Motor Operated Valves

Figure 1. Rev. 2  
Title: RESIDUAL HEAT REMOVAL SYSTEM



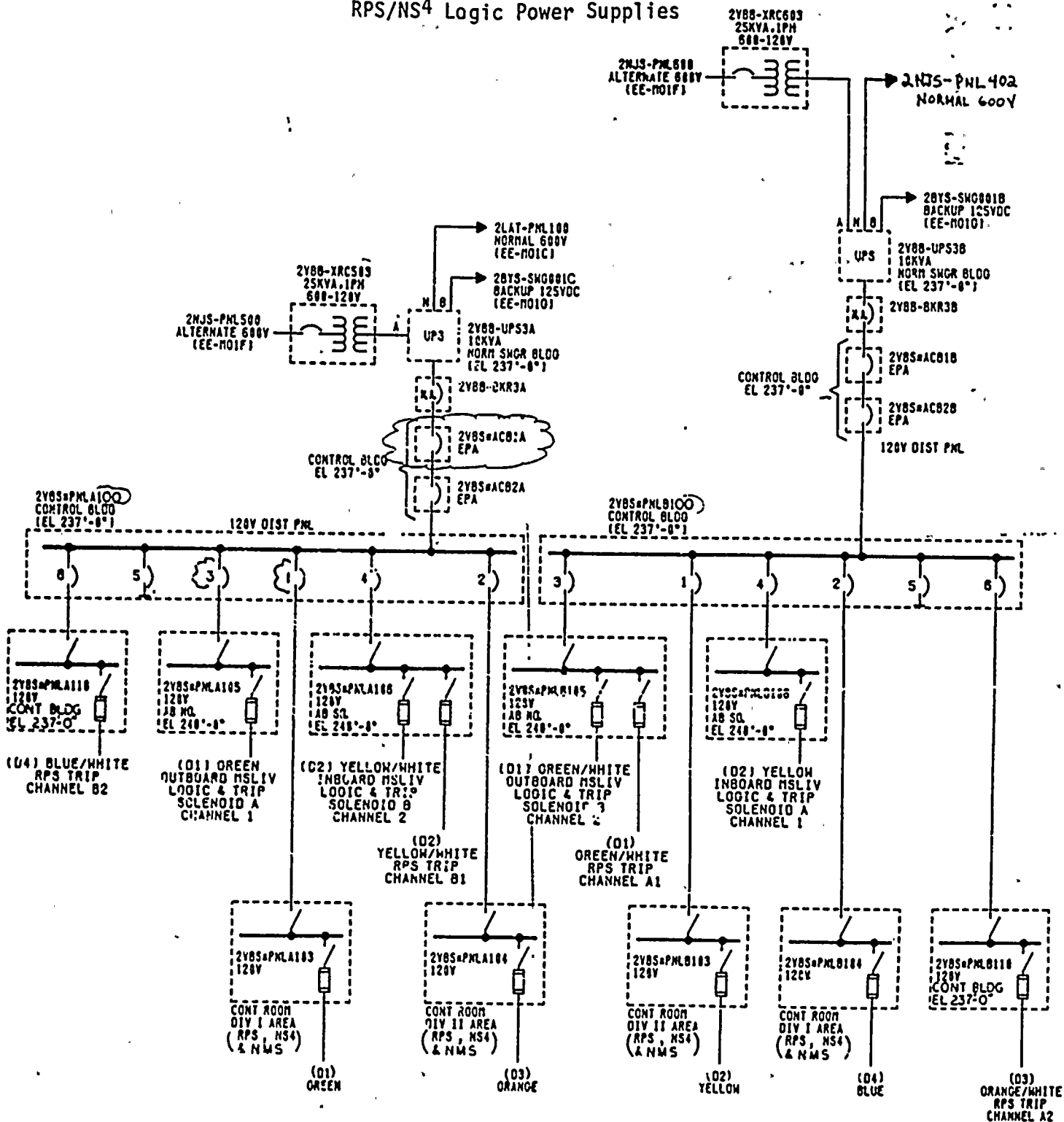


FACILITY NAME (1)  Nine Mile Point Unit 2	DOCKET NUMBER (2)  0   5   0   0   0   410	LER NUMBER (8)			PAGE (3)		
		YEAR	SEQUENTIAL NUMBER	REVISION NUMBER			
		87	051	00	08	OF	08

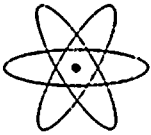
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ATTACHMENT 2

RPS/NS4 Logic Power Supplies







NIAGARA MOHAWK POWER CORPORATION

NIAGARA  MOHAWK

301 PLAINFIELD ROAD  
SYRACUSE, NY 13212

THOMAS E. LEMPGES  
VICE PRESIDENT—NUCLEAR GENERATION

September 11, 1987

United States Nuclear Regulatory Commission  
Document Control Desk  
Washington, DC 20555

RE: Docket No. 50-410  
LER 87-51

Gentlemen:

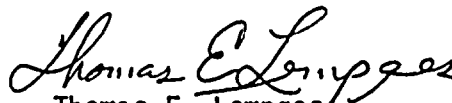
In accordance with 10 CFR 50.73, we hereby submit the following Licensee Event Report:

LER 87-51 Is being submitted in accordance with 10 CFR 50.73 (a) (2) (i) (B), "Any operation or condition prohibited by the plant's Technical Specifications" and in accordance with 10 CFR 50.73 (a) (2) (iv), "Any event or condition that resulted in manual or automatic actuation of any Engineered Safety Feature (ESF), including the Reactor Protection System (RPS). However, actuation of an ESF, including the RPS, that resulted from and was part of the preplanned sequence during testing or reactor operation need not be reported."

10 CFR 50.72 reports were made on August 13, 1987 at 0518 and 0529 hours.

This report was completed in the format designated in NUREG-1022, Supplement No. 2, dated September 1985.

Very truly yours,



Thomas E. Lempges  
Vice President  
Nuclear Generation

TEL/PB/mjd

Attachments

cc: Regional Administrator, Region 1  
Sr. Resident Inspector, W. A. Cook

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