

NINE MILE POINT UNIT 1

Startup Physics Test Results-Cycle 6

June 1979

79088104/6

1.0 Core Loading Verification

Abstract

The purpose of the test is to verify that the cycle 6 core was loaded as specified. During the end of cycle 5 refueling outage, the reactor core was completely unloaded and reloaded. All fuel moves were specified by the Reactor Analyst Department. The operator verified by checkoff that each fuel assembly was loaded in the correct core location. When the core was completely loaded, it was verified by the Reactor Analyst Department using an underwater TV system and video recorder in accordance with Fuel Handling Procedure No. 22, Core Post Alteration Inspection and Verification.

Test Results

Two independent checks of the video tape were made by the Reactor Analyst Technicians to verify that the core was arranged as specified by the core map. As shown on figure 1.1, the cycle 6 core has been loaded and verified.

| | | | | | | | | | | | | | | | | | | | | | | | | |
|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|--|
| 01 | 05 | 07 | 09 | 11 | 13 | 15 | 17 | 19 | 21 | 23 | 25 | 27 | 29 | 31 | 33 | 35 | 37 | 39 | 41 | 43 | 45 | 49 | 51 | |
| 52 | | | | | | | | | | | | | | | | | | | | | | | | |
| 50 | | | | | | | | | | | | | | | | | | | | | | | | |
| 48 | | | | | | | | | | | | | | | | | | | | | | | | |
| 46 | | | | | | | | | | | | | | | | | | | | | | | | |
| 44 | | | | | | | | | | | | | | | | | | | | | | | | |
| 42 | | | | | | | | | | | | | | | | | | | | | | | | |
| 40 | | | | | | | | | | | | | | | | | | | | | | | | |
| 38 | | | | | | | | | | | | | | | | | | | | | | | | |
| 36 | | | | | | | | | | | | | | | | | | | | | | | | |
| 34 | | | | | | | | | | | | | | | | | | | | | | | | |
| 32 | | | | | | | | | | | | | | | | | | | | | | | | |
| 30 | | | | | | | | | | | | | | | | | | | | | | | | |
| 28 | | | | | | | | | | | | | | | | | | | | | | | | |

Figure 1.1
Cycle 6 Loading

| | | | | | | | | | | | | | | | | | | | | | | | | | |
|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|
| 01 | 03 | 05 | 07 | 09 | 11 | 13 | 15 | 17 | 19 | 21 | 23 | 25 | 27 | 29 | 31 | 33 | 35 | 37 | 39 | 41 | 43 | 45 | 47 | 49 | 51 |
| 26 | | | | | | | | | | | | | | | | | | | | | | | | | |
| 24 | | | | | | | | | | | | | | | | | | | | | | | | | |
| 22 | | | | | | | | | | | | | | | | | | | | | | | | | |
| 20 | | | | | | | | | | | | | | | | | | | | | | | | | |
| 18 | | | | | | | | | | | | | | | | | | | | | | | | | |
| 16 | | | | | | | | | | | | | | | | | | | | | | | | | |
| 14 | | | | | | | | | | | | | | | | | | | | | | | | | |
| 12 | | | | | | | | | | | | | | | | | | | | | | | | | |
| 10 | | | | | | | | | | | | | | | | | | | | | | | | | |
| 08 | | | | | | | | | | | | | | | | | | | | | | | | | |
| 06 | | | | | | | | | | | | | | | | | | | | | | | | | |
| 04 | | | | | | | | | | | | | | | | | | | | | | | | | |
| 02 | | | | | | | | | | | | | | | | | | | | | | | | | |

VERIFICATION COMPLETED BY: P.O. Tession DATE: 5/31/79 APPROVED BY: William C. D... DATE: 6/1/79
Robert Halliburton TIME: 10:20 DATE: 5/31/79 TIME: 0800
TIME: 70:20

2.0 SHUTDOWN MARGIN TEST

Abstract

The purpose of the test is to demonstrate that the reactor can be made subcritical with a shutdown margin of 0.25 percent delta K at anytime in the cycle with the strongest operable rod fully withdrawn.

The shutdown margin test was performed in accordance with the Reactor Physics Surveillance Procedure No. 4, Reactivity Margin-Core Loading. With the core in its most reactive condition, cold and Xenon free, the strongest control rod was fully withdrawn from the core. A second control rod was withdrawn to a position which inserted an amount of reactivity at least equal to the required margin of 0.25 percent Delta K.

Test Result

Figure 2.1 summarizes the results of the shutdown margin test. Control rod 26-31, shown analytically to be the strongest, was fully withdrawn from the core. Control rod 22-35 was then withdrawn to position 08 which analytically resulted in an insertion of approximately 0.50 percent Delta K. As shown on Figure 2.1, the reactor remained subcritical throughout the test. Results of the test are within the criteria specified in the Technical Specifications.

Figure 2.1

Reactivity Margin - Core Loading

Procedure:

1. All Rods In

| | | | | |
|----------|----|----|----|----|
| SRM | 11 | 12 | 13 | 14 |
| Readings | 9 | 10 | 9 | 15 |

2. Rod CR1 26-31 selected

3. Rod CR1 26-31 to position 48, coupling check verified

4. Reactor Subcritical

| | | | | |
|----------|----|----|----|----|
| SRM | 11 | 12 | 13 | 14 |
| Readings | 13 | 10 | 9 | 15 |

5. Rod CR2 22-35 selected

6. Rod CR2 22-35 to position 08

7. Reactor Subcritical

| | | | | |
|----------|----|----|----|----|
| SRM | 11 | 12 | 13 | 14 |
| Readings | 17 | 11 | 9 | 17 |

3.0 Control Rod Drive Scram Time Test

Abstract

The purpose of this test is to demonstrate that the requirements of the Technical Specifications are met prior to power operation.

The control rod drive scram time test was performed in accordance with the Reactor Analyst Procedure No. N1-RAP-3, Full Core Control Rod Scram Timing Sequence. Each control rod was individually scrambled. A recording was made of control blade position versus time. From these recordings, the average scram insertion time corresponding to 5, 20, 50, and 90 percent insertion into the core was obtained.

Test Result

Figure 3.1 contains the results of the control rod drive scram time test. Results of the test are within the values specified by the Technical Specifications (see figure 3.2).

Figure 3.1

NINE MILE POINT UNIT 1
CONTROL ROD SCRAM TIME DATA

DATE JUN 1979

| ROD NO. | LOCATION X-Y | SCRAM TIME DATA | | | |
|---------|--------------|-----------------|-------|-------|-------|
| | | 5% | 20% | 50% | 90% |
| 1 | 18- 3 | 0.370 | 0.800 | 1.710 | 2.900 |
| 2 | 22- 3 | 0.360 | 0.780 | 1.640 | 2.790 |
| 3 | 26- 3 | 0.380 | 0.820 | 1.680 | 2.840 |
| 4 | 30- 3 | 0.360 | 0.780 | 1.620 | 2.700 |
| 5 | 34- 3 | 0.375 | 0.830 | 1.880 | 3.270 |
| 6 | 14- 7 | 0.350 | 0.750 | 1.540 | 2.600 |
| 7 | 18- 7 | 0.375 | 0.735 | 1.575 | 2.660 |
| 8 | 22- 7 | 0.375 | 0.810 | 1.690 | 2.810 |
| 9 | 26- 7 | 0.350 | 0.770 | 1.610 | 2.710 |
| 10 | 30- 7 | 0.350 | 0.800 | 1.700 | 2.820 |
| 11 | 34- 7 | 0.340 | 0.710 | 1.580 | 2.780 |
| 12 | 38- 7 | 0.365 | 0.775 | 1.670 | 2.825 |
| 13 | 10-11 | 0.370 | 0.840 | 1.750 | 2.940 |
| 14 | 14-11 | 0.380 | 0.800 | 1.660 | 2.790 |
| 15 | 18-11 | 0.360 | 0.780 | 1.610 | 2.695 |
| 16 | 22-11 | 0.350 | 0.785 | 1.675 | 2.850 |
| 17 | 26-11 | 0.360 | 0.780 | 1.660 | 2.810 |
| 18 | 30-11 | 0.365 | 0.820 | 1.730 | 2.915 |
| 19 | 34-11 | 0.365 | 0.780 | 1.620 | 2.730 |
| 20 | 38-11 | 0.350 | 0.770 | 1.640 | 2.780 |
| 21 | 42-11 | 0.355 | 0.800 | 1.665 | 2.815 |
| 22 | 6-15 | 0.360 | 0.820 | 1.760 | 2.980 |
| 23 | 10-15 | 0.365 | 0.750 | 1.700 | 3.140 |
| 24 | 14-15 | 0.370 | 0.790 | 1.650 | 2.770 |
| 25 | 18-15 | 0.340 | 0.790 | 1.700 | 2.920 |
| 26 | 22-15 | 0.345 | 0.775 | 1.620 | 2.710 |
| 27 | 26-15 | 0.375 | 0.795 | 1.660 | 2.820 |
| 28 | 30-15 | 0.360 | 0.720 | 1.500 | 2.550 |
| 29 | 34-15 | 0.360 | 0.815 | 1.780 | 3.040 |
| 30 | 38-15 | 0.335 | 0.805 | 1.780 | 3.060 |
| 31 | 42-15 | 0.370 | 0.800 | 1.670 | 2.830 |
| 32 | 46-15 | 0.360 | 0.800 | 1.620 | 2.840 |
| 33 | 2-19 | 0.360 | 0.760 | 1.565 | 2.650 |
| 34 | 6-19 | 0.350 | 0.770 | 1.600 | 2.650 |
| 35 | 10-19 | 0.360 | 0.780 | 1.640 | 2.760 |
| 36 | 14-19 | 0.330 | 0.700 | 1.420 | 2.390 |
| 37 | 18-19 | 0.370 | 0.800 | 1.665 | 2.780 |
| 38 | 22-19 | 0.380 | 0.830 | 1.700 | 2.845 |
| 39 | 26-19 | 0.380 | 0.830 | 1.710 | 2.870 |
| 40 | 30-19 | 0.360 | 0.770 | 1.590 | 2.665 |
| 41 | 34-19 | 0.360 | 0.730 | 1.470 | 2.460 |
| 42 | 38-19 | 0.365 | 0.800 | 1.660 | 2.810 |
| 43 | 42-19 | 0.380 | 0.850 | 1.780 | 3.010 |
| 44 | 46-19 | 0.375 | 0.790 | 1.620 | 2.720 |
| 45 | 50-19 | 0.380 | 0.800 | 1.640 | 2.750 |
| 46 | 2-23 | 0.370 | 0.810 | 1.740 | 2.870 |
| 47 | 6-23 | 0.380 | 0.815 | 1.660 | 2.770 |
| 48 | 10-23 | 0.350 | 0.780 | 1.640 | 2.780 |
| 49 | 14-23 | 0.365 | 0.755 | 1.550 | 2.560 |
| 50 | 18-23 | 0.350 | 0.790 | 1.680 | 2.880 |

Figure 1 (Continued)

NINE MILE POINT UNIT 1
CONTROL ROD SCRAM TIME DATA

DATE JUN 1979

| ROD NO. | LOCATION X-Y | SCRAM TIME DATA | | | |
|---------|--------------|-----------------|-------|-------|-------|
| | | 5% | 20% | 50% | 90% |
| 51 | 22-23 | 0.380 | 0.830 | 1.780 | 3.050 |
| 52 | 26-23 | 0.350 | 0.780 | 1.630 | 2.750 |
| 53 | 30-23 | 0.340 | 0.790 | 1.620 | 2.750 |
| 54 | 34-23 | 0.370 | 0.810 | 1.675 | 2.885 |
| 55 | 38-23 | 0.365 | 0.800 | 1.660 | 2.785 |
| 56 | 42-23 | 0.370 | 0.785 | 1.640 | 2.740 |
| 57 | 46-23 | 0.370 | 0.750 | 1.650 | 2.820 |
| 58 | 50-23 | 0.370 | 0.765 | 1.580 | 2.680 |
| 59 | 2-27 | 0.360 | 0.775 | 1.615 | 2.720 |
| 60 | 6-27 | 0.360 | 0.800 | 1.680 | 2.820 |
| 61 | 10-27 | 0.375 | 0.840 | 1.770 | 3.000 |
| 62 | 14-27 | 0.370 | 0.840 | 1.800 | 3.050 |
| 63 | 18-27 | 0.375 | 0.835 | 1.755 | 2.955 |
| 64 | 22-27 | 0.360 | 0.765 | 1.595 | 2.670 |
| 65 | 26-27 | 0.350 | 0.710 | 1.420 | 2.360 |
| 66 | 30-27 | 0.300 | 0.770 | 1.680 | 2.910 |
| 67 | 34-27 | 0.320 | 0.740 | 1.550 | 2.650 |
| 68 | 38-27 | 0.380 | 0.815 | 1.715 | 2.880 |
| 69 | 42-27 | 0.360 | 0.800 | 1.660 | 2.800 |
| 70 | 46-27 | 0.370 | 0.810 | 1.700 | 2.830 |
| 71 | 50-27 | 0.350 | 0.770 | 1.615 | 2.750 |
| 72 | 2-31 | 0.330 | 0.740 | 1.530 | 2.560 |
| 73 | 6-31 | 0.370 | 0.835 | 1.720 | 2.920 |
| 74 | 10-31 | 0.340 | 0.740 | 1.560 | 2.600 |
| 75 | 14-31 | 0.360 | 0.840 | 1.760 | 2.960 |
| 76 | 18-31 | 0.350 | 0.780 | 1.660 | 2.830 |
| 77 | 22-31 | 0.370 | 0.720 | 1.440 | 2.380 |
| 78 | 26-31 | 0.340 | 0.675 | 1.395 | 2.375 |
| 79 | 30-31 | 0.350 | 0.780 | 1.610 | 2.730 |
| 80 | 34-31 | 0.370 | 0.750 | 1.550 | 2.585 |
| 81 | 38-31 | 0.350 | 0.720 | 1.450 | 2.420 |
| 82 | 42-31 | 0.360 | 0.750 | 1.575 | 2.620 |
| 83 | 46-31 | 0.360 | 0.840 | 1.775 | 2.965 |
| 84 | 50-31 | 0.370 | 0.800 | 1.680 | 2.820 |
| 85 | 2-35 | 0.360 | 0.780 | 1.645 | 2.790 |
| 86 | 6-35 | 0.370 | 0.800 | 1.670 | 2.800 |
| 87 | 10-35 | 0.375 | 0.775 | 1.750 | 3.130 |
| 88 | 14-35 | 0.350 | 0.710 | 1.450 | 2.430 |
| 89 | 18-35 | 0.340 | 0.690 | 1.410 | 2.350 |
| 90 | 22-35 | 0.370 | 0.725 | 1.440 | 2.380 |
| 91 | 26-35 | 0.370 | 0.810 | 1.680 | 2.800 |
| 92 | 30-35 | 0.370 | 0.780 | 1.620 | 2.700 |
| 93 | 34-35 | 0.380 | 0.820 | 1.718 | 2.895 |
| 94 | 38-35 | 0.360 | 0.800 | 1.685 | 2.850 |
| 95 | 42-35 | 0.385 | 0.830 | 1.715 | 2.910 |
| 96 | 46-35 | 0.370 | 0.830 | 1.740 | 2.920 |
| 97 | 50-35 | 0.350 | 0.750 | 1.560 | 2.640 |
| 98 | 6-39 | 0.360 | 0.810 | 1.680 | 2.825 |
| 99 | 10-39 | 0.380 | 0.820 | 1.710 | 2.860 |
| 100 | 14-39 | 0.370 | 0.780 | 1.650 | 2.780 |

Figure 3.1 (Continued)

NINE MILE POINT UNIT 1
CONTROL ROD SCRAM TIME DATA

DATE JUN 1979

| ROD NO. | LOCATION X-Y | SCRAM TIME DATA | | | |
|------------|-----------------|-----------------|-------|-------|-------|
| | | 5% | 20% | 50% | 90% |
| 101 | 18-39 | 0.340 | 0.680 | 1.400 | 2.320 |
| 102 | 22-39 | 0.370 | 0.810 | 1.680 | 2.830 |
| 103 | 26-39 | 0.345 | 0.770 | 1.610 | 2.720 |
| 104 | 30-39 | 0.380 | 0.820 | 1.700 | 2.810 |
| 105 | 34-39 | 0.395 | 0.830 | 1.695 | 2.840 |
| 106 | 38-39 | 0.375 | 0.818 | 1.700 | 2.850 |
| 107 | 42-39 | 0.380 | 0.810 | 1.680 | 2.840 |
| 108 | 46-39 | 0.350 | 0.740 | 1.535 | 2.595 |
| 109 | 10-43 | 0.370 | 0.800 | 1.640 | 2.750 |
| 110 | 14-43 | 0.360 | 0.780 | 1.660 | 2.790 |
| 111 | 18-43 | 0.360 | 0.790 | 1.665 | 2.815 |
| 112 | 22-43 | 0.365 | 0.790 | 1.670 | 2.815 |
| 113 | 26-43 | 0.360 | 0.800 | 1.640 | 2.750 |
| 114 | 30-43 | 0.370 | 0.820 | 1.720 | 2.880 |
| 115 | 34-43 | 0.370 | 0.815 | 1.720 | 2.890 |
| 116 | 38-43 | 0.370 | 0.780 | 1.600 | 2.680 |
| 117 | 42-43 | 0.375 | 0.805 | 1.680 | 2.830 |
| 118 | 14-47 | 0.355 | 0.760 | 1.595 | 2.680 |
| 119 | 18-47 | 0.365 | 0.830 | 1.765 | 2.980 |
| 120 | 22-47 | 0.370 | 0.760 | 1.550 | 2.600 |
| 121 | 26-47 | 0.345 | 0.760 | 1.590 | 2.680 |
| 122 | 30-47 | 0.350 | 0.770 | 1.600 | 2.675 |
| 123 | 34-47 | 0.350 | 0.760 | 1.560 | 2.720 |
| 124 | 38-47 | 0.330 | 0.720 | 1.490 | 2.510 |
| 125 | 18-51 | 0.350 | 0.750 | 1.570 | 2.660 |
| 126 | 22-51 | 0.385 | 0.835 | 1.725 | 2.870 |
| 127 | 26-51 | 0.360 | 0.770 | 1.620 | 2.740 |
| 128 | 30-51 | 0.380 | 0.800 | 1.680 | 2.825 |
| 129 | 34-51 | 0.365 | 0.780 | 1.595 | 2.690 |

Figure 3.2

NINE MILE POINT UNIT 1
AVERAGE SCRAM INSERTION TIME COMPARISONS
DATE JUN 1979

| % INSERTED FROM FULLY WITHDRAWN | AVERAGE SCRAM INSERTION TIME(SEC) | TECH SPEC LIMIT (SEC) |
|---------------------------------------|---|-----------------------------|
| 5 | 0.362 | 0.375 |
| 20 | 0.784 | 0.900 |
| 50 | 1.641 | 2.000 |
| 90 | 2.769 | 5.000 |

4.0 Cold Critical Comparison With Actual Measurement

Abstract

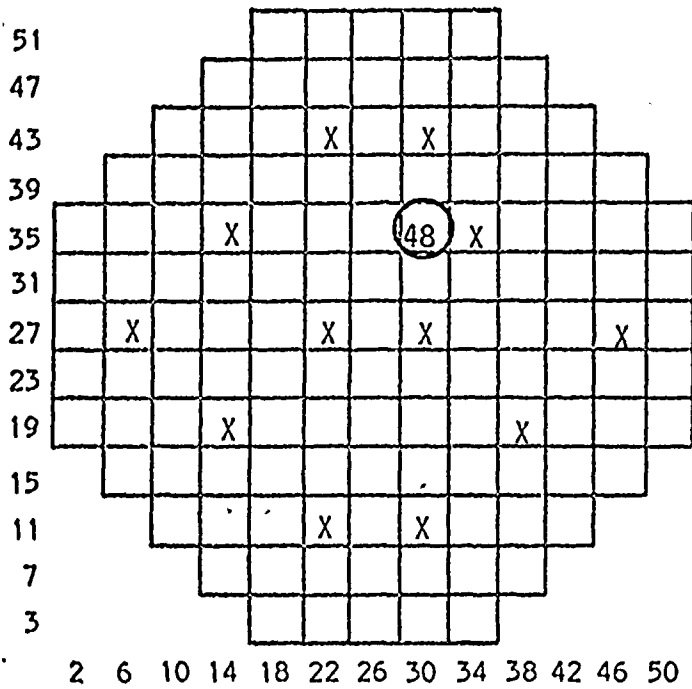
The purpose of this test is to demonstrate that the requirements of the Technical Specifications are met.

The cold critical comparison with actual measurements was performed in accordance with the Reactor Physics Surveillance Procedure No. N1-RPSP-3, Reactivity Anomalies. A beginning of Cycle 6 critical control rod pattern was determined (see figure 4.1). The actual critical control rod pattern should not exceed the equivalent of +1 percent in reactivity.

Test Report

The actual beginning of cycle 6 critical control rod pattern is shown on figure 4.2. Results of the test are within the value specified by the Technical Specifications (see figure 4.3).

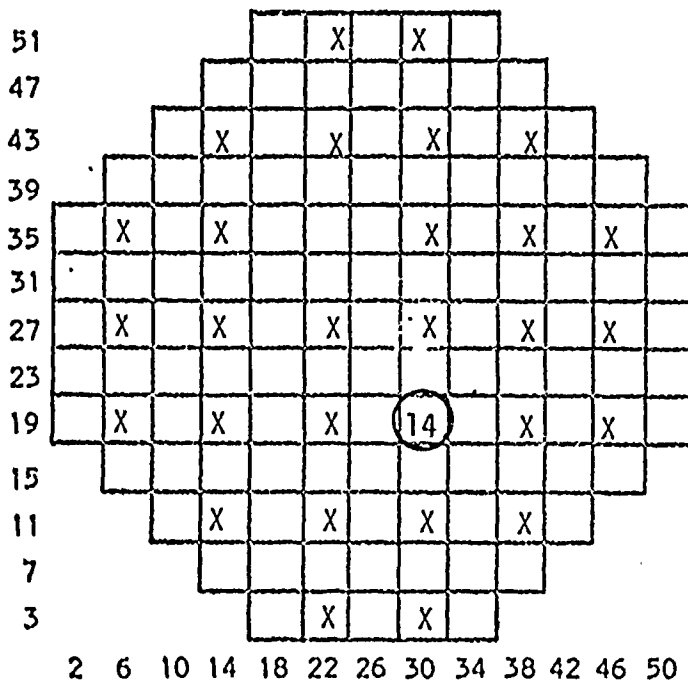
COLD CRITICAL CONTROL ROD PATTERN
 X= POSITION 48



Predicted In-sequence Critical

624 notches withdrawn
 Temperature: 68°F

Figure 4.1



Actual In-sequence Critical

1358 notches withdrawn
 Temperature: 142°F

Figure 4.2

Figure 4.3

Cold Critical Technical Specification Requirements

| | <u>Notches Withdrawn</u> |
|-------------------|------------------------------|
| +1% ΔK | 1444 |
| Predicted Cycle 6 | 624 |
| Actual Cycle 6 | 1358 |
| -1% ΔK | 480 |

5.0 TIP Uncertainty Calculation

Abstract

The purpose of this test is to ascertain the TIP uncertainty.

The TIP uncertainty calculation was performed in accordance with Reactor Core Parameter Calculation Procedure No. N1-RCPCP-18, TIP Uncertainty Calculation. TIP uncertainty consists of a random noise component and a geometric component. Measurements of the components were obtained by taking repetitive TIP readings at TIP locations which are symmetrical about the core diagonal of fuel loaded symmetrically.

Test Result

The total TIP uncertainty was calculated from the TIP data. The results of the calculation are shown on figure 5.1. The results are within the total TIP uncertainty criterion of 9 percent.

Figure 5.1

Nine Mile Point Unit 1 Cycle 6
TIP Uncertainty Calculation Results

| | |
|--------------------------------|-------|
| Total TIP Uncertainty - | 3.25% |
| TIP Random Noise Uncertainty - | 2.79% |
| TIP Geometric Uncertainty - | 1.67% |

1000

1000