

ENCLOSURE

CORE OPERATING LIMITS REPORT
DIABLO CANYON POWER PLANT
UNIT 2 CYCLE 7

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PACIFIC GAS AND ELECTRIC COMPANY
NUCLEAR POWER GENERATION
DIABLO CANYON POWER PLANT
CORE OPERATING LIMITS REPORT

DCPP
FOR
INFORMATION
ONLY

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REVISION 0
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TITLE: COLR FOR DIABLO CANYON UNIT 2 CYCLE 7

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APPROVED:

M. J. James

10/21/94
DATE

10/21/94
EFFECTIVE DATE

PROCEDURE CLASSIFICATION: QUALITY RELATED

1.0 CORE OPERATING LIMITS REPORT

This Core Operating Limits Report (COLR) for Diablo Canyon Unit 2 Cycle 7 has been prepared in accordance with the requirements of Technical Specification (TS) 6.9.1.8.

The Technical Specifications affected by this report are listed below:

- 3/4.1.3.5 - Shutdown Rod Insertion Limit
- 3/4.1.3.6 - Control Rod Insertion Limits
- 3/4.2.1 - Axial Flux Difference
- 3/4.2.2 - Heat Flux Hot Channel Factor - $F_0(z)$
- 3/4.2.3 - RCS Flow Rate and Nuclear Enthalpy Rise Hot Channel Factor

2.0 OPERATING LIMITS

The cycle-specific parameter limits for the specifications listed in Section 1.0 are presented in the following subsections. These limits have been developed using the NRC-approved methodologies specified in Technical Specification 6.9.1.8.

2.1 Shutdown Rod Insertion Limit (TS 3/4.1.3.5)

2.1.1 The shutdown rods shall be withdrawn to at least 225 steps.

2.2 Control Rod Insertion Limits (TS 3/4.1.3.6)

2.2.1 The control rod banks shall be limited in physical insertion as shown in Figure 1.

2.3 Axial Flux Difference (TS 3/4.2.1)

2.3.1 The AXIAL FLUX DIFFERENCE (AFD) Limits are provided in Figure 2.



2.4 Heat Flux Hot Channel Factor - $F_Q(z)$ (TS 3/4.2.2)

2.4.1

$$F_Q(z) < \frac{F_Q^{RTP}}{P} * K(z) \quad \text{for } P > 0.5$$

$$F_Q(z) \leq \frac{F_Q^{RTP}}{0.5} * K(z) \quad \text{for } P \leq 0.5$$

where: $P = \frac{\text{THERMAL POWER}}{\text{RATED THERMAL POWER}}$

$$F_Q^{RTP} = 2.45$$

$K(z)$ is provided in Figure 6.

2.4.2 The $W(z)$ curves for Specification 4.2.2.2.c Relaxed Axial Offset Control (RAOC) operation, provided in Figures 3 through 5, are sufficient to determine the RAOC $W(z)$ versus core height for Cycle 7 burnups through the end of full power reactivity plus a power coastdown of up to 1000 MWD/MTU.



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2.5 RCS Flow Rate and Nuclear Enthalpy Rise Hot Channel Factor
(Specification 3/4.2.3)

$$R = \frac{F_{\Delta H}^N}{F_{\Delta H}^{RTP} * [1 + PF_{\Delta H} * (1-P)]}$$

where: P = $\frac{\text{THERMAL POWER}}{\text{RATED THERMAL POWER}}$

$F_{\Delta H}^N$ = Measured values of $F_{\Delta H}^N$ obtained by using the movable
incore detectors to obtain a power distribution map

$F_{\Delta H}^{RTP} = 1.59$

$PF_{\Delta H} = 0.3$

3.0 FIGURES

- 3.1 Figure 1, Rod Bank Insertion Limits Versus Rated Thermal Power
- 3.2 Figure 2, AFD Limits as a Function of Rated Thermal Power
- 3.3 Figure 3, Load Follow $W(z)$ at 150 MWD/MTU as a Function of Core Height
- 3.4 Figure 4, Load Follow $W(z)$ at 10000 MWD/MTU as a Function of Core Height
- 3.5 Figure 5, Load Follow $W(z)$ at 18000 MWD/MTU as a Function of Core Height
- 3.6 Figure 6, $K(z)$ - Normalized $F_Q(z)$ as a Function of Core Height

4.0 RECORDS

None



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5.0 REFERENCES

Westinghouse Reload Safety Evaluation for Diablo Canyon Power Plant Unit 2
Cycle 7, Revision 2, dated October 1994.

6.0 SPONSOR

P.T. Nugent



(FULLY WITHDRAWN \geq 225 STEPS)

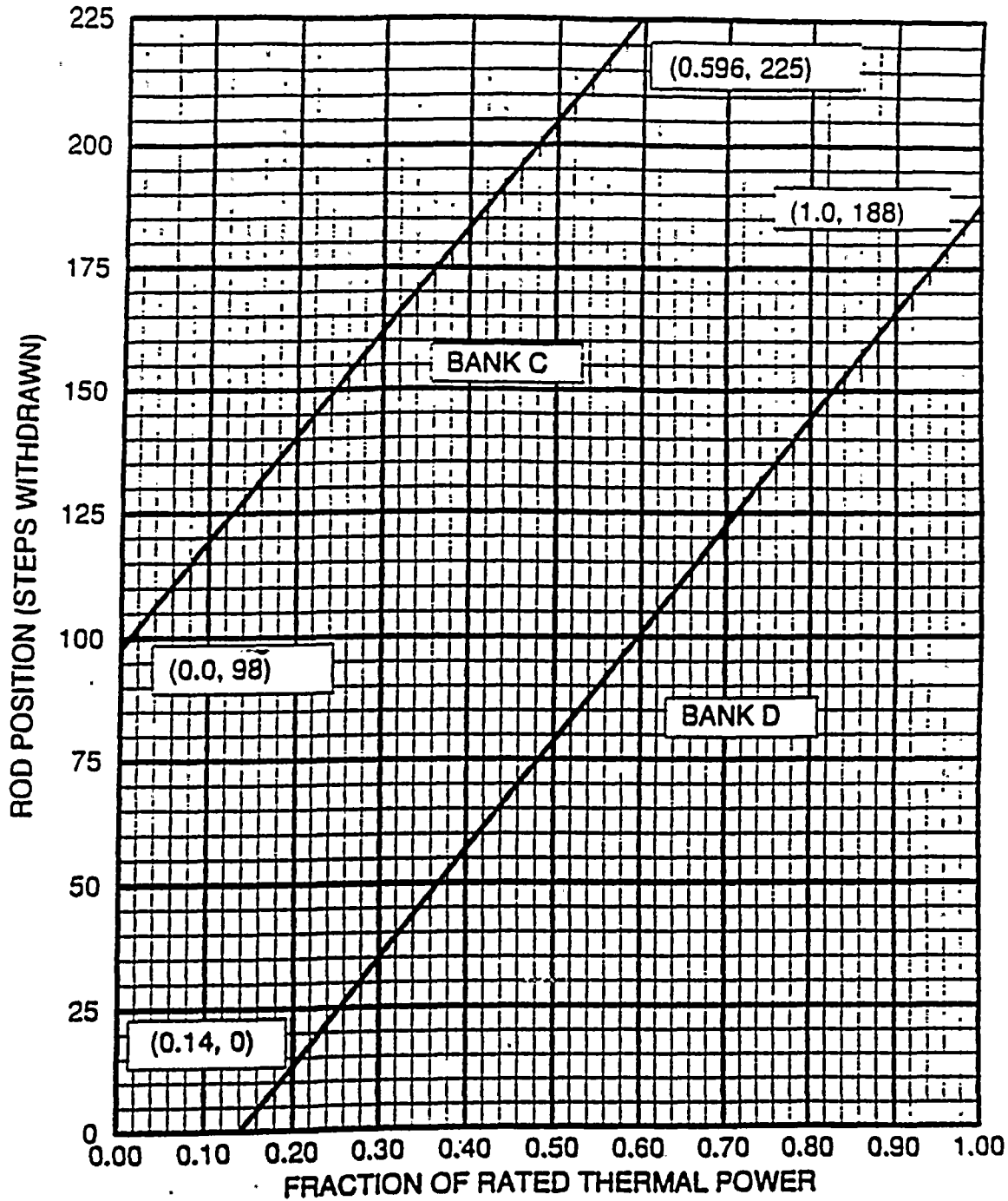


Figure 1

Rod Bank Insertion Limits Versus Rated Thermal Power



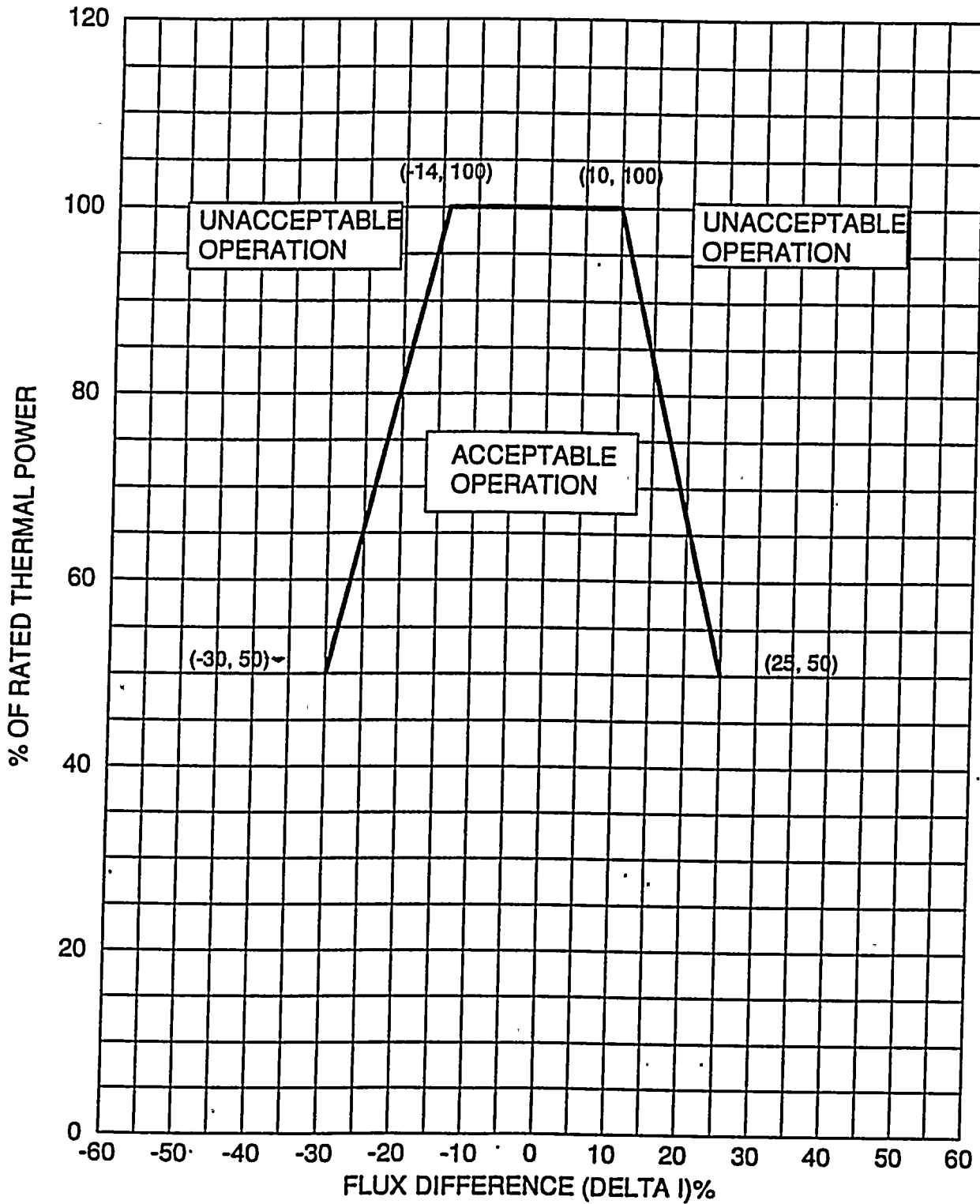
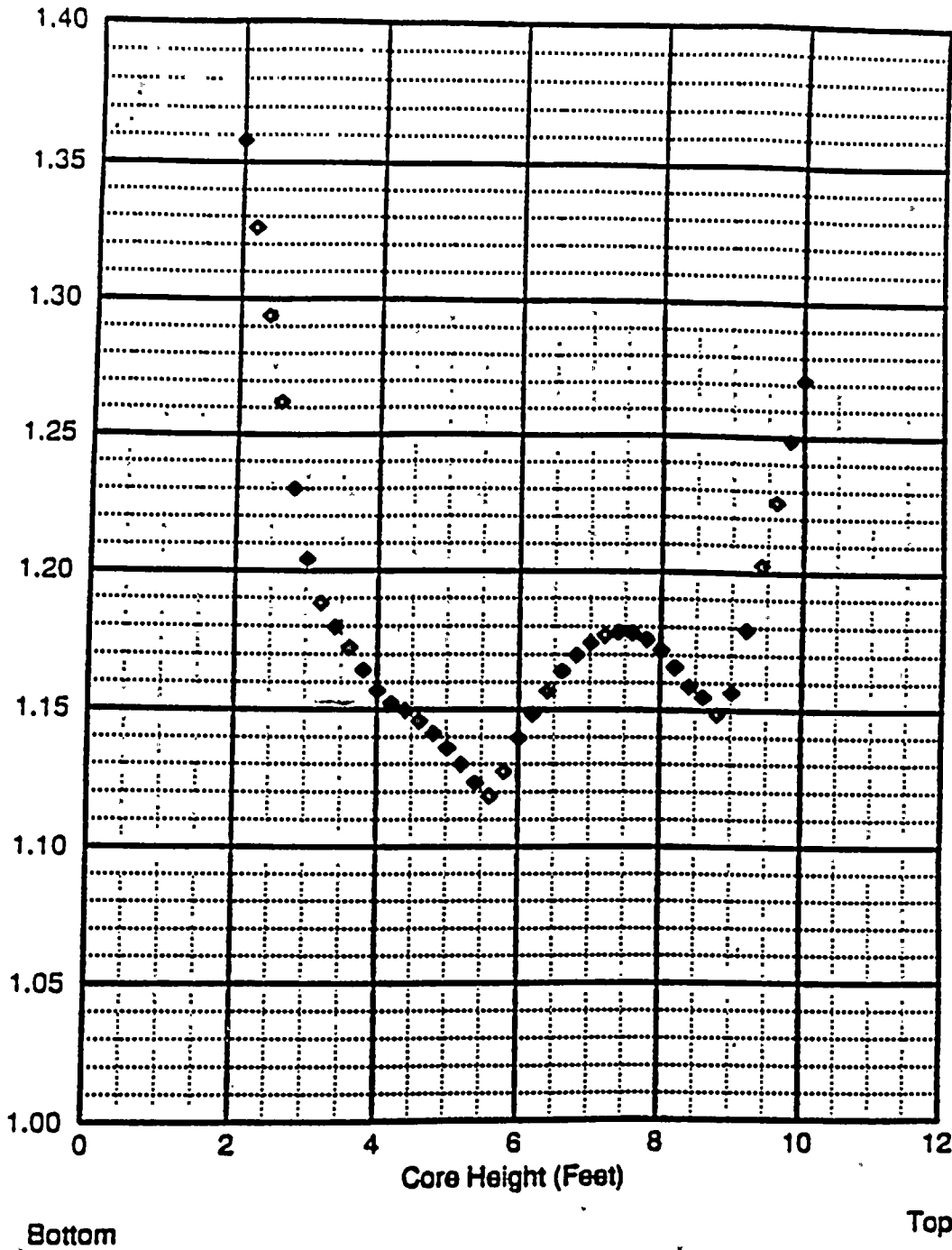


Figure 2

AFD Limits as a Function of Rated Thermal Power





HEIGHT 'FEET'	BCI W z
*0.0000	1.3000
*0.2000	1.3000
*0.4000	1.3000
*0.6000	1.3000
*0.8000	1.0000
*1.0000	1.3000
*1.2000	1.3000
*1.4000	1.3000
*1.6000	1.3000
*1.8000	1.3000
2.0000	1.3579
2.2000	1.3261
2.4000	1.2940
2.6000	1.2622
2.8000	1.2300
3.0000	1.2041
3.2000	1.1803
3.4000	1.1799
3.6000	1.1724
3.8000	1.1643
4.0000	1.1570
4.2000	1.1523
4.4000	1.1495
4.6000	1.1457
4.8000	1.1412
5.0000	1.1360
5.2000	1.1301
5.4000	1.1233
5.6000	1.1185
5.8000	1.1274
6.0000	1.1395
6.2000	1.1484
6.4000	1.1568
6.6000	1.1640
6.8000	1.1698
7.0000	1.1742
7.2000	1.1770
7.4000	1.1782
7.6000	1.1778
7.8000	1.1755
8.0000	1.1717
8.2000	1.1656
8.4000	1.1586
8.6000	1.1547
8.8000	1.1484
9.0000	1.1565
9.2000	1.1793
9.4000	1.2025
9.6000	1.2259
9.8000	1.2490
10.0000	1.2715
*10.2000	1.0000
*10.4000	1.0000
*10.6000	1.0000
*10.8000	1.0000
*11.0000	1.0000
*11.2000	1.0000
*11.4000	1.0000
*11.6000	1.0000
*11.8000	1.0000
*12.0000	1.0000

Figure 3

Load Follow W(z) at 150 MWD/MTU as a Function of Core Height

* Top and Bottom 15% excluded as per Technical Specification 4.2.2.2.g.



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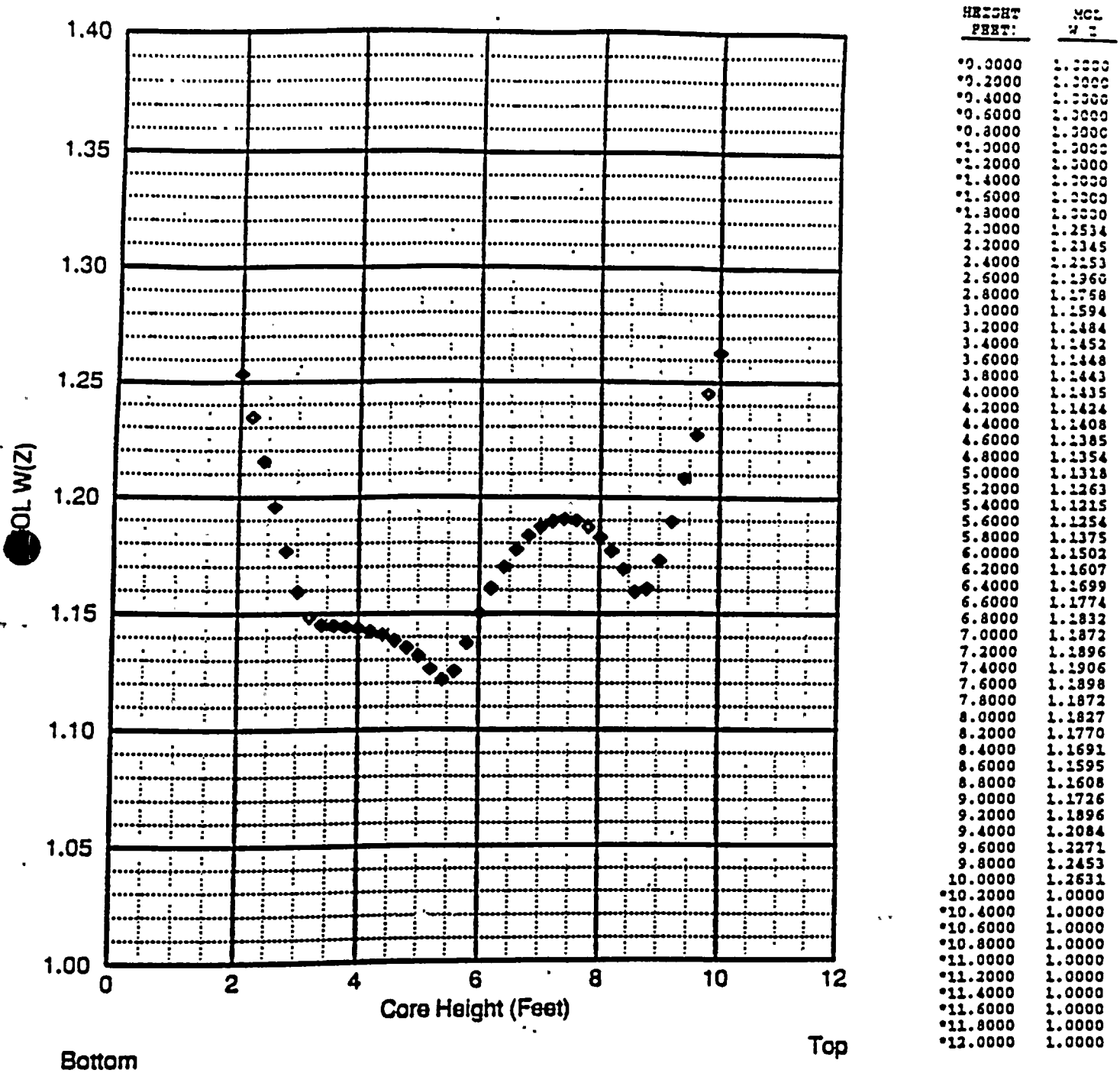


Figure 4

Load Follow W(z) at 10000 MWD/MTU as a Function of Core Height

* Top and Bottom 15% excluded as per Technical Specification 4.2.2.2.g.



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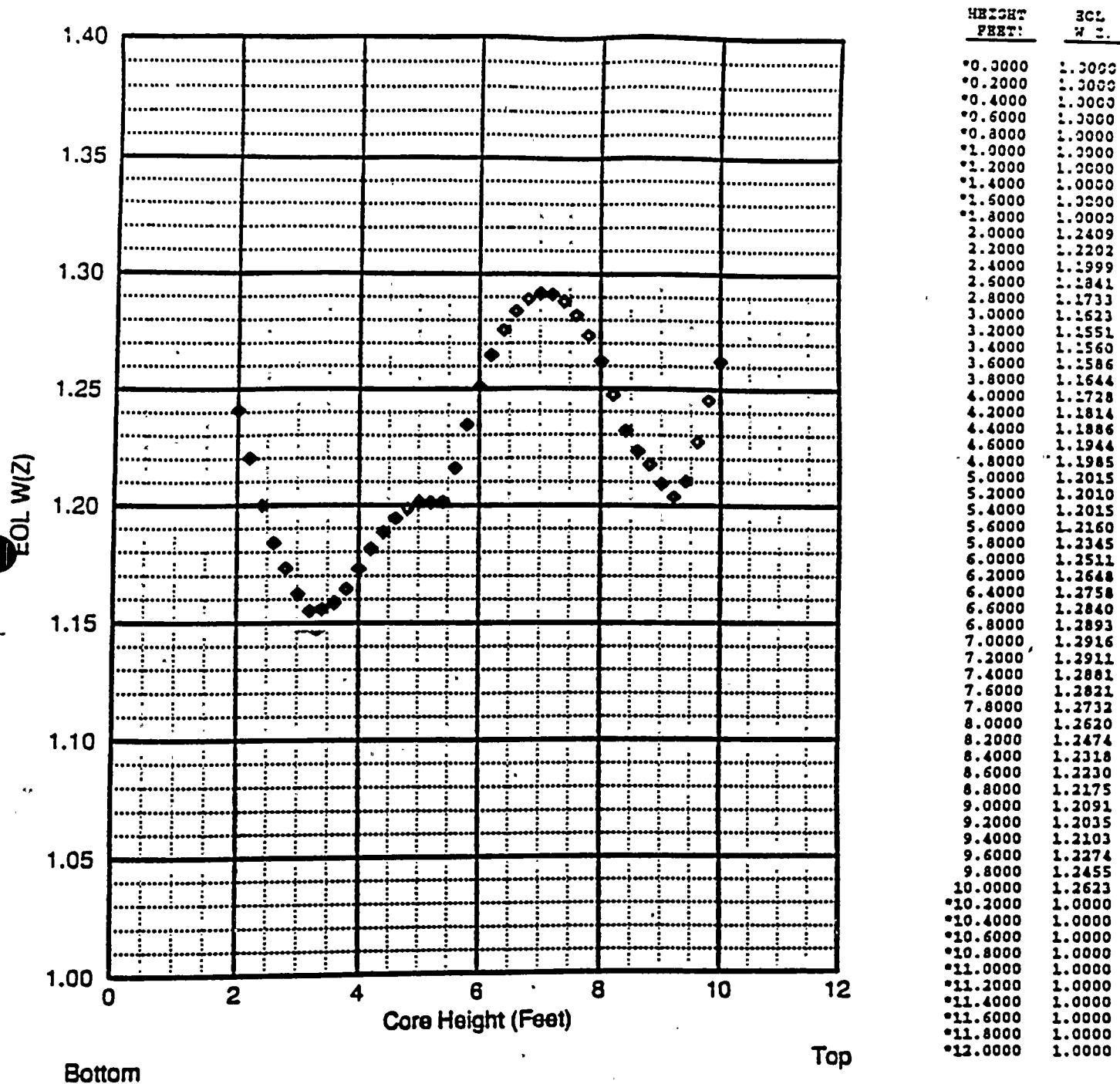
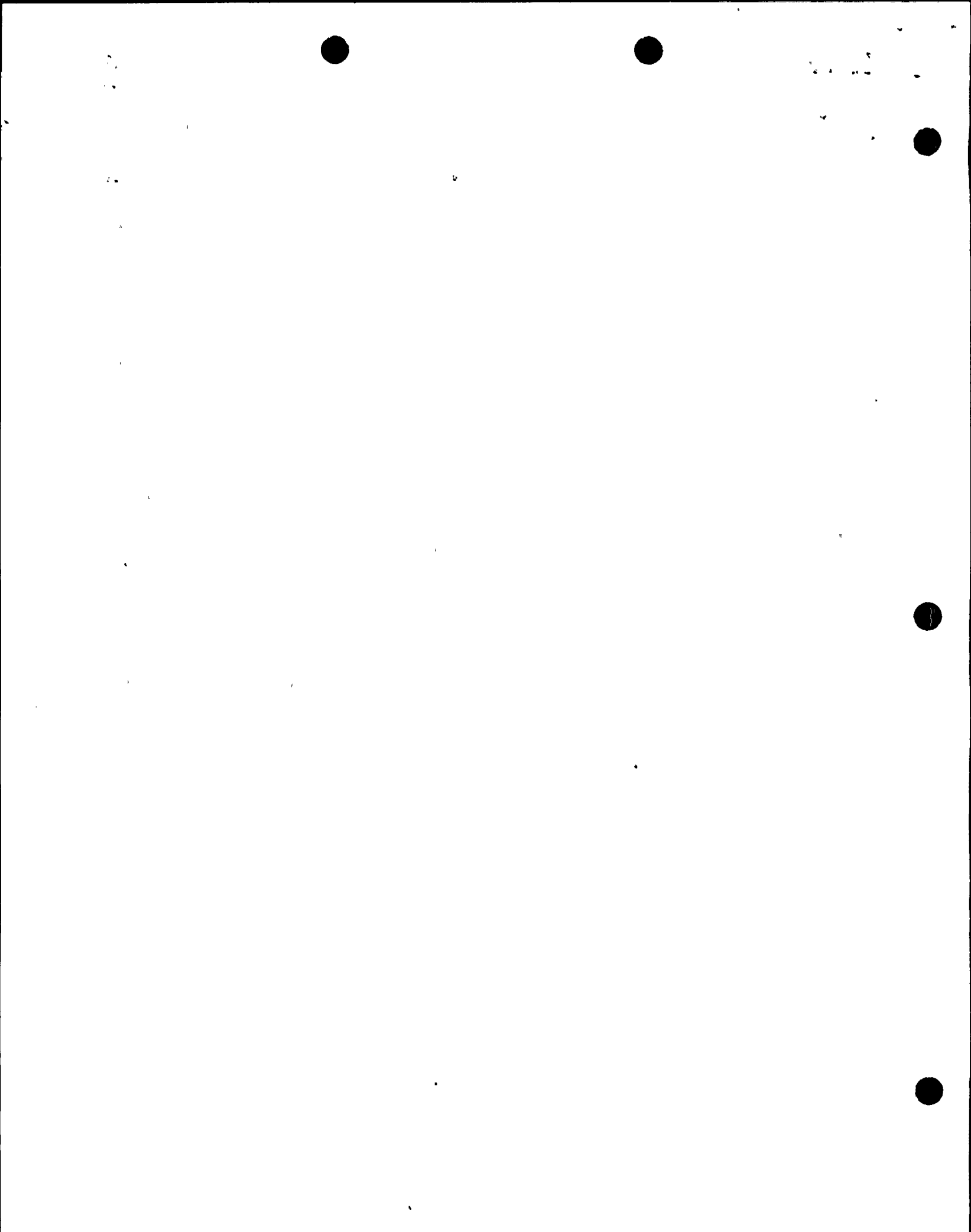


Figure 5

Load Follow W(z) at 18000 MWD/MTU as a Function of Core Height

* Top and Bottom 15% excluded as per Technical Specification 4.2.2.2.g.



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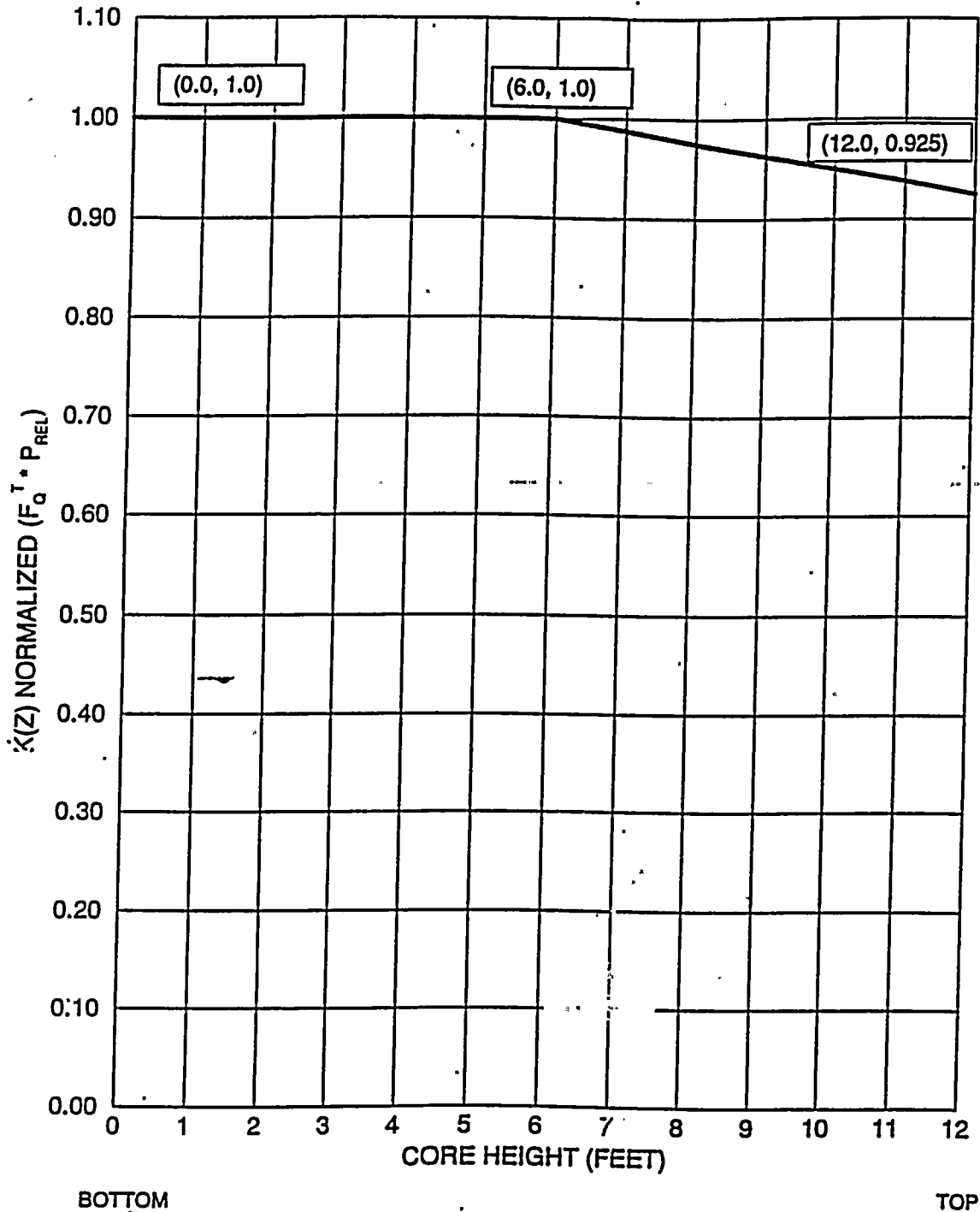


Figure 6

$K(z)$ - Normalized $F_Q(z)$ as a Function of Core Height

