

1 UNITED STATES OF AMERICA
2 ATOMIC ENERGY COMMISSION

3 DOCKET 50-323

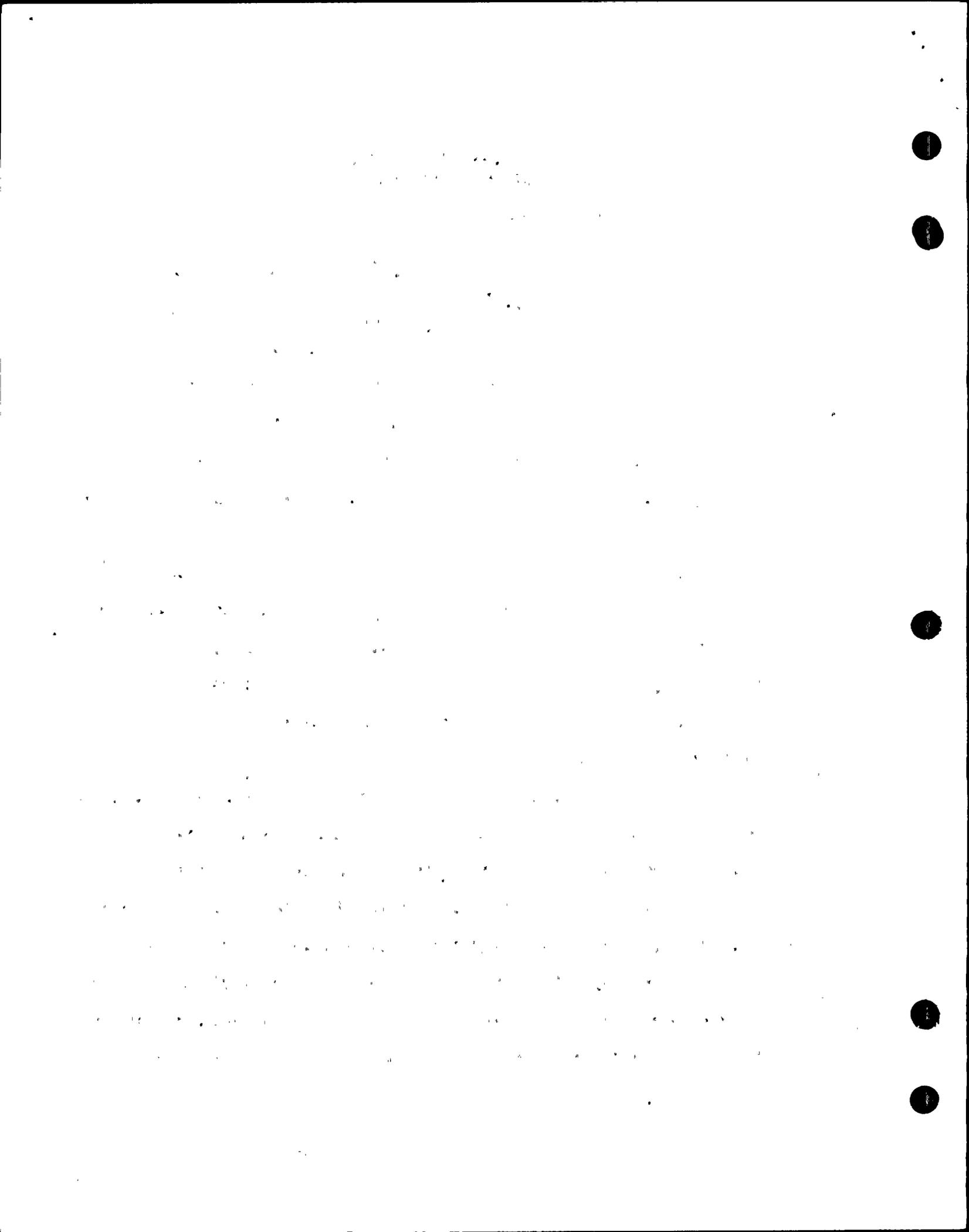
4 TESTIMONY OF WILLIAM J. LINDBLAD
5 ON BEHALF OF
6 PACIFIC GAS AND ELECTRIC COMPANY
7 SEPTEMBER __, 1973

8 My name is William J. Lindblad. I am the Project
9 Engineer for the Diablo Canyon Units 1 and 2, with responsibility
10 for directing the engineering activities of the project.

11 My business address is 77 Beale Street, San Francisco,
12 California 94106.

13 In general, my testimony covers a brief discussion of
14 the cooling water system of the Units and of various alternatives
15 thereto and why they were not adopted. In addition, I have in-
16 cluded a brief description of why two of the alternative energy
17 sources discussed in the consolidated petition to intervene are
18 not viable alternatives to the Diablo Units.

19 I am a graduate of the University of California College
20 of Engineering. I received the Bachelor of Science degree in
21 Electrical Engineering in 1951. I was then called to active duty
22 in the U. S. Navy, serving until 1954. In 1954, I joined PGandE
23 working in the technical operations groups of various steam-
24 electric generating stations. In 1956, I was transferred to the
25 Company's Department of Engineering where I have worked continu-
ously since, with increasing levels of responsibility for design



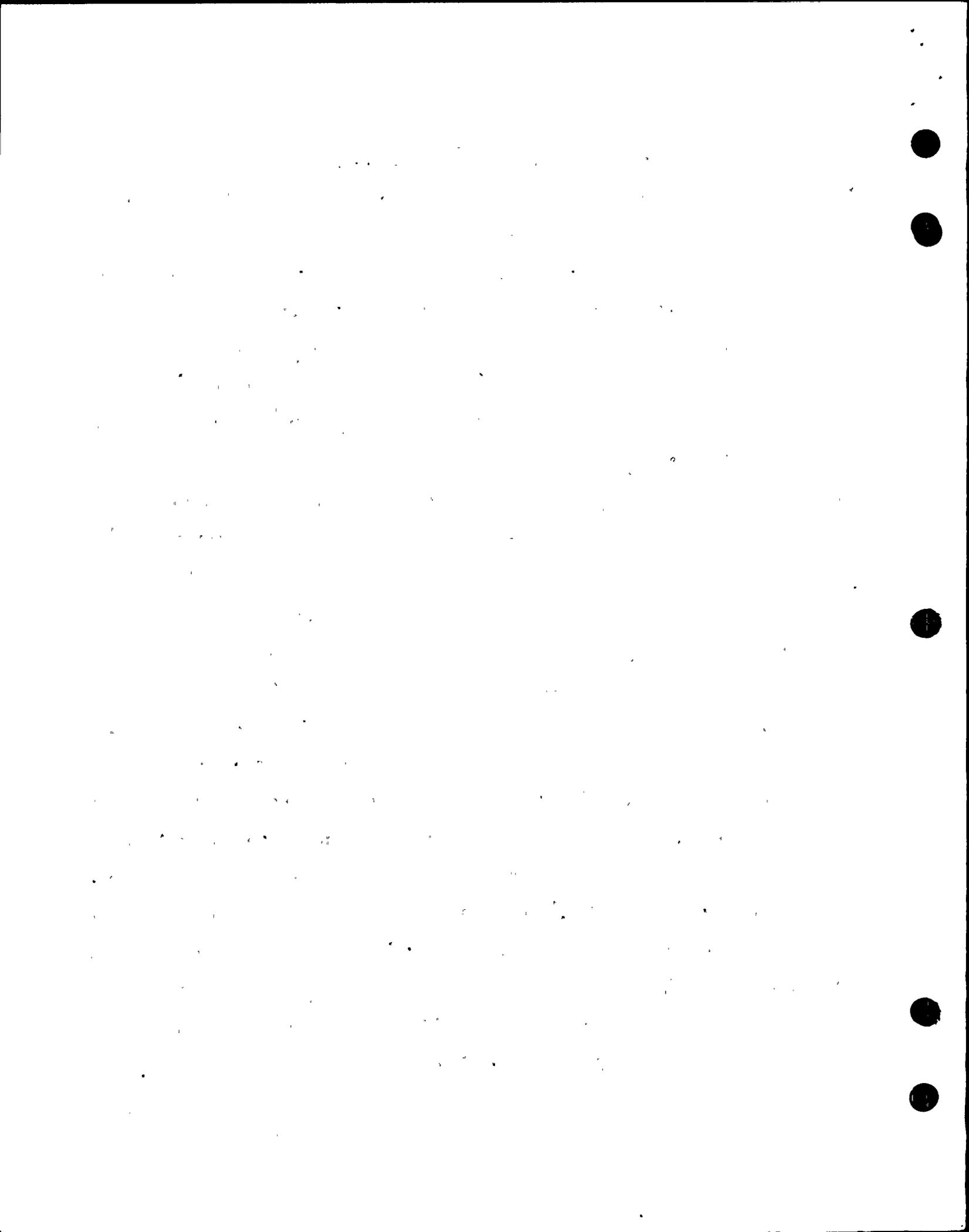
1 of fossil and nuclear fueled power plants.

2 My experience in nuclear power began in 1956 as the
3 Company's representative on the Nuclear Power Group study team,
4 which was related to the Company's participation in Commonwealth
5 Edison's Dresden Nuclear Power Station. I have been involved in
6 much of the Company's nuclear engineering activities since.
7 Beginning in 1966, I have devoted essentially full time to the
8 Diablo Canyon project. I was appointed to my present position
9 in January of 1972.

10 I am a member of the American Society of Mechanical
11 Engineers and of the Institute of Electrical and Electronic
12 Engineers.

13 I am a Professional Engineer, registered with the State
14 of California in the field of mechanical engineering.

15 Nuclear plants such as Diablo Units 1 and 2 will operate
16 with a thermal efficiency of about 32 percent, meaning that about
17 one-third of the heat released by the fission process in the re-
18 actor core is converted to electricity. The rest of the energy
19 is at too low a temperature to be efficiently converted to power
20 and must be rejected. Several methods of dissipating this heat
21 are available. After considering these methods, a once-through
22 ocean cooling system was selected. This means that ocean water
23 for cooling will be pumped through the plant from the cove located
24 to the south of Diablo Cove. Each unit has two circulating water
25 pumps capable of pumping 867,000 gallons per minute of seawater



1 from the intake structure through the two intake conduits to the
2 condensers. Facilities are installed in the intake for the pro-
3 tection of fish. As the water passes through the condenser, steam
4 from the turbine is condensed, and the waste heat transferred to
5 the circulating water.

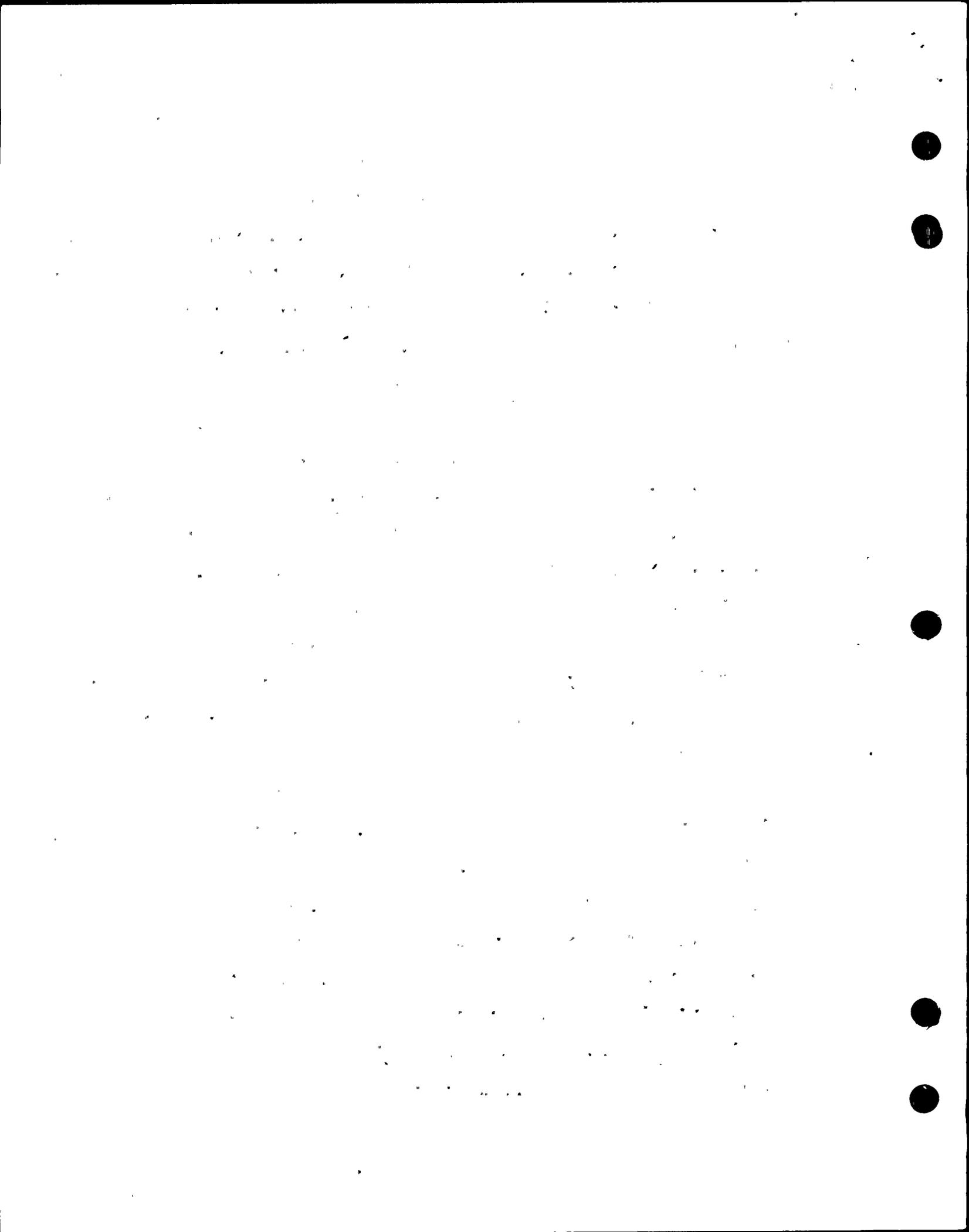
6 After leaving the condensers, the cooling water flows by
7 gravity through two discharge conduits to the discharge structure
8 located on the shoreline of Diablo Cove. Total travel time for
9 the circulating water from the intake to the discharge is approxi-
10 mately 4-1/2 minutes. The heated water returning to the ocean is
11 quickly mixed with the turbulent waters of the cove resulting in
12 limited exposures of the benthic and pelagic communities to
13 elevated temperatures.

14 It is PGandE's belief that the optimum medium, from an
15 environmental standpoint, for receiving waste heat from Diablo
16 Units 1 and 2 is the Pacific Ocean. Once-through cooling, using
17 the ocean water, is the least expensive alternative, will result
18 in the highest power plant efficiency, and requires the least
19 amount of land space. It does not create any obtrusive visual
20 impact on the landscape, and the thermal discharge causes no
21 significant adverse environmental effects. Possible alternatives
22 to the once-through cooling design include off-shore discharge,
23 several kinds of cooling towers, spray canals, and cooling ponds.
24 For the reasons outlined below each of these alternatives was
25 rejected.



1 An offshore discharge would carry the heated water out-
2 side Diablo Cove and dissipate the heat in deeper offshore waters.
3 This would be accomplished by extending the cooling water discharge
4 conduit from the shoreline to an area where the water depth would
5 permit a mixing of the heated water and the ambient ocean in the
6 vertical water column. The water depth required is dependent upon
7 the desired maximum water surface temperature rise, the number and
8 size of conduit discharge openings, and the velocity of water at
9 the discharge openings. For example, for two units the size of
10 the Diablo Units, to achieve a maximum surface temperature rise
11 of 4°F which is the temperature set by the State of California
12 thermal water standards, an offshore discharge could consist of
13 two 11-foot-diameter ports, with a 100-foot separation, discharg-
14 ing water horizontally at 20 feet per second at a depth of 45 feet.
15 Water at this depth is available approximately 1,700 feet offshore
16 from the present discharge structure.

17 A practical design of a discharge conduit to a point
18 1,700 feet offshore along the turbulent rocky coast probably would
19 require a submarine tunnel mined in the rock under Diablo Cove.
20 A buoyant flexible conduit would not be expected to survive the
21 wave action during the stormy weather and is not considered a
22 feasible alternative. A conduit laid in a trench along the bottom
23 of the cove would require a construction tramway over the water,
24 and could require a breakwater or a cofferdam. The extensive
25 construction and blasting required for a conduit-in-trench design



1 would involve a significant environmental impact in itself.

2 An approximate estimate of the cost of the tunneling
3 required is \$21,000,000. If tunneling under pressure were re-
4 quired, the cost would increase by as much as \$7,000,000. The
5 two exit ports must be drilled and set with the use of an offshore
6 drilling platform, and this is estimated to cost an additional
7 \$7,000,000. If detailed examination of the local area and heat
8 dispersion characteristics show a need for additional ports, the
9 cost for constructing these ports would be as much as \$14,000,000.
10 Thus, the total capital costs for an offshore discharge could
11 range from \$28,000,000 (without pressure, without additional
12 ports) to \$42,000,000 (with pressure, with additional ports).

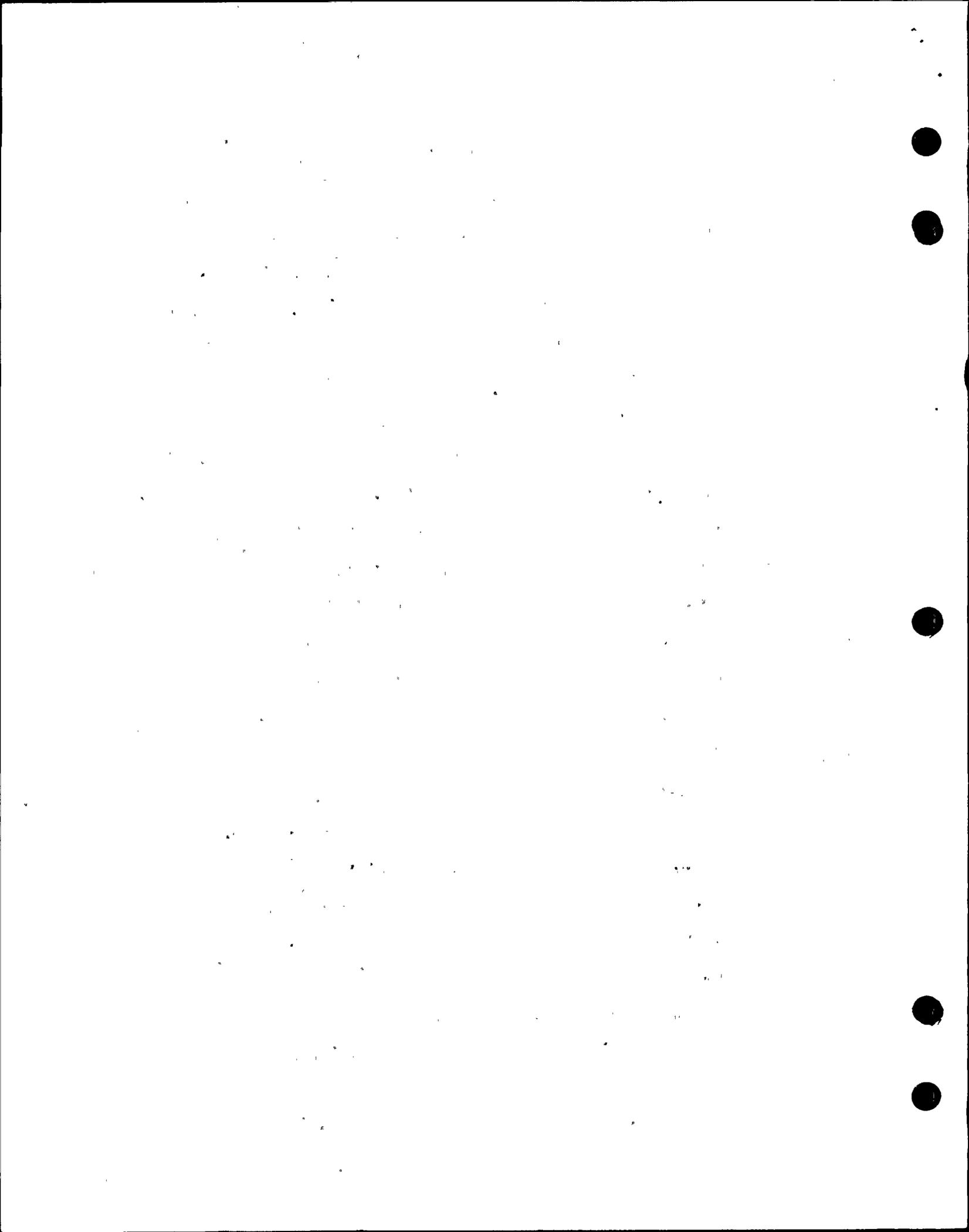
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 Alternatives to the once-through cooling system include
17 cooling towers, cooling ponds, and spray canals, all of which dis-
18 sipate heat to the atmosphere by evaporation. Cooling ponds also
19 dissipate a part of the heat through radiation and conduction.
20 In an evaporative cooling process, a closed cycle system (cooling
21 water recirculating between tower and condenser) would consume in
22 evaporation about 50,000 acre feet of water a year for the two
23 units at Diablo Canyon. These systems require an additional water
24 exchange to maintain the dissolved solids concentration below a
25 maximum limit. To maintain normal environmental quality within

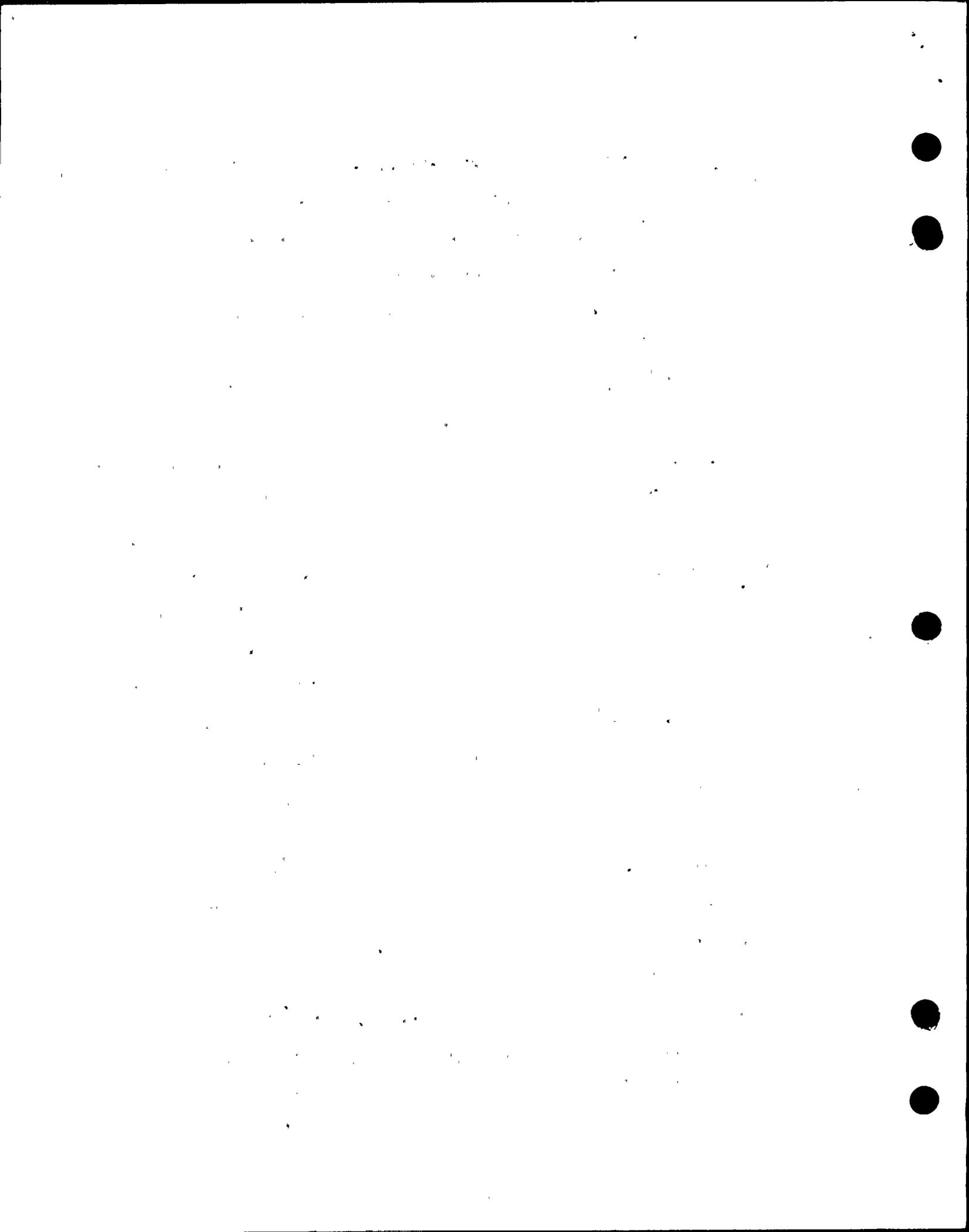


1 the system, fresh water is preferred. Fresh water in this quantity
2 is not available in the plant site region as indicated by State of
3 California, Department of Water Resources Bulletin No. 160-70. No
4 reclaimable water sources are present in the necessary quantity.
5 Therefore, only closed water systems using salt water have been
6 considered.

7 It is possible to use a cooling tower in conjunction
8 with a once-through cooling system to reduce the water temperature
9 before discharging the water back into the natural body of water.

10 At the Diablo Canyon Site, as opposed to inland sites, use of open
11 system towers of a reasonable size would not be of any significant
12 temperature-reducing benefit because the air wet bulb temperature
13 is usually about the same as or a little higher than the ocean
14 ambient temperature. In addition, the "helper" tower would give
15 rise to several adverse environmental effects associated with
16 saltwater cooling towers. These include principally damage to
17 structures and vegetation resulting from saltwater drift.

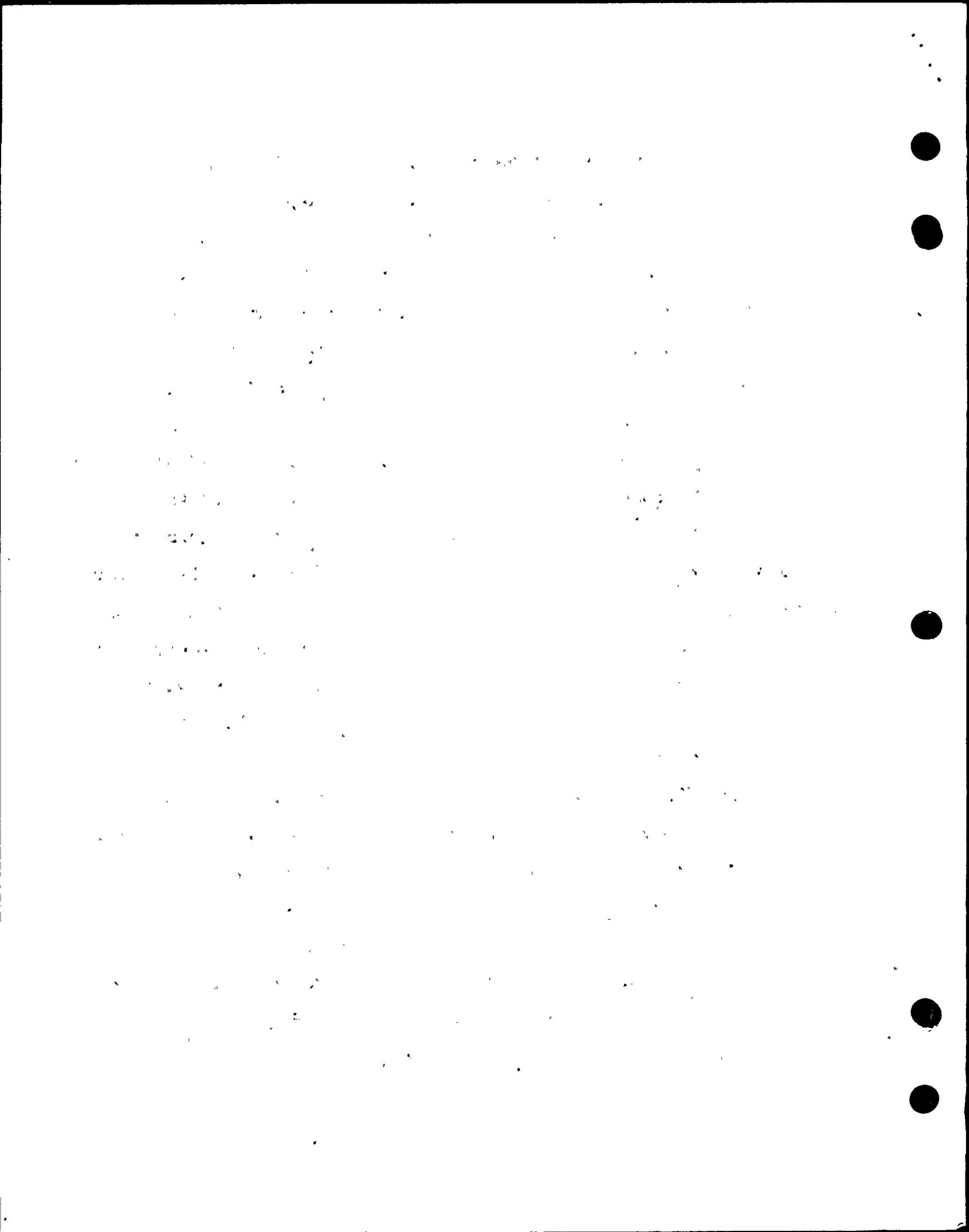
18 A closed cycle (recirculating) cooling tower system
19 using mechanical draft towers would require approximately 48
20 "cells" per unit, each cell typically 36 feet long, 51 feet wide,
21 and 49 feet high, with a 19-foot high stack over the fan. Twelve
22 of these cells would be in a row 432 feet long, with four such
23 rows required for each unit. The capital cost of a closed cycle
24 mechanical draft cooling tower system for Units 1 and 2 is esti-
25 mated at \$38,000,000. Maintenance of the system is estimated to



1 be \$350,000 annually. Reduction in turbine cycle efficiency re-
2 sults in a loss of capability of up to 85 megawatts during warm
3 periods with an additional penalty of 15 megawatts for cooling
4 tower fan requirements. The plant site would be limited to a
5 total of three units unless additional land could be obtained.

6 Natural draft towers dissipate heat in the same way as
7 the mechanical draft type but rely on the natural circulation of
8 the heated air through the tower rather than on fans. A natural
9 draft cooling tower arrangement is possible that would allow six
10 units. The tower for each unit would be at least 400 feet high
11 and more than 400 feet across the base. The capital cost of the
12 natural draft cooling tower system for Units 1 and 2 is estimated
13 at \$37,000,000. Maintenance of the system is estimated to be
14 \$300,000 annually. Reduction in turbine cycle efficiency results
15 in a loss of capability of up to 160 megawatts during warm periods.

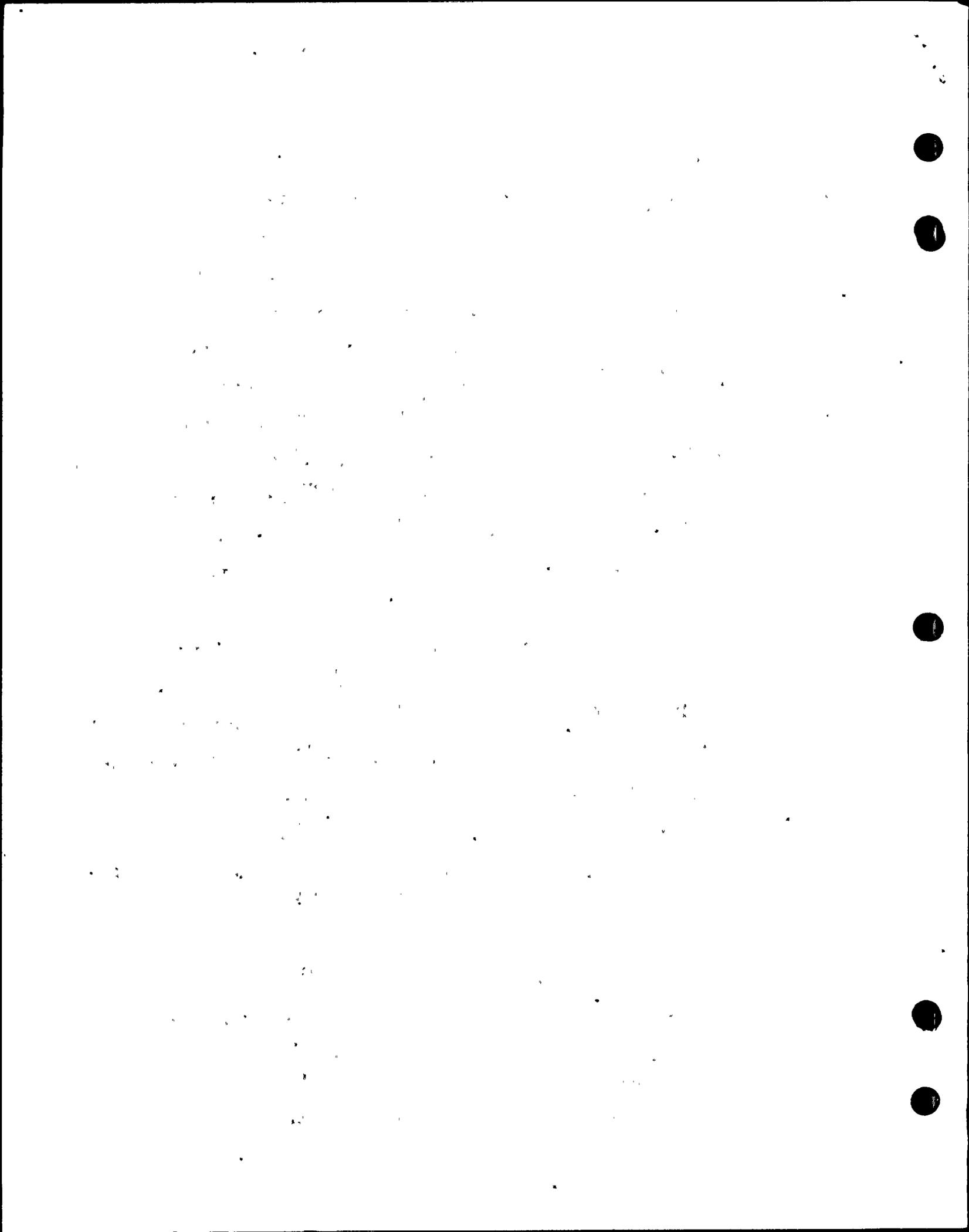
16 A dry cooling tower removes heat from the condenser in
17 a manner similar to an automobile radiator. Heat transfer occurs
18 by conduction and radiation to the air. Because the heat transfer
19 capacity of air is much less than that for water, large fin tube
20 areas are needed to remove the heat. In addition, the air dry
21 bulb temperature is the theoretical limit to which the condenser
22 water can be cooled, whereas the wet bulb temperature is the
23 theoretical limit for wet towers. In a practical size the ap-
24 proach to dry bulb in a dry tower may be 37-42°F. The condenser
25 inlet water temperature for a dry tower at the Diablo Canyon Site



1 during warm periods would be 108-113°F (71°F dry bulb plus the
2 37-42°F approach). This compares to the condenser inlet water
3 temperature of 78°F (63°F wet bulb plus 15°F approach) for the
4 evaporative cooling towers, and to 60°F for one-through ocean
5 cooling. The turbine back-pressure for condenser inlet tempera-
6 tures of 108-113°F would be about 5.5 inches of mercury absolute,
7 causing more than a 12 percent reduction of the plant's full load
8 power output and exhaust pressures and temperatures exceeding the
9 design of the turbines for the plant. Turbines of this size
10 compatible with dry cooling towers have not yet been developed.
11 The additional cost for dry towers is roughly 3-1/2 times the
12 additional cost of providing the same cooling using evaporative
13 natural draft cooling towers (Hauser 1971).

14 In short, we have rejected all cooling towers on the
15 grounds that they have a much greater adverse effect on the
16 environment than the cooling system proposed and that they cost
17 so much more than the proposed system. In addition, there are
18 technological objections to certain types of towers.

19 Topography will not permit the use of spray canals or
20 cooling ponds. The only land area that can accommodate a spray
21 canal is the coastal terrace south of the plant. Such an align-
22 ment parallels prevailing summer winds and, therefore, would not
23 work effectively as a heat transfer mechanism. Even if winds were
24 favorable, a canal for one unit would require 2.8 miles of terrace.
25 No space appears available for a spray canal for Unit 2 or



1 subsequent units.

2 Recirculating cooling ponds were investigated for the
3 Diablo Canyon Site. In cooling ponds the warm water from the
4 condensers is cooled by evaporation, conduction, and radiation to
5 the atmosphere. It was estimated that a pond size of 1,950 acres
6 would be required for cooling the thermal discharge of Units 1 and
7 2. The land required is not available at the site.

8 Turning now to some alternative energy sources fusion
9 energy is still in the early stages of development. The technical
10 questions involved in this process are highly complex and solutions
11 are not expected to be forthcoming for some time. A recent opti-
12 mistic announcement from the AEC indicated that a power plant
13 developing energy from the fusion process might be available during
14 the 1990's. This would be far too late to replace the Diablo
15 Canyon Units, which are required in 1975 and 1976.

16 Similarly, solar energy remains a potential source of
17 generation but not as an alternative to the Diablo Canyon Units.
18 The technology of using solar energy to generate electricity on
19 a scale the size of the Diablo Units simply has not yet been
20 developed. Furthermore, the environmental impact of at least
21 some of the schemes which have been proposed would greatly exceed
22 the impact of the Diablo Units, most of which has already occurred.

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