



10 CFR 50.54(f)

RS-16-169

November 3, 2016

U.S. Nuclear Regulatory Commission  
ATTN: Document Control Desk  
11555 Rockville Pike  
Rockville, MD 20852

Byron Station, Units 1 and 2  
Renewed Facility Operating License Nos. NPF-37 and NPF-66  
NRC Docket Nos. STN 50-454 and STN 50-455

Subject: Mitigating Strategies Assessment (MSA) Report for the Reevaluated Seismic Hazard Information – NEI 12-06, Appendix H, Revision 2, H.4.4 Path 4: GMRS < 2xSSE (Partial Submittal - High Frequency work scope)

References:

1. NEI 12-06, Revision 2, Diverse and Flexible Coping Strategies (FLEX) Implementation Guide, December 2015 (ML16005A625)
2. JLD-ISG-2012-01, Revision 1, Compliance with Order EA-12-049, Order Modifying Licenses with Regard to Requirements for Mitigation Strategies for Beyond-Design-Basis External Events, January 22, 2016 (ML15357A163)
3. Exelon Generation Company, LLC Letter to USNRC, Response to NRC Request for Information Pursuant to 10 CFR 50.54(f) Regarding the Seismic Aspects of Recommendation 2.1 of the Near-Term Task Force Review of Insights from the Fukushima Dai-ichi Accident – 1.5 Year Response for CEUS Sites, dated September 12, 2013 (ML13256A070)
4. Exelon Generation Company, LLC Letter to USNRC, Byron Station, Units 1 and 2 - Seismic Hazard and Screening Report (Central and Eastern United States (CEUS) Sites), Response to NRC Request for Information Pursuant to 10 CFR 50.54(f) Regarding Recommendation 2.1 of the Near-Term Task Force Review of Insights from the Fukushima Dai-ichi Accident, dated March 31, 2014 (ML14091A010)
5. NRC Letter to Exelon Generation Company, LLC, Byron Station, Units 1 and 2 – Staff Assessment of Information Provided Pursuant to Title 10 of the Code of Federal Regulations Part 50, Section 50.54(f), Seismic Hazard Reevaluations for Recommendation 2.1 of the Near-Term Task Force Review of Insights from the Fukushima Dai-ichi Accident (CAC Nos. MF3884 and MF3885), dated February 17, 2016 (ML16027A045)

6. Exelon Generation Company, LLC Letter to USNRC, Report of Full Compliance with March 12, 2012 Commission Order Modifying Licenses with Regard to Requirements for Mitigation Strategies for Beyond-Design-Basis External Events (Order Number EA-12-049), dated July 15, 2016 (RS-16-088) (ML16197A390)

The purpose of this letter is to provide the results of the partial assessment (high frequency work scope) for Byron Station, Units 1 and 2 to demonstrate that the FLEX Mitigating Strategies developed, implemented and maintained in accordance with NRC Order EA-12-049, can be implemented considering the impacts of the reevaluated seismic hazard for the high frequency evaluation scope for Path 4 (Reference 1). The assessment was performed in accordance with the guidance provided in Appendix H of NEI 12-06, Revision 2 (Reference 1) which was endorsed by the NRC (Reference 2). The Byron Station, Units 1 and 2 FLEX Mitigating Strategies are described in Reference 6.

The Mitigating Strategies Seismic Hazard Information (MSSHI) is the licensee's reevaluated seismic hazard information at Byron Station, Units 1 and 2, developed using a Probabilistic Seismic Hazard Analysis (PSHA). The MSSHI includes a performance-based Ground Motion Response Spectrum (GMRS), Uniform Hazard Response Spectra (UHRS) at various annual probabilities of exceedance, and a family of seismic hazard curves at various frequencies and fractiles developed at the site control point elevation. Byron Station, Units 1 and 2 submitted the reevaluated seismic hazard information including the UHRS, GMRS and the hazard curves to the NRC in References 3 and 4. The NRC staff concluded that the GMRS that was submitted adequately characterizes the reevaluated seismic hazard for the site (Reference 5).

Byron Station, Units 1 and 2 qualifies as a Path 4 site having exceedances of the GMRS to the Safe Shutdown Earthquake (SSE) both below and above 10 Hz and a GMRS  $<2 \times \text{SSE}$ . This submittal is limited to the high frequency portion of the Path 4 scope. The Path 4 scope is described in Section H.4.4 of Reference 1 and includes the requirement for a high frequency evaluation to be performed in accordance with Section H.4.2 (Path 2) of Reference 1. Therefore, an evaluation was performed for equipment required to implement the Mitigation Strategies that may be sensitive to high frequency ground motions. The remaining scope of evaluations required for Path 4 for Byron Station, Units 1 and 2 will be submitted in accordance with the NRC agreed schedule for Path 4 plants.

Based upon the Mitigating Strategies assessment provided in the enclosure to this letter, the Mitigating Strategies for Byron Station, Units 1 and 2 can be implemented as designed when considering the impacts of the reevaluated seismic hazard for the high frequency scope for Path 4. The remaining scope of evaluations required for Path 4 for Byron Station, Units 1 and 2 will determine the adequacy of the complete design of the Mitigating Strategies to the reevaluated seismic hazard and will be submitted in accordance with the NRC agreed schedule for Path 4 plants.

This letter contains no new regulatory commitments and no revision to existing regulatory commitments.

If you have any questions regarding this submittal, please contact Ron Gaston at (630) 657-3359.

I declare under penalty of perjury that the foregoing is true and correct. Executed on the 3<sup>rd</sup> day of November 2016.

Respectfully submitted,



Glen T. Kaegi  
Director - Licensing & Regulatory Affairs  
Exelon Generation Company, LLC

Enclosure: Seismic Mitigating Strategies Assessment for Byron Station, Units 1 and 2

cc: NRC Regional Administrator - Region III  
NRC Project Manager, NRR – Byron Station  
NRC Senior Resident Inspector – Byron Station  
Mr. Brett A. Titus, NRR/JLD/JCBB, NRC  
Mr. Stephen M. Wyman, NRR/JLD/JHMB, NRC  
Mr. Frankie G. Vega, NRR/JLD/JHMB, NRC  
Mr. John D. Hughey, NRR/JLD/JOMB, NRC  
Illinois Emergency Management Agency – Division of Nuclear Safety

**Enclosure**

Seismic Mitigating Strategies Assessment for Byron Station, Units 1 and 2

(16 pages)

**SEISMIC MITIGATING STRATEGIES  
ASSESSMENT REPORT  
IN RESPONSE TO REGULATORY GUIDE JLD-ISG-2012-01**

for the

**Byron Generating Station, Units 1 and 2  
4450 North German Church Road  
Byron, Illinois 61010-9794  
Facility Operating License Nos. NPF-37 and NPF-66  
NRC Docket Nos. STN 50-454 and STN 50-455  
Correspondence No.: RS-16-169**



Exelon Generation Company, LLC (Exelon)  
PO Box 805398  
Chicago, IL 60680-5398

Prepared by:  
Stevenson & Associates  
1661 Feehanville Drive, Suite 150  
Mount Prospect, IL 60056


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	<u>Printed Name</u>	<u>Signature</u>	<u>Date</u>
Preparer:	A. Broda	<i>Alex Broda</i>	10/06/2016
Reviewer:	M. Delaney	<i>Marilyn M Delaney</i>	10/06/2016
Approver:	M. Delaney	<i>Marilyn M Delaney</i>	10/10/2016
Lead Responsible Engineer:	Kelly Zievor	<i>Kelly Zievor</i>	10/10/16
Branch Manager:	Kevin Passmore	<i>K. Passmore</i>	10/10/16
Senior Manager Design Engineering:	Harris Well	<i>H. Well</i>	10-19-16
Corporate Acceptance:	Jeffrey S. Clark	<i>Jeffrey S. Clark</i>	10/23/16


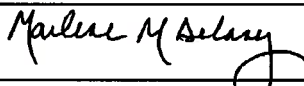
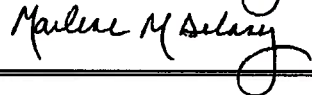
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**ATTACHMENT**

**Exelon Generation Company, LLC (Exelon)**

**Byron Generating Station, Units 1 & 2**

**NRC Docket Nos: STN 50-454 and STN 50-455**

**Facility Operating License Nos: NPF-37 and NPF-66**

**Seismic Mitigating Strategies Assessment for Byron Station, Units 1 & 2**

## **1 INTRODUCTION**

### **1.1 BACKGROUND**

Byron Station, Units 1 and 2 (Byron or BYR) has completed a partial Mitigating Strategies Assessment (MSA) of the impacts of the reevaluated seismic hazard to determine if the mitigating (FLEX) strategies developed, implemented and maintained in accordance with NRC Order EA-12-049 can be implemented for the high frequency evaluation scope for Path 4. The MSA was performed in accordance with the guidance provided in Appendix H of NEI 12-06 Revision 2 [1] which was endorsed by the NRC [2]. The BYR FLEX Mitigating Strategies are described in Reference [3] and Reference [4].

BYR submitted a reevaluated seismic hazard to the NRC [5]. By letter dated October 27, 2015 [6], the NRC transmitted the results of the screening and prioritization review of the seismic hazards reevaluation. Per the results of Reference [5] and Reference [6], BYR qualifies as a Path 4 site having exceedances of the GMRS to the SSE both below and above 10 HZ and a GMRS <2xSSE; therefore, the site falls under the guidance of Reference [1], Appendix H, Section H.4.4 (i.e., Path 4). This requires that high frequency sensitive plant equipment associated with the BYR mitigating strategies; namely, electrical contact devices, be evaluated for effects of the Mitigation Strategies Seismic Hazard Information (MSSHI) in accordance with the guidance of Reference [1], Appendix H, Section H.4.2.

This report describes the partial Mitigation Strategies Assessment undertaken for BYR, implemented using the methodologies in NEI 12-06 [1], Appendix H, which in turn specifies the methodologies from EPRI 3002004396, "High Frequency Program, Application Guidance for Functional Confirmation and Fragility Evaluation." [7]

The objective of this report is to provide summary information describing the partial high frequency evaluation assessment for BYR to demonstrate that the FLEX strategies developed, implemented and maintained in accordance with NRC Order EA-12-049 [8] can be implemented considering the impacts of the reevaluated seismic hazard for the high frequency evaluation scope for Path 4. As described in the Final Integrated Plan (FIP) [3, 4], the plant equipment relied on for FLEX strategies have previously been evaluated as seismically robust to the SSE levels. The level of detail provided in the report is intended to enable NRC to understand the inputs used, the basis for the scope selection, the evaluations performed, and the conclusions made as a result of the partial MSA.



## **1.2 APPROACH**

NEI 12-06 [1], Appendix H Section H.4.2 refers to EPRI 3002004396 [7] for the high-frequency contact device analysis approach. Reference [7] is the primary guidance document used for the BYR engineering evaluations described in this report. Acceptance criteria for the evaluations are found in Reference [1], Appendix H, Section H.5. In accordance with References [7] and [1], the following topics are addressed in the subsequent sections of this report:

- BYR SSE and GMRS/MMSHI Information
- Selection of components and a list of specific components for high-frequency confirmation
- Estimation of seismic demand for subject components
- Estimation of seismic capacity for subject components
- Summary of subject components' high-frequency evaluations
- Summary of Results

## **1.3 PLANT SCREENING**

The Mitigating Strategies Seismic Hazard Information (MSSHI) is the licensee's reevaluated seismic hazard information at BYR, developed using Probabilistic Seismic Hazard Analysis (PSHA). The MSSHI includes a performance-based Ground Motion Response Spectrum (GMRS), Uniform Hazard Response Spectra (UHRS) at various annual probabilities of exceedance, and a family of seismic hazard curves at various frequencies and fractiles developed at the BYR control point elevation. BYR submitted the reevaluated seismic hazard information including the UHRS, GMRS and the hazard curves to the NRC on March 31, 2014 [5]. The NRC summarized their screening evaluations in [Reference 6]. Reference 6, allows BYR to forgo its 2.1 Seismic commitment to perform a relay chatter evaluation given it will not rely on the IPEEE results for its mitigating strategies assessment (MSA). BYR will perform its MSA using Path 4 which does not rely on the IPEEE results. The relay chatter commitment change will be addressed in the 2.1 Seismic High Frequency submittal.

## **1.4 REPORT DOCUMENTATION**

Section 2 describes the selection of devices. The identified devices are evaluated in Reference [21] for the seismic demand specified in Section 3 using the evaluation criteria discussed in Section 4. The overall conclusion is discussed in Section 5.

Table A-1 lists the devices identified in Section 2 and provides the results of the evaluations performed in accordance with Section 3 and Section 4.

## **2 SELECTION OF COMPONENTS**

The fundamental objective of the MSA evaluation is to determine whether the FLEX/mitigating strategies developed, implemented and maintained in accordance with NRC Order EA-12-049 [8] can be implemented considering the impacts of the reevaluated seismic hazard. Within the applicable functions identified in Section H.4.2 (for Path 2 and Path 4) [1], the components that require a high frequency evaluation are contact control devices subject to intermittent states in seal-in or lockout (SILO) circuits. Plants in Path 2 and 4 are required to evaluate SILO devices in the control systems of four specific categories: (1) Reactor Trip/Scram, (2) Reactor Vessel Coolant Inventory leakage pathways, (3) FLEX Phase 1 Components, and (4) Automatically Operated FLEX Phase 2 Components to ensure their functions perform as necessary for the FLEX/mitigating strategies. The equipment selection process for each of those categories is described below.

### **2.1 REACTOR TRIP/SCRAM**

Section H.4.2 of NEI 12-06 Appendix H [1] identifies the Reactor Trip/SCRAM function as a function to be considered in the high frequency evaluation. The EPRI guidance for High Frequency Confirmation [7] notes that "the design requirements preclude the application of seal-in or lockout circuits that prevent reactor trip/SCRAM functions" and that "No high-frequency review of the reactor trip/SCRAM systems is necessary." Therefore, no additional evaluations are necessary for the reactor trip/SCRAM function.

### **2.2 REACTOR VESSEL INVENTORY CONTROL**

This category of components is shared between NEI 12-06 Appendix H [1] and EPRI 3002004396 [7]. The concern for both these programs is the actuation of valves that have the potential to cause a loss-of-coolant accident (LOCA). A LOCA following a seismic event could provide a challenge to the mitigation strategies and lead to core damage. Control circuits for the Pressurizer Power Operated Relief Valves (PORV) as well as other Reactor Coolant System (RCS) valves listed in Attachment 9.1 of Reference [20] were analyzed. Loss of AC power is a basic premise of NEI 12-06, thus control devices for AC powered valves are not included in the NEI 12-06 Appendix H selection. No devices in this category met all criteria for selection.

### **2.3 FLEX PHASE 1**

Section H.4.2 of NEI 12-06 Appendix H [1] requires the analysis of relays and contactors that may lead to circuit seal-in or lockout that could impede the Phase 1 FLEX capabilities, including vital buses fed by station batteries through inverters. Phase 1 of the FLEX Strategy is defined in NEI 12-06 [1] as the initial response period where a plant is relying solely on installed plant equipment. During this phase the plant has no AC power and is relying on batteries, steam, and air accumulators to provide the motive force necessary to operate the critical pumps, valves, instrumentation, and control circuits.

In order to select the Phase 1 SILO devices, an Expedited Seismic Equipment List (ESEL) specific to FLEX Phase 1 was derived from installed permanent plant equipment identified in the plant-specific Overall Integrated Plan (OIP) [3] and periodic updates [3.1, 3.2, 3.3, 3.4, 3.5, 3.6], using the EPRI Seismic Evaluation Guidance [7]. FLEX Strategies specific to a seismic event response or common to all external event responses were examined to identify flow paths, electrical distribution and instrumentation relied upon to accomplish the reactor

and containment safety functions identified in NEI 12-06 [1], omitting response strategies only valid in an outage.<sup>1</sup>

The ESEL is a subset of equipment relied upon to establish the credited flow paths, electrical distribution, and instrumentation identified in the FLEX responses examined. Permanent plant equipment required for implementation of Phase 1 of the FLEX Strategy [3, 3.1, 3.2, 3.3, 3.4, 3.5, 3.6] was identified by reviewing the FLEX Strategy, FLEX support documents, and associated flow path Piping and Instrumentation Diagrams (P&IDs), instrument elementary diagrams, and electrical distribution one-line diagrams. Following section 3.2 of the evaluation guidance [7] the following equipment categories were excluded from consideration:

- Structures
- Distributed systems (piping, cabling, conduit, cable trays, HVAC)
- Nuclear Steam Supply System components

The following key functions were reviewed:

- Piping Flow Paths
- Equipment/Room Cooling
- Key Parameter Instrumentation
- Diesel Fuel Oil Supply
- Instrument Air Distribution
- Electrical Power Distribution
- Control Systems

### **Piping Flow Paths**

Once the FLEX Strategy and FLEX support documents (flow diagrams) were reviewed, P&IDs were examined to identify the primary Phase 1 flow paths credited for seismic response and pressure boundaries necessary to establish those flow paths. In accordance with NEI 12-06, not all success paths need to be evaluated for all hazards; therefore, only a single success path needs to be reviewed for cooling or make-up functions. All components within these identified flow paths and pressure boundaries were screened utilizing the evaluation guidance [7] to exclude components having the following criteria:

- Non-power operated valves (manual valves, check valves, rupture disks) excluding pressure relief valves and manual valves with reach-rods
- Power operated valves, pressure relief valves, and manual valves with reach rods not required to change state to establish identified flow paths
- Sub-components mounted within equipment already included on the list
- In-line pipe-supported components
- Pumps and small heat exchangers within piping pressure boundaries but not in the flow path
- Instrumentation not relied upon for the FLEX response
- Components expected to operate during the initial reactor transient (as described in NEI 12-06, Section 3.2.1.4 [1])

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<sup>1</sup>Based on NEI 12-06 boundary conditions [6, p. 6], at-power operation is the presumed initial plant condition prior to the precipitating beyond-design-basis seismic event.

- Containment isolation valves not required to change state following the initial containment isolation action (as described in NEI 12-06, Section 3.2.1.11 [1])

The remaining components not screened out are included in the equipment list. Of these components, pumps needed to operate, power-operated valves needed to change state to establish the identified flow paths and pressure boundaries, as well as instruments that are essential to FLEX Strategy within these paths were singled out for identification of necessary motive and control sources.

For the Phase 1 FLEX response, Byron credits their Diesel Driven Auxiliary Feedwater (DDAF) Pump to provide feedwater to the Steam Generators to maintain core decay heat cooling. For this effort, the flow paths credited include: (1) water from the Ultimate Heatsink to the Steam Generators via the Essential Service Water (SX) system and the DDAF Pump; and (2) Steam from the Steam Generators (SG) to the atmosphere via the Main Steam PORVs.

### **Equipment/Room Cooling**

The motive force required to cool the DDAFW pump rooms is taken directly from the diesel shaft and the required coolers and fan are included in the pump assembly. Cooling for other rooms is normally provided by AC power, and thus components associated with fans, dampers, compressors or other systems relied upon to provide ventilation or cooling to these rooms were not considered as these would not be Phase 1 systems.

### **Key Parameter Instrumentation**

Instruments identified to monitor parameters critical to control of elements of the Phase 1 FLEX Strategy [3, 3.1, 3.2, 3.3, 3.4, 3.5, 3.6] are included in the ESEL. For each of the included instruments, flow diagrams were reviewed as applicable to confirm the transmitter is within an established FLEX flow path. Elementary diagrams were reviewed to establish the signal path between the instrument transmitter and the credited indicator. The transmitter, indicator and any signal conditioning components, as well as power supplies used to power all the components necessary to the signal path were identified. For each of these items either the component itself or the instrumentation cabinet containing it (per rule-of-the-box (ROB)) was included in the ESEL.

### **Diesel Fuel Oil Supply**

For BYR Phase 1 response the DDAF pump day tank was the credited source of fuel oil. The fuel oil transfer pumps are AC operated and thus not powered during Phase 1.

### **Instrument Air Distribution**

Instrument air P&IDs were reviewed along with the OIP [3, 3.1, 3.2, 3.3, 3.4, 3.5, 3.6] and FLEX Support Guides to determine if any tanks, accumulators, pressure regulating valves, or any power operated valves are required to provide Instrument Air (IA) to air-operated valves necessary to establish FLEX Phase 1 flow paths. In general, normal instrument air is non-safety related. Any valves credited to establish Byron's FLEX Phase 1 flow paths which use normal instrument air as a motive source either fail to their required state or will be manually overridden. The DDAF pump discharge valves have a small IA accumulator to function automatically for a short time and then they will be manually operated. Safety-related accumulators are the credited motive source for the Pressurizer PORVs. These accumulators are included on the Phase 1 ESEL. Instrument air control valves are mechanically operated from air pressure, and thus no electrical relays or switches are needed to provide the air supply required for any valve.

### **Electrical Power Distribution**

The Phase 1 response relies on station batteries for electrical power (motive force). One-line drawings were reviewed and the batteries, inverters, and electrical distribution between the batteries and the required DC MCCs and vital instrumentation power supplies were included on the equipment list.

### **Control Systems**

For every FLEX Phase 1 item on the ESEL requiring control, the associated control diagrams were reviewed and the control cabinets or panels critical to the item's control were included on the equipment list. Power sources for the required control circuits were traced and any power distribution component necessary for the control circuits (and not already identified) was added as well. Relay control logic was analyzed and relays or switches that could cause seal-in or lockout and leave the circuit in a state other than what would be desired for FLEX response were identified and added to the equipment list. The criteria for determining if a component needed to be evaluated are provided below. A component must meet all three of the following criteria to be selected.

#### **(Criterion 1)**

The Phase 1 FLEX Strategy for Byron, as described in the Overall Integrated Plan [3] and its updates [3.1, 3.2, 3.3, 3.4, 3.5, 3.6], relies on permanent plant equipment in the DDAF, SX, and SG PORV systems. Control elementary diagrams, piping and instrumentation diagrams, and system technical manuals were reviewed as necessary to determine which relays and switches have an impact on the operation of these systems. Any impact to AC powered valves in these systems was ignored as loss of AC power is a requirement for entry into FLEX.

#### **(Criterion 2)**

Before entry into FLEX a site must first (in this case) experience a beyond design-basis seismic event coupled with an Extended Loss of AC Power (ELAP) and Loss of Ultimate Heat Sink (LUHS). In this event scenario the site would need time to assess plant conditions before it would declare itself in an ELAP/LUHS condition. By the time this condition is declared it is expected the period of strong shaking would be over and thus any temporary effect of relay chatter would be cleared before entry into FLEX. In some control circuits, however, contacts are fed back into the control to electrically seal-in and cause a sustained change of state in the control circuit. This circuit seal-in may cause valves to change position, pumps to change state, or controls to lock-out operation of systems or components. Control elementary diagrams, piping and instrumentation diagrams, and system technical manuals were reviewed as necessary to determine the potential of chatter (in the relays and switches identified by Criterion 1) to cause a seal-in or lock-out. Only those relays and switches with the potential to cause seal-in or lock-out were screened-in for evaluation, relays and switches with only the potential to cause temporary conditions that clear on their own before entry into FLEX were screened out.

#### **(Criterion 3)**

In some cases, spurious chatter leads to a circuit seal-in or lock-out that either has no effect on the FLEX Response, or has a beneficial effect on the FLEX Response (for example the unintentional change of state in a valve that aids in aligning a credited flow path). Contact chatter having no system effect or beneficial system effects allow a relay or switch to be

functionally screened out of consideration for this category. Control elementary diagrams, piping and instrumentation diagrams, and system technical manuals were reviewed as necessary to determine the potential impact of chatter (in the relays and switches identified by Criterion 2) on the operation of the Phase 1 systems. Only those relays and switches which could cause an undesirable effect on these systems were screened-in.

The selection of contact devices for the Diesel Driven Auxiliary Feedwater (DDAF) Pump was based on the premise that DDAF operation is desired, thus any SILO which would lead to DDAF operation is beneficial and thus does not meet the criteria for selection [16, 17]. Only contact devices which could render the DDAF system inoperable were considered.

Any chatter which could de-energize the normally-energized Engine Failure Lockout Relay K12 would prevent engine start [18, 19]. The lockout relay itself does not seal in, however the relays with contacts in K12's coil circuit do. The Overcrank Relay K7, High Water Temperature Relay K8, Overspeed Relay K9, and Low Lube Oil Pressure Relay K10 are normally energized and sealed-in. Chatter in the seal-in contacts of K7, K8, K9, K10, or in the contacts of the Overcrank Timer Relay K4 (input to K7), High Water Temperature Switch 1TSH-AF147 (input to K8), Speed Switch 1SS-AF8002 (input to K9), Low Oil Pressure Time Delay Relay K11 (input to K10), could trip the lockout relay and prevent engine start. The time delay associated with K4 and K11 prevents chatter in their coil circuits from affecting engine start. It is presumed that pump suction pressure is above the reset pressure setting of 1PSL-AF055 and therefore chatter in this pressure switch and the Low Suction Pressure Timer Relay K6 have only a temporary effect on engine start and thus do not meet selection criteria. The devices selected based on this discussion are listed in Table A-1.

## **2.4 FLEX PHASE 2 AUTOMATIC OPERATION**

NEI 12-06 Appendix H [1] requires the inclusion of SILO relays and contactors that could impede FLEX capabilities for mitigation of seismic events in permanently installed Phase 2 SSCs that have the capability to begin operation without operator manual actions.

With the loss of AC power, Phase 2 SSCs are limited to any permanently installed FLEX generator and, if allowed to automatically start, any electrical components powered by the FLEX generator and relied upon for Phase 2 of the FLEX Strategy. Byron Station credits a portable FLEX generator for Phase 2 response, and the operator actions necessary to install and connect the generator excludes any devices from being identified in this category.

## **2.5 SUMMARY OF SELECTED COMPONENTS**

The investigation of high-frequency contact devices as described above was performed in Ref. [20]. A list of the contact devices requiring a high frequency evaluation is provided in Appendix A, Table A-1. The identified devices are evaluated in Ref. [21] per the methodology/description of Section 3 and 4. Results are presented in Section 5 and Table A-1.

### **3 SEISMIC EVALUATION**

#### **3.1 HORIZONTAL SEISMIC DEMAND**

BYR performed a High Frequency Confirmation using the criteria in Reference [7], which is the same criteria specified for the MSA Path 2 and 4 evaluation [1]. The horizontal ground motion applicable to the MSA Path 2 and 4 evaluation is the same horizontal ground motion identified in BYR submittal [10].

#### **3.2 VERTICAL SEISMIC DEMAND**

BYR performed a High Frequency Confirmation using the criteria in Reference [7], which is the same criteria specified for the MSA Path 2 and 4 evaluation which is part of the Path 4 evaluation requirements [1]. The vertical ground motion applicable to the MSA Path 2 and 4 evaluation is the same vertical ground motion identified in BYR submittal [10].

#### **3.3 COMPONENT HORIZONTAL SEISMIC DEMAND**

The components identified in Section 2 were previously evaluated in the BYR High Frequency Confirmation [10]. Therefore, the component horizontal seismic demands for the MSA are the same as the demands applied in the High Frequency Confirmation.

#### **3.4 COMPONENT VERTICAL SEISMIC DEMAND**

The components identified in Section 2 were previously evaluated in the BYR High Frequency Confirmation [10]. Therefore, the component vertical seismic demands for the MSA are the same as the demands applied in the High Frequency Confirmation.

#### **4 CONTACT DEVICES EVALUATION**

Per Reference [7], seismic capacities (the highest seismic test level reached by the contact device without chatter or other malfunction) of each subject contact device are determined by the following procedures:

- (1) If a contact device was tested as part of the EPRI High Frequency Testing program [11], then the component seismic capacity from this program is used.
- (2) If a contact device was not tested as part of Reference 10, then one or more of the following means to determine the component capacity were used:
  - (a) Device-specific seismic test reports (either from the station or from the Seismic Qualification Reporting and Testing Standardization (SQRSTS))
  - (b) Generic Equipment Ruggedness Spectra (GERS) capacities per References [12, 13, 14, 15].
  - (c) Assembly (e.g. electrical cabinet) tests where the component functional performance was monitored.

The high-frequency capacity of each device was evaluated with the component mounting point demand from Section 3 using the criteria in Section 4.5 of Reference [7] and the acceptance criteria in Section H.5 of Reference [1].

A summary of the high-frequency evaluation results is provided in Appendix A.



## **5 Conclusions**

### **5.1 GENERAL CONCLUSIONS**

BYR completed the evaluation of potentially sensitive contact devices in accordance with NEI 12-06 [1], Appendix H Section H.4.2 and EPRI 3002004396 [7]. The results of the evaluation confirm that the FLEX strategies for BYR can be implemented as designed and no further seismic evaluations are necessary.

### **5.2 IDENTIFICATION OF FOLLOW-UP ACTIONS**

No follow-up actions were identified.

## 6 References

1. NEI 12-06, Revision 2, Diverse and Flexible Coping Strategies (FLEX) Implementation Guide, December 2015, ADAMS Accession Number ML16005A625
2. JLD-ISG-2012-01, Revision 1, Compliance with Order EA-12-049, Order Modifying Licenses with Regard to Requirements for Mitigation Strategies for Beyond-Design-Basis External Events, February 2016, ADAMS Accession Number ML15357A163
3. Letter RS-13-018 from Byron to NRC (ML13060A364), "Overall Integrated Plan in Response to March 12, 2012 Commission Order Modifying Licenses with Regard to Requirements for Mitigation Strategies for Beyond-Design-Basis External Events (Order Number EA-12-049)," February 28, 2013
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  - 3.3. Letter RS-14-206 from Byron to NRC (ML14248A229), "Third Six-Month Status Report in Response to March 12, 2012 Commission Order Modifying Licenses with Regard to Requirements for Mitigation Strategies for Beyond-Design-Basis External Events (Order Number EA-12-049)," August 28, 2014
  - 3.4. Letter RS-15-017 from Byron to NRC (ML15058A476), "Fourth Six-Month Status Report in Response to March 12, 2012 Commission Order Modifying Licenses with Regard to Requirements for Mitigation Strategies for Beyond-Design-Basis External Events (Order Number EA-12-049)," February 27, 2015
  - 3.5. Letter RS-15-209 from Byron to NRC (ML15240A304), "Fifth Six-Month Status Report in Response to March 12, 2012 Commission Order Modifying Licenses with Regard to Requirements for Mitigation Strategies for Beyond-Design-Basis External Events (Order Number EA-12-049)," August 28, 2015
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17. Byron Drawing 6E-2-4030AF02 Rev. Z, Schematic Diagram Auxiliary Feedwater Pump 2B Diesel Driven 2AF01PB
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19. Byron Drawing 6E-2-4030AF12 Rev. AH, Schematic Diagram Auxiliary Building Pump 2B (Diesel-Driven) Engine Startup Panel 2AF01J
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## A Components Identified for High Frequency Evaluation

**Table A-1: Components Identified for High Frequency Evaluation**

No.	Unit	Component				Enclosure Type	Building	Component Evaluation Result
		ID	Type	System	Function			
1	1	1AF01J-K10	Control Relay	FLEX Phase 1	Low Lube Oil Pressure Relay	Control Cabinet	Auxiliary Building	Cap > Dem
2	1	1AF01J-K11	Control Relay	FLEX Phase 1	Low Oil Pressure Time Delay Relay	Control Cabinet	Auxiliary Building	Cap > Dem
3	1	1AF01J-K4	Control Relay	FLEX Phase 1	Overcrank Timer Relay	Control Cabinet	Auxiliary Building	Cap > Dem
4	1	1AF01J-K7	Control Relay	FLEX Phase 1	Overcrank relay	Control Cabinet	Auxiliary Building	Cap > Dem
5	1	1AF01J-K8	Control Relay	FLEX Phase 1	High water temperature relay	Control Cabinet	Auxiliary Building	Cap > Dem
6	1	1AF01J-K9	Control Relay	FLEX Phase 1	Overspeed relay	Control Cabinet	Auxiliary Building	Cap > Dem
7	1	1SS-AF8002 "S1"	Process Switch	FLEX Phase 1	Speed switch	Control Cabinet	Auxiliary Building	Cap > Dem
8	1	1TSH-AF147 "S10"	Process Switch	FLEX Phase 1	High water temperature switch	Control Cabinet	Auxiliary Building	Cap > Dem
9	2	2AF01J-K10	Control Relay	FLEX Phase 1	Low Lube Oil Pressure Relay	Control Cabinet	Auxiliary Building	Cap > Dem
10	2	2AF01J-K11	Control Relay	FLEX Phase 1	Low Oil Pressure Time Delay Relay	Control Cabinet	Auxiliary Building	Cap > Dem
11	2	2AF01J-K4	Control Relay	FLEX Phase 1	Overcrank Timer Relay	Control Cabinet	Auxiliary Building	Cap > Dem
12	2	2AF01J-K7	Control Relay	FLEX Phase 1	Overcrank relay	Control Cabinet	Auxiliary Building	Cap > Dem
13	2	2AF01J-K8	Control Relay	FLEX Phase 1	High water temperature relay	Control Cabinet	Auxiliary Building	Cap > Dem
14	2	2AF01J-K9	Control Relay	FLEX Phase 1	Overspeed relay	Control Cabinet	Auxiliary Building	Cap > Dem
15	2	2SS-AF8002 "S1"	Process Switch	FLEX Phase 1	Speed switch	Control Cabinet	Auxiliary Building	Cap > Dem
16	2	2TSH-AF147 "S10"	Process Switch	FLEX Phase 1	High water temperature switch	Control Cabinet	Auxiliary Building	Cap > Dem