



UNITED STATES
NUCLEAR REGULATORY COMMISSION
WASHINGTON, D. C. 20555

DUKE POWER COMPANY

DOCKET NO. 50-269

OCONEE NUCLEAR STATION, UNIT 1

AMENDMENT TO FACILITY OPERATING LICENSE

Amendment No. 182
License No. DPR-38

1. The Nuclear Regulatory Commission (the Commission) has found that:
 - A. The application for amendment to the Oconee Nuclear Station, Unit 1 (the facility) Facility Operating License No. DPR-38 filed by the Duke Power Company (the licensee) dated August 31, 1989, as supplemented January 24, 1990, complies with the standards and requirements of the Atomic Energy Act of 1954, as amended (the Act) and the Commission's rules and regulations set forth in 10 CFR Chapter I;
 - B. The facility will operate in conformity with the application, the provisions of the Act, and the rules and regulations of the Commission;
 - C. There is reasonable assurance (i) that the activities authorized by this amendment can be conducted without endangering the health and safety of the public, and (ii) that such activities will be conducted in compliance with the Commission's regulations set forth in 10 CFR Chapter I;
 - D. The issuance of this license amendment will not be inimical to the common defense and security or to the health and safety of the public; and
 - E. The issuance of this amendment is in accordance with 10 CFR Part 51 of the Commission's regulations, and all applicable requirements have been satisfied.
2. Accordingly, the license is hereby amended by page changes to the Technical Specifications as indicated in the attachment to this license amendment, and Paragraph 3.B. of Facility Operating License No. DPR-38 is hereby amended to read as follows:

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Technical Specifications

The Technical Specifications contained in Appendices A and B, as revised through Amendment No. 182 are hereby incorporated in the license. The licensee shall operate the facility in accordance with the Technical Specifications.

3. This license amendment is effective as of its date of issuance.

FOR THE NUCLEAR REGULATORY COMMISSION

DAVID B. MATTHEWS

David B. Matthews, Director
Project Directorate II-3
Division of Reactor Projects - I/II
Office of Nuclear Reactor Regulation

Attachment:
Technical Specification
Changes

Date of Issuance: April 25, 1990



UNITED STATES
NUCLEAR REGULATORY COMMISSION
WASHINGTON, D. C. 20555

DUKE POWER COMPANY

DOCKET NO. 50-270

OCONEE NUCLEAR STATION, UNIT 2

AMENDMENT TO FACILITY OPERATING LICENSE

Amendment No. 182
License No. DPR-47

1. The Nuclear Regulatory Commission (the Commission) has found that:
 - A. The application for amendment to the Oconee Nuclear Station, Unit 2 (the facility) Facility Operating License No. DPR-47 filed by the Duke Power Company (the licensee) dated August 31, 1989, as supplemented January 24, 1990, complies with the standards and requirements of the Atomic Energy Act of 1954, as amended (the Act) and the Commission's rules and regulations set forth in 10 CFR Chapter I;
 - B. The facility will operate in conformity with the application, the provisions of the Act, and the rules and regulations of the Commission;
 - C. There is reasonable assurance (i) that the activities authorized by this amendment can be conducted without endangering the health and safety of the public, and (ii) that such activities will be conducted in compliance with the Commission's regulations set forth in 10 CFR Chapter I;
 - D. The issuance of this license amendment will not be inimical to the common defense and security or to the health and safety of the public; and
 - E. The issuance of this amendment is in accordance with 10 CFR Part 51 of the Commission's regulations, and all applicable requirements have been satisfied.
2. Accordingly, the license is hereby amended by page changes to the Technical Specifications as indicated in the attachment to this license amendment, and Paragraph 3.B. of Facility Operating License No. DPR-47 is hereby amended to read as follows:

Technical Specifications

The Technical Specifications contained in Appendices A and B, as revised through Amendment No. 182, are hereby incorporated in the license. The licensee shall operate the facility in accordance with the Technical Specifications.

3. This license amendment is effective as of its date of issuance.

FOR THE NUCLEAR REGULATORY COMMISSION

David B. Matthews
for David B. Matthews, Director
Project Directorate II-3
Division of Reactor Projects - I/II
Office of Nuclear Reactor Regulation

Attachment:
Technical Specification
Changes

Date of Issuance: April 25, 1990



UNITED STATES
NUCLEAR REGULATORY COMMISSION
WASHINGTON, D. C. 20555

DUKE POWER COMPANY

DOCKET NO. 50-287

OCONEE NUCLEAR STATION, UNIT 3

AMENDMENT TO FACILITY OPERATING LICENSE

Amendment No. 179
License No. DPR-55

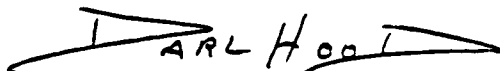
1. The Nuclear Regulatory Commission (the Commission) has found that:
 - A. The application for amendment to the Oconee Nuclear Station, Unit 3 (the facility) Facility Operating License No. DPR-55 filed by the Duke Power Company (the licensee) dated August 31, 1989, as supplemented January 24, 1990, complies with the standards and requirements of the Atomic Energy Act of 1954, as amended (the Act) and the Commission's rules and regulations set forth in 10 CFR Chapter I;
 - B. The facility will operate in conformity with the application, the provisions of the Act, and the rules and regulations of the Commission;
 - C. There is reasonable assurance (i) that the activities authorized by this amendment can be conducted without endangering the health and safety of the public, and (ii) that such activities will be conducted in compliance with the Commission's regulations set forth in 10 CFR Chapter I;
 - D. The issuance of this license amendment will not be inimical to the common defense and security or to the health and safety of the public; and
 - E. The issuance of this amendment is in accordance with 10 CFR Part 51 of the Commission's regulations, and all applicable requirements have been satisfied.
2. Accordingly, the license is hereby amended by page changes to the Technical Specifications as indicated in the attachment to this license amendment, and Paragraph 3.B. of Facility Operating License No. DPR-55 is hereby amended to read as follows:

Technical Specifications

The Technical Specifications contained in Appendices A and B, as revised through Amendment No. 179, are hereby incorporated in the license. The licensee shall operate the facility in accordance with the Technical Specifications.

3. This license amendment is effective as of its date of issuance.

FOR THE NUCLEAR REGULATORY COMMISSION

A handwritten signature in black ink, appearing to read "DAVID B. MATTHEWS".

David B. Matthews, Director
Project Directorate II-3
Division of Reactor Projects - I/II
Office of Nuclear Reactor Regulation

Attachment:
Technical Specification
Changes

Date of Issuance: April 25, 1990

ATTACHEMENT TO LICENSE AMENDMENT NO. 182

FACILITY OPERATING LICENSE NO. DRP-38

DOCKET NO. 50-269

AND

TO LICENSE AMENDMENT NO. 182

FACILITY OPERATING LICENSE NO. DPR-55

DOCKET NO. 50-270

AND

TO LICENSE AMENDMENT NO. 179

FACILITY OPERATING LICENSE NO. DPR-55

DOCKET NO. 50-287

Replace the following pages of the Appendix "A" Technical Specifications with the enclosed pages. The revised pages are identified by Amendment number and contain vertical lines indicating the areas of change.

Remove Pages

3.7-1 - 3.7-14

Insert Pages

3.7-1 - 3.7-17

3.7 AUXILIARY ELECTRICAL SYSTEMS

Applicability

Applies to the availability of off-site and on-site electrical power for station operation and for operation of station auxiliaries.

Objective

To define those conditions of electrical power availability necessary to provide for safe reactor operation and to provide for continuing availability of engineered safety features systems in an unrestricted manner and to prescribe safety evaluation and reporting requirements to be followed in the event that the auxiliary electric power systems become degraded.

Specifications

- 3.7.1 Except as permitted by 3.7.2, 3.7.3, 3.7.4, 3.7.5, 3.7.6, 3.7.7, and 3.7.8, the reactor shall not be above 200°F unless the following conditions are met.
- (a) At least two 230KV transmission lines, on separate towers, shall be in service.
 - (b) Two independent on-site emergency power paths shall be operable and shall consist of:
 - 1. One Keowee hydro unit; through the underground feeder path; through transformer CT4; through the Keowee standby bus feeder breakers (SK1 and SK2) to two standby buses; and capable of supplying emergency power through the standby bus to main feeder bus breakers (S1 and S2).
 - 2. The other (redundant) Keowee hydro unit; through the Keowee main step-up transformer and breaker PCB-9; the 230 kV switchyard yellow bus and safety related PCB-18, -27, or 30; through the respective operating unit's startup transformer (CT-1, 2, or 3) or aligned and connected alternate startup transformer; and capable of supplying emergency power through the startup transformer to main feeder bus breakers (E1 and E2). One startup transformer may not be aligned to supply power to more than one unit.
 - (c) The Emergency Power Switching Logic (EPSL) circuitry shall be operable as specified by the conditions of Table 3.7-1 for normal operation. Furthermore, if the reactor is subcritical, the conditions of Table 3.7-1 for normal operation shall be satisfied before the reactor is returned to criticality.
 - (d) Two 4160 volt main feeder buses shall be energized.

- (e) The three 4160 volt Engineered Safety Features switchgear buses (TC, TD, and TE), three 600 volt load centers (X8, 9, and 10), and the three 600-208 volt Engineered Safety Features MCC Buses (XS1, XS2, XS3) shall be energized.
- (f) For each unit, the 125 VDC Instrumentation and Control Power System shall be operable as specified below:
1. Both 125 VDC instrumentation and control distribution centers (DCA and DCB);
 2. All four 125 VDC instrumentation and control panelboards (DIA, DIB, DIC, and DID), including the associated isolating transfer diodes and diode monitors (ADA 1 & 2, ADB 1 & 2, ADC 1 & 2, ADD 1 & 2);
 3. All four 120 VAC vital instrumentation power panelboards (KVIA, KVIB, KVIC, and KVID), including the associated static inverters;
 4. The 240/120 VAC regulated power panelboard (KRA).
 5. The 125 VDC Instrumentation and Control (I&C) batteries with associated chargers shall be operable per all the following conditions:
 - (a) Each unit, when in a cold shutdown condition, shall have at least one of that unit's I&C batteries operable;
 - (b) For operation of two or more units, five of the six batteries shall be operable;
 - (c) For operation of Unit 1, three of the following four batteries shall be operable: 1CA, 1CB, 2CA, and 2CB.
For operation of Unit 2, three of the following four batteries shall be operable: 2CA, 2CB, 3CA, and 3CB.
For operation of Unit 3, three of the following four batteries shall be operable: 3CA, 3CB, 1CA, and 1CB.
- (g) Both of the 125 VDC 230KV switching station batteries (SY-1, SY-2), with associated chargers, distribution centers, and panelboards shall be operable.
- (h) Both of the 125 VDC Keowee batteries (Bank 1 & 2) with associated chargers and distribution centers (1DA & 2DA) shall be operable.
- (i) The level of Keowee Reservoir shall be at least 775 feet above sea level.

- (j) The Keowee station auxiliary transformers (1X and 2X)-and the Keowee station backup auxiliary transformer (CX) shall be operable.

3.7.2 With the reactor heated above 200°F, provisions of 3.7.1 may be modified to allow the following conditions to exist:

- (a)(1) One of the two independent on-site emergency power paths, as defined in 3.7.1(b), may be inoperable for periods not exceeding 72 hours for test or maintenance, provided the alternate power path is verified operable within one hour of the loss and every eight hours thereafter.
- (2) Both Keowee station auxiliary transformers (1X and 2X) may be inoperable for periods not exceeding 72 hours for test or maintenance, provided that the backup auxiliary transformer (CX) and its associated underground power path from Oconee switchgear 1TC is operable;
- (3) Keowee backup auxiliary transformer (CX) and its associated underground power path from Oconee switchgear 1TC may be inoperable for periods not exceeding 72 hours for test or maintenance, provided that the Keowee main step-up transformer and both auxiliary transformers (1X and 2X) are operable;
- (4) Keowee auxiliary transformer (1X) may be inoperable for test or maintenance provided that Keowee Unit 2 is aligned to the overhead path;
- (5) Keowee auxiliary transformer (2X) may be inoperable for test or maintenance provided that Keowee Unit 1 is aligned to the overhead path.
- (b) Except for the allowable conditions defined in Specifications 3.7.2(a), 3.7.2(c), 3.7.2(i), 3.7.4, 3.7.6 and 3.7.7 the circuits or channels of any single functional unit of the EPSL may be inoperable for test or maintenance for periods not exceeding 24 hours, provided that:
1. The conditions of Table 3.7-1 for degraded operation are satisfied for that specific functional unit; and
 2. The conditions of Table 3.7-1 for normal operation are satisfied for all other functional units.

Beyond the conditions allowed by 3.7.2(b)1 and 2, the circuits or channels of more than one functional unit of the EPSL may be inoperable only if:

1. The inoperability results from a loss of power due to the inoperability of a 125 VDC instrumentation and control panelboard (see 3.7.2(e) below); and

2. The conditions of Table 3.7-1 for degraded operation are satisfied for the affected functional units.

In any event, if the reactor is subcritical, the inoperable circuit(s) or channel(s) shall be restored to operability and the conditions of Table 3.7-1 for normal operation shall be satisfied for all functional units before the reactor is returned to criticality.

- (c) One 4160 volt main feeder bus may be inoperable for 24 hours.
- (d) One complete single string (i.e., 4160 volt switchgear (TC, TD, or TE), 600 volt load center, (X8, X9, or X10), 600-208 volt MCC (XS1, XS2, or XS3), and their loads) of each unit's 4160 volt Engineered Safety Features Power System may be inoperable for 24 hours.
- (e) One or more of the following DC distribution components may be inoperable for periods not exceeding 24 hours (except as noted in 3.7.2(g) below):
 1. One complete single string or single component (i.e., 125VDC battery, charger, distribution center, and panelboards) of the 125VDC 230KV Switching Station Power System.
 2. One complete single string or single component (i.e., 125VDC battery, charger, and distribution center) of the Keowee 125VDC Power System may be inoperable provided the remaining string of the Keowee 125 VDC Power System is operable and electrically connected to an operable Keowee hydro unit.
 3. One complete single string or single component (i.e., 125VDC battery, charger, distribution center, and associated isolating and transfer diodes) of any units 125VDC Instrumentation and Control Power System. Only one battery more than the number allowed to be inoperable per 3.7.1 (f) for the Station may be removed from service under this paragraph.
 4. One 125 VDC instrumentation and control panelboard and its associated loads, per unit, provided that no additional AC buses are made inoperable beyond the provisions of 3.7.2(a), (c), and (d), and provided that the conditions of Table 3.7-1 for normal operation are satisfied for all functional units of the EPSL before the 125 VDC instrumentation and control panelboard becomes inoperable. Additionally, the provisions of 3.7.2.(h) must be observed for the 120 VAC vital instrumentation power panelboard which is powered by the affected 125 VDC panelboard.
- (f) For periods not to exceed 24 hours each unit's 125 VDC system may be separated from its backup unit via the isolating and transfer diodes.
- (g) One battery each, from one or more of the following 125VDC systems may be simultaneously inoperable for 72 hours in order to perform an equalizer charge after the surveillance requirements of Specification 4.6.10 or performance test:

1. 230 KV Switching Station 125VDC Power System
 2. Keowee Hydro Station 125VDC Power System
 3. Each unit's 125VDC Instrumentation and Control Power System, provided that only one battery more than the number allowed to be inoperable per 3.7.1 (f) (5) for the station is removed from service under this paragraph.
- (h) One 120 VAC vital instrumentation power panelboard per unit and/or its associated static inverter may be inoperable for periods as specified below:

<u>Panelboard</u>	<u>Maximum Allowed Period of Inoperability</u>
KVIA	4 hours
KVIB	4 hours
KVIC	24 hours
KVID	24 hours

A single vital bus static inverter per unit may continue to be inoperable beyond the specified period, but no longer than 7 days total, provided that its associated 120 VAC vital instrumentation power panelboard is connected to the 240/120 VAC Regulated Power System (KRA) and verified to be operable once every 24 hours.

- (i) 1. A startup transformer may be inoperable for periods not exceeding 72 hours for test or maintenance, provided the underground feeder path, through transformer CT4; and to two 4160V standby buses is verified operable within one hour of loss and every eight hours thereafter. The remaining operable startup transformers can be shared between units within the same 72 hours of the above startup transformer being determined inoperable. Prior to exceeding 72 hours, they shall be aligned and connected such that each one is providing a path for power to one and only one unit.
2. In the event that a startup transformer becomes inoperable for unplanned reasons, then one unit shall be in cold shutdown within 72 hours with its loads powered from the standby buses. The remaining operable startup transformers can be shared between units within the same 72 hours of the above startup transformer being determined inoperable. Prior to exceeding 72 hours, they shall be aligned and connected such that each one is providing a path for power to one and only one unit.

3.7.3 In the event that the conditions of Specifications 3.7.1 are not met within the time specified in Specification 3.7.2, except as noted below in Specification 3.7.4, 3.7.5, 3.7.6, 3.7.7, and 3.7.8, the reactor shall be placed in a hot shutdown condition within 12 hours. If these requirements are not met within an additional 48 hours, the reactor shall be placed in the cold shutdown condition within 24 hours.

3.7.4 In the event that all conditions in Specification 3.7.1 are met except that one of the two Keowee hydro units is expected to be unavailable for longer than the test or maintenance period of 72 hours, the reactor may be heated above 200°F if previously shutdown or be permitted to remain critical or be restarted provided the following restrictions are observed.

- (a) Prior to heating the reactor above 200°F or prior to the restart of a shutdown reactor or within 72 hours of the loss of one Keowee hydro unit, the 4160 volt standby buses shall be energized by a Lee gas turbine through the 100 kV circuit. The Lee gas turbine and 100 kV transmission circuit shall be electrically separate from the system grid and offsite non-safety-related loads.
- (b) The remaining Keowee hydro unit shall be connected to the underground feeder circuit and this path shall be verified operable within 1 hour and weekly thereafter.
- (c) The remaining Keowee hydro unit shall be available to the overhead transmission circuit but generation to the system grid shall be prohibited except for periods of test.
- (d) Operation in this mode is restricted to periods not to exceed 45 days and the provisions of this specification may be utilized without prior NRC approval only once in three years for each Keowee hydro unit. The U.S. NRC Regional Office, Region II, will be notified within 24 hours.

3.7.5 In the event that all conditions of Specification 3.7.1 are met except that all 230 kV transmission lines are lost, the reactor shall be permitted to remain critical or be restarted provided the following restrictions are observed:

- (a) Prior to the restart of a shutdown reactor or within 1 hour of losing all 230 kV transmission lines for an operating reactor, the 4160 volt standby buses shall be energized by one of the Lee gas turbines through the 100 kV transmission circuit. The Lee gas turbine and the 100kV transmission circuit shall be completely separate from the system grid and offsite non-safety-related loads.
- (b) The reactor coolant T_{avg} shall be above 525°F. Reactor coolant pump power may be used to elevate the temperature from 500°F to 525° in the case of restart. If T_{avg} decreases below 500°F, restart is not permitted by this specification.

- (c) If all 230 kV transmission lines are lost, restore at least one of the inoperable 230kV offsite sources to operable status within 24 hours or be in at least hot standby within the next 6 hours. With only one offsite source restored, restore at least two 230kV offsite circuits to operable status within 72 hours from time of initial loss or be in at least hot standby within the next 6 hours and in cold shutdown within the following 30 hours.
- (d) After loss of all 230 kV transmission lines, this information shall be reported within 24 hours to the U.S. NRC Regional Office, Region II. If the outage is expected to exceed 24 hours, a written report shall be submitted detailing the circumstances of the outage and the estimated time to return the 230 kV transmission lines to operating condition.

3.7.6 In the event that all conditions of Specification 3.7.1 are met, and planned tests or maintenance are required which will make both Keowee units unavailable, the 4160 volt standby buses shall first be energized by a Lee gas turbine through the 100 kV transmission circuit and shall be separate from the system grid and offsite non-safety-related loads. The reactor shall then be permitted to remain critical for periods not to exceed 72 hours with both Keowee units unavailable.

Prior to hot restart of a reactor from a tripped condition, the causes and the effects of the shutdown shall be established and analyzed. A restart will be permitted if the cause of such trips is the result of error or of minor equipment malfunctions. A restart will not be permitted if the trip is a result of system transients or valid protection system action.

3.7.7 In the event that all conditions of Specification 3.7.1 are met except that both Keowee hydro units become unavailable for unplanned reasons, the reactor shall be permitted to remain critical for periods not to exceed 24 hours provided the 4160 volt standby buses are energized within 1 hour by the Lee gas turbine through the 100 kV transmission circuit and it shall be separate from the system grid and all offsite non-safety-related loads.

Prior to hot restart of a reactor from a tripped condition, the causes and the effects of the shutdown shall be established and analyzed. A restart will be permitted if the cause of such trips is the result of error or of minor equipment malfunctions. A restart will not be permitted if the trip is a result of system transients or valid protection system action.

3.7.8 In the event that all conditions in Specification 3.7.1 are met except that any one of the following is expected to be unavailable for longer than the test or maintenance period of 72 hours, as allowed by 3.7.2(a):

- 1) Keowee Main Step-up transformer (including both Keowee Auxiliary Transformers);
- 2) Both Keowee Auxiliary Transformers (1X and 2X);
- 3) Keowee Backup Auxiliary Transformer (CX);

the reactor may be heated above 200°F if previously shutdown or be permitted to remain critical or be restarted provided the following restrictions are observed:

- (a) Prior to heating the reactor above 200°F or prior to the re-start of a shutdown reactor or within 72 hours of the loss of any one of the following:
 - 1) Keowee Main Step-up Transformer (including both Keowee Auxiliary Transformers);
 - 2) Both Keowee Auxiliary Transformers (1X and 2X);
 - 3) Keowee Backup Auxiliary Transformer (CX);the 4160 volt standby buses shall be energized by a Lee gas turbine through the 100kV circuit. The Lee gas turbine and 100kV transmission circuit shall be electrically separate from the system grid and off-site non-safety related loads.
- (b) A Keowee hydro unit shall be connected to the underground feeder circuit and this path shall be verified operable within 1 hour and weekly thereafter.
- (c) The remaining Keowee Hydro Unit shall be available to the overhead if using this Specification due to Keowee Backup Transformer (CX) unavailability. Generation to the system grid shall be prohibited except for periods of test.

If the overhead path is unavailable, the remaining Keowee Hydro Unit must be operable and shall be available to the underground feeder circuit.

- (d) Operating in this mode is restricted to periods not to exceed 28 days and the provisions of this specification may be utilized without prior NRC approval. The U.S. NRC Regional Office Region II, will be notified within 24 hours.

3.7.9 Any degradation beyond Specifications 3.7.2, 3.7.4, 3.7.5, 3.7.6, 3.7.7, and 3.7.8 above shall be reported to the U.S. NRC Regional Office, Region II, within 24 hours. A safety evaluation shall be performed by Duke Power Company for the specific situation involved which justifies the safest course of action to be taken. The results of this evaluation together with plans for expediting the return to the unrestricted operating conditions of Specification 3.7.1 above shall be submitted in a written report to the Office of Nuclear Reactor Regulation with a copy to the U.S. NRC Regional Office, Region II, within five days.

Bases

The auxiliary electrical power systems are designed to supply the required Engineered Safeguards loads in one unit and safe shutdown loads of the other two units and are so arranged that no single contingency can inactivate enough engineered safety features to jeopardize plant safety. These systems were designed to meet the following criteria:

"Alternate power systems shall be provided and designed with adequate independency, redundancy, capacity and testability to permit the functions required of the engineered safety features of each unit."

The auxiliary power system meets the above criteria and the intent of Criterion 17 of Appendix A to 10 CFR Part 50. The adequacies of the AC and DC systems are discussed below as are the bases for permitting degraded conditions for AC power.

Capacity of AC Systems

The 4kV auxiliaries of two units in hot shutdown (6.2MVA each) plus the auxiliaries of the one unit with a LOCA (7.8MVA) require a total AC power capacity of 20.2 MVA. The continuous AC power capacity available from the on-site power systems (Keowee Hydro Units) is 22.4 MVA (limited by transformer CT4) if furnished by the underground circuit or 30 MVA (limited by CT1, CT2, or CT3) if furnished through the 230kV off-site transmission lines. Capacity available from the backup 100 kV off-site transmission line (Lee Station Gas Turbine Generator) is 22.4 MVA (limited by CT5).

Thus, the minimum available capacity from any one of the multiple sources of AC power, 22.4 MVA, is adequate.

The adequacy of the Oconee electrical distribution system voltages has been evaluated. Under the conservative assumptions of the analysis, it has been established that a single startup transformer should not be shared between two operating units. In the event a startup transformer becomes inoperable, it effectively causes one onsite emergency power path to the affected unit to become inoperable. The time frames for the degraded mode of an inoperable startup transformer are thus consistent with those for an inoperable onsite emergency power path. Because the preferred mode of unit shutdown is with reactor coolant pumps providing forced circulation and because of the low likelihood of an accident during a 72 hour period, the unit which is being shut down is allowed to share a startup transformer with another unit until the unit is in cold shutdown with loads being powered from the standby buses.

Capacity of DC Systems

Normally, for each unit AC power is rectified and supplies the DC system buses as well as keeping the storage batteries on these buses in a charged state. Upon loss of this normal AC source of power, each unit's DC auxiliary systems important to reactor safety have adequate stored capacity (ampere-hours) to independently supply their required emergency loads for at least one hour. One hour is considered to be conservative since there are redundant sources of AC power providing energy to these DC auxiliary systems. The loss of all AC power to any DC system is expected to occur very infrequently, and for very short periods of time. The following tabulation for the service test demonstrates the margin of installed battery charger rating and battery capacity when compared to one hour of operation (a) with AC power (in amps) and (b) without AC power (in ampere hours) for each of the three safety-related DC systems installed at Oconee:

A. 125 VDC Instrumentation and Control Power System

Charger XCA, XCB, or XCS
Battery XCA or XCB Capacity
(X = 1, 2, or 3)
Combined total connected loads
on both 125 VDC
I & C buses XDCA and XDCE
during 1st hour of LOCA
(x = 1, 2, or 3)

- a. 600 amps each
- b. 825 ampere-hours each
- a. Inrush (2 sec) - 709 amps
- b. next 59 min. - 566 amps
- b. 568.4 ampere-hours

B. 125 VDC Switching Station Power Systems

Charger SY-1, SY-2, or SY-s Rating
Battery SY-1 or SY-2 Capacity

- a. 50 amps each
- b. 160 ampere-hours each
- a. Inrush (2 seconds) - 130 amps
- b. next 59 min. - 10 amps
- b. 12 ampere-hours

Active load per battery
during 1st hour of LOCA

C. 125 VDC Keowee Station Power System

Charger No. 1, No. 2 or Standby Rating
Battery No. 1 or No. 2 Capacity

- a. 200 amps each
- b. 975 ampere-hours each
- a. Inrush (14 seconds) - 775.5 amps
- b. next 59 min. - 114.7 amps
- b. 125.7 ampere-hours

Active load per battery
during 1st hour of LOCA

A single string or component of the 125 VDC safety related distribution system may be inoperable for periods not exceeding 24 hours as described in Specification 3.7.2(e). In the case of the annual discharge test required by Specification 4.6.10 and the battery performance test (per IEEE Standard 450), a longer time period of up to 72 hours is allowed for the required equalizing charge.

In addition to the service test, the battery performance test may be conducted every 5 years (per IEEE standard 450), unless there are signs of degradation. Degradation is indicated when the battery capacity drops more than 10 percent of rated capacity from its average on previous performance tests, or is below 90 percent of manufacturer's rating. If there is degradation per above definition, the test should be conducted annually until the battery is replaced or until tests prove the battery is not in a degraded state.

Redundancy of AC Systems

There are three 4160 V engineered safety feature switchgear buses per unit. Each bus can receive power from either of the two 4160 V main feeder buses per unit. Each feeder bus in turn can receive power from the 230 kV switchyard through the start-up transformers, through the unit auxiliary transformer by backfeeding through the main step-up transformer, or from the 4160 V standby buses. Another unit's start-up transformer serving as an alternate supply can be placed in service in one hour.

Under normal unit auxiliary power system alignment, the main feeder buses shall be capable of receiving power automatically from:

1. The Keowee Unit aligned to the underground, through transformer CT-4, and through both standby buses; and
2. The redundant Keowee Unit, aligned through the overhead path; and through the respective Unit's startup transformer.

The standby buses can receive power from the hydro station through the underground feeder circuit or from a combustion turbine generator at the Lee Steam Station over an isolated 100 kV transmission line. The 230 kV switchyard can receive power from the on-site Keowee hydro station or from several off-site sources via transmission lines which connect the Oconee Station with the Duke Power system power distribution network.

In order to meet the single failure criteria for certain design basis scenarios, both standby buses (for the underground flow path), and both E₁ and E₂ breakers (for the overhead path) must be operable for the respective flow path to be considered operable.

Redundancy of DC System

A. 125 VDC Instrumentation and Control Power System

The 125 VDC Instrumentation and Control (I&C) Power System consists of two batteries, three battery chargers, and two I&C distribution centers per unit. All reactor protection and engineered safety features loads on this system can be powered from either the Unit 1 and Unit 2 or Unit 2 and Unit 3 or Unit 3 and Unit 1 125 VDC I&C distribution centers. The 125 VDC I&C distribution centers are normally supplied from their associated battery and charger. For one unit, in the event that only one of its batteries and associated chargers are operable, both I&C distribution centers will be tied together allowing operation of the DC loads from the unit's operable battery and charger. As shown above, one I&C battery (e.g., ICA) can supply both I&C distribution centers (e.g., IDCA and IDCB) and their associated panelboard loads. Also, one of the three battery chargers for each unit can supply all connected ESF and reactor protection loads.

In order to find and correct a DC ground on the 125 VDC Instrumentation and Control system each unit's DC system must be separated from the other two units. This is due to the interconnected design of the system. With the backup function disabled the units would be in a degraded mode but would in fact have all of its own DC system available if needed. Each unit's batteries either XCA or XCB is capable of carrying all the 125 VDC Instrumentation and Control loads on that unit.

B. 125 VDC Switching Station Power System

There are two essentially independent subsystems each complete with an AC/DC power supply (battery charger), a battery bank, a battery charger bus, motor control center (distribution panel). All safety-related equipment and the relay house in which it is located are seismic Category I design. Each subsystem provides the necessary DC power to:

- a. Continuously monitor operations of the protective relaying.

- b. Isolate Oconee (including Keowee) from all external 230 kV grid faults,
- c. Connect on-site power to Oconee from a Keowee hydro unit or,
- d. Restore off-site power to Oconee from non-faulted portions of the external 230 kV grid.

Provisions are included to manually connect a standby battery charger to either battery/charger bus.

C. 125 VDC Keowee Station Power System

There are essentially two independent physically separated seismic Category I subsystems, each complete with an AC/DC power supply (charger), a battery bank, a battery/charger bus and a DC distribution center. Each subsystem provides the necessary power to automatically or manually start, control and protect one of the hydro units.

An open or short in any one battery, charger, or DC distribution center, cannot cause loss of both hydro units.

The 230 KV sources, while expected to have excellent availability, are not under the direct control of the Oconee station and, based on past experience, cannot be assumed to be available at all times. However, the operation of the onsite hydro-station is under the direct control of the Oconee Station and requires no offsite power to start up. Therefore, an onsite backup source of auxiliary power is provided in the form of twin hydro-electric turbine generators powered through a common penstock by water taken from Lake Keowee. The use of a common penstock is justified on the basis of past hydro plant experience of the Duke Power Company (since 1919) which indicates that the cumulative need to dewater the penstock can be expected to be limited to about one day a year, principally for inspection, plus perhaps four days every tenth year.

Operation with one Keowee Hydro unit out of service for periods less than 72 hours is permitted. The operability of the remaining Keowee hydro unit is verified within one hour by starting the unit and energizing the standby buses through the underground feeder circuit. This action is repeated once every eight hours thereafter until the Keowee hydro unit is restored to service and will provide additional assurance of the operability of the remaining unit.

Provisions have been established for those conditions in which long term preventative maintenance of a Keowee Hydro unit are necessary. The primary long term maintenance items are expected to be hydro turbine runner and discharge ring welding repairs which are estimated to be necessary every six to eight years. Also, generator thrust and guide bearing replacements will be necessary. Other items which manifest as failures are expected to be extremely rare and could possibly be performed during the permitted maintenance periods. Time periods of up to 45 days for each Keowee Hydro unit are permitted every three years. During these outages the remaining Keowee Hydro unit will be verified to be operable within one hour and weekly thereafter by starting the unit and energizing the underground feeder circuit to CT-4. Credit can be taken for the operability of the SK and S breakers per the routine surveillance test. The remaining Keowee hydro unit will also be available through

the overhead transmission path and will not be used for system peaking. Additionally, the standby buses will be energized continuously by one of the Lee gas turbines through the 100 kV transmission circuits.

This transmission circuit would be electrically separated from the system grid and all off-site non-safety-related loads. This arrangement provides a high degree of reliability for the emergency power systems.

Operation with both Keowee Hydro units out of service is permitted for planned or unplanned outages for periods of 72 or 24 hours respectively. Planned outages are necessary for the inspection of common underwater areas such as the penstock and to enable the removal of one Keowee unit from service. This would be a controlled evolution in which the availability and condition of the offsite grid, startup transformers and weather would be evaluated and a Lee gas turbine would be placed in operation on the isolated 100 kV transmission line prior to commencement of the outage.

A time period of 24 hours for unplanned outages of both Keowee units is acceptable since a Lee gas turbine will be started within one hour and will energize the standby buses through the dedicated 100 kV transmission line. This period of time is reasonable to determine and rectify the situation which caused the loss of both Keowee units.

If the overhead power path from Keowee is inoperable for more than 72 hours due to an extended outage of the Keowee main step-up transformer, both Keowee Auxiliary Transformers (1X and 2X), or Keowee Backup Auxiliary Transformer (CX), operation is permitted provided that certain actions are taken to ensure the quick availability of emergency power. These actions include: continuous energization of the standby buses by a Lee gas turbine through the 100kV transmission circuits; connection of a Keowee unit to the underground feeder path and periodic verification of its operability; and, availability of the remaining Keowee unit to the underground feeder path. Operation in this mode is permitted for a maximum of 28 days, which allows a reasonable period of time to remove the existing transformer and install a replacement.

In the event that none of the sources of off-site power are available and it is considered important to continue to maintain an Oconee reactor critical or return it to criticality from a hot shutdown condition, one of the Lee gas turbines can be made available as an additional backup source of power, thus assuring continued availability as an auxiliary power to perform an orderly shutdown of a unit should a problem develop requiring shutdown of both hydro units.

The power system of the Keowee Hydro station is designed to allow the alignment of each of the two units to the Oconee emergency power systems through either the underground feeder or the overhead path via the main step-up transformer. During an emergency start one of the Keowee units will be aligned to the underground feeder and the other to the overhead path. Each Keowee unit's 600VAC auxiliaries are powered from the unit's generator through a 750KVA auxiliary transformer. Each auxiliary transformer is capable of handling auxiliary loads of both units. Unit's auxiliaries can be aligned to receive power from either transformer by a manual transfer capability at the load center level. A backup 750KVA auxiliary transformer (CX) is provided and powered from Oconee 4KV switchgear 1TC through an underground feeder.

Transformer CX is capable of backing up one or both units' auxiliary transformers.

Each Keowee unit has a generation capacity of 87.5 MVA and the main step-up transformer is rated for 230 MVA. This power capacity exceeds the Oconee emergency power requirements.

Emergency Power Switching Logic Circuits

The Emergency Power Switching Logic (EPSL) in conjunction with its associated circuits, is designed with sufficient redundancy to assure that power is supplied to the unit Main Feeder Buses and, hence, to the unit's essential loads, under accident conditions. The logic system monitors the normal and emergency power sources and, upon loss of the normal power source (the unit auxiliary transformer), the logic will seek an alternate source of power.

Operation of the unit with certain circuits or channels of the EPSL inoperable for test or maintenance is permitted for periods of up to 24 hours, provided that the inoperable circuits/channels are in only one portion, or functional unit, of the EPSL and provided that a sufficient number of circuits/channels in the affected functional unit remain operable such that the functional unit does not lose its ability to perform its designed safety function. These provisions ensure that only one portion of the EPSL is degraded at a time for test or maintenance on the EPSL and that the affected portion remains operable although degraded.

Emergency power system components (transformers, buses, Keowee Hydro Units, etc.) which become inoperable for testing or maintenance cause their associated circuitry (functional units) of the EPSL to become ineffective. Therefore, the operability of these associated functional units is irrelevant and not required. In these cases the controlling Technical Specification for the LCO will be the one associated with the inoperability of the emergency power system component(s). However, all other functional units unaffected by the inoperability of the emergency power system component(s) must meet the requirements of Table 3.7-1 to ensure the operability of the remaining emergency power system.

In the event a 125 VDC instrumentation and control power panelboard becomes inoperable (for planned or unplanned reasons) as allowed by Technical Specification 3.7.2(e) (4), circuits or channels of more than one functional unit of EPSL may become inoperable. In this case, continued operation is allowed under the LCO of T.S. 3.7.2(e) (4), provided that no functional units' circuits, etc., addressed by Table 3.7.1 are out of service, which would not have been out of service due to inoperability of the panelboard. This assures that no functional unit of Table 3.7.1 is degraded beyond the requirements for degraded operation, and that the EPSL is capable of performing its intended function.

In the event that the EPSL is in a degraded mode while the reactor is subcritical, a return to criticality may not be made unless the return to criticality is permitted by a controlling Technical Specification for an emergency power system component(s). However, all functional units of the EPSL not affected by the inoperability of the emergency power system component(s) must be operable prior to return to criticality. This ensures the availability of the EPSL during all reactor startups.

The normal source breakers (N_1 and N_2) provide power to the main feeder buses from the auxiliary transformer under normal power operation of the plant. Under accident conditions the normal breakers open to allow an emergency power flowpath to the main feeder buses. Since there is no emergency closing function, the N_1 and N_2 breakers may be opened and control circuitry deenergized without degrading the capability of the EPSL to perform its intended safety function. Therefore, while the N_1 and N_2 breakers are open, Technical Specification 3.7.2(b) is considered to be satisfied with respect to N_1 and N_2 functional units of the EPSL.

120 VAC Vital Instrumentation Power Panelboards

For each unit, four redundant 120 VAC vital instrument power panelboards are provided to supply power in a predetermined arrangement to vital power, instrumentation, and control loads under all operating conditions. Each panelboard is supplied power separately from a static inverter connected to one of the four 125 VDC instrumentation and control power panelboards. In addition, a tie with breakers is provided to each of the 120 VAC vital panelboards from the alternate 120 VAC regulated bus to provide backup for each vital panelboard and to permit servicing of the inverters.

For each unit, each of the four redundant channels of the nuclear instrumentation and reactor protective system (RPS) equipment is supplied power from a separate 120 VAC vital panelboard. Also for each unit, each of the three redundant engineered safety features actuation system (ESFAS) analog channels and each of the two redundant ESFAS digital channels are powered from separate vital panelboards.

The period allowed for corrective action on an inoperable vital panelboard depends on the loads carried by the affected panelboard. For example, panelboards KVIA and KVIB are allowed to be inoperable for only four hours because they provide power to the digital ESFAS channels, which are in turn allowed to be inoperable for only four hours by Technical Specification 3.5.1. In contrast, panelboards KVIC and KVID carry loads which do not necessarily become inoperable upon loss of power (e.g., RPS channels and ESFAS analog channels go to a tripped state upon loss of power) and thus do not necessitate immediate corrective action. Thus, these panelboards have been limited to a period of inoperability which does not exceed that allowed for their normal source of power, the 125 VDC instrumentation and control panelboards.

In the event that failure of a static inverter results in the inoperability of its associated vital panelboard, the affected panelboard may be tied to the 240/120 VAC regulated power system and unit operation may continue for seven days. This specification allows sufficient time for the inverter to be repaired without penalizing unit operation by permitting the use of alternate power sources.

Reporting Requirements

Specification 3.7.9 includes reporting requirements in the event there is degradation beyond Specifications 3.7.2, 3.7.4, 3.7.5, 3.7.6, 3.7.7, or 3.7.8. The 24 hour report to Region II is accomplished by 10 CFR 50.72 notification of the NRC operations center. The 5 day written report has been established to provide the NRC the results of safety evaluations in the event the degraded condition will be ongoing.

TABLE 3.7-1

OPERABILITY REQUIREMENTS FOR THE
EMERGENCY POWER SWITCHING LOGIC CIRCUITS

Functional Unit	Minimum Operable Circuits/Channels	
	Normal Operation Per Spec 3.7.1(c)	Degraded Operation Per Spec 3.7.2(b)
1. Normal Source Voltage Sensing Circuits (One per Phase)	3	2
2. Startup Source Voltage Sensing Circuits (One per Phase)	3	2
3. Standby Bus Voltage Sensing Circuits (One per Phase on each bus)	6	4 ^a
4. Main Feeder Bus Undervoltage Relays (Three per bus)	6	4 ^a
5. Load Shed and Transfer to Standby Circuits (Channels A and B)	2	1
6. Keowee Emergency Start Circuit (Channels A and B)	2	1
7. Retransfer to Startup Circuits (Channels A and B)	2	1
8. Normal Source Breakers N1* and N2 Control Circuitry	4 ^b	2 ^c

Notes:

- 2 per bus.
- 2 trip coils and associated trip circuitry for each breaker.
- 1 trip coil and associated trip circuitry for each breaker.

*The trip coils and associated trip circuitry for the N₁ and/or N₂ breaker(s) are not required to be operable if the breaker(s) are in the tripped position.