

Calvert Cliffs GSI-191 Program

Zone of Influence, Debris Size Distribution,
Option 2b Closure Approach, and
LAR Exemption Request

July 18, 2016



Exelon Generation®

Agenda

- Introductions
- Objectives for Meeting
 - Option 2b Simplified Risk-Informed Closure Plan
 - Strainer Performance Criteria
 - LOCA Frequency Allocation
 - LAR Exemption Request
 - Zone of Influence and Debris Size Distribution
- Staff Questions & Concerns
- Schedule for Future Periodic Meetings

CCNPP Attendees

- Doug Lauver – Senior Engineering Manager
- Andre Drake – Lead Responsible Engineer GSI-191
- Jim Landale – Lead PRA Engineer
- Ken Greene – Licensing Engineer
- Craig Sellers – Project Manager GSI-191
- Eric Federline – Project Support

Objectives of this Meeting

- Discussion of Calvert Cliffs Simplified Risk-Informed Approach
 - Strainer Performance Criteria
 - LOCA Frequency Allocation
 - LAR Exemption Request
- Discussion of Revised ZOIs and Debris Size Distributions
- Capture Staff Issues and Concerns
- Discuss Next Steps

Simplified Risk-Informed Approach

Strainer Performance Criteria

- Strainer Failure Modes:
 - Pump NPSH
 - Structural Failure
 - Deaeration – Limiting Failure Mode
- Strainer Performance Criteria
 - 1) Mass of Fine Fiber Debris
 - 2) Mass of Particulate Debris
 - 3) Mass of WCAP-16530 Chemical Precipitate Debris*
 - * Provided sufficient fiber to cover strainer $\geq \frac{1}{16}$ "
- Preliminary Results
 - 19 of 62 Welds ≥ 30 " ID Exceed Criteria of Fiber and/or Precipitate Mass
 - 7 of 19 Exceed only Precipitate Criterion
 - 2 of 72 12" ID Welds Exceed Precipitate Criterion
 - Equivalent Uniform Fiber Bed Thickness $\sim \frac{1}{23}$ " and $\frac{1}{28}$ "
 - Insufficient Debris Bed to Capture Precipitate
 - No Threat to Strainer Performance

Simplified Risk-Informed Approach (continued)

Calculate Δ CDF – Preliminary Results

- Use Conservative Approach
 - Smallest break that threatens strainer performance – 30” DEGB
 - NUREG-1829 LOCA Frequencies
 - Equally Apportion LOCA Frequency Across RCS Welds
 - Degradation mechanisms are Design and Construction for all 62 RCS welds
 - PWSCC also on 8 RCS welds
- NUREG-1829 LOCA Frequencies

LOCA Category	Break Size (in.)	Geometric Mean ¹	Arithmetic Mean ²
1	≥ 0.5	1.90E-03	1.00E-02
2	≥ 1.625	4.20E-04	3.00E-03
3	≥ 3	1.60E-05	7.30E-05
4	≥ 7	1.60E-06	9.40E-06
5	≥ 14	2.00E-07	2.40E-06
6	≥ 31	2.90E-08	1.50E-06
Notes:			
[1] Taken from Table 7-19 of NUREG-1829			
[2] Taken from Table 7-13 of NUREG-1829			

- Log-Linear Interpolation

LOCA Category	Break Size (>in.)	Geometric Mean	Arithmetic Mean
1	≥ 0.5	1.90E-03	1.00E-02
2	≥ 1.625	4.20E-04	3.00E-03
3	≥ 3	1.60E-05	7.30E-05
4	≥ 7	1.60E-06	9.40E-06
5	≥ 14	2.00E-07	2.40E-06
5.5	≥30	3.25E-08	1.54E-06
6	≥ 31	2.90E-08	1.50E-06
# Welds	#Failed	Δ CDF GM	Δ CDF AM
62	22	1.15E-08	5.47E-07

- 62 Butt Welds ≥ 30”
- 19 Welds ≥ 30” Threaten Strainer Performance
- 3 are DM Welds – Double Counted

Simplified Risk-Informed Approach (continued)

License Amendment Request

- Calvert Cliffs Planning to Request Exemption from 10CFR50.46(a)(1.)
 - Similar to South Texas Project
- Calvert Cliffs not licensed to 10CFR50 Appendix A General Design Criteria
 - Do not need exemption from GDC

Zone of Influence & Debris Size Distribution

- CCNPP Submitted Supplemental Response to GL 2004-02 on June 8, 2016
 - Addressed Revised ZOI and Debris Size Distributions for:
 - NUKON & Thermal Wrap Blanket Insulation
 - Mineral Wool Insulation in Stainless Steel Cassettes
 - Generic Fiberglass Insulation
 - Lead Wool Shielding Blankets
 - Based on data accepted at other plants

ZOI & Debris Size Distribution – NUKON & Thermal Wrap

- 3 Zones of Influence, 4 Debris Size Distribution
- ENERCON Approach using Insulation Centroid
- Based on NEI 04-07 Safety Evaluation Guidance
- Accepted at Other Plants

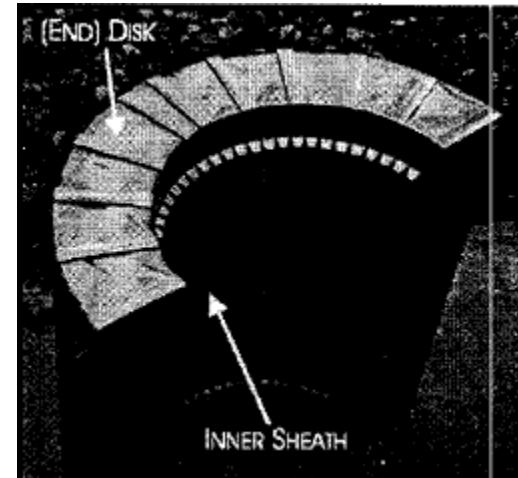
Debris Size	Average (Centroid) Distance from Break Location to Target		
	0D - 4D ZOI	4D - 15D ZOI	15D - 17D ZOI
Fines Fraction (F_{fines})	$F_{fines} = 0.2$	$F_{fines} = -0.01364 \times C + 0.2546$	$F_{fines} = -0.025 \times C + 0.425$
Small Pieces Fraction (F_{small})	$F_{small} = 0.8$	$F_{small} = -0.0682 \times C + 1.0724$	$F_{small} = -0.025 \times C + 0.425$
Large Pieces Fraction (F_{large})	$F_{large} = 0$	$F_{large} = 0.0393 \times C - 0.157$	$F_{large} = -0.215 \times C + 3.655$
Intact Pieces Fraction (F_{intact})	$F_{intact} = 0$	$F_{intact} = 0.0425 \times C - 0.170$	$F_{intact} = 0.265 \times C - 3.505$

ZOI & Debris Size Distribution – Mineral Wool

- Mineral Wool at CCNPP is Transco Stainless Steel Cassette Design
- 0.024” SS Sheath with Slotted End Panels
 - Installed in Plant



Tested at CEESI, Tests 22-1 to 22-3



- Tested cassettes contained metal foil and produced none or very little transportable debris.
- The contained material contributes no strength to the cassettes.
- Therefore, the destruction pressure for the Transco mineral wool cassettes and RMI cassettes are considered equal.
- To account for the difference in filler material, the ZOI for the mineral wool cassettes will be conservatively increased by a factor of 2 from 2.0D to 4.0D.
- The debris size for the mineral wool will be conservatively assumed to be 100% fine fibers.

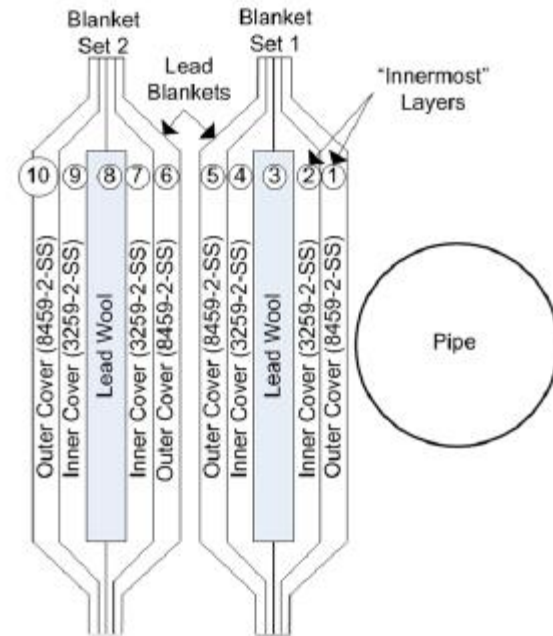
ZOI & Debris Size Distribution – Generic Fiberglass

- Anti-Sweat Insulation on Unit 1 CCW piping
- Molded of heavy density resin bonded inorganic glass fibers
- Jacketed with 0.010” riveted stainless steel
- Bulk density generally greater than Nukon and Thermal Wrap.
 - 3.5 to 5.5 lbm/ft³ verses 2.4 lbm/ft³
- The mass percentage of generic fiberglass relative to total fibrous debris load is <20% for the bounding break at Calvert Cliffs.
- Calvert Cliffs assumes that the ZOI and debris size distribution for generic fiberglass is that used for Nukon and Thermal Wrap based on the insulation density.

Debris Size	Average (Centroid) Distance from Break Location to Target		
	0D - 4D ZOI	4D - 15D ZOI	15D - 17D ZOI
Fines Fraction (F_{fines})	$F_{\text{fines}} = 0.2$	$F_{\text{fines}} = -0.01364 \times C + 0.2546$	$F_{\text{fines}} = -0.025 \times C + 0.425$
Small Pieces Fraction (F_{smalls})	$F_{\text{smalls}} = 0.8$	$F_{\text{smalls}} = -0.0682 \times C + 1.0724$	$F_{\text{smalls}} = -0.025 \times C + 0.425$
Large Pieces Fraction (F_{large})	$F_{\text{large}} = 0$	$F_{\text{large}} = 0.0393 \times C - 0.157$	$F_{\text{large}} = -0.215 \times C + 3.655$
Intact Pieces Fraction (F_{intact})	$F_{\text{intact}} = 0$	$F_{\text{intact}} = 0.0425 \times C - 0.170$	$F_{\text{intact}} = 0.265 \times C - 3.505$

ZOI & Debris Size Distribution – Lead Wool Shielding Blankets

- Two Zones of Influence, 3 Debris Size Distribution
- ZOI based on CESSI Air Jet Impact Tests
- Typical Installed Configuration



Debris Type	Size	Size Distribution	
		2.1D ZOI	2.1D – 5.4D ZOI
Lead Blanket Cover Layers Closest to Pipe Break (Open Back Configuration)	Fines	20%	0%
	Small Pieces	80%	0%
	Large/Intact Pieces	0%	100%
Remaining Lead Blanket Cover Layers (Open Back Configuration)	Fines	0%	0%
	Small Pieces	0%	0%
	Large/Intact Pieces	100%	100%
Wrapped Lead Blanket Cover Layers (Strong Back Configuration)	Fines	0%	0%
	Small Pieces	0%	0%
	Large/Intact Pieces	100%	100%

Questions/Concerns

- Jointly Review Issues, Questions, and Concerns for Future Communication

Next Steps

- Finalize Update of Deterministic Calculations
- Present Formal Risk-Informed GSI-191 Analysis and Results
- Desire Next Meeting – 4Q 2016