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Lawrence Coyle Site Vice President

NL-16-053

May 31, 2016

U.S. Nuclear Regulatory Commission Document Control Desk 11545 Rockville Pike, TWFN-2 F1 Rockville, MD 20852-2738

SUBJECT: Licensee Event Report # 2016-004-00, "Unanalyzed Condition due to Degraded Reactor Baffle-Former Bolts" Indian Point Unit No. 2 Docket No. 50-247 DPR-46

Dear Sir or Madam:

Pursuant to 10 CFR 50.73(a)(1), Entergy Nuclear Operations Inc. (ENO) hereby provides Licensee Event Report (LER) 2016-004-00. The enclosed LER identifies an event where there was an unanalyzed condition due to degraded reactor baffle-former bolts, which is reportable under 10 CFR 50.73(a)(2)(ii)(B). This condition was recorded in the Entergy Corrective Action Program as Condition Reports CR-IP2-2016-02081 and CR-IP2-2016-02348.

There are no new commitments identified in this letter. Should you have any questions regarding this submittal, please contact Mr. Robert Walpole, Manager, Regulatory Assurance at (914) 254-6710.

Sincerely,



cc: Mr. Daniel H. Dorman, Regional Administrator, NRC Region I NRC Resident Inspectors Ms. Bridget Frymire, New York State Public Service Commission

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NRC FORM 366 U.S. NUCLEAR REGULATORY COMMISSION							DN 🗌	APPROVED BY OMB: NO. 3150-0104 EXPIRES: 10/31/2018								
(11-2015)	(11-2015) LICENSEE EVENT REPORT (LER) (See Page 2 for required number of digits/characters for each block) Estimated burden per response to comply with this mandatory collection request: 80 hours Reported lessons learned are incorporated into the licensing process and fed back to industry Send comments regarding burden estimate to the FOIA, Privacy and Information Collection Branch (T-5 F53), U.S. Nuclear Regulatory Commission, Washington, DC 20555-0001, or b internet e-mail to Infoccilects.Resource@nrc.gov, and to the Desk Officer, Office of Information an Regulatory Affairs, NEOB-10202, (3150-0104), Office of Management and Budget, Washingtor DC 20050. If a means used to impose an information collection does not display a currently vali OMB control number, the NRC may not conduct or sponsor, and a person is not required to respond to, the information collection.															
1. FACILITY NAME 2. DOCKET NUMBER 3. PAGE Indian Point 2 05000-247 1 OF 6																
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5. E	5. EVENT DATE 6. LER NUMBER 7. REPORT I						T DA	TE 8. OTHER FACILITIES INVOLVED								
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9. OPERATING MODE 11. THIS REPORT IS SUBMITTED PURSUANT TO THE REQUIREMENTS OF 10 CFR §: (Check all that apply) □ 20.2201(b) □ 20.2203(a)(3)(i) □ 50.73(a)(2)(ii)(A) □ 50.73(a)(2)(viii)(A)								2)(viii)(A)								
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						12.	LICENS	ÉE CON	ÍTAC	T FO	R THI	SLER				
ICENSEE CONTACT Nelson Azevedo, Supervisor, Code Programs											NE NUMER (Inc 4) 254 -		a Code)			
13. COMPLETE ONE LINE FOR EACH COMPONENT FAILURE DESCRIBED IN THIS REPORT																
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result of the inspection, 227 battle-former bolts were identified to have either visual anomalies or ultrasonic indications or could not be examined by ultrasonic testing. A visual inspection of the baffle-former plates and edge bolts showed no discernible material degradation or distortion. All other MRP-227-A inspections of the reactor vessel internals showed no other failures or premature degradation.

The root cause of the failed baffle-former bolts is primarily Irradiation Assisted Stress Corrosion Cracking (IASCC) in combination with applied stresses and fatigue loads. Failure analyses will be conducted to confirm the cause for the degradation of the baffle-former bolts.

At the time of discovery, the unit was in a safe and stable condition with all fuel removed from the reactor vessel. The event had no impact on public health and safety.

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NRC FORM 366A U.S. NUCLEAR REGULATORY COMMISS			APPROVED BY OMB: NO. 3150-01	4 EXPIRES: 10/31/2018			
(11-2015)	LICENSEE EVENT REI		lessons learned aré incorporated into tr comments regarding burden estimate to tr F53), U.S. Nuclear Regulatory Commissic Infocollects.Resource@nrc.gov, and to the NEOB-10202, (3150-0104), Office of Mana used to impose an information collection do	ith this mandatory collection request: 80 hours. e licensing process and fed back to indus e FOIA, Privacy and Information Collections Br. n, Washington, DC 20555-0001, or by interne Desk Officer, Office of Information and Regulato gement and Budget, Washington, DC 20503. If es not display a currently valid OMB control nu a person is not required to respond to, the ir		industry. Send ns Branch (T-5 ternet e-mail to gulatory Affairs, 03. If a means ol number, the	
1. FACILITY NAME		2. DOCKET NUMBER		3. LER NUMBER			
Indian Point 2				YEAR	SEQUENTIAL NUMBER	REV NO.	
		05000-247		2016	- 004	- 00	

NARRATIVE

Note: The Energy Industry Identification System Codes are identified within the brackets {}.

DESCRIPTION OF EVENT

Indian Point Unit 2 (IP2) was shut down as scheduled on March 7th, 2016 to implement the 2R22 refueling outage. As part of the IP2 License Renewal process, Entergy committed to performing inspections of the reactor vessel internal components {AB} during the 2R22 refueling outage. The NRC has approved EPRI Technical Report MRP-227-A, "Materials Reliability Program: Pressurized Water Reactor Internals Inspection and Evaluation Guidelines," as an acceptable vehicle for performing aging-related inspections and evaluations of applicable reactor components. One set of components inspected under MRP-227-A were the baffle-former bolts through visual inspection (VT) and ultrasonic (UT) examination.

The IP2 baffle structure includes 832 baffle-former bolts which attach the baffle plates to the former plates. Of the 832 baffle-former bolts, 227 either failed to meet acceptance criteria or could not be UT inspected. The UT inspection identified indications on 182 bolts, 14 were incapable of being UT inspected and were thus conservatively assumed to have failed, and 31 bolts failed the VT. The failed baffle-former bolts are distributed throughout the vertical baffle plates with more failures found in the upper portion of the plates and more concentrated on some of the plates than others (the failures are clustered).

The 227 failed bolts and the pattern of failure did not meet the acceptance criteria for plant startup from the 2R22 refueling outage which had been provided by Westinghouse prior to the outage in an analysis of the baffle-former assembly in WCAP-18048-P. The consequence of this is that baffle-former bolt replacements were required to be completed prior to returning IP2 back to service.

The reactor vessel (RV) {RPV} is cylindrical in shape with a hemispherical bottom and a flanged and gasketed (O-rings) removable upper head. The vessel contains the reactor core, the core support structures, control rod clusters {AA}, thermal shield, and other components. The RV Lower Internal Assembly provides support for the core and channels reactor coolant flow through the fuel assemblies {AC}. The main element of the Lower Internals Assembly is the core barrel, which is a cylindrical structure fabricated from welded plate that is supported at its upper flange by a ledge in the RV main flange. The core barrel includes the baffle-former assembly, which is bolted directly to the lower core barrel. This stainless steel assembly is a bolted configuration consisting of eight (8) horizontal former plates and twenty-eight (28) vertical baffle plates which provide the transition from the cylindrical core barrel to a geometry that accepts rectangular fuel assemblies. The assembly forms a boundary for the flow of reactor coolant and provides some lateral support for the fuel assemblies for both normal and abnormal operation. The former plates are bolted to the core barrel and the baffle plates are bolted to the former plates with 832 baffle-former bolts.

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The baffle-former bolts are SA-479 Type 347 annealed stainless steel fabricated to a Westinghouse specification. Each bolt was installed within a counter-bore in the baffle plate, recessed such that the top of the bolt head is flush with the baffle plate surface. The bolts were torqued to impose a required pre-load, and a locking tab was inserted into a milled slot in the bolt head and tack welded to the baffle plate at the locking tab ends. The locking tabs ensure that the bolt does not back out, and is also intended to capture loose parts that may be generated if a bolt breaks.

CAUSE OF EVENT

The root cause of the baffle-former bolt failures is primarily Irradiation Assisted Stress Corrosion Cracking (IASCC) and increased fatigue loading resulting from loss of preload. Failure of a critical number of bolts in a localized area subsequently imposed increased loading on adjacent bolts, thus increasing the probability of failure of the adjacent bolts and generating the clustered pattern seen in the inspection results. IASCC is a type of stress corrosion cracking of austenitic stainless steels and Nickel-based alloys that appears after irradiation in aqueous (water) environments. IASCC is typically intergranular and the amount of cracking increases with neutron exposure, until a saturation level is reached.

The Failure Mode Analysis (FMA) has considered various factors and has determined whether and to what extent they possibly could have impacted the failure mechanism. Based on the FMA results, it has been concluded that IASCC was the initiating degradation mechanism that resulted in flaws in the baffle-former bolts. Failure analyses of selected removed bolts will be performed to confirm this cause.

PAST SIMILAR EVENTS

None

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LICENSEE EVENT REPORT (LER) CONTINUATION SHEET

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CORRECTIVE ACTIONS

Corrective actions for this event include the following:

• In addition to the 227 bolts that were initially identified to be replaced, 49 bolts that did not have visual anomalies or ultrasonic indications were replaced to prevent clustering of failures. During replacement activities, 2 additional bolts were determined to require replacement.

In total, replacement baffle-former bolts were installed in 278 locations. The replacement bolt material is SA-479 Type 316 cold worked stainless steel with a new type of anti-rotational/locking mechanism. These replacement baffle-former bolts have been installed and utilized successfully at other operating plants since 1998. The original bolts are 0.625 inch diameter. The size of the replacement bolts is 0.625 inch diameter or 0.750 inch diameter, depending on whether the bolt required machining of the thread major diameter to remove it.

- Failure analyses of selected removed bolts will be performed.
- Perform inspection of the baffle-former bolts in refueling outage 2R23.
- Implement a project in refueling outage 2R23 to convert reactor flow configuration from downflow to upflow to improve margin for the baffle-former assembly.
- Perform additional baffle-former bolt replacements to meet minimum bolting pattern as evaluated by Westinghouse in 2R23.

EVENT ANALYSIS

The event was initially reportable under 10 CFR 50.72(b)(3)(ii)(B); the licensee shall report any event or condition that results in the nuclear power plant being in an unanalyzed condition that significantly degrades plant safety. As a press release to communicate the condition to stakeholders was made, the event was also reportable under 10 CFR 50.72(b)(2)(xi); the licensee shall report any event or situation, related to the health and safety of the public or on-site personnel, or protection of the environment, for which a news release is planned or notification to other government agencies has been or will be made. The event notification was made on March 29, 2016 (Event Number 51829).

The event is reportable under 10CFR50.73(a)(2)(ii)(B); the licensee shall report any event or condition that resulted in the nuclear power plant being in an unanalyzed condition that significantly degrades plant safety. A minimum number of baffle-former bolts are required for structural integrity and core cooling as determined in an analysis of the baffle-former assembly in WCAP-18048-P. As determined by the visual and UT inspections, this minimum number was exceeded.

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SAFETY SIGNIFICANCE

There were no actual consequences to the general safety of the public, to nuclear safety, to industrial safety or to radiological safety, as there have been no events prior to or during 2R22 where the potentially compromised baffle-former assembly could have negatively affected the outcome of these events.

The potential consequences to the general safety of the public, to nuclear safety, to industrial safety or to radiological safety of the identified baffle-former bolt failures if a design transient or accident had occurred prior to 2R22 with the identified baffle-former assembly condition has been determined to be low, based on the discussion that follows.

The baffle-former bolting LOCA and seismic dynamic analyses and the core bypass flow evaluations confirmed that LOCA and seismic faulted events would not have caused damage to the fuel such that a core coolable geometry was maintained and the control rods would have successfully inserted. These two criteria ensure the safe shutdown of the plant. The analysis methodology used for this safety significance discussion is the same as that used in the acceptable baffle bolting pattern analysis (ABPA), with additional considerations.

A preliminary review of the IP2 piping shows that it can meet the requirements for expanded "Leak Before Break" (LBB) consideration for certain lines (10 and 14 inch diameter) interfacing with the Reactor Coolant loops, which have been analyzed at Westinghouse units similar in design to IP2. It is postulated that a flaw would develop prior to complete pipe rupture (single or double-ended), leading to leakage detectable by the existing RCS leakage detection systems and plant shutdown before the flaw could grow to an unstable size.

The original baffle former dynamic analysis assumes that all of the baffle-tobaffle edge bolts are no longer functional. Visual inspection of the baffle-tobaffle edge bolts and the fuel was also performed during 2R22. These inspections did not identify any damage to the edge bolts or evidence of baffle-gap jetting on the fuel. Therefore, the baffle edge bolts do impart some strength and rigidity to the baffle-former assembly and offset to an extent the failed baffle-former bolts.

The residual fractional strength for the failed baffle-former bolts was not credited in the analyses. However, both in shear and in tension, many if not most of the bolts with UT-identified indications retain some residual strength that would act to limit baffle plate displacement and/or flexure.

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Another consideration is the calculation of core bypass flow and momentum flux against the fuel. No baffle-gap jetting has been observed; therefore it is reasonable to conclude that the edge bolts remain functional. The edge bolts are the primary component for maintaining tight baffle gaps and the ABPA does not consider the edge bolts when calculating bypass flow. Therefore, the bypass flow condition can be considered to be bounded by the analyses in the ABPA. The momentum flux is also controlled by the baffle gaps, and no leaking assemblies or baffle gap jetting damage was noted on the fuel.

Based on the above considerations, it is reasonable to conclude that the analyses which contribute to the safe shutdown of the plant demonstrate adequate margin. Therefore, it is judged that the requirements for core coolability and safe shutdown were met, considering LOCA and seismic loads concurrent with the observed or declared 227 baffle-former bolt failures. Therefore, the safety significance of this condition has been determined to be low.